



2.0 Lateral Forces

## **Building Loads**

• Types of loads on buildings:

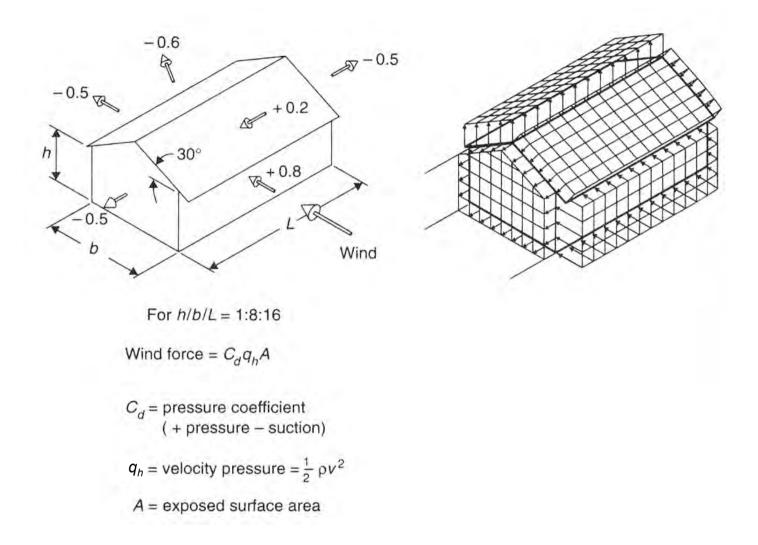
Vertical Loads (gravity)	Dead Loads: building mass (all permanent parts of a building including structure, permanent partitions, stairs, mechanical equipment and the building enclosure)
	Live Loads (also called imposed): people, non-built-in furniture, snow, water
Lateral Loads	Wind
	Earthquake (seismic)
	Sub-grade pressure (soil and/or water)
	Impact loads: blast, tsunami, avalanche

Other: Temperature (differential)

- · Types of Structure Systems and lateral resistance
  - Wall and pier structure (shear wall)
  - Post and Beam (no lateral resistance)
  - Pin connected steel frames (diagonal bracing)
  - Rigid frames both steel and reinforced concrete (stiffness achieved through rigidity of beam/column connections)
  - Three dimensional rigid forms: space frames, shell structures, etc. (over-all form does not require bracing)
  - Membrane and suspension structures (must be tied back or stiffened; ends must be laterally braced)

Loads which are constant and unchanging (like gravity) are called **static loads**. Some loads(wind, earthquake) vary in intensity and occur suddenly for an instant or over a brief time period. These are called **dynamic loads**.

Wind force



Wind loads are dynamic in nature but are applied to buildings as a static wind pressure. The applied force is a percentage of the velocity pressure,  $q_h$  dependent on the position and angle of the building's surface. Negative pressure coefficient  $C_d$  indicates suction.

The velocity pressure equation above is known as the *Bernoulli equation*. For normal atmospheric conditions, the constant p = .00256. Typical design wind loads are on the order of about 1 to 2 kN/m<sup>2</sup>.

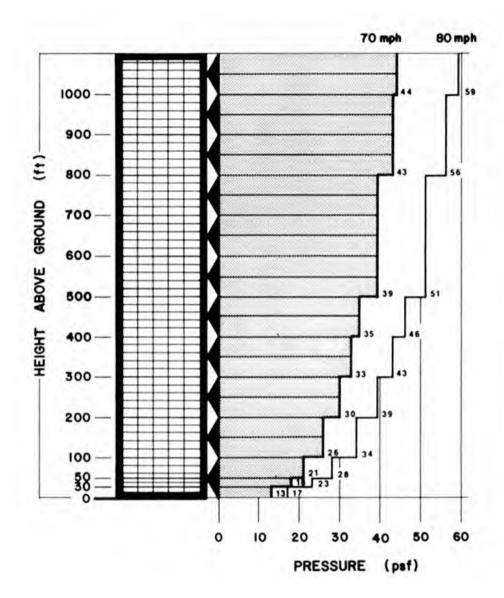
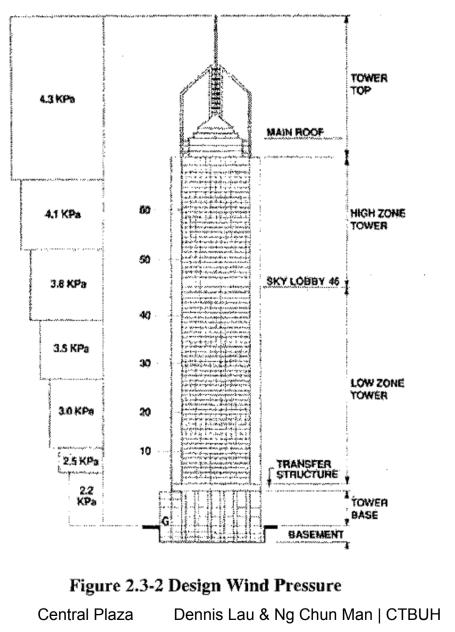


Table 1 : Design wind pressure

Height above site-ground level	Design wind pressure q <sub>z</sub> (kP <sub>a</sub> )		
$\leq 5m$	1.82		
10 m	2.01		
20 m	2.23		
30 m	2.37		
50 m	2.57		
75 m	2.73		
100 m	2.86		
150 m	3.05		
200m	3.20		
250m	3.31		
300m	3.41		
400m	3.58		
≥ 500 m	3.72		

Example of stipulated wind pressures at set heights. Building Code of New York City ca. 1990.  $60 \text{ psf} = 2.87 \text{ kN/m}^2.$  Required wind pressures at set heights for Hong Kong. Code of Practice on Wind Effects in Hong Kong 2004 http://www.bd.gov.hk/english/documents/code/windcode2004.pdf





1995 Wanchai, Hong Kong

Tallest reinforced concrete tower in Asia 1992-1996. 78 floors at 374m. Triangular floor plan. Lateral resistance to wind results in an expenditure on structure of approx. HK\$1 million for every additional 1 meter in height. This led designers to develop a very efficient floor to floor dimension of 3.6m. Design wind pressures determined by the Code of Practice on Wind Effects 1983, Building Authority Hong Kong.

Wind pressure on buildings

The wind pressure formula that determines the wind pressure acting on a surface due to a given wind speed is formulated from the Bernoulli equation (Daniel Bernoulli 1700-1782)

q (pressure in psf) = $1/2 p V^2$	where <i>p</i> is air mass density and V is the wind speed in mph

Then,  $q = 0.00256 V^2$  (for a standard atmosphere at sea level and temperature 15deg, the air density is 0.0765 lb/ft<sup>3</sup>.)

Wind speed is measured by weather stations worldwide. The maximum wind speed is determined as the fastest velocity at 30ft above ground based on a recurrence period of 50 years.

Since the velocity of the wind increases with height, the pressure on the building will vary at different heights. This variation is calculated by formula and the results given in graphic charts such as Table 1 of the Code of Practice on Wind Effects in Hong Kong 2004.

Another factor that affects wind speed is context, or the type of exposure to wind of the surrounding area. Four exposure conditions are used.

Exposure A: large, dense cities	a = 3.0	z <sub>a</sub> = 1500 ft
Exposure B: urban and suburban areas, also forested areas	a = 4.5	z <sub>a</sub> = 1200 ft
Exposure C: flat, open country and slightly rolling landscape	<i>a</i> = 7.0	$z_{a}^{"}$ = 900 ft
Exposure D: unobstructed coastal areas	<i>a</i> = 10.0	$z_{g}^{s} = 700 \text{ ft}$

The factors "a" and " $z_q$ " are used in the following exposure coefficient formula:  $K_z = 2.58 (z / z_q)^{2/a}$ 

The final consideration is the shape of the building in plan. For a typical rectangular hi-rise, the shape coefficient C<sub>p</sub>= 1.3

The full equation then for wind pressure taking into account the height above the ground (z), the exposure condition ( $K_z$ ), and the shape coefficient  $C_p$  is:

 $q = 0.00256 V^2 K_z C_p$ 

Therefore, for an exposure condition C, the wind pressure at 250ft high due to a 100mph wind speed on a rectangular bldg. is:

 $q = 0.00256 (100 \text{mph})^2 x (2.58) (250 / 900)^{2/7} (1.3) = 59.5 \text{ psf} (2.85 \text{ kN/m}^2)$ 

To convert wind pressure into kN/m<sup>2</sup>

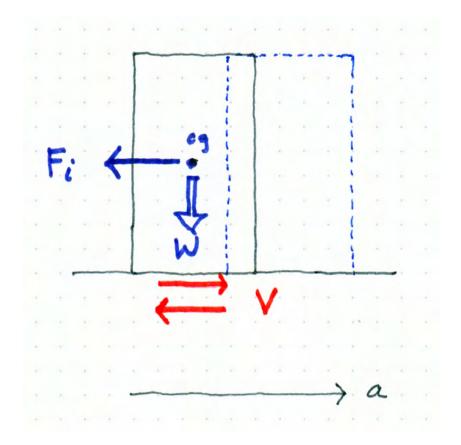
First, divide the wind speed (if given in km/hr) by 1.609 to get mph, substitute, and multiply the calculated pressure by .04788 to get kN/m<sup>2</sup>.

Note: to calculate the complex exponential (250/900)<sup>2/7</sup> it is convenient to refer to the following website: <u>http://www.analyzemath.com/Calculators 2/power calculator.html</u>

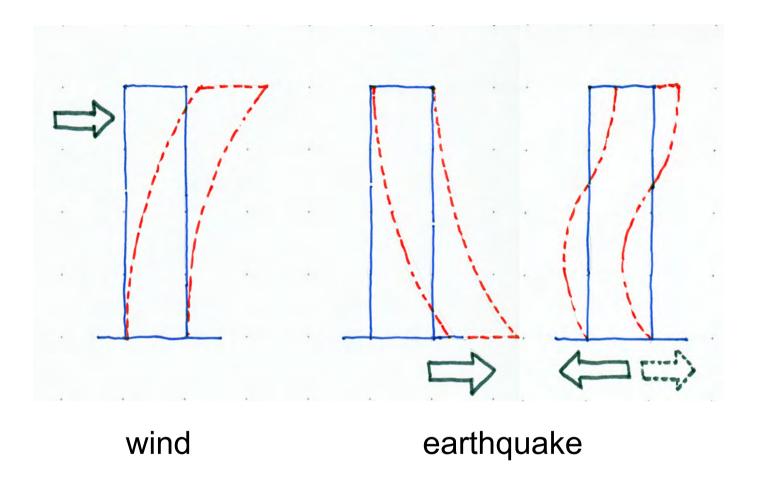
Earthquake force

Earthquake forces are the result of sudden and extreme ground movements. The ground during an earthquake can move in a complex pattern (up/down, laterally, rotating) producing dynamic movements in the structure. This phenomenon is called *ground shaking* and is the primary concern of earthquake resistant design. Other associated destructive aspects of an earthquake include:

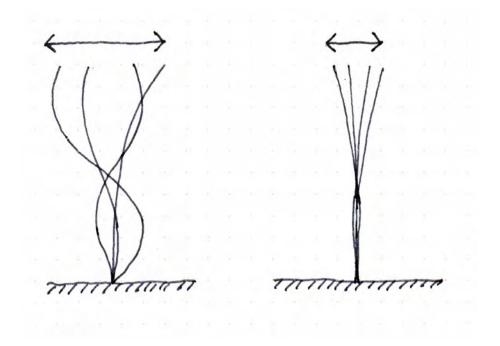
- surface fault ruptures (which may engulf a structure)
- ground failure or *subsidence* (ground becomes soft and may liquify)
- tsunami



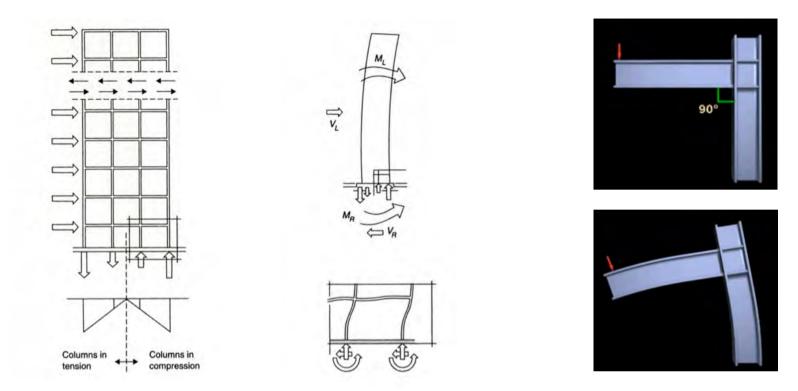
If a building were completely rigid (and weightless), the lateral movement of the ground during an earthquake (the acceleration force, a) would simply move the entire building as a unit with it. However, a building has *weight* that generates an inertial force,  $F_i$  (resistance to sudden movement) in the opposite direction. At the base of the building these opposing forces create shear (V) in the structure of the building at the ground. This is referred to as base shear.



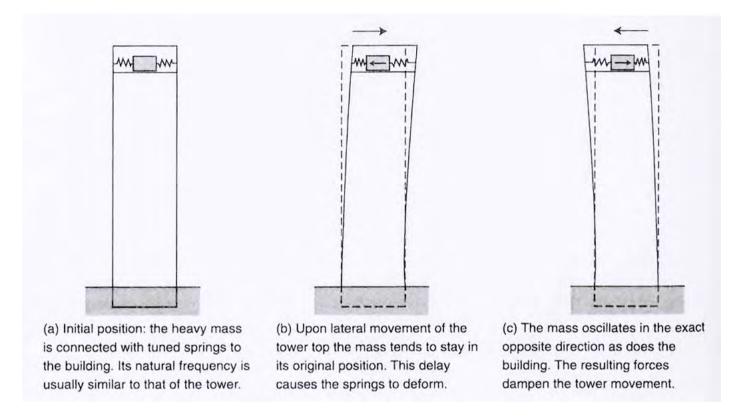
Buildings, however, are not entirely rigid. A flexible structure will have a more complex response to earthquake acceleration force. This response results in *vibratory movements* that depend on the relative stiffness of the building and its *natural period of vibration*.



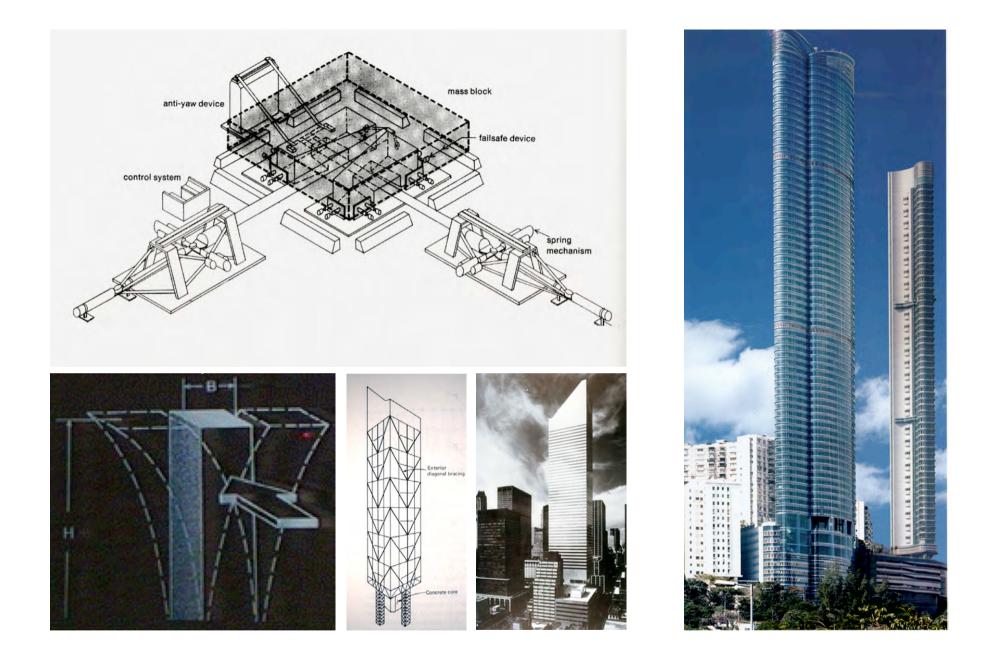
The stiffness of columns in a tall building affects the vibration of the structure. If the columns are of low stiffness, they are less able to restore the deflected structure to its original position. The top of the structure moves slowly back and forth. This is a *long natural period of vibration*. If the columns are more rigid, they provide stronger restoring forces which bring the deflected structure back to the original shape more quickly. The oscillation of the top of the structure is more rapid. The *natural period of vibration* is short.



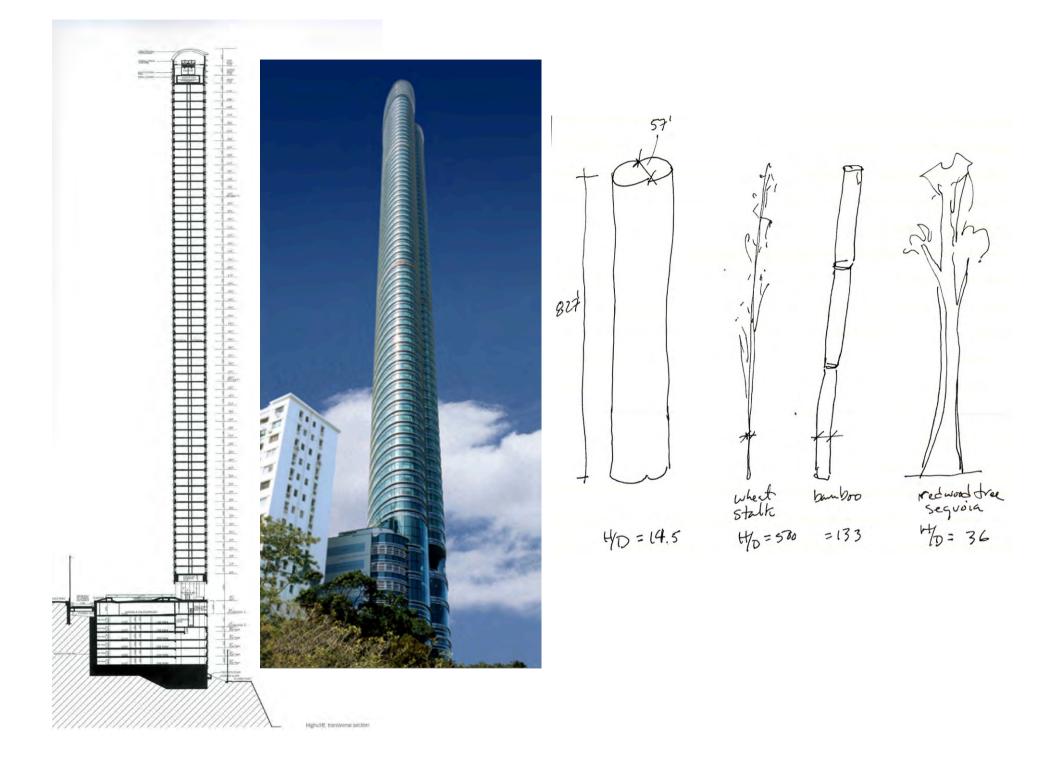
All buildings have *damping* mechanisms that absorb energy and cause the vibrational movements to come to rest. The deflection of the beams and columns in a steel frame absorbs energy and resists the vibrational movement. Other mechanisms may be more destructive, such as the cracking of partitions. As an alternative, special devices to minimize the movement caused by lateral forces have been developed. One such device is a *tuned mass damper*.



A tuned mass damper in a high-rise building. The heavy mass or pendulum swings in a controlled way to counter the swinging movement induced by dynamic loads.



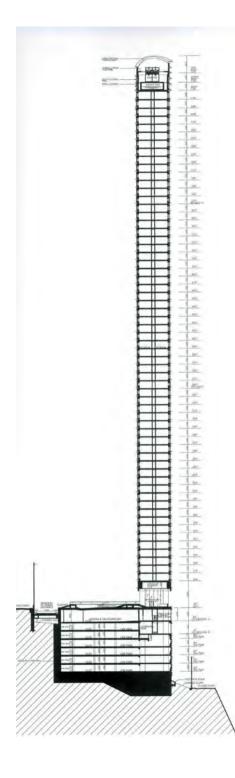
The 1977 Citicorp Tower was one of the first tall buildings to use a *tuned mass damping* device. Essentially a large concrete block. Today other types of mass damping include water tanks. The Summit and the Highcliff residential towers in Hong Kong use a specially designed water tank as a tuned mass damping device.

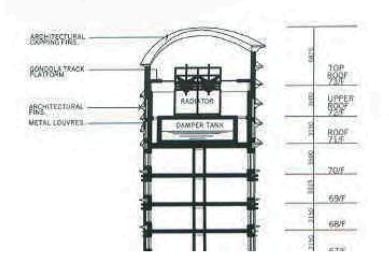


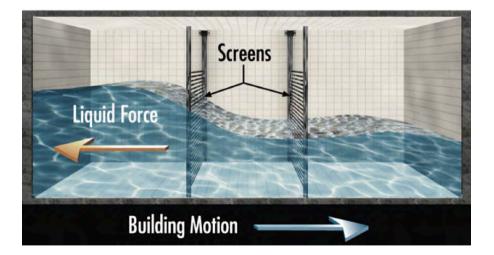












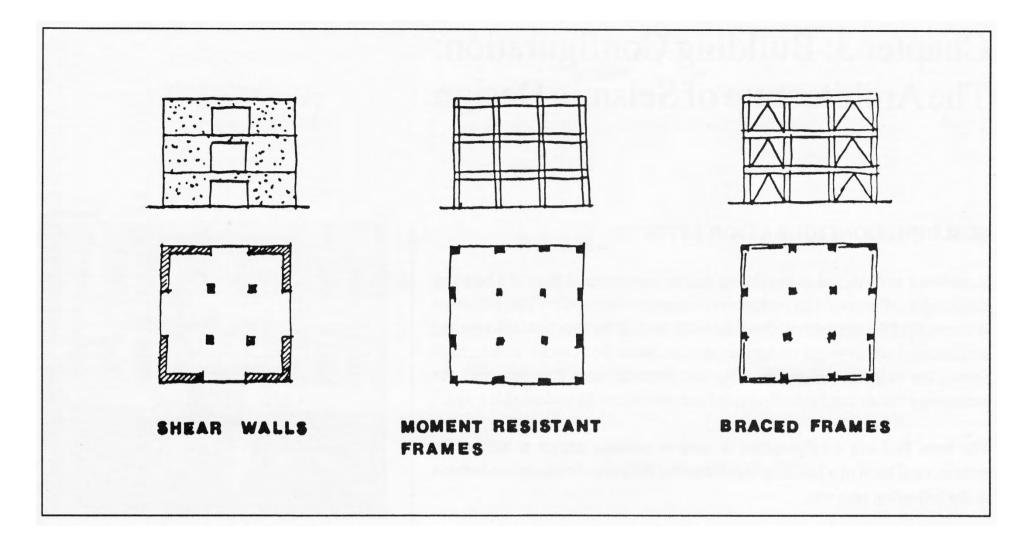
Tuned Liquid Dampener

Highelitt, transverse section

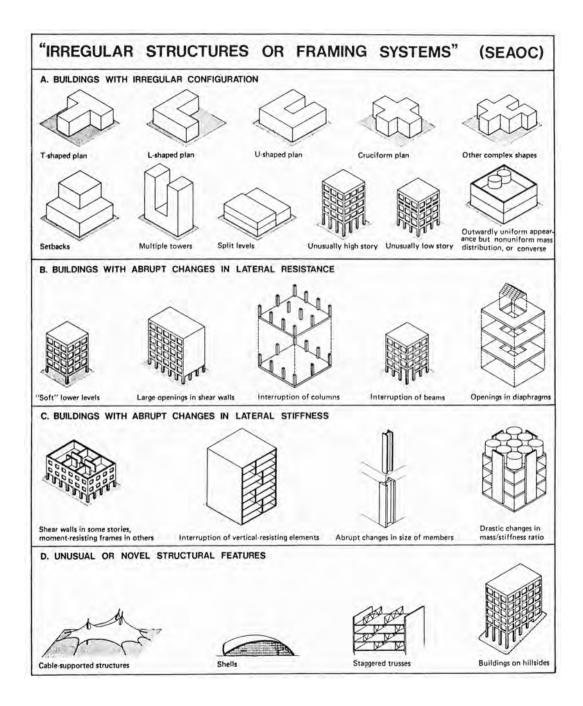
Design for earthquake force

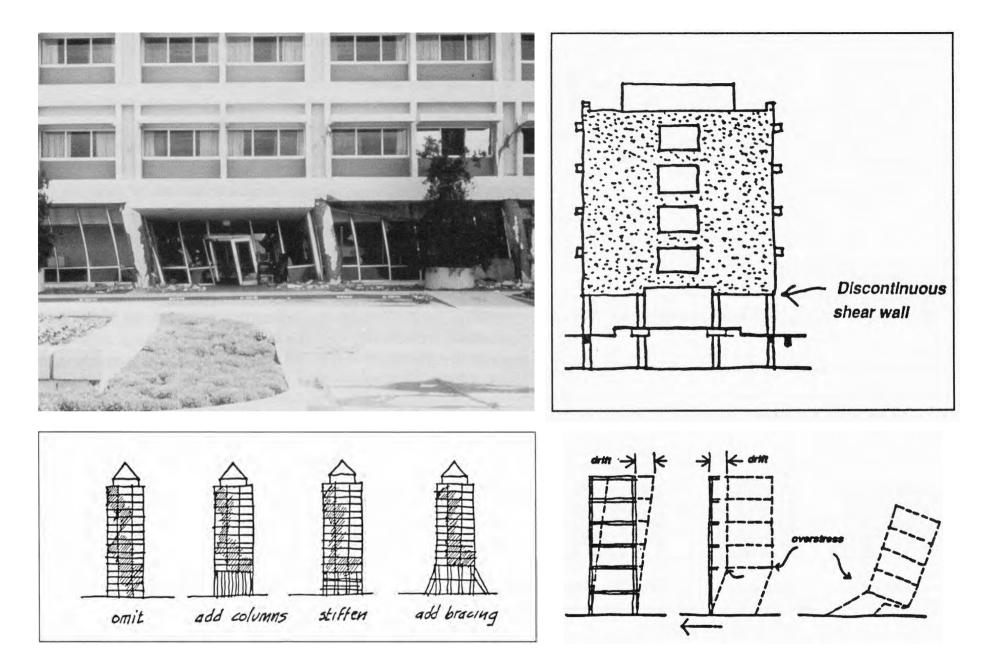
Seismic design considerations.....

- Lightweight construction (steel and wood framing) is preferred to heavy construction (concrete and masonry).
- Regular symmetrical building layout in plan (regular distribution of weight and lateral force resisting structures such as shear walls).
- Unvarying (no change) lateral force resisting elements from ground to top of building.
- Energy absorbing ductile structures (steel frame) versus rigid and brittle structure (masonry wall).
- In special cases, support elements that allow the building some movement at ground level (base isolation devices) are effective in mitigating the destructive seismic base shear forces.

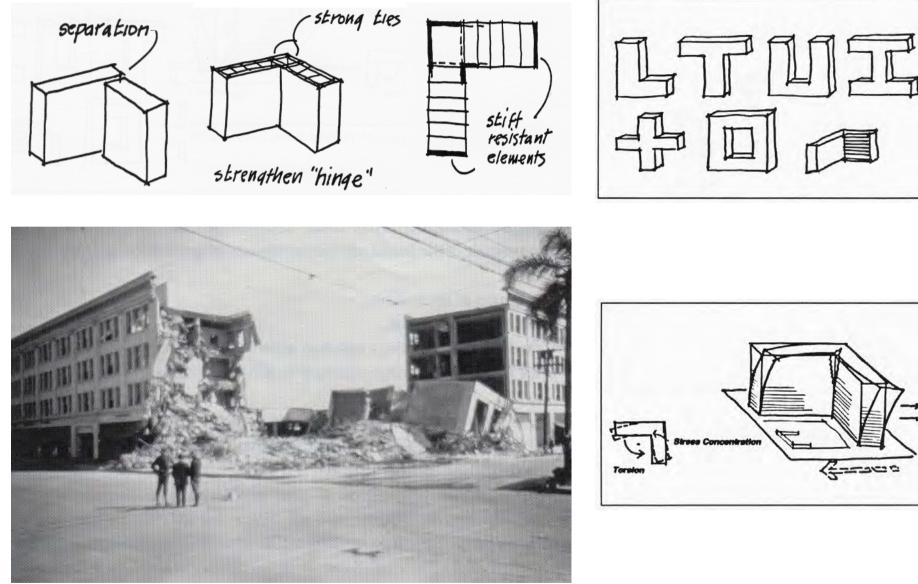


Regularity in the distribution of both mass and lateral force resisting systems is the most important design factor in achieving better earthquake resistant performance. In a building with a complex shape, different parts of the structure will react to the seismic forces unevenly, creating torsion effects.





Abrupt change in resistance is illustrated by the ground level "soft story".

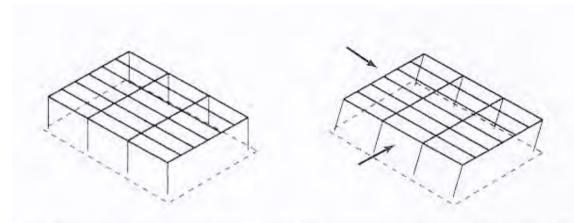


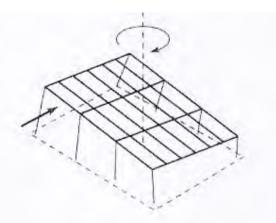
Collapse of the L-shaped San Marco Building in the 1925 Santa Barbara California earthquake.

Building shapes with inside corners and wings are susceptible to damage due to torsional forces.

Lateral force resisting systems:

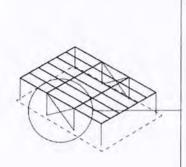
low rise structures





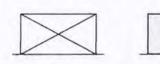
- (a) Basic structure without lateral stability devices
- (b) Major lateral deformations ("racking") due to horizontally-acting wind or earthquake loadings.
- (c) Torsional deformations.

Typical effects of laterally acting wind or earthquake forces.



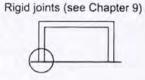
Large in-plane deformations

Vertical planes without "diaphragm action" (surfaces cannot transmit in-plane forces and deform radically)





Shear walls



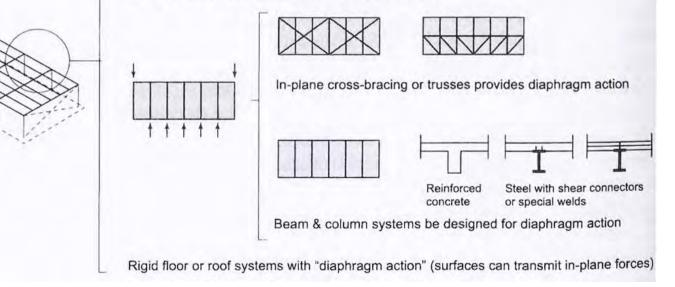
Cross-bracing or trusses 2

Rigid frame action

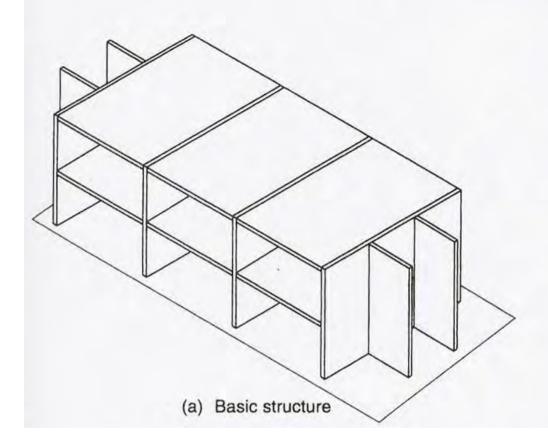
Vertical planes or wall systems with "truss", "diaphragm", or "rigid frame" action can carry in-plane horizontal forces

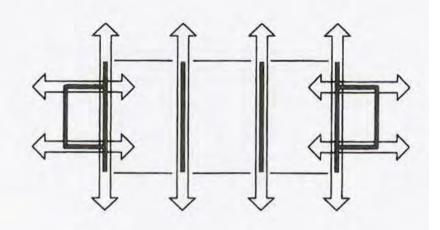


Floor or roof systems without "diaphragm action" (surfaces subjected to in-plane forces deform radically and cannot transmit in-plane forces)



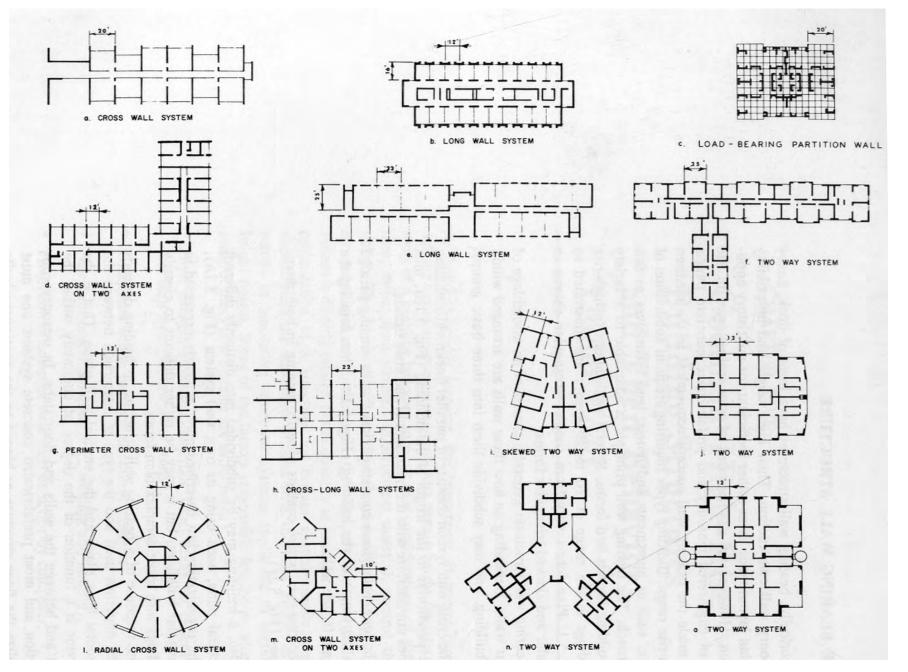
Illustrations from Structures 6th Ed. by Daniel L. Schodek and Martin Bechthold





(b) When walls are used to achieve lateral stability in buildings, they should be organized along the short dimension of the building. Stability in the longitudinal direction is often achieved through transverse walls (stairway cores, etc.).

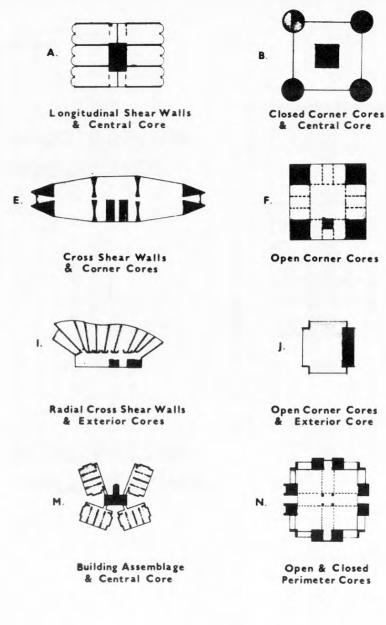
Structural bearing wall systems as lateral force resisting shear planes (concrete masonry must be reinforced).

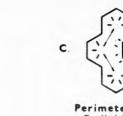


1 Bearing wall system

Three types: cross wall system, long wall system and two-way system.

Illustrations from Horizontal-Span Building Structures. Wolfgang Schueller

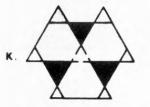




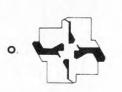
Perimeter Walls Radial Core Walls & Central Core



Core Assemblage



**Triangular Perimeter Cores** 



**Open Central Core** - Shear Wall Comb.

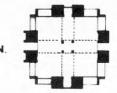


Facade Walls & Off - Center Cores

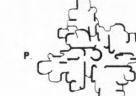


Cross Shear Walls & Central Cores

**Open Corner Cores** & Exterior Core



Open & Closed Perimeter Cores



Curved Shear Walls Forming Open Core Assemblage



## 2 Wall-core system

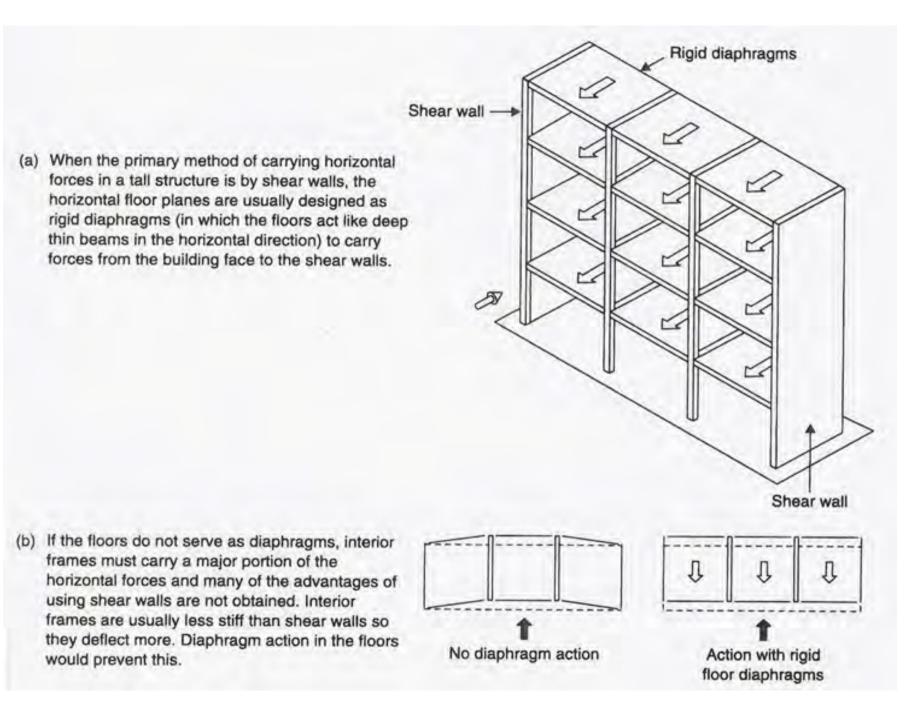
Lateral force resistance is shared between load bearing wall structure and service core structures.

Illustrations from Horizontal-Span Building Structures. Wolfgang Schueller

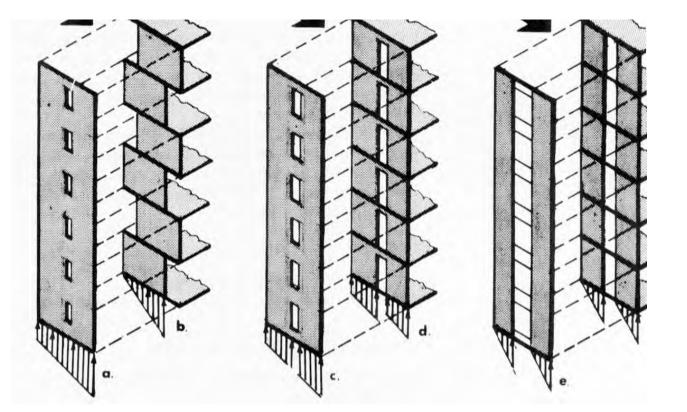


Curved Shear Walls





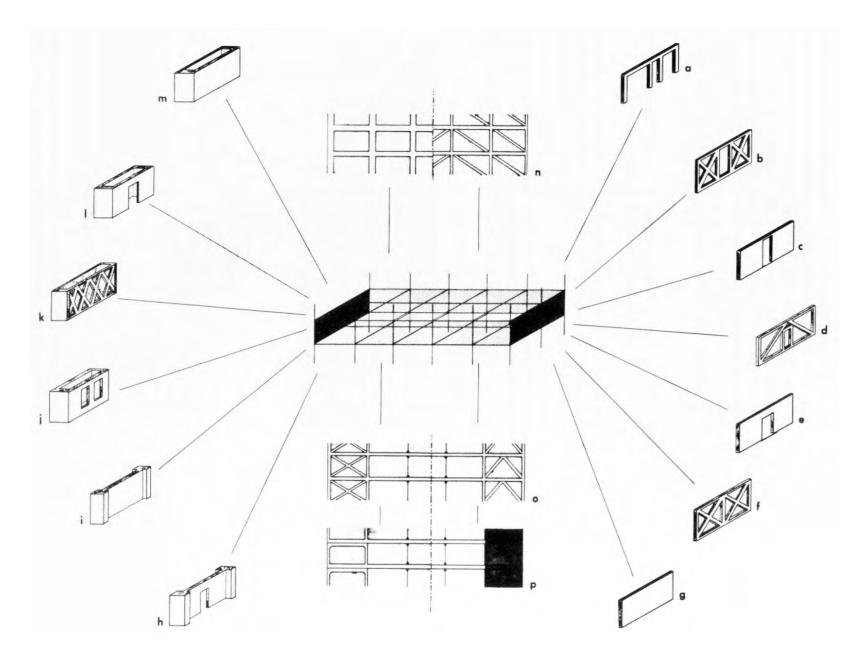




## Shear walls.

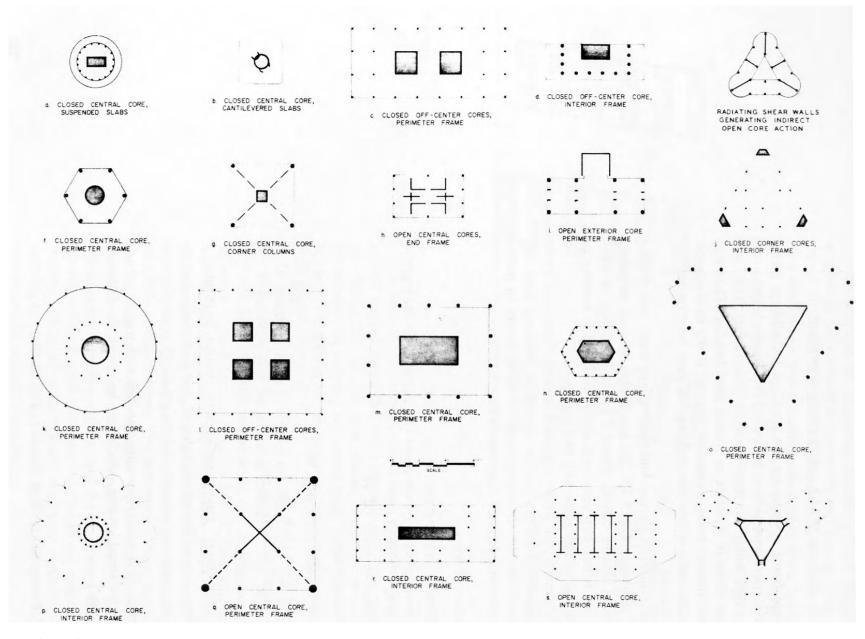
Openings in shear walls can reduce the effectiveness of lateral force resistance.

In fig. a the openings in the wall are small and do not significantly affect performance, The wall acts as a single panel to resist overturning. In fig. e the opening in the wall is continuous and causes the end-wall to act as two independent shear walls with each resisting half the lateral force. However, the total amount of lateral force the two walls can resist is much less than the amount that can be resisted by the nearly solid shear wall as shown in fig. a.



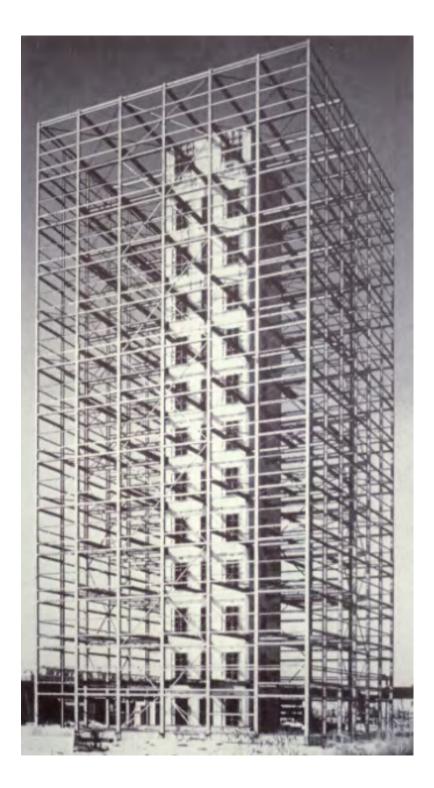
Examples of different configurations of shear resisting panels.

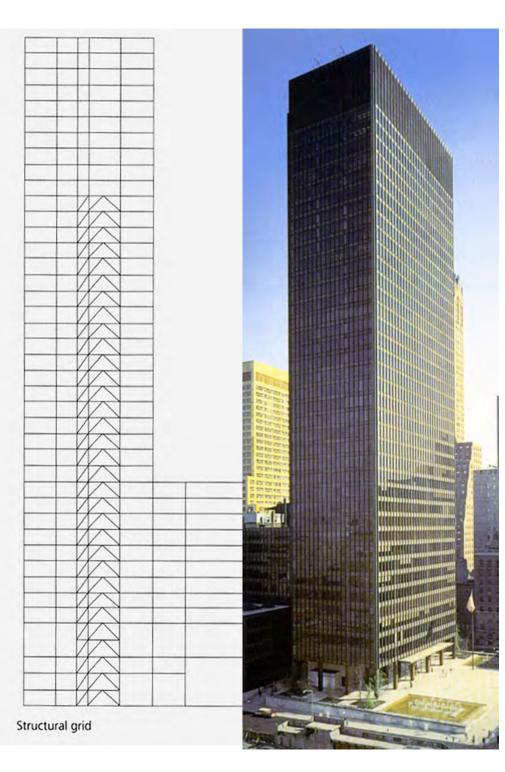
Illustrations from Horizontal-Span Building Structures. Wolfgang Schueller

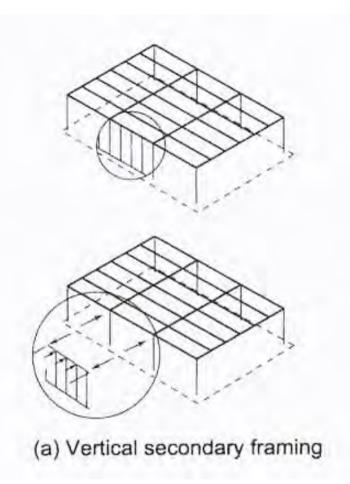


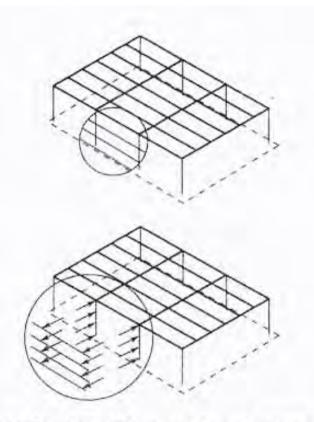
3 Core-frame system The structural core acts as a shear wall. The frame may contribute also to the lateral stiffness, depending on the type of frame. A hinged frame contributes nothing and only carries vertical loads. A rigid frame contributes significantly.

Illustrations from Horizontal-Span Building Structures. Wolfgang Schueller



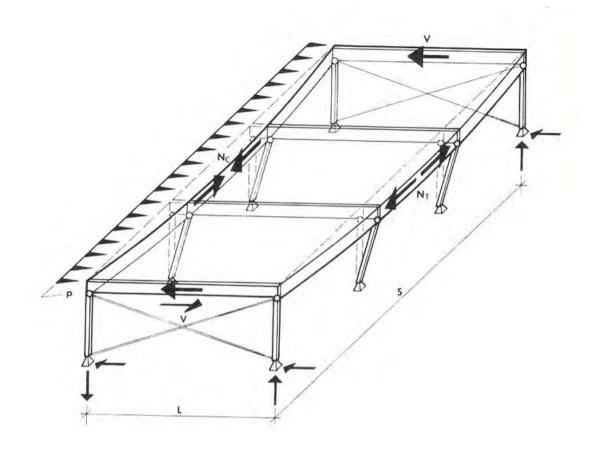




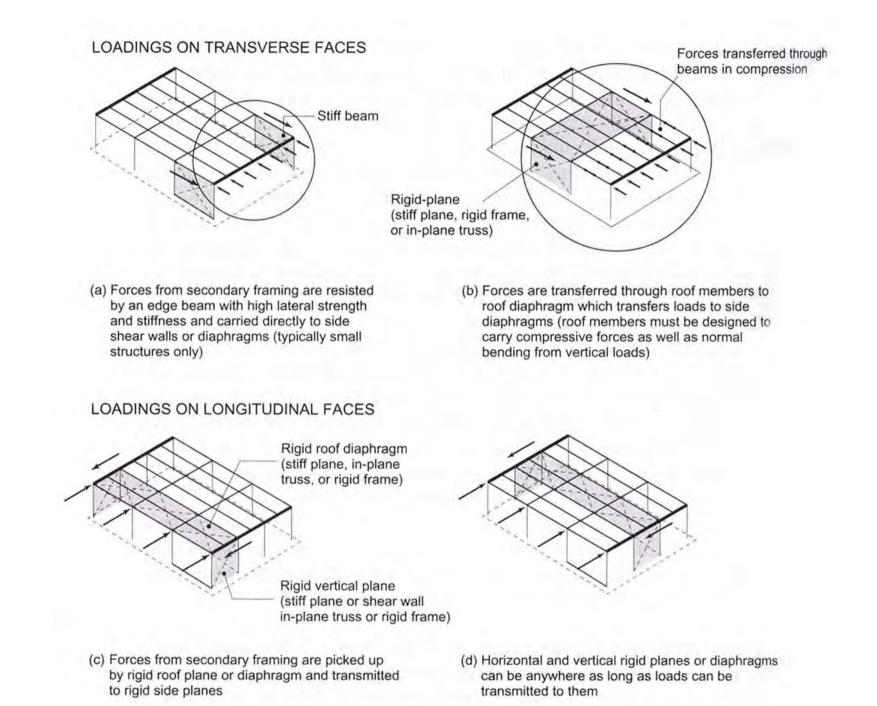


(b) Horizontal secondary framing

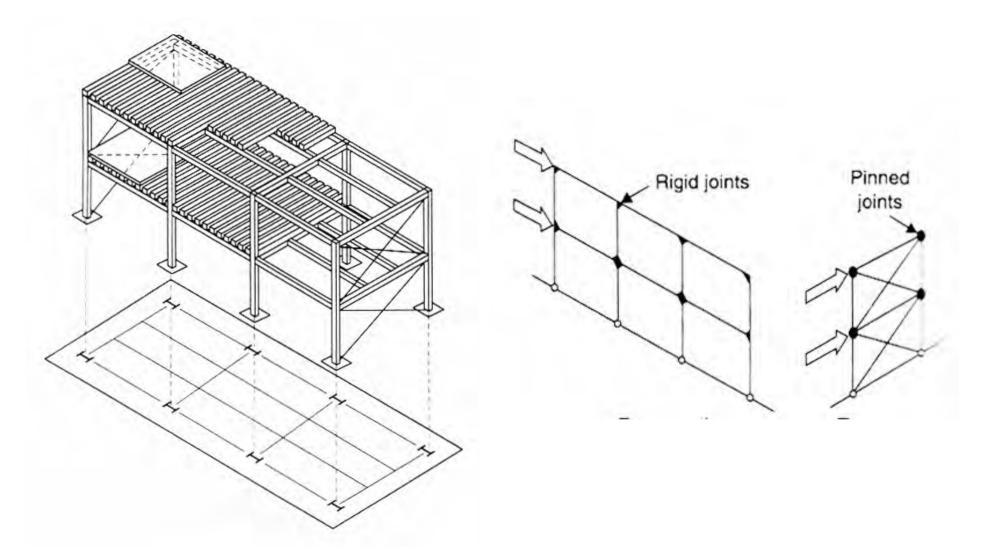
The surfaces between structural columns in a frame structure have secondary framing elements that transfer the wind force to either the ground and roof beams: (a) vertical secondary framing (wind columns) or to the columns: (b) horizontal secondary framing (wind girts).



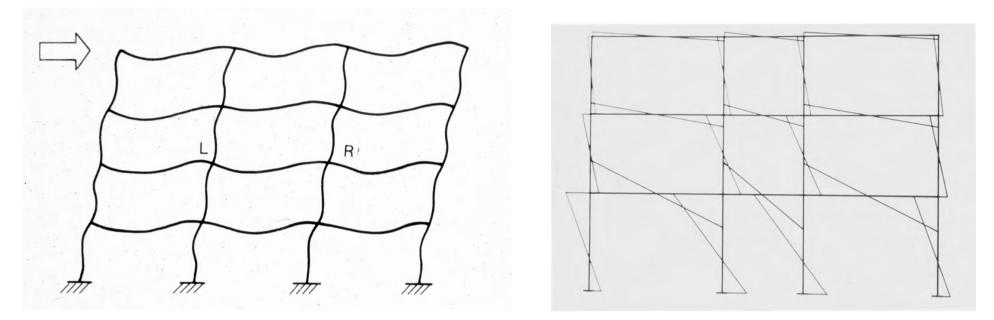
This diagram shows a one-story frame with diagonal bracing in the end bay frames but no stiffening of the two interior frames. Wind loads transmitted from the envelope to the roof beam (by secondary framing columns not shown) cause the interior frames to 'rack' distorting the roof plane. The roof beams on the edges of the long sides have no stiffness to resist the lateral forces applied along their length. Consequently they develop axial forces ( $N_c$  and  $N_T$ ) analogous to the top and bottom chords in a frame laying on its side.



Illustrations from Structures 6th Ed. by Daniel L. Schodek and Martin Bechthold



The short dimension of frame systems is the most critical. Efficient lateral load resisting mechanisms such as cross bracing with tension members is often used. In the long direction frame action is often employed upon for lateral resistance. This requires the frame elements (columns and beams) to be rigidly connected at the joints.



Distribution of bending moments in a portal frame under lateral loading.

Note the mid-span and mid-floor height locations of inflection points. These are points on the moment diagram where the curvature changes and hence the moment force changes from sign (e.g. from positive to negative bending moment). At this point the moment is zero.



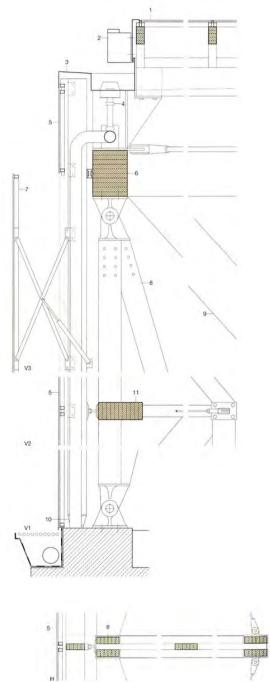
Vocational Training Center

Jourda & Perraudin, arch.

Herne-Sodingen, Germany

1998

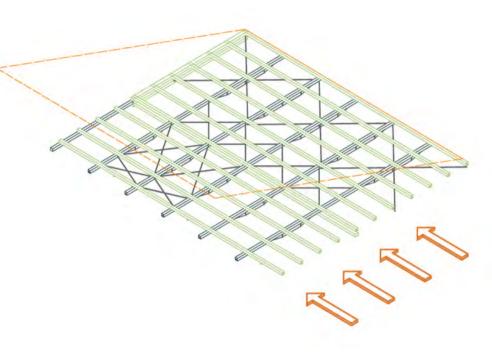




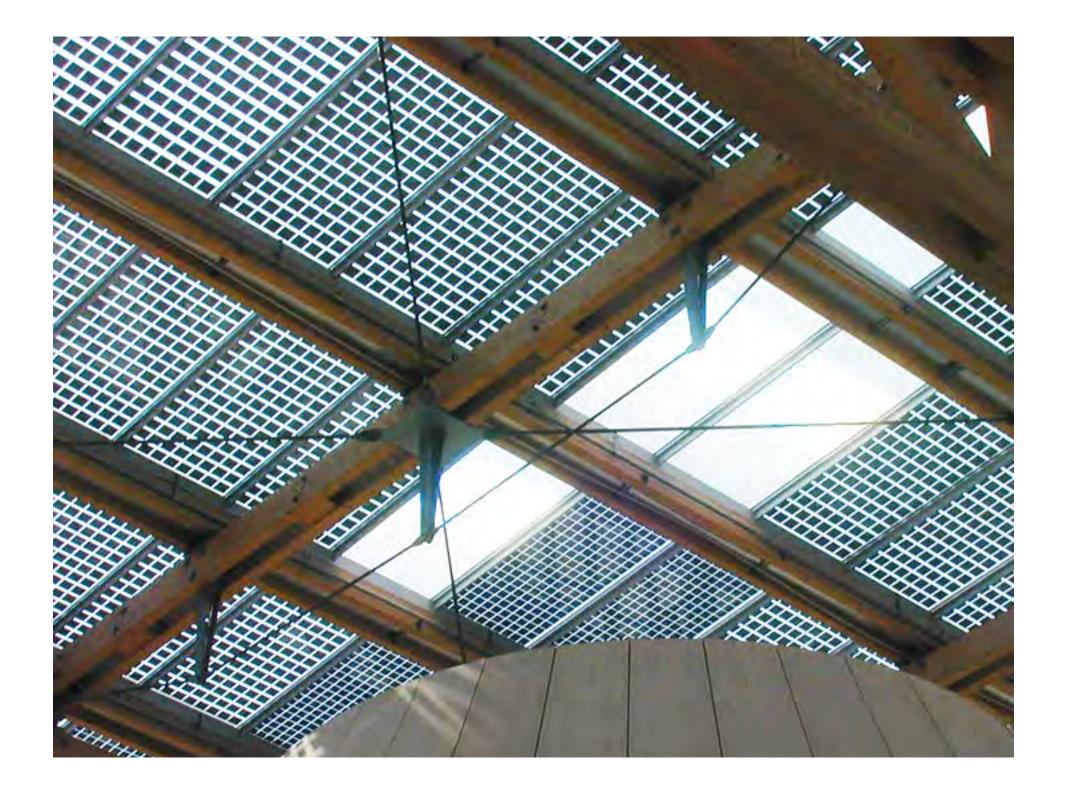


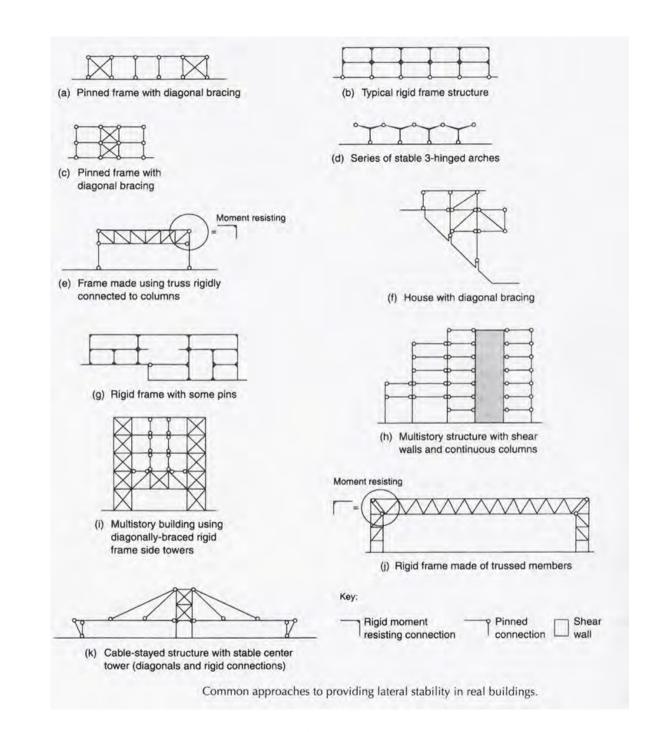






Diagonal (cross bracing) in the roof plane of the Vocational Training Center resists distortion (dashed line) under the lateral loading along its edge.





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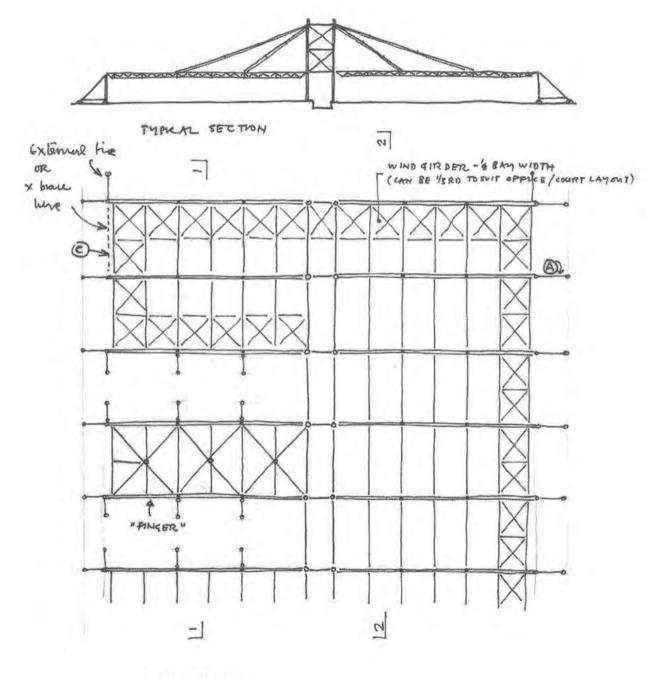


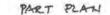
INMOS Microprocessor Factory

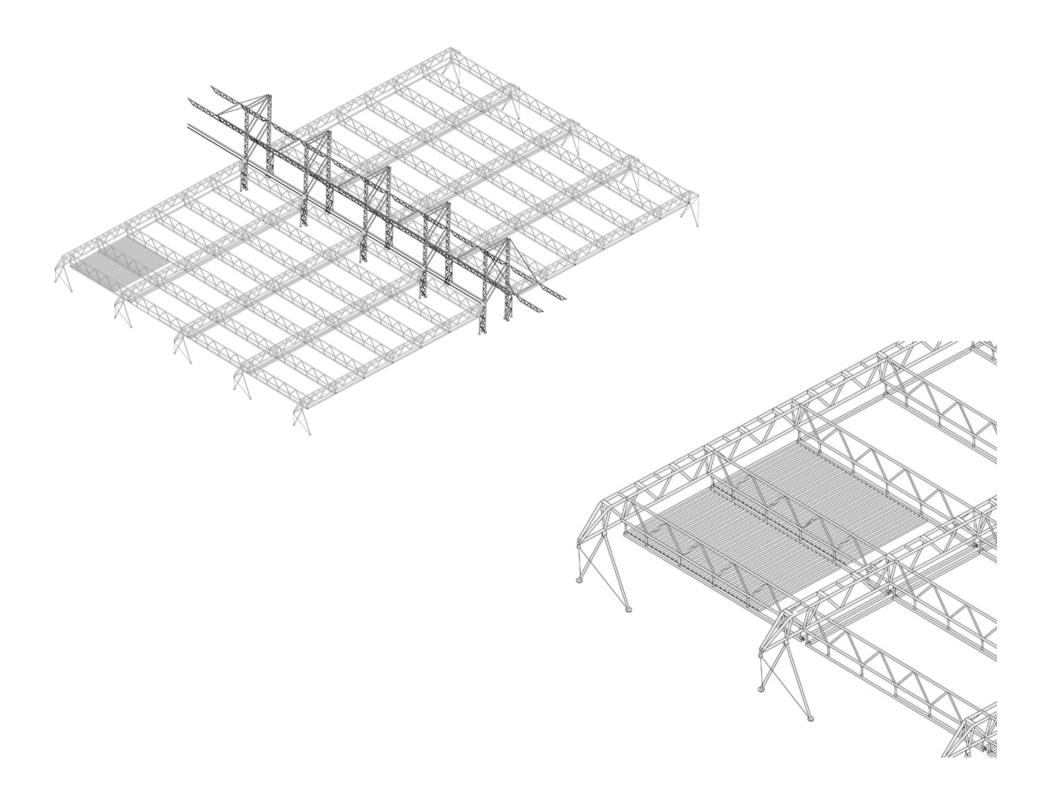
Richard Rogers Partnership / Anthony Hunt, Engr.

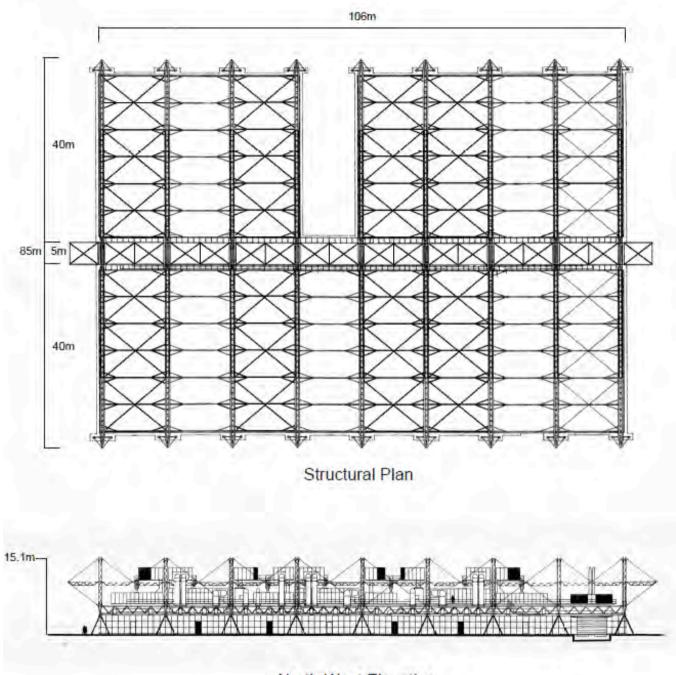
Newport, UK ca.

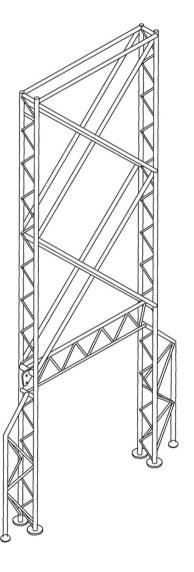
1982



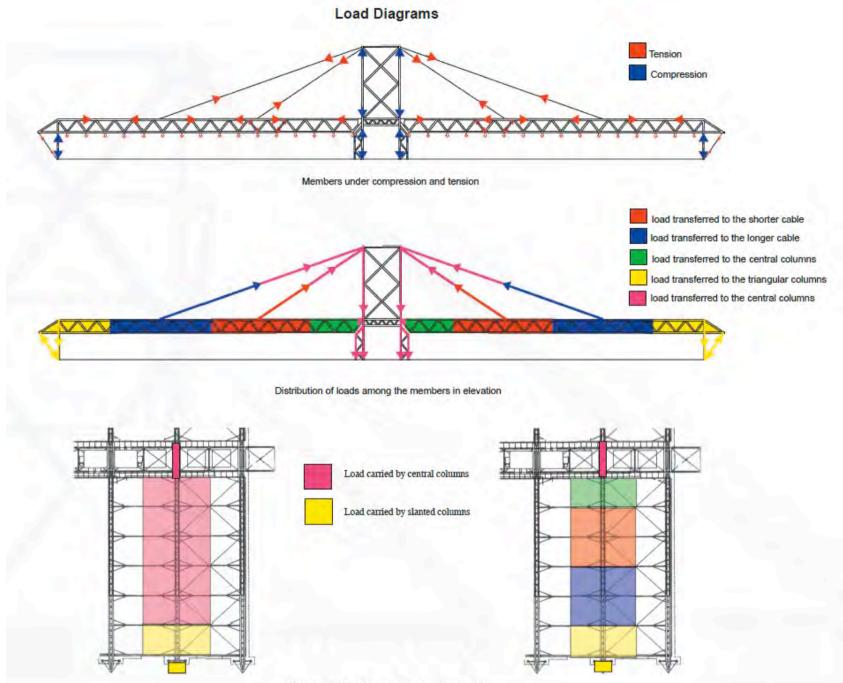




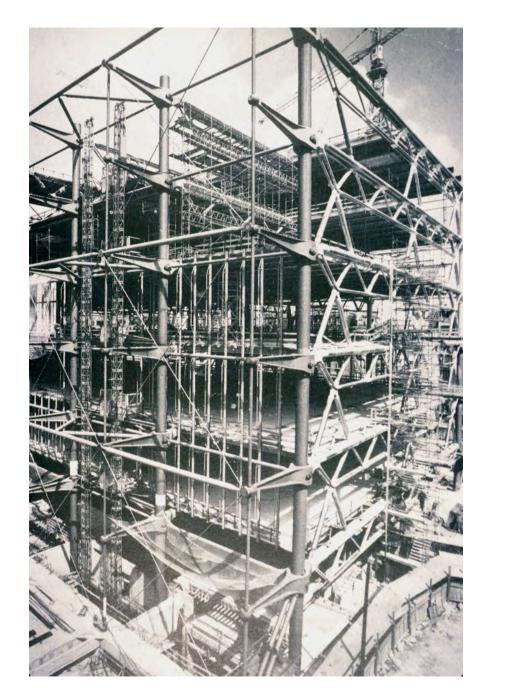


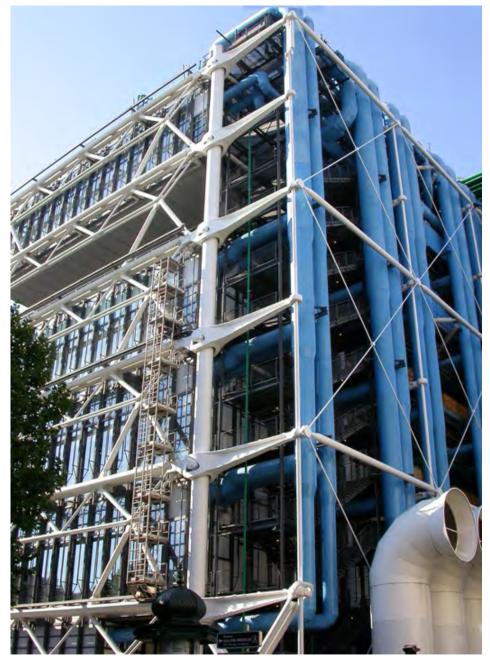


North-West Elevation



Distribution of loads among the members in plan

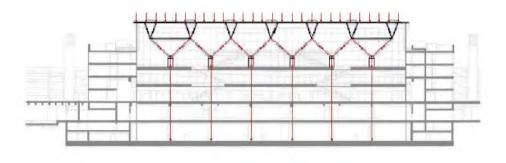




Centre Pompidou. Stiff compress struts connecting trusses together at their ends and mid-points to form a braced shear wall. On the long sides the crossed tension rods keep the frames from racking sideways.



Maintenance building at Fiumicino Airport, Rome Italy. Ricardo Morandi ca. 1960 Fuhlsbuttel Air Terminal, Hamburg Germany Von Gerken, Marg and Partners 1993



Slanted columns. Pairs of slanted columns connected across the top with a continuous beam forms a stiff, lateral force resisting structure similar to a braced frame.



Bodegas Protos

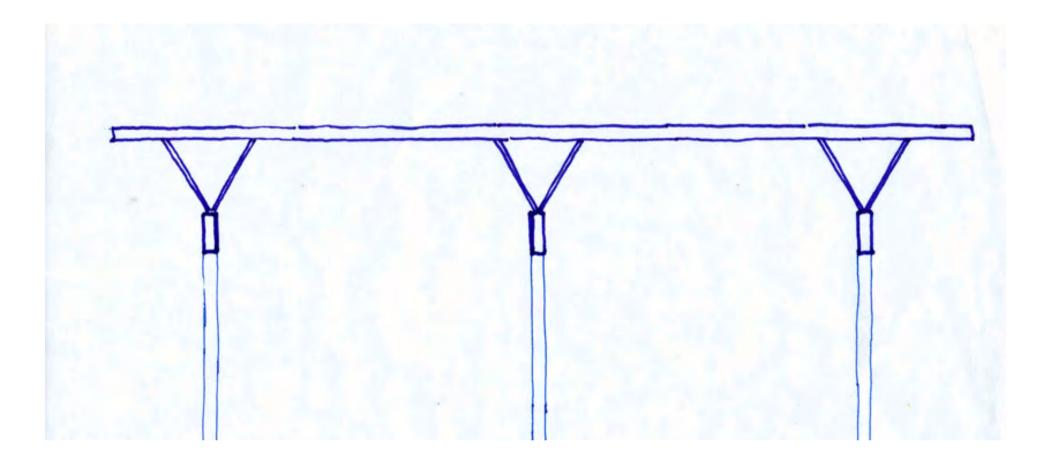
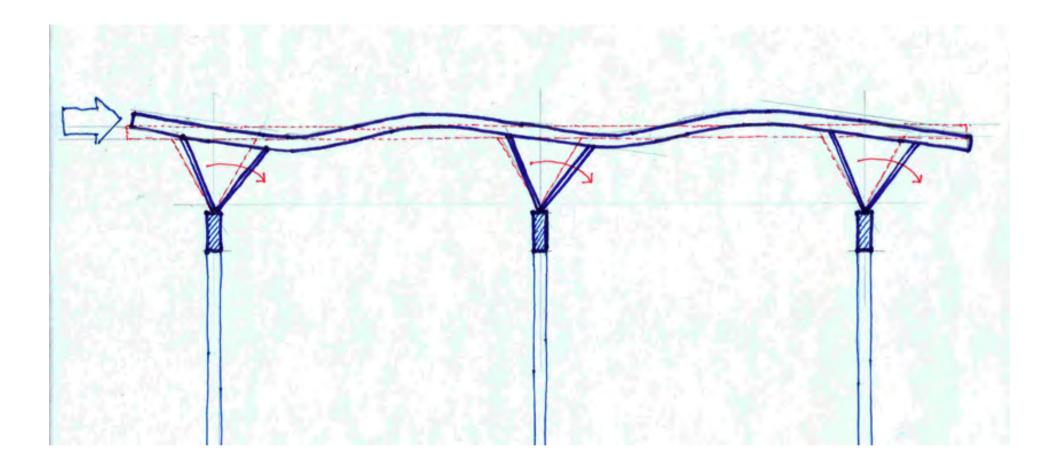
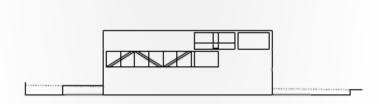


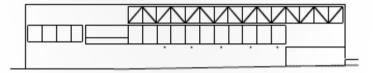
Diagram of roof beam framing structure. Slanted steel struts support the roof beams above the arches. The diagonal struts are pin-connected to the beams, but the stable triangular configuration creates a lateral force resisting mechanism.



Lateral forces acting from the left side will cause the triangular strut configuration to rotate clockwise. This rotation is resisted by the stiffness of the beams which cannot bend as shown to accommodate the deflected shape.



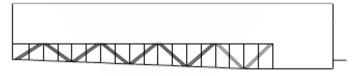
Ansicht Nord → North elevation



Ansicht West → West elevation



Ansicht Süd -> South elevation

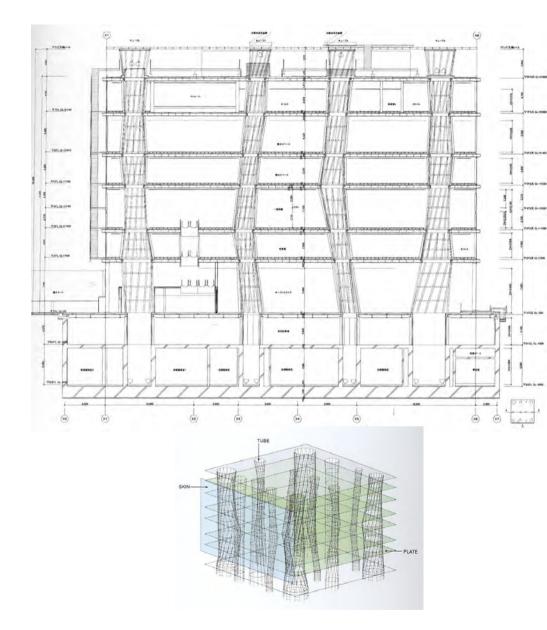








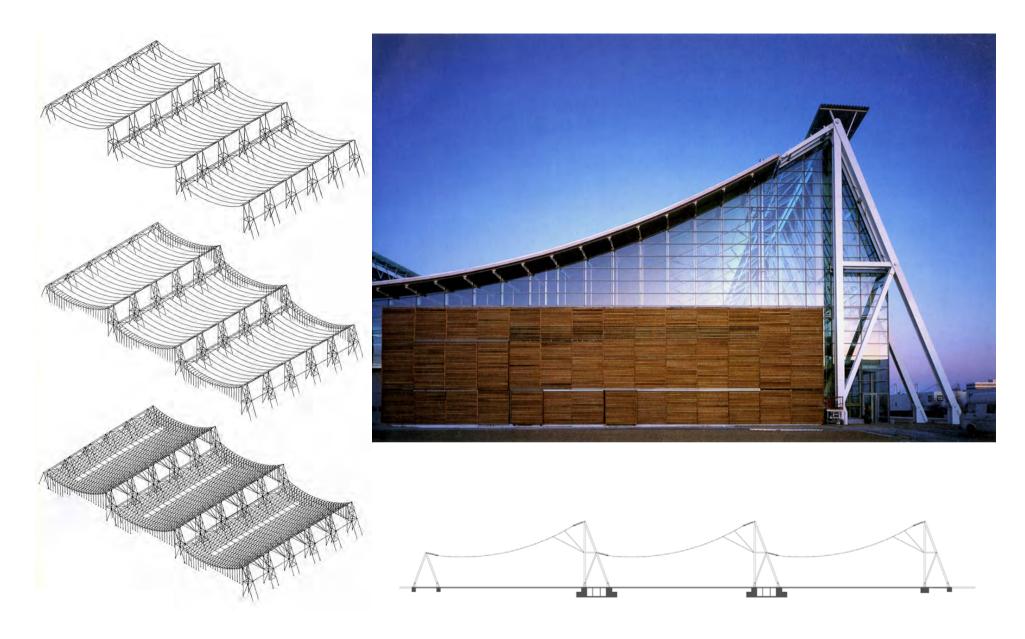
Steel trusses at various levels serve both as horizontal span structure and lateral force resisting elements.



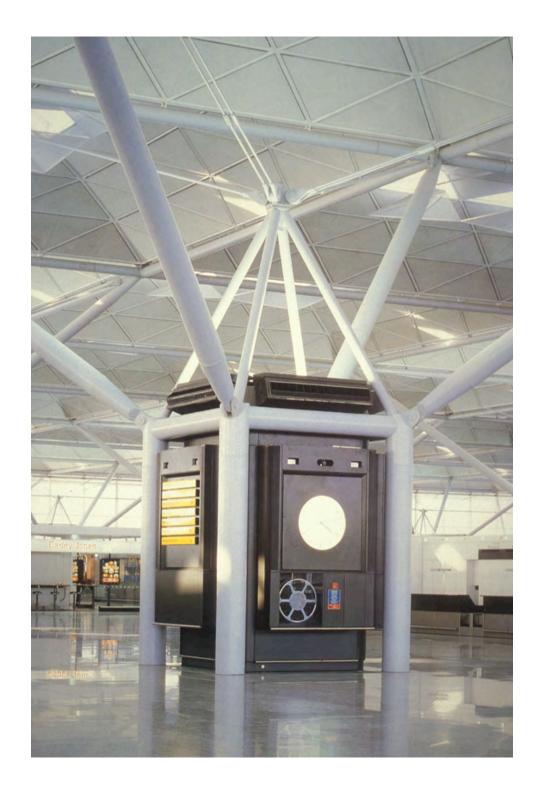
Lateral force system: stiff core-columns acting like "shear walls"



Sendai Mediatheque Toyo Ito & Associates 2000

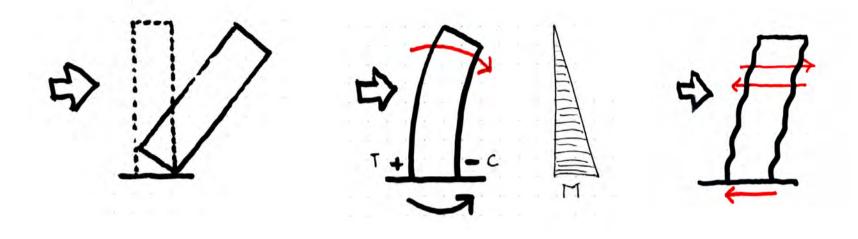


Lateral force system: braced columns acting like "shear walls". Hall 26 Thomas Herzog Hanover Expo 2000





Lateral forces on hi-rise structures

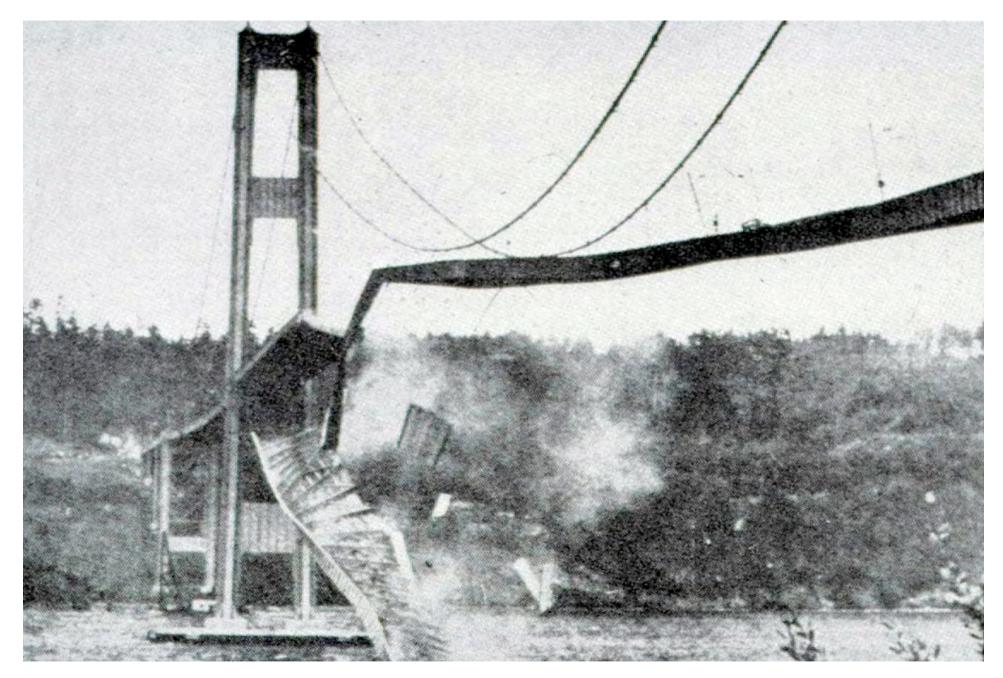


overturning

bending

shear racking

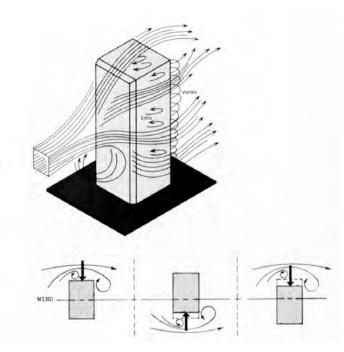
Effects of lateral forces on a tall building.

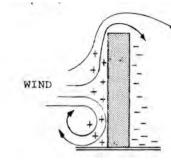


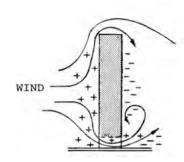
Tacoma Narrows Bridge (collapsed under moderately strong winds in 1940)

Washington State, USA

The Tacoma Narrows Bridge collapse led to research into the effects of wind induced resonating forces on structures. This led to fundamental changes in the design approach to the structures with respect to the stiffness of the structure/building as well as its fundamental period of oscillation or resonance.

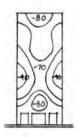






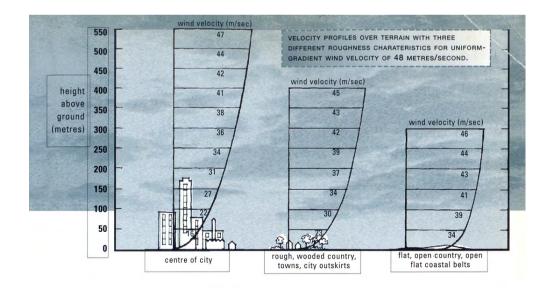




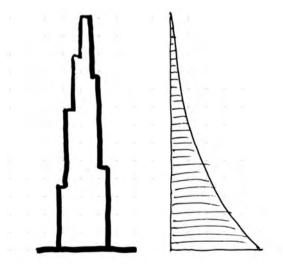


Wind forces on a tall building.

Example of variation of wind pressures as measured by a research study at MIT.



Wind profiles for three different ground conditions.

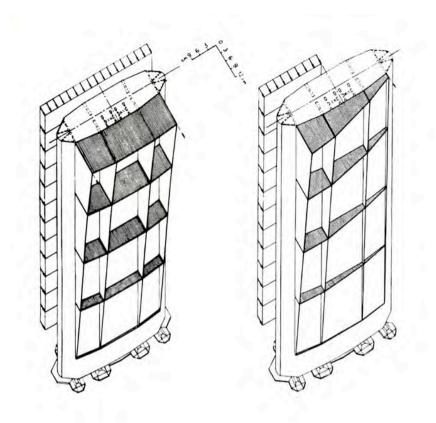


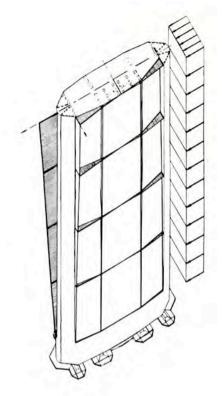
Set backs on a tall building reduces the surface area exposed to wind at the top where wind force is greatest.



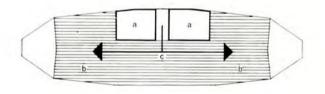
Wind induced sway of tall buildings.

As wind hits the surface of a tall building it will wrap around the side of the structure creating wind currents called "eddies" that create negative pressures. The wind fluctuates from side to side of the tall building and this constant fluctuation will cause the building to deflect laterally. If the frequency of the changing pressure from side to side matches the natural resonance frequency of the tower, it will be magnified and deflections will increase dramatically. To counter this effect it has been found that the tapered shape of a tower as well as certain asymmetries in the profile will disrupt the wind currents and counter the effect of sway. Also large openings in a tower, especially near the top, will have a similar effect.

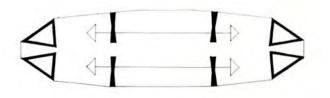




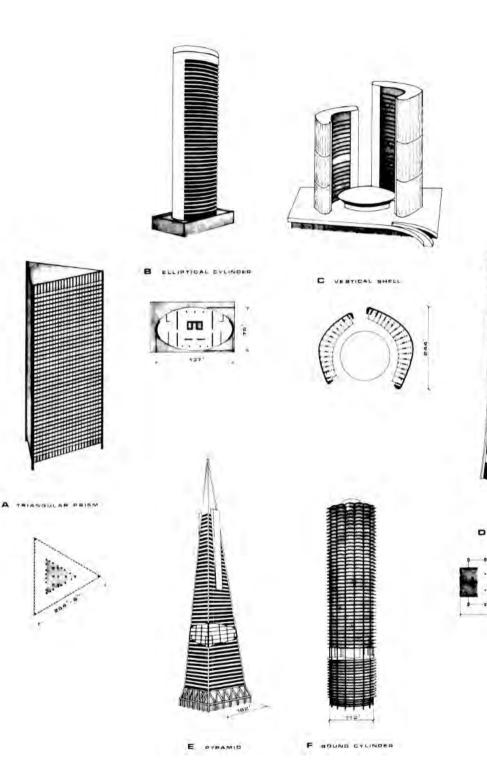




Pirelli Headquarters TowerMilan, ItalyGio Ponti with P. L. Nervica. 1963



Wind tunnel tests measured the deflection of the Pirelli tower and demonstrated the torsional deflection resulting from the asymmetric placement of the cores.



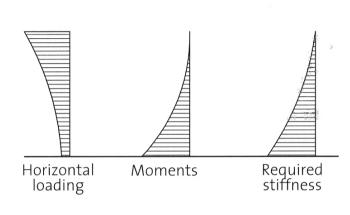
TARERED FORM

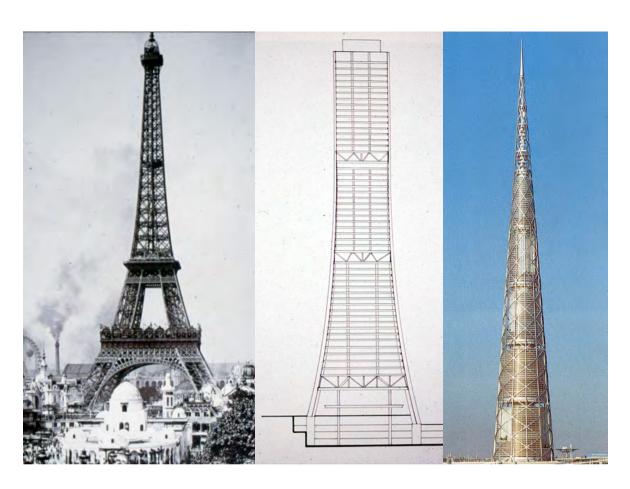
TITITI

Tall buildings with efficient shapes.

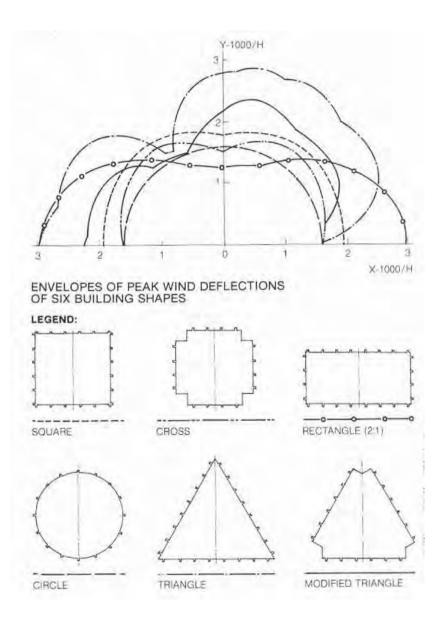
A rounded shape in plan allows wind to flow more easily around a tall building. Building Codes allow the wind pressure for octagonal and hexagonal shapes to be reduced 20% while circular and elliptical shapes may be reduced by 40%.

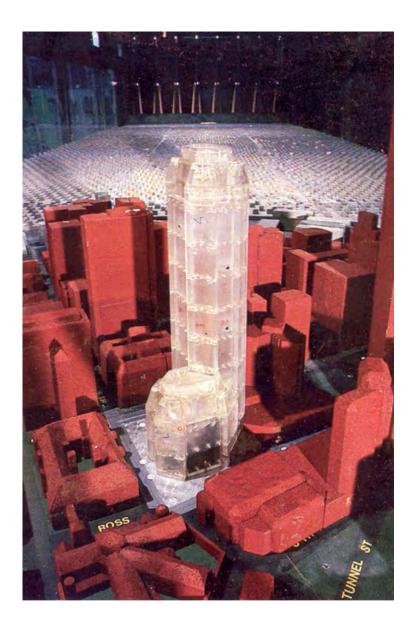
The tapering of a building as it rises effects a large reduction in wind loads and therefore drift. At higher elevations where wind speeds are high, there is less building surface providing resistance to the wind, thereby lessening the amount of wind force on the structure.





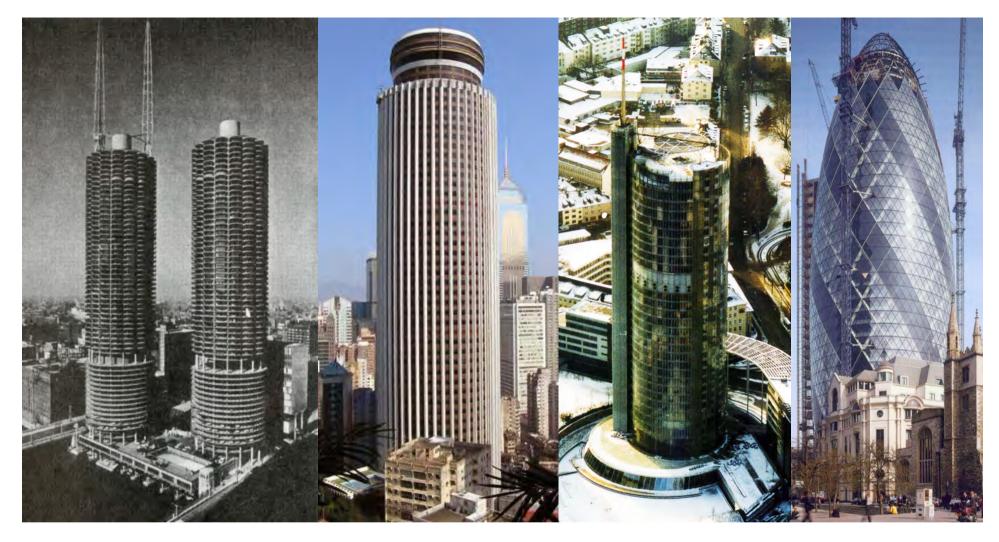
The profile of the tall building is shaped to reflect the bending moment diagram. The wider base provides a larger resisting moment to overturning without a corresponding increase in the column stress.



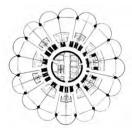


Influence of plan configuration on the amount of wind pressure on a tall building.

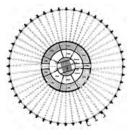
1967 wind study in conjunction with the design of the U.S. Steel Building in Pittsburg to determine variations in wind pressure on different tall building plan configurations. Besides demonstrating the advantage of circular over square or rectangular shapes, the study offered a way to calculate the effect on wind pressure of slight changes in the building profile.



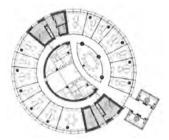
Marina City 1962



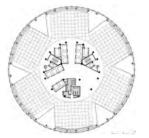
Hopewell Centre 1980

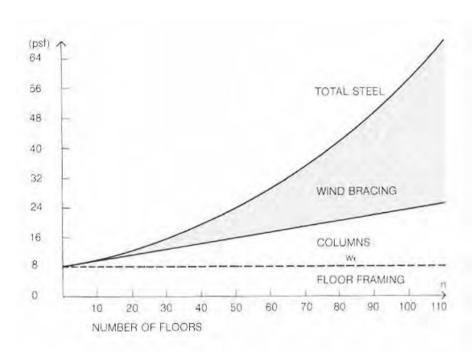


## RWE Headquarters 1996



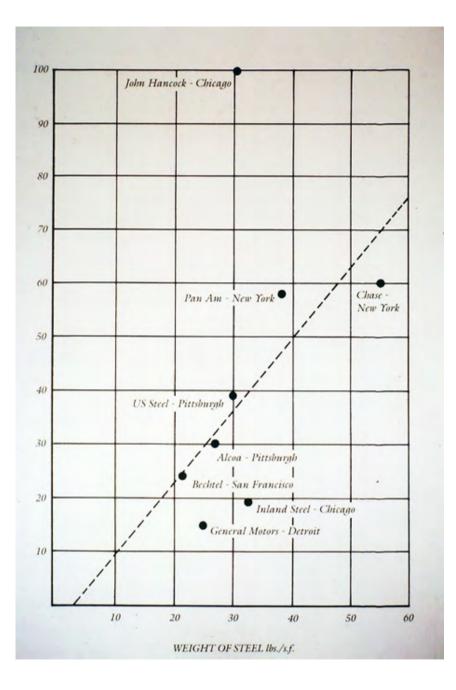
## Swiss Re Tower 2003

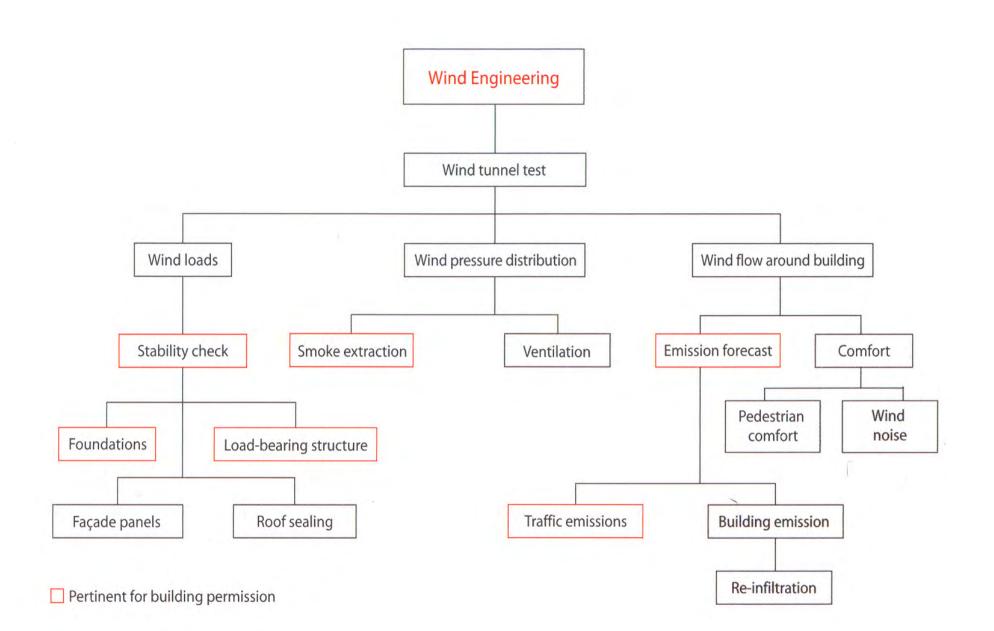




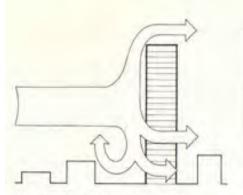
Comparison of proportional weight of steel in a steel frame building with regard to building height.

At about 50 stories (200m) the weight of steel required in the structure designed to resist the lateral loads (wind bracing) is approximately equal to the weight of steel for the vertical load bearing structure (columns) and also the steel required for the horizontal structure (floor framing). The amount of steel in the floor framing is constant and depends on the span between columns. In a typical steel frame with a span of 8-10m the weight is approximately 8 psf (383 N/m<sup>2</sup> or Pa).

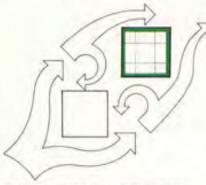




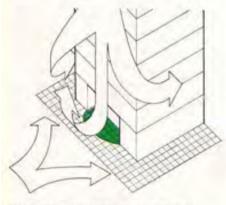
Schematic presentation of areas covered by wind engineering



A BUILDING SIGNIFICANTLY TALLER THAN ITS SURPOUNDINGS CAN EXPERENCE HIGH WIND LOADS AND CONCENTRATE PEDESTRIAN LEVEL WINDS

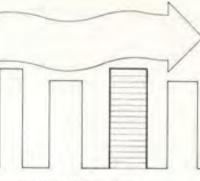


ADJACENT BUILDING PLACEMENT MAY PROTECT FROM HIGH WINDS REDUCING WIND LOADS AND PEDESTRIAN LEVEL WINDS

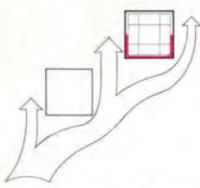


RECESSED ENTRY PROVIDES LOW WINDS AT DOOR LOCATIONS

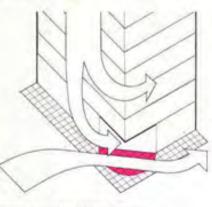
WIND EFFECTS ON TALL BUILDINGS



A BUILDING OF SIMILAR HEIGHT TO ITS SURROUNDINGS MAY BE PROTECTED FROM LARGE WIND LOADS AND CONCENTRATED PEDESTRIAN WINDS

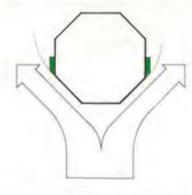


ADJACENT BUILDING PLACEMENT MAY DEFLECT WIND RESULTING IN HIGHER WIND LOADS AND PEDESTRIAN LEVEL WINDS

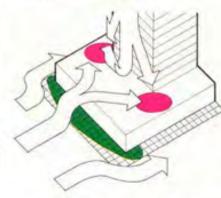


CORNER ENTRY MAY ACCENTUATE WIND CONCENTRATION AT BUILDING CORNER

A TALL BUILDING CONCENTRATES WIND AT ITS BASE

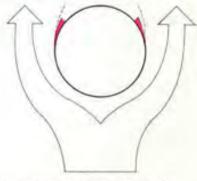


MULTI-SIDED BUILDINGS MAY NOT PERMIT FULL DEVELOPMENT OF LOCAL PRESSURES, FRAME LOADS, OF PEDESTRIAN LEVEL WINDS

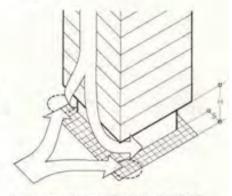


A LOW PEDESTAL BUILDING CONCENTRATES WIND ON THE ROOF, NOT AT THE BASE

OPENINGS THROUGH & BUILDING AT THE BASE MAY INDUCE HIGH VELOCITIES IN THE OPENING



CIRCULAR BUILDINGS MAY REDUCE FRAME LOADS AND PEDESTRIAN LEVEL WINDS BUT INCREASE LOCAL CLADDED LOADS AT THE POINTS WHERE THE WIND SEPARATESTROM THE BUILDING



SETBACK ALL APOUND THE BUILDING MAY IMPROVE OR WORSEN WIND CONCENTRATION DEPENDING UPON S AND H

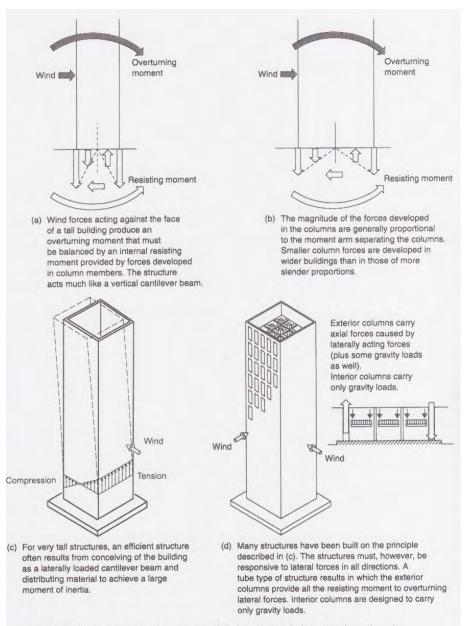
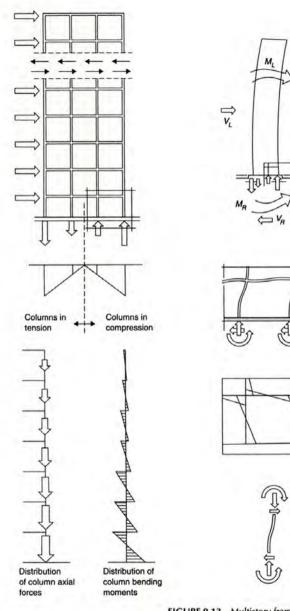
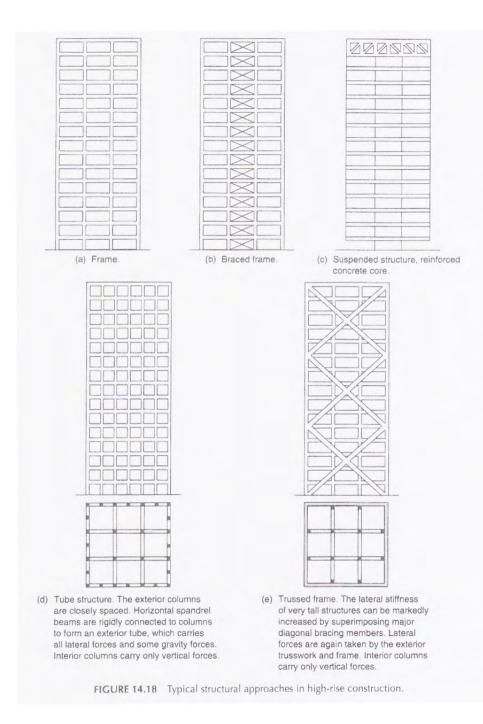


FIGURE 14.17 Very tall buildings can usefully be conceived of as vertical cantilever beams.





Illustrations from Structures 6th Ed. by Daniel L. Schodek and Martin Bechthold

Reference

Code of Practice on Wind Effects in Hong Kong 2004

http://www.bd.gov.hk/english/documents/code/windcode2004.pdf

<u>Structures</u>. Daniel L. Schodek and Martin Bechthold. See Chapter 14 Structural Systems: Design for Lateral Loadings. **TA 645 S37 2008** 

Buildings at risk: seismic design basics for practicing architects. Christopher Arnold. **TA 658.44 B85 1994**