# 2004 ASME BOILER \& PRESSURE VESSEL CODE 

AN INTERNATIONAL CODE

ASME BOILER AND PRESSURE VESSEL CODE an INTERNATIONAL CODE

# QUALIFICATION STANDARD FOR WELDING AND BRAZING PROCEDURES, WELDERS, BRAZERS, AND WELDING AND BRAZING OPERATORS 

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ASME BOILER AND PRESSURE VESSEL COMMITTEE SUBCOMMITTEE ON WELDING

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# 2004 ASME <br> BOILER AND PRESSURE VESSEL CODE 

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#### Abstract

ADDENDA Colored-sheet Addenda, which include additions and revisions to individual Sections of the Code, are published annually and will be sent automatically to purchasers of the applicable Sections up to the publication of the 2007 Code. The 2004 Code is available only in the loose-leaf format; accordingly, the Addenda will be issued in the loose-leaf, replacement-page format.


## INTERPRETATIONS

ASME issues written replies to inquiries concerning interpretation of technical aspects of the Code. The Interpretations for each individual Section will be published separately and will be included as part of the update service to that Section. They will be issued semiannually (July and December) up to the publication of the 2004 Code. Interpretations of Section III, Divisions 1 and 2, will be included with the update service to Subsection NCA.

Beginning with the 2004 Edition, Interpretations of the Code will be distributed annually in July with the issuance of the edition and subsequent addenda. Interpretations previously distributed in January will be posted in January at www.cstools.asme.org/interpretations and included in the July distribution.

## CODE CASES

The Boiler and Pressure Vessel Committee meets regularly to consider proposed additions and revisions to the Code and to formulate Cases to clarify the intent of existing requirements or provide, when the need is urgent, rules for materials or constructions not covered by existing Code rules. Those Cases which have been adopted will appear in the appropriate 2004 Code Cases book: (1) Boilers and Pressure Vessels and (2) Nuclear Components. Supplements will be sent automatically to the purchasers of the Code Cases books up to the publication of the 2007 Code.

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## FOREWORD

The American Society of Mechanical Engineers set up a committee in 1911 for the purpose of formulating standard rules for the construction of steam boilers and other pressure vessels. This committee is now called the Boiler and Pressure Vessel Committee.
The Committee's function is to establish rules of safety, relating only to pressure integrity, governing the construction ${ }^{1}$ of boilers, pressure vessels, transport tanks and nuclear components, and inservice inspection for pressure integrity of nuclear components and transport tanks, and to interpret these rules when questions arise regarding their intent. This code does not address other safety issues relating to the construction of boilers, pressure vessels, transport tanks and nuclear components, and the inservice inspection of nuclear components and transport tanks. The user of the Code should refer to other pertinent codes, standards, laws, regulations, or other relevant documents. With few exceptions, the rules do not, of practical necessity, reflect the likelihood and consequences of deterioration in service related to specific service fluids or external operating environments. Recognizing this, the Committee has approved a wide variety of construction rules in this Section to allow the user or his designee to select those which will provide a pressure vessel having a margin for deterioration in service so as to give a reasonably long, safe period of usefulness. Accordingly, it is not intended that this Section be used as a design handbook; rather, engineering judgment must be employed in the selection of those sets of Code rules suitable to any specific service or need.

This Code contains mandatory requirements, specific prohibitions, and nonmandatory guidance for construction activities. The Code does not address all aspects of these activities and those aspects which are not specifically addressed should not be considered prohibited. The Code is not a handbook and cannot replace education, experience, and the use of engineering judgment. The phrase engineering judgment refers to technical judgments made by knowledgeable designers experienced in the application of the Code. Engineering judgments must be consistent with Code philosophy and such judgments

[^0]must never be used to overrule mandatory requirements or specific prohibitions of the Code.
The Committee recognizes that tools and techniques used for design and analysis change as technology progresses and expects engineers to use good judgment in the application of these tools. The designer is responsible for complying with Code rules and demonstrating compliance with Code equations when such equations are mandatory. The Code neither requires nor prohibits the use of computers for the design or analysis of components constructed to the requirements of the Code. However, designers and engineers using computer programs for design or analysis are cautioned that they are responsible for all technical assumptions inherent in the programs they use and they are responsible for the application of these programs to their design.

The Code does not fully address tolerances. When dimensions, sizes, or other parameters are not specified with tolerances, the values of these parameters are considered nominal and allowable tolerances or local variances may be considered acceptable when based on engineering judgment and standard practices as determined by the designer.

The Boiler and Pressure Vessel Committee deals with the care and inspection of boilers and pressure vessels in service only to the extent of providing suggested rules of good practice as an aid to owners and their inspectors.

The rules established by the Committee are not to be interpreted as approving, recommending, or endorsing any proprietary or specific design or as limiting in any way the manufacturer's freedom to choose any method of design or any form of construction that conforms to the Code rules.

The Boiler and Pressure Vessel Committee meets regularly to consider revisions of the rules, new rules as dictated by technological development, Code Cases, and requests for interpretations. Only the Boiler and Pressure Vessel Committee has the authority to provide official interpretations of this Code. Requests for revisions, new rules, Code Cases, or interpretations shall be addressed to the Secretary in writing and shall give full particulars in order to receive consideration and action (see Mandatory Appendix covering preparation of technical inquiries). Proposed revisions to the Code resulting from inquiries
will be presented to the Main Committee for appropriate action. The action of the Main Committee becomes effective only after confirmation by letter ballot of the Committee and approval by ASME.

Proposed revisions to the Code approved by the Committee are submitted to the American National Standards Institute and published at http://cstools.asme.org/wbpms/ public/index.cfm?PublicReview $=$ Revisions to invite comments from all interested persons. After the allotted time for public review and final approval by ASME, revisions are published annually in Addenda to the Code.

Code Cases may be used in the construction of components to be stamped with the ASME Code symbol beginning with the date of their approval by ASME.

After Code revisions are approved by ASME, they may be used beginning with the date of issuance shown on the Addenda. Revisions, except for revisions to material specifications in Section II, Parts A and B, become mandatory six months after such date of issuance, except for boilers or pressure vessels contracted for prior to the end of the six-month period. Revisions to material specifications are originated by the American Society for Testing and Materials (ASTM) and other recognized national or international organizations, and are usually adopted by ASME. However, those revisions may or may not have any effect on the suitability of material, produced to earlier editions of specifications, for use in ASME construction. ASME material specifications approved for use in each construction Code are listed in the Guidelines for Acceptable ASTM Editions in Section II, Parts A and B. These Guidelines list, for each specification, the latest edition adopted by ASME, and earlier and later editions considered by ASME to be identical for ASME construction.

The Boiler and Pressure Vessel Committee in the formulation of its rules and in the establishment of maximum design and operating pressures considers materials, construction, methods of fabrication, inspection, and safety devices.

The Code Committee does not rule on whether a component shall or shall not be constructed to the provisions of the Code. The Scope of each Section has been established to identify the components and parameters considered by the Committee in formulating the Code rules.

Questions or issues regarding compliance of a specific component with the Code rules are to be directed to the ASME Certificate Holder (Manufacturer). Inquiries concerning the interpretation of the Code are to be directed to the ASME Boiler and Pressure Vessel Committee. ASME is to be notified should questions arise concerning improper use of an ASME Code symbol.

The specifications for materials given in Section II are identical with or similar to those of specifications
published by ASTM, AWS, and other recognized national or international organizations. When reference is made in an ASME material specification to a non-ASME specification for which a companion ASME specification exists, the reference shall be interpreted as applying to the ASME material specification. Not all materials included in the material specifications in Section II have been adopted for Code use. Usage is limited to those materials and grades adopted by at least one of the other Sections of the Code for application under rules of that Section. All materials allowed by these various Sections and used for construction within the scope of their rules shall be furnished in accordance with material specifications contained in Section II or referenced in the Guidelines for Acceptable ASTM Editions in Section II, Parts A and B, except where otherwise provided in Code Cases or in the applicable Section of the Code. Materials covered by these specifications are acceptable for use in items covered by the Code Sections only to the degree indicated in the applicable Section. Materials for Code use should preferably be ordered, produced, and documented on this basis; Guideline for Acceptable ASTM Editions in Section II, Part A and Guideline for Acceptable ASTM Editions in Section II, Part B list editions of ASME and year dates of specifications that meet ASME requirements and which may be used in Code construction. Material produced to an acceptable specification with requirements different from the requirements of the corresponding specifications listed in the Guideline for Acceptable ASTM Editions in Part A or Part B may also be used in accordance with the above, provided the material manufacturer or vessel manufacturer certifies with evidence acceptable to the Authorized Inspector that the corresponding requirements of specifications listed in the Guideline for Acceptable ASTM Editions in Part A or Part B have been met. Material produced to an acceptable material specification is not limited as to country of origin.

When required by context in this Section, the singular shall be interpreted as the plural, and vice-versa; and the feminine, masculine, or neuter gender shall be treated as such other gender as appropriate.

Either U.S. Customary units or SI units may be used for compliance with all requirements of this edition, but one system shall be used consistently throughout for all phases of construction.

Either the U.S. Customary units or SI units that are listed in Mandatory Appendix F are identified in the text, or are identified in the nomenclature for equations, shall be used consistently for all phases of construction (e.g. materials, design, fabrication, and reports). Since values in the two systems are not exact equivalents, each system shall be used independently of the other without mixing U.S. Customary units and SI units.

When SI units are selected, U.S. Customary values in referenced specifications that do not contain SI units shall be converted to SI values to at least three significant figures for use in calculations and other aspects of construction.

With the publication of the 2004 Edition, Section II, Part D is published as two separate publications. One
publication contains values only in U.S. Customary units and the other contains values only in SI units. The selection of the version to use is dependent on the set of units selected for construction.

# STATEMENT OF POLICY ON THE USE OF CODE SYMBOLS AND CODE AUTHORIZATION IN ADVERTISING 


#### Abstract

ASME has established procedures to authorize qualified organizations to perform various activities in accordance with the requirements of the ASME Boiler and Pressure Vessel Code. It is the aim of the Society to provide recognition of organizations so authorized. An organization holding authorization to perform various activities in accordance with the requirements of the Code may state this capability in its advertising literature.

Organizations that are authorized to use Code Symbols for marking items or constructions that have been constructed and inspected in compliance with the ASME Boiler and Pressure Vessel Code are issued Certificates of Authorization. It is the aim of the Society to maintain the standing of the Code Symbols for the benefit of the users, the enforcement jurisdictions, and the holders of the symbols who comply with all requirements.

Based on these objectives, the following policy has been established on the usage in advertising of facsimiles of the symbols, Certificates of Authorization, and reference to Code construction. The American Society of Mechanical Engineers does not "approve," "certify,"


"rate," or "endorse" any item, construction, or activity and there shall be no statements or implications that might so indicate. An organization holding a Code Symbol and/or a Certificate of Authorization may state in advertising literature that items, constructions, or activities "are built (produced or performed) or activities conducted in accordance with the requirements of the ASME Boiler and Pressure Vessel Code," or "meet the requirements of the ASME Boiler and Pressure Vessel Code."

The ASME Symbol shall be used only for stamping and nameplates as specifically provided in the Code. However, facsimiles may be used for the purpose of fostering the use of such construction. Such usage may be by an association or a society, or by a holder of a Code Symbol who may also use the facsimile in advertising to show that clearly specified items will carry the symbol. General usage is permitted only when all of a manufacturer's items are constructed under the rules.

The ASME logo, which is the cloverleaf with the letters ASME within, shall not be used by any organization other than ASME.

## STATEMENT OF POLICY ON THE USE OF ASME MARKING TO IDENTIFY MANUFACTURED ITEMS

The ASME Boiler and Pressure Vessel Code provides rules for the construction of boilers, pressure vessels, and nuclear components. This includes requirements for materials, design, fabrication, examination, inspection, and stamping. Items constructed in accordance with all of the applicable rules of the Code are identified with the official Code Symbol Stamp described in the governing Section of the Code.
Markings such as "ASME," "ASME Standard," or any other marking including "ASME" or the various Code

Symbols shall not be used on any item that is not constructed in accordance with all of the applicable requirements of the Code.

Items shall not be described on ASME Data Report Forms nor on similar forms referring to ASME that tend to imply that all Code requirements have been met when, in fact, they have not been. Data Report Forms covering items not fully complying with ASME requirements should not refer to ASME or they should clearly identify all exceptions to the ASME requirements.

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| B. M. Dingman | J. K. Mahaney |
| M. J. Dosdourian | A. S. Melilli |
| T. Graham | K. E. Orie |
| J. F. Grubb | E. Upitis |
| K. M. Hottle | R. Zawierucha |
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| H. D. Bushfield | H. Lorenz |
| D. A. Canonico | F. Osweiller |
| W. D. Doty | R. D. Schueler, Jr. |
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| L. G. Coffee | E. Shapiro |
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| D. A. Canonico | B. W. Roberts |
| K. K. Coleman | M. S. Shelton |
| M. Gold | R. W. Swindeman |
| F. Masuyama | B. E. Thurgood |
| O. Miyahara | T. P. Vassallo |

Subgroup on Strength of Weldments (SC II \& SC IX)

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| W. D. Doty | D. A. Swanson |
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G. M. Foster
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R. S. Hill III
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W. C. LaRochelle
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Working Group on Dynamic and Extreme Load Conditions (SG-D) (SC III)

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| R. J. Gurdal | M. S. Sills |
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## Subgroup on Surface Examination Methods (SC V)

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Subgroup on Volumetric Methods (SC V)

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| R. Kellerhall | E. F. Summers, Jr. |
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Working Group on Radiography (SG-VM) (SC V)
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Working Group on Ultrasonics (SG-VM) (SC V)

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| J. G. Feldstein | K. J. Schneider |
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Subgroup on General Requirements (SC VIII)

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| W. D. Doty | K. E. Orie |
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| P. R. Evans | M. B. Sims |
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## S. D. Reynolds, Jr.

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| Y. Imamura | G. M. Wilkowski |
| K. Koyama | K. K. Yoon |
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D. N. Hopkins
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Working Group on Liquid-Metal Reactor Covers (SG-LMCS) (SC XI)
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| G. B. Georgiev | C. J. Wirtz |

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## INTRODUCTION

The following is a brief introduction to the 2004 Edition of Section IX and cannot be considered as a substitute for the actual review of appropriate sections of the document. However, this introduction is intended to give the reader a better understanding of the purpose and organization of Section IX.

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures employed in welding or brazing in accordance with the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. As such, this is an active document subject to constant review, interpretation, and improvement to recognize new developments and research data. Section IX is a document referenced for qualification by various construction codes such as Section I, III, IV, VIII, etc. These particular construction codes apply to specific types of fabrication and may impose additional welding requirements or exemptions to Section IX qualifications. Qualification in accordance with Section IX is not a guarantee that procedures and performance qualifications will be acceptable to a particular construction code.

Section IX establishes the basic criteria for welding and brazing which are observed in the preparation of welding and brazing requirements that affect procedure and performance. It is important that the user of the 2001 Edition of Section IX understand the basic criteria in reviewing the requirements which have been established.

Section IX does not contain rules to cover all welding and brazing conditions affecting production weld or braze properties under all circumstances. Where such welding or brazing conditions are determined by the Manufacturer to affect weld or braze properties, the Manufacturer shall address those welding or brazing conditions to ensure that the required properties are achieved in the production weldment or brazement.

The purpose of the Welding Procedure Specification (WPS) and Procedure Qualification Record (PQR) is to determine that the weldment proposed for construction is capable of having the required properties for its intended application. It is presupposed that the welder or welding operator performing the welding procedure qualification test is a skilled workman. This also applies to the Brazing

Procedure Specifications (BPS) and the brazer and brazing operator qualifications. The procedure qualification test is to establish the properties of the weldment or brazement and not the skill of the personnel performing the welding or brazing. In addition, special consideration is given when notch toughness is required by other Sections of the Code. The notch-toughness variables do not apply unless referenced by the construction codes.

In Welder or Brazer/Brazing Operator Performance Qualification, the basic criterion is to determine the ability to deposit sound weld metal, or to make a sound braze. In Welding Operator Performance Qualification, the basic criterion is to determine the mechanical ability of the welding operator to operate the equipment.

In developing the present Section IX, each welding process and brazing process that was included was reviewed with regard to those items (called variables) which have an effect upon the welding or brazing operations as applied to procedure or performance criteria.

The user of Section IX should be aware of how Section IX is organized. It is divided into two parts: welding and brazing. Each part is then divided into articles. These articles deal with the following:
(a) general requirements (Article I Welding and Article XI Brazing)
(b) procedure qualifications (Article II Welding and Article XII Brazing)
(c) performance qualifications (Article III Welding and Article XIII Brazing)
(d) data (Article IV Welding and Article XIV Brazing)
(e) standard welding procedures (Article V Welding) These articles contain general references and guides that apply to procedure and performance qualifications such as positions, type and purpose of various mechanical tests, acceptance criteria, and the applicability of Section IX, which was in the Preamble of the 1980 Section IX (the Preamble has been deleted). The general requirement articles reference the data articles for specifics of the testing equipment and removal of the mechanical test specimens.

## PROCEDURE QUALIFICATIONS

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Each process that has been evaluated by Section IX is listed separately with the essential and nonessential
variables as they apply to that particular process. In general, the Welding Procedure Specifications (WPS) and the Brazing Procedure Specifications (BPS) are to list all essential and nonessential variables for each process that is included under that particular procedure specification. If a change is made in any essential variable, requalification of the procedure is required. If a change is made in a nonessential variable, the procedure need only be revised or amended to address the nonessential variable change. When notch toughness is required by the construction code, the supplementary essential variables become additional essential variables and a change requires requalification of the procedure.

In addition to covering various processes, there are also rules for procedure qualification of corrosion-resistant weld metal overlay and hard-facing weld metal overlay.

Beginning with the 2000 Addenda, the use of Standard Welding Procedure Specifications (SWPSs) was permitted. Article V provides the requirements and limitations that govern the use of these documents. The SWPSs approved for use are listed in Appendix E.

In the 2004 Edition, rules for temper bead welding were added.

## PERFORMANCE QUALIFICATIONS

These articles list separately the various welding and brazing processes with the essential variables that apply to the performance qualifications of each process. The welder, brazer, and brazing operator qualifications are limited by essential variables.

The performance qualification articles have numerous paragraphs describing general applicable variables for all processes. QW-350 and QB-350 list additional essential variables which are applicable for specific processes. The QW-350 variables do not apply to welding operators. QW-360 lists the additional essential variables for welding operators.

Generally, a welder or welding operator may be qualified by mechanical bending tests, radiography of a test plate, or radiography of the initial production weld. Brazers or brazing operators may not be qualified by radiography.

## WELDING AND BRAZING DATA

The welding and brazing data articles include the variables grouped into categories such as joints, base materials and filler materials, positions, preheat/postweld heat treatment, gas, electrical characteristics, and technique. They are referenced from other articles as they apply to each process.

These articles are frequently misused by selecting variables that do not apply to a particular process. Variables (QW-402 to QW-410 and QB-402 to QB-410) only apply as referenced for the applicable process in Article II or Article III for welding and Article XII or Article XIII for brazing. The user of Section IX should not try to apply any variable which is not referenced for that process in QW-250, QW-350, QW-360, QB-250, or QB-350.

These articles also include assignments of P-Numbers and F-Numbers to particular base materials and filler materials. Article IV also includes A-Number tables for reference by the manufacturer.

Beginning with the 1994 Addenda, the welding PNumbers, brazing P-Numbers, and nonmandatory SNumbers were consolidated into one table identified as QW/QB-422. Both the QB-422 table (brazing P-Numbers) and Appendix C table (S-Numbers) were deleted. The new QW/QB-422 table was divided into ferrous and nonferrous sections. Metals were listed in numerical order by material specification number to aid users in locating the appropriate grouping number. An abbreviated listing of metals grouped by P-Numbers, Nonmandatory Appendix D, has been included for users still wishing to locate groupings of metals by welding P-Number.

The QW-451 and QB-451 tables for procedure qualification thickness requirements and the QW-452 and QB452 tables for performance thickness qualifications are given and may only be used as referenced by other paragraphs. Generally, the appropriate essential variables reference these tables.

Revisions to the 1980 Edition of Section IX introduced new definitions for position and added a fillet weld orientation sketch to complement the groove-weld orientation sketch. The new revision to position indicates that a welder qualifies in the $1 \mathrm{G}, 2 \mathrm{G}, 3 \mathrm{G}$, etc., position and is then qualified to weld, in production, in the $\mathrm{F}, \mathrm{V}, \mathrm{H}$, or O positions as appropriate. QW-461.9 is a revised table that summarizes these new qualifications.

The data articles also give sketches of coupon orientations, removal of test specimens, and test jig dimensions. These are referenced by Articles I and XI.

QW-470 describes etching processes and reagents.
At the end of Articles IV and XIV is a list of general definitions applicable to Section IX, welding and brazing, respectively. These may differ slightly from other welding documents.

Nonmandatory Forms for welding and brazing procedure and performance qualifications appear in Appendix B. These forms are provided for the aid of those who do not wish to design their own forms. Any form(s) that address all applicable requirements of Section IX may be used.

## SUMMARY OF CHANGES

The 2004 Edition of this Code contains revisions in addition to the 2001 Edition with 2002 and 2003 Addenda. The revisions are identified with the designation 04 in the margin and, as described in the Foreword, become mandatory six months after the publication date of the 2004 Edition. To invoke these revisions before their mandatory date, use the designation "2004 Edition" in documentation required by this Code. If you choose not to invoke these revisions before their mandatory date, use the designation "2001 Edition through the 2003 Addenda" in documentation required by this Code.

Changes given below are identified on the pages by a margin note, $\mathbf{0 4}$, placed next to the affected area.

| Page | Location | Change |
| :---: | :---: | :---: |
| iii, iv | List of Sections | Updated to reflect 04 |
| vii-ix | Foreword | Editorially revised |
| xxiii, xxiv | Introduction | Procedure Qualifications revised |
| 13-15 | QW-200.2(b) | Last paragraph revised |
|  | QW-200.4(a) | Revised in its entirety |
| 16 | QW-202.4(b)(1) | Revised |
| 20 | QW-252 | QW-404.12 revised |
| 21 | QW-252.1 | QW-404.12 and QW-408.14 revised |
| 22 | QW-253 | QW-404.12 and QW-404.33 revised |
| 23 | QW-253.1 | (1) QW-404.12 and QW-407.6 revised <br> (2) QW-407.9 added |
| 24 | QW-254 | QW-404.33 revised |
| 26 | QW-254.1 | (1) QW-404.12 and QW-407.6 revised <br> (2) QW-407.9 added |
| 27, 28 | QW-255 | (1) Title corrected by errata <br> (2) QW-404.12, QW-404.33, and QW407 revised |
| 29 | QW-255.1 | (1) Title corrected by errata <br> (2) QW-404.12 and QW-407.6 revised <br> (3) QW-407.9 added |
| 30 | QW-256 | QW-404.12 and QW-404.33 revised |
| 32 | QW-256.1 | (1) QW-404.12 and QW-407.6 revised <br> (2) QW-407.9 added |
| 33 | QW-257 | QW-404.12 and QW-404.33 revised |
| 35 | QW-257.1 | (1) QW-404.12 and QW-407.6 revised <br> (2) QW-407.9 added |
| 37 | QW-258 | QW-404.12 and QW-404.33 revised |
| 38 | QW-258.1 | (1) QW-404.12 and QW-407.6 revised <br> (2) QW-407.9 added |


| Page | Location | Change |
| :---: | :---: | :---: |
| 39 | QW-259 | (1) Title corrected by errata <br> (2) QW-404.12 and QW-404.33 revised |
| 40 | QW-260 | QW-404.33 revised |
| 44 | QW-264 | QW-404.33 revised |
| 45 | QW-264.1 | (1) QW-404 and QW-407.6 revised <br> (2) QW-407.9 added |
| 47 | QW-284 | Penultimate sentence revised |
| 48-50 | QW-290 | Added |
| 57 | QW-355 | Title corrected by errata |
| 59 | QW-384 | Third sentence revised |
| 61 | QW-402.23 | Added |
|  | QW-402.24 | Added |
| 63 | QW-403.25 | Added |
|  | QW-403.26 | Added |
|  | QW-403.27 | Added |
| 64 | QW-404.12 | First two paragraphs revised |
| 65 | QW-404.33 | Revised |
| 66 | QW-404.51 | Added |
|  | QW-404.52 | Added |
| 67 | QW-406.8 | Added |
|  | QW-406.9 | Added |
|  | QW-406.10 | Added |
|  | QW-406.11 | Added |
| 68 | QW-407.9 | Added |
|  | QW-408.9 | Second line revised |
| 69 | QW-408.24 | Added |
| 70 | QW-409.29 | Added |
|  | QW-410.7 | Last line corrected by errata |
| 72 | QW-410.58 | Added |
|  | QW-410.59 | Added |
|  | QW-410.60 | Added |
|  | QW-410.61 | Added |
|  | QW-410.62 | Added |
|  | QW-410.63 | Added |
| 74 | QW-420 | Revised in its entirety |
| 75-127 | QW/QB-422 | Revised |


| Page | Location | Change |
| :---: | :---: | :---: |
| 128 | QW-423.1 | In-text table revised |
|  | QW-424.1 | In-text table revised |
| 129-135 | QW-432 | Title corrected by errata |
| 136 | QW-433 | In-text table revised |
| 138 | QW-451.1 | Note (1) corrected by errata |
| 139 | QW-451.2 | Note (1) corrected by errata |
| 142 | QW-452.4 | Revised |
| 164 | QW-462.7 | Right callout corrected by errata to read "Braze" |
| 168 | QW-462.12 | Added |
| 178, 179 | QW-466.1 | For both Customary and SI units, third entry of first column revised |
| $\begin{aligned} & 184,186,188, \\ & 189 \end{aligned}$ | QW/QB-492 | (1) Definition of filler metal, brazing corrected by errata <br> (2) Definitions of postweld hydrogen bakeout, surface temper bead reinforcing layer, and temper bead welding added |
| 210 | QB-300.3 | Second paragraph revised |
| 212 | QB-305 | First paragraph revised |
| 220 | QB-452 | Title added by errata |
| 224 | QB-462.1(c) | Revised |
| 251 | QB-484 | The sentence above "Company Name" corrected by errata |
| 252-265 | Nonmandatory Appendix D | Revised |
| 269 | Mandatory Appendix F | Added |
| 270-274 | Nonmandatory Appendix G | Added |

NOTE: Volume 54 of the Interpretations to Section IX of the ASME Boiler and Pressure Vessel Code follows the last page of the Edition to Section IX.

## ARTICLE I WELDING GENERAL REQUIREMENTS

## QW-100 GENERAL

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures that they employ in welding and brazing according to the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. It is divided into two parts: Part QW gives requirements for welding and Part QB contains requirements for brazing. Other Sections of the Code may specify different requirements than those specified by this Section. Such requirements take precedence over those of this Section, and the manufacturer or contractor shall comply with them.

QW-100.1 A Welding Procedure Specification (WPS) is a written document that provides direction to the welder or welding operator for making production welds in accordance with Code requirements. Any WPSs used by a manufacturer or contractor that will have responsible operational control of production welding shall be a WPS that has been qualified by that manufacturer or contractor in accordance with Article II, or it shall be an AWS Standard Welding Procedure Specification (SWPS) listed in Appendix E and adopted by that manufacturer or contractor in accordance with Article V.

Both WPSs and SWPSs specify the conditions (including ranges, if any) under which welding must be performed. These conditions include the base metals that are permitted, the filler metals that must be used (if any), preheat and postweld heat treatment requirements, etc. Such conditions are referred to in this Section as welding "variables."

When a WPS is to be prepared by the manufacturer or contractor, it must address, as a minimum, the specific variables, both essential and nonessential, as provided in

Article II for each process to be used in production welding. In addition, when other Sections of the Code require notch toughness qualification of the WPS, the applicable supplementary essential variables must be addressed in the WPS.

The purpose for qualification of a WPS is to determine that the weldment proposed for construction is capable of providing the required properties for its intended application. Welding procedure qualification establishes the properties of the weldment, not the skill of the welder or welding operator.

The Procedure Qualification Record (PQR) documents what occurred during welding the test coupon and the results of testing of the coupon. As a minimum, the PQR shall document the essential variables and other specific information identified in Article II for each process used during welding the test coupon and the results of the required testing. In addition, when notch toughness testing is required for procedure qualification, the applicable supplementary essential variables for each process shall be recorded.

QW-100.2 In performance qualification, the basic criterion established for welder qualification is to determine the welder's ability to deposit sound weld metal. The purpose of the performance qualification test for the welding operator is to determine the welding operator's mechanical ability to operate the welding equipment.

QW-100.3 Welding Procedure Specifications (WPS) written and qualified in accordance with the rules of this Section, and welders and welding operators of automatic and machine welding equipment also qualified in accordance with these rules may be used in any construction built to the requirements of the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

However, other Sections of the Code state the conditions under which Section IX requirements are mandatory, in whole or in part, and give additional requirements. The reader is advised to take these provisions into consideration when using this Section.

Welding Procedure Specifications, Procedure Qualification Records, and Welder/Welding Operator Performance Qualification made in accordance with the requirements of the 1962 Edition or any later Edition of Section IX may be used in any construction built to the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

Welding Procedure Specifications, Procedure Qualification Records, and Welder/Welding Operator Performance Qualification made in accordance with the requirements of the Editions of Section IX prior to 1962, in which all of the requirements of the 1962 Edition or later Editions are met, may also be used.

Welding Procedure Specifications and Welder/Welding Operator Performance Qualification records meeting the above requirements do not need to be amended to include any variables required by later Editions and Addenda.

Qualification of new Welding Procedure Specifications or Welders/Welding Operators and requalification of existing Welding Procedure Specifications or Welders/ Welding Operators shall be in accordance with the current Edition (see Foreword) and Addenda of Section IX.

## QW-101 Scope

The rules in this Section apply to the preparation of Welding Procedure Specifications and the qualification of welding procedures, welders, and welding operators for all types of manual and machine welding processes permitted in this Section. These rules may also be applied, insofar as they are applicable, to other manual or machine welding processes permitted in other Sections.

## QW-102 Terms and Definitions

Some of the more common terms relating to welding and brazing are defined in QW/QB-492.

Wherever the word pipe is designated, tube shall also be applicable.

## QW-103 Responsibility

QW-103.1 Welding. Each manufacturer ${ }^{1}$ or contractor ${ }^{1}$ is responsible for the welding done by his organization and shall conduct the tests required in this Section

[^1]to qualify the welding procedures he uses in the construction of the weldments built under this Code, and the performance of welders and welding operators who apply these procedures.

QW-103.2 Records. Each manufacturer or contractor shall maintain a record of the results obtained in welding procedure and welder and welding operator performance qualifications. These records shall be certified by the manufacturer or contractor and shall be accessible to the Authorized Inspector. Refer to recommended Forms in Nonmandatory Appendix B.

## QW-110 WELD ORIENTATION

The orientations of welds are illustrated in figure QW 461.1 or figure QW-461.2.

## QW-120 TEST POSITIONS FOR GROOVE WELDS

Groove welds may be made in test coupons oriented in any of the positions in figure QW-461.3 or figure QW-461.4 and as described in the following paragraphs, except that an angular deviation of $\pm 15 \mathrm{deg}$ from the specified horizontal and vertical planes, and an angular deviation of $\pm 5 \mathrm{deg}$ from the specified inclined plane are permitted during welding.

## QW-121 Plate Positions

QW-121.1 Flat Position 1G. Plate in a horizontal plane with the weld metal deposited from above. Refer to figure QW-461.3, illustration (a).

QW-121.2 Horizontal Position 2G. Plate in a vertical plane with the axis of the weld horizontal. Refer to figure QW-461.3, illustration (b).

QW-121.3 Vertical Position 3G. Plate in a vertical plane with the axis of the weld vertical. Refer to figure QW-461.3, illustration (c).

QW-121.4 Overhead Position 4G. Plate in a horizontal plane with the weld metal deposited from underneath. Refer to figure QW-461.3, illustration (d).

## QW-122 Pipe Positions

QW-122.1 Flat Position 1G. Pipe with its axis horizontal and rolled during welding so that the weld metal is deposited from above. Refer to figure QW-461.4, illustration (a).

QW-122.2 Horizontal Position 2G. Pipe with its axis vertical and the axis of the weld in a horizontal plane. Pipe shall not be rotated during welding. Refer to figure QW-461.4, illustration (b).

QW-122.3 Multiple Position 5G. Pipe with its axis horizontal and with the welding groove in a vertical plane.

Welding shall be done without rotating the pipe. Refer to figure QW-461.4, illustration (c).

QW-122.4 Multiple Position 6G. Pipe with its axis inclined at 45 deg to horizontal. Welding shall be done without rotating the pipe. Refer to figure QW-461.4, illustration (d).

## QW-123 Test Positions for Stud Welds

QW-123.1 Stud Welding. Stud welds may be made in test coupons oriented in any of the positions as described in QW-121 for plate and QW-122 for pipe (excluding QW-122.1). In all cases, the stud shall be perpendicular to the surface of the plate or pipe. See figures QW-461.7 and QW-461.8.

## QW-130 TEST POSITIONS FOR FILLET WELDS

Fillet welds may be made in test coupons oriented in any of the positions of figure QW-461.5 or figure QW461.6, and as described in the following paragraphs, except that an angular deviation of $\pm 15$ deg from the specified horizontal and vertical planes is permitted during welding.

## QW-131 Plate Positions

QW-131.1 Flat Position 1F. Plates so placed that the weld is deposited with its axis horizontal and its throat vertical. Refer to figure QW-461.5, illustration (a).

QW-131.2 Horizontal Position 2F. Plates so placed that the weld is deposited with its axis horizontal on the upper side of the horizontal surface and against the vertical surface. Refer to figure QW-461.5, illustration (b).

QW-131.3 Vertical Position 3F. Plates so placed that the weld is deposited with its axis vertical. Refer to figure QW-461.5, illustration (c).

QW-131.4 Overhead Position 4F. Plates so placed that the weld is deposited with its axis horizontal on the underside of the horizontal surface and against the vertical surface. Refer to figure QW-461.5, illustration (d).

## QW-132 Pipe Positions

QW-132.1 Flat Position 1F. Pipe with its axis inclined at 45 deg to horizontal and rotated during welding so that the weld metal is deposited from above and at the point of deposition the axis of the weld is horizontal and the throat vertical. Refer to figure QW-461.6, illustration (a).

## QW-132.2 Horizontal Positions 2F and 2FR

(a) Position $2 F$. Pipe with its axis vertical so that the weld is deposited on the upper side of the horizontal surface and against the vertical surface. The axis of the weld will be horizontal and the pipe is not to be rotated during welding. Refer to figure QW-461.6, illustration (b).
(b) Position $2 F R$. Pipe with its axis horizontal and the axis of the deposited weld in the vertical plane. The pipe is rotated during welding. Refer to figure QW-461.6, illustration (c).

QW-132.3 Overhead Position 4F. Pipe with its axis vertical so that the weld is deposited on the underside of the horizontal surface and against the vertical surface. The axis of the weld will be horizontal and the pipe is not to be rotated during welding. Refer to figure QW461.6, illustration (d).

QW-132.4 Multiple Position 5F. Pipe with its axis horizontal and the axis of the deposited weld in the vertical plane. The pipe is not to be rotated during welding. Refer to figure QW-461.6, illustration (e).

## QW-140 TYPES AND PURPOSES OF TESTS AND EXAMINATIONS

## QW-141 Mechanical Tests

Mechanical tests used in procedure or performance qualification are specified in QW-141.1 through QW 141.5.

QW-141.1 Tension Tests. Tension tests as described in QW-150 are used to determine the ultimate strength of groove-weld joints.

QW-141.2 Guided-Bend Tests. Guided-bend tests as described in QW-160 are used to determine the degree of soundness and ductility of groove-weld joints.

QW-141.3 Fillet-Weld Tests. Tests as described in QW-180 are used to determine the size, contour, and degree of soundness of fillet welds.

QW-141.4 Notch-Toughness Tests. Tests as described in QW-171 and QW-172 are used to determine the notch toughness of the weldment.

QW-141.5 Stud-Weld Test. Deflection bend, hammering, torque, or tension tests as shown in figures QW466.4, QW-466.5, and QW-466.6, and a macro-examination performed in accordance with QW-202.5, respectively, are used to determine acceptability of stud welds.

## QW-142 Special Examinations for Welders

Radiographic examination may be substituted for mechanical testing of QW-141 for groove-weld performance qualification as permitted in QW-304 to prove the ability of welders to make sound welds.

## QW-143 Examination for Welding Operators

An examination of a weld by radiography may be substituted for mechanical testing of QW-141 for groove weld performance qualification as permitted in QW-305 to prove the ability of welding operators to make sound welds.

## QW-144 Visual Examination

Visual examination as described in QW-194 is used to determine that the final weld surfaces meet specified quality conditions.

## QW-150 TENSION TESTS

## QW-151 Specimens

Tension test specimens shall conform to one of the types illustrated in figures QW-462.1(a) through QW462.1(e) and shall meet the requirements of QW-153.

QW-151.1 Reduced Section - Plate. Reduced-section specimens conforming to the requirements given in figure QW-462.1(a) may be used for tension tests on all thicknesses of plate.
(a) For thicknesses up to and including 1 in. ( 25 mm ), a full thickness specimen shall be used for each required tension test.
(b) For plate thickness greater than 1 in . ( 25 mm ), full thickness specimens or multiple specimens may be used, provided QW-151.1(c) and QW-151.1(d) are complied with.
(c) When multiple specimens are used, in lieu of full thickness specimens, each set shall represent a single tension test of the full plate thickness. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set.
(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QW-153.

QW-151.2 Reduced Section - Pipe. Reduced-section specimens conforming to the requirements given in figure QW-462.1(b) may be used for tension tests on all
thicknesses of pipe having an outside diameter greater than $3 \mathrm{in} .(75 \mathrm{~mm})$.
(a) For thicknesses up to and including 1 in . ( 25 mm ), a full thickness specimen shall be used for each required tension test.
(b) For pipe thicknesses greater than 1 in . ( 25 mm ), full thickness specimens or multiple specimens may be used, provided QW-151.2(c) and QW-151.2(d) are complied with.
(c) When multiple specimens are used, in lieu of full thickness specimens, each set shall represent a single tension test of the full pipe thickness. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set.
(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QW-153.

For pipe having an outside diameter of 3 in . 75 mm ) or less, reduced-section specimens conforming to the requirements given in figure QW-462.1(c) may be used for tension tests.

QW-151.3 Turned Specimens. Turned specimens conforming to the requirements given in figure QW 462.1(d) may be used for tension tests.
(a) For thicknesses up to and including 1 in . ( 25 mm ), a single turned specimen may be used for each required tension test, which shall be a specimen of the largest diameter $D$ of figure $\mathrm{QW}-462.1(\mathrm{~d})$ possible for test coupon thickness [per Note (a) of figure QW-462.1(d)].
(b) For thicknesses over 1 in. ( 25 mm ), multiple specimens shall be cut through the full thickness of the weld with their centers parallel to the metal surface and not over $1 \mathrm{in} .(25 \mathrm{~mm})$ apart. The centers of the specimens adjacent to the metal surfaces shall not exceed $5 / 8 \mathrm{in}$. $(16 \mathrm{~mm})$ from the surface.
(c) When multiple specimens are used, each set shall represent a single required tension test. Collectively, all the specimens required to represent the full thickness of the weld at one location shall comprise a set.
(d) Each specimen of the set shall be tested and meet the requirements of QW-153.

QW-151.4 Full-Section Specimens for Pipe. Tension specimens conforming to the dimensions given in figure QW-462.1(e) may be used for testing pipe with an outside diameter of 3 in . 75 mm ) or less.

## QW-152 Tension Test Procedure

The tension test specimen shall be ruptured under tensile load. The tensile strength shall be computed by dividing the ultimate total load by the least cross-sectional area
of the specimen as calculated from actual measurements made before the load is applied.

## QW-153 Acceptance Criteria - Tension Tests

QW-153.1 Tensile Strength. Minimum values for procedure qualification are provided under the column heading "Minimum Specified Tensile, ksi" of table QW/ QB-422. In order to pass the tension test, the specimen shall have a tensile strength that is not less than:
(a) the minimum specified tensile strength of the base metal; or
(b) the minimum specified tensile strength of the weaker of the two, if base metals of different minimum tensile strengths are used; or
(c) the minimum specified tensile strength of the weld metal when the applicable Section provides for the use of weld metal having lower room temperature strength than the base metal;
(d) if the specimen breaks in the base metal outside of the weld or weld interface, the test shall be accepted as meeting the requirements, provided the strength is not more than $5 \%$ below the minimum specified tensile strength of the base metal.
(e) the specified minimum tensile strength is for full thickness specimens including cladding for Aluminum Alclad materials (P-No. 21 through P-No. 23) less than $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$. For Aluminum Alclad materials $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$ and greater, the specified minimum tensile strength is for both full thickness specimens that include cladding and specimens taken from the core.

## QW-160 GUIDED-BEND TESTS <br> QW-161 Specimens

Guided-bend test specimens shall be prepared by cutting the test plate or pipe to form specimens of approximately rectangular cross section. The cut surfaces shall be designated the sides of the specimen. The other two surfaces shall be called the face and root surfaces, the face surface having the greater width of weld. The specimen thickness and bend radius are shown in figures QW-466.1, QW-466.2, and QW-466.3. Guided-bend specimens are of five types, depending on whether the axis of the weld is transverse or parallel to the longitudinal axis of the specimen, and which surface (side, face, or root) is on the convex (outer) side of bent specimen. The five types are defined as follows.

QW-161.1 Transverse Side Bend. The weld is transverse to the longitudinal axis of the specimen, which is bent so that one of the side surfaces becomes the convex surface of the bent specimen. Transverse side-bend test
specimens shall conform to the dimensions shown in figure QW-462.2.

Specimens of base metal thickness over $1 / 2 \mathrm{in}$. ( 38 mm ) may be cut into approximately equal strips between $3 / 4 \mathrm{in}$. ( 19 mm ) and $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) wide for testing, or the specimens may be bent at full width (see requirements on jig width in QW-466). If multiple specimens are used, one complete set shall be made for each required test. Each specimen shall be tested and meet the requirements in QW-163.

QW-161.2 Transverse Face Bend. The weld is transverse to the longitudinal axis of the specimen, which is bent so that the face surface becomes the convex surface of the bent specimen. Transverse face-bend test specimens shall conform to the dimensions shown in figure QW-462.3(a). For subsize transverse face bends, see QW161.4.

QW-161.3 Transverse Root Bend. The weld is transverse to the longitudinal axis of the specimen, which is bent so that the root surface becomes the convex surface of the bent specimen. Transverse root-bend test specimens shall conform to the dimensions shown in figure QW-462.3(a). For subsize transverse root bends, see QW161.4.

QW-161.4 Subsize Transverse Face and Root Bends. See Note (2) of figure QW-462.3(a).

QW-161.5 Longitudinal-Bend Tests. Longitudinalbend tests may be used in lieu of the transverse side-bend, face-bend, and root-bend tests for testing weld metal or base metal combinations, which differ markedly in bending properties between
(a) the two base metals; or
(b) the weld metal and the base metal.

QW-161.6 Longitudinal Face Bend. The weld is parallel to the longitudinal axis of the specimen, which is bent so that the face surface becomes the convex surface of the bent specimen. Longitudinal face-bend test specimens shall conform to the dimensions shown in figure QW-462.3(b).

QW-161.7 Longitudinal Root Bend. The weld is parallel to the longitudinal axis of the specimen, which is bent so that the root surface becomes the convex side of the bent specimen. Longitudinal root-bend test specimens shall conform to the dimensions shown in figure QW 462.3(b).

## QW-162 Guided-Bend Test Procedure

QW-162.1 Jigs. Guided-bend specimens shall be bent in test jigs that are in substantial accordance with QW466. When using the jigs illustrated in figure QW-466.1
or figure QW-466.2, the side of the specimen turned toward the gap of the jig shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater discontinuities, if any, for side-bend specimens. The specimen shall be forced into the die by applying load on the plunger until the curvature of the specimen is such that a $1 / 8 \mathrm{in}$. ( 3 mm ) diameter wire cannot be inserted between the specimen and the die of figure QW-466.1, or the specimen is bottom ejected if the roller type of jig (figure QW-466.2) is used.

When using the wrap around jig (figure QW-466.3), the side of the specimen turned toward the roller shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater discontinuities, if any, for side-bend specimens.

When specimens wider than $1 \frac{1}{2} \mathrm{in}$. $(38 \mathrm{~mm})$ are to be bent as permitted in figure QW-462.2, the test jig mandrel must be at least $1 / 4 \mathrm{in}$. ( 6 mm ) wider than the specimen width.

## QW-163 Acceptance Criteria - Bend Tests

The weld and heat-affected zone of a transverse weldbend specimen shall be completely within the bent portion of the specimen after testing.

The guided-bend specimens shall have no open discontinuity in the weld or heat-affected zone exceeding $1 / 8 \mathrm{in}$. ( 3 mm ), measured in any direction on the convex surface of the specimen after bending. Open discontinuities occurring on the corners of the specimen during testing shall not be considered unless there is definite evidence that they result from lack of fusion, slag inclusions, or other internal discontinuities. For corrosion-resistant weld overlay cladding, no open discontinuity exceeding $1 / 16 \mathrm{in}$. $(1.5 \mathrm{~mm})$, measured in any direction, shall be permitted in the cladding, and no open discontinuity exceeding $1 / 8 \mathrm{in}$. $(3 \mathrm{~mm})$ shall be permitted along the approximate weld interface.

## QW-170 NOTCH-TOUGHNESS TESTS <br> QW-171 Notch-Toughness Tests - Charpy V-Notch

QW-171.1 General. Charpy V-notch impact tests shall be made when required by other Sections.

Test procedures and apparatus shall conform to the requirements of SA-370.

QW-171.2 Acceptance. The acceptance criteria shall be in accordance with that Section specifying impact requirements.

QW-171.3 Location and Orientation of Test Specimen. The impact test specimen and notch location and
orientation shall be as given in the Section requiring such tests.

When qualifying pipe in the 5 G or 6 G position, the notch-toughness specimens shall be removed from the shaded portion of figure QW-463.1(f).

## QW-172 Notch-Toughness Tests - Drop Weight

QW-172.1 General. Drop weight tests shall be made when required by other Sections.

Test procedures and apparatus shall conform to the requirements of ASTM Specification E 208.

QW-172.2 Acceptance. The acceptance criteria shall be in accordance with that Section requiring drop weight tests.

QW-172.3 Location and Orientation of Test Specimen. The drop weight test specimen, the crack starter location, and the orientation shall be as given in the Section requiring such tests.

When qualifying pipe in the 5 G or 6 G position, the notch-toughness specimens shall be removed from the shaded portion of figure QW-463.1(f).

## QW-180 FILLET-WELD TESTS <br> QW-181 Procedure and Performance Qualification Specimens

QW-181.1 Procedure. The dimensions and preparation of the fillet-weld test coupon for procedure qualification as required in QW-202 shall conform to the requirements in figure $\mathrm{QW}-462.4$ (a) or figure QW 462.4(d). The test coupon for plate-to-plate shall be cut transversely to provide five test specimen sections, each approximately 2 in . ( 50 mm ) long. For pipe-to-plate or pipe-to-pipe, the test coupon shall be cut transversely to provide four approximately equal test specimen sections. The test specimens shall be macro-examined to the requirements of QW-183.

QW-181.1.1 Production Assembly Mockups. Production assembly mockups may be used in lieu of QW-181.1. The mockups for plate-to-shape shall be cut transversely to provide five approximately equal test specimens not to exceed approximately $2 \mathrm{in} .(50 \mathrm{~mm})$ in length. For pipe-to-shape mockups, the mockup shall be cut transversely to provide four approximately equal test specimens. For small mockups, multiple mockups may be required to obtain the required number of test specimens. The test specimens shall be macro-examined to the requirements of QW-183.

QW-181.2 Performance. The dimensions and the preparation of the fillet-weld test coupon for performance
qualification shall conform to the requirements in figure QW-462.4(b) or figure QW-462.4(c). The test coupon for plate-to-plate shall be cut transversely to provide a center section approximately 4 in . $(100 \mathrm{~mm}$ ) long and two end sections, each approximately 1 in . $(25 \mathrm{~mm}$ ) long. For pipe-to-plate or pipe-to-pipe, the test coupon shall be cut to provide two quarter sections test specimens opposite to each other. One of the test specimens shall be fracture tested in accordance with QW-182 and the other macroexamined to the requirements of QW-184. When qualifying pipe-to-plate or pipe-to-pipe in the 5 F position, the test specimens shall be removed as indicated in figure QW-463.2(h).

QW-181.2.1 Production Assembly Mockups. Production assembly mockups may be used in lieu of the fillet-weld test coupon requirements of QW-181.2.

## (a) Plate-to-shape

(1) The mockup for plate-to-shape shall be cut transversely to provide three approximately equal test specimens not to exceed approximately 2 in . 50 mm ) in length. The test specimen that contains the start and stop of the weld shall be fracture tested in accordance with QW182. A cut end of one of the remaining test specimens shall be macro-examined in accordance with QW-184.

## (b) Pipe-to-shape

(1) The mockup for pipe-to-shape shall be cut transversely to provide two quarter sections approximately opposite to each other. The test specimen that contains the start and stop of the weld shall be fracture tested in accordance with QW-182. A cut end of the other quarter section shall be macro-examined in accordance with QW184. When qualifying pipe-to-shape in the 5 F position, the fracture specimen shall be removed from the lower 90 deg section of the mockup.

## QW-182 Fracture Tests

The stem of the 4 in . ( 100 mm ) performance specimen center section in figure QW-462.4(b) or the stem of the quarter section in figure QW-462.4(c), as applicable, shall be loaded laterally in such a way that the root of the weld is in tension. The load shall be steadily increased until the specimen fractures or bends flat upon itself.

If the specimen fractures, the fractured surface shall show no evidence of cracks or incomplete root fusion, and the sum of the lengths of inclusions and porosity visible on the fractured surface shall not exceed $3 / 8 \mathrm{in}$. ( 10 mm ) in figure QW-462.4(b) or $10 \%$ of the quarter section in figure QW-462.4(c).

## QW-183 Macro-Examination - Procedure Specimens

One face of each cross section of the five test specimens in figure QW-462.4(a) or four test specimens in figure QW-462.4(d), as applicable shall be smoothed and etched with a suitable etchant (see QW-470) to give a clear definition to the weld metal and heat affected zone. The examination of the cross sections shall include only one side of the test specimen at the area where the plate or pipe is divided into sections i.e., adjacent faces at the cut shall not be used. In order to pass the test
(a) visual examination of the cross sections of the weld metal and heat-affected zone shall show complete fusion and freedom from cracks
(b) there shall be not more than $\frac{1}{8} \mathrm{in}$. ( 3 mm ) difference in the length of the legs of the fillet

## QW-184 Macro-Examination - Performance Specimens

The cut end of one of the end plate sections, approximately 1 in . 25 mm ) long, in figure QW-462.4(b) or the cut end of one of the pipe quarter sections in figure QW462.4(c), as applicable, shall be smoothed and etched with a suitable etchant (see QW-470) to give a clear definition of the weld metal and heat affected zone. In order to pass the test
(a) visual examination of the cross section of the weld metal and heat-affected zone shall show complete fusion and freedom from cracks, except that linear indications at the root not exceeding $1 / 32$ in. $(0.8 \mathrm{~mm})$ shall be acceptable
(b) the weld shall not have a concavity or convexity greater than $1 / 16 \mathrm{in}$. $(1.5 \mathrm{~mm})$
(c) there shall be not more than $\frac{1}{8} \mathrm{in}$. ( 3 mm ) difference in the lengths of the legs of the fillet

## QW-190 OTHER TESTS AND EXAMINATIONS

## QW-191 Radiographic Examination

QW-191.1 Method. The radiographic examination in QW-142 for welders and in QW-143 for welding operators shall meet the requirements of Article 2, Section V, except as follows:
(a) A written radiographic examination procedure is not required. Demonstration of density and penetrameter image requirements on production or technique radiographs shall be considered satisfactory evidence of compliance with Article 2 of Section V.
(b) The requirements of T-285 of Article 2 of Section V are to be used only as a guide. Final acceptance of
radiographs shall be based on the ability to see the prescribed penetrameter image and the specified hole or the designated wire or a wire penetrameter. The acceptance standards of QW-191.2 shall be met.

## QW-191.2 Radiographic Acceptance Criteria QW-191.2.1 Terminology

(a) Linear Indications. Cracks, incomplete fusion, inadequate penetration, and slag are represented on the radiograph as linear indications in which the length is more than three times the width.
(b) Rounded Indications. Porosity and inclusions such as slag or tungsten are represented on the radiograph as rounded indications with a length three times the width or less. These indications may be circular, elliptical, or irregular in shape; may have tails; and may vary in density.

QW-191.2.2 Acceptance Standards. Welder and welding operator performance tests by radiography of welds in test assemblies shall be judged unacceptable when the radiograph exhibits any imperfections in excess of the limits specified below.

## (a) Linear Indications

(1) any type of crack or zone of incomplete fusion or penetration
(2) any elongated slag inclusion which has a length greater than
(a) $1 / 8 \mathrm{in}$. $(3 \mathrm{~mm})$ for $t$ up to $3 / 8 \mathrm{in} .(10 \mathrm{~mm})$, inclusive
(b) $\frac{1}{3} t$ for $t$ over $3 / 8 \mathrm{in}$. $(10 \mathrm{~mm})$ to $2 \frac{1}{4} \mathrm{in}$. $(57 \mathrm{~mm})$, inclusive
(c) $3 / 4$ in. $(19 \mathrm{~mm})$ for $t$ over $2 \frac{1}{4} \mathrm{in}$. ( 57 mm )
(3) any group of slag inclusions in line that have an aggregate length greater than $t$ in a length of $12 t$, except when the distance between the successive imperfections exceeds $6 L$ where $L$ is the length of the longest imperfection in the group

## (b) Rounded Indications

(1) The maximum permissible dimension for rounded indications shall be $20 \%$ of $t$ or $1 / 8 \mathrm{in}$. ( 3 mm ), whichever is smaller.
(2) For welds in material less than $1 / 8 \mathrm{in}$. $(3 \mathrm{~mm})$ in thickness, the maximum number of acceptable rounded indications shall not exceed 12 in a 6 in. $(150 \mathrm{~mm})$ length of weld. A proportionately fewer number of rounded indications shall be permitted in welds less than 6 in . $(150 \mathrm{~mm})$ in length.
(3) For welds in material $1 / 8$ in. ( 3 mm ) or greater in thickness, the charts in Appendix I represent the maximum acceptable types of rounded indications illustrated in typically clustered, assorted, and randomly dispersed configurations. Rounded indications less than $\frac{1}{32} \mathrm{in}$.
$(0.8 \mathrm{~mm})$ in maximum diameter shall not be considered in the radiographic acceptance tests of welders and welding operators in these ranges of material thicknesses.

QW-191.2.3 Production Welds. The acceptance standard for welding operators who qualify on production welds shall be that specified in the referencing Code Section. The acceptance standard for welders who qualify on production welds as permitted by QW-304.1 shall be per QW-191.2.2.

QW-191.3 Record of Tests. The results of welder and welding operator performance tests by radiography shall be recorded in accordance with QW-301.4.

## QW-192 Stud-Weld Tests - Procedure Qualification Specimens

QW-192.1 Required Tests. Ten stud-weld tests are required to qualify each procedure. The equipment used for stud welding shall be completely automatic except for manual starting.

Every other welding stud (five joints) shall be tested either by hammering over until one-fourth of its length is flat on the test piece, or by bending the stud to an angle of at least 15 deg and returning it to its original position using a test jig and an adapter location dimension that are in accordance with figure QW-466.4.

The remaining five welded stud joints shall be tested in torque using a torque testing arrangement that is substantially in accordance with figure QW-466.5. Alternatively, where torquing is not feasible, tensile testing may be used, and the fixture for tensile testing shall be similar to that shown in figure QW-466.6, except that studs without heads may be gripped on the unwelded end in the jaws of the tensile testing machine.

## QW-192.2 Acceptance Criteria - Bend and Ham-

mer Tests. In order to pass the test(s), each of the five stud welds and heat-affected zones shall be free of visible separation or fracture after bending and return bending or after hammering.

QW-192.3 Acceptance Criteria - Torque Tests. In order to pass the test(s), each of the five stud welds shall be subjected to the required torque shown in the following table before failure occurs.

| Nominal Diameter of Studs, in. (mm) | uired Torque for Testing aded Carbon Steel Studs | Testing Torque, ft-lb (J) |
| :---: | :---: | :---: |
|  | Threads/in. and Series Designated |  |
| $1 / 4$ (6.4) | 28 UNF | 5.0 (6.8) |
| 1/4 (6.4) | 20 UNC | 4.2 (5.7) |
| 5/16 (7.9) | 24 UNF | 9.5 (12.9) |
| 5/16 (7.9) | 18 UNC | 8.6 (11.7) |
| $3 / 8$ (9.5) | 24 UNF | 17 (23.0) |
| $3 / 8$ (9.5) | 16 UNC | 15 (20.3) |
| $7 / 16$ (11.1) | 20 UNF | 27 (36.6) |
| 7/16 (11.1) | 14 UNC | 24 (32.5) |
| 1/2 (12.7) | 20 UNF | 42 (57.0) |
| $1 / 2$ (12.7) | 13 UNC | 37 (50.2) |
| $9 / 16$ (14.3) | 18 UNF | 60 (81.4) |
| $9 / 16$ (14.3) | 12 UNC | 54 (73.2) |
| 5/8 (15.9) | 18 UNF | 84 (114.0) |
| 5/8 (15.9) | 11 UNC | 74 (100.0) |
| $3 / 4$ (19.0) | 16 UNF | 147 (200.0) |
| $3 / 4$ (19.0) | 10 UNC | 132 (180.0) |
| $7 / 8$ (22.2) | 14 UNF | 234 (320.0) |
| 7/8 (22.2) | 9 UNC | 212 (285.0) |
| 1 (25.4) | 12 UNF | 348 (470.0) |
| 1 (25.4) | 8 UNC | 318 (430.0) |

Required Torque for Testing

| Nominal Diameter of Studs, in. (mm) | Threads/in. and Series Designated | Testing Torque, ft-lb (J) |
| :---: | :---: | :---: |
| $1 / 4$ (6.4) | 28 UNF | 4.5 (6.1) |
| $1 / 4$ (6.4) | 20 UNC | 4.0 (5.4) |
| 5/16 (7.9) | 24 UNF | 9.0 (12.2) |
| 5/16 (7.9) | 18 UNC | 8.0 (10.8) |
| $3 / 8$ (9.5) | 24 UNF | 16.5 (22.4) |
| 3/8 (9.5) | 16 UNC | 14.5 (19.7) |
| 7/16 (11.1) | 20 UNF | 26.0 (35.3) |
| 7/16 (11.1) | 14 UNC | 23.0 (31.2) |
| 1/2 (12.7) | 20 UNF | 40.0 (54.2) |
| 1/2 (12.7) | 13 UNC | 35.5 (48.1) |
| 5/8 (15.9) | 18 UNF | 80.00 (108.5) |
| 5/8 (15.9) | 11 UNC | 71.00 (96.3) |
| $3 / 4$ (19.0) | 16 UNF | 140.00 (189.8) |
| $3 / 4$ (19.0) | 10 UNC | 125.00 (169.5) |
| $7 / 8$ (22.2) | 14 UNF | 223.00 (302.3) |
| 7/8 (22.2) | 9 UNC | 202.00 (273.9) |
| 1 (25.4) | 14 UNF | 339.00 (459.6) |
| 1 (25.4) | 8 UNC | 303.00 (410.8) |

Alternatively, where torquing to destruction is not feasible, tensile testing may be used. For carbon and austenitic stainless steel studs, the failure strength shall be not less than $35,000 \mathrm{psi}(240 \mathrm{MPa})$ and $30,000 \mathrm{psi}(210 \mathrm{MPa})$, respectively. For other metals, the failure strength shall not be less than $\frac{1}{2}$ of the minimum specified tensile strength of the stud material. The failure strength shall
be based on the minor diameter of the threaded section of externally threaded studs, except where the shank diameter is less than the minor diameter, or on the original cross-sectional area where failure occurs in a nonthreaded, internally threaded, or reduced-diameter stud.

QW-192.4 Acceptance Criteria - Macro-Examination. In order to pass the macro-examination, each of five sectioned stud welds and the heat-affected zone shall be free of cracks when examined at 10X magnification, which is required by QW-202.5 when studs are welded to metals other than P-No. 1.

## QW-193 Stud-Weld Tests - Performance Qualification Specimens

QW-193.1 Required Tests. Five stud-weld tests are required to qualify each stud-welding operator. The equipment used for stud welding shall be completely automatic except for manual starting. The performance test shall be welded in accordance with a qualified WPS per QW-301.2.

Each stud (five joints) shall be tested either by hammering over until one-fourth of its length is flat on the test piece or by bending the stud to an angle of at least 15 deg and returning it to its original position using a test jig and an adapter location dimension that are in accordance with figure QW-466.4.

QW-193.2 Acceptance Criteria - Bend and Hammer Tests. In order to pass the test(s), each of the five stud welds and heat affected zones shall be free of visible separation or fracture after bending and return bending or after hammering.

## QW-194 Visual Examination - Performance

Performance test coupons shall show complete joint penetration with complete fusion of weld metal and base metal.

## QW-195 Liquid Penetrant Examination

QW-195.1 The liquid penetrant examination in QW214 for corrosion-resistant weld metal overlay shall meet the requirements of Section V, Article 6. The acceptance standards of QW-195.2 shall be met.

## QW-195.2 Liquid Penetrant Acceptance Criteria QW-195.2.1 Terminology

relevant indications: indications with major dimensions greater than $1 / 16$ in. ( 1.5 mm ).
linear indications: an indication having a length greater than three times the width.
rounded indications: an indication of circular or elliptical shape with the length equal to or less than three times the width.

QW-195.2.2 Acceptance Standards. Procedure and performance tests examined by liquid penetrant techniques shall be judged unacceptable when the examination exhibits any indication in excess of the limits specified below:
(a) relevant linear indications
(b) relevant rounded indications greater than $3 / 16 \mathrm{in}$. ( 5 mm )
(c) four or more relevant rounded indications in a line separated by $1 / 16 \mathrm{in}$. ( 1.5 mm ) or less (edge-to-edge)

## QW-196 Resistance Weld Testing <br> QW-196.1 Metallographic Examination

QW-196.1.1 Welds shall be cross-sectioned, polished, and etched to reveal the weld metal. The section shall be examined at 10 X magnification.

QW-196.1.2 The weld nugget shall be sound for 1.25 times the thickness of the thinner member.

QW-196.1.3 For spot welds, the nugget size shall be measured at the interface between the sheets being joined, and it shall equal or exceed $0.9 \sqrt{t}(4.5 \sqrt{t})$, where $t$ is the thickness of the thinner sheet. For projection welds, the nugget size shall not be less than the initial size of the projection. For seam welds, the width of the fused weld cut transverse to the seam shall be not less than $0.9 \sqrt{t}(4.5 \sqrt{t})$, where $t$ is the thickness of the thinnest sheet.

## QW-196.2 Mechanical Testing

QW-196.2.1 Shear test specimens shall be prepared as shown on figure QW-462.9. For spot and projection welds, each test specimen shall equal or exceed the minimum strength, and the average strength specified in tables QW-462.10 and QW-462.11 for the appropriate material. Further, for each set, $90 \%$ shall have shear strength values between 0.9 and 1.1 times the set average value. The remaining $10 \%$ shall lie between 0.8 and 1.2 times the set average value.

QW-196.2.2 Peel test specimens shall be prepared as shown in figure QW-462.8. The specimens shall be peeled or separated mechanically, and fracture shall occur in the base metal by tearing out of the weld in order for the specimen to be acceptable.

QW-197 Laser Beam Welding (LBW) Lap Joint Tests - Procedure Qualification Specimens
QW-197.1 Required Tests. Six tension shear specimens and eight macro specimens are required to qualify
each procedure. The qualification test coupon shall be prepared in accordance with figure QW-464.1. The tension shear specimens shall conform to the dimensions indicated in the table of figure QW-464.1. The longitudinal and traverse sections indicated in figure QW-464.1 shall be cross-sectioned as closely as possible through the centerline of the weld. A minimum of 1 in . $(25 \mathrm{~mm}$ ) shall be provided for examination of each longitudinal specimen. The traverse specimens shall be of sufficient length to include weld, the heat-affected zone, and portions of the unaffected base material. Cross-sections shall be smoothed and etched with a suitable etchant (see QW470 ), and examined at a minimum magnification of 25 X . The dimensions of the fusion zone and penetration of each weld of the traverse specimens shall be measured to the nearest hundredth of an inch and recorded.

QW-197.2 Acceptance Criteria - Tension Shear Tests. In order to pass the tension shear test(s), the requirements of QW-153 shall apply.

QW-197.3 Acceptance Criteria - Macro-Examination. In order to pass the macro-examination, each of the eight specimens shall meet the following criteria:
(a) The outline of the fusion zone shall be generally consistent in size and regular in shape and uniformity of penetration.
(b) The examination of the weld area shall reveal sound weld metal, complete fusion along the bond line, and complete freedom from cracks in the weld metal and heat-affected zone.

## QW-198 Laser Beam Welding (LBW) Lap Joint Tests - Performance Qualification Specimens

QW-198.1 Required Tests. A peel test specimen at least 6 in . $(150 \mathrm{~mm})$ long shall be prepared as shown in figure QW-464.2 illustration (a) and macro specimens as shown in figure QW-464.2 illustration (b). The peel test specimens shall be peeled apart to destruction and the fusion zone and penetration measured to the nearest hundredth of an inch. The end of each strip of the macro coupon shall be polished and etched to clearly reveal the weld metal. The width and depth of penetration of each weld shall be measured to the nearest hundredth of an inch. Each specimen shall be examined in accordance with QW-197.1.

QW-198.2 Acceptance Criteria - Peel Test and Macro-Examination. In order to pass the peel test and macro-examination, the dimensions of the fusion zone (averaged) and the penetration (averaged) shall be within the range of dimensions of those specified on the WPS that was used to make the test coupon.

## QW-199 Flash Welding

QW-199.1 Procedure Qualification Test Coupons and Testing

QW-199.1.1 Test Coupon Preparation. For coupons NPS 1 (DN 25) and smaller, four test welds shall be made, and for pipes over NPS 1 (DN 25), three test coupons shall be made using one set of welding parameters (i.e., the same equipment, base metals, joint preparation, and other essential variables to be utilized for production welding.) These variables shall be recorded on the qualification record.

QW-199.1.2 Tensile Tests. For pipes NPS 1 (DN 25) and smaller, two full-section tensile specimens shall be prepared in accordance with figure QW-462.1(e). For pipes greater than NPS 1 (DN 25), two reduced section tension specimens shall be prepared in accordance with figure QW-462.1(b) or figure QW-462.1(c) from one coupon. The specimens shall be tested in accordance with QW-160.

QW-199.1.3 Section and Bend Testing. The entire circumference of each remaining coupon shall be cut along the axis of the pipe into an even number of strips of a length sufficient to perform bend tests. The maximum width of each strip shall be $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) and the minimum width

$$
\begin{aligned}
& w=t+D / 4 \text { for pipes NPS } 2(\mathrm{DN} 50) \text { and smaller } \\
& w=t+D / 8 \text { for pipes greater than NPS } 2(\mathrm{DN} 50)
\end{aligned}
$$

where
$D=$ OD of the tube
$t=$ nominal wall thickness
$w=$ width of the specimen
One edge of one strip from each coupon shall be polished to a 600 grit finish with the final grinding parallel to the long axis of the strip. The polished surface shall be examined at 5 X magnification. No incomplete fusion or other open flaws on the polished surface are acceptable. Defects occurring in the base metal not associated with the weld may be disregarded.

All flash shall be removed from the strips and the welds shall be visually examined per QW-194. Half of the strips from each specimen shall then be prepared as root bend specimens and the remaining strips shall be prepared as face bend specimens in accordance with QW-160. The specimens shall be tested in accordance with QW-160, except for the following:
(a) For P-No. 1, Groups 2 through 4 materials, the minimum bend radius (dimension $B$ in figure $\mathrm{QW}-466.1$ ) shall be three times the thickness of the specimen.
(b) In lieu of QW-163, the sum of lengths of individual open flaws on the convex surface of all the bend test specimens taken from each pipe individually shall not exceed $5 \%$ of the outside circumference of that test pipe.

QW-199.2 Flash Welding - Performance Qualification Test Coupons and Testing. One test coupon shall be welded, cut into strips, visually examined, and bend tested in accordance with QW-197.3. Polishing and examination of a cross-section is not required.

## APPENDIX I

ROUNDED INDICATION CHARTS
(See QW-191.2)


Typical Quantity and Size Permitted in 6 in. $(150 \mathrm{~mm})$ Length of Weld
Over $1 / 4 \mathrm{in}$. $(6 \mathrm{~mm})$ to $\frac{1}{2} \mathrm{in}$. $(13 \mathrm{~mm})$
Thickness


Typical Quantity and Size Permitted
in 6 in. ( 150 mm ) Length of Weld
Over $\frac{1}{2} \mathrm{in}$. ( 13 mm ) to 1 in . ( 25 mm )
Thickness


Typical Quantity and Size Permitted
in 6 in. ( 150 mm ) Length of Weld
Over 1 in. ( 25 mm ) Thickness

# ARTICLE II WELDING PROCEDURE QUALIFICATIONS 

## QW-200 GENERAL

QW-200.1 Each manufacturer and contractor shall prepare written Welding Procedure Specifications that are defined as follows:
(a) Welding Procedure Specification (WPS). A WPS is a written qualified welding procedure prepared to provide direction for making production welds to Code requirements. The WPS or other documents may be used to provide direction to the welder or welding operator to assure compliance with the Code requirements.
(b) Contents of the WPS. The completed WPS shall describe all of the essential, nonessential, and, when required, supplementary essential variables for each welding process used in the WPS. These variables are listed in QW-250 through QW-280 and are defined in Article IV, Welding Data.

The WPS shall reference the supporting Procedure Qualification Record(s) (PQR) described in QW-200.2. The manufacturer or contractor may include any other information in the WPS that may be helpful in making a Code weldment.
(c) Changes to the WPS. Changes may be made in the nonessential variables of a WPS to suit production requirements without requalification provided such changes are documented with respect to the essential, nonessential, and, when required, supplementary essential variables for each process. This may be by amendment to the WPS or by use of a new WPS.

Changes in essential or supplementary essential (when required) variables require requalification of the WPS (new or additional PQRs to support the change in essential or supplementary essential variables).
(d) Format of the WPS. The information required to be in the WPS may be in any format, written or tabular, to fit the needs of each manufacturer or contractor, as long as every essential, nonessential, and, when required, supplementary essential variables outlined in QW-250 through QW-280 is included or referenced.

Form QW-482 (see Nonmandatory Appendix B) has been provided as a guide for the WPS. This Form includes the required data for the SMAW, SAW, GMAW, and GTAW processes. It is only a guide and does not list
all required data for other processes. It also lists some variables that do not apply to all processes (e.g., listing shielding gas which is not required for SAW). The guide does not easily lend itself to multiple process procedure specification (e.g., GTAW root with SMAW fill).
(e) Availability of the WPS. A WPS used for Code production welding shall be available for reference and review by the Authorized Inspector (AI) at the fabrication site.

QW-200.2 Each manufacturer or contractor shall be required to prepare a procedure qualification record which is defined as follows:
(a) Procedure Qualification Record (PQR). A PQR is a record of the welding data used to weld a test coupon. The PQR is a record of variables recorded during the welding of the test coupons. It also contains the test results of the tested specimens. Recorded variables normally fall within a small range of the actual variables that will be used in production welding.
(b) Contents of the PQR. The completed PQR shall document all essential and, when required, supplementary essential variables of QW-250 through QW-280 for each welding process used during the welding of the test coupon. Nonessential or other variables used during the welding of the test coupon may be recorded at the manufacturer's or contractor's option. All variables, if recorded, shall be the actual variables (including ranges) used during the welding of the test coupon. If variables are not monitored during welding, they shall not be recorded. It is not intended that the full range or the extreme of a given range of variables to be used in production be used during qualification unless required due to a specific essential or, when required, supplementary essential variable.
The $\operatorname{PQR}$ shall be certified accurate by the manufacturer or contractor. The manufacturer or contractor may not subcontract the certification function. This certification is intended to be the manufacturer's or contractor's verification that the information in the PQR is a true record of the variables that were used during the welding of the test coupon and that the resulting tensile, bend, or
macro (as required) test results are in compliance with Section IX.

One or more combinations of welding processes, filler metal, and other variables may be used when welding a test coupon. The approximate thickness of weld metal deposited shall be recorded for each set of essential and, when required, supplementary essential variables. Weld metal deposited using each set of variables shall be included in the tension, bend, notch toughness, and other mechanical test specimens that are required.
(c) Changes to the $P Q R$. Changes to the PQR are not permitted except as described below. It is a record of what happened during a particular welding test. Editorial corrections or addenda to the PQR are permitted. An example of an editorial correction is an incorrect P -Number, F-Number, or A-Number that was assigned to a particular base metal or filler metal. An example of an addendum would be a change resulting from a Code change. For example, Section IX may assign a new FNumber to a filler metal or adopt a new filler metal under an established F-Number. This may permit, depending on the particular construction Code requirements, a manufacturer or contractor to use other filler metals that fall within that particular F-Number where, prior to the Code revision, the manufacturer or contractor was limited to the particular electrode classification that was used during qualification. Additional information can be incorporated into a PQR at a later date provided the information is substantiated as having been part of the original qualification condition by lab record or similar data.

All changes to a PQR require recertification (including date) by the manufacturer or contractor.
(d) Format of the PQR. Form QW-483 (see Nonmandatory Appendix B) has been provided as a guide for the $P Q R$. The information required to be in the PQR may be in any format to fit the needs of each manufacturer or contractor, as long as every essential and, when required, supplementary essential variable, required by QW-250 through QW-280, is included. Also the type of tests, number of tests, and test results shall be listed in the PQR.

Form QW-483 does not easily lend itself to cover combinations of welding processes or more than one FNumber filler metal in one test coupon. Additional sketches or information may be attached or referenced to record the required variables.
(e) Availability of the PQR. PQRs used to support WPSs shall be available, upon request, for review by the Authorized Inspector (AI). The PQR need not be available to the welder or welding operator.
(f) Multiple WPSs With One PQR/Multiple PQRs With One WPS. Several WPSs may be prepared from the data on a single PQR (e.g., a 1G plate PQR may support WPSs
for the $\mathrm{F}, \mathrm{V}, \mathrm{H}$, and O positions on plate or pipe within all other essential variables). A single WPS may cover several essential variable changes as long as a supporting PQR exists for each essential and, when required, supplementary essential variable [e.g., a single WPS may cover a thickness range from $1 / 16 \mathrm{in}$. $(1.5 \mathrm{~mm})$ through $1 \frac{1}{4} \mathrm{in}$. ( 32 mm ) if PQRs exist for both the $1 / 16 \mathrm{in}$. $(1.5 \mathrm{~mm}$ ) through $3 / 16$ in. ( 5 mm ) and $3 / 16$ in. ( 5 mm ) through $1 \frac{1}{4} \mathrm{in}$. ( 32 mm ) thickness ranges].

QW-200.3 To reduce the number of welding procedure qualifications required, P-Numbers are assigned to base metals dependent on characteristics such as composition, weldability, and mechanical properties, where this can logically be done; and for steel and steel alloys (table QW/QB-422) Group Numbers are assigned additionally to P-Numbers. These Group Numbers classify the metals within P-Numbers for the purpose of procedure qualification where notch-toughness requirements are specified. The assignments do not imply that base metals may be indiscriminately substituted for a base metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, postweld heat treatment, design, mechanical properties, and service requirements. Where notch toughness is a consideration, it is presupposed that the base metals meet the specific requirements.

In general, notch-toughness requirements are mandatory for all P-No. 11 quenched and tempered metals, for low temperature applications of other metals as applied to Section VIII, and for various classes of construction required by Section III. Acceptance criteria for the notchtoughness tests are as established in the other Sections of the Code.

For certain materials permitted by the ASME/ANSI B31 Code for Pressure Piping or by selected Code Cases of the ASME Boiler and Pressure Vessel Code but which are not included within the ASME Boiler and Pressure Vessel Code Material Specifications (Section II), S-Number groupings are assigned in table QW/QB-422. These groupings are similar to the P-Number groupings of table QW/QB-422. Qualification limits are given in QW-420.2.

## QW-200.4 Combination of Welding Procedures

(a) More than one WPS having different essential, supplementary essential, or nonessential variables may be used in a single production joint. Each WPS may include one or a combination of processes, filler metals, or other variables.

Where more than one WPS specifying different processes, filler metals, or other essential or supplementary essential variables is used in a joint, QW-451 shall be used to determine the range of base metal thickness and
maximum weld metal thickness qualified for each process, filler metal, or set of variables, and those limits shall be observed. Alternatively, qualification of WPSs for root deposits only may be made in accordance with QW-200.4(b).

When following a WPS that has more than one welding process, filler metal, or set of variables, each process, filler metal, or set of variables may be used individually or in different combinations, provided
(1) the essential, nonessential, and required supplementary essential variables associated with the process, filler metal, or set of variables are applied
(2) the base metal and deposited weld metal thickness limits of QW-451 for each process, filler metal, or set of variables are applied.
(b) For GTAW, SMAW, GMAW, PAW, and SAW, or combinations of these processes, a PQR for a process recording a test coupon that was at least $1 / 2 \mathrm{in}$. ( 13 mm ) thick may be combined with one or more other PQRs recording another welding process and any greater base metal thickness. In this case, the process recorded on the first PQR may be used to deposit the root layers using the process(es) recorded on that PQR up to 2 t (for shortcircuiting type of GMAW, see QW-404.32) in thickness on base metal of the maximum thickness qualified by the other PQR(s) used to support the WPS. The requirements of Note (1) of tables QW-451.1 and QW-451.2 shall apply.

## QW-201 Manufacturer's or Contractor's Responsibility

Each manufacturer or contractor shall list the parameters applicable to welding that he performs in construction of weldments built in accordance with this Code. These parameters shall be listed in a document known as a Welding Procedure Specification (WPS).

Each manufacturer or contractor shall qualify the WPS by the welding of test coupons and the testing of specimens (as required in this Code), and the recording of the welding data and test results in a document known as a Procedure Qualification Record (PQR). The welders or welding operators used to produce weldments to be tested for qualification of procedures shall be under the full supervision and control of the manufacturer or contractor during the production of these test weldments. The weldments to be tested for qualification of procedures shall be welded either by direct employees or by individuals engaged by contract for their services as welders or welding operators under the full supervision and control of the manufacturer or contractor. It is not permissible for the manufacturer or contractor to have the supervision and control of welding of the test weldments performed
by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test metal for welding and subsequent work on preparation of test specimens from the completed weldment, performance of nondestructive examination, and mechanical tests, provided the manufacturer or contractor accepts the responsibility for any such work.

The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the weldments to be made in accordance with this Code. If in an organization effective operational control of welding procedure qualification for two or more companies of different names exists, the companies involved shall describe in their Quality Control system/Quality Assurance Program, the operational control of procedure qualifications. In this case separate welding procedure qualifications are not required, provided all other requirements of Section IX are met.

A WPS may require the support of more than one $P Q R$, while alternatively, one $P Q R$ may support a number of WPSs.

The manufacturer or contractor shall certify that he has qualified each Welding Procedure Specification, performed the procedure qualification test, and documented it with the necessary Procedure Qualification Record (PQR).

QW-201.1 The Code recognizes that manufacturers or contractors may maintain effective operational control of PQRs and WPSs under different ownership than existed during the original procedure qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the PQRs and WPSs may be used by the new owner(s) without requalification, provided all of the following are met:
(a) the new owner(s) takes responsibility for the WPSs and PQRs
(b) the WPSs reflect the name of the new owner(s)
(c) the Quality Control System/Quality Assurance Program reflects the source of the PQRs as being from the former manufacturer or contractor

## QW-202 Type of Tests Required

QW-202.1 Mechanical Tests. The type and number of test specimens that shall be tested to qualify a groove weld procedure are given in QW-451, and shall be removed in a manner similar to that shown in QW-463. If any test specimen required by QW-451 fails to meet the applicable acceptance criteria, the test coupon shall be considered as failed.

When it can be determined that the cause of failure is not related to welding parameters, another test coupon may be welded using identical welding parameters.

Alternatively, if adequate material of the original test coupon exists, additional test specimens may be removed as close as practicable to the original specimen location to replace the failed test specimens.

When it has been determined that the test failure was caused by an essential or supplementary essential variable, a new test coupon may be welded with appropriate changes to the variable(s) that was determined to cause the test failure. If the new test passes, the essential and supplementary variables shall be documented on the PQR.

When it is determined that the test failure was caused by one or more welding conditions other than essential or supplementary essential variables, a new test coupon may be welded with the appropriate changes to the welding conditions that were determined to cause the test failure. If the new test passes, the welding conditions that were determined to cause the previous test failure shall be addressed by the manufacturer to ensure that the required properties are achieved in the production weldment.

Where qualification is for fillet welds only, the requirements are given in QW-202.2(c) and (d); and where qualification is for stud welds only, the requirements are given in QW-202.5.

## QW-202.2 Groove and Fillet Welds

(a) Qualification for Groove Full Penetration Welds. Groove-weld test coupons shall qualify the thickness ranges of both base metal and deposited weld metal to be used in production. Limits of qualification shall be in accordance with QW-451. WPS qualification for groove welds shall be made on groove welds using tension and guided-bend specimens. Notch-toughness tests shall be made when required by other Section(s) of the Code. The WPS shall be qualified for use with groove welds within the range of essential variables listed.
(b) Qualification for Partial Penetration Groove Welds. Partial penetration groove welds shall be qualified in accordance with the requirements of QW-451 for both base metal and deposited weld metal thickness, except there need be no upper limit on the base metal thickness provided qualification was made on base metal having a thickness of $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) or more.
(c) Qualification for Fillet Welds. WPS qualification for fillet welds may be made on groove-weld test coupons using test specimens specified in QW-202.2(a) or (b). Fillet-weld procedures so qualified may be used for welding all thicknesses of base metal for all sizes of fillet welds, and all diameters of pipe or tube in accordance with table QW-451.4. Nonpressure-retaining fillet welds,
as defined in other Sections of the Code, may as an alternate be qualified with fillet welds only. Tests shall be made in accordance with QW-180. Limits of qualification shall be in accordance with table QW-451.3.

QW-202.3 Weld Repair and Buildup. WPS qualified on groove welds shall be applicable for weld repairs to groove and fillet welds and for weld buildup under the following provisions:
(a) There is no limitation on the thickness of base metal or deposited weld metal for fillet welds.
(b) For other than fillet welds, the thickness range for base metal and deposited weld metal for each welding process shall be in accordance with QW-451, except there need be no upper limit on the base metal thickness provided qualification was made on base metal having a thickness of $1 \frac{1}{2} \mathrm{in}$. $(38 \mathrm{~mm})$ or more.

QW-202.4 Dissimilar Base Metal Thicknesses. WPS qualified on groove welds shall be applicable for production welds between dissimilar base metal thicknesses provided:
(a) the thickness of the thinner member shall be within the range permitted by QW-451
(b) the thickness of the thicker member shall be as follows:
(1) For P-No. 8, P-No. 41, P-No. 42, P-No. 43, PNo. 44, P-No. 45, P-No. 46, P-No. 49, P-No. 51, P-No. 52, P-No. 53, P-No. 61, and P-No. 62 metal, there shall be no limitation on the maximum thickness of the thicker production member in joints of similar P-Number materials provided qualification was made on base metal having a thickness of $1 / 4 \mathrm{in}$. $(6 \mathrm{~mm})$ or greater.
(2) For all other metal, the thickness of the thicker member shall be within the range permitted by QW-451, except there need be no limitation on the maximum thickness of the thicker production member provided qualification was made on base metal having a thickness of $1 / 2 \mathrm{in}$. (38 mm) or more.

More than one procedure qualification may be required to qualify for some dissimilar thickness combinations.

QW-202.5 Stud Welding. Procedure qualification tests for stud welds shall be made in accordance with QW-192. The procedure qualification tests shall qualify the welding procedures for use within the range of the essential variables of QW-261. For studs welded to other than P-No. 1 metals, five additional welds shall be made and subjected to a macro-test, except that this is not required for studs used for extended heating surfaces.

## QW-203 Limits of Qualified Positions for Procedures

Unless specifically required otherwise by the welding variables (QW-250), a qualification in any position qualifies the procedure for all positions. The welding process and electrodes must be suitable for use in the positions permitted by the WPS. A welder or welding operator making and passing the WPS qualification test is qualified for the position tested. See QW-301.2.

## QW-210 PREPARATION OF TEST COUPON <br> QW-211 Base Metal

The base metals may consist of either plate, pipe, or other product forms. Qualification in plate also qualifies for pipe welding and vice versa. The dimensions of the test coupon shall be sufficient to provide the required test specimens.

## QW-212 Type and Dimensions of Groove Welds

Except as otherwise provided in QW-250, the type and dimensions of the welding groove are not essential variables.

## QW-213 P-No. 11 Base Metals

For vessels or parts of vessels constructed with P-No. 11 base metals, weld grooves for thickness less than $5 / 8$ in. $(16 \mathrm{~mm})$ shall be prepared by thermal processes, when such processes are to be employed during fabrication. This groove preparation shall also include back gouging, back grooving, or removal of unsound weld metal by thermal processes, when these processes are to be employed during fabrication.

## QW-214 Corrosion-Resistant Weld Metal Overlay

QW-214.1 The size of test coupons, limits of qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.

QW-214.2 Essential variables shall be as specified in QW-250 for the applicable welding process.

## QW-215 Electron Beam Welding and Laser Beam Welding

QW-215.1 The WPS qualification test coupon shall be prepared with the joint geometry duplicating that to be used in production. If the production weld is to include a lap-over (completing the weld by rewelding over the
starting area of the weld, as for a girth weld), such lapover shall be included in the WPS qualification test coupon.

QW-215.2 The mechanical testing requirements of QW-451 shall apply.

QW-215.3 Essential variables shall be as specified in tables QW-260 and QW-264 for the applicable welding process.

## QW-216 Hard-Facing Weld Metal Overlay

Hard-Facing Weld Metal Overlay refers to weld deposits made, using a variety of processes, to deter the effects of wear and/or abrasion. The requirements specified in QW-216.1 through QW-216.4 apply regardless of which hard-facing process is used.

QW-216.1 The size of test coupons, limits of qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.

QW-216.2 Welding variables shall be as specified in QW-250 for the applicable process.

QW-216.3 Where Spray Fuse methods of hard-facing (e.g., Oxyfuel and Plasma Arc) are to be used, the coupons for these methods shall be prepared and welding variables applied in accordance with QW-216.1 and QW-216.2, respectively.

QW-216.4 If a weld deposit is to be used under a hard-facing weld metal overlay, a base metal with an assigned P-Number and a chemical analysis nominally matching the weld deposit chemical analysis may be substituted to qualify the PQR .

## QW-217 Joining of Composite (Clad Metals)

The WPS for groove welds in clad metal shall be qualified as provided in $\mathrm{QW}-217$ (a) when any part of the cladding thickness, as permitted by the referencing Code Section, is included in the design calculations. Either QW-217(a) or (b) may be used when the cladding thickness is not included in the design calculations.
(a) The essential and nonessential variables of QW-250 shall apply for each welding process used in production. The procedure qualification test coupon shall be made using the same P-Number base metal, cladding, and welding process, and filler metal combination to be used in production welding. For metal not included in table QW/QB-422, the metal used in the composite test plate shall be within the range of chemical composition of that to be used in production. The qualified thickness range for the base metal and filler metal(s) shall be based
on the actual test coupon thickness for each as applied to QW-451, except that the minimum thickness of filler metal joining the cladding portion of the weldment shall be based on a chemical analysis performed in accordance with table QW-453. Tensile and bend tests required in QW-451 for groove welds shall be made, and they shall contain the full thickness of cladding through the reduced section of the specimen. The bond line between the original cladding and the base metal may be disregarded when evaluating side-bend tests if the cladding was applied by a process other than fusion welding.
(b) The essential and nonessential variables of QW-250 shall apply for each welding process used in production for joining the base metal portion of the weldment. The PQRs that support this portion of the WPS need not be based on test coupons made with clad metal. For the corrosion-resistant overlay portion of the weld, the essential variables of QW-251.4 shall apply and the test coupon and testing shall be in accordance with table QW-453. The WPS shall limit the depth of the groove, which will receive the corrosion-resistant overlay in order to ensure development of the full strength of the underlying weld in the base metal.

## QW-218 Applied Linings

QW-218.1 WPSs for attaching applied linings shall be qualified in accordance with QW-202.2(a), (b), or (c).

QW-218.2 As an alternative to the above, each process to be used in attaching applied linings to base metal shall be qualified on a test coupon welded into the form and arrangement to be used in construction using materials that are within the range of chemical composition of the metal to be used for the base plate, the lining, and the weld metal. The welding variables of QW-250 shall apply except for those regarding base metal or weld metal thickness. Qualification tests shall be made for each position to be used in production welding in accordance with table QW-461.9, except that qualification in the vertical position, uphill progression shall qualify for all positions. One cross-section for each position tested shall be sectioned, polished, and etched to clearly show the demarcation between the base metal and the weld metal. In order to be acceptable, each specimen shall exhibit complete fusion of the weld metal with the base metal and freedom from cracks.

QW-218.3 When chemical analysis of the weld deposit for any elements is required, a chemical analysis shall be performed per table QW-453, Note 9 for those elements.

## QW-219 Flash Welding

Flash welding shall be limited to automatic electrical resistance flash welding of tubular cross-sections. Procedure qualification tests shall be conducted in accordance with QW-199.1.

QW-219.1 Tolerances on Variables. Flash welding variables that may require adjustment during production welding are synergistically related. Accordingly, even though the variables shown in table QW-265 provide tolerances on many welding conditions, the WPS shall specify the same conditions shown on the PQR with tolerance shown for no more than one variable (e.g., if it is desired to provide a tolerance on the upset current, all other variables shown on the WPS must be the same as they are shown on the PQR ). If it is desired to provide tolerances in the WPS for two variables, the first variable with a tolerance shall be set at the midpoint of its tolerance and two test coupons shall be welded with each of the upper and lower extremes of the tolerance for the second variable (i.e., four coupons must be welded). These coupons shall be examined and tested in accordance with QW-199.1.3.

If it is desired to provide tolerance for a third variable, the first two variables shall be set at the midpoint of their tolerance, and two test coupons shall be welded with each of the upper and lower extremes of the new tolerances for the third variable (i.e., four coupons must be welded). These coupons shall be examined and tested in accordance with QW-199.1.3.

No more than three essential variables on a WPS may show tolerances.

Production tests conducted in accordance with the requirements of other Sections may be used to satisfy this requirement.

## QW-250 WELDING VARIABLES QW-251 General

QW-251.1 Types of Variables for Welding Procedure Specifications (WPS). These variables (listed for each welding process in tables QW-252 through QW-265) are subdivided into essential variables, supplementary essential variables, and nonessential variables (QW-401). The "Brief of Variables" listed in the Tables are for reference only. See the complete variable in Welding Data of Article IV.

QW-251.2 Essential Variables. Essential variables are those in which a change, as described in the specific variables, is considered to affect the mechanical proper-
ties of the weldment, and shall require requalification of the WPS.

Supplementary essential variables are required for metals for which other Sections specify notch-toughness tests and are in addition to the essential variables for each welding process.

QW-251.3 Nonessential Variables. Nonessential variables are those in which a change, as described in the specific variables, may be made in the WPS without requalification.

## QW-251.4 Special Processes

(a) The special process essential variables for corro-sion-resistant and hard-surfacing weld metal overlays are as indicated in the following tables for the specified process. Only the variables specified for special processes shall apply. A change in the corrosion-resistant or hardsurfacing welding process shall require requalification.
(b) WPS qualified for corrosion-resistant and hardsurfacing overlay welding, in accordance with other Sections when such qualification rules were included in those Sections, may be used with the same provisions as provided in QW-100.3.

QW-252
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Oxyfuel Gas Welding (OFW)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 |  | Groove design |  |  | X |
|  | . 2 |  | Backing |  |  | X |
|  | . 3 |  | Backing comp. |  |  | X |
|  | . 10 |  | Roof spacing |  |  | X |
| QW-403 <br> Base Metals | . 1 | $\phi$ | P-Number | X |  |  |
|  | . 2 |  | Max. $T$ Qualified | X |  |  |
|  | . 13 |  | P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 3 |  | Size |  |  | X |
|  | . 4 |  | F-Number | X |  |  |
|  | . 5 |  | A-Number | X |  |  |
|  | . 12 |  | Classification | X |  |  |
| QW-405 Positions | . 1 |  | Position |  |  | X |
| QW-406 <br> Preheat | . 1 |  | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ |  |  | X |
| QW-407 <br> PWHT | . 1 |  | PWHT | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 7 | $\phi$ | Type fuel gas | X |  |  |
| QW-410 <br> Technique | . 1 |  | String/weave |  |  | X |
|  | . 2 |  | Flame characteristics |  |  | X |
|  | . 4 |  | $\rightarrow$ Technique |  |  | X |
|  | . 5 |  | Method cleaning |  |  | X |
|  | . 26 |  | Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion | $>$ Increase/greater than <br> < Decrease/less than |  |  |  | Forehand Backhand | $\phi$ Change |

## WELDING PROCEDURE QUALIFICATIONS

QW-252.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Oxyfuel Gas Welding (OFW)


QW-253
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Shielded Metal-Arc Welding (SMAW)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ Groove design |  |  | X |
|  | . 4 | - Backing |  |  | X |
|  | . 10 | $\phi$ Root spacing |  |  | X |
|  | . 11 | $\pm$ Retainers |  |  | X |
| QW-403 <br> Base <br> Metals | . 5 | $\phi$ Group Number |  | X |  |
|  | . 6 | $T$ Limits impact |  | X |  |
|  | . 7 | T/t Limits > 8 in. (200 mm) | X |  |  |
|  | . 8 | $\phi \quad T$ Qualified | X |  |  |
|  | . 9 | $t$ Pass > $1 / 2$ in. (13 mm) | X |  |  |
|  | . 11 | $\phi \quad \mathrm{P}$-No. qualified | X |  |  |
|  | . 13 | $\phi$ P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 4 | $\phi \quad$ F-Number | X |  |  |
|  | . 5 | $\phi$ A-Number | X |  |  |
|  | . 6 | $\phi$ Diameter |  |  | X |
|  | . 7 | $\phi$ Diameter $>1 / 4 \mathrm{in}$. $(6 \mathrm{~mm}$ ) |  | X |  |
|  | . 12 | $\phi$ Classification |  | X |  |
|  | . 30 | $\phi t$ | X |  |  |
|  | . 33 | $\phi$ Classification |  |  | X |
| QW-405 <br> Positions | . 1 | + Position |  |  | X |
|  | . 2 | $\phi$ Position |  | X |  |
|  | . 3 | $\phi \uparrow \downarrow$ Vertical welding |  |  | X |
| QW-406 Preheat | . 1 | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
|  | . 2 | $\phi \quad$ Preheat maint. |  |  | X |
|  | . 3 | Increase $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right.$ ) (IP) |  | X |  |
| $\begin{aligned} & \text { QW-407 } \\ & \text { PWHT } \end{aligned}$ | . 1 | $\phi$ PWHT | X |  |  |
|  | . 2 | $\phi$ PWHT (T \& T range) |  | X |  |
|  | . 4 | $T$ Limits | X |  |  |
| QW-409 <br> Electrical Characteristics | . 1 | $>$ Heat input |  | X |  |
|  | . 4 | $\phi$ Current or polarity |  | X | X |
|  | . 8 | $\phi$ I \& E range |  |  | X |
| QW-410 <br> Technique | . 1 | $\phi$ String/weave |  |  | $x$ |
|  | . 5 | $\phi$ Method cleaning |  |  | $x$ |
|  | . 6 | $\phi$ Method back gouge |  |  | X |
|  | . 9 | $\phi$ Multiple to single pass/side |  | X | X |
|  | . 25 | $\phi$ Manual or automatic |  |  | X |
|  | . 26 | $\pm$ Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion | $\begin{aligned} & \text { creas } \\ & \text { creas } \end{aligned}$ | than $\uparrow$ Uphill $\leftarrow$ <br> an $\downarrow$ Downhill $\rightarrow$ | $\phi$ Change |  |  |

## WELDING PROCEDURE QUALIFICATIONS

QW-253.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Shielded Metal-Arc Welding (SMAW)

| Special Process Variables |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Paragraph |  | Essential Variables |  |  |  | Nonessential Variables for HFO and CRO |
|  |  |  | Hard-Facing Overlay (HFO) (QW-216) |  | Corrosion-Resistant Overlay (CRO) (QW-214) |  |
| QW-402 Joints | . 16 | < | Finished $t$ | < | Finished $t$ |  |
| QW-403 | . 20 | $\phi$ | P-Number | $\phi$ | P-Number |  |
| Metals | . 23 | $\phi$ | $T$ Qualified | $\phi$ | $T$ Qualified |  |
| QW-404 <br> Filler <br> Metals | . 12 | $\phi$ | Classification |  |  |  |
|  | . 37 |  |  | $\phi$ | A-Number |  |
|  | . 38 |  |  |  |  | $\phi$ Diameter (1st layer) |
| QW-405 <br> Positions | . 4 | + | Position | + | Position |  |
| QW-406 Preheat | . 4 |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat <br> $>$ Interpass |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat <br> $>$ Interpass |  |
| QW-407 PWHT | . 6 | $\phi$ | PWHT |  |  |  |
|  | . 9 |  |  | $\phi$ | PWHT |  |
| QW-409 <br> Electrical Characteristics | . 4 | $\phi$ | Current or polarity | $\phi$ | Current or polarity |  |
|  | . 22 |  | Inc. > 10\% 1st layer |  | Inc. > 10\% 1st layer |  |
| QW-410 <br> Technique | . 1 |  |  |  |  | $\phi$ String/weave |
|  | . 5 |  |  |  |  | $\phi$ Method of cleaning |
|  | . 26 |  |  |  |  | $\pm$ Peening |
|  | . 38 | $\phi$ | Multiple to single layer |  | Multiple to single layer |  |


| Legend: |  |  |  |
| :--- | :--- | :--- | :--- |
| + Addition | $>$ Increase/greater than | $\uparrow$ Uphill | $\leftarrow$ Forehand |$\quad \phi$ Change

QW-254
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Submerged-Arc Welding (SAW)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ Groove design |  |  | X |
|  | . 4 | - Backing |  |  | X |
|  | . 10 | $\phi$ Root spacing |  |  | X |
|  | . 11 | $\pm$ Retainers |  |  | X |
| QW-403 <br> Base <br> Metals | . 5 | $\phi$ Group Number |  | X |  |
|  | . 6 | $T$ Limits |  | X |  |
|  | . 7 | T/t Limits > 8 in . $(200 \mathrm{~mm}$ ) | X |  |  |
|  | . 8 | $\phi \quad T$ Qualified | X |  |  |
|  | . 9 | $t$ Pass $>1 / 2$ in. $(13 \mathrm{~mm})$ | X |  |  |
|  | . 11 | $\phi$ P-No. qualified | X |  |  |
|  | . 13 | $\phi$ P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 4 | $\phi$ F-Number | X |  |  |
|  | . 5 | $\phi$ A-Number | X |  |  |
|  | . 6 | $\phi$ Diameter |  |  | X |
|  | . 9 | $\phi$ Flux/wire class. | X |  |  |
|  | . 10 | $\phi$ Alloy flux | X |  |  |
|  | . 24 | $\pm$ Supplemental <br> $\phi$ | X |  |  |
|  | . 27 | $\phi$ Alloy elements | X |  |  |
|  | . 29 | $\phi$ Flux designation |  |  | X |
|  | . 30 | $\phi t$ | X |  |  |
|  | . 33 | $\phi$ Classification |  |  | X |
|  | . 34 | $\phi$ Flux type | X |  |  |
|  | . 35 | $\phi$ Flux/wire class. |  | X | X |
|  | . 36 | Recrushed slag | X |  |  |
| QW-405 <br> Positions | . 1 | + Position |  |  | X |
| QW-406 Preheat | . 1 | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
|  | . 2 | $\phi$ Preheat maint. |  |  | X |
|  | . 3 | Increase $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)($ IP ) |  | X |  |
| $\begin{aligned} & \text { QW-407 } \\ & \text { PWHT } \end{aligned}$ | . 1 | $\phi$ PWHT | X |  |  |
|  | . 2 | $\phi$ PWHT (T \& T range) |  | X |  |
|  | . 4 | $T$ Limits | X |  |  |
| QW-409 <br> Electrical <br> Characteristics | . 1 | $>$ Heat input |  | X |  |
|  | . 4 | $\phi$ Current or polarity |  | X | X |
|  | . 8 | $\phi$ I \& E range |  |  | X |

## WELDING PROCEDURE QUALIFICATIONS

QW-254
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Submerged-Arc Welding (SAW) (Cont'd)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-410 <br> Technique | . 1 | $\phi$ String/weave |  |  | X |
|  | . 5 | $\phi$ Method cleaning |  |  | X |
|  | . 6 | $\phi$ Method back gouge |  |  | X |
|  | . 7 | $\phi$ Oscillation |  |  | x |
|  | . 8 | $\phi$ Tube-work distance |  |  | X |
|  | . 9 | $\phi$ Multi to single pass/side |  | X | X |
|  | . 10 | $\phi$ Single to multi electrodes |  | X | X |
|  | . 15 | $\phi$ Electrode spacing |  |  | X |
|  | . 25 | $\phi$ Manual or automatic |  |  | X |
|  | . 26 | $\pm$ Peening |  |  | X |
| Legend: <br> + Addition > Increase/greater than $\uparrow$ Uphill <br> - Deletion < Decrease/less than $\downarrow$ Downhill |  |  | $\leftarrow$ Forehand $\quad \phi$ <br> $\rightarrow$ Backhand | hange |  |

QW-254.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Submerged-Arc Welding (SAW)

| Special Process Variables |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Paragraph |  | Essential Variables |  |  |  | Nonessential Variables for HFO and CRO |
|  |  |  | Hard-Facing Overlay (HFO) (QW-216) |  | Corrosion-Resistant Overlay (CRO) (QW-214) |  |
| QW-402 Joints | . 16 | $<$ | Finished $t$ | $<$ | Finished $t$ |  |
| QW-403 <br> Base <br> Metals | . 20 | $\phi$ | P-Number | $\phi$ | P-Number |  |
|  | . 23 | $\phi$ | $T$ Qualified | $\phi$ | $T$ Qualified |  |
| QW-404 <br> Filler <br> Metals | . 6 |  |  |  |  | $\phi$ Nominal size of electrode |
|  | . 12 | $\phi$ | Classification |  |  |  |
|  | . 24 | $\pm$ | or $\phi>10 \%$ in supplemental filler metal | $\pm$ | or $\phi>10 \%$ in supplemental filler metal |  |
|  | . 27 | $\phi$ | Alloy elements |  |  |  |
|  | . 37 |  |  | $\phi$ | A-Number |  |
|  | . 39 | $\phi$ | Nominal flux comp. | $\phi$ | Nominal flux comp. |  |
| QW-405 <br> Positions | . 4 | + | Position | + | Position |  |
| QW-406 <br> Preheat | . 4 |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass |  |
| $\begin{aligned} & \text { QW-407 } \\ & \text { PWHT } \end{aligned}$ | . 6 | $\phi$ | PWHT |  |  |  |
|  | . 9 |  |  | $\phi$ | PWHT |  |
| QW-409 <br> Electrical <br> Characteristics | . 4 | $\phi$ | Current or polarity | $\phi$ | Current or polarity |  |
|  | . 26 |  | $\begin{aligned} & \text { lst layer - Heat input } \\ & >10 \% \end{aligned}$ |  | $\begin{aligned} & \text { lst layer - Heat input } \\ & >10 \% \end{aligned}$ |  |
| QW-410 <br> Technique | . 1 |  |  |  |  | $\phi$ String/weave |
|  | . 5 |  |  |  |  | $\phi$ Method of cleaning |
|  | . 7 |  |  |  |  | $\phi$ Oscillation |
|  | . 8 |  |  |  |  | $\phi$ Tube to work distance |
|  | . 15 |  |  |  |  | $\phi$ Electrode spacing |
|  | . 25 |  |  |  |  | $\phi$ Manual or automatic |
|  | . 26 |  |  |  |  | $\pm$ Peening |
|  | . 38 | $\phi$ | Multiple to single layer | $\phi$ | Multiple to single layer |  |
|  | . 40 |  |  | - | Supplemental device |  |
|  | . 50 | $\phi$ | No. of electrodes | $\phi$ | No. of electrodes |  |

Legend:

| + Addition | $>$ Increase/greater than | $\uparrow$ Uphill | $\leftarrow$ Forehand |
| :--- | :--- | :--- | :--- |$\quad \phi$ Change

## WELDING PROCEDURE QUALIFICATIONS

QW-255
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Metal-Arc Welding (GMAW and FCAW)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 Joints | . 1 | $\phi$ Groove design |  |  | X |
|  | . 4 | - Backing |  |  | X |
|  | . 10 | $\phi$ Root spacing |  |  | X |
|  | . 11 | $\pm$ Retainers |  |  | X |
| QW-403 <br> Base Metals | . 5 | $\phi$ Group Number |  | x |  |
|  | . 6 | $T$ Limits |  | X |  |
|  | . 7 | T/t Limits > 8 in. (200 mm) | X |  |  |
|  | . 8 | $\phi T$ Qualified | X |  |  |
|  | . 9 | $t$ Pass $>1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$ | X |  |  |
|  | . 10 | $T$ limits (S. cir. arc) | X |  |  |
|  | . 11 | $\phi$ P-No. qualified | X |  |  |
|  | . 13 | $\phi$ P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 4 | $\phi$ F-Number | $x$ |  |  |
|  | . 5 | $\phi$ A-Number | X |  |  |
|  | . 6 | $\phi$ Diameter |  |  | X |
|  | . 12 | $\phi$ Classification |  | X |  |
|  | . 23 | $\phi$ Filler metal product form | $x$ |  |  |
|  | . 24 | $\pm \text { Supplemental }$ | X |  |  |
|  | . 27 | $\phi$ Alloy elements | X |  |  |
|  | . 30 | $\phi t$ | X |  |  |
|  | . 32 | $t$ Limits (S. cir. arc) | X |  |  |
|  | . 33 | $\phi$ Classification |  |  | X |
| QW-405 <br> Positions | . 1 | + Position |  |  | X |
|  | . 2 | $\phi$ Position |  | X |  |
|  | . 3 | $\phi \uparrow \downarrow$ Vertical welding |  |  | X |
| QW-406 <br> Preheat | . 1 | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
|  | . 2 | $\phi$ Preheat maint. |  |  | X |
|  | . 3 | Increase $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)(\mathrm{IP})$ |  | X |  |
| QW-407 PWHT | . 1 | $\phi$ PWHT | X |  |  |
|  | . 2 | $\phi$ PWHT (T \& T range) |  | X |  |
|  | . 4 | $T$ Limits | X |  |  |

QW-255
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Gas Metal-Arc Welding (GMAW and FCAW) (Cont'd)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential <br> X |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 1 | $\pm$ Trail or $\phi$ comp. |  |  |  |
|  | . 2 | $\phi$ Single, mixture, or \% | X |  |  |
|  | . 3 | $\phi$ Flow rate |  |  | X |
|  | . 5 | $\pm$ or $\phi$ Backing flow |  |  | X |
|  | . 9 | - Backing or $\phi$ comp. | X |  |  |
|  | . 10 | $\phi$ Shielding or trailing | X |  |  |
| QW-409 <br> Electrical <br> Characteristics | . 1 | $>$ Heat input |  | X |  |
|  | . 2 | $\phi$ Transfer mode | X |  |  |
|  | . 4 | $\phi$ Current or polarity |  | X | $x$ |
|  | . 8 | $\phi$ I \& E range |  |  | X |
| QW-410 <br> Technique | . 1 | $\phi$ String/weave |  |  | X |
|  | . 3 | $\phi$ Orifice, cup, or nozzle size |  |  | X |
|  | . 5 | $\phi$ Method cleaning |  |  | X |
|  | . 6 | $\phi$ Method back gouge |  |  | X |
|  | . 7 | $\phi$ Oscillation |  |  | X |
|  | . 8 | $\phi$ Tube-work distance |  |  | X |
|  | . 9 | $\phi$ Multiple to single pass/side |  | X | X |
|  | . 10 | $\phi$ Single to multiple electrodes |  | $X$ | X |
|  | . 15 | $\phi$ Electrode spacing |  |  | X |
|  | . 25 | $\phi$ Manual or automatic |  |  | X |
|  | . 26 | $\pm$ Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion | creas | than $\uparrow$ Uphill <br> an $\downarrow$ Downhill |  |  |  |

WELDING PROCEDURE QUALIFICATIONS
QW-255.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Metal-Arc Welding (GMAW and FCAW)

| Special Process Variables |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Paragraph |  | Essential Variables |  |  |  | Nonessential Variables for HFO and CRO |
|  |  |  | Hard-Facing Overlay (HFO) (QW-216) |  | Corrosion-Resistant Overlay (CRO) (QW-214) |  |
| QW-402 <br> Joints | . 16 | < | Finished $t$ | < | Finished $t$ |  |
| QW-403 <br> Base <br> Metals | . 20 | $\phi$ | P-Number | $\phi$ | P-Number |  |
|  | . 23 | $\phi$ | $T$ Qualified | $\phi$ | $T$ Qualified |  |
| QW-404 <br> Filler <br> Metals | . 6 |  |  |  |  | $\phi$ Nominal size of electrode |
|  | . 12 | $\phi$ | Classification |  |  |  |
|  | . 23 | $\phi$ | Filler metal product form | $\phi$ | Filler metal product form |  |
|  | . 24 | $\pm$ | or $\phi>10 \%$ in supplemental filler metal | $\pm$ | or $\phi>10 \%$ in supplemental filler metal |  |
|  | . 27 | $\phi$ | Alloy elements |  |  |  |
|  | . 37 |  |  | $\phi$ | A-Number |  |
| QW-405 <br> Positions | . 4 | + | Position | + | Position |  |
| QW-406 <br> Preheat | . 4 |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat $>$ Interpass |  | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass |  |
| $\begin{aligned} & \text { QW-407 } \\ & \text { PWHT } \end{aligned}$ | . 6 | $\phi$ | PWHT |  |  |  |
|  | . 9 |  |  | $\phi$ | PWHT |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 2 | $\phi$ | Single, mixture, or \% | $\phi$ | Single, mixture, or \% |  |
|  | . 3 |  |  |  |  | $\phi$ Flow rate |
| $\begin{aligned} & \text { QW-409 } \\ & \text { Electrical } \\ & \text { Characteristics } \end{aligned}$ | . 4 | $\phi$ | Current or polarity | $\phi$ | Current or polarity |  |
|  | . 26 |  | $\begin{aligned} & \text { 1st layer - Heat input } \\ & >10 \% \end{aligned}$ |  | $\begin{aligned} & \text { 1st layer - Heat input } \\ & >10 \% \end{aligned}$ |  |
| QW-410 <br> Technique | . 1 |  |  |  |  | $\phi$ String/weave |
|  | . 3 |  |  |  |  | $\phi$ Orifice/cup or nozzle size |
|  | . 5 |  |  |  |  | $\phi$ Method of cleaning |
|  | . 7 |  |  |  |  | $\phi$ Oscillation |
|  | . 8 |  |  |  |  | $\phi$ Tube to work distance |
|  | . 25 |  |  |  |  | $\phi$ Manual or automatic |
|  | . 26 |  |  |  |  | $\pm$ Peening |
|  | . 38 | $\phi$ | Multiple to single Iayer | $\phi$ | Multiple to single layer |  |
|  | . 50 | $\phi$ | No. of electrodes | $\phi$ | No. of electrodes |  |
| Legend: <br> + Addition <br> - Deletion | $>$ Increase/greater than $\uparrow$ Uphill <br> < Decrease/less than $\downarrow$ Downhill |  |  | $\underset{\rightarrow}{\leftarrow} \text { Forehand Backhand } \quad \phi \text { Change }$ |  |  |

QW-256
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW)

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ Groove design |  |  | X |
|  | . 5 | + Backing |  |  | X |
|  | . 10 | $\phi$ Root spacing |  |  | X |
|  | . 11 | $\pm$ Retainers |  |  | X |
| QW-403 <br> Base <br> Metals | . 5 | $\phi$ Group Number |  | X |  |
|  | . 6 | $T$ Limits |  | X |  |
|  | . 7 | T/t Limits > 8 in. ( 200 mm ) | X |  |  |
|  | . 8 | $\phi \quad T$ Qualified | X |  |  |
|  | . 11 | $\phi$ P-No. qualified | X |  |  |
|  | . 13 | $\phi$ P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 3 | $\phi$ Size |  |  | X |
|  | . 4 | $\phi$ F-Number | X |  |  |
|  | . 5 | $\phi$ A-Number | X |  |  |
|  | . 12 | $\phi$ Classification |  | X |  |
|  | . 14 | $\pm$ Filler | X |  |  |
|  | . 22 | $\pm$ Consum. insert |  |  | X |
|  | . 23 | $\phi$ Filler metal product form | X |  |  |
|  | . 30 | $\phi t$ | X |  |  |
|  | . 33 | $\phi$ Classification |  |  | X |
|  | . 50 | $\pm$ Flux |  |  | X |
| QW-405 <br> Positions | . 1 | + Position |  |  | X |
|  | . 2 | $\phi$ Position |  | X |  |
|  | . 3 | $\phi \uparrow \downarrow$ Vertical welding |  |  | X |
| QW-406 <br> Preheat | . 1 | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
|  | . 3 | $\begin{aligned} & \text { Increase }>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right) \\ & (I P) \end{aligned}$ |  | X |  |
| QW-407 <br> PWHT | . 1 | $\phi$ PWHT | X |  |  |
|  | . 2 | $\phi$ PWHT (T \& T range) |  | X |  |
|  | . 4 | $T$ Limits | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 1 | $\pm$ Trail or $\phi$ comp. |  |  | X |
|  | . 2 | $\phi$ Single, mixture, or \% | X |  |  |
|  | . 3 | $\phi$ Flow rate |  |  | X |
|  | . 5 | $\pm$ or $\phi$ Backing flow |  |  | X |
|  | . 9 | - Backing or $\phi$ comp. | X |  |  |
|  | . 10 | $\phi$ Shielding or trailing | X |  |  |

## WELDING PROCEDURE QUALIFICATIONS

QW-256

## WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW) (Cont'd)

| Paragraph |  | Brief of Variables |  | Essential | Supplementary <br> Essential <br> $x$ | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-409 <br> Electrical Characteristics | . 1 |  | Heat input |  |  |  |
|  | . 3 | $\pm$ | Pulsing I |  |  | X |
|  | . 4 | $\phi$ | Current or polarity |  | X | X |
|  | . 8 | $\phi$ | I \& E range |  |  | X |
|  | . 12 | $\phi$ | Tungsten electrode |  |  | X |
| QW-410 <br> Technique | . 1 | $\phi$ | String/weave |  |  | X |
|  | . 3 | $\phi$ | Orifice, cup, or nozzle size |  |  | X |
|  | . 5 | $\phi$ | Method cleaning |  |  | X |
|  | . 6 | $\phi$ | Method back gouge |  |  | X |
|  | . 7 | $\phi$ | Oscillation |  |  | X |
|  | . 9 | $\phi$ | Multi to single pass/side |  | X | X |
|  | . 10 | $\phi$ | Single to multi electrodes |  | X | X |
|  | . 11 | $\phi$ | Closed to out chamber | X |  |  |
|  | . 15 | $\phi$ | Electrode spacing |  |  | X |
|  | . 25 | $\phi$ | Manual or automatic |  |  | X |
|  | . 26 |  | Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion |  | ncre Decre | se/greater than $\uparrow$ Up <br>  $\downarrow$ Doss than | $\stackrel{\leftarrow}{\rightarrow}$ | Forehand <br> Backhand | $\phi$ Change |

## QW-256.1

WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW)


## WELDING PROCEDURE QUALIFICATIONS

QW-257
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Plasma-Arc Welding (PAW)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ | Groove design |  | X |  |
|  | . 5 | + | Backing |  |  | X |
|  | . 10 | $\phi$ | Root spacing |  |  | X |
|  | . 11 | $\pm$ | Retainers |  |  | X |
| QW-403 <br> Base Metals | . 5 | $\phi$ | Group Number |  | X |  |
|  | . 6 |  | $T$ Limits |  | X |  |
|  | . 8 | $\phi$ | $T$ Qualified | X |  |  |
|  | . 12 | $\phi$ | P-Number/melt-in | X |  |  |
|  | . 13 | $\phi$ | P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler Metals | . 3 | $\phi$ | Size |  |  | X |
|  | . 4 | $\phi$ | F-Number | X |  |  |
|  | . 5 | $\phi$ | A-Number | X |  |  |
|  | . 12 | $\phi$ | Classification |  | X |  |
|  | . 14 | $\pm$ | Filler metal | X |  |  |
|  | . 22 | $\pm$ | Consum. insert |  |  | X |
|  | . 23 | $\phi$ | Filler metal product form | X |  |  |
|  | . 27 | $\phi$ | Alloy elements | X |  |  |
|  | . 30 | $\phi$ | $t$ | X |  |  |
|  | . 33 | $\phi$ | Classification |  |  | X |
| QW-405 <br> Positions | . 1 | + | Position |  |  | X |
|  | . 2 | $\phi$ | Position |  | X |  |
|  | . 3 | $\phi$ | $\uparrow \downarrow$ Vertical welding |  |  | X |
| QW-406 <br> Preheat | . 1 |  | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
|  | . 3 |  | Increase $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)(\mathrm{IP})$ |  | X |  |
| $\begin{aligned} & \text { QW-407 } \\ & \text { PWHT } \end{aligned}$ | . 1 | $\phi$ | PWHT | X |  |  |
|  | . 2 | $\phi$ | PWHT ( T \& T range) |  | X |  |
|  | . 4 |  | $T$ Limits | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 1 | $\pm$ | Trail or $\phi$ comp. |  |  | X |
|  | . 4 | $\phi$ | Composition | X |  |  |
|  | . 5 | $\pm$ | Or $\phi$ backing flow |  |  | X |
|  | . 9 | - | Backing or $\phi$ comp. | X |  |  |
|  | . 10 | $\phi$ | Shielding or trailing | X |  |  |
|  | . 21 | $\phi$ | Flow rate |  |  | X |

QW-257
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Plasma-Arc Welding (PAW) (CONT'D)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-409 <br> Electrical <br> Characteristics | . 1 | > | Heat input |  | X |  |
|  | . 4 | $\phi$ | Current or polarity |  | X | X |
|  | . 8 | $\phi$ | I \& E range |  |  | $X$ |
|  | . 12 | $\phi$ | Tungsten electrode |  |  | X |
| QW-410 <br> Technique | . 1 | $\phi$ | String/weave |  |  | X |
|  | . 3 | $\phi$ | Orifice, cup, or nozzle size |  |  | X |
|  | . 5 | $\phi$ | Method cleaning |  |  | X |
|  | . 6 | $\phi$ | Method back gouge |  |  | X |
|  | . 7 | $\phi$ | Oscillation |  |  | X |
|  | . 9 | $\phi$ | Multiple to single pass/side |  | X | X |
|  | . 10 | $\phi$ | Single to multiple electrodes |  | X | X |
|  | . 11 | $\phi$ | Closed to out chamber | X |  |  |
|  | . 12 | $\phi$ | Melt-in to keyhole |  | X |  |
|  | . 15 | $\phi$ | Electrode spacing |  |  | X |
|  | . 26 | $\pm$ | Peening |  |  | X |

Legend:

+ Addition $>$ Increase/greater than $\uparrow$ Uphill $\leftarrow$ Forehand $\phi$ Change
- Deletion < Decrease/less than $\downarrow$ Downhill $\rightarrow$ Backhand


## WELDING PROCEDURE QUALIFICATIONS

QW-257.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Plasma-Arc Welding (PAW)

| Special Process Variables |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Paragraph |  | Essential Variables |  |  | Nonessential Variables for HFO, CRO, and HFSF |
|  |  | Hard-Facing Overlay (HFO) (QW-216) | Corrosion-Resistant Overlay (CRO) (QW-214) | Hard-Facing Spray Fuse (HFSF) (QW-216) |  |
| QW-402 <br> Joints | . 16 | < Finished $t$ | < Finished $t$ |  |  |
|  | . 17 |  |  | > Finished $t$ |  |
| QW-403 <br> Base Metals | . 20 | $\phi$ P-Number | $\phi$ P-Number | $\phi$ P-Number |  |
|  | . 23 | $\phi T$ Qualified | $\phi T$ Qualified |  |  |
| QW-404 <br> Filler Metals | . 12 | $\phi$ Classification |  | $\phi$ Classification |  |
|  | . 14 | $\pm$ Filler metal | $\pm$ Filler metal |  |  |
|  | . 37 |  | $\phi$ A-Number |  |  |
|  | . 41 | $\phi>10 \%$ Powder feed rate | $\phi>10 \%$ Powder feed rate |  |  |
|  | . 42 |  |  | $\phi>5 \%$ Particle size |  |
|  | . 43 | $\phi$ Particle size | $\phi$ Particle size |  |  |
|  | . 44 | $\phi$ Powder type | $\phi$ Powder type |  |  |
|  | . 45 | $\phi$ Filler metal form | $\phi$ Filler metal form |  |  |
|  | . 46 |  |  | $\phi$ Powder feed rate |  |
| QW-405 <br> Positions | . 4 | + Position | + Position | + Position |  |
| QW-406 <br> Preheat | . 4 | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat > Interpass |  |
|  | . 5 |  |  | $\phi$ Preheat maintenance |  |
| QW-407 <br> PWHT | . 6 | $\phi$ PWHT |  | $\phi$ PWHT |  |
|  | . 7 |  |  | $\phi$ PWHT after fusing |  |
|  | . 9 |  | $\phi$ PWHT |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 1 |  |  |  | $\pm$ Trail or $\phi$ comp. |
|  | . 16 | $\phi>5 \%$ Arc or metal feed gas | $\phi>5 \%$ Arc or metal feed gas | $\phi>5 \%$ Arc or metal feed gas |  |
|  | . 17 | $\phi$ Type or mixture | $\phi$ Type or mixture |  |  |
|  | . 18 | $\phi>10 \%$ Mix. comp. | $\phi>10 \%$ Mix. comp. |  |  |
|  | . 19 |  |  | $\phi$ Plasma/feed gas comp. |  |
|  | . 20 |  |  | $\phi$ Plasma gas flow-rate range |  |
| QW-409 <br> Electrical Characteristics | . 4 | $\phi$ Current or polarity | $\phi$ Current or polarity |  |  |
|  | 12 |  |  | $\phi$ Type or size of electrode |  |
|  | . 23 |  |  | $\phi>10 \%$ I \& E |  |
|  | . 24 | $\phi>10 \%$ Filler wire watt. | $\phi>10 \%$ Filler wire watt. |  |  |
|  | . 25 | $\phi>10 \%$ I \& E | $\phi>10 \%$ I \& E |  |  |

QW-257.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Plasma-Arc Welding (PAW) (CONT'D)


## WELDING PROCEDURE QUALIFICATIONS

QW-258
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Electroslag Welding (ESW)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ | Groove design |  |  | X |
|  | . 10 | $\phi$ | Root spacing |  |  | X |
|  | . 11 | $\pm$ | Retainers | X |  |  |
| QW-403 <br> Base <br> Metals | . 1 | $\phi$ | P-Number | X |  |  |
|  | . 4 | $\phi$ | Group Number |  | X |  |
|  | . 9 |  | $t$ Pass > $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm}$ ) | X |  |  |
|  | . 13 | $\phi$ | P-No. 5/9/10 | X |  |  |
| $\begin{aligned} & \text { QW-404 } \\ & \text { Filler } \\ & \text { Metals } \end{aligned}$ | . 4 | $\phi$ | F-Number | x |  |  |
|  | . 5 | $\phi$ | A-Number | X |  |  |
|  | . 6 | $\phi$ | Diameter |  |  | X |
|  | . 12 | $\phi$ | Classification |  | x |  |
|  | . 17 | $\phi$ | Flux type or comp. | x |  |  |
|  | . 18 | $\phi$ | Wire to plate | X |  |  |
|  | . 19 | $\phi$ | Consum. guide | X |  |  |
|  | . 33 | $\phi$ | Classification |  |  | X |
| QW-407 <br> PWHT | . 1 | $\phi$ | PWHT | x |  |  |
|  | . 2 | $\phi$ | PWHT (T \& T range) |  | x |  |
|  | . 4 |  | $T$ Limits | X |  |  |
| QW-409 <br> Electrical Characteristics | . 5 | $\phi$ | $\pm 15 \%$ I \& E range | X |  |  |
| QW-410 <br> Technique | . 5 | $\phi$ | Method cleaning |  |  | X |
|  | . 7 | $\phi$ | Oscillation | X |  |  |
|  | . 10 | $\phi$ | Single to multiple electrodes | X |  |  |
|  | . 15 | $\phi$ | Electrode spacing |  |  | X |
|  | . 26 | $\pm$ | Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion |  | cre | ase/greater than $\uparrow$ Up <br> ase/less than $\downarrow$ Do |  | Forehand Backhand | $\phi$ Change |

QW-258.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Electroslag Welding (ESW)


## WELDING PROCEDURE QUALIFICATIONS

QW-259
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Electrogas Welding (EGW)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 |  | Groove design |  |  | X |
|  | . 10 |  | Root spacing |  |  | X |
|  | . 11 | $\pm$ | Retainers | X |  |  |
| QW-403 <br> Base <br> Metals | . 1 | $\phi$ | P-Number | X |  |  |
|  | . 5 | $\phi$ | Group Number |  | X |  |
|  | . 6 |  | $T$ Limits |  | X |  |
|  | . 8 | $\phi$ | $T$ Qualified | X |  |  |
|  | . 9 |  | $t$ Pass > $1 / 2$ in. ( 13 mm ) | X |  |  |
|  | . 13 | $\phi$ | P-No. 5/9/10 | X |  |  |
| QW-404 <br> Filler <br> Metals | . 4 | $\phi$ | F-Number | X |  |  |
|  | . 5 | $\phi$ | A-Number | X |  |  |
|  | . 6 | $\phi$ | Diameter |  |  | X |
|  | . 12 | $\phi$ | Classification |  | X |  |
|  | . 23 | $\phi$ | Filler metal product form | X |  |  |
|  | . 33 | $\phi$ | Classification |  |  | X |
| QW-406 <br> Preheat | . 1 |  | crease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ |  |  | X |
| QW-407 <br> PWHT | . 1 | $\phi$ | PWHT | X |  |  |
|  | . 2 | $\phi$ | PWHT (T \& T range) |  | X |  |
|  | . 4 |  | $T$ Limits | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 2 | $\phi$ | Single, mixture, or \% | x |  |  |
|  | . 3 | $\phi$ | Flow rate |  |  | X |
| QW-409 <br> Electrical Characteristics | . 1 | > | Heat input |  | x |  |
|  | . 4 | $\phi$ | Current or polarity |  | X | X |
|  | . 8 | $\phi$ | I \& E range |  |  | X |
| QW-410 <br> Technique | . 5 | $\phi$ | Method cleaning |  |  | X |
|  | . 7 | $\phi$ | Oscillation |  |  | X |
|  | . 8 | $\phi$ | Tube-work distance |  |  | X |
|  | . 9 | $\phi$ | Multiple to single pass/side |  | X | X |
|  | . 10 | $\phi$ | Single to multiple electrodes | X |  |  |
|  | . 15 | $\phi$ | Electrode spacing |  |  | X |
|  | . 26 | $\pm$ | Peening |  |  | X |
| Legend: <br> + Addition <br> - Deletion |  | cre | ase/greater than $\uparrow$ Up <br> ase/less than $\downarrow$ Do |  | Forehand Backhand | $\phi$ Change |

GENERAL NOTE: Automated vertical gas metal-arc welding for vertical position only.

QW-260
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Electron Beam Welding (EBW)


## WELDING PROCEDURE QUALIFICATIONS

QW-261
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Stud Welding

| Paragraph |  | Brief of Variables |  | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 8 | $\phi$ Stud | size | X |  |  |
|  | . 9 | - Flux | rule | x |  |  |
| QW-403 Base Metal | . 17 | $\phi$ Bas | or stud metal P-No. | x |  |  |
| QW-405 <br> Positions | . 1 | + Pos |  | x |  |  |
| QW-406 <br> Preheat | . 1 | Dec | $100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
| QW-407 <br> PWHT | . 1 | $\phi$ PW |  | x |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 2 | $\phi$ Sing | xture, or \% | x |  |  |
| QW-409 <br> Electrical Characteristics | . 4 | $\phi$ Cur | polarity |  | x | $x$ |
|  | . 8 | $\phi$ I \& |  |  |  | X |
|  | . 9 | $\phi$ Arc |  | x |  |  |
|  | . 10 | $\phi$ Amp |  | X |  |  |
|  | . 11 | $\phi$ Pow |  | X |  |  |
| QW-410 <br> Technique | . 22 | $\phi$ Gun | or lift | X |  |  |
| Legend: <br> + Addition <br> - Deletion | Increase/greater than <br> < Decrease/less than |  | $\begin{array}{ll} \uparrow \text { Uphill } & \leftarrow \\ \downarrow \text { Downhill } & \rightarrow \end{array}$ |  |  |  |

QW-262
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Inertia and Continuous Drive Friction Welding

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 12 | $\phi \pm 10 \mathrm{deg}$ | X |  |  |
|  |  | $\phi$ Cross section $>10 \%$ | X |  |  |
|  |  | $\phi$ O.D. $> \pm 10 \%$ | X |  |  |
|  |  | $\phi$ Solid-to-tube | X |  |  |
| QW-403 <br> Base <br> Metals | . 19 | $\phi$ Base metal | X |  |  |
| QW-406 <br> Preheat | . 1 | $\phi$ Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
| QW-407 <br> PWHT | . 1 | $\phi$ PWHT | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 6 | $\phi$ Environment | X |  |  |
| QW-410 <br> Technique | . 27 | $\phi \quad$ Spp. $> \pm 10 \%$ | X |  |  |
|  | . 28 | $\phi \quad$ Load $> \pm 10 \%$ | X |  |  |
|  | . 29 | $\phi$ Energy $> \pm 10 \%$ | X |  |  |
|  | . 30 | $\phi$ Upset $> \pm 10 \%$ | X |  |  |
| Legend: <br> + Addition <br> - Deletion |  | crease/greater than crease/less than |  | Forehand <br> Backhand | $\phi$ Change |

## WELDING PROCEDURE QUALIFICATIONS

QW-263
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Resistance Welding

| Paragraph |  | Brief of Variables | Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 13 | $\phi$ Spot, projection, seam | X |  |
|  | . 14 | $\phi$ Overlap, spacing | X |  |
|  | . 15 | $\phi$ Projection, shape, size | X |  |
| QW-403 <br> Base <br> Metals | . 1 | $\phi$ P-No. | X |  |
|  | . 21 | $\pm$ Coating, plating | X |  |
|  | . 22 | $\pm T$ | X |  |
| QW-406 <br> Preheat | . 6 | $\phi$ Amplitude, cycles | X |  |
| QW-407 <br> PWHT | . 5 | $\phi$ PWHT | X |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 23 | - Gases | X |  |
| QW-409 <br> Electrical | . 13 | $\phi$ RWMA class | X |  |
|  | . 14 | $\pm \phi$ Slope | X |  |
|  | . 15 | $\phi$ Pressure, current, time | X |  |
|  | . 16 | Timing | X |  |
|  | . 17 | $\phi$ Power supply |  | X |
|  | . 18 | Tip cleaning |  | X |
| QW-410 <br> Technique | . 31 | $\phi$ Cleaning method | X |  |
|  | . 32 | $\phi$ Pressure, time | X |  |
|  | . 33 | $\phi$ Equipment | X |  |
|  | . 34 | $\phi$ Cooling medium |  | X |
|  | . 35 | $\phi$ Throat |  | X |
| Legend: <br> + Addition <br> - Deletion | Incre <br> Decr | eater than $\uparrow$ Uphill <br> ss than $\downarrow$ Downhill | $\leftarrow$ Forehand <br> $\rightarrow$ Backhand | $\phi$ Change |

QW-264
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Laser Beam Welding (LBW)

| Paragraph |  |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 1 | $\phi$ | Groove design | X |  |  |
|  | . 2 | $\pm$ | Backing | X |  |  |
|  | . 6 | > | Fit-up gap | X |  |  |
|  | . 18 | $\phi$ | Lap joint config. | X |  |  |
| QW-403 <br> Base Metals | . 1 | $\phi$ | P-Number | X |  |  |
|  | . 3 | $\phi$ | Penetration | X |  |  |
|  | . 13 | $\phi$ | P-No. 5/9/10 | X |  |  |
|  | . 15 | $\phi$ | P-Number | X |  |  |
| QW-404 <br> Filler Metals | . 1 | $\phi$ | Cross section or speed | X |  |  |
|  | . 2 | $<$ | $t$ or $\phi$ comp. | X |  |  |
|  | . 8 | $\pm$ | or $\phi$ chem. comp. | X |  |  |
|  | . 14 | $\pm$ | Filler metal | X |  |  |
|  | . 20 | $\phi$ | Method of addition | X |  |  |
|  | . 21 | $\phi$ | Analysis | X |  |  |
|  | . 33 | $\phi$ | Classification |  |  | X |
| QW-406 <br> Preheat | . 1 |  | Decrease $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ | X |  |  |
| QW-407 <br> PWHT | . 1 | $\phi$ | PWHT | X |  |  |
| QW-408 <br> Gas | . 2 | $\phi$ | Single, mixture, or \% | X |  |  |
|  | . 6 | $\phi$ | Environment | X |  |  |
|  | . 11 | $\pm$ | Gases | X |  |  |
|  | . 12 | $\phi$ | > 5\% Gases | X |  |  |
|  | . 13 | $\phi$ | Plasma jet position | X |  |  |
| QW-409 <br> Electrical <br> Characteristics | . 19 | $\phi$ | Pulse | $X$ |  |  |
|  | . 20 | $\phi$ | Mode, energy | X |  |  |
|  | . 21 | $\phi$ | Power, speed, d/ff, distance | X |  |  |
| QW-410 <br> Technique | . 5 | $\phi$ | Method cleaning |  |  | X |
|  | . 7 | $\phi$ | Oscillation | X |  |  |
|  | . 14 | $\phi$ | Angle of beam axis | X |  |  |
|  | . 17 | $\phi$ | Type/model of equipment | X |  |  |
|  | . 20 | + | Wash pass | X |  |  |
|  | . 21 |  | 1 vs. 2 side welding | $x$ |  |  |
|  | . 37 | $\phi$ | Single to multiple pass | X |  |  |

Legend:

+ Addition $>$ Increase/greater than $\uparrow$ Uphill $\leftarrow$ Forehand $\phi$ Change
- Deletion < Decrease/less than $\downarrow$ Downhill $\rightarrow$ Backhand


## WELDING PROCEDURE QUALIFICATIONS

QW-264.1
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Laser Beam Welding (LBW)

| Special Process Variables |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Paragraph |  | Essential Variables |  | Nonessential Variables for HFO and CRO |
|  |  | Hard-Facing Overlay (HFO) (QW-216) | Corrosion-Resistant Overlay (CRO) (QW-214) |  |
| QW-402 <br> Joints | . 16 | $<$ Finished $t$ | $<$ Finished $t$ |  |
| QW-403 <br> Base Metals | . 13 | $\phi$ P-Number 5/9/10 | $\phi$ P-Number 5/9/10 |  |
|  | . 20 | $\phi$ P-Number | $\phi$ P-Number |  |
| QW-404 <br> Filler Metals | . 12 | $\phi$ Classification | $\phi$ Classification |  |
|  | . 27 | $\phi$ Alloy elements | $\phi$ Alloy elements |  |
|  | . 44 | $\phi$ Particle type | $\phi$ Particle type |  |
|  | . 47 | $\phi$ Filler/powder metal size | $\phi$ Filler/powder metal size |  |
|  | . 48 | $\phi$ Powder metal density | $\phi$ Powder metal density |  |
|  | . 49 | $\phi$ Filler metal powder feed rate | $\phi$ Filler metal powder feed rate |  |
| QW-405 Positions | . 1 | + Position | + Position |  |
| QW-406 <br> Preheat | . 4 | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat $>$ Interpass | Dec. $>100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ preheat $>$ Interpass |  |
| QW-407 <br> PWHT | . 6 | $\phi$ PWHT |  |  |
|  | . 9 |  | $\phi$ PWHT |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 2 | $\phi$ Single, mixture, or \% | $\phi$ Single, mixture, or \% |  |
|  | . 6 | $\phi$ Environment | $\phi$ Environment |  |
|  | . 11 | $\pm$ Gases | $\pm$ Gases |  |
|  | . 12 | $\phi$ \% Flow rate | $\phi$ \% Flow rate |  |
|  | . 13 | $\phi$ Plasma jet position | $\phi$ Plasma jet position |  |
| QW-409 <br> Electrical <br> Characteristics | . 19 | $\phi$ Pulse | $\phi$ Pulse |  |
|  | . 20 | $\phi$ Mode, energy | $\phi$ Mode, energy |  |
|  | . 21 | $\phi$ Power, speed, d/fl, distance | $\phi$ Power, speed, d/fl, distance |  |
| QW-410 <br> Technique | . 5 |  |  | $\phi$ Method of cleaning |
|  | . 7 | $\phi$ Oscillation | $\phi$ Oscillation |  |
|  | . 14 | $\phi$ Angle of beam axis | $\phi$ Angle of beam axis |  |
|  | . 17 | $\phi$ Type/model of equipment | $\phi$ Type/model of equipment |  |
|  | . 38 | $\phi$ Multiple to single layer | $\phi$ Multiple to single layer |  |
|  | . 45 | $\phi$ Method of surface prep. | $\phi$ Method of surface prep. |  |
|  | . 52 | $\phi$ Filler metal delivery | $\phi$ Filler metal delivery |  |
|  | . 53 | $\phi$ Overlap, spacing | $\phi$ Overlap, spacing |  |
| Legend: <br> + Addition <br> - Deletion | $>$ Increase/greater than $\uparrow$ Uphill <br> < Decrease/less than $\downarrow$ Downhill |  | $\underset{\rightarrow}{\leftarrow} \text { Forehand } \quad \phi \text { Change }$ |  |

## 2004 SECTION IX

QW-265
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Flash Welding

| Paragraph |  | Brief of Variables | Essential | Supplementary Essential | Nonessential |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 <br> Joints | . 19 | $\phi$ Diameter or thickness | X |  |  |
|  | . 20 | $\phi$ Joint configuration | X |  |  |
|  | . 21 | $\phi$ Method or equip. used to minimize ID flash | X |  |  |
|  | . 22 | $\phi$ End preparation method | X |  |  |
| QW-403 <br> Base <br> Metals | . 24 | $\phi$ Spec., type, or grade | X |  |  |
| QW-406 <br> Preheat | . 7 | $\phi>10 \%$ Amperage or number of preheat cycles, or method, or $>25^{\circ} \mathrm{F}$ temperature | X |  |  |
| QW-407 <br> PWHT | . 8 | $\phi$ PWHT, PWHT cycles, or separate PWHT time or temperature | X |  |  |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 22 | $\phi$ Shielding gas composition, pressure, or purge time | X |  |  |
| QW-409 <br> Electrical <br> Characteristics | . 27 | $\phi>10 \%$ Flashing time | X |  |  |
|  | . 28 | $\phi>10 \%$ Upset current time | X |  |  |
| QW-410 <br> Technique | . 17 | $\phi$ Type/model of equipment | X |  |  |
|  | . 54 | $\phi>10 \%$ Upset length or force | X |  |  |
|  | . 55 | $\phi>10 \%$ Distance between clamping dies or preparation of clamping area | X |  |  |
|  | . 56 | $\phi$ Clamping force | X |  |  |
|  | . 57 | $\begin{array}{cc} \phi & 10 \% \text { Forward or reverse } \\ \text { speed } \end{array}$ | X |  |  |
| Legend: <br> + Addition <br> - Deletion | $>$ Increas <br> < Decreas | than $\uparrow$ Uphill $\leftarrow$ <br> an $\downarrow$ Downhill $\rightarrow$ |  |  |  |

## QW-283 Welds With Buttering

QW-283.1 Scope. This paragraph only applies when the essential variables for the buttering process are different than the essential variables for the process used for subsequent completion of the joint. Common examples are:
(a) the buttered member is heat treated and the completed weld is not heat treated after welding
(b) the filler metal used for buttering has a different F-Number from that used for the subsequent completion of the weld

QW-283.2 Tests Required. The procedure shall be qualified by buttering the test coupon (including heat treating of the buttered member when this will be done in production welding) and then making the subsequent weld joining the members. The variables for the buttering and for the subsequent weld shall be in accordance with QW-250, except that QW-409.1 shall be an essential variable for the welding process(es) used to complete the weld when the minimum buttering thickness is less than $3 / 16$ in. ( 5 mm ). Mechanical testing of the completed weldment shall be in accordance with QW-202.2(a).

If the buttering is done with filler metal of the same composition as the filler metal used to complete the weld, one weld test coupon may be used to qualify the dissimilar metal joint by welding the first member directly to the second member in accordance with Section IX.

QW-283.3 Buttering Thickness. The thickness of buttering which shall remain on the production buttered member after all machining and grinding is completed and before subsequent completion of the joint shall be required by the WPS. When this thickness is less than $3 / 16 \mathrm{in}$. ( 5 mm ), the thickness of buttering on the test coupon shall be measured before the buttered member is welded to the second member. This thickness shall become the minimum qualified thickness of buttering.

QW-283.4 Qualification Alternative. When an essential variable is changed in the portion of the weld to be made after buttering or when a different organization is performing the portion of the weld to be made after buttering, a new qualification shall be performed in accordance with one of the following methods:
(a) Qualify in accordance with QW-283.2 and QW-283.3. When the original qualification buttering thickness is less than $3 / 16 \mathrm{in}$. ( 5 mm ), the buttering thickness shall not be greater, nor the heat input higher than was used on the original qualification.
(b) When the original qualification buttering thickness is $3 / 16 \mathrm{in}$. ( 5 mm ) or greater, qualify the portion of the weld to be made after buttering using any P-Number material that nominally matches the chemical analysis of
the buttering weld metal for the buttered base metal of the test coupon.

## QW-284 Resistance Welding Machine Qualification

Each resistance welding machine shall be tested to determine its ability to make welds consistently and reproducibly. A machine shall be requalified whenever it is rebuilt, moved to a new location requiring a change in power supply, when the power supply is changed, or any other significant change is made to the equipment. Spot and projection welding machine qualification testing shall consist of making a set of 100 consecutive welds. Every fifth of these welds shall be subjected to mechanical shear tests. Five welds, which shall include one of the first five and one of the last five of the set shall be metallographically examined. Seam welding machine qualification testing shall be the same as procedure qualification testing required per QW-286. Maintenance or adjustment of the welding machine shall not be permitted during welding of a set of test welds. Qualification testing on any P-No. 21 through P-No. 25 aluminum alloy shall qualify the machine for all materials. Qualification on P-No. 1 through P-No. 11 iron-base alloys and any P-No. 41 through P-No. 47 nickel-base alloys shall qualify the machine for all P-No. 1 through P-No. 11 and P-No. 41 through P-No. 49 metals. Testing and acceptance criteria shall be in accordance with QW-196.

## QW-285 Resistance Spot and Projection Weld Procedure Qualification

Procedure qualification testing for spot or projection welds shall be done following a Welding Procedure Specification, and it shall consist of making a set of ten consecutive welds. Five of these welds shall be subjected to mechanical shear tests and five to metallographic examination. Examination, testing, and acceptance criteria shall be in accordance with QW-196.

## QW-286 Resistance Seam Weld Procedure Qualification

Plates shall be prepared by welding or brazing a pipe nipple to one of the plates at a hole in one of the plates, and then the plates shall be welded around the edges, sealing the space between the plates as shown in figure QW-462.7. The space between the plates shall be pressurized until failure occurs. The procedure qualification is acceptable if failure occurs in the base metal. An additional seam weld at least 6 in. $(150 \mathrm{~mm})$ long shall be made between plates of the same thickness as to be used
in production welding, and this plate shall be cut into six approximately equal width strips and one cross section of each strip shall be metallographically examined and meet the requirements of QW-196.

## 04 QW-290 TEMPER BEAD WELDING

When the applicable Code Section specifies the use of this paragraph for temper bead welding, QW-290.1 through QW-290.6 shall apply.

QW-290.1 Basic Qualification and Upgrading Existing WPSs. All WPSs for temper bead welding of groove and fillet weld shall be qualified for groove welding in accordance with the rules in QW-202 for qualification by groove welding or the rules in QW-283 for welds with buttering. WPSs for overlay shall be qualified in accordance with QW-214 or QW-216. Once these requirements and any additional qualification requirements of the applicable construction code have been satisfied, then it is necessary only to prepare an additional test coupon using the same procedure with the same essential and, if applicable, the supplementary essential variables with the coupon long enough to obtain the required temper bead test specimens. Qualification for groove welding, welding with buttering or cladding, and temper bead welding may also be done in a single test coupon.

When a procedure has been previously qualified to satisfy all requirements including temper bead welding, but one or more temper bead welding variables is
changed, then it is necessary only to prepare an additional test coupon using the same procedure with the same essential and, if applicable, the supplementary essential variables and the new temper bead welding essential variable(s) with the coupon long enough to obtain the required test specimens.

QW-290.2 Welding Process Restrictions. Temper bead welding is limited to SMAW, GTAW, SAW, GMAW (including FCAW), and PAW. Manual and semiautomatic GTAW and PAW are prohibited, except for the root pass of groove welds made from one side and as described for making repairs to temper bead welds in QW-290.5. The essential variables listed in table QW290.4 apply in addition to the variables applicable for the process(es) qualified as given in QW-250. When impact testing is the basis for acceptance, the supplementary essential variables of QW-250 applicable to the process being qualified shall apply. When these variables conflict with or provide more stringent limitations than those of QW-250, these variables shall govern.

QW-290.3 Variables for Temper Bead Welding Qualifications. Table QW-290.4 lists the essential and nonessential variables that apply when temper bead qualification is required. The column "Hardness Test Essential Variables" shall apply, except that when the applicable Construction Code or Design Specification specifies acceptance based on impact testing, the column "Impact Test Essential Variables" shall apply. The column "Nonessential Variables" applies in all cases.

QW-290.4
WELDING VARIABLES FOR TEMPER BEAD PROCEDURE QUALIFICATION

| Paragraph |  | Brief of Variables | Hardness Test Essential Variables | Impact Test Essential Variables | Nonessential Variables |
| :---: | :---: | :---: | :---: | :---: | :---: |
| QW-402 | . 23 | + Fluid backing | X |  |  |
|  | . 24 | + Fluid backing |  | X |  |
| QW-403 | . 25 | $\phi$ P-No. or Gr. No. |  | X |  |
|  | . 26 | > Carbon equivalent | X |  |  |
|  | . 27 | > T | X |  |  |
| QW-404 | . 51 | Storage |  |  | X |
|  | . 52 | Diffusible hydrogen |  |  | X |
| QW-406 | . 8 | > Interpass temperature |  | X |  |
|  | . 9 | < Preheat temperature | X |  |  |
|  | . 10 | Preheat soak time |  |  | X |
|  | . 11 | Postweld bakeout |  |  | X |
| QW-408 | . 24 | Gas moisture |  |  | X |
| QW-409 | . 29 | $\phi$ Heat input ratio | X | X |  |
| QW-410 | . 10 | $\phi$ Single to multiple electrode | X | X |  |
|  | . 58 | - Surface temper beads | X | X |  |
|  | . 59 | $\phi$ Type of welding | X | X |  |
|  | . 60 | + Themal preparation | X | X |  |
|  | . 61 | Surface bead placement |  |  | X |
|  | . 62 | Surface bead removal |  |  | X |
|  | . 63 | Bead overlap |  |  | X |

Legend:

## + Addition $>$ Increase/greater than $\phi$ Change <br> - Deletion <br> < Decrease/less than

QW-290.5 Test Coupon Preparation and Testing
(a) The test coupon may be any geometry that is suitable for removal of the required specimens. It shall consist of a groove weld, a cavity in a plate, overlay, or other suitable geometry. The distance from each edge of the weld preparation to the edge of the test coupon shall be at least 3 in . measured transverse to the direction of welding. The depth of preparation shall be such that at least two layers of weld metal are deposited, one of which may be the surface temper bead layer and deep enough to remove the required test specimens.
(b) The test coupon shall be bend-tested in accordance with QW-451.
(c) When hardness testing is specified by a Construction Code or Design Specification or no specific testing is required, measurements shall be taken across the weld metal, heat-affected zone, and base metal using the Vickers method with a 10 kg load. Increments shall be not greater than 0.010 in . $(0.25 \mathrm{~mm})$ apart and shall include
(1) a minimum of two measurements in the weld metal fill layers
(2) measurements across all weld metal temper bead layers
(3) measurements across the heat-affected zone
(4) a minimum of two measurements in the unaffected base metal

The measurements shall be taken along a line at approximately mid-plane of the thickness of the test coupon weld metal, along a line 0.040 in . ( 1 mm ) below the original base metal surface and, when the coupon was welded using a full-penetration groove weld made from one side, $1 / 16 \mathrm{in}$. ( 1.5 mm ) above the root side surface. The path of HAZ hardness measurements may angle across the HAZ as necessary to obtain the required spacing without interference of one impression with others.

Full-penetration groove weld test coupons qualify full and partial penetration groove welds, fillet welds, and weld build-up. Partial penetration groove weld test coupons only qualify partial penetration groove welds, fillet
welds, and build-up. Overlay test coupons only qualify overlay welds.

Hardness readings shall not exceed the hardness limits specified by the Construction Code or Design Specification. Where hardness is not specified, the data shall be reported.
(d) When specified by the applicable Construction Code or Design Specification, the test coupon shall be Charpy V-notch impact tested. The extent of testing (i.e., weld metal, HAZ, unaffected base metal), the testing temperature, and the acceptance criteria shall be as provided in the applicable Construction Code or Design Specification. Impact test specimens shall be removed from the coupon in the weld metal and HAZ as near as practical to a depth of one-half the thickness of the weld metal for each process. For HAZ specimens, the specimen shall be oriented so as to include as much of the HAZ as possible at the notch. The impact specimens and testing shall be in accordance with SA-370 using the largest size specimen that can be removed from the test coupon with the notch cut approximately normal to the test coupon surface. More than one set of impact test specimens shall be removed and tested when weld metal and heat-affected zone material from each process or set of variables cannot be included in a single set of test specimens.

## QW-290.6 In-Process Repair Welding

(a) In-process repairs to welds made using temper bead welding are permitted. In-process repairs are defined as repairs in which a flaw is mechanically removed and a repair weld is made before welding of a joint is presented for final visual inspection. Examples of such repairs are areas of removal of porosity, incomplete fusion, etc., where sufficient metal has been mechanically removed that localized addition of weld metal is necessary in order to make the surface geometry suitable for continuation of normal welding.
(b) Surfaces to be repaired shall be prepared by mechanical removal of flaws and preparation of the surface to a suitable geometry.
(c) For processes other than manual and semiautomatic GTAW and PAW, repairs shall be made using the parameters given in the WPS for production temper bead welding. The approximate location of beads to be deposited relative to the original base metal surface shall be identified, and the applicable parameters shall be used for the layers to be deposited as specified by the WPS.
(d) When it is necessary to make repairs using manual or semiautomatic GTAW or PAW, a WPS shall be prepared based on PQRs developed for temper bead welding using machine or automatic GTAW or PAW, respectively. This WPS shall describe the size of the beads to be deposited and the volts, amps, and travel speed to be used for the beads against the base metal, for each temper bead layer and for the fill and surface temper bead layers corresponding to the locations where repair welding is to be done. These shall be within the equivalent power ratio for machine or automatic welding for the respective layers given in QW-409.29.
(e) Welders who will use manual and semiautomatic GTAW or PAW shall be qualified to use these welding processes as required by QW-300. In addition, each welder shall complete a proficiency demonstration. For this demonstration, each welder shall deposit two or more weld beads using WPS parameters for each deposit layer The test coupon size shall be sufficiently large to make the required weld bead passes. The minimum pass length shall be 4 in . ( 100 mm ). The heat input used by the welder shall be measured for each pass, and the size of each weld bead shall be measured for each pass, and they shall be as required by the WPS. The following essential variables shall apply for this demonstration:
(1) a change from one welding procedure to another
(2) a change from manual to semiautomatic welding and vice versa
(3) a change in position based on a groove weld in either plate or pipe as shown in table QW-461.9
(4) continuity of qualification in accordance with QW-322 shall be based on following the WPS that was demonstrated in addition to using the process as required by QW-322.

# ARTICLE III WELDING PERFORMANCE QUALIFICATIONS 

## QW-300 GENERAL

QW-300.1 This Article lists the welding processes separately, with the essential variables that apply to welder and welding operator performance qualifications.

The welder qualification is limited by the essential variables given for each welding process. These variables are listed in QW-350, and are defined in Article IV Welding Data. The welding operator qualification is limited by the essential variables given in QW-360 for each type of weld.

A welder or welding operator may be qualified by radiography of a test coupon, radiography of his initial production welding, or by bend tests taken from a test coupon except as stated in QW-304 and QW-305.

## QW-300.2

(a) The basic premises of responsibility in regard to welding are contained within QW-103 and QW-301.2. These paragraphs require that each manufacturer or contractor (an assembler or an installer is to be included within this premise) shall be responsible for conducting tests to qualify the performance of welders and welding operators in accordance with qualified Welding Procedure Specifications, which his organization employs in the construction of weldments built in accordance with the Code. The purpose of this requirement is to ensure that the manufacturer or contractor has determined that his welders and welding operators using his procedures are capable of developing the minimum requirements specified for an acceptable weldment. This responsibility cannot be delegated to another organization.
(b) The welders or welding operators used to produce such weldments shall be tested under the full supervision and control of the manufacturer, contractor, assembler, or installer during the production of these test weldments. It is not permissible for the manufacturer, contractor, assembler, or installer to have the welding performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test materials for welding and subsequent work on the preparation of test specimens from the completed weldments,
performance of nondestructive examination and mechanical tests, provided the manufacturer, contractor, assembler, or installer accepts full responsibility for any such work.
(c) The Code recognizes a manufacturer, contractor, assembler, or installer as the organization which has responsible operational control of the production of the weldments to be made in accordance with this Code. If in an organization effective operational control of the welder performance qualification for two or more companies of different names exists, the companies involved shall describe in the Quality Control system, the operational control of performance qualifications. In this case requalification of welders and welding operators within the companies of such an organization will not be required, provided all other requirements of Section IX are met.
(d) The Code recognizes that manufacturers or contractors may maintain effective operational control of Welder/Welding Operator Performance Qualification (WPQ) records under different ownership than existed during the original welder or weld operator qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the WPQs may be used by the new owner(s) without requalification, provided all of the following are met:
(1) the new owner(s) takes responsibility for the WPQs
(2) the WPQs reflect the name of the new owner(s)
(3) the Quality Control System/Quality Assurance Program reflects the source of the WPQs as being from the former manufacturer or contractor

QW-300.3 More than one manufacturer, contractor, assembler, or installer may simultaneously qualify one or more welders or welding operators. When simultaneous qualifications are conducted, each participating organization shall be represented during welding of test coupons by an employee who is responsible for welder performance qualification.

The welding procedure specifications (WPS) that are followed during simultaneous qualifications shall be compared by the participating organizations. The WPSs shall
be identical for all the essential variables, except for the preheat temperature and PWHT requirements. The qualified thickness ranges for base metal and deposited weld metal need not be identical, but these thicknesses shall be adequate to permit welding of the test coupons. Alternatively, the participating organizations shall agree upon the use of a single WPS provided each participating organization has a $\mathrm{PQR}(\mathrm{s})$ to support the WPS covering the range of variables to be followed in the performance qualification. When a single WPS is to be followed, each participating organization shall review and accept that WPS.

Each participating organization's representative shall positively identify each welder or welding operator who is being tested. Each organizational representative shall also verify marking of the test coupon with the welder's or welding operator's identification, and marking of the top of the test coupon when the orientation must be known in order to remove test specimens.

Each organization's representative shall perform a visual examination of each completed test coupon and shall examine each test specimen to determine its acceptability. Alternatively, after visual examination, when the test coupon(s) are prepared and tested by an independent laboratory, that laboratory's report may be used as the basis for accepting the test results. When the test coupon(s) is radiographically examined (QW-302.2), the radiographic testing facility's report may be used as the basis for acceptance of the radiographic test.

Each organizational representative shall complete and sign a Welder/Welding Operator Performance Qualification (WPQ) Record for each welder or welding operator. Forms QW-484A/QW-484B (see Nonmandatory Appendix B) have been provided as a guide for the WPQ.

When a welder or welding operator changes employers between participating organizations, the employing organization shall verify that the welder's continuity of qualifications has been maintained as required by QW-322 by previous employers since his qualification date. If the welder or welding operator has had his qualification withdrawn for specific reasons, the employing organization shall notify all other participating organizations that the welder's or welding operator's qualification(s) has been revoked in accordance with QW-322.1(b). The remaining participating organizations shall determine that the welder or welding operator can perform satisfactory work in accordance with this Section.

When a welder's or welding operator's qualifications are renewed in accordance with the provisions of QW-322.2, each renewing organization shall be represented by an employee who is responsible for welder performance qualification. The testing procedures shall follow the rules of this paragraph.

## QW-301 Tests

QW-301.1 Intent of Tests. The performance qualification tests are intended to determine the ability of welders and welding operators to make sound welds.

QW-301.2 Qualification Tests. Each manufacturer or contractor shall qualify each welder or welding operator for each welding process to be used in production welding. The performance qualification test shall be welded in accordance with qualified Welding Procedure Specifications (WPS), or Standard Welding Procedure Specifications (SWPS) listed in Appendix E, except that when performance qualification is done in accordance with a WPS or SWPS that requires a preheat or postweld heat treatment, these may be omitted. Changes beyond which requalification is required are given in $\mathrm{QW}-350$ for welders and in QW-360 for welding operators. Allowable visual, mechanical, and radiographic examination requirements are described in QW-304 and QW-305. Retests and renewal of qualification are given in QW-320.

The welder or welding operator who prepares the WPS qualification test coupons meeting the requirements of QW-200 is also qualified within the limits of the performance qualifications, listed in QW-304 for welders and in QW-305 for welding operators. He is qualified only within the limits for positions specified in QW-303.

The performance test may be terminated at any stage of the testing procedure, whenever it becomes apparent to the supervisor conducting the tests that the welder or welding operator does not have the required skill to produce satisfactory results.

QW-301.3 Identification of Welders and Welding Operators. Each qualified welder and welding operator shall be assigned an identifying number, letter, or symbol by the manufacturer or contractor, which shall be used to identify the work of that welder or welding operator.

QW-301.4 Record of Tests. The record of Welder/Welding Operator Performance Qualification (WPQ) tests shall include the essential variables (QW-350 or QW-360), the type of test and test results, and the ranges qualified in accordance with QW-452 for each welder and welding operator. Suggested forms for these records are given in Forms QW-484A/QW-484B (see Nonmandatory Appendix B).

## QW-302 Type of Test Required

QW-302.1 Mechanical Tests. Except as may be specified for special processes (QW-380), the type and number of test specimens required for mechanical testing shall be in accordance with QW-452. Groove weld test specimens shall be removed in a manner similar to that shown in figures QW-463.2(a) through QW-463.2(h). Fillet weld
test specimens shall be removed in a manner similar to that shown in figures QW-462.4(a) through QW-462.4(d) and figure QW-463.2(h).

All mechanical tests shall meet the requirements prescribed in QW-160 or QW-180, as applicable.

QW-302.2 Radiographic Examination. When the welder or welding operator is qualified by radiographic examination, as permitted in QW-304 for welders and QW-305 for welding operators, the minimum length of coupon(s) to be examined shall be 6 in . $(150 \mathrm{~mm})$ and shall include the entire weld circumference for pipe(s), except that for small diameter pipe, multiple coupons may be required, but the number need not exceed four consecutively made test coupons. The radiographic technique and acceptance criteria shall be in accordance with QW-191.

QW-302.3 Test Coupons in Pipe. For test coupons made on pipe in position 1 G or 2G of figure QW-461.4, two specimens shall be removed as shown for bend specimens in figure QW-463.2(d) or figure QW-463.2(e), omitting the specimens in the upper-right and lower-left quadrants, and replacing the root-bend specimen in the upper-left quadrant of figure QW-463.2(d) with a facebend specimen. For test coupons made on pipe in position 5 G or 6 G of figure $\mathrm{QW}-461.4$, specimens shall be removed in accordance with figure $\mathrm{QW}-463.2(\mathrm{~d})$ or figure QW-463.2(e) and all four specimens shall pass the test. For test coupons made in both positions 2G and 5 G on a single pipe test coupon, specimens shall be removed in accordance with figure QW-463.2(f) or figure QW-463.2(g).

QW-302.4 Visual Examination. For plate coupons all surfaces (except areas designated "discard") shall be examined visually per QW-194 before cutting of bend specimens. Pipe coupons shall be visually examined per QW-194 over the entire circumference, inside and outside.

## QW-303 Limits of Qualified Positions and Diameters (See QW-461)

QW-303.1 Groove Welds - General. Welders and welding operators who pass the required tests for groove welds in the test positions of table QW-461.9 shall be qualified for the positions of groove welds and fillet welds shown in table QW-461.9. In addition, welders and welding operators who pass the required tests for groove welds shall also be qualified to make fillet welds in all thicknesses and pipe diameters of any size within the limits of the welding variables of QW-350 or QW-360, as applicable.

QW-303.2 Fillet Welds - General. Welders and welding operators who pass the required tests for fillet welds in the test positions of table QW-461.9 shall be qualified for the positions of fillet welds shown in table QW-461.9. Welders and welding operators who pass the tests for fillet welds shall be qualified to make fillet welds only in the thicknesses of material, sizes of fillet welds, and diameters of pipe and tube $27 / 8$ in. ( 73 mm ) O.D. and over, as shown in table QW-452.5, within the applicable essential variables. Welders and welding operators who make fillet welds on pipe or tube less than $2^{7} / 8 \mathrm{in}$. ( 73 mm ) O.D. must pass the pipe fillet weld test per table QW-452.4 or the required mechanical tests in QW-304 and QW-305 as applicable.

QW-303.3 Special Positions. A fabricator who does production welding in a special orientation may make the tests for performance qualification in this specific orientation. Such qualifications are valid only for the flat position and for the special positions actually tested, except that an angular deviation of $\pm 15$ deg is permitted in the inclination of the weld axis and the rotation of the weld face, as defined in figures QW-461.1 and QW-461.2.

QW-303.4 Stud-Weld Positions. Qualification in the 4 S position also qualifies for the 1 S position. Qualification in the $4 S$ and $2 S$ positions qualifies for all positions.

## QW-304 Welders

Except for the special requirements of QW-380, each welder who welds under the rules of the Code shall have passed the mechanical and visual examinations prescribed in QW-302.1 and QW-302.4 respectively. Alternatively, welders making a groove weld using SMAW, SAW, GTAW, PAW, and GMAW (except short-circuiting mode) or a combination of these processes, may be qualified by radiographic examination, except for P-No. 21 through P-No. 25, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals. Welders making groove welds in P-No. 21 through P-No. 25 and P-No. 51 through P-No. 53 metals with the GTAW process may also be qualified by radiographic examination. The radiographic examination shall be in accordance with QW-302.2.

A welder qualified to weld in accordance with one qualified WPS is also qualified to weld in accordance with other qualified WPSs, using the same welding process, within the limits of the essential variables of QW-350.

QW-304.1 Examination. Welds made in test coupons for performance qualification may be examined by visual and mechanical examinations (QW-302.1, QW-302.4) or by radiography (QW-302.2) for the process(es) and mode
of arc transfer specified in QW-304. Alternatively, a minimum 6 in. ( 150 mm ) length of the first production weld(s) made by a welder using the process(es) and/or mode of arc transfer specified in QW-304 may be examined by radiography.
(a) For pipe(s) welded in the 5G, 6G, or special positions, the entire production weld circumference made by the welder shall be radiographed.
(b) For small diameter pipe where the required minimum length of weld cannot be obtained from a single production pipe circumference, additional consecutive circumferences made by the welder shall be radiographed, except that the total number of circumferences need not exceed four.
(c) The radiographic technique and acceptance criteria for production welds shall be in accordance with QW-191.1 and QW-191.2.2.

QW-304.2 Failure to Meet Radiographic Standards. If a production weld is selected for welder performance qualification and it does not meet the radiographic standards, the welder has failed the test. In this event, the entire production weld made by this welder shall be radiographed and repaired by a qualified welder or welding operator. Alternatively, retests may be made as permitted in QW-320.

## QW-305 Welding Operators

Except for the special requirements of QW-380, each welding operator who welds under the rules of this Code shall have passed the mechanical and visual examinations prescribed in QW-302.1 and QW-302.4 respectively. Alternatively, welding operators making a groove weld using SMAW, SAW, GTAW, PAW, EGW, and GMAW (except short-circuiting mode) or a combination of these processes, may be qualified by radiographic examination, except for P-No. 21 through P-No. 25, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals. Welding operators making groove welds in P-No. 21 through P-No. 25 and P-No. 51 through P-No. 53 metals with the GTAW process may also be qualified by radiographic examination. The radiographic examination shall be in accordance with QW-302.2.

A welding operator qualified to weld in accordance with one qualified WPS is also qualified to weld in accordance with other qualified WPSs within the limits of the essential variables of QW-360.

QW-305.1 Examination. Welds made in test coupons may be examined by radiography (QW-302.2) or by visual and mechanical examinations (QW-302.1, QW-302.4). Alternatively, a minimum $3 \mathrm{ft}(1 \mathrm{~m})$ length of the first production weld(s) made entirely by the welding
operator in accordance with a qualified WPS may be examined by radiography.
(a) For pipe(s) welded in the $5 \mathrm{G}, 6 \mathrm{G}$, or special positions, the entire production weld circumference made by the welding operator shall be radiographed.
(b) For small diameter pipe where the required minimum length of weld cannot be obtained from a single production pipe circumference, additional consecutive circumferences made by the welding operator shall be radiographed except that the total number of circumferences need not exceed four.
(c) The radiographic technique and acceptance criteria for production welds shall be in accordance with QW-191.1 and QW-191.2.3.

QW-305.2 Failure to Meet Radiographic Standards. If a portion of a production weld is selected for welding operator performance qualification, and it does not meet the radiographic standards, the welding operator has failed the test. In this event, the entire production weld made by this welding operator shall be radiographed completely and repaired by a qualified welder or welding operator. Alternatively, retests may be made as permitted in QW-320.

## QW-306 Combination of Welding Processes

Each welder or welding operator shall be qualified within the limits given in QW-301 for the specific welding process(es) he will be required to use in production welding. A welder or welding operator may be qualified by making tests with each individual welding process in separate test coupons, or with a combination of welding processes in a single test coupon. Two or more welders or welding operators, each using the same or a different welding process, may be qualified in combination in a single test coupon. For combination qualifications in a single test coupon, the limits for thicknesses of deposited weld metal, and bend and fillet testing are given in QW-452 and shall be considered individually for each welder or welding operator for each welding process or whenever there is a change in an essential variable. A welder or welding operator qualified in combination on a single test coupon is qualified to weld in production using any of his processes individually or in different combinations, provided he welds within his limits of qualification with each specific process.

Failure of any portion of a combination test in a single test coupon constitutes failure of the entire combination.

## QW-310 QUALIFICATION TEST COUPONS

QW-310.1 Test Coupons. The test coupons may be plate, pipe, or other product forms. When all position
qualifications for pipe are accomplished by welding one pipe assembly in both the 2 G and 5 G positions (figure QW-461.4), NPS 6 (DN 150), NPS 8 (DN 200), NPS 10 (DN 250), or larger diameter pipe shall be employed to make up the test coupon as shown in figure QW-463.2(f) for NPS 10 (DN 250) or larger pipe and in figure QW-463.2(g) for NPS 6 (DN 150) or NPS 8 (DN 200) diameter pipe.

QW-310.2 Welding Groove With Backing. The dimensions of the welding groove on the test coupon used in making qualification tests for double-welded groove welds or single-welded groove welds with backing shall be the same as those for any Welding Procedure Specification (WPS) qualified by the manufacturer, or shall be as shown in figure QW-469.1.

A single-welded groove-weld test coupon with backing or a double-welded groove-weld test coupon shall be considered welding with backing. Partial penetration groove welds and fillet welds are considered welding with backing.

QW-310.3 Welding Groove Without Backing. The dimensions of the welding groove of the test coupon used in making qualification tests for single-welded groove welds without backing shall be the same as those for any WPS qualified by the manufacturer, or as shown in figure QW-469.2.

## QW-320 RETESTS AND RENEWAL OF QUALIFICATION

## QW-321 Retests

A welder or welding operator who fails one or more of the tests prescribed in QW-304 or QW-305, as applicable, may be retested under the following conditions.

QW-321.1 Immediate Retest Using Visual Examination. When the qualification coupon has failed the visual examination of $\mathrm{QW}-302.4$, retesting shall be by visual examination before conducting the mechanical testing.

When an immediate retest is made, the welder or welding operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the visual examination requirements.

The examiner may select one of the successful test coupons from each set of retest coupons which pass the visual examination for conducting the mechanical testing.

QW-321.2 Immediate Retest Using Mechanical Testing. When the qualification coupon has failed the mechanical testing of QW-302.1, retesting shall be by mechanical testing.

When an immediate retest is made, the welder or welding operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the test requirements.

QW-321.3 Immediate Retest Using Radiography. When the qualification coupon has failed the radiographic examination of QW-302.2, the immediate retest shall be by the radiographic examination method.
(a) For welders and welding operators the retest shall be to radiographically examine two $6 \mathrm{in} .(150 \mathrm{~mm})$ plate coupons; for pipe, to examine two pipes for a total of $12 \mathrm{in} .(300 \mathrm{~mm})$ of weld, which shall include the entire weld circumference for pipe or pipes (for small diameter pipe the total number of consecutively made test coupons need not exceed eight).
(b) At the option of the manufacturer, the welder who has failed the production weld alternative test may be retested by radiographing an additional twice the required length or number of pipe circumferences of the same or consecutively made production weld(s) specified in QW-304.1. If this length of weld passes the test, the welder is qualified and the area of weld on which he had previously failed the test shall be repaired by him or another qualified welder. If this length does not meet the radiographic standards, the welder has failed the retest and all of the production welds made by this welder shall be radiographed completely and repaired by a qualified welder or welding operator.
(c) At the option of the manufacturer, the welding operator who has failed the production weld alternative test may be retested by radiographing an additional twice the required length or number of pipe circumferences of the same or consecutively made production weld(s) specified in QW-305.1. If this length of weld passes the test, the welding operator is qualified and the area of weld on which he had previously failed the test shall be repaired by him or another qualified welder or welding operator. If this length does not meet the radiographic standards, the welding operator has failed the retest and all of the production welds made by this welding operator shall be radiographed completely and repaired by a qualified welder or welding operator.

QW-321.4 Further Training. When the welder or the welding operator has had further training or practice, a new test shall be made for each position on which he failed to meet the requirements.

## QW-322 Expiration and Renewal of Qualification

QW-322.1 Expiration of Qualification. The performance qualification of a welder or welding operator
shall be affected when one of the following conditions occurs:
(a) When he has not welded with a process during a period of 6 months or more, his qualifications for that process shall expire; unless, within the 6 -month period, prior to his expiration of qualification
(1) a welder has welded using a manual or semiautomatic welding process that will maintain his qualification for manual and semiautomatic welding with that process
(2) a welding operator has welded with a machine or automatic welding process that will maintain his qualification for machine and automatic welding with that process
(b) When there is a specific reason to question his ability to make welds that meet the specification, the qualifications that support the welding he is doing shall be revoked. All other qualifications not questioned remain in effect.

## QW-322.2 Renewal of Qualification

(a) Renewal of qualification expired under QW-322.1(a) may be made for any process by welding a single test coupon of either plate or pipe, of any material, thickness or diameter, in any position, and by testing of that coupon as required by QW-301 and QW-302. A successful test renews the welder or welding operator's previous qualifications for that process for those materials, thicknesses, diameters, positions, and other variables for which he was previously qualified.

Providing the conditions of QW-304 and QW-305 are satisfied, renewal of qualification under QW-322.1(a) may be done on production work.
(b) Welders and welding operators whose qualifications have been revoked under QW-322.1(b) above shall requalify. Qualification shall utilize a test coupon appropriate to the planned production work. The coupon shall be welded and tested as required by QW-301 and QW-302. Successful test restores the qualification.

## QW-350 WELDING VARIABLES FOR WELDERS

## QW-351 General

A welder shall be requalified whenever a change is made in one or more of the essential variables listed for each welding process.

Where a combination of welding processes is required to make a weldment, each welder shall be qualified for the particular welding process or processes he will be required to use in production welding. A welder may be qualified by making tests with each individual welding process, or with a combination of welding processes in a single test coupon.

The limits of weld metal thickness for which he will be qualified are dependent upon the approximate thickness of the weld metal he deposits with each welding process, exclusive of any weld reinforcement, this thickness shall be considered the test coupon thickness as given in QW-452.

In any given production weldment, welders may not deposit a thickness greater than that permitted by QW-452 for each welding process in which they are qualified.

QW-352
OXYFUEL GAS WELDING (OFW)
Essential Variables

| Paragraph |  | Brief of Variables |
| :--- | :---: | :---: |
| QW-402 <br> Joints | .7 | + Backing |
| QW-403 <br> Base Metals | .2 | Maximum qualified |
|  | .18 | $\phi$ P-Number |
| QW-404 <br> Filler Metals | .14 | $\pm$ Filler |
|  | .15 | $\phi$ F-Number |
| QW-405 <br> Positions | .31 | $\phi$ t Weld deposit |
| QW-408 <br> Gas | .1 | + Position |
| SHIELDED METAL-ARC WELDING (SMAW) |  |  |
| Essential Variables |  |  |


| Paragraph |  | Brief of Variables |
| :--- | :---: | :---: |
| QW-402 <br> Joints | .4 | - Backing |
| QW-403 <br> Base Metals | .16 | $\phi$ Pipe diameter |
|  | .18 | $\phi$ P-Number |
| QW-405 <br> Positions | .15 | $\phi$ F-Number |

## WELDING PERFORMANCE QUALIFICATIONS

QW-354
SEMIAUTOMATIC SUBMERGED-ARC WELDING (SAW)
Essential Variables

| Paragraph |  | Brief of Variables |
| :---: | :---: | :---: |
| QW-404 | . 16 | $\phi$ Pipe diameter |
| Base Metals | . 18 | $\phi$ P-Number |
| QW-404 | . 15 | $\phi$ F-Number |
| Filler Metals | . 30 | $t$ Weld deposit |
| QW-405 <br> Positions | . 1 | + Position |

QW-355
SEMIAUTOMATIC GAS METAL-ARC WELDING (GMAW)
[This Includes Flux-Cored Arc Welding (FCAW)] Essential Variables

| Paragraph |  | Brief of Variables |
| :--- | :---: | :---: |
| QW-402 <br> Joints | .4 | - Backing |
| QW-403 <br> Base Metals | .16 | $\phi$ Pipe diameter |
|  | .18 | $\phi$ P-Number |
|  | .15 | $\phi$ F-Number |
| QW-405 <br> Positions | .32 | $\phi t$ Weld deposit |
| QW-408 <br> Gas | .1 | $t$ Limit (S. Cir. Arc.) |
| QW-409 <br> Electrical | .8 | $\phi$ Position |

QW-356
MANUAL AND SEMIAUTOMATIC GAS TUNGSTEN-ARC WELDING (GTAW)

Essential Variables

| Paragraph |  | Brief of Variables |
| :--- | :---: | :---: |
| QW-402 <br> Joints | .4 | - Backing |
| QW-403 <br> Base Metals | .16 | $\phi$ Pipe diameter |
|  | .18 | $\phi$ P-Number |
| QW-404 <br> Filler Metals | .14 | $\pm$ Filler |
|  | .15 | $\phi$ F-Number |
|  | .23 | $\pm$ Inserts |
| QW-405 <br> Positions | .30 | $\phi$ Solid or metal-cored |
| QW-408 flux-cored |  |  |
| Gas |  |  |

QW-357
MANUAL AND SEMIAUTOMATIC PLASMA-ARC WELDING (PAW) Essential Variables

| Paragraph |  | Brief of Variables |
| :--- | :---: | :---: |
| QW-402 <br> Joints | .4 | - Backing |
| QW-403 <br> Base Metals | .16 | $\phi$ Pipe diameter |
|  | .18 | $\phi$ P-Number |
| QW-404 <br> Filler Metals | .14 | $\pm$ Filler |
|  | .15 | $\phi$ F-Number |
|  | .22 | $\pm$ Inserts |
| QW-405 <br> Positions | .30 | $\phi$ Solid or metal-cored |

Legend for QW-352 through QW-357:

| $\phi$ Change | $\uparrow$ | Uphill |
| :--- | :--- | :--- |
| + Addition | $\downarrow$ | Downhill |
| - Deletion |  |  |

- Deletion


## QW-360 WELDING VARIABLES FOR WELDING OPERATORS

## QW-361 General

A welding operator shall be requalified whenever a change is made in one of the following essential variables (QW-361.1 and QW-361.2). There may be exceptions or additional requirements for the processes of $\mathrm{QW}-362$, QW-363, and the special processes of QW-380.

QW-361.1 Essential Variables - Automatic Welding
(a) A change from automatic to machine welding.
(b) A change in the welding process.
(c) For electron beam and laser welding, the addition or deletion of filler metal.
(d) For laser welding, a change in laser type (e.g., a change from $\mathrm{CO}_{2}$ to YAG).
(e) For friction welding, a change from continous drive to inertia welding or vice versa.
$(f)$ For electron beam welding, a change from vacuum to out-of-vacuum equipment, and vice versa.

## QW-361.2 Essential Variables - Machine Welding

(a) A change in the welding process.
(b) A change from direct visual control to remote visual control and vice-versa.
(c) The deletion of an automatic arc voltage control system for GTAW.
(d) The deletion of automatic joint tracking.
(e) The addition of welding positions other than those already qualified (see QW-120, QW-130, and QW-303).
$(f)$ The deletion of consumable inserts, except that qualification with consumable inserts shall also qualify for fillet welds and welds with backing.
$(g)$ The deletion of backing. Double-welded groove welds are considered welding with backing.
(h) A change from single pass per side to multiple passes per side but not the reverse.

## QW-362 Electron Beam Welding (EBW), Laser Beam Welding (LBW), and Friction Welding (FRW)

The performance qualification test coupon shall be production parts or test coupons that have joint designs permitted by any qualified WPS. The coupon shall be mechanically tested in accordance with QW-452. Alternatively, when the part or coupon does not readily lend itself to the preparation of bend test specimens, the part may be cut so that at least two full-thickness weld cross sections are exposed. Those cross sections shall be smoothed and etched with a suitable etchant (see

QW-470) to give a clear definition of the weld metal and heat affected zone. The weld metal and heat affected zone shall exhibit complete fusion and freedom from cracks. The essential variables for welding operator qualification shall be in accordance with QW-361.

## QW-363 Stud Welding

Stud welding operators shall be performance qualified in accordance with the test requirements of QW-193 and the position requirements of QW-303.4.

## QW-380 SPECIAL PROCESSES <br> QW-381 Corrosion-Resistant Weld Metal Overlay

(a) The size of test coupons, limits of base metal thickness qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.
(b) Welders or welding operators who pass the tests for corrosion-resistant weld metal overlay cladding shall only be qualified to apply corrosion-resistant weld metal overlay portion of a groove weld joining composite clad or lined materials.
(c) The essential variables of QW-350 and QW-360 shall apply for welders and welding operators, respectively, except there is no limit on the maximum thickness of corrosion-resistant overlay that may be applied in production. When specified as essential variables, the limitations of position and diameter qualified for groove welds shall apply to overlay welds, except the limitations on diameter qualified shall apply only to welds deposited in the circumferential direction.
(d) A welder or welding operator who has qualified on composite welds in clad or lined material, as provided in QW-383.1(b) is also qualified to deposit corrosionresistant weld metal overlay.

## QW-382 Hard-Facing Weld Metal Overlay (Wear Resistant)

(a) The size of the test coupons, limits of base metal thickness qualification, required examinations and tests, and test specimens shall be as specified in table QW-453. Base material test coupons may be as permitted in QW-423.
(b) Welders and welding operators who pass the tests for hard-facing weld metal overlay are qualified for hardfacing overlay only.
(c) The essential variable, of QW-350 and QW-360, shall apply for welders and welding operators, respectively, except there is no limit on the maximum thickness
of hard-facing overlay that may be applied in production. When specified as essential variables, the limitations of position and diameter qualified for groove welds shall apply to overlay welds except the limitations on diameter qualified shall apply only to welds deposited in the circumferential direction.
(d) Qualification with one AWS classification within an SFA specification qualifies for all other AWS classifications in that SFA specification.
(e) A change in welding process shall require welder and welding operator requalification.

## QW-383 Joining of Clad Materials and Applied Linings

## QW-383.1 Clad Materials

(a) Welders and welding operators who will join the base material portion of clad materials shall be qualified for groove welding in accordance with QW-301. Welders and welding operators who will apply the cladding portion of a weld between clad materials shall be qualified in accordance with QW-381. Welders and welding operators need only be qualified for the portions of composite welds that they will make in production.
(b) As an alternative to QW-383.1(a), welders and welding operators may be qualified using composite test coupons. The test coupon shall be at least $3 / 8 \mathrm{in}$. $(10 \mathrm{~mm})$ thick and of dimensions such that a groove weld can be made to join the base materials and the corrosion-resistant weld metal overlay can be applied to the completed groove weld. Four side bend test specimens shall be removed from the completed test coupon and tested. The groove weld portion and the corrosion-resistant weld metal overlay portion of the test coupon shall be evaluated using the respective criteria in QW-163. Welders and welding operators qualified using composite test coupons are qualified to join base materials as provided by QW-301, and they are qualified to apply corrosion-resistant weld metal overlay as provided by QW-381.

## QW-383.2 Applied Linings

(a) Welders and welding operators shall be qualified following the rules for making groove or fillet welds in accordance with QW-301. Plug welds for attaching applied linings shall be considered equivalent to fillet welds for the purpose of performance qualification.
(b) An alternate test coupon shall consist of the geometry to be welded, except the base material need not exceed 1 in. $(25 \mathrm{~mm})$ in thickness. The welded test coupon shall be sectioned and etched to reveal the weld and heataffected zone. The weld shall show penetration into the base metal.

## QW-384 Resistance Welding Operator Qualification

Each welding operator shall be tested on each machine type which he will use. Qualification testing on any P-No. 21 through P-No. 25 metal shall qualify the operator for all materials. Qualification on any P-No. 1 through P-No. 11 or any P-No. 41 through P-No. 49 metals shall qualify the operator for all P-No. 1 through P-No. 11 or P-No. 41 through P-No. 49 metals. Qualification testing shall consist of making a set of ten consecutive welds, five of which shall be subjected to mechanical shear tests or peel tests, and five to metallographic examination. Examination, testing, and acceptance criteria shall be in accordance with QW-196.

## QW-385 Flash Welding Operator Qualification

Each welding operator shall be tested by welding a test coupon following any WPS. The test coupon shall be welded and tested in accordance with QW-198. Qualification following any flash welding WPS qualifies the operator to follow all flash welding WPSs.

Production weld sampling tests required by other Sections may be used to qualify welding operators. The test method, extent of tests, and acceptance criteria of the other Sections and QW-199.2 shall be met when this is done.

# ARTICLE IV WELDING DATA 

## QW-400 VARIABLES <br> QW-401 General

Each welding variable described in this Article is applicable as an essential, supplementary essential, or nonessential variable for procedure qualification when referenced in QW-250 for each specific welding process. Essential variables for performance qualification are referenced in QW-350 for each specific welding process. A change from one welding process to another welding process is an essential variable and requires requalification.

QW-401.1 Essential Variable (Procedure). A change in a welding condition which will affect the mechanical properties (other than notch toughness) of the weldment (e.g., change in P-Number, welding process, filler metal, electrode, preheat or postweld heat treatment).

QW-401.2 Essential Variable (Performance). A change in a welding condition which will affect the ability of a welder to deposit sound weld metal (such as a change in welding process, deletion of backing, electrode, FNumber, technique, etc.).

QW-401.3 Supplementary Essential Variable (Procedure). A change in a welding condition which will affect the notch-toughness properties of a weldment (for example, change in welding process, uphill or down vertical welding, heat input, preheat or PWHT, etc.). Supplementary essential variables are in addition to the essential variables for each welding process.
When a procedure has been previously qualified to satisfy all requirements other than notch toughness, it is then necessary only to prepare an additional test coupon using the same procedure with the same essential variables, but additionally with all of the required supplementary essential variables, with the coupon long enough to provide the necessary notch-toughness specimens.
When a procedure has been previously qualified to satisfy all requirements including notch toughness, but one or more supplementary essential variable is changed, then it is only necessary to prepare an additional test
coupon using the same welding procedure and the new supplementary essential variable(s), with the coupon long enough to provide the necessary notch-toughness specimens. If a previously qualified weld procedure has satisfactory notch-toughness values in the weld metal, then it is necessary only to test notch-toughness specimens from the heat affected zone when such are required.
When essential variables are qualified by one or more PQRs and supplementary essential variables are qualified by other PQRs, the ranges of essential variables established by the former PQRs are only affected by the latter to the extent specified in the applicable supplementary essential variable (e.g., essential variable QW-403.8 governs the minimum and maximum thickness of base metal qualified. When supplementary essential variable QW-403.6 applies, it modifies only the minimum thickness qualified, not the maximum).

QW-401.4 Nonessential Variable (Procedure). A change in a welding condition which will not affect the mechanical properties of a weldment (such as joint design, method of back gouging or cleaning, etc.)

QW-401.5 The welding data includes the welding variables grouped as joints, base metals, filler metals, position, preheat, postweld heat treatment, gas, electrical characteristics, and technique. For convenience, variables for each welding process are summarized in table QW-416 for performance qualification.

## QW-402 Joints

QW-402.1 A change in the type of groove (Veegroove, U-groove, single-bevel, double-bevel, etc.).

QW-402.2 The addition or deletion of a backing.
QW-402.3 A change in the nominal composition of the backing.

QW-402.4 The deletion of the backing in singlewelded groove welds. Double-welded groove welds are considered welding with backing.

QW-402.5 The addition of a backing or a change in its nominal composition.

QW-402.6 An increase in the fit-up gap, beyond that initially qualified.

QW-402.7 The addition of backing.
QW-402.8 A change in nominal size or shape of the stud at the section to be welded.

QW-402.9 In stud welding, a change in shielding as a result of ferrule or flux type.

QW-402.10 A change in the specified root spacing.
QW-402.11 The addition or deletion of nonmetallic retainers or nonfusing metal retainers.

QW-402.12 The welding procedure qualification test shall duplicate the joint configuration to be used in production within the limits listed, except that pipe or tube to pipe or tube may be used for qualification of a pipe or tube to other shapes, and solid round to solid round may be used for qualification of a solid round to other shapes:
(a) any change exceeding $\pm 10$ deg in the angle measured for the plane of either face to be joined, to the axis of rotation
(b) a change in cross-sectional area of the weld joint greater than $10 \%$
(c) a change in the outside diameter of the cylindrical weld interface of the assembly greater than $\pm 10 \%$
(d) a change from solid to tubular cross section at the joint or vice versa regardless of QW-402.12(b)

QW-402.13 A change in the joint from spot to projection to seam or vice versa.

QW-402.14 A decrease in the center-to-center distance when the welds overlap. An increase or decrease of more than $10 \%$ in the spacing of the welds when they are within two diameters of each other.

QW-402.15 A change in the size or shape of the projection in projection welding.

QW-402.16 A decrease in the distance between the approximate weld interface and the final surface of the production corrosion-resistant or hard-facing weld metal overlay below the minimum thickness qualified as shown in figures QW-462.5(a) through QW-462.5(e). There is no limit on the maximum thickness for corrosion-resistant or hard-facing weld metal overlay that may be used in production.

QW-402.17 An increase in the thickness of the production spray fuse hard-facing deposit above the thickness deposited on the procedure qualification test coupon.

QW-402.18 When the joint is a lap joint, the following additional variables shall apply:
(a) a change of more than $10 \%$ in the distance to the edge of the material
(b) a change of more than $10 \%$ in the joint overlap
(c) a change in the number of layers of material
(d) a change in the method of surface conditioning at the metal-to-metal interfaces

QW-402.19 A change in the nominal diameter or nominal tube thickness.

QW-402.20 A change in the joint configuration.
QW-402.21 A change in the method or equipment used to minimize internal flash.

QW-402.22 A change in the end preparation method.
QW-402.23 For test coupons less than $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) thick, the addition of a cooling medium (water, flowing gas, etc.) to the back side of the weld. Qualification on test coupons less than $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) thick with a cooling medium on the back side of the weld qualifies base metal thickness equal to or greater than the test coupon thickness with and without coolant.

QW-402.24 Qualification with a cooling medium (water, flowing gas, etc.) on the root side of a test coupon weld that is welded from one side qualifies all thicknesses of base metal with cooling medium down to the thickness of the test coupon at the root or $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$, whichever is less.

## QW-403 Base Metals

QW-403.1 A change from a base metal listed under one P-Number in table QW/QB-422 to a metal listed under another P-Number or to any other base metal. When joints are made between two base metals that have different P-Numbers, a procedure qualification shall be made for the applicable combination of P-Numbers, even though qualification tests have been made for each of the two base metals welded to itself.

QW-403.2 The maximum thickness qualified is the thickness of the test coupon.

QW-403.3 Where the measurement of penetration can be made by visual or mechanical means, requalification is required where the base metal thickness differs by $20 \%$ from that of the test coupon thickness when the test coupon thickness is 1 in . ( 25 mm ) and under, and $10 \%$ when the test coupon thickness is over 1 in . $(25 \mathrm{~mm})$ Where the measurement of penetration cannot be made, requalification is required where the base metal thickness differs by $10 \%$ from that of the test coupon when the test coupon thickness is 1 in . ( 25 mm ) and under, and $5 \%$ when the test coupon thickness is over 1 in . ( 25 mm ).

QW-403.4 Welding procedure qualifications shall be made using a base metal of the same type or grade or another base metal listed in the same group (see table QW/QB-422) as the base metal to be used in production welding. When joints are to be made between base metals from two different groups, a procedure qualification must be made for the applicable combination of base metals, even though procedure qualification tests have been made for each of the two base metals welded to itself.

QW-403.5 Welding procedure specifications shall be qualified using one of the following:
(a) the same base metal (including type or grade) to be used in production welding
(b) for ferrous materials, a base metal listed in the same P-Number Group Number in table QW/QB-422 as the base metal to be used in production welding
(c) for nonferrous materials, a base metal listed with the same P-Number UNS Number in table QW/QB-422 as the base metal to be used in production welding

For ferrous materials in table QW/QB-422, a procedure qualification shall be made for each P-Number Group Number combination of base metals, even though procedure qualification tests have been made for each of the two base metals welded to itself. If, however, the procedure specification for welding the combination of base metals specifies the same essential variables, including electrode or filler metal, as both specifications for welding each base metal to itself, such that base metals is the only change, then the procedure specification for welding the combination of base metals is also qualified. In addition, when base metals of two different P-Number Group Number combinations are qualified using a single test coupon, that coupon qualifies the welding of those two P-Number Group Numbers to themselves as well as to each other using the variables qualified.

This variable does not apply when impact testing of the heat-affected zone is not required by other Sections.

QW-403.6 The minimum base metal thickness qualified is the thickness of the test coupon $T$ or $5 / 8 \mathrm{in}$. $(16 \mathrm{~mm})$, whichever is less. However, where $T$ is less than $1 / 4 \mathrm{in}$. $(6 \mathrm{~mm})$, the minimum thickness qualified is $1 / 2 T$. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-403.7 For the multipass processes of shielded metal-arc, submerged-arc, gas tungsten-arc, and gas metal-arc, the maximum thickness qualified for $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) and over thickness $T$ of the test coupon of table QW- 451.1 shall be 8 in . ( 200 mm ) for the conditions shown in table QW-451.1. For thicknesses greater than

8 in. ( 200 mm ), the maximum thicknesses of base metal and deposited weld metal qualified is $1.33 T$ or $1.33 t$, as applicable.

QW-403.8 A change in base metal thickness beyond the range qualified in QW-451, except as otherwise permitted by QW-202.4(b).

QW-403.9 For single-pass or multipass welding in which any pass is greater than $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$ thick, an increase in base metal thickness beyond 1.1 times that of the qualification test coupon.

QW-403.10 For the short-circuiting transfer mode of the gas metal-arc process, when the qualification test coupon thickness is less than $1 / 2 \mathrm{in}$. ( 13 mm ), an increase in thickness beyond 1.1 times that of the qualification test coupon. For thicknesses of $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$ and greater, use table QW-451.1 or table QW-451.2, as applicable.

QW-403.11 Base metals specified in the WPS shall be qualified by a procedure qualification test that was made using base metals in accordance with QW-424.

QW-403.12 A change from a base metal listed under one P-Number of table QW/QB-422 to a base metal listed under another P-Number. When joints are made between two base metals that have different P-Numbers, requalification is required even though the two base metals have been independently qualified using the same procedure. When the melt-in technique is used for joining P-No. 1, P-No. 3, P-No. 4, and P-No. 5A, a procedure qualification test with one P-Number metal shall also qualify for that P-Number metal welded to each of the lower P-Number metals, but not vice versa.

QW-403.13 A change from one P-No. 5 to any other P-No. 5 (viz P-No. 5A to P-No. 5B or P-No. 5C or vice versa). A change from P-No. 9A to P-No. 9B but not vice versa. A change from one P-No. 10 to any other P-No. 10 (viz P-No. 10A to P-No. 10B or P-No. 10C, etc., or vice versa).

QW-403.15 Welding procedure qualifications for laser beam welding and electron beam welding shall be made using a base metal of the same type or grade or another base metal listed in the same P-Number (and the same group where given - see table QW/QB-422) as the base metal to be used in production welding. When joints are to be made between base metals from two different P-Numbers (or two different groups), a procedure qualification must be made for the applicable combination of base metals even though procedure qualification tests have been made for each of the two base metals welded to itself.

QW-403.16 A change in the pipe diameter beyond the range qualified in $\mathrm{QW}-452$, except as otherwise permitted in QW-303.1, QW-303.2, QW-381(c), or QW-382(c).

QW-403.17 In stud welding, a change in combination of base metal listed under one P-Number in table QW/QB-422 and stud metal P-Number (as defined in Note below), or to any other base metal/stud metal combination.

NOTE: Stud metal shall be classified by nominal chemical composition and can be assigned a P-Number when it meets the nominal composition of any one of the P-Number metals.

QW-403.18 A change from one P-Number to any other P-Number or to a base metal not listed in table QW/QB-422, except as permitted in QW-423, and in QW-420.2.

QW-403.19 A change to another base material type or grade (type or grade are materials of the same nominal chemical analysis and mechanical property range, even though of different product form), or to any other base material type or grade. When joints are made between two different types or grades of base material, a procedure qualification must be made for the applicable combinations of materials, even though procedure qualification tests have been made for each of the two base materials welded to itself.

QW-403.20 A change from a base metal, listed under one P-Number in table QW/QB-422, to a metal listed under another P-Number or to any other base metal; from a base metal of one subgroup to any other grouping in P-No. 10 or 11 .

QW-403.21 The addition or deletion of a coating, plating or cladding, or a change in the nominal chemical analysis or thickness range of the plating or cladding, or a change in type of coating as specified in the WPS.

QW-403.22 A change in the nominal base metal thickness exceeding $5 \%$ of any outer sheet thickness or $10 \%$ of the nominal thickness of the total joint from that qualified.

QW-403.23 A change in base metal thickness beyond the range qualified in table QW-453.

QW-403.24 A change in the specification, type, or grade of the base metal. When joints are to be made between two different base metals, a procedure qualification must be made for the applicable combination even though procedure qualifications have been made for each of the two base metals welded to themselves.

QW-403.25 Welding procedure qualifications shall be made using a base metal of the same P-Number and

Group Number as the base metal to be temper bead welded. When joints are to be made between base metals from two different P-Number/Group Number combinations, a temper bead procedure qualification must be made for each base metal P-Number/Group Number to be used in production; this may be done in separate test coupons or in combination on a single test coupon. When base metals of different P-Number/Group Numbers are tested in the same coupon, the welding conditions and test results on each side of the coupon shall be documented independently but may be reported on the same qualification record. Where temper bead welding is to be applied to only one side of a joint (e.g., on the P-No. 1 side of a joint between P-No. 1 and P-No. 8 metals) or where cladding is being applied or repaired using temper bead techniques, qualification in accordance with QW-290 is required only for the portion of the WPS that applies to welding on the material to be temper bead welded.

QW-403.26 An increase in the base metal carbon equivalent using the following formula:

$$
\mathrm{CE}=\mathrm{C}+\frac{\mathrm{Mn}}{6}+\frac{\mathrm{Cr}+\mathrm{Mo}+\mathrm{V}}{5}+\frac{\mathrm{Ni}+\mathrm{Cu}}{15}
$$

QW-403.27 The maximum thickness qualified is the thickness of the test coupon, $T$, or it is unlimited if the test coupon is $1 / 2 \mathrm{in}$. ( 38 mm ) thick or thicker. However, where $T$ is $1 / 4 \mathrm{in}$. ( 6 mm ) or less, the maximum thickness qualified is $2 T$. This limitation applies to fillet welds as well as to groove welds.

## QW-404 Filler Metals

QW-404.1 A change in the cross-sectional area of the filler metal added (excluding buttering) or in the wirefeed speed greater than $\pm 10 \%$ beyond that qualified.

QW-404.2 A decrease in the thickness or change in nominal specified chemical analysis of weld metal buttering beyond that qualified. (Buttering or surfacing is the deposition of weld metal on one or both faces of the joint prior to preparation of the joint for final electron beam welding.)

QW-404.3 A change in the size of the filler metal.
QW-404.4 A change from one F-Number in table QW-432 to any other F-Number or to any other filler metal not listed in table QW-432.

QW-404.5 (Applicable only to ferrous metals.) A change in the chemical composition of the weld deposit from one A-Number to any other A-Number in table QW-442. Qualification with A-No. 1 shall qualify for A-No. 2 and vice versa.

The weld metal chemical composition may be determined by any of the following:
(a) For all welding processes - from the chemical analysis of the weld deposit taken from the procedure qualification test coupon.
(b) For SMAW, GTAW, and PAW - from the chemical analysis of the weld deposit prepared according to the filler metal specification, or from the chemical composition as reported either in the filler metal specification or the manufacturer's or supplier's certificate of compliance.
(c) For GMAW and EGW - from the chemical analysis of the weld deposit prepared according to the filler metal specification or the manufacturer's or supplier's certificate of compliance when the shielding gas used was the same as that used to weld the procedure qualification test coupon.
(d) For SAW - from the chemical analysis of the weld deposit prepared according to the filler metal specification or the manufacturer's or supplier's certificate of compliance when the flux used was the same as that used to weld the procedure qualification test coupon.

In lieu of an A-Number designation, the nominal chemical composition of the weld deposit shall be indicated on the WPS and on the PQR. Designation of nominal chemical composition may also be by reference to the AWS classification (where such exists), the manufacturer's trade designation, or other established procurement documents.

QW-404.6 A change in the nominal size of the electrode or electrodes specified in the WPS.

QW-404.7 A change in the nominal diameter of the electrode to over $\frac{1}{4} \mathrm{in}$. ( 6 mm ). This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-404.8 Addition or deletion, or a change in nominal amount or composition of supplementary deoxidation material (in addition to filler metal) beyond that qualified. (Such supplementary metal may be required for weld metal deoxidation for some metals being welded.)

## QW-404.9

(a) A change in the indicator for minimum tensile strength (e.g., the 7 in F7A2-EM12K) when the flux wire combination is classified in Section II, Part C.
(b) A change in either the flux trade name or wire trade name when neither the flux nor the wire is classified in Section II, Part C.
(c) A change in the flux trade name when the wire is classified in Section II, Part C but the flux is not classified. A change in the wire classification within the requirements of QW-404.5 does not require requalification.
(d) A change in the flux trade name for A-No. 8 deposits.

QW-404.10 Where the alloy content of the weld metal is largely dependent upon the composition of the flux used, any change in any part of the welding procedure which would result in the important alloying elements in the weld metal being outside of the specification range of chemistry given in the Welding Procedure Specification. If there is evidence that the production welds are not being made in accordance with the procedure specification, the authorized inspector may require that a check be made on the chemical composition of the weld metal. Such a check shall preferably be made on a production weld.

QW-404.12 A change in the filler metal classification within an SFA specification or to a filler metal not covered by an SFA specification, or from one filler metal not covered by an SFA specification to another filler metal that is not covered by an SFA specification.

When a filler metal conforms to a filler metal classification within an SFA specification, requalification is not required if a change is made in any of the following:
(a) from a filler metal that is designated as moistureresistant to one that is not designated as moisture-resistant and vice versa (i.e., from E7018R to E7018)
(b) from one diffusible hydrogen level to another (i.e., from E7018-H8 to E7018-H16)
(c) for carbon, low alloy, and stainless steel filler metals having the same minimum tensile strength and the same nominal chemical composition, a change from one low hydrogen coating type to another low hydrogen coating type (i.e., a change among EXX15, 16, or 18 or EXXX15, 16, or 17 classifications)
(d) from one position-usability designation to another for flux-cored electrodes (i.e., a change from E70T-1 to E71T-1 or vice versa)
(e) from a classification that requires impact testing to the same classification which has a suffix which indicates that impact testing was performed at a lower temperature or exhibited greater toughness at the required temperature or both, as compared to the classification which was used during procedure qualification (i.e., a change from E7018 to E7018-1)
$(f)$ from the classification qualified to another filler metal within the same SFA specification when the weld metal is exempt from Impact Testing by other Sections

This exemption does not apply to hard-facing and cor-rosion-resistant overlays.

QW-404.14 The deletion or addition of filler metal.
QW-404.15 A change from one F-Number in table QW-432 to any other F-Number or to any other filler metal, except as permitted in QW-433.

QW-404.17 A change in the type of flux or composition of the flux.

QW-404.18 A change from wire to plate electrodes, and vice versa.

QW-404.19 A change from consumable guide to nonconsumable guide, and vice versa.

QW-404.20 Any change in the method by which filler metal is added, such as preplaced shim, top strip, wire, wire feed, or prior weld metal buttering of one or both joint faces.

QW-404.21 For filler metal additions, any change from the nominal specified analysis of the filler metal qualified.

QW-404.22 The omission or addition of consumable inserts. Qualification in a single-welded butt joint, with or without consumable inserts, qualifies for fillet welds and single-welded butt joints with backing or doublewelded butt joints. Consumable inserts that conform to SFA-5.30, except that the chemical analysis of the insert conforms to an analysis for any bare wire given in any SFA specification or AWS Classification, shall be considered as having the same F-Number as that bare wire as given in table QW-432.

QW-404.23 A change from one of the following filler metal product forms to another:
(a) flux cored
(b) bare (solid) or metal cored
(c) powder

QW-404.24 The addition, deletion, or change of more than $10 \%$ in the volume of supplemental filler metal.

QW-404.27 Where the alloy content of the weld metal is largely dependent upon the composition of the supplemental filler metal (including powder filler metal for PAW), any change in any part of the welding procedure that would result in the important alloying elements in the weld metal being outside of the specification range of chemistry given in the Welding Procedure Specification.

QW-404.29 A change in the flux trade name and designation.

QW-404.30 A change in deposited weld metal thickness beyond the range qualified in $\mathrm{QW}-451$ for procedure qualification or QW-452 for performance qualification, except as otherwise permitted in QW-303.1 and QW-303.2. When a welder is qualified using radiography, the thickness ranges of table QW-452.1 apply.

QW-404.31 The maximum thickness qualified is the thickness of the test coupon.

QW-404.32 For the low voltage short-circuiting type of gas metal-arc process when the deposited weld metal thickness is less than $1 / 2 \mathrm{in}$. ( 13 mm ), an increase in deposited weld metal thickness beyond 1.1 times that of the qualification test deposited weld metal thickness. For weld metal thicknesses of $1 / 2 \mathrm{in}$. ( 13 mm ) and greater, use table QW-451.1, table QW-451.2, or table QW-452.1, as applicable.

QW-404.33 A change in the filler metal classification within an SFA specification, or, if not conforming to a filler metal classification within an SFA specification, a change in the manufacturer's trade name for the filler metal. When optional supplemental designators, such as those which indicate moisture resistance (i.e., XXXXR), diffusible hydrogen (i.e., XXXX H16, H8, etc.), and supplemental impact testing (i.e., XXXX-1 or EXXXXM), are specified on the WPS, only filler metals which conform to the classification with the optional supplemental designator(s) specified on the WPS shall be used.

QW-404.34 A change in flux type (i.e., neutral to active or vice versa) for multilayer deposits in P-No. 1 materials.

QW-404.35 A change in the flux/wire classification or a change in either the electrode or flux trade name when not classified in an SFA specification. Requalification is not required when a wire/flux combination conforms to an SFA specification and a change is made from one diffusible hydrogen level to another (i.e., a change from F7A2-EA1-A1H4 to F7A2-EA1-A1H16). This variable does not apply when the weld metal is exempt from impact testing by other Sections. This exemption does not apply to hard facing and corrosion-resistant overlays.

QW-404.36 When flux from recrushed slag is used, each batch or blend, as defined in SFA-5.01, shall be tested in accordance with Section II, Part C by either the manufacturer or user, or qualified as an unclassified flux in accordance with QW-404.9.

QW-404.37 A change in the composition of the deposited weld metal from one A-Number in table QW-442 to any other A-Number, or to an analysis not listed in the table. Each AWS classification of A-No. 8 or A-No. 9 analysis of table QW-442, or each nonferrous alloy in table QW-432, shall require separate WPS qualification. A-Numbers may be determined in accordance with QW-404.5.

QW-404.38 A change in the nominal electrode diameter used for the first layer of deposit.

QW-404.39 For submerged-arc welding and electroslag welding, a change in the nominal composition or
type of flux used. Requalification is not required for a change in flux particle size.

QW-404.41 A change of more than $10 \%$ in the powdered metal feed rate recorded on the PQR .

QW-404.42 A change of more than $5 \%$ in the particle size range of the powder.

QW-404.43 A change in the powdered metal particle size range recorded on the PQR .

QW-404.44 A change from a homogeneous powdered metal to a mechanical mixed powdered metal or vice versa.

QW-404.45 A change in the form of filler metal from solid to fabricated wire, flux-cored wire, powdered metal, or vice versa.

QW-404.46 A change in the powder feed rate range qualified.

QW-404.47 A change of more than $10 \%$ in the filler metal size and/or powder metal particle size.

QW-404.48 A change of more than $10 \%$ in the powder metal density.

QW-404.49 A change of more than $10 \%$ in the filler metal or powder metal feed rate.

QW-404.50 The addition or deletion of flux to the face of a weld joint for the purpose of affecting weld penetration.

QW-404.51 The method of control of moisture pickup during storage and distribution for SMAW and GMAW-FC electrodes and flux for SAW (e.g., purchasing in hermetically sealed containers and storage in heated ovens, controlled distribution time, high-temperature baking prior to use).

QW-404.52 A change in the diffusible hydrogen level (e.g., from E7018-H8 to E7018-H16 or to no controlled diffusible hydrogen).

## QW-405 Positions

QW-405.1 The addition of other welding positions than those already qualified. See QW-120, QW-130, and QW-303.

QW-405.2 A change from any position to the vertical position uphill progression. Vertical-uphill progression (e.g., $3 \mathrm{G}, 5 \mathrm{G}$, or 6 G position) qualifies for all positions. In uphill progression, a change from stringer bead to weave bead. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-405.3 A change from upward to downward, or from downward to upward, in the progression specified for any pass of a vertical weld, except that the cover or wash pass may be up or down. The root pass may also be run either up or down when the root pass is removed to sound weld metal in the preparation for welding the second side.

QW-405.4 Except as specified below, the addition of other welding positions than already qualified.
(a) Qualification in the horizontal, vertical, or overhead position shall also qualify for the flat position. Qualification in the horizontal fixed position, 5G, shall qualify for the flat, vertical, and overhead positions. Qualification in the horizontal, vertical, and overhead positions shall qualify for all positions. Qualification in the inclined fixed position, 6 G , shall qualify for all positions.
(b) A fabricator who does production welding in a particular orientation may make the tests for procedure qualification in this particular orientation. Such qualifications are valid only for the positions actually tested, except that an angular deviation of $\pm 15 \mathrm{deg}$ is permitted in the inclination of the weld axis and the rotation of the weld face as defined in figure QW-461.1. A test specimen shall be taken from the test coupon in each special orientation.
(c) For hard-facing and corrosion-resistant weld metal overlay, qualification in the $3 \mathrm{G}, 5 \mathrm{G}$, or 6 G positions, where 5 G or 6 G pipe coupons include at least one vertical segment completed utilizing the up-hill progression or a 3G plate coupon is completed utilizing the up-hill progression, shall qualify for all positions. Chemical analysis, hardness, macro-etch, and at least two of the bend tests, as required in table QW-453, shall be removed from the vertical up-hill overlaid segment as shown in figure QW-462.5(b).
(d) A change from the vertical down to vertical uphill progression shall require requalification.

## QW-406 Preheat

QW-406.1 A decrease of more than $100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ in the preheat temperature qualified. The minimum temperature for welding shall be specified in the WPS.

QW-406.2 A change in the maintenance or reduction of preheat upon completion of welding prior to any required postweld heat treatment.

QW-406.3 An increase of more than $100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ in the maximum interpass temperature recorded on the PQR. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-406.4 A decrease of more than $100^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$ in the preheat temperature qualified or an increase in the maximum interpass temperature recorded on the PQR. The minimum temperature for welding shall be specifed in the WPS.

QW-406.5 A change in the maintenance or reduction of preheat upon completion of spraying and prior to fusing.

QW-406.6 A change of more than $10 \%$ in the amplitude or number of preheating cycles from that qualified.

QW-406.7 A change of more than $10 \%$ in the amplitude or number of preheating cycles from that qualified, or if other preheating methods are employed, a change in the preheating temperature of more than $25^{\circ} \mathrm{F}\left(15^{\circ} \mathrm{C}\right)$.

QW-406.10 The minimum preheating soaking time prior to the start of welding.

QW-406.11 The addition or deletion of a postweld hydrogen bakeout. When specified, the minimum soaking temperature and time shall be specified.

## QW-407 Postweld Heat Treatment

QW-407.1 A separate procedure qualification is required for each of the following conditions:
(a) For P-No. 1, P-No. 3, P-No. 4, P-No. 5, P-No. 6, P-No. 9, P-No. 10, and P-No. 11 materials, the following postweld heat treatment conditions apply:
(1) no PWHT
(2) PWHT below the lower transformation temperature
(3) PWHT above the upper transformation temperature (e.g., normalizing)
(4) PWHT above the upper transformation temperature followed by heat treatment below the lower transformation temperature (e.g., normalizing or quenching followed by tempering)
(5) PWHT between the upper and lower transformation temperatures
(b) For all other materials, the following postweld heat treatment conditions apply:
(1) no PWHT
(2) PWHT within a specified temperature range

QW-407.2 A change in the postweld heat treatment (see QW-407.1) temperature and time range

The procedure qualification test shall be subjected to PWHT essentially equivalent to that encountered in the fabrication of production welds, including at least $80 \%$ of the aggregate times at temperature(s). The PWHT total time(s) at temperature(s) may be applied in one heating cycle.

QW-407.4 For a procedure qualification test coupon receiving a postweld heat treatment in which the upper transformation temperature is exceeded, the maximum qualified thickness for production welds is 1.1 times the thickness of the test coupon.

QW-407.5 A separate procedure qualification is required for each of the following conditions:
(a) no PWHT
(b) a change of more than $10 \%$ in the number of post heating cycles following the welding interval
(c) PWHT within a specified temperature and time range if heat treatment is performed separately from the welding operation

QW-407.6 A change in postweld heat treatment condition in QW-407.1 or an increase of $25 \%$ or more in total time at postweld heat treating temperature.

QW-407.7 A change in the heat treatment temperature range qualified if heat treatment is applied after fusing.

QW-407.8 A separate PQR is required for each of the following:
(a) no PWHT
(b) a change of more than $10 \%$ in the number of PWHT heating current cycles following the welding cycle
(c) PWHT within a specified temperature and time range if heat treatment is performed separately from the welding operation

QW-407.9 A separate procedure qualification is required for each of the following conditions:
(a) For weld corrosion-resistant overlay of A-No. 8 on all base materials, a change in post weld heat treatment
condition in QW-407.1, or when the total time at post weld heat treatment encountered in fabrication exceeds 200 hr , an increase of $25 \%$ or more in total time at post weld heat treating temperature.
(b) For weld corrosion-resistant overlay of A-No. 9 on all base materials, a change in post weld heat treatment condition in QW-407.1, or an increase of $25 \%$ or more in total time at post weld heat treating temperature.
(c) For all other weld corrosion-resistant overlays on all base materials, a change in post weld heat treatment condition in QW-407.1.

## QW-408 Gas

QW-408.1 The addition or deletion of trailing shielding gas and/or a change in its composition.

QW-408.2 A separate procedure qualification is required for each of the following conditions:
(a) a change from a single shielding gas to any other single shielding gas
(b) a change from a single shielding gas to a mixture of shielding gasses, and vice versa
(c) a change in the specified percentage composition of a shielding gas mixture
(d) the addition or omission of shielding gas

The AWS classification of SFA-5.32 may be used to specify the shielding gas composition.

QW-408.3 A change in the specified flow rate range of the shielding gas or mixture of gases.

QW-408.4 A change in the composition of the orifice or shielding gas.

QW-408.5 The addition or deletion of gas backing, a change in backing gas composition, or a change in the specified flow rate range of the backing gas.

QW-408.6 Any change of environment shielding such as from vacuum to an inert gas, or vice versa.

QW-408.7 A change in the type of fuel gas.
QW-408.8 The omission of inert gas backing except that requalification is not required when welding a singlewelded butt joint with a backing strip or a double-welded butt joint or a fillet weld. This exception does not apply to P-No. 51 through P-No. 53, P-No. 61 through P-No. 62, and P-No. 10I metals.

QW-408.9 For groove welds in P-No. 41 through P-No. 49 and all welds of P-No. 10I, P-No. 10J, P-No. 10K, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals, the deletion of backing gas or a change in the nominal composition of the backing gas from an inert gas to a mixture including non-inert gas(es).

QW-408.10 For P-No. 10I, P-No. 10J, P-No. 10K, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals, the deletion of trailing shielding gas, or a change in the nominal composition of the trailing gas from an inert gas to a mixture including non-inert gas(es), or a decrease of $10 \%$ or more in the trailing gas flow rate.

QW-408.11 The addition or deletion of one or more of the following:
(a) shielding gas
(b) trailing shielding gas
(c) backing gas
(d) plasma-removing gas

QW-408.12 A change of more than 5\% in the flow rate of one or more of the following: shielding gas, trailer shielding gas, backing gas, and plasma-removing gas.

QW-408.13 A change in the position or orientation of plasma-removing gas jet relative to the workpiece (e.g., coaxial transverse to beam).

QW-408.14 A change in the oxygen or fuel gas pressure beyond the range qualified.

QW-408.16 A change of more than $5 \%$ in the flow rate of the plasma-arc gas or powdered metal feed gas recorded on the PQR .

QW-408.17 A change in the plasma-arc gas, shielding gas, or powdered metal feed gas from a single gas to any other single gas, or to a mixture of gases, or vice versa.

QW-408.18 A change of more than $10 \%$ in the gas mixture composition of the plasma-arc gas, shielding gas, or powdered metal feed gas recorded on the PQR .

QW-408.19 A change in the nominal composition of the powder feed gas or (plasma-arc spray) plasma gas qualified.

QW-408.20 A change of more than 5\% in the plasma gas flow rate range qualified.

QW-408.21 A change in the flow rate of the orifice or shielding gas.

QW-408.22 A change in the shielding gas type, gas pressure, or purging time.

QW-408.23 For titanium, zirconium, and their alloys, the deletion of one or more of the following:
(a) shielding gas
(b) trailing shielding gas
(c) backing gas

QW-408.24 For gas-shielded processes, the maximum moisture content (dew point) of the shielding gas. Moisture control may be by specification of shielding gas classifications in SFA-5.32.

## QW-409 Electrical Characteristics

QW-409.1 An increase in heat input, or an increase in volume of weld metal deposited per unit length of weld, over that qualified. The increase may be measured by either of the following:
(a) Heat input [J/in. (J/mm)]

$$
=\frac{\text { Voltage } \times \text { Amperage } \times 60}{\text { Travel Speed }[\mathrm{in} . / \mathrm{min}(\mathrm{~mm} / \mathrm{min})]}
$$

(b) Volume of Weld Metal $=$ an increase in bead size or a decrease in length of weld bead per unit length of electrode.

The requirement for measuring the heat input or volume of deposited weld metal does not apply when the WPS is qualified with a PWHT above the upper transformation temperature or a solution anneal after welding austenitic materials.

QW-409.2 A change from spray arc, globular arc, or pulsating arc to short circuiting arc, or vice versa.

QW-409.3 The addition or deletion of pulsing current to dc power source.

QW-409.4 A change from AC to DC , or vice versa; and in DC welding, a change from electrode negative (straight polarity) to electrode positive (reverse polarity), or vice versa.

QW-409.5 A change of $\pm 15 \%$ from the amperage or voltage ranges in the qualified WPS.

QW-409.6 A change in the beam current of more than $\pm 5 \%$, voltage of more than $\pm 2 \%$, welding speed of more than $\pm 2 \%$, beam focus current of more than $\pm 5 \%$, gun-to-work distance of more than $\pm 5 \%$, or a change in oscillation length or width of more than $\pm 20 \%$ from those previously qualified.

QW-409.7 Any change in the beam pulsing frequency duration from that qualified.

QW-409.8 A change in the range of amperage, or except for SMAW and GTAW welding, a change in the range of voltage. A change in the range of electrode wire feed speed may be used as an alternative to amperage.

QW-409.9 A change in the arc timing of more than $\pm 1 / 10 \mathrm{sec}$.

QW-409.10 A change in amperage of more than $\pm 10 \%$.

QW-409.11 A change in the power source from one model to another.

QW-409.12 A change in type or size of tungsten electrode.

QW-409.13 A change in the shape or dimensions of the welding electrode; a change from one RWMA (Resistance Welding Manufacturer's Association) class electrode material to another.

QW-409.14 Addition or deletion of upslope or downslope current control, or a change of more than $10 \%$ in the slope current time or amplitude.

QW-409.15 A change of more than 5\% in the electrode pressure, the welding current, or the welding time cycle from that qualified, except that requalification is not required if there is a change of not more than $10 \%$ in either the electrode pressure or the welding current or the welding time cycle, provided the remaining two variables remain at the values qualified. A change from AC to DC or vice versa. The addition or deletion of pulsing current to a DC power source. When using pulsing DC current, a change of more than $5 \%$ in the pulse amplitude, width, or number of pulses per cycle from that qualified.

QW-409.16 A change from synchronous to asynchronous timing.

QW-409.17 A change in the power supply primary voltage or frequency, or in the transformer turns ratio, tap setting, choke position, secondary open circuit voltage or phase control setting.

QW-409.18 A change in the procedure or frequency of tip cleaning.

QW-409.19 Any change in the beam pulsing frequency and pulse duration from that qualified.

QW-409.20 Any change in the following variables: mode of operation (from pulsed to continuous and vice versa), energy distribution across the beam (i.e., multimode or gaussian).

QW-409.21 Any change in the following variables: a change of more than $5 \%$ in the power delivered to the work surface as measured by calorimeter or other equivalent methods; a change of more than $2 \%$ in the travel speed; a change of more than $2 \%$ of the ratio of the beam diameter to focal length; a change of more than $2 \%$ of the lens to work distance.

QW-409.22 An increase of more than $10 \%$ in the amperage used in application for the first layer.

QW-409.23 A change of more than $10 \%$ in the ranges of amperage or voltage qualified.

QW-409.24 A change of more than $10 \%$ in the filler wire wattage recorded on the PQR. Wattage is a function of current voltage, and stickout dimension.

QW-409.25 A change of more than $10 \%$ in the plasma-arc current or voltage recorded on the PQR.

QW-409.26 For the first layer only, an increase in heat input of more than $10 \%$ or an increase in volume of weld metal deposited per unit length of weld of more than $10 \%$ over that qualified. The increase may be measured by either of the following:
(a) Heat input [J/in. (J/mm)]

$$
=\frac{\text { Voltage } \times \text { Amperage } \times 60}{\text { Travel Speed }[\mathrm{in} . / \mathrm{min}(\mathrm{~mm} / \mathrm{min})]}
$$

(b) Volume of Weld Metal $=$ an increase in bead size or a decrease in length of weld bead per unit length of electrode.

QW-409.27 A change in the flashing time of more than $10 \%$.

QW-409.28 A change in the upset current time by more than $10 \%$.

QW-409.29
(a) A change in the ratios of heat input or in the volume of weld metal deposited per unit length beyond the following (see figure QW-462.12):
(1) An increase or decrease in the ratio of heat input between the first tempering bead layer and the weld beads deposited against the base metal of more than $20 \%$ for P- or S-No. 1 and P- or S-No. 3 metals and $10 \%$ for all other P- or S-Number metals.
(2) An increase or decrease in the ratio of heat input between the second tempering bead layer and the first tempering bead layer of more than $20 \%$ for P-No. 1 and P-No. 3 metals and $10 \%$ for all other P-Number metals.
(3) The ratio of heat input between subsequent layers shall be maintained until a minimum of $3 / 16 \mathrm{in}$. ( 5 mm ) of weld metal has been deposited over the base metal.
(4) For qualifications where the basis for acceptance is impact testing and the filler metal is exempt from temper bead qualification, the heat input may not exceed $50 \%$ above the heat input qualified for the remaining fill passes.
(5) For qualifications where the basis for acceptance is hardness testing, a decrease of more than $20 \%$ in heat input for the remainder of the fill passes.
(b) Heat input and volume of weld metal per unit length of weld shall be measured using the following methods:
(1) For machine or automatic GTAW or PAW, an increase or decrease of $10 \%$ in the power ratio measured as:

$$
\text { Power Ratio }=\frac{\text { Amperage } \times \text { Voltage }}{\left[(\mathrm{WFS} / \mathrm{TS}) \times A_{f}\right]}
$$

where
$A_{f}=$ the cross-section area of the filler metal wire
$T S=$ the welding travel speed
$W F S=$ the filler metal wire feed speed
(2) For processes other than machine or automatic GTAW or PAW, heat input shall be measured by any of the following methods:
(a) see formula

## (U.S. Customary Units)

Heat Input (J/in.) $=\frac{\text { Voltage } \times \text { Amperage } \times 60}{\text { Travel Speed (in. } / \mathrm{min} \text { ) }}$
(SI Units)
Heat Input $(\mathrm{J} / \mathrm{mm})=\frac{\text { Voltage } \times \text { Amperage } \times 60}{\text { Travel Speed }(\mathrm{mm} / \mathrm{min})}$
(b) Volume of Weld Metal $=$ an increase in bead size or a decrease in length of weld bead per unit length of electrode.
(3) If manual GTAW or PAW is used for making in-process repairs in accordance with QW-290.5, a record of bead size shall be made.

## QW-410 Technique

QW-410.1 For manual or semiautomatic welding, a change from the stringer bead technique to the weave bead technique, or vice versa.

QW-410.2 A change in the nature of the flame, oxidizing to reducing, or vice versa.

QW-410.3 A change in the orifice, cup, or nozzle size.
QW-410.4 A change in the welding technique, forehand to backhand, or vice versa.

QW-410.5 A change in the method of initial and interpass cleaning (brushing, grinding, etc.)

QW-410.6 A change in the method of back gouging.
QW-410.7 For the machine or automatic welding process, a change in width, frequency, or dwell time of oscillation technique.

QW-410.8 A change in the contact tube to work distance.

QW-410.9 A change from multipass per side to single pass per side. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-410.10 A change from single electrode to multiple electrode, or vice versa, for machine or automatic welding only. This limitation does not apply when a WPS
is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

QW-410.11 A change from closed chamber to out-ofchamber conventional torch welding in P-No. 51 through P-No. 53 metals, but not vice versa.

QW-410.12 A change from the melt-in technique to the keyhole technique of welding, or vice versa, or the inclusion of both techniques though each has been individually qualified.

QW-410.14 A change in the angle of the axis of the beam relative to the workpiece.

QW-410.15 A change in the spacing of multiple electrodes for machine or automatic welding.

QW-410.17 A change in the type or model of the welding equipment.

QW-410.18 An increase in the absolute pressure of the vacuum welding environment beyond that qualified.

QW-410.19 Any change in filament type, size, or shape.

QW-410.20 The addition of a wash pass.
QW-410.21 A change of welding from one side to welding from both sides, or vice versa.

QW-410.22 A change in either of the following stud welding parameters: a change of stud gun model; a change in the lift more than $\pm 1 / 32$ in. $(0.8 \mathrm{~mm})$.

QW-410.25 A change from manual or semiautomatic to machine or automatic welding and vice versa.

QW-410.26 The addition or deletion of peening.
QW-410.27 A change in the rotational speed producing a change in the outside surface velocity [ft/min $(\mathrm{m} / \mathrm{min})$ ] greater than $\pm 10 \%$ of the outside surface velocity qualified.

QW-410.28 A change in the thrust load greater than $\pm 10 \%$ of the thrust load qualified.

QW-410.29 A change in the rotational energy greater than $\pm 10 \%$ of the rotational energy qualified.

QW-410.30 Any change in upset dimension (overall loss in length of parts being joined) greater than $\pm 10 \%$ of the upset qualified.

QW-410.31 A change in the method of preparing the base metal prior to welding (e.g., changing from mechanical cleaning to chemical cleaning or to abrasive cleaning, or vice versa).

QW-410.32 A change of more than $10 \%$ in the holding pressure prior to or after welding. A change of more than $10 \%$ in the electrode holding time.

QW-410.33 A change from one welding type to another, or modification of equipment, including Manufacturer, control panel, model number, electrical rating or capacity, type of electrical energy source, or method of applying pressure.

QW-410.34 Addition or deletion of an electrode cooling medium and where it is used.

QW-410.35 A change in the distance between arms or a change in the throat depth.

QW-410.37 A change from single to multiple pass or vice versa.

QW-410.38 A change from multiple-layer to single layer cladding/hardsurfacing, or vice versa.

QW-410.39 A change in the torch type or tip size.
QW-410.40 For submerged-arc welding and electroslag welding, the deletion of a supplementary device for controlling the magnetic field acting on the weld puddle.

QW-410.41 A change of more than $15 \%$ in the travel speed range recorded on the PQR .

QW-410.43 For the torch or workpiece, a change of more than $10 \%$ in the travel speed range qualified.

QW-410.44 A change of more than $15 \%$ in the spraytorch to workpiece distance qualified.

QW-410.45 A change in the method of surface preparation of the base metal to be hard-faced (example: sandblasting versus chemical cleaning).

QW-410.46 A change in the spray-torch model or tip orifice size.

QW-410.47 A change of more than $10 \%$ in the fusing temperature range qualified. A change in the rate of cooling from the fusing temperature of more than $50^{\circ} \mathrm{F} / \mathrm{hr}$ $\left(28^{\circ} \mathrm{C} / \mathrm{hr}\right)$, a change in the fusing method (e.g., torch, furnace, induction).

QW-410.48 A change in the constricted arc from transferable to nontransferable or vice versa.

QW-410.49 A change in the diameter of the plasma torch-arc constricting orifice.

QW-410.50 A change in the number of electrodes acting on the same welding puddle.

QW-410.52 A change in the method of delivering the filler metal to the molten pool, such as from the
leading or trailing edge of the torch, the sides of the torch, or through the torch.

QW-410.53 A change of more than $20 \%$ in the center-to-center weld bead distance.

QW-410.54 A change in the upset length or force of more than $10 \%$.

QW-410.55 A change in the distance between the clamping dies of more than $10 \%$ or a change in the surface preparation of the clamping area.

QW-410.56 A change in the clamping force by more than $10 \%$.

QW-410.57 A change in more than $10 \%$ of the forward or reverse speed.

QW-410.58 The deletion of surface temper beads (see figure QW-462.12) or a change from surface temper
beads that cover the weld surface to beads that are only deposited along the toes of the weld.

QW-410.59 A change from machine or automatic welding to manual or semiautomatic welding.

QW-410.60 The addition of thermal methods to prepare the surface to be welded unless the WPS requires that the metal be ground to bright metal before welding.

QW-410.61 A change in the approximate distance from the edge of the surface temper beads to the toe of the weld (see figure QW-462.12).

QW-410.62 The method of removal of surface temper bead reinforcing layer when it will be removed, including provisions to prevent overheating of the weld surface.

QW-410.63 The extent of overlap of beads in a layer.

QW-416
WELDING VARIABLES
Welder Performance

| Paragraph ${ }^{1}$ |  |  | Brief of Variables | Essential |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \text { OFW } \\ \text { QW-352 } \end{gathered}$ | $\begin{aligned} & \text { SMAW } \\ & \text { QW-353 } \end{aligned}$ | $\begin{gathered} \text { SAW } \\ \text { QW-354 } \end{gathered}$ | $\begin{aligned} & \text { GMAW }{ }^{2} \\ & \text { QW-355 } \end{aligned}$ | $\begin{aligned} & \text { GTAW } \\ & \text { QW-356 } \end{aligned}$ | $\begin{gathered} \text { PAW } \\ \text { QW-357 } \end{gathered}$ |
| QW-402 <br> Joints | . 4 |  | Backing |  | X |  | X | X | X |
|  | . 7 |  | Backing | X |  |  |  |  |  |
| QW-403 <br> Base <br> Metal | . 2 |  | Maximum qualified | X |  |  |  |  |  |
|  | . 16 |  | Pipe diameter |  | X | X | X | X | X |
|  | . 18 |  | P-Number | X | X | X | X | X | X |
| QW-404 <br> Filler <br> Metals | . 14 |  | Filler | X |  |  |  | X | X |
|  | . 15 |  | F-Number | X | X | X | X | X | X |
|  | . 22 |  | Inserts |  |  |  |  | X | X |
|  | . 23 |  | Solid or metal-cored to flux-cored |  |  |  |  | X | X |
|  | . 30 |  | $t$ Weld deposit |  | X | X | X | X | X |
|  | . 31 |  | $t$ Weld deposit | X |  |  |  |  |  |
|  | . 32 |  | $t$ Limit (s. cir. arc) |  |  |  | X |  |  |
| QW-405 <br> Positions | . 1 |  | Position | X | X | X | X | X | X |
|  | . 3 |  | $\uparrow \downarrow$ Vert. welding |  | X |  | X | X | X |
| $\begin{aligned} & \text { QW-408 } \\ & \text { Gas } \end{aligned}$ | . 7 |  | Type fuel gas | X |  |  |  |  |  |
|  | . 8 |  | Inert backing |  |  |  | X | X | X |
| QW-409 <br> Electrical | . 2 |  | Transfer mode |  |  |  | X |  |  |
|  | . 4 |  | Current or polarity |  |  |  |  | X |  |

Welding Processes:

| OFW | Oxyfuel gas welding |
| :--- | :--- |
| SMAW | Shielded metal-arc welding |
| SAW | Submerged-arc welding |
| GMAW | Gas metal-arc welding |
| GTAW | Gas tungsten-arc welding |
| PAW | Plasma-arc welding |

Legend:

| $\phi$ | Change | $t$ | Thickness |
| :--- | :--- | :--- | :--- |
| + | Addition | $\uparrow$ | Uphill |
| - | Deletion | $\downarrow$ | Downhill |

NOTES:
(1) For description, see Section IV.
(2) Flux-cored arc welding as shown in QW-355, with or without additional shielding from an externally supplied gas or gas mixture, is included.

## 04 QW-420 Material Groupings

QW-420.1 P-Numbers and S-Numbers. Base metals have been assigned P -Numbers or S-Numbers for the purpose of reducing the number of welding and brazing procedure qualifications required. In addition, ferrous base metals have been assigned Group Numbers creating subsets of P-Numbers and S-Numbers that are used when WPSs are required to be qualified by impact testing by other Sections or Codes. These assignments are based essentially on comparable base metal characteristics, such as composition, weldability, brazeability, and mechanical properties, where this can logically be done. These assignments do not imply that base metals may be indiscriminately substituted for a base metal that was used in the qualification test without consideration of compatibility from the standpoint of metallurgical properties, postweld heat treatment, design, mechanical properties, and service requirements. The following table shows the assignment groups for various alloy systems:

| Base Metal | Welding | Brazing |
| :---: | :---: | :---: |
| Steel and steel alloys | P- or S-No. 1 through P - or S No. 11 incl. P- or S-No. 5A, 5B, and 5C | $\begin{aligned} & \text { P- or S-No. } 101 \\ & \text { through P- or S- } \\ & \text { No. } 103 \end{aligned}$ |
| Aluminum and alu-minum-base alloys | P- or S-No. 21 through P - or S No. 25 | P- or S-No. 104 and P- or S-No. 105 |
| Copper and copperbase alloys | P- or S-No. 31 through P - or S No. 35 | P- or S-No. 107 and P- or S-No. 108 |
| Nickel and nickelbase alloys | P- or S-No. 41 through P - or S No. 49 | P- or S-No. 110 through P- or SNo. 112 |
| Titanium and tita-nium-base alloys | P- or S-No. 51 through P - or S No. 53 | P- or S-No. 115 |
| Zirconium and zir-conium-base alloys | P- or S-No. 61 through P - or S No. 62 | P- or S-No. 117 |

When a base metal with a UNS number designation is assigned a P - or S -Number or P - or S -Number plus Group Number, then a base metal listed in a different ASME material specification with the same UNS number shall be considered that P - or $\mathrm{S}-\mathrm{Number}$ or P - or S Number plus Group Number. For example, SB-163, UNS N08800 is P-No. 45; therefore, all ASME specifications listing a base metal with the UNS N08800 designation
shall be considered P-No. 45 (i.e., SB-407, SB-408, SB514 , etc.) whether or not these specifications are listed in table QW/QB-422. When utilizing this provision, only base metals listed in table QW/QB-422 may be used for test coupons since a minimum tensile value is required for procedure qualification.

There are instances where materials assigned to one P- or S-Number or Group Number have been reassigned to a different P - or S-Number or Group Number in later editions. Procedure and performance qualifications that were qualified under the previous P - or S-Numbers or Group Number assignment may continue to be used under the new P- or S-Number or Group Number assignment. See QW-200.2(c).
The values given in the column heading "Minimum Specified Tensile" of table QW/QB-422, are the acceptance values for the tensile tests of the welding or brazing procedure qualification, except as otherwise allowed in QW-153 or QB-153.

QW-420.2 S-Numbers. S-Numbers are assigned to materials that are acceptable for use by the ASME B31 Code for Pressure Piping, or by selected Boiler and Pressure Vessel Code Cases, but which are not included within ASME Boiler and Pressure Vessel Code Material Specifications (Section II).

Material produced under an ASTM specification shall be considered to have the same S-Number or S-Number plus Group Number as that of the P-Number or P-Number plus Group Number assigned to the same grade or type material in the corresponding ASME specification (i.e., SA-240 Type 304 is assigned P-No. 8, Group No. 1; therefore, A 240 Type 304 is considered S-No. 8, Group No. 1).

Some variables and figures may not specifically address S-Numbers. When this occurs, the requirements regarding P-Numbers and P-Number Group Numbers shall apply equally to materials that are assigned to corresponding S-Numbers and S-Number Group Numbers. However, if procedure qualification testing was done using material assigned an S-Number or S-Number Group Number, the range qualified is limited to materials that are assigned S-Numbers or S-Numbers Group Numbers (i.e., qualification using a P -Number material qualifies corresponding S-Number materials; qualification using an S-Number material qualifies corresponding S-Number materials but not corresponding P-Number materials; qualification of welders using a P-Number material qualifies them to weld on corresponding S-Number materials and vice versa).
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS Grouping of Base Metals for Qualification

 Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| A 167 | Type 309 | S30900 | 75 (515) | $\ldots$ | . . | 8 | 2 | $\ldots$ | 102 | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Plate, sheet, \& strip |
| A 167 | Type 309S | S30908 | 75 (515) | ... |  | 8 | 2 | . . | 102 | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Plate, sheet, \& strip |
| A 167 | Type 310 | S31000 | 75 (515) | $\ldots$ | $\ldots$ | 8 | 2 | $\ldots$ | 102 | 25Cr-20Ni | Plate, sheet, \& strip |
| A 167 | Type 310S | S31008 | 75 (515) | ... | . . . | 8 | 2 | ... | 102 | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Plate, sheet, \& strip |
| A 167 | Type 316L | S31603 | 70 (485) | $\ldots$ |  | 8 | 1 | . . | 102 | 16Cr-12Ni-2Mo | Plate, sheet, \& strip |
| A 167 | Type 317 | S31700 | 75 (515) | $\ldots$ | $\ldots$ | 8 | 1 | $\ldots$ | 102 | 18Cr-13Ni-3Mo | Plate, sheet, \& strip |
| A 167 | Type 317L | S31703 | 75 (515) | $\ldots$ | $\ldots$ | 8 | 1 | ... | 102 | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Plate, sheet, \& strip |
| A 167 | Type 321 | S32100 | 75 (515) | $\ldots$ | $\ldots$ | 8 | 1 | $\ldots$ | 102 | 18Cr-10Ni-Ti | Plate, sheet, \& strip |
| A 167 | Type 347 | S34700 | 75 (515) | ... | ... | 8 | 1 | ... | 102 | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Plate, sheet, \& strip |
| A 167 | Type 348 | S34800 | 75 (515) | $\ldots$ | . | 8 | 1 | $\ldots$ | 102 | 18Cr-10Ni-Cb | Plate, sheet, \& strip |
| SA-178 | A | K01200 | 47 (325) | 1 | 1 | . . | $\ldots$ | 101 | ... | C | E.R.W. tube |
| SA-178 | C | K03503 | 60 (415) | 1 | 1 | . . | $\ldots$ | 101 | $\ldots$ | C | E.R.W. tube |
| SA-178 | D | ... | 70 (485) | 1 | 2 |  | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | E.R.W. tube |
| SA-179 |  | K01200 | 47 (325) | 1 | 1 |  | $\ldots$ | 101 | $\ldots$ | C | Smls. tube |
| SA-181 | Cl. 60 | K03502 | 60 (415) | 1 | 1 | $\ldots$ | ... | 101 | $\ldots$ | C-Si | Pipe flange \& fittings |
| SA-181 | CI. 70 | K03502 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Si | Pipe flange \& fittings |
| SA-182 | F12, Cl. 1 | K11562 | 60 (415) | 4 | 1 | ... | ... | 102 | ... | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forgings |
| SA-182 | F12, Cl. 2 | K11564 | 70 (485) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forgings |
| SA-182 | F11, Cl. 2 | K11572 | 70 (485) | 4 | 1 | . . . | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Forgings |
| SA-182 | F11, Cl. 3 | K11572 | 75 (515) | 4 | 1 | $\ldots$ | . . . | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Forgings |
| SA-182 | F11, Cl. 1 | K11597 | 60 (415) | 4 | 1 |  |  | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Forgings |
| SA-182 | F2 | K12122 | 70 (485) | 3 | 2 | ... | $\ldots$ | 101 | ... | 0.5Cr-0.5Mo | Forgings |
| SA-182 | F1 | K12822 | 70 (485) | 3 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-0.5Mo | Forgings |
| SA-182 | F22, Cl. 1 | K21590 | 60 (415) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-182 | F22, Cl. 3 | K21590 | 75 (515) | 5A | 1 | . . . | $\ldots$ | 102 | ... | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-182 | FR | K22035 | 63 (435) | 9 A | 1 | $\ldots$ | $\ldots$ | 101 | ... | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Forgings |
| SA-182 | F21 | K31545 | 75 (515) | 5A | 1 | $\ldots$ | ... | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-182 | F3V | K31830 | 85 (585) | 5 C | 1 | . . . | $\ldots$ | 102 | . . | 3Cr-1Mo-V-Ti-B | Forgings |
| SA-182 | F22V | K31835 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-182 | F5 | K41545 | 70 (485) | 5B | 1 | $\ldots$ | ... | 102 | $\ldots$ | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forgings |
| SA-182 | F5a | K42544 | 90 (620) | 5B | 1 | . . . | . . | 102 | . . | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forgings |
| SA-182 | F9 | K90941 | 85 (585) | 5B | 1 | ... | $\ldots$ | 102 | . . | $9 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-182 | F91 | K90901 | 85 (585) | 5B | 2 | $\ldots$ |  | 102 | . . | $9 \mathrm{Cr}-1 \mathrm{Mo-V}$ | Forgings |
| SA-182 | F6a, Cl. 1 | S41000 | 70 (485) | 6 | 1 | . . . | ... | 102 | ... | 13 Cr | Forgings |
| SA-182 | F6a, CI. 2 | S41000 | 85 (585) | 6 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 13 Cr | Forgings |
| SA-182 | FXM-19 | S20910 | 100 (690) | 8 | 3 | . . . | . . | 102 | $\ldots$ | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Forgings |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. |  |  |  | P- <br> No. | Group No. | SNo. | Group No. | P- <br> No. | S- <br> No. |  |  |
| SA-182 | FXM-11 | S21904 | 90 (620) | 8 | 3 | . . |  | 102 | . . | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Forgings |
| SA-182 | F304 | S30400 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings > 5 in . ( 127 mm ) |
| SA-182 | F304 | S30400 | 75 (515) | 8 | 1 | . . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-182 | F304L | S30403 | 65 (450) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F304L | S30403 | 70 (485) | 8 | 1 | . . |  | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-182 | F304H | S30409 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F304H | S30409 | 75 (515) | 8 | 1 | $\ldots$. |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-182 | F304N | S30451 | 80 (550) | 8 | 1 | $\ldots$ |  | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forgings |
| SA-182 | F304LN | S30453 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F304LN | S30453 | 75 (515) | 8 | 1 | . . |  | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forgings |
| SA-182 | F46 | S30600 | 78 (540) | 8 | 1 | . . |  | 102 | . . | $18 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Si}$ | Forgings |
| SA-182 | F45 | S30815 | 87 (600) | 8 | 2 | . . |  | 102 |  | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Forgings |
| SA-182 | F310 | S31000 | 70 (485) | 8 | 2 | . . |  | 102 |  | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F310 | S31000 | 75 (515) | 8 | 2 | $\ldots$ | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Forgings |
| SA-182 | F50 | S31200 | 100 (690) | 10 H | 1 | . . . | . . | 102 | . . . | $25 \mathrm{Cr}-6 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Forgings |
| SA-182 | F44 | S31254 | 94 (650) | 8 | 4 | . . | . . | 102 | . . | 20Cr-18Ni-6Mo | Forgings |
| SA-182 | F316 | S31600 | 70 (485) | 8 | 1 | $\ldots$ |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings $>5 \mathrm{in}$. $(127 \mathrm{~mm}$ ) |
| SA-182 | F316 | S31600 | 75 (515) | 8 | 1 | . . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings |
| SA-182 | F316L | S31603 | 65 (450) | 8 | 1 | $\ldots$ | . . | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | . . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings |
| SA-182 | F316H | S31609 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings > 5 in . ( 127 mm ) |
| SA-182 | F316H | S31609 | 75 (515) | 8 | 1 | $\cdots$ |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings |
| SA-182 | F316N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Forgings |
| SA-182 | F316LN | S31653 | 70 (485) | 8 | 1 | $\ldots$ | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F316LN | S31653 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Forgings |
| SA-182 | F317 | S31700 | 70 (485) | 8 | 1 | . . . | . . | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F317 | S31700 | 75 (515) | 8 | 1 |  | . $\cdot$ | 102 |  | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Forgings |
| SA-182 | F317L | S31703 | 65 (450) | 8 | 1 | . . | . . | 102 | $\ldots$ | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F317L | S31703 | 70 (485) | 8 | 1 | . . | . . | 102 | . . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Forgings |
| SA-182 | F51 | S31803 | 90 (620) | 10 H | 1 | . . | . . | 102 | . . . | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Forgings |
| SA-182 | F321 | S32100 | 70 (485) | 8 | 1 | . . . | . . . | 102 | . . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forgings $>5 \mathrm{in}$. ( 127 mm ) |
| SA-182 | F321 | S32100 | 75 (515) | 8 | 1 | $\cdots$ | . $\cdot$ | 102 | . $\cdot$ | 18Cr-10Ni-Ti | Forgings |
| SA-182 | F321H | S32109 | 70 (485) | 8 | 1 | $\ldots$ |  | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F321H | S32109 | 75 (515) | 8 | 1 | . | $\ldots$ | 102 | . . | 18Cr-10Ni-Ti | Forgings |
| SA-182 | F55 | S32760 | 109 (750) | . . | . . | 10 H | 1 | . | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Forgings |
| SA-182 | F10 | S33100 | 80 (550) | 8 | 2 | . . . | . | 102 | . . | $20 \mathrm{Ni}-8 \mathrm{Cr}$ | Forgings |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS No. |  | P. <br> No. | Group No. | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ | Group No. | P. <br> No. | S- <br> No. |  |  |
| SA-182 | F347 | S34700 | 70 (485) | 8 | 1 |  | $\ldots$ | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F347 | S34700 | 75 (515) | 8 | 1 | . . . |  | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-182 | F347H | S34709 | 70 (485) | 8 | 1 | . . | . . | 102 | . . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F347H | S34709 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-182 | F348 | S34800 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings > 5 in. ( 127 mm ) |
| SA-182 | F348 | S34800 | 75 (515) | 8 | 1 | . . | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-182 | F348H | S34809 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings > 5 in . ( 127 mm ) |
| SA-182 | F348H | S34809 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-182 | F6b | S41026 | 110 (760) | 6 | 3 | . . . | . . | 102 | . . | $13 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forgings |
| SA-182 | F6NM | S41500 | 115 (795) | 6 | 4 | . . | . . | 102 | . . | $13 \mathrm{Cr}-4.5 \mathrm{Ni}-\mathrm{Mo}$ | Forgings |
| SA-182 | F429 | S42900 | 60 (415) | 6 | 2 | $\ldots$ | . . | 102 | . . | 15 Cr | Forgings |
| SA-182 | F430 | S43000 | 60 (415) | 7 | 2 | . . | . . | 102 | . . | 17 Cr | Forgings |
| SA-182 | FXM-27Cb | S44627 | 60 (415) | 10I | 1 |  |  | 102 |  | $27 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| A 182 | F60 | S32205 | 95 (655) | $\ldots$ | . . | 10 H | 1 | . . | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Forgings |
| A 182 | F6a, CI. 3 | S41000 | 110 (760) | . . . | . . | 6 | 3 | . . | 102 | 13 Cr | Forgings |
| A 182 | F6a, CI. 4 | S41000 | 130 (895) | $\ldots$ | $\ldots$ | 6 | 3 | . . | 102 | 13 Cr | Forgings |
| A 182 | S34565 | S34565 | 115 (795) | . $\cdot$ | . . | 8 | 4 |  | . . . | $24 \mathrm{Cr}-17 \mathrm{Ni}-6 \mathrm{Mn}-4.5 \mathrm{Mo}-\mathrm{N}$ | Forgings |
| SA-192 |  | K01201 | 47 (325) | 1 | 1 | . . | $\ldots$ | 101 |  | C-Si | Smls. tube |
| SA-202 | A | K11742 | 75 (515) | 4 | 1 | . . | . . | 101 | . . | $0.5 \mathrm{Cr}-1.25 \mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-202 | B | K12542 | 85 (585) | 4 | 1 |  | $\ldots$ | 101 |  | $0.5 \mathrm{Cr}-1.25 \mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-203 | A | K21703 | 65 (450) | 9 A | 1 | . . | . . | 101 | . . | 2.5 Ni | Plate |
| SA-203 | B | K22103 | 70 (485) | 9 A | 1 | . . | $\ldots$ | 101 | . . | 2.5 Ni | Plate |
| SA-203 | D | K31718 | 65 (450) | 9 B | 1 | . . | $\ldots$ | 101 | . . | 3.5 Ni | Plate |
| SA-203 | E | K32018 | 70 (485) | 9 B | 1 | . . | . . | 101 | . . | 3.5 Ni | Plate |
| SA-203 | F | . . . | 75 (515) | 9 B | 1 | . . | $\ldots$ | 101 | . . | 3.5 Ni | Plate $>2$ in. ( 51 mm ) |
| SA-203 | F | . . | 80 (550) | 9 B | 1 | . . | . . | 101 | . . . | 3.5 Ni | Plate, 2 in. (51 mm) \& under |
| SA-204 | A | K11820 | 65 (450) | 3 | 1 | . . | $\ldots$ | 101 | . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Plate |
| SA-204 | B | K12020 | 70 (485) | 3 | 2 | . . | . . | 101 | . . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Plate |
| SA-204 | C | K12320 | 75 (515) | 3 | 2 | $\cdots$ | $\ldots$ | 101 | . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Plate |
| SA-209 | Tlb | K11422 | 53 (365) | 3 | 1 | . . . | . . | 101 | . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Smls. tube |
| SA-209 | T1 | K11522 | 55 (380) | 3 | 1 | . . . | . . | 101 | . . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Smls. tube |
| SA-209 | Tla | K12023 | 60 (415) | 3 | 1 | $\cdots$ | $\ldots$ | 101 | . $\cdot$ | $\mathrm{C}-0.5 \mathrm{Mo}$ | Smls. tube |
| SA-210 | A-1 | K02707 | 60 (415) | 1 | 1 | . . . | . . | 101 | . . . | $\mathrm{C}-\mathrm{Si}$ | Smls. tube |
| SA-210 | C | K03501 | 70 (485) | 1 | 2 | . $\cdot$ | $\ldots$ | 101 | $\cdots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Smls. tube |
| A 211 | A570-30 | K02502 | 49 (340) | . . . | . . | 1 | 1 | . . . | 101 | C | Welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT’D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum <br> Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P- No. | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-213 | TP316N | S31651 | 80 (550) | 8 | 1 | . | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Smls. tube |
| SA-213 | TP316LN | S31653 | 75 (515) | 8 | 1 | . . . | . . . | 102 | . . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Smls. tube |
| SA-213 | S31725 | S31725 | 75 (515) | 8 | 4 |  |  | 102 |  | 19Cr-15Ni-4Mo | Smls. tube |
| SA-213 | S31726 | S31726 | 80 (550) | 8 | 4 | $\ldots$ | . . | 102 | . . | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Smls. tube |
| SA-213 | TP321 | S32100 | 75 (515) | 8 | 1 | . . . | ... | 102 | . . | 18Cr-10Ni-Ti | Smls. tube |
| SA-213 | TP321H | S32109 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-10Ni-Ti | Smls. tube |
| SA-213 | TP347 | S34700 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. tube |
| SA-213 | TP347H | S34709 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. tube |
| SA-213 | TP347HFG |  | 80 (550) | 8 | 1 | . . . | . . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. tube |
| SA-213 | TP348 | S34800 | 75 (515) | 8 | 1 | . . | . . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. tube |
| SA-213 | TP348H | S34809 | 75 (515) | 8 | 1 | . . . | $\ldots$ | 102 | . . | 18Cr-10Ni-Cb | Smls. tube |
| SA-213 | XM-15 | S38100 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-18 \mathrm{Ni}-2 \mathrm{Si}$ | Smls. tube |
| SA-214 | ... | K01807 | 47 (325) | 1 | 1 | .. | $\ldots$ | 101 | ... | C | E.R.W. tube |
| SA-216 | WCA | J02502 | 60 (415) | 1 | 1 | . . . | $\ldots$ | 101 | ... | C-Si | Castings |
| SA-216 | WCC | J02503 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Castings |
| SA-216 | WCB | J03002 | 70 (485) | 1 | 2 | . . | $\ldots$ | 101 | . . | C-Si | Castings |
| SA-217 | WC6 | J12072 | 70 (485) | 4 | 1 | ... | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-217 | WC4 | J12082 | 70 (485) | 4 | 1 | . . . | $\ldots$ | 101 | . . | $1 \mathrm{Ni}-0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-217 | WC1 | J12524 | 65 (450) | 3 | 1 | . . . | ... | 101 | . . | C-0.5Mo | Castings |
| SA-217 | WC9 | J21890 | 70 (485) | 5 A | 1 | . . | . . . | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Castings |
| SA-217 | WC5 | J22000 | 70 (485) | 4 | 1 | . . . | $\ldots$ | 101 | . . | $0.75 \mathrm{Ni}-1 \mathrm{Mo}-0.75 \mathrm{Cr}$ | Castings |
| SA-217 | C5 | J42045 | 90 (620) | 5B | 1 | . . . | $\ldots$ | 102 | . . . | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-217 | C12 | J82090 | 90 (620) | 5B | 1 | . . . | . . | 102 | . . . | $9 \mathrm{Cr-1Mo}$ | Castings |
| SA-217 | CA15 | J91150 | 90 (620) | 6 | 3 | ... |  | 102 |  | 13 Cr | Castings |
| A 217 | Cl2A | J84090 | 85 (585) | $\ldots$ | ... | 5B | 2 | $\ldots$ | 102 | $9 \mathrm{Cr-1Mo-V}$ | Castings |
| SA-225 | D | K12004 | 75 (515) | 10A | 1 | ... | $\ldots$ | 101 | . . | Mn-0.5Ni-V | Plate > 3 in. ( 76 mm ) |
| SA-225 | D | K12004 | 80 (550) | 10 A | 1 | . . . | . . . | 101 | ... | $\mathrm{Mn}-0.5 \mathrm{Ni}-\mathrm{V}$ | Plate, 3 in. (76 mm) \& under |
| SA-225 | C | K12524 | 105 (725) | 10A | 1 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{Mn}-0.5 \mathrm{Ni}-\mathrm{V}$ | Plate |
| SA-234 | WPB | K03006 | 60 (415) | 1 | 1 | ... | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Piping fitting |
| SA-234 | WPC | K03501 | 70 (485) | 1 | 2 | $\ldots$ | . . | 101 | . . . | C-Mn-Si | Piping fitting |
| SA-234 | WP11, CI. 1 | ... | 60 (415) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 1.25Cr-0.5Mo-Si | Piping fitting |
| SA-234 | WP12, Cl. 1 | K12062 | 60 (415) | 4 | 1 | . . . | ... | 101 | $\ldots$ | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Piping fitting |
| SA-234 | WP1 | K12821 | 55 (380) | 3 | 1 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Piping fitting |
| SA-234 | WP22, Cl. 1 | K21590 | 60 (415) | 5 A | 1 | $\ldots$ | . . | 102 | ... | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Piping fitting |
| SA-234 | WPR | K22035 | 63 (435) | 9 A | 1 | . . | . . | 101 | . . | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Piping fitting |
| SA-234 | WP5 | K41545 | 60 (415) | 5 B | 1 | . . . | $\ldots$ | 102 | . . . | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Piping fitting |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

（a，LNOJ）Syヨgwnn－s anv Syヨgwnn－d SnOyyヨコNON／Snoyyヨa ટてt－go／MO Grouping of Base Metals for Qualification

| Ferrous（CONT＇D） |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | UNS No． | Minimum Specified Tensile， ksi（MPa） | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec．No． | Type or Grade |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No． | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ | Group No． | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA－240 | Type 316 | S31600 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 |  | 16Cr－12Ni－2Mo | Plate，sheet，\＆strip |
| SA－240 | Type 316L | S31603 | 70 （485） | 8 | 1 |  |  | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Plate，sheet，\＆strip |
| SA－240 | Type 316H | S31609 | 75 （515） | 8 | 1 | $\ldots$ | ．． | 102 | $\ldots$ | 16Cr－12Ni－2Mo | Plate，sheet，\＆strip |
| SA－240 | Type 316Ti | S31635 | 75 （515） | 8 | 1 | $\ldots$ |  | 102 |  | 16Cr－12Ni－2Mo－Ti | Plate，sheet，\＆strip |
| SA－240 | Type 316Cb | S31640 | 75 （515） | 8 | 1 | ．． | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{Cb}$ | Plate，sheet，\＆strip |
| SA－240 | Type 316N | S31651 | 80 （550） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr－12Ni－2Mo－N | Plate，sheet，\＆strip |
| SA－240 | Type 316LN | S31653 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Plate，sheet，\＆strip |
| SA－240 | Type 317 | S31700 | 75 （515） | 8 | 1 | $\ldots$ | ．．． | 102 | ．．． | 18Cr－13Ni－3Mo | Plate，sheet，\＆strip |
| SA－240 | Type 317L | S31703 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Plate，sheet，\＆strip |
| SA－240 | S31725 | S31725 | 75 （515） | 8 | 4 |  |  | 102 | $\ldots$ | $19 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Mo}$ | Plate，sheet，\＆strip |
| SA－240 | S31726 | S31726 | 80 （550） | 8 | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 19Cr－15．5Ni－4Mo | Plate，sheet，\＆strip |
| SA－240 | S31753 | S31753 | 80 （550） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr－13Ni－3Mo－N | Plate，sheet，\＆strip |
| SA－240 | S31803 | S31803 | 90 （620） | 10 H | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Plate，sheet，\＆strip |
| SA－240 | Type 321 | S32100 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr－10Ni－Ti | Plate，sheet，\＆strip |
| SA－240 | Type 321H | S32109 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Plate，sheet，\＆strip |
| SA－240 | S32550 | S32550 | 110 （760） | 10 H | 1 | ．．． | $\ldots$ | 102 | $\ldots$ | $25 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-2 \mathrm{Cu}$ | Plate，sheet，\＆strip |
| SA－240 | S32760 | S32760 | 108 （745） | ．．． | ．． | 10 H | 1 | ．．． | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Plate，sheet，\＆strip |
| SA－240 | Type 329 | S32900 | 90 （620） | 10 H | 1 | ．．． | ．．． | 102 | ．．． | $26 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}$ | Plate，sheet，\＆strip |
| SA－240 | S32950 | S32950 | 100 （690） | 10 H | 1 |  | $\ldots$ | 102 | ．． | $26 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Plate，sheet，\＆strip |
| SA－240 | Type 347 | S34700 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Plate，sheet，\＆strip |
| SA－240 | Type 347H | S34709 | 75 （515） | 8 | 1 |  |  | 102 |  | 18Cr－10Ni－Cb | Plate，sheet，\＆strip |
| SA－240 | Type 348 | S34800 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr－10Ni－Cb | Plate，sheet，\＆strip |
| SA－240 | Type 348H | S34809 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ．． | 18Cr－10Ni－Cb | Plate，sheet，\＆strip |
| SA－240 | Type XM－15 | S38100 | 75 （515） | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ．．． | $18 \mathrm{Cr}-18 \mathrm{Ni}-2 \mathrm{Si}$ | Plate，sheet，\＆strip |
| SA－240 | Type 405 | S40500 | 60 （415） | 7 | 1 | $\ldots$ |  | 102 | $\ldots$ | $12 \mathrm{Cr}-1 \mathrm{Al}$ | Plate，sheet，\＆strip |
| SA－240 | Type 409 | S40910 | 55 （380） | 7 | 1 | $\ldots$ | $\ldots$ | 102 | ．． | $11 \mathrm{Cr}-\mathrm{Ti}$ | Plate，sheet，\＆strip |
| SA－240 | Type 409 | S40920 | 55 （380） | 7 | 1 | $\ldots$ | $\ldots$ | 102 | ．．． | $11 \mathrm{Cr}-\mathrm{Ti}$ | Plate，sheet，\＆strip |
| SA－240 | Type 409 | S40930 | 55 （380） | 7 | 1 | ．．． | ．． | 102 | ．． | $11 \mathrm{Cr}-\mathrm{Ti}$ | Plate，sheet，\＆strip |
| SA－240 | Type 410 | S41000 | 65 （450） | 6 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | ${ }^{13 \mathrm{Cr}}$ | Plate，sheet，\＆strip |
| SA－240 | Type 410S | S41008 | 60 （415） | 7 | 1 | ．．． | ．．． | 102 | ．．． | 13 Cr | Plate，sheet，\＆strip |
| SA－240 | S41500 | S41500 | 115 （795） | 6 | 4 | $\ldots$ | ．．． | 102 | ．． | $13 \mathrm{Cr}-4.5 \mathrm{Ni}-\mathrm{Mo}$ | Plate，sheet，\＆strip |
| SA－240 | Type 429 | S42900 | 65 （450） | 6 | 2 | ．．． | $\ldots$ | 102 |  | 15 Cr | Plate，sheet，\＆strip |
| SA－240 | Type 430 | S43000 | 65 （450） | 7 | 2 | $\ldots$ |  | 102 | ．． | 17 Cr | Plate，sheet，\＆strip |
| SA－240 | Type 439 | S43035 | 60 （415） | 7 | 2 | ．． | $\cdots$ | 102 | ．．． | 18Cr－Ti | Plate，sheet，\＆strip |
| SA－240 | S44400 | S44400 | 60 （415） | 7 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr－2Mo | Plate，sheet，\＆strip |
| SA－240 | Type XM－33 | S44626 | 68 （470） | 101 | 1 | ．．． | ．． | 102 | ．．． | $27 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{Ti}$ | Plate，sheet，\＆strip |
| SA－240 | Type XM－27 | S44627 | 65 （450） | 10I | 1 | $\ldots$ | ． | 102 | $\ldots$ | $27 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate，sheet，\＆strip |

WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P. <br> No. | Group No. | S- <br> No. | Group No. | P. <br> No. | S- <br> No. |  |  |
| SA-240 | S44635 | S44635 | 90 (620) | 10 I | 1 | . . | . . | 102 | . . . | $25 \mathrm{Cr}-4 \mathrm{Ni}-4 \mathrm{Mo}-\mathrm{Ti}$ | Plate, sheet, \& strip |
| SA-240 | S44660 | S44660 | 85 (585) | 10K | 1 | . . . |  | 102 |  | $26 \mathrm{Cr}-3 \mathrm{Ni}-3 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SA-240 | S44700 | S44700 | 80 (550) | 10 J | 1 | $\ldots$ |  | 102 |  | $29 \mathrm{Cr}-4 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SA-240 | S44800 | S44800 | 80 (550) | 10K | 1 | . . |  | 102 | . . | $29 \mathrm{Cr}-4 \mathrm{Mo}-2 \mathrm{Ni}$ | Plate, sheet, \& strip |
| A 240 | S32205 | S32205 | 90 (620) | . . |  | 10 H | 1 | . | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Plate, sheet, \& strip |
| A 240 | S34565 | S34565 | 115 (795) |  |  | 8 | 4 | . . | . . | $24 \mathrm{Cr}-17 \mathrm{Ni}-6 \mathrm{Mn}-4.5 \mathrm{Mo}-\mathrm{N}$ | Plate, sheet, \& strip |
| SA-249 | TP201 | S20100 | 95 (655) | 8 | 3 | . . |  | 102 |  | $17 \mathrm{Cr}-4 \mathrm{Ni}-6 \mathrm{Mn}$ | Welded tube |
| SA-249 | TP202 | S20200 | 90 (620) | 8 | 3 | . . |  | 102 | . . | $18 \mathrm{Cr}-5 \mathrm{Ni}-9 \mathrm{Mn}$ | Welded tube |
| SA-249 | TPXM-19 | S20910 | 100 (690) | 8 | 3 | . . | . . | 102 | . . | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Welded tube |
| SA-249 | TPXM-29 | S24000 | 100 (690) | 8 | 3 | . . . |  | 102 |  | $18 \mathrm{Cr}-3 \mathrm{Ni}-12 \mathrm{Mn}$ | Welded tube |
| SA-249 | TP304 | S30400 | 75 (515) | 8 | 1 |  |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP304L | S30403 | 70 (485) | 8 | 1 | . . . |  | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP304H | S30409 | 75 (515) | 8 | 1 | . . |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP304N | S30451 | 80 (550) | 8 | 1 |  |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded tube |
| SA-249 | TP304LN | S30453 | 75 (515) | 8 | 1 | . . |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded tube |
| SA-249 | S30815 | S30815 | 87 (600) | 8 | 2 |  |  | 102 |  | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Welded tube |
| SA-249 | TP309S | S30908 | 75 (515) | 8 | 2 | . . |  | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP309H | S30909 | 75 (515) | 8 | 2 | . . . | . . . | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP309Cb | S30940 | 75 (515) | 8 | 2 | . . . | . . | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Welded tube |
| SA-249 | TP309HCb | S30941 | 75 (515) | 8 | 2 |  |  | 102 |  | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Welded tube |
| SA-249 | TP310S | S31008 | 75 (515) | 8 | 2 | . . | $\ldots$ | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP310H | S31009 | 75 (515) | 8 | 2 | . . . |  | 102 | $\cdots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Welded tube |
| SA-249 | TP310Cb | S31040 | 75 (515) | 8 | 2 | . . |  | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Welded tube |
| SA-249 | TP310HCb | S31041 | 75 (515) | 8 | 2 | . . | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Welded tube |
| SA-249 | TP310MoLN | S31050 | 78 (540) | 8 | 2 | . . . |  | 102 | . . . | $25 \mathrm{Cr}-22 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded tube, $t>1 / 4 \mathrm{in}$. $(6 \mathrm{~mm}$ ) |
| SA-249 | TP310MoLN | S31050 | 84 (580) | 8 | 2 | . . |  | 102 | . . | $25 \mathrm{Cr}-22 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded tube, $t \leq 1 / 4 \mathrm{in}$. $(6 \mathrm{~mm}$ ) |
| SA-249 | S31254 | S31254 | 94 (650) | 8 | 4 | . . |  | 102 | . . | 20Cr-18Ni-6Mo | Welded tube |
| SA-249 | TP316 | S31600 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded tube |
| SA-249 | TP316L | S31603 | 70 (485) | 8 | 1 | . . . | $\cdots$ | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded tube |
| SA-249 | TP316H | S31609 | 75 (515) | 8 | 1 | $\cdots$ |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded tube |
| SA-249 | TP316N | S31651 | 80 (550) | 8 | 1 | . . . |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded tube |
| SA-249 | TP316LN | S31653 | 75 (515) | 8 | 1 |  |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded tube |
| SA-249 | TP317 | S31700 | 75 (515) | 8 | 1 | . . . |  | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Welded tube |
| SA-249 | TP317L | S31703 | 75 (515) | 8 | 1 | . . . | . . | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Welded tube |
| SA-249 | S31725 | S31725 | 75 (515) | 8 | 4 | $\cdots$ |  | 102 | . . | $19 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Mo}$ | Welded tube |
| SA-249 | S31726 | S31726 | 80 (550) | 8 | 4 | $\ldots$ | . . | 102 | . . | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Welded tube |

 Grouping of Base Metals for Qualification

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | $\begin{aligned} & \text { UNS } \\ & \text { No. } \end{aligned}$ | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | S- <br> No. | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-268 | S44735 | S44735 | 75 (515) | 10J | 1 | ... | ... | 102 | ... | $29 \mathrm{Cr}-4 \mathrm{Mo}-\mathrm{Ti}$ | Smls. \& welded tube |
| SA-268 | 29-4-2 | S44800 | 80 (550) | 10K | 1 | $\ldots$ |  | 102 |  | $29 \mathrm{Cr}-4 \mathrm{Mo}-2 \mathrm{Ni}$ | Smls. \& welded tube |
| A 269 | TP316 | S31600 | 75 (515) | ... | ... | 8 | 1 | $\ldots$ | 102 | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. \& welded tube |
| A 269 | TP316L | S31603 | 70 (485) | . . | . . | 8 | 1 | $\ldots$ | 102 | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. \& welded tube |
| A 269 | TP304 | S30400 | 75 (515) | ... | . . | 8 | 1 | $\ldots$ | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. \& welded tube |
| A 269 | TP304L | S30403 | 70 (485) | ... | . . . | 8 | 1 | . . . | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. \& welded tube |
| A 271 | TP304 | S30400 | 75 (515) |  |  | 8 | 1 | ... | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. tube |
| A 271 | TP304L | S30403 | 70 (485) | $\ldots$ | $\ldots$ | 8 | 1 | $\ldots$ | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. tube |
| A 276 | TP304 | S30400 | 75 (515) | ... | ... | 8 | 1 | ... | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bar |
| A 276 | TP304L | S30403 | 70 (485) | ... | . . . | 8 | 1 | $\ldots$ | 102 | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bar |
| A 276 | TP316 | S31600 | 75 (515) | ... | . . . | 8 | 1 | ... | 102 | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Bar |
| A 276 | TP316L | S31603 | 70 (485) | $\ldots$ | $\ldots$ | 8 | 1 | $\ldots$ | 102 | 16Cr-12Ni-2Mo | Bar |
| A 276 | S32205 | S32205 | 95 (655) | ... | . . . | 10 H | 1 | $\ldots$ | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Bar |
| A 276 | TP410 | S41000 | 65 (450) | $\ldots$ | $\ldots$ | 6 | 1 |  | 102 | 13 Cr | Bar |
| SA-283 | A | K01400 | 45 (310) | 1 | 1 | ... | ... | 101 | . . . | C | Plate |
| SA-283 | B | K01702 | 50 (345) | 1 | 1 | ... | $\ldots$ | 101 | . . | C | Plate |
| SA-283 | C | K02401 | 55 (380) | 1 | 1 | . . . | . . | 101 | . . . | C | Plate |
| SA-283 | D | K02702 | 60 (415) | 1 | 1 | ... | . . . | 101 | ... | C | Plate |
| SA-285 | A | K01700 | 45 (310) | 1 | 1 | ... | ... | 101 | ... | C | Plate |
| SA-285 | B | K02200 | 50 (345) | 1 | 1 | $\ldots$ | . . | 101 | ... | C | Plate |
| SA-285 | C | K02801 | 55 (380) | 1 | 1 | ... |  | 101 | . . . | C | Plate |
| SA-299 | $\ldots$ | K02803 | 75 (515) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-302 | A | K12021 | 75 (515) | 3 | 2 | ... | $\ldots$ | 101 | . | $\mathrm{Mn}-0.5 \mathrm{Mo}$ | Plate |
| SA-302 | B | K12022 | 80 (550) | 3 | 3 | ... | . . . | 101 | ... | $\mathrm{Mn}-0.5 \mathrm{Mo}$ | Plate |
| SA-302 | C | K12039 | 80 (550) | 3 | 3 | ... | . . . | 101 | . . . | $\mathrm{Mn}-0.5 \mathrm{Mo}-0.5 \mathrm{Ni}$ | Plate |
| SA-302 | D | K12054 | 80 (550) | 3 | 3 | . . |  | 101 | . . | $\mathrm{Mn}-0.5 \mathrm{Mo}-0.75 \mathrm{Ni}$ | Plate |
| SA-312 | TPXM-19 | S20910 | 100 (690) | 8 | 3 | $\ldots$ | ... | 102 | ... | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Smls. \& welded pipe |
| SA-312 | TPXM-11 | S21904 | 90 (620) | 8 | 3 | . . . | . . . | 102 | . . . | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Smls. \& welded pipe |
| SA-312 | TPXM-29 | S24000 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | . . . | $18 \mathrm{Cr}-3 \mathrm{Ni}-12 \mathrm{Mn}$ | Smls. \& welded pipe |
| SA-312 | TP304 | S30400 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP304L | S30403 | 70 (485) | 8 | 1 | . . . | . . . | 102 | . . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP304H | S30409 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP304N | S30451 | 80 (550) | 8 | 1 | . . | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-312 | TP304LN | S30453 | 75 (515) | 8 | 1 | . . . | . . | 102 | . . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-312 | S30600 | S30600 | 78 (540) | 8 | 1 | . . | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Si}$ | Smls. \& welded pipe |
| SA-312 | S30815 | S30815 | 87 (600) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Smls. \& welded pipe |



| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P- <br> No. | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | P- <br> No. | S- <br> No. |  |  |
| SA-312 | TP309S | S30908 | 75 (515) | 8 | 2 | . . | . . | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP309H | S30909 | 75 (515) | 8 | 2 |  |  | 102 |  | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP309Cb | S30940 | 75 (515) | 8 | 2 | $\ldots$ |  | 102 |  | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP309HCb | S30941 | 75 (515) | 8 | 2 | . . | . . | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP310S | S31008 | 75 (515) | 8 | 2 | . . |  | 102 | $\ldots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP310H | S31009 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-312 | TP310Cb | S31040 | 75 (515) | 8 | 2 | $\ldots$ | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP310HCb | S31041 | 75 (515) | 8 | 2 | $\ldots$ |  | 102 |  | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP310MoLN | S31050 | 78 (540) | 8 | 2 |  |  | 102 |  | $25 \mathrm{Cr}-22 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded pipe, $t>1 / 4 \mathrm{in}$. $(6 \mathrm{~mm}$ ) |
| SA-312 | TP310MoLN | S31050 | 84 (580) | 8 | 2 | . . |  | 102 | . . | $25 \mathrm{Cr}-22 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Welded pipe, $t \leq \frac{1}{4} \mathrm{in}$. $(6 \mathrm{~mm}$ ) |
| SA-312 | S31254 | S31254 | 94 (650) | 8 | 4 | . . | $\ldots$ | 102 | $\ldots$ | $20 \mathrm{Cr}-18 \mathrm{Ni}-6 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | TP316 | S31600 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | TP316L | S31603 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | TP316H | S31609 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | TP316N | S31651 | 80 (550) | 8 | 1 | . . |  | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-312 | TP316LN | S31653 | 75 (515) | 8 | 1 | . . |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-312 | TP317 | S31700 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | TP317L | S31703 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | S31725 | S31725 | 75 (515) | 8 | 4 |  |  | 102 |  | $19 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-312 | S31726 | S31726 | 80 (550) | 8 | 4 | . . | $\ldots$ | 102 | . . | 19Cr-15.5Ni-4Mo | Smls. \& welded pipe |
| SA-312 | TP321 | S32100 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $>3 / 8 \mathrm{in}$. (10 mm) |
| SA-312 | TP321 | S32100 | 75 (515) | 8 | 1 | . . | $\ldots$ | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $\leq 3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-312 | TP321 | S32100 | 75 (515) | 8 | 1 | . . | . . . | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Welded pipe |
| SA-312 | TP321H | S32109 | 70 (485) | 8 | 1 | . . . | . . . | 102 | . $\cdot$. | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $>3 / 8 \mathrm{in}$. (10 mm) |
| SA-312 | TP321H | S32109 | 75 (515) | 8 | 1 | . . . | . . . | 102 | . . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $\leq 3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-312 | TP321H | S32109 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Welded pipe |
| SA-312 | TP347 | S34700 | 75 (515) | 8 | 1 | . . | ... | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP347 H | S34709 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP348 | S34800 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TP348H | S34809 | 75 (515) | 8 | 1 | . . |  | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. \& welded pipe |
| SA-312 | TPXM-15 | S38100 | 75 (515) | 8 | 1 | . . | $\cdots$ | 102 | - . | $18 \mathrm{Cr}-18 \mathrm{Ni}-2 \mathrm{Si}$ | Smls. \& welded pipe |
| A 312 | S34565 | S34565 | 115 (795) | . . | . . | 8 | 4 | $\cdots$ | . $\cdot$ | $24 \mathrm{Cr}-17 \mathrm{Ni}-6 \mathrm{Mn}-4.5 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| A 331 | 8620 CW | G86200 | 90 (620) | $\cdots$ | $\cdots$ | 3 | 3 | $\cdots$ | 102 | $0.5 \mathrm{Ni}-0.5 \mathrm{Cr}-\mathrm{Mo}$ | Bar |
| SA-333 | 6 | K03006 | 60 (415) | 1 | 1 | . . | . . | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Smls. \& welded pipe |
| SA-333 | 1 | K03008 | 55 (380) | 1 | 1 | . . | . . | 101 | . $\cdot$ | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe |
| SA-333 | 10 | . . . | 80 (550) | 1 | 3 | . . | . . | 101 | . . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Smls. \& welded pipe |
| SA-333 | 4 | K11267 | 60 (415) | 4 | 2 | $\cdot$ | $\ldots$ | 102 | . . | $0.75 \mathrm{Cr}-0.75 \mathrm{Ni}-\mathrm{Cu}-\mathrm{Al}$ | Smls. \& welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS No. | Tensile, ksi (MPa) | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-336 | F91 | K90901 | 85 (585) | 5B | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $9 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-336 | F46 | S30600 | 78 (540) | 8 | 1 | ... | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Si}$ | Forgings |
| SA-336 | FXM-19 | S20910 | 100 (690) | 8 | 3 |  |  | 102 |  | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Forgings |
| SA-336 | FXM-11 | S21904 | 90 (620) | 8 | 3 |  |  | 102 |  | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Forgings |
| SA-336 | F304 | S30400 | 70 (485) | 8 | 1 | ... |  | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-336 | F304L | S30403 | 65 (450) | 8 | 1 |  | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-336 | F304H | S30409 | 70 (485) | 8 | 1 |  | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forgings |
| SA-336 | F304N | S30451 | 80 (550) | 8 | 1 |  | ... | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forgings |
| SA-336 | F304LN | S30453 | 70 (485) | 8 | 1 | ... | . . | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forgings |
| SA-336 | F310 | S31000 | 75 (515) | 8 | 2 | . . | $\ldots$ | 102 | ... | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Forgings |
| SA-336 | F316 | S31600 | 70 (485) | 8 | 1 |  | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings |
| SA-336 | F316L | S31603 | 65 (450) | 8 | 1 |  |  | 102 |  | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forgings |
| SA-336 | F316H | S31609 | 70 (485) | 8 | 1 | ... | ... | 102 | ... | 16Cr-12Ni-2Mo | Forgings |
| SA-336 | F316N | S31651 | 80 (550) | 8 | 1 |  | $\cdots$ | 102 | . $\cdot$ | 16Cr-12Ni-2Mo-N | Forgings |
| SA-336 | F316LN | S31653 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | 16Cr-12Ni-2Mo-N | Forgings |
| SA-336 | F321 | S32100 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forgings |
| SA-336 | F321H | S32109 | 70 (485) | 8 | 1 |  |  | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forgings |
| SA-336 | F347 | S34700 | 70 (485) | 8 | 1 |  | $\ldots$ | 102 | $\ldots$ | 18Cr-10Ni-Cb | Forgings |
| SA-336 | F347 H | S34709 | 70 (485) | 8 | 1 | $\ldots$ | . . | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-336 | F348 | S34800 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forgings |
| SA-336 | F348H | S34809 | 65 (450) | 8 | 1 |  | $\ldots$ | 102 | . . | 18Cr-10Ni-Cb | Forgings |
| SA-350 | LFI | K03009 | 60 (415) | 1 | 1 | $\ldots$ | ... | 101 | $\ldots$ | C-Mn-Si | Forgings |
| SA-350 | LF2 | K03011 | 70 (485) | 1 | 2 |  | $\ldots$ | 101 | ... | C-Mn-Si | Forgings |
| SA-350 | LF5, Cl. 1 | K13050 | 60 (415) | 9A | 1 | $\ldots$ | $\ldots$ | 101 | ... | 1.5 Ni | Forgings |
| SA-350 | LF5, Cl. 2 | K13050 | 70 (485) | 9A | 1 | . . | . . | 101 | ... | 1.5 Ni | Forgings |
| SA-350 | LF9 | K22036 | 63 (435) | 9A | 1 |  | . . | 101 | . . | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Forgings |
| SA-350 | LF3 | K32025 | 70 (485) | 9 B | 1 |  |  | 101 |  | 3.5 Ni | Forgings |
| SA-351 | CF3 | J92500 | 70 (485) | 8 | 1 | ... | ... | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Castings |
| SA-351 | CF3A | J92500 | 77 (530) | 8 | 1 | $\ldots$ | . . | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Castings |
| SA-351 | CF8 | J92600 | 70 (485) | 8 | 1 |  | ... | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Castings |
| SA-351 | CF8A | J92600 | 77 (530) | 8 | 1 | . . . | . . | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Castings |
| SA-351 | CF8C | J92710 | 70 (485) | 8 | 1 | ... | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Castings |
| SA-351 | CF3M | J92800 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-12Ni-2Mo | Castings |
| SA-351 | CF8M | J92900 | 70 (485) | 8 | 1 | $\ldots$ | ... | 102 | ... | 18Cr-12Ni-2Mo | Castings |
| SA-351 | CFio | J92590 | 70 (485) | 8 | 1 | . $\cdot$ | $\ldots$ | 102 | . . | $19 \mathrm{Cr}-9 \mathrm{Ni}-0.5 \mathrm{Mo}$ | Castings |
| SA-351 | CFIOM | J92901 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $19 \mathrm{Cr}-9 \mathrm{Ni}-2 \mathrm{Mo}$ | Castings |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS No. | Tensile, ksi (MPa) | PNo. | Group No. | SNo. | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-351 | CG8M | J93000 | 75 (515) | 8 | 1 | ... | ... | 102 | . . | 19Cr-10Ni-3Mo | Castings |
| SA-351 | CK3MCuN | J93254 | 80 (550) | 8 | 4 |  |  | 102 | ... | $20 \mathrm{Cr}-18 \mathrm{Ni}-6 \mathrm{Mo}$ | Castings |
| SA-351 | CD3MWCuN | J93380 | 100 (690) | ... | $\ldots$ | 10 H | 1 | . . | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Castings |
| SA-351 | CH8 | J93400 | 65 (450) | 8 | 2 | ... | . . . | 102 | . . . | $25 \mathrm{Cr}-12 \mathrm{Ni}$ | Castings |
| SA-351 | CH2O | J93402 | 70 (485) | 8 | 2 |  | . . | 102 | . . | $25 \mathrm{Cr}-12 \mathrm{Ni}$ | Castings |
| SA-351 | CG6MMN | J93790 | 85 (585) | 8 | 3 | ... | . . | 102 | . . | 22Cr-12Ni-5Mn | Castings |
| SA-351 | CK20 | J94202 | 65 (450) | 8 | 2 | ... | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Castings |
| SA-351 | CN7M | N08007 | 62 (425) | 45 | . . | . . . | ... | 111 | . . | $28 \mathrm{Ni}-19 \mathrm{Cr}-\mathrm{Cu}-\mathrm{Mo}$ | Castings |
| SA-351 | CT15C | N08151 | 63 (435) | 45 | . . . | . . . | . . | 111 | . . . | $32 \mathrm{Ni}-45 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Castings |
| SA-351 | CN3MN | J94651 | 80 (550) | 45 | $\ldots$ | $\ldots$ | $\ldots$ | 111 | $\ldots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Castings |
| A 351 | CA15 | . . . | 90 (620) | ... | . | 6 | 3 | ... | 102 | 13 Cr | Castings |
| A 351 | CE20N | . $\cdot$ | 80 (550) | $\ldots$ | . . | 8 | 2 | $\ldots$ | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Castings |
| A 351 | CFIOMC | J92971 | 70 (485) | ... | . . | 8 | 1 | . . . | 102 | $16 \mathrm{Cr}-14 \mathrm{Ni}-2 \mathrm{Mo}$ | Castings |
| A 351 | CH10 | J93401 | 70 (485) | $\ldots$ | . . . | 8 | 2 | . . | 102 | $25 \mathrm{Cr}-12 \mathrm{Ni}$ | Castings |
| A 351 | HK30 | J94203 | 65 (450) | $\ldots$ | $\ldots$ | 8 | 2 | . . | 102 | $25 \mathrm{Cr}-20 \mathrm{Ni}-0.5 \mathrm{Mo}$ | Castings |
| A 351 | HK40 | J94204 | 62 (425) | ... | . . | 8 | 2 | . . . | 102 | $25 \mathrm{Cr}-20 \mathrm{Ni}-0.5 \mathrm{Mo}$ | Castings |
| A 351 | HT30 | N08603 | 65 (450) | . . | . . | 45 | ... |  | 111 | $35 \mathrm{Ni}-15 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-352 | LCA | J02504 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Si | Castings |
| SA-352 | LCC | J02505 | 70 (485) | 1 | 2 | ... | . . | 101 | ... | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Castings |
| SA-352 | LCB | J03003 | 65 (450) | 1 | 1 | $\ldots$ | . . | 101 | . . . | C-Si | Castings |
| SA-352 | LCI | J12522 | 65 (450) | 3 | 1 | ... | ... | 101 | . . | C-0.5Mo | Castings |
| SA-352 | LC2 | J22500 | 70 (485) | 9 A | 1 | . . | . . | 101 | . . | 2.5 Ni | Castings |
| SA-352 | LC3 | J31550 | 70 (485) | 9 B | 1 | $\ldots$ | ... | 101 | $\ldots$ | 3.5 Ni | Castings |
| SA-352 | LC4 | J41500 | 70 (485) | 9 C | 1 | . . . | . . | 101 | ... | 4.5 Ni | Castings |
| SA-352 | LC2-1 | J42215 | 105 (725) | 11 A | 5 | . . . | $\ldots$ | 102 | . . . | $3 \mathrm{Ni}-1.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-352 | CA6NM | J91540 | 110 (760) | 6 | 4 | $\ldots$ |  | 102 | $\ldots$ | $13 \mathrm{Cr}-4 \mathrm{Ni}$ | Castings |
| SA-353 | ... | K81340 | 100 (690) | 11 A | 1 | ... | ... | 101 | ... | 9 Ni | Plate |
| A 356 | 1 | J03502 | 70 (485) | $\ldots$ | $\ldots$ | 1 | 2 | . | 101 | C-Si | Castings |
| A 356 | 2 | J12523 | 65 (450) | . . . | . . . | 3 | 1 | ... | 101 | C-0.5Mo | Castings |
| A 356 | 6 | J12073 | 70 (485) | $\ldots$ | $\ldots$ | 4 | 1 | ... | 102 | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| A 356 | 8 | J11697 | 80 (550) | $\ldots$ | . . | 4 | 1 | ... | 102 | 1Cr-1Mo-V | Castings |
| A 356 | 9 | J21610 | 85 (585) | $\ldots$ | . . . | 4 | 1 | . . . | 102 | $1 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Castings |
| A 356 | 10 | J22090 | 85 (585) | ... | ... | 5 A | 1 | . . . | 102 | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Castings |
| A 356 | 12 | J80490 | 85 (585) | ... | ... | 5B | 2 | ... | 102 | $9 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Castings |
| SA-358 | XM-19 | S20910 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Fusion welded pipe |
| SA-358 | XM-29 | S24000 | 100 (690) | 8 | 3 | . . | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-3 \mathrm{Ni}-12 \mathrm{Mn}$ | Fusion welded pipe |
| SA-358 | 304 | S30400 | 75 (515) | 8 | 1 | . . | . . | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Fusion welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-358 | 304L | S30403 | 70 (485) | 8 | 1 | . . | ... | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Fusion welded pipe |
| SA-358 | 304 H | S30409 | 75 (515) | 8 | 1 |  | . . | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Fusion welded pipe |
| SA-358 | 304 N | S30451 | 80 (550) | 8 | 1 | ... | ... | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Fusion welded pipe |
| SA-358 | 304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Fusion welded pipe |
| SA-358 | S30815 | S30815 | 87 (600) | 8 | 2 |  |  | 102 | $\ldots$ | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Fusion welded pipe |
| SA-358 | 3095 | S30908 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Fusion welded pipe |
| SA-358 | 309 Cb | S30940 | 75 (515) | 8 | 2 |  |  | 102 | $\ldots$ | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Fusion welded pipe |
| SA-358 | 310 S | S31008 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | . . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Fusion welded pipe |
| SA-358 | 310 Cb | S31040 | 75 (515) | 8 | 2 | . . . | ... | 102 | $\ldots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Fusion welded pipe |
| SA-358 | S31254 | S31254 | 94 (650) | 8 | 4 |  | . . | 102 | . . | $20 \mathrm{Cr}-18 \mathrm{Ni}-6 \mathrm{Mo}$ | Fusion welded pipe |
| SA-358 | 316 | S31600 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | ... | 16Cr-12Ni-2Mo | Fusion welded pipe |
| SA-358 | 316 L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | 16Cr-12Ni-2Mo | Fusion welded pipe |
| SA-358 | 316 H | S31609 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo | Fusion welded pipe |
| SA-358 | 316 N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | $\cdots$ | 102 | ... | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Fusion welded pipe |
| SA-358 | 316 LN | S31653 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Fusion welded pipe |
| SA-358 | S31725 | S31725 | 75 (515) | 8 | 4 | ... | $\ldots$ | 102 | ... | 19Cr-15Ni-4Mo | Fusion welded pipe |
| SA-358 | S31726 | S31726 | 80 (550) | 8 | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Fusion welded pipe |
| SA-358 | 321 | S32100 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Fusion welded pipe |
| SA-358 | 347 | S34700 | 75 (515) | 8 | 1 | . . . | $\ldots$ | 102 | . . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Fusion welded pipe |
| SA-358 | 348 | S34800 | 75 (515) | 8 | 1 |  | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Fusion welded pipe |
| SA-369 | FPA | K02501 | 48 (330) | 1 | 1 | $\ldots$ | ... | 101 | ... | C-Si | Forged pipe |
| SA-369 | FPB | K03006 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | ... | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Forged pipe |
| SA-369 | FPI | K11522 | 55 (380) | 3 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-0.5Mo | Forged pipe |
| SA-369 | FP2 | K11547 | 55 (380) | 3 | 1 | . . . | . . . | 101 | . . | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP12 | K11562 | 60 (415) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP11 | K11597 | 60 (415) | 4 | 1 | $\ldots$ | ... | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Forged pipe |
| SA-369 | FP22 | K21590 | 60 (415) | 5 A | 1 | . . . | $\ldots$ | 102 | . . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP21 | K31545 | 60 (415) | 5 A | 1 | ... | . . | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP5 | K41545 | 60 (415) | 5B | 1 | $\ldots$ | $\ldots$ | 102 | ... | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP9 | K90941 | 60 (415) | 5B | 1 | . . . | $\ldots$ | 102 | . . . | $9 \mathrm{Cr}-1 \mathrm{Mo}$ | Forged pipe |
| SA-369 | FP91 | K90901 | 85 (585) | 5B | 2 | . . | $\ldots$ | 102 | . . | $9 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Forged pipe |
| SA-372 | A | K03002 | 60 (415) | 1 | 1 | . . | ... | 101 | ... | C-Si | Forgings |
| SA-372 | B | K04001 | 75 (515) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Forgings |
| SA-376 | 16-8-2 H | S16800 | 75 (515) | 8 | 1 | . . . | $\ldots$ | 102 | . . . | $16 \mathrm{Cr}-8 \mathrm{Ni}-2 \mathrm{Mo}$ | Smls. pipe |
| SA-376 | TP304 | S30400 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. pipe $\geq 0.812$ in. (21 mm) |
| SA-376 | TP304 | S30400 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. pipe < 0.812 in . (21 mm) |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ | Group No. | $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-376 | TP304H | S30409 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Smls. pipe |
| SA-376 | TP304N | S30451 | 80 (550) | 8 | 1 | $\ldots$ | $\ldots$ | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Smls. pipe |
| SA-376 | TP304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Smls. pipe |
| SA-376 | TP316 | S31600 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 |  | 16Cr-12Ni-2Mo | Smls. pipe |
| SA-376 | TP316H | S31609 | 75 (515) | 8 | 1 | . | $\ldots$ | 102 | . . | 16Cr-12Ni-2Mo | Smls. pipe |
| SA-376 | TP316N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | . . | 102 | ... | 16Cr-12Ni-2Mo-N | Smls. pipe |
| SA-376 | TP316LN | S31653 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Smls. pipe |
| SA-376 | S31725 | S31725 | 75 (515) | 8 | 4 | . . . | $\ldots$ | 102 | $\ldots$ | 19Cr-15Ni-4Mo | Smls. pipe |
| SA-376 | S31726 | S31726 | 80 (550) | 8 | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Smls. pipe |
| SA-376 | TP321 | S32100 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $>3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-376 | TP321 | S32100 | 75 (515) | 8 | 1 | . . . | . . . | 102 | . . . | 18Cr-10Ni-Ti | Smls. pipe $\leq 3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-376 | TP321H | S32109 | 70 (485) | 8 | 1 | $\ldots$ | . . | 102 | . . | 18Cr-10Ni-Ti | Smls. pipe $>3 / 8$ in. $(10 \mathrm{~mm}$ ) |
| SA-376 | TP321H | S32109 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Smls. pipe $\leq 3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-376 | TP347 | S34700 | 75 (515) | 8 | 1 | ... | . . | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. pipe |
| SA-376 | TP347 H | S34709 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Smls. pipe |
| SA-376 | TP348 | S34800 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 |  | 18Cr-10Ni-Cb | Smls. pipe |
| A 381 | Y 35 | K03013 | 60 (415) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Welded pipe |
| A 381 | Y42 | ... | 60 (415) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Welded pipe |
| A 381 | Y48 | $\ldots$ | 62 (425) | ... | $\ldots$ | 1 | 1 | ... | 101 | C | Welded pipe $>3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| A 381 | Y46 |  | 63 (435) |  |  | 1 | 1 |  | 101 | C | Welded pipe |
| A 381 | Y50 | $\ldots$ | 64 (440) | $\ldots$ | $\ldots$ | 1 | 1 |  | 101 | C | Welded pipe $>3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| A 381 | Y52 | ... | 66 (455) | ... | . . | 1 | 2 | ... | 101 | C | Welded pipe $>3 / 8 \mathrm{in}$. ( 10 mm ) |
| A 381 | Y56 |  | 71 (490) | $\ldots$ | . . | 1 | 2 | $\ldots$ | 101 | C | Welded pipe $>3 / 8 \mathrm{in}$. (10 mm) |
| A 381 | Y52 | ... | 72 (495) | . . . | $\ldots$ | 1 | 2 | ... | 101 | C | Welded pipe, to $3 / 8 \mathrm{in}$. ( 10 mm ) |
| A 381 | Y56 | $\ldots$ | 75 (515) | $\ldots$ | $\ldots$ | 1 | 2 | . . | 101 | C | Welded pipe, to $3 / 8 \mathrm{in}$. ( 10 mm ) |
| A 381 | Y60 |  | 75 (515) | $\ldots$ |  | 1 | 2 |  | 101 | C | Welded pipe $>3 / 8 \mathrm{in}$. (10 mm) |
| A 381 | Y60 |  | 78 (540) | $\ldots$ | $\ldots$ | 1 | 2 |  | 101 | C | Welded pipe $\leq 3 / 8 \mathrm{in}$. $(10 \mathrm{~mm}$ ) |
| SA-387 | 12, CI. 1 | K11757 | 55 (380) | 4 | 1 | . . | ... | 102 | ... | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | 12, C. 2 | K11757 | 65 (450) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | 11, CI. 1 | K11789 | 60 (415) | 4 | 1 | $\ldots$ |  | 102 | ... | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Plate |
| SA-387 | 11, CI. 2 | K11789 | 75 (515) | 4 | 1 | $\ldots$ | ... | 102 | . . | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Plate |
| SA-387 | Gr. 2, CI. 1 | K12143 | 55 (380) | 3 | 1 | . . | . . | 101 | ... | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | Gr. 2, Cl. 2 | K12143 | 70 (485) | 3 | 2 | $\ldots$ |  | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | 22, CI. 1 | K21590 | 60 (415) | 5A | 1 | ... | ... | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-387 | 22, CI. 2 | K21590 | 75 (515) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-387 | 21, CI. 1 | K31545 | 60 (415) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | . . | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-387 | 21, CI. 2 | K31545 | 75 (515) | 5A | 1 | . . | $\ldots$ | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |

 Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum <br> Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-387 | 5, Cl. 1 | K41545 | 60 (415) | 5B | 1 | $\ldots$ | $\ldots$ | 102 | ... | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | 5, Cl. 2 | K41545 | 75 (515) | 5B | 1 | . . | . | 102 | $\ldots$ | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-387 | Gr. 91, Cl. 2 | K90901 | 85 (585) | 5B | 2 | $\ldots$ | $\ldots$ | 102 | ... | $9 \mathrm{Cr}-1 \mathrm{Mo}$-V | Plate |
| SA-403 | WPXM-19 | S20910 | 100 (690) | 8 | 3 | $\ldots$ | ... | 102 | ... | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Wrought piping fittings |
| SA-403 | WP304 | S30400 | 75 (515) | 8 | 1 |  |  | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Wrought piping fittings |
| SA-403 | WP304L | S30403 | 70 (485) | 8 | 1 | ... | $\ldots$ | 102 |  | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Wrought piping fittings |
| SA-403 | WP304H | S30409 | 75 (515) | 8 | 1 | ... | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Wrought piping fittings |
| SA-403 | WP304N | S30451 | 80 (550) | 8 | 1 | $\ldots$ |  | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Wrought piping fittings |
| SA-403 | WP304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Wrought piping fittings |
| SA-403 | WP309 | S30900 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Wrought piping fittings |
| SA-403 | WP310 | S31000 | 75 (515) | 8 | 2 | . . | . | 102 |  | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Wrought piping fittings |
| SA-403 | WP316 | S31600 | 75 (515) | 8 | 1 | $\ldots$ | ... | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Wrought piping fittings |
| SA-403 | WP316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | 16Cr-12Ni-2Mo | Wrought piping fittings |
| SA-403 |  | S31254 | 94 (650) | 8 | 4 | $\ldots$ |  | 102 |  | 20Cr-18Ni-6Mo | Wrought piping fittings |
| SA-403 | WP316H | S31609 | 75 (515) | 8 | 1 | ... | ... | 102 | ... | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Wrought piping fittings |
| SA-403 | WP316N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | - | 102 | ... | 16Cr-12Ni-2Mo-N | Wrought piping fittings |
| SA-403 | WP316LN | S31653 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Wrought piping fittings |
| SA-403 | WP317 | S31700 | 75 (515) | 8 | 1 | ... | ... | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Wrought piping fittings |
| SA-403 | WP317L | S31703 | 75 (515) | 8 | 1 |  | . . | 102 | . . | 18Cr-13Ni-3Mo | Wrought piping fittings |
| SA-403 | WP321 | S32100 | 75 (515) | 8 | 1 | ... | ... | 102 | ... | 18Cr-10Ni-Ti | Wrought piping fittings |
| SA-403 | WP321H | S32109 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | 18Cr-10Ni-Ti | Wrought piping fittings |
| SA-403 | WP347 | S34700 | 75 (515) | 8 | 1 | .. | ... | 102 | . . | 18Cr-10Ni-Cb | Wrought piping fittings |
| SA-403 | WP347H | S34709 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | . . | 18Cr-10Ni-Cb | Wrought piping fittings |
| SA-403 | WP348 | S34800 | 75 (515) | 8 | 1 | $\ldots$ |  | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Wrought piping fittings |
| SA-403 | WP348H | S34809 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Wrought piping fittings |
| A 403 | S34565 | S34565 | 115 (795) | $\ldots$ | $\ldots$ | 8 | 4 |  | ... | 24Cr-17Ni-6Mn-4.5Mo-N | Wrought piping fittings |
| SA-409 | TP304 | S30400 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded pipe |
| SA-409 | TP304L | S30403 | 70 (485) | 8 | 1 | ... | ... | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded pipe |
| SA-409 | S30815 | S30815 | 87 (600) | 8 | 2 | ... | $\ldots$ | 102 | . . | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Welded pipe |
| SA-409 | TP309S | S30908 | 75 (515) | 8 | 2 | ... |  | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Welded pipe |
| SA-409 | TP309Cb | S30940 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | ... | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-409 | TP310S | S31008 | 75 (515) | 8 | 2 | ... | $\ldots$ | 102 | ... | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Welded pipe |
| SA-409 | TP310Cb | S31040 | 75 (515) | 8 | 2 | $\ldots$ |  | 102 | ... | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-409 | S31254 | S31254 | 94 (650) | 8 | 4 | . . | . . | 102 | . . | $20 \mathrm{Cr}-18 \mathrm{Ni}-6 \mathrm{Mo}$ | Welded pipe |
| SA-409 | TP316 | S31600 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded pipe |
| SA-409 | TP316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Type or Grade | UNS No. | Minimum <br> Specified <br> Tensile, <br> ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-409 | TP317 | S31700 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-13Ni-3Mo | Welded pipe |
| SA-409 | S31725 | S31725 | 75 (515) | 8 | 4 | $\ldots$ | ... | 102 | $\ldots$ | 19Cr-15Ni-4Mo | Welded pipe |
| SA-409 | S31726 | S31726 | 80 (550) | 8 | 4 | $\ldots$ | . . | 102 | . . | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Welded pipe |
| SA-409 | TP321 | S32100 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Welded pipe |
| SA-409 | TP347 | S34700 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-409 | TP348 | S34800 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-414 | A | K01501 | 45 (310) | 1 | 1 | $\ldots$ | ... | 101 | ... | C | Sheet |
| SA-414 | B | K02201 | 50 (345) | 1 | 1 | . . | ... | 101 | ... | C | Sheet |
| SA-414 | C | K02503 | 55 (380) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Sheet |
| SA-414 | D | K02505 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | ... | C-Mn | Sheet |
| SA-414 | E | K02704 | 65 (450) | 1 | 1 | . . | . . | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}$ | Sheet |
| SA-414 | F | K03102 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | ... | C-Mn | Sheet |
| SA-414 | G | K03103 | 75 (515) | 1 | 2 |  | $\ldots$ | 101 | . . | C-Mn | Sheet |
| SA-420 | WPL6 | K03006 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | ... | C-Mn-Si | Piping fitting |
| SA-420 | WPL9 | K22035 | 63 (435) | 9 A | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Piping fitting |
| SA-420 | WPL3 | K31918 | 65 (450) | 9 B | 1 | ... | ... | 101 | ... | 3.5 Ni | Piping fitting |
| SA-420 | WPL8 | K81340 | 100 (690) | 11 A | 1 | $\ldots$ | $\ldots$ | 101 | . . | 9 Ni | Piping fitting |
| SA-423 | 1 | K11535 | 60 (415) | 4 | 2 | $\ldots$ | ... | 102 | $\ldots$ | $0.75 \mathrm{Cr}-0.5 \mathrm{Ni}-\mathrm{Cu}$ | Smls. \& welded tube |
| SA-423 | 2 | K11540 | 60 (415) | 4 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Cu}-\mathrm{Mo}$ | Smls. \& welded tube |
| SA-426 | CP15 | J11522 | 60 (415) | 3 | 1 | $\ldots$ | . . | 101 | $\ldots$ | $\mathrm{C}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Centrifugal cast pipe |
| SA-426 | CP2 | J11547 | 60 (415) | 3 | 1 | $\ldots$ | ... | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP12 | J11562 | 60 (415) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP11 | J12072 | 70 (485) | 4 | 1 | $\ldots$ | . . | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP1 | J12521 | 65 (450) | 3 | 1 | $\ldots$ | $\ldots$ | 101 | ... | C-0.5Mo | Centrifugal cast pipe |
| SA-426 | CP22 | J21890 | 70 (485) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP21 | J31545 | 60 (415) | 5A | 1 | $\ldots$ | ... | 102 | . . | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP5 | J42045 | 90 (620) | 5B | 1 | $\ldots$ | ... | 102 | $\ldots$ | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP5b | J51545 | 60 (415) | 5B | 1 | $\ldots$ | $\ldots$ | 102 | . . | $5 \mathrm{Cr}-1.5 \mathrm{Si}-0.5 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CP9 | J82090 | 90 (620) | 5B | 1 | . | . . | 102 | ... | $9 \mathrm{Cr}-1 \mathrm{Mo}$ | Centrifugal cast pipe |
| SA-426 | CPCAl5 | J91150 | 90 (620) | 6 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 13 Cr | Centrifugal cast pipe |
| SA-430 | FP16-8-2H | S16800 | 70 (485) | 8 | 1 | $\ldots$ | ... | 102 | $\ldots$ | $16 \mathrm{Cr}-8 \mathrm{Ni}-2 \mathrm{Mo}$ | Forged pipe |
| SA-430 | FP304 | S30400 | 70 (485) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forged pipe |
| SA-430 | FP304H | S30409 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Forged pipe |
| SA-430 | FP304N | S30451 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Forged pipe |
| SA-430 | FP316 | S31600 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Forged pipe |



| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum <br> Specified <br> Tensile, <br> ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-430 | FP316H | S31609 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo | Forged pipe |
| SA-430 | FP316N | S31651 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Forged pipe |
| SA-430 | FP321 | S32100 | 70 (485) | 8 | 1 | . | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forged pipe |
| SA-430 | FP321H | S32109 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Forged pipe |
| SA-430 | FP347 | S34700 | 70 (485) | 8 | 1 | $\ldots$ |  | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forged pipe |
| SA-430 | FP347H | S34709 | 70 (485) | 8 | 1 | $\cdots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Forged pipe |
| A 441 | 1 | K12211 | 70 (485) | $\ldots$ |  | 1 | 2 | $\ldots$ | 101 | $\mathrm{Mn}-\mathrm{Cu}-\mathrm{V}$ | Shapes |
| A 441 | 2 | K12211 | 70 (485) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | $\mathrm{Mn}-\mathrm{Cu}-\mathrm{V}$ | Shapes |
| A 446 | A | $\ldots$ | 45 (310) | $\ldots$ |  | 1 | 1 |  | 101 | C | Sheet |
| SA-451 | CPF8 | J92600 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPF8A | J92600 | 77 (530) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPF8C | J92710 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Centrifugal cast pipe |
| SA-451 | CPF8M | J92900 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-12Ni-2Mo | Centrifugal cast pipe |
| SA-451 | CPF3 | J92500 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPF3M | J92800 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo | Centrifugal cast pipe |
| SA-451 | CPF3A | J92500 | 77 (530) | 8 | 1 | $\ldots$ | ... | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPH8 | J93400 | 65 (450) | 8 | 2 | $\ldots$ | . . | 102 | $\ldots$ | $25 \mathrm{Cr}-12 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPH20 | J93402 | 70 (485) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $25 \mathrm{Cr}-12 \mathrm{Ni}$ | Centrifugal cast pipe |
| SA-451 | CPK20 | J94202 | 65 (450) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Centrifugal cast pipe |
| A 451 | CPFIOMC | J92971 | 70 (485) | $\ldots$ | $\ldots$ | 8 | 1 | $\ldots$ | 102 | $16 \mathrm{Cr}-14 \mathrm{Ni}-2 \mathrm{Mo}$ | Centrifugal cast pipe |
| A 451 | CPE20N |  | 80 (550) |  |  | 8 | 2 |  | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Centrifugal cast pipe |
| SA-455 | $\ldots$ | K03300 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | $\begin{aligned} & \text { Plate }>0.580-0.750 \mathrm{in} \text {. } \\ & \quad(15-19 \mathrm{~mm}) \end{aligned}$ |
| SA-455 | $\ldots$ | K03300 | 73 (505) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | $\begin{aligned} & \text { Plate }>0.375-0.580 \mathrm{in} \text {. } \\ & \quad(10-15 \mathrm{~mm}) \end{aligned}$ |
| SA-455 |  | K03300 | 75 (515) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Plate, up to 0.375 in . (10 mm) |
| SA-479 | XM-19 | S20910 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Bars \& shapes |
| SA-479 | XM-17 | S21600 | 90 (620) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 19Cr-8Mn-6Ni-Mo-N | Bars \& shapes |
| SA-479 | XM-18 | S21603 | 90 (620) | 8 | 3 | . . | ... | 102 | ... | $19 \mathrm{Cr}-8 \mathrm{Mn}-6 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | S21800 | S21800 | 95 (655) | 8 | 3 | $\ldots$ | . . | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}-4 \mathrm{Si}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | XM-11 | S21904 | 90 (620) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Bars \& shapes |
| SA-479 | XM-29 | S24000 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-3Ni-12Mn | Bars \& shapes |
| SA-479 | 302 | S30200 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bars \& shapes |
| SA-479 | 304 | S30400 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bars \& shapes |
| SA-479 | 304L | S30403 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bars \& shapes |
| SA-479 | 304 H | S30409 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Bars \& shapes |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum <br> Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | PNo. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-479 | 304N | S30451 | 80 (550) | 8 | 1 | . | $\ldots$ | 102 | $\ldots$ | 18Cr-8Ni-N | Bars \& shapes |
| SA-479 | 304LN | S30453 | 75 (515) | 8 | 1 | ... | . . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | S30600 | S30600 | 78 (540) | 8 | 1 | $\ldots$ |  | 102 |  | $18 \mathrm{Cr}-15 \mathrm{Ni}-4 \mathrm{Si}$ | Bars \& shapes |
| SA-479 | S30815 | S30815 | 87 (600) | 8 | 2 | . . . | ... | 102 | $\ldots$ | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | 3095 | S30908 | 75 (515) | 8 | 2 | . . . | $\ldots$ | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Bars \& shapes |
| SA-479 | 309 Cb | S30940 | 75 (515) | 8 | 2 | $\ldots$ |  | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Bars \& shapes |
| SA-479 | 310 S | S31008 | 75 (515) | 8 | 2 | $\ldots$ | ... | 102 | ... | 25Cr-20Ni | Bars \& shapes |
| SA-479 | 310 Cb | S31040 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Bars \& shapes |
| SA-479 | S31254 | S31254 | 95 (655) | 8 | 4 | ... | $\ldots$ | 102 | . . . | 20Cr-18Ni-6Mo | Bars \& shapes |
| SA-479 | 316 | S31600 | 75 (515) | 8 | 1 | . . . | $\ldots$ | 102 | . . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | 316 L | S31603 | 70 (485) | 8 | 1 | . . | $\ldots$ | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | 316 H | S31609 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | 316 Ti | S31635 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-Ti | Bars \& shapes |
| SA-479 | 316 Cb | S31640 | 75 (515) | 8 | 1 | $\cdots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{Cb}$ | Bars \& shapes |
| SA-479 | 316 N | S31651 | 80 (550) | 8 | 1 | . . . | . . | 102 | ... | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | 316LN | S31653 | 75 (515) | 8 | 1 | $\cdots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | S31725 | S31725 | 75 (515) | 8 | 4 | . . | $\ldots$ | 102 | . . | 19Cr-15Ni-4Mo | Bars \& shapes |
| SA-479 | S31726 | S31726 | 80 (550) | 8 | 4 | . . . | $\ldots$ | 102 | . . . | $19 \mathrm{Cr}-15.5 \mathrm{Ni}-4 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | ... | S31803 | 90 (620) | 10 H | 1 | $\ldots$ | . . | 102 | . . | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Bars \& shapes |
| SA-479 | 321 | S32100 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | ... | 18Cr-10Ni-Ti | Bars \& shapes |
| SA-479 | 321 H | S32109 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | . . | 18Cr-10Ni-Ti | Bars \& shapes |
| SA-479 | S32550 | S32550 | 110 (760) | 10 H | 1 | . . . | $\ldots$ | 102 | . . | $25 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-2 \mathrm{Cu}$ | Bars \& shapes |
| SA-479 | 347 | S34700 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | . | 18Cr-10Ni-Cb | Bars \& shapes |
| SA-479 | 347 H | S34709 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Bars \& shapes |
| SA-479 | 348 | S34800 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | ... | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Bars \& shapes |
| SA-479 | 348 H | S34809 | 75 (515) | 8 | 1 | ... | $\ldots$ | 102 | . . | 18Cr-10Ni-Cb | Bars \& shapes |
| SA-479 | 403 | S40300 | 70 (485) | 6 | 1 | ... | $\cdots$ | 102 | . . | 12 Cr | Bars \& shapes |
| SA-479 | 405 | S40500 | 60 (415) | 7 | 1 | $\ldots$ | $\ldots$ | 102 | ... | $12 \mathrm{Cr}-1 \mathrm{Al}$ | Bars \& shapes |
| SA-479 | 410 | S41000 | 70 (485) | 6 | 1 | . . | $\ldots$ | 102 | . . | 13 Cr | Bars \& shapes |
| SA-479 | 414 | S41400 | 115 (795) | 6 | 4 | . . . | $\ldots$ | 102 | ... | $12.5 \mathrm{Cr}-2 \mathrm{Ni}-\mathrm{Si}$ | Bars \& shapes |
| SA-479 | S41500 | S41500 | 115 (795) | 6 | 4 | $\ldots$ | . . | 102 | ... | $13 \mathrm{Cr}-4.5 \mathrm{Ni}-\mathrm{Mo}$ | Bars \& shapes |
| SA-479 | 430 | S43000 | 70 (485) | 7 | 2 | . . | $\ldots$ | 102 | . . | 17 Cr | Bars \& shapes |
| SA-479 | 439 | S43035 | 70 (485) | 7 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-Ti | Bars \& shapes |
| SA-479 | S44400 | S44400 | 60 (415) | 7 | 2 | ... | $\ldots$ | 102 | $\cdots$ | 18Cr-2Mo | Bars \& shapes |
| SA-479 | XM-27 | S44627 | 65 (450) | 10 I | 1 | . . | ... | 102 | . . | $27 \mathrm{Cr}-1 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | S44700 | S44700 | 70 (485) | 10J | 1 | $\ldots$ | . . | 102 | $\cdots$ | $29 \mathrm{Cr}-4 \mathrm{Mo}$ | Bars \& shapes |
| SA-479 | S44800 | S44800 | 70 (485) | 10K | 1 | ... | ... | 102 | . . | $29 \mathrm{Cr}-4 \mathrm{Mo}-2 \mathrm{Ni}$ | Bars \& shapes |

 Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS <br> No. | Tensile, ksi (MPa) | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-487 | Gr. 16, CI. A | J31200 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | Low C-Mn-Ni | Castings |
| SA-487 | Gr. 1, Cl. A | J13002 | 85 (585) | 10A | 1 |  | $\ldots$ | 101 | $\ldots$ | $\mathrm{Mn}-\mathrm{V}$ | Castings |
| SA-487 | Gr. 1, Cl. B | J13002 | 90 (620) | 10A | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | Mn-V | Castings |
| SA-487 | Gr. 2, Cl. A | J13005 | 85 (585) | 3 | 3 | $\ldots$ | ... | 101 | $\ldots$ | Mn-0.25Mo-V | Castings |
| SA-487 | Gr. 2, Cl. B | J13005 | 90 (620) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{Mn}-0.25 \mathrm{Mo}-\mathrm{V}$ | Castings |
| SA-487 | Gr. 4, Cl. A | J13047 | 90 (620) | 3 | 3 | $\ldots$ | ... | 101 | ... | $0.5 \mathrm{Ni}-0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{V}$ | Castings |
| SA-487 | Gr. 4, Cl. B | J13047 | 105 (725) | 11 A | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Ni}-0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{V}$ | Castings |
| SA-487 | Gr. 4, CI. E | J13047 | 115 (795) | 11 A | 3 |  | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Ni}-0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{V}$ | Castings |
| SA-487 | Gr. 8, Cl. A | J22091 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Castings |
| SA-487 | Gr. 8, CI. C | J22091 | 100 (690) | 5 C | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Castings |
| SA-487 | Gr. 8, Cl. B | J22091 | 105 (725) | 5 C | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Castings |
| SA-487 | CA15M CI. A | J91151 | 90 (620) | 6 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 13 Cr -Mo | Castings |
| SA-487 | CAl5 CI. C | J91150 | 90 (620) | 6 | 3 |  | ... | 102 | ... | 13 Cr | Castings |
| SA-487 | CA15 Cl. B | J91171 | 90 (620) | 6 | 3 | $\ldots$ | $\ldots$ | 102 | . . | 13 Cr | Castings |
| SA-487 | CAl5 CI. D | J91171 | 100 (690) | 6 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 13 Cr | Castings |
| SA-487 | CA6NM CI. B | J91540 | 100 (690) | 6 | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $13 \mathrm{Cr}-4 \mathrm{Ni}$ | Castings |
| SA-487 | CA6NM CI. A | J91540 | 110 (760) | 6 | 4 | $\ldots$ | $\ldots$ | 102 | . . | $13 \mathrm{Cr}-4 \mathrm{Ni}$ | Castings |
| SA-494 | CX2MW | N26022 | 80 (550) | 44 | ... | $\ldots$ | $\ldots$ | 112 | $\ldots$ | $59 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{Mo}-4 \mathrm{Fe}-3 \mathrm{~W}$ | Castings |
| A 494 | CW-6M | N30107 | 72 (495) | . . | $\ldots$ | 44 | $\ldots$ | . . . | 112 | $56 \mathrm{Ni}-19 \mathrm{Mo}-18 \mathrm{Cr}-2 \mathrm{Fe}$ | Castings |
| A 500 | C | K02705 | 62 (425) | $\ldots$ | $\ldots$ | 1 | 1 | ... | 101 | C | Tube |
| A 500 | B | K03000 | 58 (400) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Tube |
| A 501 |  | K03000 | 58 (400) | $\ldots$ | $\ldots$ | 1 | 1 |  | 101 | C | Tube |
| SA-508 | 3, Cl. 1 | K12042 | 80 (550) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | . . | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-\mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-508 | 3, CI. 2 | K12042 | 90 (620) | 3 | 3 | $\ldots$ | ... | 102 | . . | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-\mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-508 | 2, CI. 1 | K12766 | 80 (550) | 3 | 3 |  | ... | 101 | ... | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-0.3 \mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-508 | 2, Cl. 2 | K12766 | 90 (620) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-0.3 \mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-508 | 1 | K13502 | 70 (485) | 1 | 2 |  |  | 101 | $\ldots$ | C-Si | Forgings |
| SA-508 | 1A | K13502 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | ... | C-Mn-Si | Forgings |
| SA-508 | 22, CI. 3 | K21590 | 85 (585) | 5 C | 1 |  | ... | . . . |  | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-508 | 4N, Cl. 3 | K22375 | 90 (620) | 3 | 3 | $\ldots$ | $\ldots$ | 102 | ... | $3.5 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-508 | $4 \mathrm{~N}, \mathrm{Cl} .1$ | K22375 | 105 (725) | 11 A | 5 | $\ldots$ | $\ldots$ | 102 | ... | $3.5 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-508 | $4 \mathrm{~N}, \mathrm{Cl} .2$ | K22375 | 115 (795) | 11B | 10 | $\ldots$ | $\ldots$ | 102 | ... | $3.5 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-508 | 3 V | K31830 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | ... | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Forgings |
| SA-508 | 5, Cl. 1 | K42365 | 105 (725) | 11 A | 5 | . . | ... | 102 | ... | $3.5 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-508 | 5, CI. 2 | K42365 | 115 (795) | 11B | 10 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $3.5 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-513 | 1008 | G10080 | 42 (290) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Tube |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum <br> Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | S- <br> No. | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-513 | 1010 | G10100 | 45 (310) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C | Tube |
| SA-513 | 1015 | G10150 | 48 (330) | 1 | 1 |  |  | 101 | $\ldots$ | C | Tube |
| A 513 | 1015 CW | G10150 | 65 (450) | $\ldots$ |  | 1 | 1 |  | 101 | C | Tube |
| A 513 | 1020 CW | G10200 | 70 (485) |  | $\ldots$ | 1 | 2 | $\ldots$ | 101 | C | Tube |
| A 513 | 1025 CW | G10250 | 75 (515) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | C | Tube |
| A 513 | 1026 CW | G10260 | 80 (550) | $\ldots$ | $\ldots$ | 1 | 3 |  | 101 | C | Tube |
| A 514 | F | K11576 | 110 (760) | ... |  | 11B | 3 | . . | 101 | $0.75 \mathrm{Ni}-0.5 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Plate, $2^{1} / 2$ in. ( 64 mm ) max. |
| A 514 | J | K11625 | 110 (760) | $\ldots$ | $\ldots$ | 11B | 6 | $\ldots$ | 101 | $\mathrm{C}-0.5 \mathrm{Mo}$ | Plate, $1^{1 / 4} \mathrm{in}$. $(32 \mathrm{~mm}$ ) max. |
| A 514 | B | K11630 | 110 (760) | ... | . . | 11B | 4 | $\ldots$ | 101 | $0.5 \mathrm{Cr}-0.2 \mathrm{Mo}-\mathrm{V}$ | Plate, $1^{1 / 4} \mathrm{in}$. (32 mm) max. |
| A 514 | D | K11662 | 110 (760) | $\ldots$ | $\ldots$ | 11B | 5 | $\ldots$ | 101 | $1 \mathrm{Cr}-0.2 \mathrm{Mo}-\mathrm{Si}$ | Plate, $1^{1 / 4} \mathrm{in}$. (32 mm) max. |
| A 514 | A | K11856 | 110 (760) | $\ldots$ | $\ldots$ | 11B | 1 | $\ldots$ | 101 | $0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{Si}$ | Plate, $1^{1 / 4}$ in. $(32 \mathrm{~mm}$ ) max. |
| A 514 | E | K21604 | 100 (690) | $\ldots$ | $\ldots$ | 11B | 2 | $\ldots$ | 102 | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | Plate $>2^{1} / 2-6 \mathrm{in}$. ( $64-152 \mathrm{~mm}$ ), incl. |
| A 514 | E | K21604 | 110 (760) | $\ldots$ | $\ldots$ | 11B | 2 |  | 102 | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | Plate, $2^{1 / 2} \mathrm{in}$. ( 64 mm ) max. |
| A 514 | P | K21650 | 100 (690) | $\ldots$ | $\ldots$ | 11B | 8 | $\ldots$ | 102 | $1.25 \mathrm{Ni}-1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | $\begin{aligned} & \text { Plate }>2^{1} / 2-6 \text { in. } \\ & \quad(64-152 \mathrm{~mm}) \text {, incl. } \end{aligned}$ |
| A 514 | P | K21650 | 110 (760) | ... | $\ldots$ | 11B | 8 | $\ldots$ | 102 | $1.25 \mathrm{Ni}-1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate, $2^{1 / 2} \mathrm{in}$. (64 mm) max. |
| A 514 | Q | ... | 100 (690) | $\ldots$ | $\ldots$ | 11B | 9 | $\ldots$ | 102 | $1.3 \mathrm{Ni}-1.3 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | $\begin{aligned} & \text { Plate }>2^{1} / 2-6 \text { in. } \\ & \quad(64-152 \mathrm{~mm}) \text {, incl. } \end{aligned}$ |
| A 514 | Q | . . | 110 (760) | $\ldots$ | $\ldots$ | 11B | 9 |  | 102 | $1.3 \mathrm{Ni}-1.3 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Plate, $2^{1} / 2 \mathrm{in}$. (64 mm) max. |
| SA-515 | 60 | K02401 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Plate |
| SA-515 | 65 | K02800 | 65 (450) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Si | Plate |
| SA-515 | 70 | K03101 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 |  | C-Si | Plate |
| SA-516 | 55 | K01800 | 55 (380) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Si | Plate |
| SA-516 | 60 | K02100 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-516 | 65 | K02403 | 65 (450) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | . . | C-Mn-Si | Plate |
| SA-516 | 70 | K02700 | 70 (485) | 1 | 2 |  |  | 101 | $\ldots$ | C-Mn-Si | Plate |
| SA-517 | F | K11576 | 115 (795) | 11 B | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Plate $\leq 2^{1} / 2 \mathrm{in}$. $(64 \mathrm{~mm})$ |
| SA-517 | J | K11625 | 115 (795) | 11B | 6 |  |  | 101 |  | C-0.5Mo | Plate $\leq 1^{1 / 4} / \mathrm{in}$. $(32 \mathrm{~mm}$ ) |
| SA-517 | B | K11630 | 115 (795) | 11B | 4 | $\ldots$ | $\ldots$ | 101 | ... | $0.5 \mathrm{Cr}-0.2 \mathrm{Mo}-\mathrm{V}$ | Plate $\leq 1^{1 / 4}$ in. $(32 \mathrm{~mm})$ |
| SA-517 | A | K11856 | 115 (795) | 11B | 1 | . . |  | 101 |  | $0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{Si}$ | Plate $\leq 1 \frac{1}{4} \mathrm{in} .(32 \mathrm{~mm})$ |
| SA-517 | E | K21604 | 105 (725) | 11 B | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | $\begin{aligned} & \text { Plate }>2^{1} / 2-6 \mathrm{in} . \\ & \quad(64-152 \mathrm{~mm}) \end{aligned}$ |
| SA-517 | E | K21604 | 115 (795) | 11B | 2 | $\ldots$ | ... | 102 | ... | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | Plate $\leq 2^{1 / 2}$ in. ( 64 mm ) |
| SA-517 | P | K21650 | 105 (725) | 11B | 8 | ... | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Ni}-1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate $>2^{1 / 2}-4 \mathrm{in}$. ( $64-102 \mathrm{~mm}$ ) |
| SA-517 | P | K21650 | 115 (795) | 11B | 8 | $\ldots$ | . $\cdot$ | 102 | $\ldots$ | $1.25 \mathrm{Ni}-1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate $\leq 21 / 2 \mathrm{in}$. $(64 \mathrm{~mm}$ ) |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)



| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS <br> No. | Tensile, ksi (MPa) | $\begin{gathered} \mathrm{P}- \\ \mathrm{N} \end{gathered}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-537 | Cl. 3 | K12437 | 80 (550) | 1 | 3 | ... | . . | 101 |  | C-Mn-Si | Plate $\leq 21 / 2$ in. ( 64 mm ) |
| SA-541 | 1 | K03506 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Si | Forgings |
| SA-541 | 1A | K03020 | 70 (485) | 1 | 2 | $\ldots$ |  | 101 |  | $\mathrm{C}-\mathrm{Mn}$-Si | Forgings |
| SA-541 | 11, CI. 4 | K11572 | 80 (550) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Forgings |
| SA-541 | 3, Cl. 1 | K12045 | 80 (550) | 3 | 3 | . . . | . . | 101 | $\ldots$ | $0.5 \mathrm{Ni}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-541 | 3, CI. 2 | K12045 | 90 (620) | 3 | 3 | $\ldots$ |  | 101 | . . | $0.5 \mathrm{Ni}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-541 | 2, Cl. 1 | K12765 | 80 (550) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-0.3 \mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-541 | 2, Cl. 2 | K12765 | 90 (620) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | . . | $0.75 \mathrm{Ni}-0.5 \mathrm{Mo}-0.3 \mathrm{Cr}-\mathrm{V}$ | Forgings |
| SA-541 | 22, CI. 3 | K21390 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-541 | 22, CI. 4 | K21390 | 105 (725) | 5 C | 4 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-541 | 22, CI. 5 | K21390 | 115 (795) | 5 C | 5 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Forgings |
| SA-541 | 3 V | K31830 | 85 (585) | 5 C | 1 | . . |  | 102 | ... | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Forgings |
| SA-541 | 22 V | K31835 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | . . . |  | $2.25 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Forgings |
| SA-542 | B, CI. 4a | K21590 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | B, CI. 4 | K21590 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | A, Cl. 4 | K21590 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | ... | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | A, CI. 4a | K21590 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | A, CI. 3 | K21590 | 95 (655) | 5 C | 3 | $\ldots$ |  | 102 |  | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | B, Cl. 3 | K21590 | 95 (655) | 5 C | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | A, Cl. 1 | K21590 | 105 (725) | 5 C | 4 | $\ldots$ | $\ldots$ | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | B, CI. 1 | K21590 | 105 (725) | 5 C | 4 | $\ldots$ | . . | 102 | ... | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | B, CI. 2 | K21590 | 115 (795) | 5 C | 5 | $\ldots$ | $\ldots$ | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | A, CI. 2 | K21590 | 115 (795) | 5 C | 5 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Plate |
| SA-542 | C, Cl. 4 | K31830 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-542 | C, CI. 4a | K31830 | 85 (585) | 5 C | 1 | $\ldots$ | $\ldots$ | 102 | ... | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-542 | C, Cl. 3 | K31830 | 95 (655) | 5 C | 3 | $\ldots$ | $\ldots$ | 102 | . . | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-542 | C, Cl. 1 | K31830 | 105 (725) | 5 C | 4 | $\ldots$ | $\ldots$ | 102 | . . | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-542 | C, Cl. 2 | K31830 | 115 (795) | 5 C | 5 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-542 | D, CI. 4a | K31835 | 85 (585) | 5 C | 1 | $\cdots$ | $\ldots$ | . . . | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Plate |
| SA-543 | B, Cl. 3 | K42339 | 90 (620) | 3 | 3 | ... | ... | 102 | ... | $3 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-543 | B, CI. 1 | K42339 | 105 (725) | 11 A | 5 | $\ldots$ | $\ldots$ | 102 | ... | $3 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-543 | B, CI. 2 | K42339 | 115 (795) | 11B | 10 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $3 \mathrm{Ni}-1.75 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-543 | C, Cl. 3 | ... | 90 (620) | 3 | 3 | ... | $\ldots$ | 102 |  | $2.75 \mathrm{Ni}-1.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-543 | C, Cl. 1 | . . | 105 (725) | 11 A | 5 | $\ldots$ | . . | 102 | . . | $2.75 \mathrm{Ni}-1.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-543 | C, Cl. 2 | ... | 115 (795) | 11B | 10 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.75 \mathrm{Ni}-1.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Plate |
| SA-553 | II | K71340 | 100 (690) | 11 A | 1 |  |  | 101 |  | 8 Ni | Plate |




WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| A 576 | G10200 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Bar |
| A 576 | G10210 | ... | ... | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Bar |
| A 576 | G10220 |  |  |  | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Bar |
| A 576 | G10230 | ... |  | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Bar |
| A 576 | G10250 | $\ldots$ |  | $\ldots$ | $\ldots$ | 1 | 1 | . . | 101 | C | Bar |
| SA-587 | $\ldots$ | K11500 | 48 (330) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C | E.R.W. pipe |
| A 588 | A, a | K11430 | 63 (435) | $\ldots$ | $\ldots$ | 3 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-0.5 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& bar |
| A 588 | A, b | K11430 | 67 (460) | $\ldots$ | $\ldots$ | 3 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-0.5 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& bar |
| A 588 | A, c | K11430 | 70 (485) | $\ldots$ | $\ldots$ | 3 | 1 | ... | 101 | $\mathrm{Mn}-0.5 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& shapes |
| A 588 | B, a | K12043 | 63 (435) | $\ldots$ | $\ldots$ | 3 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-0.6 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& bar |
| A 588 | B, b | K12043 | 67 (460) | $\ldots$ | $\ldots$ | 3 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-0.6 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& bar |
| A 588 | B, C | K12043 | 70 (485) | $\ldots$ | . | 3 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-0.6 \mathrm{Cr}-0.3 \mathrm{Cu}-\mathrm{Si}-\mathrm{V}$ | Plate \& shapes |
| SA-592 | F | K11576 | 105 (725) | 11B | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | $\begin{aligned} & \text { Forgings, } 2^{1} / 2-4 \text { in. } \\ & (64-102 \mathrm{~mm}) \end{aligned}$ |
| SA-592 | F | K11576 | 115 (795) | 11B | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.75 \mathrm{Ni}-0.5 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{V}$ | Forgings, $2^{1} / 2$ in. $(64 \mathrm{~mm})$ \& under |
| SA-592 | E | K11695 | 105 (725) | 11B | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | Forgings, $2 \not 1 / 2-4 \mathrm{in}$. (64-102 mm) |
| SA-592 | E | K11695 | 115 (795) | 11B | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.75 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Cu}$ | $\begin{aligned} & \text { Forgings, } 2^{1} / 2 \mathrm{in} \text {. }(64 \mathrm{~mm}) \\ & \text { \& under } \end{aligned}$ |
| SA-592 | A | K11856 | 105 (725) | 11B | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{Si}$ | Forgings, $2^{1} / 2-4$ in. (64-102 mm) |
| SA-592 | A | K11856 | 115 (795) | 11B | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.25 \mathrm{Mo}-\mathrm{Si}$ | Forgings, $2^{1} / 2 \mathrm{in}$. ( 64 mm ) \& under |
| A 611 | A | G10170 | 42 (290) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Sheet |
| A 611 | B | G10170 | 45 (310) | . . | $\ldots$ | 1 | 1 | $\ldots$ | 101 | C | Sheet |
| A 611 | C | G10170 | 48 (330) | $\ldots$ | $\ldots$ | 1 | 1 |  | 101 | C | Sheet |
| SA-612 | $\ldots$ | K02900 | 81 (560) | 10C | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Plate $>1 / 2-1$ in. ( $13-25 \mathrm{~mm}$ ) |
| SA-612 | $\cdots$ | K02900 | 83 (570) | 10C | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate, $1 / 2 \mathrm{in}$. ( 13 mm ) \& under |
| A 618 | II, b | K12609 | 67 (460) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | Mn-Cu-V | Tube $>3 / 4-1 \frac{1}{2} \mathrm{in}$. (19-38 mm) |
| A 618 | II, a | K12609 | 70 (485) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | $\mathrm{Mn}-\mathrm{Cu}-\mathrm{V}$ | Tube, $3 / 4 \mathrm{in}$. (19 mm) \& under |
| A 618 | III | K12700 | 65 (450) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | $\mathrm{Mn}-\mathrm{V}$ | Tube |
| A 633 | A | K01802 | 63 (435) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | Mn -Cb | Plate \& shapes |
| A 633 | Cb | K12000 | 65 (450) | $\cdots$ | $\cdots$ | 1 | 1 | ... | 101 | Mn -Cb | Plate $>2 \frac{1}{2}-4 \mathrm{in}$. ( $64-102 \mathrm{~mm}$ ), shapes |
| A 633 | Ca | K12000 | 70 (485) | $\ldots$ | . | 1 | 2 | $\ldots$ | 101 | $\mathrm{Mn}-\mathrm{Cb}$ | Plate to $21 / 2 \mathrm{in}$. $(64 \mathrm{~mm})$, |



QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. |  |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-672 | J80 | $\ldots$ | 80 (550) | 3 | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{Mn}-0.5 \mathrm{Mo}-0.75 \mathrm{Ni}$ | Fusion welded pipe |
| SA-672 | J90 | ... | 90 (620) | 3 | 3 | ... | . . | 101 | . . | $\mathrm{Mn}-0.5 \mathrm{Mo}-0.75 \mathrm{Ni}$ | Fusion welded pipe |
| SA-675 | 45 | ... | 45 (310) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | ... | C | Bar |
| SA-675 | 50 | $\ldots$ | 50 (345) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Bar |
| SA-675 | 55 | $\ldots$ | 55 (380) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C | Bar |
| SA-675 | 60 | ... | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | ... | C | Bar |
| SA-675 | 65 | $\ldots$ | 65 (450) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Bar |
| SA-675 | 70 | $\ldots$ | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C | Bar |
| A 675 | 75 | $\ldots$ | 75 (515) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | C | Bar |
| SA-688 | XM-29 | S24000 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 18Cr-3Ni-12Mn | Welded tube |
| SA-688 | TP304 | S30400 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded tube |
| SA-688 | TP304L | S30403 | 70 (485) | 8 | 1 | $\ldots$ | ... | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded tube |
| SA-688 | TP304N | S30451 | 80 (550) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded tube |
| SA-688 | TP304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded tube |
| SA-688 | TP316 | S31600 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo | Welded tube |
| SA-688 | TP316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo | Welded tube |
| SA-688 | TP316N | S31651 | 80 (550) | 8 | 1 | ... | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Welded tube |
| SA-688 | TP316LN | S31653 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 16Cr-12Ni-2Mo-N | Welded tube |
| SA-691 | CMSH-70 | K12437 | 65 (450) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Fusion welded pipe > $2^{1} / 2-4 \mathrm{in} .(64-102 \mathrm{~mm})$ |
| SA-691 | CMSH-70 | K12437 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Fusion welded pipe $\leq 2 \frac{1}{2}$ in. ( 64 mm ) |
| SA-691 | CMSH-80 | K12437 | 75 (515) | 1 | 3 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Fusion welded pipe > $2^{1} / 2-4 \mathrm{in} .(64-102 \mathrm{~mm})$ |
| SA-691 | CMSH-80 | K12437 | 80 (550) | 1 | 3 | $\cdots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Fusion welded pipe $\leq 2^{1} / 2$ in. ( 64 mm ) |
| SA-691 | CMS-75 | K02803 | 75 (515) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Fusion welded pipe |
| SA-691 | $1 \mathrm{CR}, \mathrm{Cl} .1$ | K11757 | 55 (380) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | 1CR, Cl. 2 | K11757 | 65 (450) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | 1.25CR, Cl. 1 | K11789 | 60 (415) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Fusion welded pipe |
| SA-691 | 1.25CR, CI. 2 | K11789 | 75 (515) | 4 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}-\mathrm{Si}$ | Fusion welded pipe |
| SA-691 | CM-65 | K11820 | 65 (450) | 3 | 1 | $\ldots$ | . . | 101 | . . . | C-0.5Mo | Fusion welded pipe |
| SA-691 | CM-70 | K12020 | 70 (485) | 3 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-0.5Mo | Fusion welded pipe |
| SA-691 | $0.5 \mathrm{CR}, \mathrm{Cl} .1$ | K12143 | 55 (380) | 3 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | $0.5 \mathrm{CR}, \mathrm{Cl} .2$ | K12143 | 70 (485) | 3 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $0.5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | CM-75 | K12320 | 75 (515) | 3 | 2 | ... | $\ldots$ | 101 | . . | $\mathrm{C}-0.5 \mathrm{Mo}$ | Fusion welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ |  |  |
| SA-691 | $2.25 \mathrm{CR}, \mathrm{Cl}$. 1 | K21590 | 60 (415) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | 2.25Cr-1 Mo | Fusion welded pipe |
| SA-691 | 2.25CR, Cl. 2 | K21590 | 75 (515) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | $3 \mathrm{CR}, \mathrm{Cl} .1$ | K31545 | 60 (415) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | 3CR, Cl. 2 | K31545 | 75 (515) | 5A | 1 | $\ldots$ | $\ldots$ | 102 | ... | $3 \mathrm{Cr}-1 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | $5 \mathrm{CR}, \mathrm{Cl} .1$ | K41545 | 60 (415) | 5B | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| SA-691 | $5 \mathrm{CR}, \mathrm{Cl} .2$ | K41545 | 75 (515) | 5B | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $5 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Fusion welded pipe |
| A 691 | $9 \mathrm{CR}, \mathrm{Cl} .2$ | $\ldots$ | 85 (585) | $\ldots$ | $\ldots$ | 5B | 2 | $\ldots$ | $\ldots$ | $9 \mathrm{Cr-1Mo-V}$ | Fusion welded pipe |
| A 694 | F42 | K03014 | 60 (415) | . . | . . | 1 | 1 | ... | 101 | C-Mn | Forgings |
| A 694 | F46 | K03014 | 60 (415) | $\ldots$ | $\ldots$ | 1 | 1 | . | 101 | C-Mn | Forgings |
| A 694 | F52 | K03014 | 66 (455) | $\ldots$ | $\ldots$ | 1 | 1 | $\ldots$ | 101 | $\mathrm{C}-\mathrm{Mn}$ | Forgings |
| A 694 | F56 | K03014 | 68 (470) | $\ldots$ | . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Forgings |
| A 694 | F60 | K03014 | 75 (515) | $\ldots$ | $\ldots$ | 1 | 2 | $\ldots$ | 101 | C-Mn | Forgings |
| A 694 | F65 | K03014 | 77 (530) | ... | $\ldots$ | 1 | 2 |  | 101 | $\mathrm{C}-\mathrm{Mn}$ | Forgings |
| A 694 | F70 | K03014 | 82 (565) |  |  | 1 | 3 |  | 101 | C-Mn | Forgings |
| SA-695 | Type B, Gr. 35 | K03504 | 60 (415) | 1 | 1 | . . | ... | 101 | ... | C-Mn-Si | Bar |
| SA-695 | Type B, Gr. 40 | K03504 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Bar |
| SA-696 | B | K03200 | 60 (415) | 1 | 1 | . . . | ... | 101 | ... | $\mathrm{C}-\mathrm{Mn}$-Si | Bar |
| SA-696 | C | K03200 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Bar |
| A 714 | Gr. V, Tp. E | K22035 | 65 (450) | $\ldots$ | $\ldots$ | 9A | 1 | ... | 102 | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Smls. \& welded pipe |
| A 714 | Gr. V | K22035 | 65 (450) | $\ldots$ |  | 9A | 1 |  | 102 | $2 \mathrm{Ni}-1 \mathrm{Cu}$ | Smls. \& welded pipe |
| SA-724 | A | K11831 | 90 (620) | 1 | 4 | $\ldots$ | $\ldots$ | 101 | ... | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-724 | B | K12031 | 95 (655) | 1 | 4 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}$-Si | Plate |
| SA-724 | C | K12037 | 90 (620) | 1 | 4 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-727 | $\ldots$ | K02506 | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si | Forgings |
| SA-731 | S41500 | S41500 | 115 (795) | 6 | 4 | ... | ... | 102 |  | $13 \mathrm{Cr}-4.5 \mathrm{Ni}-\mathrm{Mo}$ | Smls. \& welded pipe |
| SA-731 | TP439 | S43035 | 60 (415) | 7 | 2 | $\ldots$ | . . | 102 | ... | $18 \mathrm{Cr}-\mathrm{Ti}$ | Smls. \& welded pipe |
| SA-731 | 18Cr-2Mo | S44400 | 60 (415) | 7 | 2 | $\ldots$ | $\ldots$ | 102 | ... | 18Cr-2Mo | Smls. \& welded pipe |
| SA-731 | TPXM-33 | S44626 | 65 (450) | 101 | 1 | $\ldots$ | . . | 102 | . . | $27 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{Ti}$ | Smls. \& welded pipe |
| SA-731 | TPXM-27 | S44627 | 65 (450) | 101 | 1 | $\ldots$ | . . | 102 | ... | $27 \mathrm{Cr}-1 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-731 | S44660 | S44660 | 85 (585) | 10K | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $26 \mathrm{Cr}-3 \mathrm{Ni}-3 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-731 | S44700 | S44700 | 80 (550) | 10J | 1 | ... | ... | 102 | $\ldots$ | $29 \mathrm{Cr}-4 \mathrm{Mo}$ | Smls. \& welded pipe |
| SA-731 | S44800 | S44800 | 80 (550) | 10K | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $29 \mathrm{Cr}-4 \mathrm{Mo}-2 \mathrm{Ni}$ | Smls. \& welded pipe |
| SA-737 | B | K12001 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | C-Mn-Si-Cb | Plate |
| SA-737 | C | K12202 | 80 (550) | 1 | 3 | . . . | $\ldots$ | 101 | . . . | C-Mn-Si-V | Plate |



| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS No. |  | P- <br> No. | Group No. | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ | Group No. | P- <br> No. | S- <br> No. |  |  |
| SA-738 | A | K12447 | 75 (515) | 1 | 2 | . . | . . | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate |
| SA-738 | B | K12001 | 85 (585) | 1 | 3 | . . . | $\ldots$ | 101 | . . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}-\mathrm{Cb}$ | Plate, $21 / 2$ in. ( 64 mm ) \& under |
| SA-738 | C |  | 70 (485) | 1 | 3 | . . | . . | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate > 4-6 in. (102-152 mm), incl. |
| SA-738 | C |  | 75 (515) | 1 | 3 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate $>2 \frac{1}{2}-4$ in. ( $64-102 \mathrm{~mm}$ ) |
| SA-738 | C |  | 80 (550) | 1 | 3 | $\ldots$ | $\cdots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate, $21 / 2$ in. ( 64 mm ) \& under |
| SA-739 | Bl1 | K11797 | 70 (485) | 4 | 1 | $\ldots$ | . . | 102 | . . | $1.25 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Bar |
| SA-739 | B22 | K21390 | 75 (515) | 5 A | 1 | $\ldots$ | . . | 102 | . . | $2.25 \mathrm{Cr}-1 \mathrm{Mo}$ | Bar |
| SA-765 | I | K03046 | 60 (415) | 1 | 1 | $\ldots$ | . . | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Forgings |
| SA-765 | II | K03047 | 70 (485) | 1 | 2 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Forgings |
| SA-765 | III | K32026 | 70 (485) | 9B | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | 3.5 Ni | Forgings |
| SA-765 | IV | K02009 | 80 (550) | 1 | 3 |  |  | 101 |  | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Forgings |
| SA-789 | S31200 | S31200 | 100 (690) | 10 H | 1 | $\ldots$ | . . | 102 | . . | $25 \mathrm{Cr}-6 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S31260 | S31260 | 100 (690) | 10 H | 1 | $\ldots$ | . $\cdot$ | 102 | . $\cdot$ | $25 \mathrm{Cr}-6.5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S31500 | S31500 | 92 (635) | 10 H | 1 | $\ldots$ | $\ldots$ | 102 | . . | $18 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S31803 | S31803 | 90 (620) | 10 H | 1 | . . | . . | 102 | . $\cdot$. | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S32304 | S32304 | 87 (600) | 10 H | 1 | . $\cdot$ | . $\cdot$ | 102 | . . . | $23 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. \& welded tube $>1$ in. ( 25 mm ) |
| SA-789 | S32304 | S32304 | 100 (690) | 10 H | 1 | . . | . . | 102 | . . | $23 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. \& welded tube $\leq 1 \mathrm{in}$. 25 mm ) |
| SA-789 | S32550 | S32550 | 110 (760) | 10 H | 1 | $\ldots$ | . . | 102 | . . | $25 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-2 \mathrm{Cu}$ | Smls. \& welded tube |
| SA-789 | S32750 | S32750 | 116 (800) | 10 H | 1 | . $\cdot$ | . $\cdot$ | 102 | . . . | $25 \mathrm{Cr}-7 \mathrm{Ni}-4 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S32900 | S32900 | 90 (620) | 10 H | 1 | . . | . . | 102 | . . . | $26 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}$ | Smls. \& welded tube |
| SA-789 | S32950 | S32950 | 100 (690) | 10 H | 1 | $\cdots$ | . $\cdot$ | 102 | . . | $26 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-789 | S32760 | S32760 | 109 (750) | $\cdots$ | $\cdots$ | 10 H | 1 | $\ldots$ | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Smls. \& welded tube |
| A 789 | S32205 | S32205 | 95 (655) | $\cdots$ | $\cdots$ | 10 H | 1 |  | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-790 | S31200 | S31200 | 100 (690) | 10 H | 1 | . . | $\ldots$ | 102 | . . | $25 \mathrm{Cr}-6 \mathrm{Ni}-\mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-790 | S31260 | S31260 | 100 (690) | 10 H | 1 | . . | . . | 102 | . . | $25 \mathrm{Cr}-6.5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-790 | S31500 | S31500 | 92 (635) | 10 H | 1 | $\cdots$ | . . | 102 | . . | $18 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-790 | S31803 | S31803 | 90 (620) | 10 H | 1 | . . . | . . | 102 | . . | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-790 | S32304 | S32304 | 87 (600) | 10 H | 1 | . $\cdot$. | . . | 102 | . . . | $23 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. \& welded pipe |
| SA-790 | S32550 | S32550 | 110 (760) | 10 H | 1 | . . | . . | 102 | . . | $25 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-2 \mathrm{Cu}$ | Smls. \& welded pipe |
| SA-790 | S32750 | S32750 | 116 (800) | 10 H | 1 | . . | . . | 102 | . . . | $25 \mathrm{Cr}-7 \mathrm{Ni}-4 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-790 | S32900 | S32900 | 90 (620) | 10 H | 1 | . . . | $\cdots$ | 102 | - | $26 \mathrm{Cr}-4 \mathrm{Ni}-\mathrm{Mo}$ | Smls. \& welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade |  |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA-790 | S32950 | S32950 | 100 (690) | 10 H | 1 | $\ldots$ | $\ldots$ | 102 | . . | 26Cr-4Ni-Mo-N | Smls. \& welded pipe |
| SA-790 | S32760 | S32760 | 109 (750) | $\ldots$ | $\ldots$ | 10 H | 1 | $\ldots$ | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Smls. \& welded tube |
| A 790 | S32205 | S32205 | 90 (620) |  |  | 10 H | 1 | ... | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Smls. \& welded tube |
| SA-803 | TP439 | S43035 | 60 (415) | 7 | 2 |  |  | 102 |  | $18 \mathrm{Cr}-\mathrm{Ti}$ | Welded tube |
| SA-803 | 26-3-3 | S44660 | 85 (585) | 10K | 1 |  | $\ldots$ | 102 | $\ldots$ | $26 \mathrm{Cr}-3 \mathrm{Ni}-3 \mathrm{Mo}$ | Welded tube |
| SA-812 | Gr. 65 |  | 85 (585) | 1 | 3 |  |  | 101 | $\ldots$ | C-Mn-Cb | Sheet |
| SA-812 | Gr. 80 |  | 100 (690) | 1 | 4 |  |  | 101 | $\ldots$ | C-Mn-Si-Cb | Sheet |
| SA-813 | TPXM-19 | S20910 | 100 (690) | 8 | 3 | $\ldots$ | ... | 102 | ... | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Welded pipe |
| SA-813 | TPXM-11 | S21904 | 90 (620) | 8 | 3 | ... | ... | 102 | ... | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Welded pipe |
| SA-813 | TPXM-29 | S24000 | 100 (690) | 8 | 3 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-3 \mathrm{Ni}-12 \mathrm{Mn}$ | Welded pipe |
| SA-813 | TP304 | S30400 | 75 (515) | 8 | 1 |  | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded pipe |
| SA-813 | TP304L | S30403 | 70 (485) | 8 | 1 |  |  | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded pipe |
| SA-813 | TP304H | S30409 | 75 (515) | 8 | 1 | $\ldots$ | ... | 102 | ... | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Welded pipe |
| SA-813 | TP304N | S30451 | 80 (550) | 8 | 1 |  | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded pipe |
| SA-813 | TP304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Welded pipe |
| SA-813 | S30815 | S30815 | 87 (600) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | ... | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Welded pipe |
| SA-813 | TP309S | S30908 | 75 (515) | 8 | 2 |  |  | 102 | $\ldots$ | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Welded pipe |
| SA-813 | TP309Cb | S30940 | 75 (515) | 8 | 2 | $\ldots$ | ... | 102 | ... | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-813 | TP310S | S31008 | 75 (515) | 8 | 2 |  | ... | 102 | ... | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Welded pipe |
| SA-813 | TP310Cb | S31040 | 75 (515) | 8 | 2 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-813 | S31254 | S31254 | 94 (650) | 8 | 4 | . . | . . | 102 | ... | 20Cr-18Ni-6Mo | Welded pipe |
| SA-813 | TP316 | S31600 | 75 (515) | 8 | 1 |  | $\ldots$ | 102 | ... | 16Cr-12Ni-2Mo | Welded pipe |
| SA-813 | TP316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Welded pipe |
| SA-813 | TP316H | S31609 | 75 (515) | 8 | 1 |  | ... | 102 | ... | 16Cr-12Ni-2Mo | Welded pipe |
| SA-813 | TP316N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | ... | 102 | ... | 16Cr-12Ni-2Mo-N | Welded pipe |
| SA-813 | TP316LN | S31653 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | ... | 16Cr-12Ni-2Mo-N | Welded pipe |
| SA-813 | TP317 | S31700 | 75 (515) | 8 | 1 |  |  | 102 | ... | 18Cr-13Ni-3Mo | Welded pipe |
| SA-813 | TP317L | S31703 | 75 (515) | 8 | 1 | ... |  | 102 | ... | 18Cr-13Ni-3Mo | Welded pipe |
| SA-813 | TP321 | S32100 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Welded pipe |
| SA-813 | TP321H | S32109 | 75 (515) | 8 | 1 | ... | ... | 102 | ... | 18Cr-10Ni-Ti | Welded pipe |
| SA-813 | TP347 | S34700 | 75 (515) | 8 | 1 |  | ... | 102 | ... | 18Cr-10Ni-Cb | Welded pipe |
| SA-813 | TP347 H | S34709 | 75 (515) | 8 | 1 |  |  | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-813 | TP348 | S34800 | 75 (515) | 8 | 1 | . . | ... | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-813 | TP348H | S34809 | 75 (515) | 8 | 1 | $\ldots$ | ... | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Welded pipe |
| SA-813 | TPXM-15 | S38100 | 75 (515) | 8 | 1 | $\ldots$ | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-18 \mathrm{Ni}-2 \mathrm{Si}$ | Welded pipe |

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| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS No. |  | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ | Group No. | P. <br> No. | S- <br> No. |  |  |
| SA-814 | TPXM-19 | S20910 | 100 (690) | 8 | 3 | . . . | . . | 102 | . . . | $22 \mathrm{Cr}-13 \mathrm{Ni}-5 \mathrm{Mn}$ | Cold worked welded pipe |
| SA-814 | TPXM-11 | S21904 | 90 (620) | 8 | 3 |  |  | 102 |  | $21 \mathrm{Cr}-6 \mathrm{Ni}-9 \mathrm{Mn}$ | Cold worked welded pipe |
| SA-814 | TPXM-29 | S24000 | 100 (690) | 8 | 3 | . . | . . | 102 | . . | $18 \mathrm{Cr}-3 \mathrm{Ni}-12 \mathrm{Mn}$ | Cold worked welded pipe |
| SA-814 | TP304 | S30400 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Cold worked welded pipe |
| SA-814 | TP304L | S30403 | 70 (485) | 8 | 1 | $\ldots$. | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Cold worked welded pipe |
| SA-814 | TP304H | S30409 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}$ | Cold worked welded pipe |
| SA-814 | TP304N | S30451 | 80 (550) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Cold worked welded pipe |
| SA-814 | TP304LN | S30453 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | $\ldots$ | $18 \mathrm{Cr}-8 \mathrm{Ni}-\mathrm{N}$ | Cold worked welded pipe |
| SA-814 | S30815 | S30815 | 87 (600) | 8 | 2 | . . | . . | 102 | . . | $21 \mathrm{Cr}-11 \mathrm{Ni}-\mathrm{N}$ | Cold worked welded pipe |
| SA-814 | TP309S | S30908 | 75 (515) | 8 | 2 |  | . . | 102 |  | $23 \mathrm{Cr}-12 \mathrm{Ni}$ | Cold worked welded pipe |
| SA-814 | TP309Cb | S30940 | 75 (515) | 8 | 2 | . . | . . | 102 | . . | $23 \mathrm{Cr}-12 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | TP310S | S31008 | 75 (515) | 8 | 2 | . . . | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}$ | Cold worked welded pipe |
| SA-814 | TP310Cb | S31040 | 75 (515) | 8 | 2 | . . | . . | 102 | . . | $25 \mathrm{Cr}-20 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | S31254 | S31254 | 94 (650) | 8 | 4 | . . | $\ldots$ | 102 | . . . | 20Cr-18Ni-6Mo | Cold worked welded pipe |
| SA-814 | TP316 | S31600 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Cold worked welded pipe |
| SA-814 | TP316L | S31603 | 70 (485) | 8 | 1 | $\ldots$ |  | 102 | . . $\cdot$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Cold worked welded pipe |
| SA-814 | TP316H | S31609 | 75 (515) | 8 | 1 | . . |  | 102 | . . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}$ | Cold worked welded pipe |
| SA-814 | TP316N | S31651 | 80 (550) | 8 | 1 | $\ldots$ | . . | 102 | $\ldots$ | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Cold worked welded pipe |
| SA-814 | TP316LN | S31653 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $16 \mathrm{Cr}-12 \mathrm{Ni}-2 \mathrm{Mo}-\mathrm{N}$ | Cold worked welded pipe |
| SA-814 | TP317 | S31700 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | . . | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Cold worked welded pipe |
| SA-814 | TP317L | S31703 | 75 (515) | 8 | 1 | . . | $\ldots$ | 102 |  | $18 \mathrm{Cr}-13 \mathrm{Ni}-3 \mathrm{Mo}$ | Cold worked welded pipe |
| SA-814 | TP321 | S32100 | 75 (515) | 8 | 1 |  | . $\cdot$ | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Cold worked welded pipe |
| SA-814 | TP321H | S32109 | 75 (515) | 8 | 1 | . . | . . | 102 |  | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Ti}$ | Cold worked welded pipe |
| SA-814 | TP347 | S34700 | 75 (515) | 8 | 1 | . . | . . | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | TP347 H | S34709 | 75 (515) | 8 | 1 | . . | $\ldots$ | 102 | $\ldots$ | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | TP348 | S34800 | 75 (515) | 8 | 1 | . . | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | TP348H | S34809 | 75 (515) | 8 | 1 | $\ldots$ | . . | 102 | . . | $18 \mathrm{Cr}-10 \mathrm{Ni}-\mathrm{Cb}$ | Cold worked welded pipe |
| SA-814 | TPXM-15 | S38100 | 75 (515) | 8 | 1 | $\ldots$ | . $\cdot$ | 102 | . . | $18 \mathrm{Cr}-18 \mathrm{Ni}-2 \mathrm{Si}$ | Cold worked welded pipe |
| SA-815 | S31803 | S31803 | 90 (620) | 10 H | 1 | . . | $\ldots$ | 102 | . . | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Fittings |
| SA-815 | S41500 | S41500 | 110 (760) | 6 | 4 | $\cdots$ | $\ldots$ | 102 | . $\cdot$ | $13 \mathrm{Cr}-4.5 \mathrm{Ni}-\mathrm{Mo}$ | Fittings |
| SA-815 | S32760 | S32760 | 109 (750) | . . | . . | 10 H | 1 |  | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Fittings |
| A 815 | S32205 | S32205 | 95 (655) |  |  | 10 H | 1 |  | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Fittings |
| SA-832 | 21 V | K31830 | 85 (585) | 5 C | 1 | . . | . . | 102 | . . | $3 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}-\mathrm{Ti}-\mathrm{B}$ | Plate |
| SA-832 | 22 V | K31835 | 85 (585) | 5 C | 1 | $\cdots$ | . $\cdot$ |  | - | $2.25 \mathrm{Cr}-1 \mathrm{Mo}-\mathrm{V}$ | Plate |
| SA-836 | . | $\ldots$ | 55 (380) | 1 | 1 | . . | . . | 101 | . . | $\mathrm{C}-\mathrm{Si}-\mathrm{Ti}$ | Forgings |

WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT’D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec. No. | Type or Grade | UNS No. | Minimum Specified Tensile, ksi (MPa) | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P- <br> No. | Group No. | S- <br> No. | Group No. | P- <br> No. | S- <br> No. |  |  |
| A 890 | CD3MWCuN | $J 93380$ | 100 (690) | . . . | . . | 10 H | 1 | . . | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Castings |
| A 928 |  | S32760 | 109 (750) | . . | . . | 10 H | 1 | . . | 102 | $25 \mathrm{Cr}-8 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{W}-\mathrm{Cu}-\mathrm{N}$ | Welded pipe |
| A 928 | S32205 | S32205 | 90 (620) | . . | $\ldots$ | 10 H | 1 | . . | 102 | $22 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-\mathrm{N}$ | Welded pipe |
| A 992 | . . . | . . . | 65 (450) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Shapes |
| SA-995 | 2A | J93345 | 95 (655) | 10 H | 1 | . . | . . | 102 | . . . | 24Cr-10Ni-4Mo-N | Castings |
| SA-995 | 1 B | J93372 | 100 (690) | 10 H | 1 | . . | . . | 102 | . . | $25 \mathrm{Cr}-5 \mathrm{Ni}-3 \mathrm{Mo}-2 \mathrm{Cu}$ | Castings |
| SA-1008 | CS Type A | . . . | 40 (275) | 1 | 1 | . . | . . | 101 | . . | C | Sheet |
| SA-1008 | CS Type B | $\ldots$ | 40 (275) | 1 | 1 | . . | . . | 101 | . . | C | Sheet |
| A 1008 | DS Type B | . . | 40 (275) | . . | . . | 1 | 1 | . . | 101 | C | Sheet \& strip |
| A 1011 | CS Type B | . . | 40 (275) | . . . | . . . | 1 | 1 | . . | 101 | C | Sheet \& strip |
| A 1011 | DS Type B | $\ldots$ | 40 (275) | . . | . . | 1 | 1 | . . . | 101 | C | Sheet \& strip |
| API 5L | A $25, \mathrm{Cl}$. I | . . | 45 (310) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | A25, Cl. II | . . . | 45 (310) | . . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | A | . . . | 48 (330) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | B | . . | 60 (415) | . . | . . | 1 | 1 | . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | X42 | . . . | 60 (415) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | X46 | . . | 63 (435) | . . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | $\times 52$ | . . . | 66 (455) | . . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | $\times 56$ | . . | 71 (490) | . . . | $\ldots$ | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | X60 | . . | 75 (515) | . . . | . . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | X65 | . . | 77 (530) | . . | . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | $\times 70$ | . . | 82 (565) | . . | . . | 1 | 3 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| API 5L | X80 | $\cdots$ | 90 (620) | . $\cdot$ | $\ldots$ | 1 | 4 |  | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls. \& welded pipe \& tubes |
| MSS SP-75 | WPHY-42 | . . | 60 (415) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-46 | . . . | 63 (435) | . . . | . . | 1 | 1 | . . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-52 | . . . | 66 (455) | . . | . . | 1 | 1 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-56 | . . . | 71 (490) | . . | . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-60 | . . | 75 (515) | . . | . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-65 | $\ldots$ | 77 (530) | . . . | . . | 1 | 2 | . . | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| MSS SP-75 | WPHY-70 | - | 82 (565) | . $\cdot$ |  | 1 | 3 |  | 101 | $\mathrm{C}-\mathrm{Mn}$ | Smls./welded fittings |
| SA/AS 1548 | 5-490 | . . . | 71 (490) | 1 | 2 | . . | . . | 101 |  | C | Plate |
| SA/AS 1548 | 7-430 | . . | 62.5 (430) | 1 | 1 | $\ldots$ | . . | 101 |  | C | Plate |
| SA/AS 1548 | 7-460 | . . . | 66.5 (460) | 1 | 1 | . . | . . . | 101 |  | C | Plate |
| SA/AS 1548 | 7-490 | . | 71 (490) | 1 | 2 |  | . . | 101 |  | C | Plate |
| SA/CSA-G40.21 | Gr. 38W | $\cdots$ | 60 (415) | 1 | 1 | $\cdots$ | $\cdot$ | 101 | $\cdots$ | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate, bar, \& shapes |
| SA/CSA-G40.21 | Gr. 44W | . . | 60 (415) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | . . | $\mathrm{C}-\mathrm{Mn}-\mathrm{Si}$ | Plate, bar, \& shapes |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT’D)

| Ferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Welding |  |  |  | Brazing |  | Nominal Composition | Product Form |
| Spec. No. | Type or Grade | UNS | Tensile, ksi (MPa) | $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Group No. | $\begin{gathered} \text { S- } \\ \text { No. } \end{gathered}$ | Group No. | $\begin{gathered} \text { P- } \end{gathered}$ | $\begin{aligned} & \text { S- } \\ & \text { No. } \end{aligned}$ |  |  |
| SA/EN 10028-2 | 295 GH | $\ldots$ | 64 (440) | 1 | 1 | $\ldots$ | $\ldots$ | 101 | $\ldots$ | $\mathrm{C}-\mathrm{Mn}$-Si | Plate > 4 in. (102 mm) |
| SA/EN 10028-2 | 295 GH |  | 67 (460) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C-Mn-Si | Plate $\leq 4 \mathrm{in} .(102 \mathrm{~mm})$ |
| SA/EN 10028-3 | P275NH | $\ldots$ | 53.5 (370) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C | $\begin{gathered} \text { Plate }>2 \text { in. } \leq 4 \text { in. } \\ (51-102 \mathrm{~mm}) \end{gathered}$ |
| SA/EN 10028-3 | 275GH | $\ldots$ | 56.5 (390) | 1 | 1 | $\ldots$ | $\ldots$ | 101 |  | C | Plate $\leq 2 \mathrm{in}$. $(51 \mathrm{~mm}$ ) |
| SA/JIS G3118 | SGV480 | $\ldots$ | 70 (485) | 1 | 2 |  |  | 101 |  | C-Mn-Si | Plate |

WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi ( MPa ) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| B 16 | C36000 | $\ldots$ | 48 (330) | $\ldots$ | $\ldots$ | $\ldots$ | 107 | $65 \mathrm{Cu}-\mathrm{Zn}-3 \mathrm{~Pb}$ | Rod $\leq 1 \mathrm{in}$. ( 25 mm ) |
| B 16 | C36000 |  | 44 (305) | $\ldots$ | $\ldots$ | $\ldots$ | 107 | 65 Cu -Zn-3Pb | Rod > 1-2 in. (25-51 mm), incl. |
| B 16 | C36000 | $\ldots$ | 40 (275) |  |  |  | 107 | 65 Cu -Zn-3Pb | Rod > 2 in. ( 51 mm ) |
| B 16 | C36000 | . . | 44 (305) | ... | ... | $\ldots$ | 107 | 65 Cu -Zn-3Pb | Bar $\leq 1$ in. $(25 \mathrm{~mm})$ |
| B 16 | C36000 |  | 40 (275) | $\ldots$ | $\ldots$ | $\ldots$ | 107 | $65 \mathrm{Cu}-\mathrm{Zn}-3 \mathrm{~Pb}$ | Bar > 1 in. (25 mm) |
| B 26 | A24430 |  | 17 (115) | ... | 21 | $\ldots$ | 104 | Al-Si | Castings |
| B 26 | A03560 | T71 | 25 (170) | $\ldots$ | 21 | $\ldots$ | 104 | Al-Si | Castings |
| B 26 | A03560 | T6 | 30 (205) |  | 21 | . . | 104 | Al-Si | Castings |
| SB-42 | C10200 |  | 30 (205) | 31 | $\ldots$ | 107 | $\ldots$ | $99.95 \mathrm{Cu}-\mathrm{P}$ | Smls. pipe |
| SB-42 | C12000 | $\ldots$ | 30 (205) | 31 | . . | 107 | $\ldots$ | 99.9Cu-P | Smls. pipe |
| SB-42 | C12200 | . . | 30 (205) | 31 | . . | 107 | $\ldots$ | 99.9Cu-P | Smls. pipe |
| SB-43 | C23000 | . . | 40 (275) | 32 | . . | 107 | $\ldots$ | 85 Cu -15Zn | Smls. pipe |
| SB-61 | C92200 |  | 30 (205) | ... | ... | 107 | ... | 88Cu-Sn-Zn-Pb | Castings |
| SB-62 | C83600 |  | 28 (195) |  | $\ldots$ | 107 | $\ldots$ | 85Cu-5Sn-5Zn-5Pb | Castings |
| B 68 | C10200 | 102 | 30 (205) | ... | 31 | ... | 107 | 99.95Cu-P | Tube |
| B 68 | C12000 | 120 | 30 (205) |  | 31 | ... | 107 | 99.9Cu-P | Tube |
| B 68 | C12200 | 122 | 30 (205) | $\ldots$ | 31 | . . | 107 | 99.9Cu-P | Tube |
| SB-75 | C10200 |  | 30 (205) | 31 |  | 107 | ... | $99.95 \mathrm{Cu}-\mathrm{P}$ | Smls. tube |
| SB-75 | C12000 | . . | 30 (205) | 31 | ... | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |
| SB-75 | C12200 |  | 30 (205) | 31 | $\ldots$ | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |
| B 88 | C10200 | 102 | 30 (205) | $\ldots$ | 31 | ... | 107 | 99.95Cu-P | Tube |
| B 88 | C12000 | 120 | 30 (205) | ... | 31 | $\ldots$ | 107 | 99.9Cu-P | Tube |
| B 88 | C12200 | 122 | 30 (205) |  | 31 | $\ldots$ | 107 | 99.9Cu-P | Tube |
| SB-96 | C65500 | ... | 50 (345) | 33 | ... | 107 | $\ldots$ | 97Cu-3.3Si | Plate, sht, strip, \& bar |
| SB-98 | C65100 |  | 40 (275) | 33 | . . | 107 | $\ldots$ | $98.5 \mathrm{Cu}-1.5 \mathrm{Si}$ | Rod, bar, \& shapes |
| SB-98 | C65500 |  | 52 (360) | 33 | . . | 107 | ... | $97 \mathrm{Cu}-3 \mathrm{Si}$ | Rod, bar, \& shapes |
| SB-98 | C66100 |  | 52 (360) | 33 | $\ldots$ | 107 | $\ldots$ | $94 \mathrm{Cu}-3 \mathrm{Si}$ | Rod, bar, \& shapes |
| SB-111 | C10200 |  | 30 (205) | 31 | . . | 107 | ... | $99.95 \mathrm{Cu}-\mathrm{P}$ | Smls. tube |
| SB-111 | C12000 |  | 30 (205) | 31 | ... | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |
| SB-111 | C12200 |  | 30 (205) | 31 |  | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |
| SB-111 | C14200 |  | 30 (205) | 31 | ... | 107 | $\ldots$ | 99.4Cu-As-P | Smls. tube |
| SB-111 | C19200 | $\ldots$ | 38 (260) | 31 | $\ldots$ | 107 | $\ldots$ | 99.7Cu-Fe-P | Smls. tube |
| SB-111 | C23000 |  | 40 (275) | 32 | ... | 107 | ... | $85 \mathrm{Cu}-15 \mathrm{Zn}$ | Smls. tube |
| SB-111 | C28000 |  | 50 (345) | 32 | $\ldots$ | 107 | . | 60Cu-40Zn | Smls. tube |
| SB-111 | C44300 |  | 45 (310) | 32 | . . | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}$-1Sn-0.06As | Smls. tube |
| SB-111 | C44400 | $\cdots$ | 45 (310) | 32 | $\ldots$ | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{Sb}$ | Smls. tube |



| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, |  |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-111 | C44500 | . . | 45 (310) | 32 | . | 107 | . . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{P}$ | Smls. tube |
| SB-111 | C60800 |  | 50 (345) | 35 | . . . | 108 | . . . | 95Cu-5AI | Smls. tube |
| SB-111 | C68700 | . . | 50 (345) | 32 | . . | 108 | . . . | 78Cu-20Zn-2AI | Smls. tube |
| SB-111 | C70400 | . . | 38 (260) | 34 | . . | 107 | . . | $95 \mathrm{Cu}-5 \mathrm{Ni}$ | Smls. tube |
| SB-111 | C70600 | . . | 40 (275) | 34 | . . | 107 | . . | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Smls. tube |
| SB-111 | C71000 | . . | 45 (310) | 34 | . . | 107 | $\ldots$ | $80 \mathrm{Cu}-20 \mathrm{Ni}$ | Smls. tube |
| SB-111 | C71500 | . . | 52 (360) | 34 | . . | 107 | . . | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Smls. tube |
| SB-111 | C71640 | $\ldots$ | 63 (435) | 34 | . . | 107 | . . | $66 \mathrm{Cu}-30 \mathrm{Ni}-2 \mathrm{Fe}-2 \mathrm{Mn}$ | Smls. tube |
| SB-111 | C72200 | . . . | 45 (310) | 34 | . . . | 107 | . . . | $80 \mathrm{Cu}-16 \mathrm{Ni}-0.75 \mathrm{Fe}-0.5 \mathrm{Cr}$ | Smls. tube |
| SB-127 | N04400 |  | 70 (485) | 42 | . . . | 110 | . . | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Plate, sheet, \& strip |
| SB-135 | C23000 |  | 40 (275) | 32 | . . . | 107 | . . . | 85Cu-15Zn | Smls. tube |
| SB-148 | C95200 |  | 65 (450) | 35 | . . . | 108 | . . . | 88Cu-9AI-3Fe | Castings |
| SB-148 | C95400 |  | 75 (515) | 35 | . . | 108 | . $\cdot$. | $85 \mathrm{Cu}-11 \mathrm{Al}-4 \mathrm{Fe}$ | Castings |
| B 148 | C95300 |  | 65 (450) | . . . | 35 | . . . | 108 | 89Cu-10AI-1Fe | Castings |
| B 148 | C95500 | . . | 90 (620) | . . | 35 | . . . | 108 | $82 \mathrm{Cu}-11 \mathrm{Al}-4 \mathrm{Fe}-3 \mathrm{Mn}$ | Castings |
| B 148 | C95600 |  | 60 (415) |  | 35 |  | 108 | $90 \mathrm{Cu}-7 \mathrm{Al}-3 \mathrm{Si}$ | Castings |
| SB-150 | C61400 | $\ldots$ | 70 (485) | 35 | $\ldots$ | 108 | $\ldots$ | $90 \mathrm{Cu}-7 \mathrm{Al}-3 \mathrm{Fe}$ | Rod \& bar |
| SB-150 | C62300 | . $\cdot$ | 75 (515) | 35 | . . . | 108 | . . . | 88Cu-9AI-3Fe | Rod (round) |
| SB-150 | C63000 | . . . | 85 (585) | 35 | . . . | 108 | . . . | 81Cu-10Al-5Ni-3Fe | Rod \& bar |
| SB-150 | C64200 | . . | 70 (485) | 35 | . | 108 | . | 91Cu-7Al-2Si | Rod \& bar |
| SB-151 | C70600 | $\ldots$ | 38 (260) | 34 | . . . | 107 | . . . | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Rod \& bar |
| SB-152 | C10200 | . . | 30 (205) | 31 | . . | 107 | . . | 99.95Cu-P | Plt, sht, strip, \& bar |
| SB-152 | C10400 | . . . | 30 (205) | 31 | . . . | 107 | . . . | 99.95Cu +Ag | Plt, sht, strip, \& bar |
| SB-152 | C10500 | . . | 30 (205) | 31 | . . | 107 | $\ldots$ | $99.95 \mathrm{Cu}+\mathrm{Ag}$ | Plt, sht, strip, \& bar |
| SB-152 | C10700 | . . | 30 (205) | 31 | . . | 107 | $\ldots$ | $99.95 \mathrm{Cu}+\mathrm{Ag}$ | Plt, sht, strip, \& bar |
| SB-152 | C11000 | $\cdots$ | 30 (205) | 31 | . $\cdot$. | 107 | $\ldots$ | 99.90 Cu | Plt, sht, strip, \& bar |
| SB-152 | C12200 | . . | 30 (205) | 31 | . . . | 107 | $\ldots$ | 99.9Cu-P | Plt, sht, strip, \& bar |
| SB-152 | C12300 |  | 30 (205) | 31 | . . . | 107 | $\cdots$ | 99.9Cu-P | Plt, sht, strip, \& bar |
| SB-152 | C12500 | . $\cdot$ | 30 (205) | 31 | . $\cdot$ | 107 | $\ldots$ | 99.88 Cu | Plt, sht, strip, \& bar |
| SB-152 | C14200 | . . | 30 (205) | 31 | - | 107 | . . | 99.4Cu-As-P | Plt, sht, strip, \& bar |
| SB-160 | N02200 | . . | 55 (380) | 41 | . . | 110 | $\ldots$ | 99.0Ni | Rod \& bar |
| SB-160 | N02201 | . . | 50 (345) | 41 | . . . | 110 | . . . | 99.0Ni-Low C | Rod \& bar |
| SB-161 | N02200 | . . . | 55 (380) | 41 | . . . | 110 | . . . | 99.0 Ni | Smls. pipe \& tube |
| SB-161 | N02201 | . . | 50 (345) | 41 | . . | 110 | . . | 99.0Ni-Low C | Smls. pipe \& tube |
| SB-162 | N02200 | . . | 55 (380) | 41 | . $\cdot$ | 110 | $\cdots$ | 99.0 Ni | Plate, sheet, \& strip |
| SB-162 | N02201 | -. | 50 (345) | 41 | - . | 110 | $\cdots$ | 99.0Ni-Low C | Plate, sheet, \& strip |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-163 | N02200 |  | 55 (380) | 41 | . . | 110 | $\ldots$ | 99.0Ni | Smls. tube |
| SB-163 | N02201 |  | 50 (345) | 41 |  | 110 | $\ldots$ | 99.0Ni-Low C | Smls. tube |
| SB-163 | N04400 |  | 70 (485) | 42 |  | 110 |  | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Smls. tube |
| SB-163 | N06600 |  | 80 (550) | 43 | . . | 111 | ... | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Smls. tube |
| SB-163 | N06690 |  | 85 (585) | 43 | $\ldots$ | 111 | $\ldots$ | $58 \mathrm{Ni}-29 \mathrm{Cr}-9 \mathrm{Fe}$ | Smls. tube |
| SB-163 | N08800 |  | 75 (515) | 45 |  | 111 | $\ldots$ | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Smls. tube |
| SB-163 | N08810 |  | 65 (450) | 45 | $\ldots$ | 111 | ... | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Smls. tube |
| SB-163 | N08811 |  | 65 (450) | 45 | $\ldots$ | . | $\ldots$ | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Smls. tube |
| SB-163 | N08825 |  | 85 (585) | 45 | ... | 111 | $\ldots$ | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Smls. tube |
| SB-164 | N04400 |  | 70 (485) | 42 |  | 110 |  | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Rod, bar, \& wire |
| SB-164 | N04405 | ... | 70 (485) | 42 | $\ldots$ | 110 | $\ldots$ | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Rod, bar, \& wire |
| SB-165 | N04400 |  | 70 (485) | 42 | $\ldots$ | 110 | $\ldots$ | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Smls. pipe \& tube |
| SB-166 | N06045 |  | 90 (620) | 46 | . $\cdot$ | ... | . . | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Rod, bar, \& wire |
| SB-166 | N06600 |  | 80 (550) | 43 | $\ldots$ | 111 | $\ldots$ | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Rod, bar, \& wire |
| SB-166 | N06617 |  | 95 (655) | 43 | $\ldots$ | 111 | $\ldots$ | $52 \mathrm{Ni}-22 \mathrm{Cr}-13 \mathrm{Co}-9 \mathrm{Mo}$ | Rod, bar, \& wire |
| SB-166 | N06690 |  | 85 (585) | 43 |  | 111 |  | $58 \mathrm{Ni}-29 \mathrm{Cr}-9 \mathrm{Fe}$ | Rod, bar, \& wire |
| SB-167 | N06045 | . . | 90 (620) | 46 | $\ldots$ | $\ldots$ | $\ldots$ | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Smls. pipe \& tube |
| SB-167 | N06600 | $\ldots$ | 75 (515) | 43 | $\ldots$ | 111 | $\ldots$ | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Smls. pipe \& tube |
| SB-167 | N06617 |  | 95 (655) | 43 |  | 111 | $\ldots$ | $52 \mathrm{Ni}-22 \mathrm{Cr}-13 \mathrm{Co}-9 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-167 | N06690 | $\ldots$ | 75 (515) | 43 | $\ldots$ | 111 | $\ldots$ | $58 \mathrm{Ni}-29 \mathrm{Cr}-9 \mathrm{Fe}$ | Smls. pipe \& tube |
| SB-168 | N06045 | $\ldots$ | 90 (620) | 46 | $\ldots$ | ... | $\ldots$ | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Plate, sheet, \& strip |
| SB-168 | N06600 |  | 80 (550) | 43 | $\ldots$ | 111 | $\ldots$ | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Plate, sheet, \& strip |
| SB-168 | N06617 | . . | 95 (655) | 43 | $\ldots$ | 111 | $\ldots$ | $52 \mathrm{Ni}-22 \mathrm{Cr}-13 \mathrm{Co}-9 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-168 | N06690 | $\ldots$ | 85 (585) | 43 | . . | 111 | ... | $58 \mathrm{Ni}-29 \mathrm{Cr}-9 \mathrm{Fe}$ | Plate, sheet, \& strip |
| SB-169 | C61400 |  | 65 (450) | 35 |  | 108 | $\ldots$ | 90Cu-7Al-3Fe | Plt, sht, strip, \& bar |
| SB-171 | C36500 |  | 40 (275) | 32 | ... | 107 | $\ldots$ | $60 \mathrm{Cu}-39 \mathrm{Zn}-\mathrm{Pb}$ | Plate \& sheet |
| SB-171 | C44300 | ... | 45 (310) | 32 | ... | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}$-1Sn-0.06As | Plate \& sheet |
| SB-171 | C44400 |  | 45 (310) | 32 | ... | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{Sb}$ | Plate \& sheet |
| SB-171 | C44500 |  | 45 (310) | 32 | . . | 107 | ... | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{P}$ | Plate \& sheet |
| SB-171 | C46400 | $\ldots$ | 50 (345) | 32 | $\ldots$ | 107 | $\ldots$ | $60 \mathrm{Cu}-39 \mathrm{Zn}$-Sn | Plate \& sheet |
| SB-171 | C46500 |  | 50 (345) | 32 |  | 107 | ... | $60 \mathrm{Cu}-39 \mathrm{Zn}$-As | Plate \& sheet |
| SB-171 | C61400 |  | 65 (450) | 35 |  | 108 | $\ldots$ | $90 \mathrm{Cu}-7 \mathrm{Al}-3 \mathrm{Fe}$ | Plate \& sheet > 2-5 in. ( $51-127 \mathrm{~mm}$ ), incl. |
| SB-171 | C61400 | ... | 70 (485) | 35 | ... | 108 | ... | $90 \mathrm{Cu}-7 \mathrm{Al}-3 \mathrm{Fe}$ | Plate \& sheet $\leq 2 \mathrm{in}$. ( 51 mm ) |
| SB-171 | C63000 |  | 80 (550) | 35 | ... | 108 | ... | 81Cu-10Al-5Ni-3Fe | Plate \& sheet > $3^{1 / 2-5} \mathrm{in}$. ( $89-127 \mathrm{~mm}$ ), incl. |
| SB-171 | C63000 |  | 85 (585) | 35 | ... | 108 | ... | $81 \mathrm{Cu}-10 \mathrm{Al}-5 \mathrm{Ni}-3 \mathrm{Fe}$ | Plate \& sheet > 2-3.5 in. ( $51-89 \mathrm{~mm}$ ), incl. |
| SB-171 | C63000 | ... | 90 (620) | 35 | $\ldots$ | 108 | $\ldots$ | 81Cu-10Al-5Ni-3Fe | Plate \& sheet $\leq 2 \mathrm{in}$. $(51 \mathrm{~mm}$ ) |
| SB-171 | C70600 |  | 40 (275) | 34 | $\ldots$ | 107 | $\ldots$ | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Plate \& sheet |
| SB-171 | C71500 | $\ldots$ | 45 (310) | 34 | $\ldots$ | 107 | $\ldots$ | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Plate \& sheet > 2.5-5 in. (64-127 mm), incl. |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-171 | C71500 |  | 50 (345) | 34 | $\ldots$ | 107 | $\ldots$ | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Plate \& sheet $\leq 2.5 \mathrm{in}$. $(64 \mathrm{~mm}$ ) |
| SB-187 | C10200 | 060 | 28 (195) | 31 |  | . . . | $\ldots$ | 99.95Cu-P | Rod \& bar |
| SB-187 | C11000 | 060 | 28 (195) | 31 |  |  | $\ldots$ | 99.9 Cu | Rod \& bar |
| SB-209 | A91060 | 1060 | 8 (55) | 21 | ... | 104 | $\ldots$ | 99.60AI | Plate \& sheet |
| SB-209 | A91100 | 1100 | 11 (76) | 21 | $\ldots$ | 104 | $\ldots$ | $99.0 \mathrm{Al}-\mathrm{Cu}$ | Plate \& sheet |
| SB-209 | A93003 | 3003 | 14 (97) | 21 | $\ldots$ | 104 | $\ldots$ | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Plate \& sheet |
| SB-209 | A93004 | 3004 | 22 (150) | 22 | $\ldots$ | 104 | $\ldots$ | Al-Mn-Mg | Plate \& sheet |
| SB-209 | A95052 | 5052 | 25 (170) | 22 | $\ldots$ | 105 | $\ldots$ | Al-2.5Mg | Plate \& sheet |
| SB-209 | A95083 | 5083 | 36 (250) | 25 | $\ldots$ | 105 | $\ldots$ | Al-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 7-8 in. (178-203 mm), incl. |
| SB-209 | A95083 | 5083 | 37 (255) | 25 | $\ldots$ | 105 | $\ldots$ | Al-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 5-7 in. (127-178 mm), incl. |
| SB-209 | A95083 | 5083 | 38 (260) | 25 | ... | 105 | $\ldots$ | Al $-4.4 \mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 3-5 in. (76-127 mm), incl. |
| SB-209 | A95083 | 5083 | 39 (270) | 25 | $\ldots$ | 105 | $\ldots$ | Al-4.4Mg-Mn | Plate \& sheet > 1.5-3 in. ( $38-76 \mathrm{~mm}$ ), incl. |
| SB-209 | A95083 | 5083 | 40 (275) | 25 | $\ldots$ | 105 | $\ldots$ | Al-4.4 Mg-Mn | Plate \& sheet $>0.05-1.5 \mathrm{in}$. ( $1.3-38 \mathrm{~mm}$ ), incl. |
| SB-209 | A95086 | 5086 | 34 (235) | 25 |  | 105 |  | $\mathrm{Al}-4.0 \mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 2-3 in. ( $51-76 \mathrm{~mm}$ ), incl. |
| SB-209 | A95086 | 5086 | 35 (240) | 25 | $\ldots$ | 105 | $\ldots$ | Al-4.0 Mg-Mn | Plate \& sheet $>$ 0.05-2 in. ( $1.3-51 \mathrm{~mm}$ ), incl. |
| SB-209 | A95154 | 5154 | 30 (205) | 22 | $\ldots$ | 105 | $\ldots$ | Al -3.5 Mg | Plate \& sheet |
| SB-209 | A95254 | 5254 | 30 (205) | 22 | $\ldots$ | 105 | $\ldots$ | Al- 3.5 Mg | Plate \& sheet |
| SB-209 | A95454 | 5454 | 31 (215) | 22 | $\ldots$ | 105 | . | Al-2.7 Mg-Mn | Plate \& sheet |
| SB-209 | A95456 | 5456 | 38 (260) | 25 | $\ldots$ | 105 | $\ldots$ | Al-5.1 Mg-Mn | Plate \& sheet > 7-8 in. (178-203 mm), incl. |
| SB-209 | A95456 | 5456 | 39 (270) | 25 | $\ldots$ | 105 | $\ldots$ | Al-5.1 $\mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 5-7 in. (127-178 mm), incl. |
| SB-209 | A95456 | 5456 | 40 (275) | 25 | $\ldots$ | 105 | $\ldots$ | Al-5.1 $\mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 3-5 in. (76-127 mm), incl. |
| SB-209 | A95456 | 5456 | 41 (285) | 25 | $\ldots$ | 105 | $\ldots$ | Al-5.1 $\mathrm{Mg}-\mathrm{Mn}$ | Plate \& sheet > 1.5-3 in. ( $38-76 \mathrm{~mm}$ ), incl. |
| SB-209 | A95456 | 5456 | 42 (290) | 25 | $\ldots$ | 105 | $\ldots$ | Al-5.1 Mg-Mn | Plate \& sheet $>0.05-1.5 \mathrm{in}$. ( $1.3-38 \mathrm{~mm}$ ), incl. |
| SB-209 | A95652 | 5652 | 25 (170) | 22 | $\ldots$ | 105 | $\ldots$ | Al-2.5Mg | Plate \& sheet |
| SB-209 | A96061 | 6061 | 24 (165) | 23 | $\ldots$ | 105 | . . | Al-Mg-Si-Cu | Plate \& sheet |
| SB-209 | ... | Alclad 3003 | 13 (90) | 21 | $\ldots$ | 104 | $\ldots$ | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | ```Plate & sheet > 0.05 in. < 0.5 in. (> 1.3 mm < 13 mm)``` |
| SB-209 | ... | Alclad 3003 | 14 (97) | 21 | $\ldots$ | 104 | $\ldots$ | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Plate \& sheet $\geq 0.5-3 \mathrm{in}$. ( $13-76 \mathrm{~mm}$ ), incl. |
| SB-209 | $\ldots$ | Alclad 3004 | 21 (145) | 22 | $\ldots$ | 104 | $\ldots$ | Al-Mn-Mg | ```Plate & sheet > 0.05 in. < 0.5 in. (>1.3 mm < < 13 mm)``` |
| SB-209 | $\ldots$ | Alclad 3004 | 22 (150) | 22 | $\ldots$ | 104 | $\ldots$ | Al-Mn-Mg | Plate \& sheet $\geq 0.5-3 \mathrm{in}$. ( $13-76 \mathrm{~mm}$ ), incl. |
| SB-209 | ... | Alclad 6061 | 24 (165) | 23 | $\ldots$ | 105 | $\ldots$ | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Plate \& sheet |
| B 209 | A95050 | 5050 | 18 (125) | ... | 21 | $\ldots$ | 105 | Al-1.5Mg | Plate \& sheet |
| SB-210 | A91060 | 1060 | 8.5 (59) | 21 | $\ldots$ | 104 | $\ldots$ | 99.60AI | Smls. tube |
| SB-210 |  | Alclad 3003 | 13 (90) | 21 | $\ldots$ | 104 | $\ldots$ | Al-Mn-Cu | Smls. tube |
| SB-210 | A93003 | 3003 | 14 (97) | 21 | $\ldots$ | 104 | ... | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Smls. tube |
| SB-210 | A95052 | 5052 | 25 (170) | 22 | $\ldots$ | 105 | $\ldots$ | Al- 2.5 Mg | Smls. tube |
| SB-210 | A95154 | 5154 | 30 (205) | 22 | $\cdots$ | 105 | $\cdots$ | Al- 3.5 Mg | Smls. tube |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, | We |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-210 | A96061 | 6061 | 24 (165) | 23 | . . . | 105 | . . | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Smls. tube |
| SB-210 | A96063 | 6063 | 17 (115) | 23 | . . | 105 | . . | AI-Mg-Si | Smls. tube |
| B 210 | A95083 | 5083 | 39 (270) | . . . | 25 | . . . | 105 | AI-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Smls. tube |
| B 210 | A95086 | 5086 | 35 (240) |  | 25 |  | 105 | Al-4.0 Mg-Mn | Smls. tube |
| B 210 | A95456 | 5456 | 41 (285) |  | 25 | $\ldots$ | . . . | Al-5.1 Mg-Mn | Smls. tube |
| SB-211 | A96061 | 6061 | 24 (165) | 23 | . . . | 105 |  | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Bar, rod, \& wire |
| SB-221 | A91060 | 1060 | 8.5 (59) | 21 | . . | 104 | $\ldots$ | 99.60 Al | Bar, rod, \& shapes |
| SB-221 | A91100 | 1100 | 11 (76) | 21 | . . . | 104 | . . . | 99.0AI-Cu | Bar, rod, \& shapes |
| SB-221 | A93003 | 3003 | 14 (97) | 21 | . . | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Bar, rod, \& shapes |
| SB-221 | A95083 | 5083 | 39 (270) | 25 | . . | 105 |  | Al-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Bar, rod, \& shapes |
| SB-221 | A95154 | 5154 | 30 (205) | 22 | . . | 105 | . . | Al-3.5 Mg | Bar, rod, \& shapes |
| SB-221 | A95454 | 5454 | 31 (215) | 22 | . . | 105 | . . | Al-2.7 Mg-Mn | Bar, rod, \& shapes |
| SB-221 | A95456 | 5456 | 41 (285) | 25 | . . | 105 | $\ldots$ | Al-5.1 Mg-Mn | Bar, rod, \& shapes |
| SB-221 | A96061 | 6061 | 24 (165) | 23 | . . | 105 | . . | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Bar, rod, \& shapes |
| SB-221 | A96063 | 6063 | 17 (115) | 23 |  | 105 |  | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}$ | Bar, rod, \& shapes |
| SB-234 | A91060 | 1060 | 8.5 (59) | 21 | . . | 104 |  | 99.60 Al | Smls. tube |
| SB-234 |  | Alclad 3003 | 13 (90) | 21 | . . | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Smls. tube |
| SB-234 | A93003 | 3003 | 14 (97) | 21 | $\ldots$ | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Smls. tube |
| SB-234 | A95052 | 5052 | 25 (170) | 22 | . . | 105 | . . | Al-2.5Mg | Smls. tube |
| SB-234 | A95454 | 5454 | 31 (215) | 22 | . . | 105 | . . . | AI-2.7 Mg-Mn | Smls. tube |
| SB-234 | A96061 | 6061 | 24 (165) | 23 |  | 105 |  | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Smls. tube |
| SB-241 | A91060 | 1060 | 8.5 (59) | 21 | . . | 104 | . . | 99.60AI | Smls. pipe \& tube |
| SB-241 | A91100 | 1100 | 11 (76) | 21 | . . | 104 | . . | $99.0 \mathrm{Al}-\mathrm{Cu}$ | Smls. pipe \& tube |
| SB-241 | ... | Alclad 3003 | 13 (90) | 21 | . . | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Smls. pipe \& tube |
| SB-241 | A93003 | 3003 | 14 (97) | 21 | . . | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Pipe \& tube |
| SB-241 | A95052 | 5052 | 25 (170) | 22 | . . . | 105 | . . . | Al-2.5 Mg | Smls. pipe \& tube |
| SB-241 | A95083 | 5083 | 39 (270) | 25 | . . . | 105 |  | AI-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Smls. pipe \& tube |
| SB-241 | A95086 | 5086 | 35 (240) | 25 | . . . | 105 | . . . | Al-4.0 Mg-Mn | Smls. pipe \& tube |
| SB-241 | A95454 | 5454 | 31 (215) | 22 | . . . | 105 | . . . | AI-2.7 Mg-Mn | Smls. pipe \& tube |
| SB-241 | A95456 | 5456 | 41 (285) | 25 | . . | 105 | . . | Al-5.1 Mg-Mn | Smls. pipe \& tube |
| SB-241 | A96061 | 6061 | 24 (165) | 23 | . . | 105 | . . | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Smls. pipe \& tube |
| SB-241 | A96063 | 6063 | 17 (115) | 23 | . . | 105 | $\ldots$ | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}$ | Smls. pipe \& tube |
| SB-247 | A93003 | 3003 | 14 (97) | 21 | . . | 104 | . . | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Forgings |
| SB-247 | A95083 | 5083 | 38 (260) | 25 | . . | 105 | . . . | Al-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Forgings |
| SB-247 | A96061 | 6061 | 24 (165) | 23 | . $\cdot$ | 105 | . $\cdot$ | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Forgings |
| SB-265 | R50250 | 1 | 35 (240) | 51 | . . | 115 | . . . | Ti | Plate, sheet, \& strip |
| SB-265 | R50400 | 2 | 50 (345) | 51 | . . . | 115 | . . . | Ti | Plate, sheet, \& strip |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, |  | ing |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-265 | R50550 | 3 | 65 (450) | 52 | . . | 115 | . . | Ti | Plate, sheet, \& strip |
| SB-265 | R52250 | 11 | 35 (240) | 51 |  | 115 |  | Ti-Pd | Plate, sheet, \& strip |
| SB-265 | R52252 | 17 | 35 (240) | 51 | . . | . . . | $\ldots$ | Ti-Pd | Plate, sheet, \& strip |
| SB-265 | R52254 | 27 | 35 (220) | 51 | . . | 115 | $\ldots$ | Ti-Ru | Plate, sheet, \& strip |
| SB-265 | R52400 | 7 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Pd | Plate, sheet, \& strip |
| SB-265 | R52402 | 16 | 50 (345) | 51 | . . | 115 | . . | Ti-Pd | Plate, sheet, \& strip |
| SB-265 | R52404 | 26 | 50 (345) | 51 | $\ldots$ | 115 | . . | Ti-Ru | Plate, sheet, \& strip |
| SB-265 | R53400 | 12 | 70 (485) | 52 | $\ldots$ | 115 | $\ldots$ | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Plate, sheet, \& strip |
| SB-265 | R56320 | 9 | 90 (620) | 53 | . $\cdot$ | 115 | . $\cdot$ | Ti-3Al-2.5V | Plate, sheet, \& strip |
| SB-271 | C95200 |  | 65 (450) | 35 | . . | 108 | $\ldots$ | 88Cu-9AI-3Fe | Castings |
| SB-271 | C95400 | -. | 75 (515) | 35 | $\ldots$ | 108 | $\cdots$ | 85Cu-11Al-4Fe | Castings |
| B 280 | C10200 | 102 | 30 (205) | . . | 31 | . . | 107 | 99.95Cu-P | Smls. tube |
| B 280 | C12000 | 120 | 30 (205) | $\ldots$ | 31 | $\ldots$ | 107 | 99.9Cu-P | Smls. tube |
| B 280 | C12200 | 122 | 30 (205) | . $\cdot$. | 31 | $\ldots$ | 107 | 99.9Cu-P | Smls. tube |
| B 283 | Cl1000 | Cu | 33 (230) | $\ldots$ | 31 | $\ldots$ | 107 | 99.9 Cu | Forgings |
| B 283 | C37700 | Forging brass | 46 (315) | . . | . . . | . . | 107 | $60 \mathrm{Cu}-38 \mathrm{Zn}-2 \mathrm{~Pb}$ | Forgings > $1.5 \mathrm{in} .(38 \mathrm{~mm}$ ) |
| B 283 | C37700 | Forging brass | 50 (345) | . . | . . | $\ldots$ | 107 | $60 \mathrm{Cu}-38 \mathrm{Zn}-2 \mathrm{~Pb}$ | Forgings $\leq 1.5 \mathrm{in}$. $(38 \mathrm{~mm}$ ) |
| B 283 | C46400 | Naval brass | 64 (440) | . . | 32 | . . | 107 | $60 \mathrm{Cu}-39 \mathrm{Zn}$-Sn | Forgings |
| B 283 | C65500 | High Si bronze | 52 (360) | $\ldots$ | 33 | . . | 107 | 97Cu-3Si | Forgings |
| B 283 | C67500 | Mn bronze | 72 (495) | . . | 32 | . | 107 | 59Cu-39Zn-Fe-Sn | Forgings |
| B 302 | C12000 | . . . | 36 (250) | . . | 31 | . | 107 | 99.9Cu-P | Pipe |
| B 302 | C12200 |  | 36 (250) |  | 31 | $\cdots$ | 107 | 99.9Cu-P | Pipe |
| SB-308 | A96061 | 6061 | 24 (165) | 23 | . . | 105 | $\ldots$ | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Shapes |
| SB-315 | C65500 | . . . | 50 (345) | 33 |  | 107 | . . . | 97Cu-3Si | Smls. pipe \& tube |
| SB-333 | N10001 | $\cdots$ | 100 (690) | 44 | . $\cdot$ | 112 | $\cdots$ | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Plate, sheet, \& strip $\geq 0.1875-2.5 \mathrm{in}$. (4.8-64 mm), incl. |
| SB-333 | N10001 | . . | 115 (795) | 44 | . . | 112 | . . | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Plate, sheet, \& strip < 0.1875 in. (48 mm) |
| SB-333 | N10629 | . . | 110 (760) | 44 | . $\cdot$ | . . | . $\cdot$. | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Plate, sheet, \& strip |
| SB-333 | N10665 | -. | 110 (760) | 44 | . $\cdot$ | 112 | $\ldots$ | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Plate, sheet, \& strip |
| SB-333 | N10675 | . . | 110 (760) | 44 | -•• | 112 | $\cdots$ | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mn}-\mathrm{W}$ | Plate, sheet, \& strip |
| SB-335 | N10001 | $\cdots$ | 100 (690) | 44 | . . | 112 | . . | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Rod $>1.5-3.5 \mathrm{in}$. ( $38-89 \mathrm{~mm}$ ), incl. |
| SB-335 | N10001 | . . | 115 (795) | 44 | . . . | 112 | . $\cdot$. | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Rod $\geq 0.3125-1.5 \mathrm{in} .(8-38 \mathrm{~mm})$, incl. |
| SB-335 | N10629 |  | 110 (760) | 44 | . . . | . . | . . . | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Rod |
| SB-335 | N10665 | . . . | 110 (760) | 44 | . . . | 112 | . . | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Rod |
| SB-335 | N10675 | . . | 110 (760) | 44 | . . . | 112 | . . . | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mn}-\mathrm{W}$ | Rod |
| SB-338 | R50250 | 1 | 35 (240) | 51 | . . | 115 | . . | Ti | Smls. \& welded tube |
| SB-338 | R50400 | 2 | 50 (345) | 51 | . . | 115 | . . | Ti | Smls. \& welded tube |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, |  |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-338 | R50550 | 3 | 65 (450) | 52 | . . | 115 | . . | Ti | Smls. \& welded tube |
| SB-338 | R52400 | 7 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Pd | Smls. \& welded tube |
| SB-338 | R52402 | 16 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Pd | Smls. \& welded tube |
| SB-338 | R52404 | 26 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Ru | Smls. \& welded tube |
| SB-338 | R53400 | 12 | 70 (485) | 52 | . . | 115 | . . | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Smls. \& welded tube |
| SB-338 | R56320 | 9 | 90 (620) | 53 | . . | 115 | . . | Ti-3Al-2.5V | Smls. \& welded tube |
| B 345 | A91060 | 1060 | 8.5 (59) | . . | 21 | . . . | 104 | 99.60 Al | Smls. pipe \& tube |
| B 345 | A93003 | 3003 | 14 (97) | . . | 21 | . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Smls. pipe \& tube |
| B 345 | A95083 | 5083 | 39 (270) | . . | 25 | . . . | 105 | AI-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Smls. pipe \& tube |
| B 345 | A95086 | 5086 | 37 (255) | . . . | 25 | $\ldots$ | 105 | Al-4.0 Mg-Mn | Smls. pipe \& tube |
| B 345 | A96061 | 6061 | 24 (165) | . . | 23 | $\ldots$ | 105 | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Smls. pipe \& tube |
| B 345 | A96063 | 6063 | 17 (115) |  | 23 | . . | 105 | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}$ | Smls. pipe \& tube |
| SB-348 | R50250 | 1 | 35 (240) | 51 | . . | 115 | $\ldots$ | Ti | Bars \& billets |
| SB-348 | R50400 | 2 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti | Bars \& billets |
| SB-348 | R50550 | 3 | 65 (450) | 52 | . . | 115 | . . | Ti | Bars \& billets |
| SB-348 | R52400 | 7 | 50 (345) | 51 | . . | 115 | . . | Ti-Pd | Bars \& billets |
| SB-348 | R52404 | 26 | 50 (345) | 51 | . | 115 | . . | Ti-Ru | Bars \& billets |
| SB-348 | R53400 | 12 | 70 (485) | 52 | . . . | 115 | . . | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Bars \& billets |
| SB-348 | R52402 | 16 | 50 (345) | 51 | . . . | . | . . . | $\mathrm{Ti}-\mathrm{Pd}$ | Bars \& billets |
| SB-348 | R56320 | 9 | 90 (620) | 53 | . . | 115 | . . . | Ti-3AI-2.5V | Bars \& billets |
| A 351 | N08603 | HT30 | 65 (450) |  | 45 |  | 111 | $35 \mathrm{Ni}-15 \mathrm{Cr}-0.5 \mathrm{Mo}$ | Castings |
| SA-351 | J94651 | CN3MN | 80 (550) | 45 | . . | 111 | $\ldots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Castings |
| SA-351 | N08007 | CN7M | 62 (425) | 45 | . . | 111 | $\ldots$ | $28 \mathrm{Ni}-19 \mathrm{Cr}-\mathrm{Cu}-\mathrm{Mo}$ | Castings |
| SA-351 | N08151 | CT15C | 63 (435) | 45 |  | 111 | $\cdots$ | $32 \mathrm{Ni}-45 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Castings |
| SB-359 | C10200 | . . | 30 (205) | 31 | . . | 107 | $\ldots$ | 99.95Cu-P | Smls. tube |
| SB-359 | C12000 | . . . | 30 (205) | 31 | . . . | 107 | . . . | 99.9Cu-P | Smls. tube |
| SB-359 | C12200 | . . | 30 (205) | 31 | . . . | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |
| SB-359 | C14200 | . . . | 30 (205) | 31 | . . | 107 | . . | 99.4Cu-As-P | Smls. tube |
| SB-359 | C19200 | . . | 38 (260) | 31 | . . . | 107 | . . . | 99.7Cu-Fe-P | Smls. tube |
| SB-359 | C23000 | . . | 40 (275) | 32 | . . | 107 | . . | $85 \mathrm{Cu}-15 \mathrm{Zn}$ | Smls. tube |
| SB-359 | C44300 | . . . | 45 (310) | 32 | . . . | 107 | . . . | $71 \mathrm{Cu}-28 \mathrm{Zn}$-1Sn-0.06As | Smls. tube |
| SB-359 | C44400 | . . . | 45 (310) | 32 | . . . | 107 | . . . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{Sb}$ | Smls. tube |
| SB-359 | C44500 | . . | 45 (310) | 32 | . . | 107 | . . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{P}$ | Smls. tube |
| SB-359 | C60800 | - | 50 (345) | 35 | - | 108 | . | 95Cu-5AI | Smls. tube |
| SB-359 | C68700 | . . | 50 (345) | 32 | . . | 108 | $\ldots$ | 78Cu-20Zn-2AI | Smls. tube |
| SB-359 | C70400 | . . . | 38 (260) | 34 | . . . | 107 | . . . | $95 \mathrm{Cu}-5 \mathrm{Ni}$ | Smls. tube |



| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, | We |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-359 | C70600 |  | 40 (275) | 34 | . . | 107 | . . | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Smls. tube |
| SB-359 | C71000 |  | 45 (310) | 34 |  | 107 |  | $80 \mathrm{Cu}-20 \mathrm{Ni}$ | Smls. tube |
| SB-359 | C71500 |  | 52 (360) | 34 | $\ldots$ | 107 | $\ldots$ | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Smls. tube |
| B 361 | A91060 | WP1060 | 8 (55) | . . | 21 | . . | 104 | 99.60 Al | Fittings |
| B 361 | A91100 | WP1100 | 11 (76) | . . | 21 | . . | 104 | 99.0AI-Cu | Fittings |
| B 361 | . . . | WP Alclad 3003 | 13 (90) | . . | 21 | . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Fittings |
| B 361 | A93003 | WP3003 | 14 (97) | . . | 21 | . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Fittings |
| B 361 | A95083 | 5083 | 39 (270) | . . | 25 | . . | 105 | Al-4.4 Mg-Mn | Fittings |
| B 361 | A95154 | 5154 | 30 (205) | $\ldots$ | 22 | . . | 105 | Al-3.5Mg | Fittings |
| B 361 | A96061 | WP6061 | 24 (165) | . . | 23 | . . | 105 | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Fittings |
| B 361 | A96063 | WP6063 | 17 (115) | . . | 23 | . . | 105 | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}$ | Fittings |
| SB-363 | R50250 | WPT 1 | 35 (240) | 51 | . . | 115 | $\ldots$ | Ti | Smls. \& welded fittings |
| SB-363 | R50400 | WPT 2 | 50 (345) | 51 | $\ldots$ | 115 | $\ldots$ | Ti | Smls. \& welded fittings |
| SB-363 | R50550 | WPT 3 | 65 (450) | 52 | $\ldots$ | 115 | $\ldots$ | Ti | Smls. \& welded fittings |
| SB-363 | R52400 | 7 | 50 (345) | 51 | . . | 115 | . . | Ti-Pd | Smls. \& welded pipe |
| SB-363 | R52404 | WPT-26 | 50 (345) | 51 | . . | 115 | . . | Ti-Ru | Smls. \& welded fittings |
| SB-363 | R53400 | 12 | 70 (485) | 52 | . . | 115 | . . | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Smls. \& welded pipe |
| SB-363 | R56320 | WPT-9 | 90 (620) | 53 |  | 115 | $\ldots$ | Ti-3Al-2.5V | Smls. \& welded fittings |
| SB-366 | N02200 |  | 55 (380) | 41 | $\ldots$ | 110 | $\ldots$ | 99 Ni | Fittings |
| SB-366 | N02201 | . . | 50 (345) | 41 | . . | 110 | $\ldots$ | 99Ni-Low C | Fittings |
| SB-366 | N04400 | . $\cdot$ | 70 (485) | 42 | . . | 110 | $\ldots$ | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Fittings |
| SB-366 | N06002 | . . | 100 (690) | 43 | $\ldots$ | 111 | . . | $47 \mathrm{Ni}-22 \mathrm{Cr}-18 \mathrm{Fe}-9 \mathrm{Mo}$ | Fittings |
| SB-366 | N06007 |  | 90 (620) | 45 |  | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Fittings |
| SB-366 | N06022 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Fittings |
| SB-366 | N06030 | . . | 85 (585) | 45 | . . | 111 | $\ldots$ | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Fittings |
| SB-366 | N06045 | . $\cdot$. | 90 (620) | 46 | . . | 111 | . . | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Fittings |
| SB-366 | N06059 | . . . | 100 (690) | 43 | . $\cdot$. | 112 | . . | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Fittings |
| SB-366 | N06200 |  | 100 (690) | 43 | . $\cdot$ | 112 | . . | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Fittings |
| SB-366 | N06230 | $\cdots$ | 110 (760) | 43 | . . | . . | $\ldots$ | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Fittings |
| SB-366 | N06455 |  | 100 (690) | 43 | . . | 112 | . . | $61 \mathrm{Ni}-15 \mathrm{Mo}-16 \mathrm{Cr}$ | Fittings |
| SB-366 | N06600 | . . | 80 (550) | 43 | . . | 111 | . . | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Fittings |
| SB-366 | N06625 | . . . | 110 (760) | 43 | . . . | 111 | $\ldots$ | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Fittings |
| SB-366 | N06985 | $\cdots$ | 90 (620) | 45 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Fittings |
| SB-366 | N08020 |  | 80 (550) | 45 | . . | 111 | $\ldots$ | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Fittings |
| SB-366 | N08031 |  | 94 (650) | 45 | . . | 111 | . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Fittings |
| SB-366 | N08330 | . . . | 70 (485) | 46 | . . | 111 | . . | $35 \mathrm{Ni}-19 \mathrm{Cr}-1.25 \mathrm{SI}$ | Fittings |
| SB-366 | N08367 | $\ldots$ | 95 (655) | 45 | . $\cdot$ | 111 | $\cdots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Co}-\mathrm{N}$ | Fittings |

WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition |  | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |  |
| SB-366 | N08800 | ... | 75 (515) | 45 | $\ldots$ | 111 | $\ldots$ | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Fittings |  |
| SB-366 | N08825 | $\ldots$ | 85 (585) | 45 |  | 111 |  | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Fittings |  |
| SB-366 | N08925 | $\ldots$ | 87 (600) | 45 | $\ldots$ | 111 | $\ldots$ | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Fittings |  |
| SB-366 | N10001 | $\ldots$ | 100 (690) | 44 | $\ldots$ | 112 | $\ldots$ | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Fittings |  |
| SB-366 | N10003 | ... | 100 (690) | 44 | $\ldots$ | 112 | ... | $70 \mathrm{Ni}-16 \mathrm{Mo}-7 \mathrm{Cr}-5 \mathrm{Fe}$ | Fittings |  |
| SB-366 | N10276 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Fittings |  |
| SB-366 | N10629 | ... | 110 (760) | 44 | ... | $\ldots$ | ... | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Fittings |  |
| SB-366 | N10665 | $\ldots$ | 110 (760) | 44 | $\ldots$ | 112 | $\ldots$ | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Fittings |  |
| SB-366 | N10675 | $\ldots$ | 110 (760) | 44 | $\ldots$ | 112 | $\ldots$ | 65Ni-29.5Mo-2Cr-2Fe-Mn-W | Fittings |  |
| SB-366 | N12160 | ... | 90 (620) | 46 | . . | . . . | . . | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Fittings |  |
| SB-366 | R20033 | $\ldots$ | 109 (750) | 45 | $\ldots$ | $\ldots$ | $\ldots$ | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Fittings |  |
| B 366 | N08926 | $\ldots$ | 94 (650) | $\ldots$ | 45 | ... | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Fittings |  |
| SB-367 | R50400 | Gr. C-2 | 50 (345) | 51 | $\ldots$ | 115 | $\ldots$ | Ti | Castings |  |
| SB-367 | R50550 | Gr. C-3 | 65 (450) | 52 | $\ldots$ | 115 |  | Ti | Castings |  |
| SB-369 | C96200 | $\ldots$ | 45 (310) | 34 | $\ldots$ | 107 | $\ldots$ | 87.5Cu-10Ni-Fe-Mn | Castings |  |
| SB-381 | R50250 | F-1 | 35 (240) | 51 | ... | 115 | ... | Ti | Forgings |  |
| SB-381 | R50400 | F-2 | 50 (345) | 51 | $\ldots$ | 115 | $\ldots$ | Ti | Forgings |  |
| SB-381 | R50550 | F-3 | 65 (450) | 52 | $\ldots$ | 115 | $\ldots$ | Ti | Forgings |  |
| SB-381 | R52400 | F-7 | 50 (345) | 51 | $\ldots$ | 115 | $\ldots$ | Ti-Pd | Forgings |  |
| SB-381 | R52402 | F-16 | 50 (345) | 51 | $\ldots$ | . . | $\ldots$ | Ti-Pd | Forgings |  |
| SB-381 | R52404 | F-26 | 50 (345) | 51 | $\ldots$ | 115 | $\ldots$ | Ti-Ru | Forgings |  |
| SB-381 | R53400 | F-12 | 70 (485) | 52 | $\ldots$ | 115 | $\ldots$ | Ti-0.3Mo-0.8Ni | Forgings |  |
| SB-381 | R56320 | F-9 | 90 (620) | 53 | $\ldots$ | 115 | $\ldots$ | Ti-3Al-2.5V | Forgings |  |
| SB-395 | C10200 | $\ldots$ | 36 (250) | 31 | $\ldots$ | 107 | $\ldots$ | $99.95 \mathrm{Cu}-\mathrm{P}$ | Smls. tube |  |
| SB-395 | C12000 | . . | 36 (250) | 31 | ... | 107 | ... | 99.9Cu-P | Smls. tube |  |
| SB-395 | C12200 | $\ldots$ | 36 (250) | 31 | $\ldots$ | 107 | $\ldots$ | 99.9Cu-P | Smls. tube |  |
| SB-395 | C14200 | $\ldots$ | 36 (250) | 31 | $\ldots$ | 107 | $\ldots$ | 99.4Cu-As-P | Smls. tube |  |
| SB-395 | C19200 |  | 38 (260) | 31 | $\ldots$ | 107 | $\ldots$ | 99.7Cu-Fe-P | Smls. tube |  |
| SB-395 | C23000 | ... | 40 (275) | 32 | $\ldots$ | 107 | $\ldots$ | $85 \mathrm{Cu}-15 \mathrm{Zn}$ | Smls. tube |  |
| SB-395 | C44300 | ... | 45 (310) | 32 | ... | 107 | ... | 71Cu-28Zn-1Sn-0.06As | Smls. tube |  |
| SB-395 | C44400 |  | 45 (310) | 32 | $\ldots$ | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{Sb}$ | Smls. tube |  |
| SB-395 | C44500 |  | 45 (310) | 32 | $\ldots$ | 107 | $\ldots$ | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{P}$ | Smls. tube |  |
| SB-395 | C60800 |  | 50 (345) | 35 | $\ldots$ | 108 | $\ldots$ | 95Cu-5AI | Smls. tube |  |
| SB-395 | C68700 | ... | 50 (345) | 32 | $\ldots$ | 108 | $\ldots$ | $78 \mathrm{Cu}-20 \mathrm{Zn}-2 \mathrm{Al}$ | Smls. tube |  |
| SB-395 | C70600 | $\ldots$ | 40 (275) | 34 | $\ldots$ | 107 | $\ldots$ | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Smls. tube |  |
| SB-395 | C71000 | $\ldots$ | 45 (310) | 34 | $\ldots$ | 107 | $\ldots$ | $80 \mathrm{Cu}-20 \mathrm{Ni}$ | Smls. tube |  |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, |  |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-395 | C71500 | . . | 52 (360) | 34 | . . . | 107 | . . | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Smls. tube |
| SB-407 | N08800 |  | 75 (515) | 45 | . . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Smls. pipe \& tube |
| SB-407 | N08810 |  | 65 (450) | 45 | . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Smls. pipe \& tube |
| SB-407 | N08811 | . . | 65 (450) | 45 | . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Smls. pipe \& tube |
| SB-408 | N08800 | . . | 75 (515) | 45 | . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Rod \& bar |
| SB-408 | N08810 | . . | 65 (450) | 45 | . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Rod \& bar |
| SB-408 | N08811 | . . . | 65 (450) | 45 | . . . | 111 | . . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Rod \& bar |
| SB-409 | N08800 | . . | 75 (515) | 45 | . . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Plate, sheet, \& strip |
| SB-409 | N08810 | . . | 65 (450) | 45 | . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Plate, sheet, \& strip |
| SB-409 | N08811 |  | 65 (450) | 45 | . . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Plate, sheet, \& strip |
| SB-423 | N08825 |  | 75 (515) | 45 | . . | 111 | . . | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Smls. pipe \& tube |
| SB-424 | N08825 |  | 85 (585) | 45 | . . | 111 | . . | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Plate, sheet, \& strip |
| SB-425 | N08825 |  | 85 (585) | 45 |  | 111 |  | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Rod \& bar |
| SB-434 | N10003 | . . | 100 (690) | 44 | . . | 112 |  | $70 \mathrm{Ni}-16 \mathrm{Mo}-7 \mathrm{Cr}-5 \mathrm{Fe}$ | Plate, sheet, \& strip |
| SB-435 | N06002 | . . . | 95 (655) | 43 | . . . | 111 | . . . | $47 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-18 \mathrm{Fe}$ | Plate, sheet, \& strip |
| SB-435 | N06230 | . . | 110 (760) | 43 | . . | 111 | . . | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-435 | N12160 |  | 90 (620) | 46 | $\ldots$ | . . |  | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Plate, sheet, \& strip |
| SB-435 | R30556 |  | 100 (690) | 45 | . . | 111 | . . | $21 \mathrm{Ni}-30 \mathrm{Fe}-22 \mathrm{Cr}-18 \mathrm{Co}-3 \mathrm{Mo}-3 \mathrm{~W}$ | Plate, sheet, \& strip |
| SB-443 | N06625 | 2 | 100 (690) | 43 | . . | 111 | . . . | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Plate, sheet, \& strip |
| SB-443 | N06625 | 1 | 110 (760) | 43 |  | 111 |  | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Plate, sheet, \& strip |
| SB-444 | N06625 | 1 | 120 (825) | 43 | $\ldots$ | 111 | . . | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Smls. Pipe \& tube |
| SB-444 | N06625 | 2 | 100 (690) | 43 | . . | 111 | . $\cdot$ | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Smls. Pipe \& tube |
| SB-446 | N06625 | 1 | 120 (825) | 43 | . . | 111 | . . | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Rod \& bar |
| SB-446 | N06625 | 2 | 100 (690) | 43 | . . | 111 | . . | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Rod \& bar |
| SB-462 | N06022 | . . . | 100 (690) | 43 | . . | 112 | . . | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Forgings |
| SB-462 | N06030 |  | 85 (585) | 45 |  | 111 |  | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Forgings |
| SB-462 | N06200 |  | 100 (690) | 43 | . . | 112 | . . | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Forgings |
| SB-462 | N08020 |  | 80 (550) | 45 | . . | 111 | . . | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Forgings |
| SB-462 | N08367 |  | 95 (655) | 45 | . . . | 111 | . . . | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Forgings |
| SB-462 | N10276 | . . | 100 (690) | 43 | . . . | 112 | . . . | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Forgings |
| SB-462 | N10665 | . . | 110 (760) | 44 | . . | 112 | . | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Forgings |
| SB-462 | N10675 | . . . | 110 (760) | 44 | . . . | 112 | . . . | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Fe}-2 \mathrm{Cr}$ | Forgings |
| SB-463 | N08020 | . . . | 80 (550) | 45 | . . . | 111 | . . . | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Plate, sheet, \& strip |
| SB-463 | N08024 | . . | 80 (550) | 45 | . . | 111 | . . | $37 \mathrm{Ni}-33 \mathrm{Fe}-23 \mathrm{Cr}-4 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-463 | N08026 | $\cdots$ | 80 (550) | 45 | . . | 111 | $\ldots$ | $35 \mathrm{Ni}-30 \mathrm{Fe}-24 \mathrm{Cr}-6 \mathrm{Mo}-3 \mathrm{Cu}$ | Plate, sheet, \& strip |
| SB-464 | N08020 | . . | 80 (550) | 45 | . . | 111 | . . | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Welded pipe |
| SB-464 | N08024 | . . . | 80 (550) | 45 | . . | 111 | . . . | $37 \mathrm{Ni}-33 \mathrm{Fe}-23 \mathrm{Cr}-4 \mathrm{Mo}$ | Welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-464 | N08026 | . | 80 (550) | 45 | . . | 111 | . . . | $35 \mathrm{Ni}-30 \mathrm{Fe}-24 \mathrm{Cr}-6 \mathrm{Mo}-3 \mathrm{Cu}$ | Welded pipe |
| SB-466 | C70600 |  | 38 (260) | 34 |  | 107 |  | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Smls. Pipe \& tube |
| SB-466 | C71000 |  | 45 (310) | 34 |  | 107 |  | $80 \mathrm{Cu}-20 \mathrm{Ni}$ | Smls. Pipe \& tube |
| SB-466 | C71500 |  | 50 (345) | 34 |  | 107 | $\ldots$ | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Smls. Pipe \& tube |
| SB-467 | C70600 | . . | 38 (260) | 34 | . . . | 107 | $\ldots$ | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Welded pipe $>4.5 \mathrm{in}$. $(114 \mathrm{~mm})$ O.D. |
| SB-467 | C70600 | . . | 40 (275) | 34 | . . . | 107 | . . . | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Welded pipe $\leq 4.5 \mathrm{in}$. (114 mm) 0. D. |
| SB-467 | C71500 | . . | 45 (310) | 34 | . . | 107 | $\ldots$ | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Welded pipe $>4.5 \mathrm{in}$. $(114 \mathrm{~mm})$ O.D. |
| SB-467 | C71500 | . . | 50 (345) | 34 | . . | 107 | . . | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Welded pipe $\leq 4.5 \mathrm{in}$. $(114 \mathrm{~mm}$ ) O.D. |
| SB-468 | N08020 |  | 80 (550) | 45 | . . . | 111 | . . | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Welded tube |
| SB-468 | N08024 |  | 80 (550) | 45 | . . | 111 | . . | $37 \mathrm{Ni}-33 \mathrm{Fe}-23 \mathrm{Cr}-4 \mathrm{Mo}$ | Welded tube |
| SB-468 | N08026 |  | 80 (550) | 45 | . . | 111 | . . | $35 \mathrm{Ni}-30 \mathrm{Fe}-24 \mathrm{Cr}-6 \mathrm{Mo}-3 \mathrm{Cu}$ | Welded tube |
| SB-473 | N08020 |  | 80 (550) | 45 |  | 111 | . . | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Bar |
| B 491 | A93003 | 3003 | 14 (97) | . . . | 21 | . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Extruded tubes |
| SB-493 | R60702 | R60702 | 55 (380) | 61 | . . | 117 | . . | 99.2Zr | Forgings |
| SB-493 | R60705 | R60705 | 70 (485) | 62 | . . | 117 | . . | 95.5Zr+2.5Cb | Forgings |
| SA-494 | N26022 | CX2MW | 80 (550) | 43 | . . | . . | $\ldots$ | 59Ni-22Cr-14Mo-4Fe-3W | Castings |
| SB-505 | C95200 | ... | 68 (470) | 35 | . . | 108 | . . | 88Cu-9AI-3Fe | Castings |
| SB-511 | N08330 |  | 70 (485) | 46 |  | 111 |  | $35 \mathrm{Ni}-19 \mathrm{Cr}-1.25 \mathrm{Si}$ | Bars \& shapes |
| SB-514 | N08800 |  | 75 (515) | 45 | . . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Welded pipe |
| SB-514 | N08810 | . . | 65 (450) | 45 | . . | 111 |  | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Welded pipe |
| SB-515 | N08800 | . . | 75 (515) | 45 | . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Welded tube |
| SB-515 | N08810 | . . | 65 (450) | 45 | . . | 111 | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Welded tube |
| SB-515 | N08811 | . . | 65 (450) | 45 | . . | . . | . . | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Welded tube |
| SB-516 | N06045 | . . | 90 (620) | 46 | . . | . $\cdot$ | $\ldots$ | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Welded tube |
| SB-516 | N06600 | . . | 80 (550) | 43 | . . | 111 | . . | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Welded tube |
| SB-517 | N06045 |  | 90 (620) | 46 | . . | . . | . . | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Welded pipe |
| SB-517 | N06600 |  | 80 (550) | 43 | . . | 111 | . . . | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Welded pipe |
| SB-523 | R60702 | R60702 | 55 (380) | 61 | . . | 117 | . . | 99.2Zr | Smls. \& welded tube |
| SB-523 | R60705 | R60705 | 80 (550) | 62 | . . | 117 | . . | 95.5Zr+2.5Cb | Smls. \& welded tube |
| SB-535 | N08330 | . . . | 70 (485) | 46 | . . | 111 | . . . | $35 \mathrm{Ni}-19 \mathrm{Cr}-1.25 \mathrm{Si}$ | Smls. pipe |
| SB-536 | N08330 |  | 70 (485) | 46 | . . | 111 | . . . | $35 \mathrm{Ni}-19 \mathrm{Cr}-1.25 \mathrm{Si}$ | Plate, sheet, \& strip |
| SB-543 | C12200 | . . . | 30 (205) | 31 | . . | 107 | . . | 99.9Cu-P | Welded tube |
| SB-543 | C19400 | . . | 45 (310) | 31 | . . | 107 | . . . | 97.5Cu-P | Welded tube |
| SB-543 | C23000 |  | 40 (275) | 32 | . . | 107 | . . | $85 \mathrm{Cu}-15 \mathrm{Zn}$ | Welded tube |
| SB-543 | C44300 |  | 45 (310) | 32 | . . . | 107 | . . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{As}$ | Welded tube |
| SB-543 | C44400 |  | 45 (310) | 32 | . . | 107 | . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{Sb}$ | Welded tube |
| SB-543 | C44500 | . . . | 45 (310) | 32 | $\ldots$ | 107 | . . . | $71 \mathrm{Cu}-28 \mathrm{Zn}-1 \mathrm{Sn}-0.06 \mathrm{P}$ | Welded tube |



| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, | We |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-543 | C68700 | . . | 50 (345) | 32 | . . | 108 | . . | 78Cu-20Zn-2AI | Welded tube |
| SB-543 | C70400 |  | 38 (260) | 34 |  | 107 |  | $95 \mathrm{Cu}-5 \mathrm{Ni}$ | Welded tube |
| SB-543 | C70600 |  | 40 (275) | 34 | . . | 107 | . . | $90 \mathrm{Cu}-10 \mathrm{Ni}$ | Welded tube |
| SB-543 | C71500 |  | 52 (360) | 34 | . . | 107 | . . | $70 \mathrm{Cu}-30 \mathrm{Ni}$ | Welded tube |
| SB-543 | C71640 |  | 63 (435) | 34 | . . | 107 | . . | 66Cu-30Ni-2Fe-2Mn | Welded tube |
| B 547 | . . | Alclad 3003 | 13 (90) | . . . | 21 | . . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Welded tube |
| B 547 | A93003 | 3003 | 14 (97) | . . | 21 | . . | 104 | $\mathrm{Al}-\mathrm{Mn}-\mathrm{Cu}$ | Welded tube |
| B 547 | A95083 | 5083 | 40 (275) | $\ldots$ | 25 | . . | 105 | Al-4.4 $\mathrm{Mg}-\mathrm{Mn}$ | Welded tube |
| B 547 | A95454 | 5454 | 31 (215) | . . | 22 | . . | 105 | Al-2.7 Mg-Mn | Welded tube |
| B 547 | A96061 | 6061 | 24 (165) | . . | 23 | $\ldots$ | 105 | $\mathrm{Al}-\mathrm{Mg}-\mathrm{Si}-\mathrm{Cu}$ | Welded tube |
| SB-550 | R60702 | R60702 | 55 (380) | 61 | . . | 117 | . . | 99.2Zr | Bar \& wire |
| SB-550 | R60705 | R60705 | 80 (550) | 62 | $\ldots$ | 117 | . . | 95.5Zr+2.5Cb | Bar \& wire |
| SB-551 | R60702 | R60702 | 55 (380) | 61 | . . | 117 | . $\cdot$ | 99.2Zr | Plate, sheet, \& strip |
| SB-551 | R60705 | R60705 | 80 (550) | 62 | $\ldots$ | 117 | $\cdots$ | $95.5 \mathrm{Zr}+2.5 \mathrm{Cb}$ | Plate, sheet, \& strip |
| SB-564 | N04400 |  | 70 (485) | 42 | . . | 110 | . . | $67 \mathrm{Ni}-30 \mathrm{Cu}$ | Forgings |
| SB-564 | N06022 |  | 100 (690) | 43 | . . | 112 | $\ldots$ | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Forgings |
| SB-564 | N06045 | . . | 90 (620) | 46 | $\ldots$ | . . | $\ldots$ | $46 \mathrm{Ni}-27 \mathrm{Cr}-23 \mathrm{Fe}-2.75 \mathrm{Si}$ | Forgings |
| SB-564 | N06059 | . . | 100 (690) | 43 | $\ldots$ | 111 | . . | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Forgings |
| SB-564 | N06200 |  | 100 (690) | 43 |  | 112 | $\cdots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Forgings |
| SB-564 | N06230 | $\ldots$ | 110 (760) | 43 | $\ldots$ | . $\cdot$ | $\ldots$ | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Forgings |
| SB-564 | N06600 | $\ldots$ | 80 (550) | 43 | . . | 111 | $\ldots$ | $72 \mathrm{Ni}-15 \mathrm{Cr}-8 \mathrm{Fe}$ | Forgings |
| SB-564 | N06617 | . $\cdot$ | 95 (655) | 43 | . . | 111 | $\ldots$ | $52 \mathrm{Ni}-22 \mathrm{Cr}-13 \mathrm{Co}-9 \mathrm{Mo}$ | Forgings |
| SB-564 | N06625 | . . . | 110 (760) | 43 | . $\cdot$. | 111 | $\ldots$ | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Forgings $>4-10 \mathrm{in}$. (102-254 mm), incl. |
| SB-564 | N06686 | . $\cdot$ | 100 (690) | 43 | . . | 111 | $\cdots$ | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Forgings |
| SB-564 | N06625 | . . | 120 (825) | 43 | . . | 111 | $\ldots$ | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Forgings $\leq 4 \mathrm{in}$. $(102 \mathrm{~mm}$ ) |
| SB-564 | N06690 | . . | 85 (585) | 43 | $\ldots$ | . . | $\ldots$ | $58 \mathrm{Ni}-29 \mathrm{Cr}-9 \mathrm{Fe}$ | Forgings |
| SB-564 | N08031 | . . | 94 (650) | 45 | . . | 111 | $\ldots$ | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Forgings |
| SB-564 | N08367 | . . | 95 (655) | 45 | . . | 111 | $\ldots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Forgings |
| SB-564 | N08800 | $\cdots$ | 75 (515) | 45 | - | 111 | - | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Forgings |
| SB-564 | N08810 | . . | 65 (450) | 45 | . . | 111 | $\ldots$ | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}$ | Forgings |
| SB-564 | N08811 | . $\cdot$. | 65 (450) | 45 | . $\cdot$. | . . | $\ldots$ | $33 \mathrm{Ni}-42 \mathrm{Fe}-21 \mathrm{Cr}-\mathrm{Al}-\mathrm{Ti}$ | Forgings |
| SB-564 | N08825 | . . | 85 (585) | 45 | . . | 111 | . . | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Forgings |
| SB-564 | N10276 |  | 100 (690) | 43 | . . . | 112 | . . . | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Forgings |
| SB-564 | N10629 | . . | 110 (760) | 44 | . $\cdot$. | . . . | . . | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Forgings |
| SB-564 | N10675 | . . | 110 (760) | 44 | . . | 112 | . . | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mn}-\mathrm{W}$ | Forgings |
| SB-564 | R20033 | $\cdots$ | 109 (750) | 45 | . . | . . . | $\cdots$ | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Forgings |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-564 | N12160 | $\ldots$ | 90 (620) | 46 | $\ldots$ | $\ldots$ | $\ldots$ | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Forgings |
| B 564 | N08825 |  | 85 (585) | $\ldots$ | 45 | $\ldots$ | 111 | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Forgings |
| SB-572 | N06002 |  | 95 (655) | 43 | ... | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-18 \mathrm{Fe}$ | Rod |
| SB-572 | N06230 |  | 110 (760) | 43 |  | 111 | $\ldots$ | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Rod |
| SB-572 | N12160 |  | 90 (620) | 46 |  |  | $\ldots$ | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Rod |
| SB-572 | R30556 |  | 100 (690) | 45 |  | 111 | ... | $21 \mathrm{Ni}-30 \mathrm{Fe}-22 \mathrm{Cr}-18 \mathrm{Co}-3 \mathrm{Mo}-3 \mathrm{~W}$ | Rod |
| SB-573 | N10003 | $\ldots$ | 100 (690) | 44 | $\ldots$ | 112 | $\ldots$ | $70 \mathrm{Ni}-16 \mathrm{Mo}-7 \mathrm{Cr}-5 \mathrm{Fe}$ | Rod |
| SB-574 | N06022 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Rod |
| SB-574 | N06059 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Rod |
| SB-574 | N06200 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | ... | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Rod |
| SB-574 | N06455 | . . | 100 (690) | 43 | . . | 112 | $\ldots$ | $61 \mathrm{Ni}-16 \mathrm{Mo}-16 \mathrm{Cr}$ | Rod |
| SB-574 | N06686 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 111 | $\ldots$ | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Rod |
| SB-574 | N10276 |  | 100 (690) | 43 |  | 112 | $\ldots$ | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Rod |
| SB-575 | N06022 | ... | 100 (690) | 43 | $\ldots$ | 112 | ... | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-575 | N06059 |  | 100 (690) | 43 |  | 112 | ... | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-575 | N06200 | $\ldots$ | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Plate, sheet, \& strip |
| SB-575 | N06455 | ... | 100 (690) | 43 | $\ldots$ | 112 | ... | $61 \mathrm{Ni}-16 \mathrm{Mo}-16 \mathrm{Cr}$ | Plate, sheet, \& strip |
| SB-575 | N06686 |  | 100 (690) | 43 |  | 111 | ... | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Plate, sheet, \& strip |
| SB-575 | N10276 |  | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Plate, sheet, \& strip |
| SB-581 | N06007 |  | 85 (585) | 45 |  | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Rod > 0.75-3.5 in. (19-89 mm), incl. |
| SB-581 | N06007 | . . | 90 (620) | 45 | ... | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Rod, $0.3125-0.75 \mathrm{in}$. (8-19 mm), incl. |
| SB-581 | N06030 |  | 85 (585) | 45 | $\ldots$ | 111 | ... | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Rod |
| SB-581 | N06975 | $\ldots$ | 85 (585) | 45 | ... | 111 | ... | $49 \mathrm{Ni}-25 \mathrm{Cr}-18 \mathrm{Fe}-6 \mathrm{Mo}$ | Rod |
| SB-581 | N06985 | ... | 85 (585) | 45 | . . | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Rod > 0.75-3.5 in. (19-89 mm), incl. |
| SB-581 | N06985 | $\ldots$ | 90 (620) | 45 | ... | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Rod, 0.3125-0.75 in. ( $8-19 \mathrm{~mm}$ ), incl. |
| SB-581 | N08031 |  | 94 (650) | 45 |  | 111 | $\ldots$ | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Rod |
| SB-582 | N06007 | $\ldots$ | 85 (585) | 45 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Plate, sheet, \& strip > 0.75-2.5 in. (19-64 mm), incl. |
| SB-582 | N06007 |  | 90 (620) | 45 | $\ldots$ | 111 | ... | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Plate, sheet, \& strip $\leq 0.75 \mathrm{in}$. $(19 \mathrm{~mm}$ ) |
| SB-582 | N06030 |  | 85 (585) | 45 |  | 111 | ... | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-582 | N06975 | ... | 85 (585) | 45 | . . | 111 | ... | $49 \mathrm{Ni}-25 \mathrm{Cr}-18 \mathrm{Fe}-6 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-582 | N06985 | $\ldots$ | 85 (585) | 45 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Plate, sheet, \& strip > 0.75-2.5 in. ( $19-64 \mathrm{~mm}$ ), incl. |
| SB-582 | N06985 | ... | 90 (620) | 45 | ... | 111 | ... | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Plate, sheet, \& strip $\leq 0.75 \mathrm{in}$. (19 mm) |
| SB-599 | N08700 | $\ldots$ | 80 (550) | 45 | $\ldots$ | 111 | $\ldots$ | $25 \mathrm{Ni}-47 \mathrm{Fe}-21 \mathrm{Cr}-5 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-619 | N06002 |  | 100 (690) | 43 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-18 \mathrm{Fe}$ | Welded pipe |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, |  |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-619 | N06007 |  | 90 (620) | 45 | . . | 111 | . . | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N06022 |  | 100 (690) | 43 |  | 112 |  | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N06030 |  | 85 (585) | 45 |  | 111 |  | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N06059 | . . | 100 (690) | 43 | . . | 112 | $\ldots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N06200 |  | 100 (690) | 43 | . . . | 112 |  | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Welded pipe |
| SB-619 | N06230 | . . | 110 (760) | 43 | . . | 111 | . . | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Welded pipe |
| SB-619 | N06455 | . . | 100 (690) | 43 | $\ldots$ | 112 | . . | $61 \mathrm{Ni}-16 \mathrm{Mo}-16 \mathrm{Cr}$ | Welded pipe |
| SB-619 | N06686 |  | 100 (690) | 43 | . . | 111 | $\ldots$ | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Welded pipe |
| SB-619 | N06975 |  | 85 (585) | 45 | $\ldots$ | 111 | . . | $49 \mathrm{Ni}-25 \mathrm{Cr}-18 \mathrm{Fe}-6 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N06985 |  | 90 (620) | 45 |  | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N08031 |  | 94 (650) | 45 | . . | 111 | . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Welded pipe |
| SB-619 | N08320 |  | 75 (515) | 45 | . . | 111 | $\ldots$ | $26 \mathrm{Ni}-22 \mathrm{Cr}-5 \mathrm{Mo}-\mathrm{Ti}$ | Welded pipe |
| SB-619 | N10001 |  | 100 (690) | 44 | $\ldots$ | 112 | $\ldots$ | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Welded pipe |
| SB-619 | N10276 | . . | 100 (690) | 43 | $\ldots$ | 112 | $\ldots$ | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Welded pipe |
| SB-619 | N10629 |  | 110 (760) | 44 | . . | . . | . . | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Welded pipe |
| SB-619 | N10665 |  | 110 (760) | 44 |  | 112 |  | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Welded pipe |
| SB-619 | N10675 | . . | 110 (760) | 44 | $\ldots$ | 112 | $\ldots$ | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mn}-\mathrm{W}$ | Welded pipe |
| SB-619 | N12160 | $\ldots$ | 90 (620) | 46 | . . | . . . | $\ldots$ | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Welded pipe |
| SB-619 | R20033 | $\ldots$ | 109 (750) | 45 | . . | . . | . . | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Welded pipe |
| SB-619 | R30556 | . . | 100 (690) | 45 | . . | 111 | . . | $21 \mathrm{Ni}-30 \mathrm{Fe}-22 \mathrm{Cr}-18 \mathrm{Co}-3 \mathrm{Mo}-3 \mathrm{~W}$ | Welded pipe |
| SB-620 | N08320 | $\ldots$ | 75 (515) | 45 | . . | 111 | . . | $26 \mathrm{Ni}-22 \mathrm{Cr}-5 \mathrm{Mo}-\mathrm{Ti}$ | Plate, sheet, \& strip |
| SB-621 | N08320 |  | 75 (515) | 45 |  | 111 |  | $26 \mathrm{Ni}-22 \mathrm{Cr}-5 \mathrm{Mo}-\mathrm{Ti}$ | Rod |
| SB-622 | N06002 |  | 100 (690) | 43 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-18 \mathrm{Fe}$ | Smls. pipe \& tube |
| SB-622 | N06007 | $\ldots$ | 90 (620) | 45 | $\ldots$ | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06022 | $\ldots$ | 100 (690) | 43 | . . | 112 | . . | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06030 | . . . | 85 (585) | 45 | . . | 111 | . . | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06059 |  | 100 (690) | 43 | . . | 112 | $\cdots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06200 | $\cdots$ | 100 (690) | 43 | . . | 112 | $\ldots$ | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Smls. pipe \& tube |
| SB-622 | N06230 | . . . | 110 (760) | 43 | . . | 111 | . . | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06455 | . . . | 100 (690) | 43 | . . . | 112 | . . . | $61 \mathrm{Ni}-16 \mathrm{Mo}-16 \mathrm{Cr}$ | Smls. pipe \& tube |
| SB-622 | N06686 | . . . | 100 (690) | 43 | . . . | 111 | . . . | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Smls. pipe and tube |
| SB-622 | N06975 | . . | 85 (585) | 45 | . . . | 111 | . . . | $49 \mathrm{Ni}-25 \mathrm{Cr}-18 \mathrm{Fe}-6 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N06985 | $\cdots$ | 90 (620) | 45 | . . | 111 | . . | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N08031 |  | 94 (650) | 45 | . . . | 111 | . . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Smls. pipe \& tube |
| SB-622 | N08320 |  | 75 (515) | 45 | . . . | 111 | . . . | $26 \mathrm{Ni}-22 \mathrm{Cr}-5 \mathrm{Mo}-\mathrm{Ti}$ | Smls. pipe \& tube |
| SB-622 | N10001 | . . . | 100 (690) | 44 | . . . | 112 | . . . | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Smls. pipe \& tube |
| SB-622 | N10276 | . $\cdot$ | 100 (690) | 43 | $\cdots$ | 112 | $\cdots$ | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Smls. pipe \& tube |

QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-622 | N10629 |  | 110 (760) | 44 | . . . | . . . |  | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Smls. pipe \& tube |
| SB-622 | N10665 |  | 110 (760) | 44 |  | 112 |  | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Smls. pipe \& tube |
| SB-622 | R20033 | . . | 109 (750) | 45 | . . | . . . | . . | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Smls pipe \& tube |
| SB-622 | R30556 |  | 100 (690) | 45 | . . | 111 | . . | $21 \mathrm{Ni}-30 \mathrm{Fe}-22 \mathrm{Cr}-18 \mathrm{Co}-3 \mathrm{Mo}-3 \mathrm{~W}$ | Smls. pipe \& tube |
| SB-622 | N10675 |  | 110 (760) | 44 | . . | 112 | . . | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mo}-\mathrm{W}$ | Smls. pipe \& tube |
| SB-622 | N12160 |  | 90 (620) | 46 | . . . | . . . | . . | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Smls. pipe \& tube |
| B 625 | N08926 | . . . | 94 (650) | . . . | 45 | . . . | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Co}-\mathrm{N}$ | Plate, sheet, \& strip |
| SB-625 | N08031 | . . | 94 (650) | 45 | . . | 111 | . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-625 | N08904 |  | 71 (490) | 45 | . . | 111 | . . | $44 \mathrm{Fe}-25 \mathrm{Ni}-21 \mathrm{Cr}-\mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-625 | N08925 |  | 87 (600) | 45 | . . | 111 | . . | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Plate, sheet, \& strip |
| SB-625 | R20033 |  | 109 (750) | 45 | . . | . . . |  | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Plate, sheet, \& strip |
| SB-626 | N06002 |  | 100 (690) | 43 | . . | 111 |  | $47 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-18 \mathrm{Fe}$ | Welded tube |
| SB-626 | N06007 |  | 90 (620) | 45 | . . | 111 | $\ldots$ | $47 \mathrm{Ni}-22 \mathrm{Cr}-19 \mathrm{Fe}-6 \mathrm{Mo}$ | Welded tube |
| SB-626 | N06022 |  | 100 (690) | 43 | . . | 112 | $\ldots$ | $55 \mathrm{Ni}-21 \mathrm{Cr}-13.5 \mathrm{Mo}$ | Welded tube |
| SB-626 | N06030 |  | 85 (585) | 45 | . . | 111 | . . | $40 \mathrm{Ni}-29 \mathrm{Cr}-15 \mathrm{Fe}-5 \mathrm{Mo}$ | Welded tube |
| SB-626 | N06059 | . . | 100 (690) | 43 | . . | 112 | . . | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}$ | Welded tube |
| SB-626 | N06200 |  | 100 (690) | 43 | . . | 112 |  | $59 \mathrm{Ni}-23 \mathrm{Cr}-16 \mathrm{Mo}-1.6 \mathrm{Cu}$ | Welded tube |
| SB-626 | N06230 |  | 110 (760) | 43 | ... | 111 | $\ldots$ | $53 \mathrm{Ni}-22 \mathrm{Cr}-14 \mathrm{~W}-\mathrm{Co}-\mathrm{Fe}-\mathrm{Mo}$ | Welded tube |
| SB-626 | N06455 | . . | 100 (690) | 43 | . . | 112 | $\ldots$ | $61 \mathrm{Ni}-16 \mathrm{Mo}-16 \mathrm{Cr}$ | Welded tube |
| SB-626 | N06686 | . . | 100 (690) | 43 | . . | 111 | . . | $58 \mathrm{Ni}-21 \mathrm{Cr}-16 \mathrm{Mo}-3.5 \mathrm{~W}$ | Welded tube |
| SB-626 | N06975 | . . | 85 (585) | 45 | $\ldots$ | 111 | . . | $49 \mathrm{Ni}-25 \mathrm{Cr}-18 \mathrm{Fe}-6 \mathrm{Mo}$ | Welded tube |
| SB-626 | N06985 |  | 90 (620) | 45 | $\ldots$ | 111 |  | $47 \mathrm{Ni}-22 \mathrm{Cr}-20 \mathrm{Fe}-7 \mathrm{Mo}$ | Welded tube |
| SB-626 | N08031 | . . | 94 (650) | 45 | . . | 111 | . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-27 \mathrm{Cr}-7 \mathrm{Mo}$ | Welded tube |
| SB-626 | N08320 |  | 75 (515) | 45 | . . . | 111 | . . | $26 \mathrm{Ni}-22 \mathrm{Cr}-5 \mathrm{Mo}-\mathrm{Ti}$ | Welded tube |
| SB-626 | N10001 |  | 100 (690) | 44 | . . | 112 | . . | $62 \mathrm{Ni}-28 \mathrm{Mo}-5 \mathrm{Fe}$ | Welded tube |
| SB-626 | N10276 | . . | 100 (690) | 43 | . . | 112 | . . . | $54 \mathrm{Ni}-16 \mathrm{Mo}-15 \mathrm{Cr}$ | Welded tube |
| SB-626 | N10629 | . $\cdot$ | 110 (760) | 44 | . . | . . . | . $\cdot$ | $66 \mathrm{Ni}-28 \mathrm{Mo}-3 \mathrm{Fe}-1.3 \mathrm{Cr}-0.25 \mathrm{Al}$ | Welded tube |
| SB-626 | N10665 |  | 110 (760) | 44 | . . . | 112 | . . | $65 \mathrm{Ni}-28 \mathrm{Mo}-2 \mathrm{Fe}$ | Welded tube |
| SB-626 | R20033 | . . | 109 (750) | 45 | . . | . . | . . | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Welded tube |
| SB-626 | R30556 | . . | 100 (690) | 45 | . . | 111 | . . | $21 \mathrm{Ni}-30 \mathrm{Fe}-22 \mathrm{Cr}-18 \mathrm{Co}-3 \mathrm{Mo}-3 \mathrm{~W}$ | Welded tube |
| SB-626 | N10675 | . . | 110 (760) | 44 | . . . | 112 | . . . | $65 \mathrm{Ni}-29.5 \mathrm{Mo}-2 \mathrm{Cr}-2 \mathrm{Fe}-\mathrm{Mn}-\mathrm{W}$ | Welded tube |
| SB-626 | N12160 |  | 90 (620) | 46 | . . | . . . | . . | $37 \mathrm{Ni}-30 \mathrm{Co}-28 \mathrm{Cr}-2.7 \mathrm{Si}$ | Welded tube |
| B 649 | N08926 | . . | 94 (650) | . . | 45 | . . | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Bar \& wire |
| SB-649 | N08904 |  | 71 (490) | 45 | . . | 111 | . . | $44 \mathrm{Fe}-25 \mathrm{Ni}-21 \mathrm{Cr}-\mathrm{Mo}$ | Bar \& wire |
| SB-649 | N08925 |  | 87 (600) | 45 |  | 111 | . . | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Bar \& wire |
| SB-649 | R20033 | $\ldots$ | 109 (750) | 45 | . | . . . | . . | $33 \mathrm{Cr}-31 \mathrm{Ni}-32 \mathrm{Fe}-1.5 \mathrm{Mo}-0.6 \mathrm{Cu}-\mathrm{N}$ | Bar \& Wire |



| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNS | Alloy, Type, or | Minimum Specified Tensile, | We |  |  |  |  |  |
| Spec No. | No. | Grade | ksi (MPa) | P-No. | S-No. | P-No. | S-No. | Nominal Composition | Product Form |
| SB-658 | R60702 | R60702 | 55 (380) | 61 | . . | 117 | . . . | 99.2Zr | Smls. \& welded pipe |
| SB-658 | R60705 | R60705 | 80 (550) | 62 |  | 117 | $\ldots$ | 95.5Zr+2.5Cb | Smls. \& welded pipe |
| SB-668 | N08028 |  | 73 (505) | 45 | . . | 111 | $\ldots$ | $31 \mathrm{Ni}-31 \mathrm{Fe}-29 \mathrm{Cr}-\mathrm{Mo}$ | Smls. tube |
| SB-672 | N08700 | . . | 80 (550) | 45 | . . | 111 | $\ldots$ | $25 \mathrm{Ni}-47 \mathrm{Fe}-21 \mathrm{Cr}-5 \mathrm{Mo}$ | Bar \& wire |
| B 673 | N08926 | $\ldots$ | 94 (650) | . . | 45 | $\ldots$ | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded pipe |
| SB-673 | N08904 | . . | 71 (490) | 45 | . . | 111 | . . | $44 \mathrm{Fe}-25 \mathrm{Ni}-21 \mathrm{Cr}-\mathrm{Mo}$ | Welded pipe |
| SB-673 | N08925 | . . | 87 (600) | 45 | $\ldots$ | 111 | $\ldots$ | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded pipe |
| SB-674 | N08904 | . . | 71 (490) | 45 | . . | 111 | . . | $44 \mathrm{Fe}-25 \mathrm{Ni}-21 \mathrm{Cr}-\mathrm{Mo}$ | Welded tube |
| SB-674 | N08925 | . . | 87 (600) | 45 | $\ldots$ | 111 | $\ldots$ | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded tube |
| B 674 | N08926 | . . | 94 (650) | . . | 45 |  | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded tube |
| SB-675 | N08367 | . . | 95 (655) | 45 | $\ldots$ | 111 | . . | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded pipe |
| SB-676 | N08367 | $\ldots$ | 100 (690) | 45 | . . | 111 | . $\cdot$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Welded tube |
| B 677 | N08926 | . . | 94 (650) | . . | 45 | . . | 111 | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. pipe \& tube |
| SB-677 | N08904 | . . | 71 (490) | 45 | . . | 111 | . . | $44 \mathrm{Fe}-25 \mathrm{Ni}-21 \mathrm{Cr}-\mathrm{Mo}$ | Smls. pipe \& tube |
| SB-677 | N08925 | $\ldots$ | 87 (600) | 45 | . . | 111 | . . | $25 \mathrm{Ni}-20 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. pipe \& tube |
| SB-688 | N08367 | . . . | 104 (715) | 45 | . . | 111 | $\ldots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Plate, sheet, \& strip $<^{3} 16 \mathrm{in}$. ( 4.8 mm ) |
| SB-688 | N08367 | . $\cdot$ | 100 (690) | 45 | . $\cdot$ | . . . | . $\cdot$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Plate, sheet, \& strip $\geq 3 / 16$ in. $\leq 3 / 4$ in. ( $\geq 4.8 \mathrm{~mm} \leq 19 \mathrm{~mm}$ ) |
| SB-688 | N08367 | . . | 95 (655) | 45 | . . . | $\cdots$ | $\ldots$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Plate, sheet, \& strip $>3 / 4 \mathrm{in}$. (19 mm) |
| SB-690 | N08367 | . $\cdot$. | 104 (715) | 45 | . . | 111 | . $\cdot$ | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Smls. pipe \& tube |
| SB-691 | N08367 | . $\cdot$. | 95 (655) | 45 | . . | 111 | . $\cdot$. | $46 \mathrm{Fe}-24 \mathrm{Ni}-21 \mathrm{Cr}-6 \mathrm{Mo}-\mathrm{Cu}-\mathrm{N}$ | Rod, bar, \& wire |
| SB-704 | N06625 | . . . | 120 (825) | 43 | . . . | 111 | . . . | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Welded tube |
| SB-704 | N08825 | . . | 85 (585) | 45 | . . . | 111 | . . | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Welded tube |
| SB-705 | N06625 | . . . | 120 (825) | 43 | . $\cdot$ | 111 | . $\cdot$ | $60 \mathrm{Ni}-22 \mathrm{Cr}-9 \mathrm{Mo}-3.5 \mathrm{Cb}$ | Welded pipe |
| SB-705 | N08825 | . . | 85 (585) | 45 | . . | 111 | . . | $42 \mathrm{Ni}-21.5 \mathrm{Cr}-3 \mathrm{Mo}-2.3 \mathrm{Cu}$ | Welded pipe |
| SB-709 | N08028 | . $\cdot$. | 73 (505) | 45 | . . . | 111 | . . | $31 \mathrm{Ni}-31 \mathrm{Fe}-29 \mathrm{Cr}-\mathrm{Mo}$ | Plate, sheet, \& strip |
| SB-710 | N08330 | . . | 70 (485) | 46 | . . . | 111 | . | $35 \mathrm{Ni}-19 \mathrm{Cr}-1.25 \mathrm{Si}$ | Welded pipe |
| SB-729 | N08020 | . . . | 80 (550) | 45 | . . | . . . | 111 | $35 \mathrm{Ni}-35 \mathrm{Fe}-20 \mathrm{Cr}-\mathrm{Cb}$ | Smls. pipe \& tube |
| B 725 | N02200 | . $\cdot$ | 55 (380) | . . | 41 | . . | 110 | 99.0 Ni | Welded pipe |
| SB-815 | R31233 | . . | 120 (825) | 49 | . . | . . | . . | $\mathrm{Co}-26 \mathrm{Cr}-9 \mathrm{Ni}-5 \mathrm{Mo}-3 \mathrm{Fe}-2 \mathrm{~W}$ | Rod |
| SB-818 | R31233 |  | 120 (825) | 49 | . $\cdot$ | $\cdots$ | -. | $\mathrm{Co}-26 \mathrm{Cr}-9 \mathrm{Ni}-5 \mathrm{Mo}-3 \mathrm{Fe}-2 \mathrm{~W}$ | Plate, sheet, \& strip |
| B 819 | C12200 | C12200 | 30 (205) | $\cdots$ | . . | . . | 107 | 99.9Cu-P | Wrought pipe |
| SB-861 | R50250 | 1 | 35 (240) | 51 | . . | 115 | . . | Ti | Smls. pipe |
| SB-861 | R50400 | 2 | 50 (345) | 51 | . . | 115 | . . . | Ti | Smls. pipe |
| SB-861 | R50550 | 3 | 65 (450) | 52 | - | 115 | $\ldots$ | Ti | Smls. pipe |

WELDING DATA
QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D)

| Nonferrous (CONT'D) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spec No. | UNS No. | Alloy, Type, or Grade | Minimum Specified Tensile, ksi (MPa) | Welding |  | Brazing |  | Nominal Composition | Product Form |
|  |  |  |  | P-No. | S-No. | P-No. | S-No. |  |  |
| SB-861 | R52400 | 7 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Pd | Smls. pipe |
| SB-861 | R52404 | 26 | 50 (345) | 51 | $\ldots$ | 115 | . . | Ti-Ru | Smls. pipe |
| SB-861 | R53400 | 12 | 70 (485) | 52 | $\ldots$ | 115 | $\ldots$ | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Smls. pipe |
| SB-861 | R56320 | 9 | 90 (620) | 53 | . . | 115 | $\ldots$ | Ti-3AI-2.5V | Smls. pipe |
| SB-862 | R50250 | 1 | 35 (240) | 51 | . . | 115 | . . | Ti | Welded pipe |
| SB-862 | R50400 | 2 | 50 (345) | 51 | . . | 115 | . . | Ti | Welded pipe |
| SB-862 | R50550 | 3 | 65 (450) | 52 | . . | 115 | $\ldots$ | Ti | Welded pipe |
| SB-862 | R52400 | 7 | 50 (345) | 51 | . . | 115 | . . | Ti-Pd | Welded pipe |
| SB-862 | R52404 | 26 | 50 (345) | 51 | . . | 115 | $\ldots$ | Ti-Ru | Welded pipe |
| SB-862 | R53400 | 12 | 70 (485) | 52 | . . | 115 | $\ldots$ | $\mathrm{Ti}-0.3 \mathrm{Mo}-0.8 \mathrm{Ni}$ | Welded pipe |
| SB-862 | R56320 | 9 | 90 (620) | 53 | $\ldots$ | 115 | $\ldots$ | Ti-3AI-2.5V | Welded pipe |
| B 16.18 | C83600 | . . | 40 (275) | . . | . . | . . | 107 | $5 \mathrm{Sn}-5 \mathrm{Zn}-5 \mathrm{~Pb}$ | Cast fittings |
| B 16.18 | C83800 | . . | 40 (275) | . . | . . | . . | 107 | $4 \mathrm{Sn}-6.5 \mathrm{Zn}-6 \mathrm{~Pb}$ | Cast fittings |
| B 16.18 | C84400 | . $\cdot$. | 40 (275) | . . | . . | . . | 107 | $2.5 \mathrm{Sn}-8.5 \mathrm{Zn}-7 \mathrm{~Pb}$ | Cast fittings |
| B 16.22 | C10200 |  | 30 (205) | . . | . . | . . | 107 | 99.95Cu-P | Wrought pipe fittings |
| B 16.22 | C12000 | . . . | 30 (205) | . . | . . | . . | 107 | 99.9Cu-P | Wrought pipe fittings |
| B 16.22 | C12200 | . . | 30 (205) | . . | . . | . . | 107 | 99.9Cu-P | Wrought pipe fittings |
| B 16.22 | C23000 | . . | 30 (205) | . . | . . | . . | 107 | $85 \mathrm{Cu}-15 \mathrm{Zn}$ | Wrought pipe fittings |

## QW-423 Alternate Base Materials for Welder Qualification

QW-423.1 Base metal used for welder qualification may be substituted for the metal specified in the WPS in accordance with the following table. When a base metal shown in the left column is used for welder qualification, the welder is qualified to weld all combinations of base metals shown in the right column, including unassigned metals of similar chemical composition to these metals.

| Base Metals for Welder Qualification | Qualified Production Base Metals |
| :---: | :---: |
| P- or S-No. 1 through P- or SNo. 11, P- or S-No. 34, and P - or S-No. 41 through P - or S-No. 49 | P- or S-No. 1 through P- or SNo. 11, P- or S-No. 34, and P- or S-No. 41 through P- or S-No. 49 |
| P- or S-No. 21 through P- or S- <br> No. 25 | P- or S-No. 21 through P- or SNo. 25 |
| P- or S-No. 51 through P - or S-No. 53 or P- or S-No. 61 through P- or S-No. 62 | P- or S-No. 51 through P- or SNo. 53 and P- or S-No. 61 through P- or S-No. 62 |

QW-423.2 Metals used for welder qualification conforming to national or international standards or specifications may be considered as having the same P - or S-Number as an assigned metal provided it meets the mechanical and chemical requirements of the assigned metal. The base metal specification and corresponding P- or S-Number shall be recorded on the qualification record.

## QW-424 Base Metals Used for Procedure Qualification

04 QW-424.1 Base metals are assigned P- or S-Numbers in table QW/QB-422; metals that do not appear in table QW/QB-422 are considered to be unassigned metals except as otherwise defined in QW-420.1 for base metals having the same UNS numbers. Unassigned metals shall be identified in the WPS and on the PQR by specification, type and grade, or by chemical analysis and mechanical properties. The minimum tensile strength shall be defined by the organization that specified the unassigned metal if the tensile strength of that metal is not defined by the material specification.

Base Metal(s) Used for
Procedure Qualification Coupon
One metal from a P-Number to any metal from the same P Number
One metal from a P-Number to any metal from any other P Number

One metal from P-No. 3 to any metal from P-No. 3

One metal from P-No. 4 to any metal from P-No. 4

One metal from P-No. 5A to any metal from P-No. 5A

One metal from P-No. 5A to a metal from P-No. 4, or P-No. 3 , or P-No. 1
One metal from P-No. 4 to a metal from P-No. 3 or P-No. 1

Any unassigned metal to the same unassigned metal
Any unassigned metal to any PNumber metal

Any unassigned metal to any other unassigned metal
$\frac{\text { Base Metals Qualified }}{\text { Any metals assigned that P-or S- }}$ Number

Any metal assigned the first Por S-Number to any metal assigned the second P - or S Number
Any P- or S-No. 3 metal to any metal assigned P - or S-No. 3 or 1
Any P- or S-No. 4 metal to any metal assigned P - or S-No. 4, 3 , or 1
Any P- or S-No. 5A metal to any metal assigned P - or $\mathrm{S}-\mathrm{No}$. $5 \mathrm{~A}, 4,3$, or 1
Any P- or S-No. 5A metal to any metal assigned to P - or S-No. 4,3 , or 1
Any P- or S-No. 4 metal to any metal assigned to P - or S-No. 3 or 1
The unassigned metal to itself
The unassigned metal to any metal assigned to the same P or S-Number as the qualified metal
The first unassigned metal to the second unassigned metal

## QW-430 F-NUMBERS QW-431 General

The following F-Number grouping of electrodes and welding rods in table QW-432 is based essentially on their usability characteristics, which fundamentally determine the ability of welders to make satisfactory welds with a given filler metal. This grouping is made to reduce the number of welding procedure and performance qualifications, where this can logically be done. The grouping does not imply that base metals or filler metals within a group may be indiscriminately substituted for a metal that was used in the qualification test without consideration of the compatibility of the base and filler metals from the standpoint of metallurgical properties, postweld heat treatment design and service requirements, and mechanical properties.

QW-432.1
Steel and Steel Alloys
QW-432.2 Aluminum and Aluminum-Base Alloys
QW-432.3 Copper and Copper-Base Alloys
QW-432.4 Nickel and Nickel-Base Alloys
QW-432.5 Titanium and Titanium Alloys
QW-432.6 Zirconium and Zirconium Alloys QW-432.7 Hard-Facing Weld Metal Overlay

## WELDING DATA

QW-432
F-NUMBERS
Grouping of Electrodes and Welding Rods for Qualification

|  | F-No. | ASME Specification | AWS Classification |
| :--- | :--- | :--- | :--- | UNS No.

## Steel and Steel Alloys

| 1 | SFA-5.1 | EXX20 | ... |
| :---: | :---: | :---: | :---: |
| 1 | SFA-5.1 | EXX22 | ... |
| 1 | SFA-5.1 | EXX24 | $\ldots$ |
| 1 | SFA-5.1 | EXX27 | $\ldots$ |
| 1 | SFA-5.1 | EXX28 | $\ldots$ |
| 1 | SFA-5.4 | EXXX(X)-25 | $\ldots$ |
| 1 | SFA-5.4 | EXXX(X)-26 |  |
| 1 | SFA-5.5 | EXX20-X | $\ldots$ |
| 1 | SFA-5.5 | EXX27-X | $\ldots$ |
| 2 | SFA-5.1 | EXX12 | $\ldots$ |
| 2 | SFA-5.1 | EXX13 | $\ldots$ |
| 2 | SFA-5.1 | EXX14 | $\ldots$ |
| 2 | SFA-5.1 | EXX19 | . . . |
| 2 | SFA-5.5 | E(X)XX13-X | $\ldots$ |
| 3 | SFA-5.1 | EXX10 | $\ldots$ |
| 3 | SFA-5.1 | EXX11 | $\ldots$ |
| 3 | SFA-5.5 | E(X)XX10-X | $\ldots$ |
| 3 | SFA-5.5 | E(X)XX11-X | $\ldots$ |
| 4 | SFA-5.1 | EXX15 | $\ldots$ |
| 4 | SFA-5.1 | EXX16 | $\ldots$ |
| 4 | SFA-5.1 | EXX18 | $\ldots$ |
| 4 | SFA-5.1 | EXX18M | $\ldots$ |
| 4 | SFA-5.1 | EXX48 | ... |
| 4 | SFA-5.4 other than austenitic and duplex | EXXX(X)-15 | $\ldots$ |
| 4 | SFA-5.4 other than austenitic and duplex | EXXX(X)-16 | ... |
| 4 | SFA-5.4 other than austenitic and duplex | EXXX ${ }^{\text {( }}$ )-17 | $\ldots$ |
| 4 | SFA-5.5 | $E(X) X \times 15-X$ | $\ldots$ |
| 4 | SFA-5.5 | $E(X) X X 16-X$ | $\ldots$ |
| 4 | SFA-5.5 | $E(X) X \times 18-X$ | $\ldots$ |
| 4 | SFA-5.5 | $E(X) X \times 18 \mathrm{M}$ | $\ldots$ |
| 4 | SFA-5.5 | $\mathrm{E}(\mathrm{X}) \mathrm{XX18} 181$ | . . |
| 5 | SFA-5.4 austenitic and duplex | EXXX (X)-15 | . . . |
| 5 | SFA-5.4 austenitic and duplex | EXXX(X)-16 | $\ldots$ |
| 5 | SFA-5.4 austenitic and duplex | EXXX $(\mathrm{X})-17$ | $\ldots$ |
| 6 | SFA-5.2 | All classifications | . . |
| 6 | SFA-5.9 | All classifications | $\ldots$ |
| 6 | SFA-5.17 | All classifications | . . . |
| 6 | SFA-5.18 | All classifications | $\ldots$ |
| 6 | SFA-5.20 | All classifications | $\ldots$ |
| 6 | SFA-5.22 | All classifications | $\ldots$ |
| 6 | SFA-5.23 | All classifications | $\ldots$ |
| 6 | SFA-5.25 | All classifications | $\ldots$ |
| 6 | SFA-5.26 | All classifications | . . . |
| 6 | SFA-5.28 | All classifications | $\ldots$ |
| 6 | SFA-5.29 | All classifications | $\ldots$ |
| 6 | SFA-5.30 | INMs-X | $\ldots$ |
| 6 | SFA-5.30 | IN5XX | $\ldots$ |
| 6 | SFA-5.30 | IN3XX(X) | $\ldots$ |

## 2004 SECTION IX

QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification

| F-No. | ASME Specification | AWS Classification | UNS No. |
| :---: | :---: | :---: | :---: |
| Aluminum and Aluminum Alloys |  |  |  |
| 21 | SFA-5.3 | El100 | A91100 |
| 21 | SFA-5.3 | E3003 | A93003 |
| 21 | SFA-5.10 | ER1100 | A91100 |
| 21 | SFA-5.10 | ER1188 | A91188 |
| 21 | SFA-5.10 | R1100 | A91100 |
| 21 | SFA-5.10 | R1188 | A91188 |
| 22 | SFA-5.10 | ER5183 | A95183 |
| 22 | SFA-5.10 | ER5356 | A95356 |
| 22 | SFA-5.10 | ER5554 | A95554 |
| 22 | SFA-5.10 | ER5556 | A95556 |
| 22 | SFA-5.10 | ER5654 | A95654 |
| 22 | SFA-5.10 | R5183 | A95183 |
| 22 | SFA-5.10 | R5356 | A95356 |
| 22 | SFA-5.10 | R5554 | A95554 |
| 22 | SFA-5.10 | R5556 | A95556 |
| 22 | SFA-5.10 | R5654 | A95654 |
| 23 | SFA-5.3 | E4043 | A94043 |
| 23 | SFA-5.10 | ER4009 | A94009 |
| 23 | SFA-5.10 | ER4010 | A94010 |
| 23 | SFA-5.10 | ER4043 | A94043 |
| 23 | SFA-5.10 | ER4047 | A94047 |
| 23 | SFA-5.10 | ER4145 | A94145 |
| 23 | SFA-5.10 | ER4643 | A94643 |
| 23 | SFA-5.10 | R4009 | A94009 |
| 23 | SFA-5.10 | R4010 | A94010 |
| 23 | SFA-5.10 | R4011 | A94011 |
| 23 | SFA-5.10 | R4043 | A94043 |
| 23 | SFA-5.10 | R4047 | A94047 |
| 23 | SFA-5.10 | R4145 | A94145 |
| 23 | SFA-5.10 | R4643 | A94643 |
| 24 | SFA-5.10 | R-A356.0 | A13560 |
| 24 | SFA-5.10 | R-A357.0 | A13570 |
| 24 | SFA-5.10 | R-C355.0 | A33550 |
| 24 | SFA-5.10 | R206.0 | A02060 |
| 24 | SFA-5.10 | R357.0 | A03570 |
| 25 | SFA-5.10 | ER2319 | A92319 |
| 25 | SFA-5.10 | R2319 | A92319 |
|  |  |  |  |
| 31 | SFA-5.6 | ECu | W60189 |
| 31 | SFA-5.7 | ERCu | C18980 |
| 32 | SFA-5.6 | ECuSi | W60656 |
| 32 | SFA-5.7 | ERCuSi-A | C65600 |
| 33 | SFA-5.6 | ECuSn-A | W60518 |
| 33 | SFA-5.6 | ECuSn-C | W60521 |
| 33 | SFA-5.7 | ERCuSn-A | WC51800 |
| 34 | SFA-5.6 | ECuNi | W60715 |
| 34 | SFA-5.7 | ERCuNi | C71580 |
| 34 | SFA-5.30 | IN67 | C71581 |
| 35 | SFA-5.8 | RBCuZn-A | C47000 |
| 35 | SFA-5.8 | RBCuZn-B | C68000 |
| 35 | SFA-5.8 | RBCuZn-C | C68100 |
| 35 | SFA-5.8 | RBCuZn-D | C77300 |
| 36 | SFA-5.6 | ECuAI-A2 | W60614 |
| 36 | SFA-5.6 | ECuAI-B | W60619 |
| 36 | SFA-5.7 | ERCuAI-A1 | C61000 |

## WELDING DATA

QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification

| F-No. | ASME Specification | AWS Classification | UNS No. |
| :--- | :--- | :--- | :--- |

Copper and Copper Alloys (CONT'D)

| 36 | SFA-5.7 | ERCuAI-A2 | C61800 |
| :--- | :--- | :--- | :--- |
| 36 | SFA-5.7 | ERCuAI-A3 | C62400 |
| 37 | SFA-5.6 | ECuMnNiAI | C60633 |
| 37 | SFA-5.6 | ECuNiAI | C60632 |
| 37 | SFA-5.7 | ERCuMnNiAI | C63380 |
| 37 | SFA-5.7 | ERCuNiAI | C63280 |

Nickel and Nickel Alloys
SFA-5.11
SFA-5.14

| ENi-1 | W82141 |
| :--- | :---: |
| ERNi-1 | N02061 |
| IN61 | N02061 |
| ENiCu-7 | W84190 |
| ERNiCu-7 | N04060 |
| ERNiCu-8 | N05504 |
| IN60 | W04060 |
| ENiCrCoMo-1 | W86117 |
| ENiCrFe-1 | W86132 |
| ENiCrFe-2 | W86183 |
| ENiCrFe-3 | W86134 |
| ENiCrFe-4 | W86152 |
| ENirFe-7 | W86094 |
| ENirrFe-9 | W86095 |
| ENiCrFe-10 | W86002 |
| ENiCrMo-2 | W86112 |
| ENiCrMo-3 | W80276 |
| ENiCrMo-4 | W80002 |
| ENiCrMo-5 | W86620 |
| ENiCrMo-6 | W86455 |
| ENiCrMo-7 | W86022 |
| ENiCrMo-10 | W86032 |
| ENiCrMo-12 | W86059 |
| ENiCrMo-13 | W86026 |
| ENiCrMo-14 | N06082 |
| ERNiCr-3 | N06072 |
| ERNiCr-4 | N06076 |
| ERNiCr-6 | N06617 |
| ERNiCrCoMo-1 | N06062 |
| ERNiCrFe-5 | N07092 |
| ERNiCrFe-6 | N06052 |
| ERNiCrFe-7 | N07069 |
| ERNiCrFe-8 | N06601 |
| ERNiCrFe-11 | N06002 |
| ERNiCrMo-2 | N06625 |
| ERNiCrMo-3 | N10276 |
| ERNiCrMo-4 | N06455 |
| ERNiCrMo-7 | N06022 |
| ERNiCrMo-10 | N06059 |
| ERNiCrMo-13 | N06686 |
| ERNiCrMo-14 | N06231 |
| ERNiCrWMo-1 | N06052 |
| IN52 | N06062 |
| IN62 | No7092 |
| IN6A |  |
| IN82 |  |
| ENiMo-1 |  |
|  |  |

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QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification


## WELDING DATA

QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification

| F-No. | ASME Specification | AWS Classification | UNS No. |
| :--- | :--- | :--- | :--- |

Hard-Facing Weld Metal Overlay (CONT'D)

| 71 | SFA-5.13 | ECuSi | W60656 |
| :---: | :---: | :---: | :---: |
| 71 | SFA-5.13 | ECuSn-A | W60518 |
| 71 | SFA-5.13 | ECuSn-C | W60521 |
| 71 | SFA-5.13 | EFel | W74001 |
| 71 | SFA-5.13 | EFe2 | W74002 |
| 71 | SFA-5.13 | EFe3 | W74003 |
| 71 | SFA-5.13 | EFe4 | W74004 |
| 71 | SFA-5.13 | EFe5 | W75110 |
| 71 | SFA-5.13 | EFe6 | W77510 |
| 71 | SFA-5.13 | EFe7 | W77610 |
| 71 | SFA-5.13 | EFeCr-AlA | W74011 |
| 71 | SFA-5.13 | EFeCr-A2 | W74012 |
| 71 | SFA-5.13 | EFeCr-A3 | W74013 |
| 71 | SFA-5.13 | EFeCr-A4 | W74014 |
| 71 | SFA-5.13 | EFeCr-A5 | W74015 |
| 71 | SFA-5.13 | EFeCr-A6 | W74016 |
| 71 | SFA-5.13 | EFeCr-A7 | W74017 |
| 71 | SFA-5.13 | EFeCr-A8 | W74018 |
| 71 | SFA-5.13 | EFeCr-El | W74211 |
| 71 | SFA-5.13 | EFeCr-E2 | W74212 |
| 71 | SFA-5.13 | EFeCr-E3 | W74213 |
| 71 | SFA-5.13 | EFeCr-E4 | W74214 |
| 71 | SFA-5.13 | EFeMn-A | W79110 |
| 71 | SFA-5.13 | EFeMn-B | W79310 |
| 71 | SFA-5.13 | EFeMn-C | W79210 |
| 71 | SFA-5.13 | EFeMn-D | W79410 |
| 71 | SFA-5.13 | EFeMn-E | W79510 |
| 71 | SFA-5.13 | EFeMn-F | W79610 |
| 71 | SFA-5.13 | EFeMnCr | W79710 |
| 71 | SFA-5.13 | ENiCr-C | W89606 |
| 71 | SFA-5.13 | ENiCrFeCo | W83002 |
| 71 | SFA-5.13 | ENiCrMo-5A | W80002 |
| 71 | SFA-5.13 | EWCX-12/30 | . . . |
| 71 | SFA-5.13 | EWCX-20/30 | . . . |
| 71 | SFA-5.13 | EWCX-30/40 | ... |
| 71 | SFA-5.13 | EWCX-40 | . . |
| 71 | SFA-5.13 | EWCX-40/120 |  |
| 72 | SFA-5.21 | ERCCoCr-A | W73036 |
| 72 | SFA-5.21 | ERCCOCr-B | W73042 |
| 72 | SFA-5.21 | ERCCOCr-C | W73031 |
| 72 | SFA-5.21 | ERCCOCr-E | W73041 |
| 72 | SFA-5.21 | ERCCOCr-G | W73032 |
| 72 | SFA-5.21 | ERCCuAI-A2 | W60618 |
| 72 | SFA-5.21 | ERCCUAI-A3 | W60624 |
| 72 | SFA-5.21 | ERCCuAI-C | W60626 |
| 72 | SFA-5.21 | ERCCUAI-D | W61626 |
| 72 | SFA-5.21 | ERCCUAI-E | W62626 |
| 72 | SFA-5.21 | ERCCuSi-A | W60657 |
| 72 | SFA-5.21 | ERCCuSn-A | W60518 |
| 72 | SFA-5.21 | ERCCuSn-D | W60524 |
| 72 | SFA-5.21 | ERCFe-1 | W74030 |
| 72 | SFA-5.21 | ERCFe-1A | W74031 |
| 72 | SFA-5.21 | ERCFe-2 | W74032 |
| 72 | SFA-5.21 | ERCFe-3 | W74033 |
| 72 | SFA-5.21 | ERCFe-5 | W74035 |

## 2004 SECTION IX

QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification

| F-No. | ASME Specification | AWS Classification | UNS No. |
| :---: | :---: | :---: | :---: |

Hard-Facing Weld Metal Overlay (CONT'D)

| 72 | SFA-5.21 | ERCFe-6 | W77530 |
| :---: | :---: | :---: | :---: |
| 72 | SFA-5.21 | ERCFe-8 | W77538 |
| 72 | SFA-5.21 | ERCFeCr-A | W74531 |
| 72 | SFA-5.21 | ERCFeCr-AlA | W74530 |
| 72 | SFA-5.21 | ERCFeCr-A3A | W74533 |
| 72 | SFA-5.21 | ERCFeCr-A4 | W74534 |
| 72 | SFA-5.21 | ERCFeCr-A5 | W74535 |
| 72 | SFA-5.21 | ERCFeCr-A9 | W74539 |
| 72 | SFA-5.21 | ERCFeCr-Al0 | W74540 |
| 72 | SFA-5.21 | ERCFeMn-C | W79230 |
| 72 | SFA-5.21 | ERCFeMn-F | W79630 |
| 72 | SFA-5.21 | ERCFeMn-G | W79231 |
| 72 | SFA-5.21 | ERCFeMn- ${ }^{\text {d }}$ | W79232 |
| 72 | SFA-5.21 | ERCFeMnCr | W79730 |
| 72 | SFA-5.21 | ERCNiCr-A | W89634 |
| 72 | SFA-5.21 | ERCNiCr-B | W89635 |
| 72 | SFA-5.21 | ERCNiCr-C | W89636 |
| 72 | SFA-5.21 | ERCNiCrFeCo | W83032 |
| 72 | SFA-5.21 | ERCNiCrMo-5A | W80036 |
| 72 | SFA-5.21 | ERCOCr-A | R30006 |
| 72 | SFA-5.21 | ERCOCr-B | R30012 |
| 72 | SFA-5.21 | ERCOCr-C | R30001 |
| 72 | SFA-5.21 | ERCoCr-E | R30021 |
| 72 | SFA-5.21 | ERCOCr-F | R30002 |
| 72 | SFA-5.21 | ERCoCr-G | R30014 |
| 72 | SFA-5.21 | ERCuAI-A2 | C61800 |
| 72 | SFA-5.21 | ERCuAI-A3 | C62400 |
| 72 | SFA-5.21 | ERCuAI-C | C62580 |
| 72 | SFA-5.21 | ERCuAI-D | C62581 |
| 72 | SFA-5.21 | ERCuAI-E | C62582 |
| 72 | SFA-5.21 | ERCuSi-A | C65600 |
| 72 | SFA-5.21 | ERCuSn-A | C51800 |
| 72 | SFA-5.21 | ERCuSn-D | C52400 |
| 72 | SFA-5.21 | ERFe-1 | T74000 |
| 72 | SFA-5.21 | ERFe-1A | T74001 |
| 72 | SFA-5.21 | ERFe-2 | T74002 |
| 72 | SFA-5.21 | ERFe-3 | T74003 |
| 72 | SFA-5.21 | ERFe-5 | T74005 |
| 72 | SFA-5.21 | ERFe-6 | T74006 |
| 72 | SFA-5.21 | ERFe-8 | T74008 |
| 72 | SFA-5.21 | ERFeCr-A | . . . |
| 72 | SFA-5.21 | ERFeCr-AlA | ... |
| 72 | SFA-5.21 | ERFeCr-A3A | . . . |
| 72 | SFA-5.21 | ERFeCr-A4 | . . |
| 72 | SFA-5.21 | ERFeCr-A5 | . . |
| 72 | SFA-5.21 | ERFeCr-A9 | ... |
| 72 | SFA-5.21 | ERFeCr-Al0 | . . . |
| 72 | SFA-5.21 | ERFeMn-C | $\ldots$ |
| 72 | SFA-5.21 | ERFeMn-F | . . |
| 72 | SFA-5.21 | ERFeMn-G | . . . |
| 72 | SFA-5.21 | ERFeMn-H | ... |
| 72 | SFA-5.21 | ERFeMnCr | ... |
| 72 | SFA-5.21 | ERNiCr-A | N99644 |
| 72 | SFA-5.21 | ERNiCr-B | N99645 |
| 72 | SFA-5.21 | ERNiCr-C | N99646 |

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## WELDING DATA

QW-432
F-NUMBERS (CONT'D)
Grouping of Electrodes and Welding Rods for Qualification

| F-No. | ASME Specification | AWS Classification | UNS No. |
| :---: | :---: | :---: | :---: |
|  |  | Hard-Facing Weld Metal Overlay (CONT'D) |  |
| 7 |  | ERNiCr-D |  |
| 72 | SFA-5.21 | ERNiCr-E | N99647 |
| 72 | SFA-5.21 | ERNiCrFeCo | N99648 |
| 72 | SFA-5.21 | ERNiCrMo-5A | F46100 |
| 72 | SFA-5.21 | ERWCX-20/30 | N10006 |
| 72 | SFA-5.21 | ERWCX-30/40 | $\ldots$ |
| 72 | SFA-5.21 | ERWCX-40 | $\ldots$ |
| 72 | SFA-5.21 | ERWCX-40/120 | $\ldots$ |
| 72 | SFA-5.21 | RWCX-20/30 | $\ldots$ |
|  | RFA-5.21 | RWCX-30/40 | $\ldots$ |

## Alternate F-Numbers for Welder Performance Qualification

The following tables identify the filler metal or electrode that the welder used during qualification testing as
"Qualified With," and the electrodes or filler metals that the welder is qualified to use in production welding as "Qualified For." See table QW-432 for the F-Number assignments.

| Qualified With $\rightarrow$ Qualified For $\downarrow$ | F-No. 1 <br> With Backing | F-No. 1 <br> Without Backing | F-No. 2 <br> With <br> Backing | F-No. 2 <br> Without Backing | F-No. 3 <br> With Backing | F-No. 3 <br> Without <br> Backing | F-No. 4 <br> With Backing | F-No. 4 <br> Without Backing | F-No. 5 <br> With Backing | F-No. 5 Without Backing |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F-No. 1 With Backing | X | X | X | X | X | X | X | X | X | X |
| F-No. 1 Without Backing |  | X |  |  |  |  |  |  |  |  |
| F-No. 2 With Backing |  |  | X | X | X | X | X | X |  |  |
| F-No. 2 Without Backing |  |  |  | X |  |  |  |  |  |  |
| F-No. 3 With Backing |  |  |  |  | X | X | X | X |  |  |
| F-No. 3 Without Backing |  |  |  |  |  | X |  |  |  |  |
| F-No. 4 With Backing |  |  |  |  |  |  | X | X |  |  |
| F-No. 4 Without Backing |  |  |  |  |  |  |  | X |  |  |
| F-No. 5 With Backing |  |  |  |  |  |  |  |  | X | X |
| F-No. 5 Without Backing |  |  |  |  |  |  |  |  |  | X |


| Qualified With | Qualified For |
| :---: | :---: |
| Any F-No. 6 | All F-No. 6 [Note (1)] |
| Any F-No. 21 through F-No. 25 | All F-No. 21 through F-No. 25 |
| Any F-No. 31, F-No. 32, F-No. 33, F-No. 35, F-No. 36, or FNo. 37 | Only the same F-Number as was used during the qualification test |
| F-No. 34 or any F-No. 41 through F-No. 45 | F-No. 34 and all F-No. 41 through F-No. 45 |
| Any F-No. 51 through F-No. 55 | All F-No. 51 through F-No. 55 |
| Any F-No. 61 | All F-No. 61 |
| Any F-No. 71 through F-No. 72 | Only the same F-Number as was used during the qualification test |

NOTE:
(1) Deposited weld metal made using a bare rod not covered by an SFA Specification but which conforms to an analysis listed in QW442 shall be considered to be classified as F-No. 6.

## QW-440 WELD METAL CHEMICAL

 COMPOSITION
## QW-441 General

Identification of weld metal chemical composition designated on the PQR and WPS shall be as given in QW-404.5.

QW-442
A-NUMBERS
Classification of Ferrous Weld Metal Analysis for Procedure Qualification

| A-No. | Types of Weld Deposit | Analysis, \% [Note (1)] |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | C | Cr | Mo | Ni | Mn | Si |
| 1 | Mild Steel | 0.20 |  | . . | . . | 1.60 | 1.00 |
| 2 | Carbon-Molybdenum | 0.15 | 0.50 | 0.40-0.65 | . . | 1.60 | 1.00 |
| 3 | Chrome (0.4\% to 2\%)-Molybdenum | 0.15 | 0.40-2.00 | 0.40-0.65 |  | 1.60 | 1.00 |
| 4 | Chrome (2\% to 6\%)-Molybdenum | 0.15 | 2.00-6.00 | 0.40-1.50 |  | 1.60 | 2.00 |
| 5 | Chrome (6\% to 10.5\%)-Molybdenum | 0.15 | 6.00-10.50 | 0.40-1.50 | . . | 1.20 | 2.00 |
| 6 | Chrome-Martensitic | 0.15 | 11.00-15.00 | 0.70 | . . | 2.00 | 1.00 |
| 7 | Chrome-Ferritic | 0.15 | 11.00-30.00 | 1.00 | . . | 1.00 | 3.00 |
| 8 | Chromium-Nickel | 0.15 | 14.50-30.00 | 4.00 | 7.50-15.00 | 2.50 | 1.00 |
| 9 | Chromium-Nickel | 0.30 | 19.00-30.00 | 6.00 | 15.00-37.00 | 2.50 | 1.00 |
| 10 | Nickel to 4\% | 0.15 | . . | 0.55 | 0.80-4.00 | 1.70 | 1.00 |
| 11 | Manganese-Molybdenum | 0.17 | $\ldots$ | 0.25-0.75 | 0.85 | 1.25-2.25 | 1.00 |
| 12 | Nickel-Chrome-Molybdenum | 0.15 | 1.50 | 0.25-0.80 | 1.25-2.80 | 0.75-2.25 | 1.00 |

NOTE:
(1) Single values shown above are maximum.

2004 SECTION IX
QW-451.1
QW-450 SPECIMENS
QW-451 Procedure Qualification Thickness Limits and Test Specimens
GROOVE-WELD TENSION TESTS AND TRANSVERSE-BEND TESTS

| Thickness $T$ of Test Coupon, Welded, in. (mm) | Range of Thickness $T$ of Base Metal, Qualified, in. (mm) <br> [Notes (1) and (2)] |  | Maximum Thickness $t$ of Deposited Weld Metal, Qualified, in. (mm) <br> [Notes (1) and (2)] | Type and Number of Tests Required (Tension and Guided-Bend Tests) [Note (2)] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension, | Side <br> Bend, | Face <br> Bend, | Root <br> Bend, |
|  | Min. | Max. |  | QW-150 | QW-160 | QW-160 | QW-160 |
| Less than 1/16 (1.5) | $T$ | $2 T$ |  | $2 t$ | 2 | $\ldots$ | 2 | 2 |
| 1/16 to $3 / 8$ (1.5 to 10), incl. | $\begin{aligned} & 1 / 16 \\ & (1.5) \end{aligned}$ | $2 T$ | $2 t$ | 2 | Note (5) | 2 | 2 |
| Over $3 / 8$ (10), but less than $3 / 4$ (19) | 3/16 (5) | $2 T$ | $2 t$ | 2 | Note (5) | 2 | 2 |
| $3 / 4$ (19) to less than $1 \frac{1}{2}$ (38) | 3/16 (5) | $2 T$ | $2 t$ when $t<3 / 4$ (19) | 2 [Note (4)] | 4 | . . | . . |
| $3 / 4$ (19) to less than $1 \frac{1}{2}$ (38) | $3 / 16$ (5) | $2 T$ | $2 T$ when $t \geq 3 / 4$ (19) | 2 [Note (4)] | 4 | . $\cdot$ | . . . |
| $11 / 2$ (38) and over | 3/16 (5) | 8 (200) [Note (3)] | $2 t$ when $t<3 / 4$ (19) | 2 [Note (4)] | 4 | . . | . . |
| $1 / 2$ (38) and over | 3/16 (5) | 8 (200) [Note (3)] | 8 (200) [Note (3)] when $t \geq 3 / 4$ (19) | 2 [Note (4)] | 4 | . $\cdot$ | . . . |

[^2]GROOVE-WELD TENSION TESTS AND LONGITUDINAL-BEND TESTS

|  | Range of Thickness $T$ of Base Metal Qualified, in. (mm) <br> [Notes (1) and (2)] |  | Thickness $t$ of Deposited Weld Metal Qualified, in. (mm) [Notes (1) and (2)] | Type and Number of Tests Required (Tension and Guided-Bend Tests) [Note (2)] |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thickness $T$ of Test Coupon Welded, in. (mm) | Min. | Max. | Max. | Tension, QW-150 | Face Bend, QW-160 |  |
| Less than $1 / 16$ (1.5) | $T$ | $2 T$ | $2 t$ | 2 | 2 | 2 |
| $1 / 16$ to $3 / 8$ (1.5 to 10), incl. | 1/16(1.5) | $2 T$ | $2 t$ | 2 | 2 | 2 |
| Over $3 / 8$ (10) | 3/16 (5) | $2 T$ | $2 t$ | 2 | 2 | 2 |
| NOTES: |  |  |  |  |  |  |
| (1) The following variables further restrict the limits shown in this table when they are referenced in QW-250 for the process under consideration: QW-403.9, QW-403.10, QW-404. and QW-407.4. Also, QW-202.2, QW-202.3, and QW-202.4 provide exemptions that supersede the limits of this table. |  |  |  |  |  |  |

## 2004 SECTION IX

## QW-451. 3 <br> FILLET-WELD TESTS

| Type of <br> Joint | Thickness of Test <br> Coupons as Welded, in. | Type and Number of Tests <br> Fillet |
| :---: | :---: | :---: |
| Per QW-462.4(a) | All fillet sizes on all base <br> metal thicknesses and all <br> diameters | Macro |

GENERAL NOTE: A production assembly mockup may be substituted in accordance with QW-181.1.1. When a production assembly mockup is used, the range qualified shall be limited to the fillet weld size, base metal thickness, and configuration of the mockup. Alternatively, multiple production assembly mockups may be qualified. The range of thickness of the base metal qualified shall be no less than the thickness of the thinner member tested and no greater than the thickness of the thicker member tested. The range for fillet weld sizes qualified shall be limited to no less than the smallest fillet weld tested and no greater than the largest fillet weld tested. The configuration of production assemblies shall be the same as that used in the production assembly mockup.

QW-451.4
FILLET WELDS QUALIFIED BY GROOVE-WELD TESTS

| Thickness $T$ of Test <br> Coupon (Plate or Pipe) <br> as Welded | Range Qualified |
| :---: | :---: | | Type and Number of Tests |
| :---: |
| Required |

## QW-452 Performance Qualification Thickness

## Limits and Test Specimens

QW-452.1 Groove-Weld Test. The following tables identify the required type and number of tests and the thickness of weld metal qualified.

| $\begin{gathered} \text { QW-452.1(a) } \\ \text { TEST SPECIMENS } \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Type and Number of Examinations and Test Specimens Required |  |  |  |
| Thickness of Weld Metal, in. (mm) | Visual Examination per QW-302.4 | Side Bend QW-462.2 <br> [Note (1)] | Face Bend QW-462.3(a) or QW- $462.3(b)$ [Notes (1), (2)] | $\begin{gathered} \text { Root Bend } \\ \text { QW-462.3(a) } \\ \text { or QW- } \\ 462.3(b) \\ \text { [Notes (1), (2)] } \end{gathered}$ |
| Less than $3 / 8$ (10) $3 / 8$ (10) to less than 3/4 (19) | $X$ $X$ | $2\left[\right.$ … ${ }^{\text {[ }}$ (3)] | $\begin{gathered} 1 \\ \text { Note (3) } \end{gathered}$ | $\begin{gathered} 1 \\ \text { Note (3) } \end{gathered}$ |
| $3 / 4$ (19) and over | X | 2 | . . . | . . . |

GENERAL NOTE: The "Thickness of Weld Metal" is the total weld metal thickness deposited by all welders and all processes in the test coupon exclusive of the weld reinforcement.
NOTES:
(1) To qualify using positions 5 G or 6 G, a total of four bend specimens are required. To qualify using a combination of $2 G$ and $5 G$ in a single test coupon, a total of six bend specimens are required. See QW302.3. The type of bend test shall be based on weld metal thickness.
(2) Coupons tested by face and root bends shall be limited to weld deposit made by one welder with one or two processes or two welders with one process each. Weld deposit by each welder and each process shall be present on the convex surface of the appropriate bent specimen.
(3) One face and root bend may be substituted for the two side bends.

QW-452.1(b)
THICKNESS OF WELD METAL QUALIFIED

| Thickness, $t$, of Weld Metal in <br> the Coupon, in. $(\mathrm{mm})$ [Notes <br> $(1)$ and $(2)]$ | Thickness of Weld <br> Metal Qualified <br> [Note (3)] |
| :--- | :---: |
| All $2 t$ <br> $1 / 2(13)$ and over with a  <br> minimum of three layers  | Maximum to be <br> welded |

NOTES:
(1) When more than one welder and/or more than one process and more than one filler metal F-Number is used to deposit weld metal in a coupon, the thickness, $t$, of the weld metal in the coupon deposited by each welder with each process and each filler metal F-Number in accordance with the applicable variables under QW404 shall be determined and used individually in the "Thickness, $t$, of Weld Metal in the Coupon" column to determine the "Thickness of Weld Metal Qualified."
(2) Two or more pipe test coupons with different weld metal thickness may be used to determine the weld metal thickness qualified and that thickness may be applied to production welds to the smallest diameter for which the welder is qualified in accordance with QW-452.3.
(3) Thickness of test coupon of $3 / 4 \mathrm{in}$. ( 19 mm ) or over shall be used for qualifying a combination of three or more welders each of whom may use the same or a different welding process.

## 2004 SECTION IX

QW-452.3
GROOVE-WELD DIAMETER LIMITS

| Outside Diameter <br> of Test Coupon, in. (mm) | Outside Diameter <br> Qualified, in. (mm) |  |
| :--- | :--- | ---: |
|  |  |  |

GENERAL NOTES:
(a) Type and number of tests required shall be in accordance with QW-452.1.
(b) $2 \frac{7}{8} \mathrm{in}$. ( 73 mm ) O.D. is the equivalent of NPS $2 \frac{1}{2}$ (DN 65).

| QW-452.4 <br> SMALL DIAMETER FILLET-WELD TEST |  |  |
| :---: | :---: | :---: |
| Outside Diameter of Test Coupon, in. (mm) | Minimum Outside Diameter, Qualified, in. (mm) | Qualified <br> Thickness |
| Less than 1 (25) | Size welded | All |
| $1(25)$ to $2^{7} / 8$ (73) | 1 (25) | All |
| Over $27 / 8$ (73) | 27/8(73) | All |

GENERAL NOTES:
(a) Type and number of tests required shall be in accordance with QW-452.5.
(b) $2 \frac{7}{8} \mathrm{in}$. ( 73 mm ) 0.D. is considered the equivalent of NPS $2 \frac{1}{2}$ (DN 65).

## WELDING DATA

## QW-452.5

FILLET-WELD TEST

| Type of Joint | Thickness of Test Coupon as Welded, in. (mm) | Qualified Range | Type and Number of Tests Required [QW-462.4(b) or QW-462.4(c)] |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Macro | Fracture |
| Tee fillet | $3 / 16-3 / 8(5-10)$ | All base material thicknesses, fillet sizes, and diameters $2^{7} / 8(73)$ O.D. and over [Note (1)] | 1 | 1 |
|  | Less than $3 / 16$ (5) | $T$ to $2 T$ base material thickness, $T$ maximum fillet size, and all diameters $2^{7} / 8$ (73) O.D. and over [Note (1)] | 1 | 1 |

GENERAL NOTE: Production assembly mockups may be substituted in accordance with QW-181.2.1. When production assembly mockups are used, range qualified shall be limited to the fillet sizes, base metal thicknesses, and configuration of the mockup.
NOTE:
(1) $2 \frac{7}{8}$ in. ( 73 mm ) 0.D. is considered the equivalent of $N P S 21 / 2$ (DN 65). For smaller diameter qualifications, refer to QW-452.4 or QW-452.6.

QW-452.6
FILLET QUALIFICATION BY GROOVE-WELD TESTS

| Type of Joint | Thickness of Test Coupon as Welded, <br> in. (mm) | Qualified Range | Type and Number of <br> Tests Required |
| :--- | :---: | :---: | :---: |
| Any groove | All thicknesses | All base material thicknesses, <br> fillet sizes, and diameters | Fillet welds are qualified when a welder/welding <br> operator qualifies on a groove weld test |

## 2004 SECTION IX

## QW-453

PROCEDURE/PERFORMANCE QUALIFICATION THICKNESS LIMITS AND TEST SPECIMENS FOR HARD-FACING (WEAR-RESISTANT) AND CORROSIONRESISTANT OVERLAYS

| Thickness of Test Coupon ( $T$ ) | Corrosion-Resistant [Note (1)]Overlay |  | Hard-facing Overlay (Wear-Resistant) [Note (2)] |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Nominal Base Metal Thickness Qualified ( $T$ ) | Type and Number of Tests Required | Nominal Base Metal Thickness Qualified ( $T$ ) | Type and Number of Tests Required |
| Procedure Qualification Testing | $\left.\begin{array}{l}T \text { qualified to unlimited } \\ \text { l in. (25 mm) } \\ \text { to unlimited }\end{array}\right\}$ Notes (4), (5), and (9) |  |  | Notes (3), (7), (8), and (9) |
| Less than $1 \mathrm{in} .(25 \mathrm{~mm}) T$ <br> $1 \mathrm{in} .(25 \mathrm{~mm})$ and over $T$ |  |  |  |  |
| Performance Qualification Testing | $\left.\begin{array}{c}T \text { qualified to unlimited } \\ 1 \text { in. }(25 \mathrm{~mm}) \\ \text { to unlimited }\end{array}\right\}$ | Note (6) | $T$ qualified to unlimited <br> 1 in . 25 mm ) <br> to unlimited | Notes (8) and (10) |
| Less than $1 \mathrm{in}.(25 \mathrm{~mm}) T$ <br> $1 \mathrm{in} .(25 \mathrm{~mm})$ and over $T$ |  |  |  |  |

NOTES:
(1) The qualification test coupon shall consist of base metal not less than 6 in . ( 150 mm ) $\times 6 \mathrm{in}$. ( 150 mm ). The weld overlay cladding shall be a minimum of $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) wide by approximately 6 in . ( 150 mm ) long. For qualification on pipe, the pipe length shall be a minimum of 6 in . ( 150 mm ), and a minimum diameter to allow the required number of test specimens. The weld overlay shall be continuous around the circumference of the test coupon. For processes (performance qualification only) depositing a weld bead width greater than $1 / 2 \mathrm{in}$. ( 13 mm ) wide, the weld overlay shall consist of a minimum of three weld beads in the first layer.
(2) The test base metal coupon shall have minimum dimensions of 6 in . ( 150 mm ) wide $\times$ approximately 6 in . ( 150 mm ) long with a hardfaced layer a minimum of $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) wide $\times 6 \mathrm{in}$. ( 150 mm ) long. The minimum hard-faced thickness shall be as specified in the Welding Procedure Specification. Alternatively, the qualification may be performed on a test base metal coupon that represents the size of the production part. For qualification on pipe, the pipe length shall be 6 in . ( 150 mm ) minimum, and of a minimum diameter to allow the required number of test specimens. The weld overlay shall be continuous around the circumference of the test coupon.
(3) The hard-facing surface shall be examined by the liquid penetrant method and shall meet the acceptance standards in QW-195.2 or as specified in the WPS. Surface conditioning prior to liquid penetrant examination is permitted.
(4) The corrosion-resistant surface shall be examined by the liquid penetrant method and shall meet the acceptance standards as specified in QW-195.
(5) Following the liquid penetrant examination, four guided side-bend tests shall be made from the test coupon in accordance with QW-161. The test specimens shall be cut so that there are either two specimens parallel and two specimens perpendicular to the direction of the welding, or four specimens perpendicular to the direction of the welding. For coupons that are less than $3 / 8 \mathrm{in}$. ( 10 mm ) thick, the width of the side-bend specimens may be reduced to the thickness of the test coupon. The side-bend specimens shall be removed from locations specified in QW-462.5(c) or QW-462.5(d).
(6) The test coupon shall be sectioned to make side-bend test specimens perpendicular to the direction of the welding in accordance with QW161. Test specimens shall be removed at locations specified in QW-462.5(c) or QW-462.5(d).
(7) After surface conditioning to the minimum thickness specified in the WPS, a minimum of three hardness readings shall be made on each of the specimens from the locations shown in $Q W-462.5(b)$ or $Q W-462.5(e)$. All readings shall meet the requirements of the WPS.
(8) The base metal shall be sectioned transversely to the direction of the hard-facing overlay. The two faces of the hard-facing exposed by sectioning shall be polished and etched with a suitable etchant and shall be visually examined with $\times 5$ magnification for cracks in the base metal or the heat-affected zone, lack of fusion, or other linear defects. The overlay and the base metal shall meet the requirements specified in the WPS. All exposed faces shall be examined. See QW-462.5(b) for pipe and QW-462.5(e) for plate.
(9) When a chemical composition is specified in the WPS, chemical analysis specimens shall be removed at locations specified in QW-462.5(b) or QW-462.5(e). The chemical analysis shall be performed in accordance with QW-462.5(a) and shall be within the range specified in the WPS. This chemical analysis is not required when a chemical composition is not specified on the WPS.
(10) At a thickness greater than or equal to the minimum thickness specified in the WPS, the weld surface shall be examined by the liquid penetrant method and shall meet the acceptance standards in QW-195.2 or as specified in the WPS. Surface conditioning prior to liquid penetrant examination is permitted.

QW-460 GRAPHICS
QW-461 Positions

| Tabulation of Positions of Welds |  |  |  |
| :---: | :---: | :---: | :---: |
| Position | Diagram <br> Reference | Inclination of Axis, deg. | Rotation of Face, deg |
| Flat | A | 0 to 15 | 150 to 210 |
| Horizontal | B | 0 to 15 | $\begin{array}{r} 80 \text { to } 150 \\ -210 \text { to } 280 \end{array}$ |
| Overhead | C | 0 to 80 | $\begin{array}{r} 0 \text { to } 80 \\ 280 \text { to } 360 \end{array}$ |
| Vertical | $\begin{aligned} & D \\ & E \end{aligned}$ | 15 to 80 80 to 90 | $\begin{array}{r} 80 \text { to } 280 \\ 0 \text { to } 360 \end{array}$ |



GENERAL NOTE:
The horizontal reference plane is taken to lie always below the weld under consideration.
Inclination of axis is measured from the horizontal reference plane toward the vertical.
Angle of rotation of face is measured from a line perpendicular to the axis of the weld and lying in a vertical plane containing this axis. The reference position ( 0 deg .) of rotation of the face invariably points in the direction opposite to that in which the axis angle increases. The angle of rotation of the face of weld is measured in a clockwise direction from this reference position ( 0 deg.) when looking at point $P$.

QW-461.1 POSITIONS OF WELDS - GROOVE WELDS

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| Tabulation of Positions of Fillet Welds |  |  |  |
| :---: | :---: | :---: | :---: |
| Position | Diagram <br> Reference | Inclination of Axis, deg. | Rotation of Face, deg. |
| Flat | A | 0 to 15 | 150 to 210 |
| Horizontal | B | 0 to 15 | $\begin{array}{r} 125 \text { to } 150 \\ -210 \text { to } 235 \end{array}$ |
| Overhead | C | 0 to 80 | $\begin{array}{r} 0 \text { to } 125 \\ -\quad 235 \text { to } 360 \end{array}$ |
|  | D | $15 \text { to } 80$ | 125 to 235 |
| Vertical | E | 80 to 90 | 0 to 360 |



QW-461.2 POSITIONS OF WELDS - FILLET WELDS


QW-461.3 GROOVE WELDS IN PLATE - TEST POSITIONS

(a) 1G Rotated


(c) 5 G
(b) 2G

(d) $\mathbf{6 G}$

QW-461.4 GROOVE WELDS IN PIPE - TEST POSITIONS

(a) 1 F

(b) $2 F$

(c) $3 F$

QW-461.5 FILLET WELDS IN PLATE - TEST POSITIONS

(a) 1F (Rotated)

(b) $2 F$

(c) 2FR (Rotated)

(d) $4 F$

(e) 5 F

QW-461.6 FILLET WELDS IN PIPE - TEST POSITIONS


QW-461.7 STUD WELDS - TEST POSITIONS


QW-461.8 STUD WELDS - WELDING POSITIONS

QW-461.9
PERFORMANCE QUALIFICATION - POSITION AND DIAMETER LIMITATIONS (Within the Other Limitations of QW-303)


NOTES:
(1) Positions of welding as shown in QW-461.1 and QW-461.2.

F = Flat
$H=$ Horizontal
$\mathrm{V}=$ Vertical
$0=$ Overhead
(2) Pipe $27 / 8$ in. $(72 \mathrm{~mm}$ ) O.D. and over.
(3) See diameter restrictions in QW-452.3, QW-452.4, and QW-452.6.

## QW-462 Test Specimens

The purpose of the QW-462 figures is to give the manufacturer or contractor guidance in dimensioning test specimens for tests required for procedure and performance qualifications. Unless a minimum, maximum, or tolerance is given in the figures (or as $\mathrm{QW}-150, \mathrm{QW}-160$,
or QW-180 requires), the dimensions are to be considered approximate. All welding processes and filler material to be qualified must be included in the test specimen.
$x=$ coupon thickness including reinforcement
$y=$ specimen thickness
$T=$ coupon thickness excluding reinforcement
$W=$ specimen width, $3 / 4 \mathrm{in}$. $(19 \mathrm{~mm}$ )


QW-462.1(a) TENSION - REDUCED SECTION - PLATE


QW-462.1(b) TENSION - REDUCED SECTION - PIPE

$1 \frac{1}{16} \mathrm{in}$. $(27 \mathrm{~mm}) \quad$ Edge of widest face of weld
NOTES:
(1) The weld reinforcement shall be ground or machined so that the weld thickness does not exceed the base metal thickness $T$. Machine minimum amount to obtain approximately parallel surfaces.
(2) The reduced section shall not be less than the width of the weld plus $2 y$.

QW-462.1(c) TENSION - REDUCED SECTION ALTERNATE FOR PIPE

WELDING DATA

|  | Standard Dimensions, in. (mm) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | (a) <br> 0.505 Specimen | (b) <br> 0.353 Specimen | (c) <br> 0.252 Specimen | (d) <br> 0.188 Specimen |
| $A$-Length of reduced section | Note (1) | Note (1) | Note (1) | Note (1) |
| D-Diameter | $\begin{aligned} & 0.500 \pm 0.010(12.7 \pm \\ & 0.25) \end{aligned}$ | $\begin{aligned} & 0.350 \pm 0.007(8.89 \pm \\ & 0.18) \end{aligned}$ | $\begin{aligned} & 0.250 \pm 0.005(6.35 \pm \\ & 0.13) \end{aligned}$ | $\begin{aligned} & 0.188 \pm 0.003(4.78 \pm \\ & 0.08) \end{aligned}$ |
| $R$-Radius of fillet | $3 / 8$ (10) min. | $1 / 4(6) \mathrm{min}$. | 3/16 (5) min. | $1 / 8$ (3) min. |
| $B$-Length of end section | $13 / 8$ (35) approx. | 1/1/8 (29) approx. | 7/8 (22) approx. | 1/2 (13) approx. |
| $C$-Diameter of end section | 3/4 (19) | 1/2 (13) | 3/8(10) | $1 / 4$ (6) |
| GENERAL NOTES: |  |  |  |  |
| (a) Use maximum diameter specimen (a), (b), (c), or (d) that can be cut from the section. <br> (b) Weld should be in center of reduced section. |  |  |  |  |
|  |  |  |  |  |
| (c) Where only a single coupon is required, the center of the specimen should be midway between the surfaces. |  |  |  |  |
| (d) The ends may be of any shape to fit the holders of the testing machine in such a way that the load is applied axially. |  |  |  |  |
| NOTE: |  |  |  |  |
| (1) Reduced section $A$ should not be less than width of weld plus $2 D$. |  |  |  |  |
| QW-462.1(d) TENSION - REDUCED SECTION - TURNED SPECIMENS |  |  |  |  |



QW-462.1(e) TENSION - FULL SECTION - SMALL DIAMETER PIPE



GENERAL NOTE: Weld reinforcement and backing strip or backing ring, if any, may be removed flush with the surface of the specimen. Thermal cutting, machining, or grinding may be employed. Cold straightening is permitted prior to removal of the reinforcement.

NOTE:
(1) When specimen thickness $T$ exceeds $1 \frac{1}{2} \mathrm{in}$. (38 mm), use one of the following.
(a) Cut specimen into multiple test specimens $y$ of approximately equal dimensions $\left[3 / 4\right.$ in. ( 19 mm ) to $1 \frac{1}{2}$ in. $(38 \mathrm{~mm})] . y=$ tested specimen thickness when multiple specimens are taken from one coupon.
(b) The specimen may be bent at full width. See requirements on jig width in QW-466.1.

QW-462.2 SIDE BEND
$1 \frac{1}{2}$ in. (38 mm)


Face-Bend Specimen - Plate and Pipe


GENERAL NOTES:
(a) Weld reinforcement and backing strip or backing ring, if any, shall be removed flush with the surface of the specimen. If a recessed ring is used, this surface of the specimen may be machined to a depth not exceeding the depth of the recess to remove the ring, except that in such cases the thickness of the finished specimen shall be that specified above. Do not flame-cut nonferrous material.
(b) If the pipe being tested has a diameter of NPS 4 (DN 100) or less, the width of the bend specimen may be $3 / 4 \mathrm{in}$. (19 mm) for pipe diameters NPS 2 (DN 50) to and including NPS 4 (DN 100). The bend specimen width may be $3 / 8 \mathrm{in}$. ( 10 mm ) for pipe diameters less than NPS 2 (DN 50) down to and including NPS $3 / 8$ (DN 10) and as an alternative, if the pipe being tested is equal to or less than NPS 1 (DN 25) pipe size, the width of the bend specimens may be that obtained by cutting the pipe into quarter sections, less an allowance for saw cuts or machine cutting. These specimens cut into quarter sections are not required to have one surface machined flat as shown in QW-462.3(a). Bend specimens taken from tubing of comparable sizes may be handled in a similar manner.

## QW-462.3(a) FACE AND R00T BENDS TRANSVERSE



GENERAL NOTE: Weld reinforcements and backing strip or backing ring, if any, shall be removed essentially flush with the undisturbed surface of the base material. If a recessed strip is used, this surface of the specimen may be machined to a depth not exceeding the depth of the recess to remove the strip, except that in such cases the thickness of the finished specimen shall be that specified above.


| $T_{1}$ | $T_{2}$ |
| :---: | :---: |
| $1 / 8$ in. $(3 \mathrm{~mm})$ and less | $T_{1}$ |
| Over $1 / 8 \mathrm{in} .(3 \mathrm{~mm})$ | Equal to or less than $T_{1}$, but <br> not less than $1 / 8 \mathrm{in} .(3 \mathrm{~mm})$ |



GENERAL NOTE: Macro-test - the fillet shall show fusion at the root of the weld but not necessarily beyond the root. The weld metal and heat-affected zone shall be free of cracks.

QW-462.4(a) FILLET WELDS - PROCEDURE


GENERAL NOTE: Refer to QW-452.5 for $T$ thickness/qualification ranges.
QW-462.4(b) FILLET WELDS - PERFORMANCE

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QW-462.4(c) FILLET WELDS IN PIPE - PERFORMANCE

(a) Either pipe-to-plate or pipe-to-pipe may be used as shown.
(b) Macro test:
(1) The fillet shall show fusion at the root of the weld but not necessarily beyond the root.
(2) The weld metal and the heat-affected zone shall be free of cracks.

QW-462.4(d) FILLET WELDS IN PIPE - PROCEDURE


NOTES:
(1) When a chemical analysis or hardness test is conducted on the as welded surface, the distance from the approximate weld interface to the final as welded surface shall become the minimum qualified overlay thickness. The chemical analysis may be performed directly on the as welded surface or on chips of material taken from the as welded surface.
(2) When a chemical analysis or hardness test is conducted after material has been removed from the as welded surface, the distance from the approximate weld interface to the prepared surface shall become the minimum qualified overlay thickness. The chemical analysis may be made directly on the prepared surface or from chips removed from the prepared surface.
(3) When a chemical analysis test is conducted on material removed by a horizontal drilled sample, the distance from the approximate weld interface to the uppermost side of the drilled cavity shall become the minimum qualified overlay thickness. The chemical analysis shall be performed on chips of material removed from the drilled cavity.

## QW-462.5(a) CHEMICAL ANALYSIS AND HARDNESS SPECIMEN CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY



Test Specimen Location for 5G Overlay Qualification (Specimens Required From a Minimum of Three Locations)

Fixed Pipe on 45 deg. Angle


Test Specimen Location for 6G Overlay Qualification (Specimens Required From a Minimum of Three Locations)


Test Specimen Location for 2G and 1G Rotated Overlay Qualification (Specimens Required From One Location)

## GENERAL NOTE:

Overlay may be on the inside or outside of pipe.
NOTES:
(1) Location of required test specimen removal (QW-453). Refer to QW-462.5(a) for chemical analysis and hardness test surface locations and minimum qualified thickness.
(2) Testing of circumferential hard-facing weld metal on pipe procedure qualification coupons may be limited to a single segment (completed utilizing the vertical, up-hill progression) for the chemical analysis, hardness, and macro-etch tests required in QW-453. Removal is required for a change from vertical down to vertical up-hill progression (but not vice-versa).
(3) Location of test specimens shall be in accordance with the angular position limitations of QW-120.
(4) When overlay welding is performed using machine or automatic welding and the vertical travel direction of adjacent weld beads is reversed on alternate passes, only one chemical analysis or hardness specimen is required to represent the vertical portion. Qualification is then restricted in production to require alternate pass reversal of rotation direction method.

## QW-462.5(b) CHEMICAL ANALYSIS SPECIMEN, HARD-FACING OVERLAY HARDNESS, AND MACRO TEST

 LOCATION(S) FOR CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY
## WELDING DATA



GENERAL NOTE: Overlay may be on the inside or outside of pipe.
NOTES:
(1) Location for required test specimen removal - Procedure (QW-453).
(2) Location for required test specimen removal - Performance (QW-453).

QW-462.5(c) PIPE BEND SPECIMEN - CORROSION-RESISTANT WELD METAL OVERLAY


NOTES:
(1) Location for required test specimen removal - Procedure (QW-453). Four-side-bend test specimens are required for each position.
(2) Location for required test specimen removal - Performance (OW-453). Two-side-bend test specimens are required for each position.

QW-462.5(d) PLATE BEND SPECIMENS - CORROSION-RESISTANT WELD METAL OVERLAY


GENERAL NOTES:
(a) Location of required test specimen removal (QW-453). One required for each position. Refer to QW-462.5(a) for chemical analysis and hardness test surface locations and minimum qualified thickness.
(b) Removal required for a change from vertical up to vertical down and vice versa.

QW-462.5(e) PLATE MACRO, HARDNESS, AND CHEMICAL ANALYSIS SPECIMENS - CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY



Peel Test
Step 1 - Grip in vise or other suitable device.
Step 2 - Bend specimen.
Step 3 - Peel pieces apart with pincers or other suitable tool.

(a) Single Spot Shear Specimen

(b) Multiple Spot Shear Specimen [Note (2)]

Nominal Thickness of Thinner Sheet, in. (mm)
Over 0.008 to 0.030 ( 0.20 to 0.8 )
Over 0.030 to 0.100 ( 0.8 to 2.5)
Over 0.100 to 0.130 ( 2.5 to 3 )
Over 0.130 (3)
NOTES:
(1) $L$ shall be not less than $4 W$.
(2) Sketch (b) shall be made of 5 specimens or more.

QW-462.9 SPOT WELDS IN SHEET
SHEAR STRENGTH REQUIREMENTS FOR SPOT OR PROJECTION WELD SPECIMENS

| Customary Units |  |  |  |  | SI Units |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P-No. 1 Through P-No. 11 and P-No. 41 Through P-No. 47 Metals |  |  |  |  | P-1 Through P-11 and P-4X Metals |  |  |  |  |
| Nominal Thickness of Thinner Sheet, in. | Ultimate Strength 90,000 to 149,000 psi |  | Ultimate Strength Below 90,000 psi |  | Nominal Thickness of Thinner Sheet, mm | Ultimate Strength 620 MPa to 1027 MPa |  | Ultimate Strength Below 620 MPa |  |
|  |  | Spot |  | Spot |  |  | Spot |  | Spot |
|  | Min. | Min. Avg. | Min. | Min. Avg. |  | Min. | Min. Avg. | Min. | Min. Avg. |
| 0.009 | 130 | 160 | 100 | 125 | 0.2 | 59 | 73 | 45 | 57 |
| 0.010 | 160 | 195 | 115 | 140 | 0.25 | 73 | 88 | 52 | 64 |
| 0.012 | 200 | 245 | 150 | 185 | 0.30 | 91 | 111 | 68 | 84 |
| 0.016 | 295 | 365 | 215 | 260 | 0.41 | 134 | 166 | 98 | 118 |
| 0.018 | 340 | 415 | 250 | 305 | 0.46 | 154 | 188 | 113 | 138 |
| 0.020 | 390 | 480 | 280 | 345 | 0.51 | 177 | 218 | 127 | 156 |
| 0.022 | 450 | 550 | 330 | 405 | 0.56 | 204 | 249 | 150 | 184 |
| 0.025 | 530 | 655 | 400 | 495 | 0.64 | 240 | 297 | 181 | 225 |
| 0.028 | 635 | 785 | 465 | 575 | 0.71 | 288 | 356 | 211 | 261 |
| 0.032 | 775 | 955 | 565 | 695 | 0.81 | 352 | 433 | 256 | 315 |
| 0.036 | 920 | 1,140 | 690 | 860 | 0.91 | 417 | 517 | 313 | 390 |
| 0.040 | 1,065 | 1,310 | 815 | 1,000 | 1.0 | 483 | 594 | 370 | 454 |
| 0.045 | 1,285 | 1,585 | 1,005 | 1,240 | 1.1 | 583 | 719 | 456 | 562 |
| 0.050 | 1,505 | 1,855 | 1,195 | 1,475 | 1.3 | 683 | 841 | 542 | 669 |
| 0.056 | 1,770 | 2,185 | 1,460 | 1,800 | 1.4 | 803 | 991 | 662 | 816 |
| 0.063 | 2,110 | 2,595 | 1,760 | 2,170 | 1.6 | 957 | 1177 | 798 | 984 |
| 0.071 | 2,535 | 3,125 | 2,080 | 2,560 | 1.8 | 1150 | 1418 | 943 | 1161 |
| 0.080 | 3,005 | 3,705 | 2,455 | 3,025 | 2.0 | 1363 | 1681 | 1114 | 1372 |
| 0.090 | 3,515 | 4,335 | 2,885 | 3,560 | 2.3 | 1594 | 1966 | 1309 | 1615 |
| 0.100 | 4,000 | 4,935 | 3,300 | 4,070 | 2.54 | 1814 | 2239 | 1497 | 1846 |
| 0.112 | 4,545 | 5,610 | 3,795 | 4,675 | 2.84 | 2062 | 2545 | 1721 | 2121 |
| 0.125 | 5,065 | 6,250 | 4,300 | 5,310 | 3.18 | 2297 | 2835 | 1950 | 2409 |

WELDING DATA

| QW-462.11HEAR STRENGTH REQUIREMENTS FOR SPOT OR PROJECTION WELD SPECIMENS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| U.S. Customary Units |  |  |  |  |  |  | SI Units |  |  |  |  |  |  |
| P-No. 21 Through P-No. 25 Aluminum Alloys |  |  |  |  |  |  | P-2X Aluminum Alloys |  |  |  |  |  |  |
| Nominal Thickness of Thinner Sheet, in. | $\begin{gathered} \text { Ultimate Strength } \\ 35,000 \text { to } 55,999 \\ \text { psi, } \\ \text { ib per Spot } \\ \hline \end{gathered}$ |  | $\begin{gathered} \text { Ultimate Strength } \\ \text { 19,500 to } 34,999 \\ \text { psi, } \\ \text { lb per Spot } \\ \hline \end{gathered}$ |  | $\begin{gathered} \text { Ultimate } \\ \text { Strength Below } \\ 19,500 \text { psi, } 1 \mathrm{l} \\ \text { per Spot } \\ \hline \end{gathered}$ |  | Nominal Thickness of Thinner Sheet, mm | Ultimate Strength 241 MPa to 386 $\mathrm{MPa}_{\text {, }}$ kg per Spot |  | Ultimate <br> Strength 134 MPa to 241 MPa , kg per Spot |  | Ultimate <br> Strength Below 134 MPa , kg per Spot |  |
|  | Min. | $\begin{aligned} & \text { Min. } \\ & \text { Avg. } \end{aligned}$ | Min. | Min. Avg. | Min. | $\begin{aligned} & \hline \text { Min. } \\ & \text { Avg. } \end{aligned}$ |  | Min. | Min. Avg. | Min. | $\begin{aligned} & \text { Min. } \\ & \text { Avg. } \end{aligned}$ | Min. | Min. Avg. |
| 0.010 | 50 | 65 |  |  |  |  | 0.25 | 23 | 29 |  |  |  |  |
| 0.012 | 65 | 85 | 30 | 40 | 20 | 25 | 0.30 | 29 | 39 | 14 | 18 | 9 | 11 |
| 0.016 | 100 | 125 | 70 | 90 | 50 | 65 | 0.41 | 45 | 57 | 32 | 41 | 23 | 29 |
| 0.018 | 115 | 145 | 85 | 110 | 65 | 85 | 0.46 | 52 | 66 | 39 | 50 | 29 | 39 |
| 0.020 | 135 | 170 | 100 | 125 | 80 | 100 | 0.51 | 61 | 77 | 45 | 57 | 36 | 45 |
| 0.022 | 155 | 195 | 120 | 150 | 95 | 120 | 0.56 | 70 | 88 | 54 | 68 | 43 | 54 |
| 0.025 | 175 | 200 | 145 | 185 | 110 | 140 | 0.64 | 79 | 91 | 66 | 84 | 50 | 64 |
| 0.028 | 205 | 260 | 175 | 220 | 135 | 170 | 0.71 | 93 | 118 | 79 | 100 | 61 | 77 |
| 0.032 | 235 | 295 | 210 | 265 | 165 | 210 | 0.81 | 107 | 134 | 95 | 120 | 75 | 95 |
| 0.036 | 275 | 345 | 255 | 320 | 195 | 245 | 0.91 | 125 | 156 | 116 | 145 | 88 | 111 |
| 0.040 | 310 | 390 | 300 | 375 | 225 | 285 | 1.0 | 141 | 177 | 136 | 170 | 102 | 129 |
| 0.045 | 370 | 465 | 350 | 440 | 260 | 325 | 1.1 | 168 | 211 | 159 | 200 | 118 | 147 |
| 0.050 | 430 | 540 | 400 | 500 | 295 | 370 | 1.3 | 195 | 245 | 181 | 227 | 134 | 168 |
| 0.057 | 515 | 645 | 475 | 595 | 340 | 425 | 1.45 | 234 | 293 | 215 | 270 | 154 | 193 |
| 0.063 | 610 | 765 | 570 | 715 | 395 | 495 | 1.6 | 277 | 347 | 259 | 324 | 179 | 225 |
| 0.071 | 720 | 900 | 645 | 810 | 450 | 565 | 1.8 | 327 | 408 | 293 | 367 | 204 | 256 |
| 0.080 | 855 | 1,070 | 765 | 960 | 525 | 660 | 2.0 | 388 | 485 | 347 | 435 | 238 | 299 |
| 0.090 | 1,000 | 1,250 | 870 | 1,090 | 595 | 745 | 2.3 | 454 | 567 | 395 | 494 | 270 | 338 |
| 0.100 | 1,170 | 1,465 | 940 | 1,175 | 675 | 845 | 2.54 | 531 | 665 | 426 | 533 | 306 | 383 |
| 0.112 | 1,340 | 1,675 | 1,000 | 1,255 | 735 | 920 | 2.84 | 608 | 760 | 454 | 569 | 333 | 417 |
| 0.125 | 1,625 | 2,035 | 1,050 | 1,315 | 785 | 985 | 3.18 | 737 | 923 | 476 | 596 | 356 | 447 |
| 0.140 | 1,920 | 2,400 | ... | ... | ... | ... | 3.56 | 871 | 1089 | ... | ... | ... | ... |
| 0.160 | 2,440 | 3,050 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 4.06 | 1107 | 1383 | $\ldots$ | $\ldots$ | $\ldots$ | $\cdots$ |
| 0.180 | 3,000 | 3,750 | $\ldots$ | ... | ... | $\ldots$ | 4.57 | 1361 | 1701 | $\ldots$ | $\ldots$ | ... | $\ldots$ |
| 0.190 | 3,240 | 4,050 | $\ldots$ | ... | $\ldots$ | $\ldots$ | 4.83 | 1470 | 1837 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 0.250 | 6,400 | 8,000 | . | ... | $\ldots$ | $\ldots$ | 6.35 | 2903 | 3629 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |

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QW-463.1(a) PLATES - LESS THAN $3 / 4 \mathrm{in}$. ( 19 mm ) THICKNESS PROCEDURE QUALIFICATION


QW-463.1(b) PLATES - $3 / 4 \mathrm{in}$. ( 19 mm ) AND OVER THICKNESS AND ALTERNATE FROM $3 / 8 \mathrm{in}$. ( 10 mm ) BUT LESS THAN $3 / 4 \mathrm{in}$. ( 19 mm ) THICKNESS PROCEDURE QUALIFICATION



QW-463.1(d) PROCEDURE QUALIFICATION


QW-463.1(e) PROCEDURE QUALIFICATION


QW-463.1(f) NOTCH-TOUGHNESS TEST SPECIMEN LOCATION


QW-463.2(a) PLATES - LESS THAN $3 / 4 \mathrm{in}$. ( 19 mm ) THICKNESS PERFORMANCE QUALIFICATION


QW-463.2(b) PLATES - $3 / 4 \mathrm{in}$. ( 19 mm ) AND OVER THICKNESS AND ALTERNATE FROM $3 / 8$ in. ( 10 mm ) BUT LESS THAN $3 / 4 \mathrm{in}$. ( 19 mm ) THICKNESS PERFORMANCE QUALIFICATION


QW--463.2(c) PLATES - LONGITUDINAL PERFORMANCE QUALIFICATION


QW-463.2(d) PERFORMANCE QUALIFICATION


QW-463.2(e) PERFORMANCE QUALIFICATION


QW-463.2(f) PIPE - NPS 10 (DN 250) ASSEMBLY PERFORMANCE QUALIFICATION


GENERAL NOTE: When side bend tests are made in accordance with QW-452.1 and QW-452.3, they shall be removed as shown in $\mathrm{OW}-463.2(\mathrm{~g})$ in place of the face and root bends.

QW-463.2(g) NPS 6 (DN 150) OR NPS 8 (DN 200) ASSEMBLY PERFORMANCE QUALIFICATION


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## WELDING DATA

|  | Discard | $\varlimsup_{\downarrow} 1 \mathrm{in} .(25 \mathrm{~mm}) \mathrm{min} .$ |
| :---: | :---: | :---: |
|  | Peel test specimen |  |
|  |  | $\bar{\uparrow}^{3 / 4} \mathrm{in} .(19 \mathrm{~mm}) \mathrm{min} .$ |
|  | Peel test specimen | W |
|  | Discard | $\uparrow$ |


$1 / 2 \mathrm{in}$. (13 mm)

(a) Peel Test Coupon and Specimens

QW-464.2 PERFORMANCE QUALIFICATION TEST COUPONS
AND TEST SPECIMENS


QW-466.1 TEST JIG DIMENSIONS

## WELDING DATA

| SI Units |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Material | Thickness of Specimen, mm | $A, \mathrm{~mm}$ | $B, \mathrm{~mm}$ | C, mm | D, mm |
| P-No. 23 to P-No. 21 through P-No. 25; P-No. 21 through P-No. 25 with F-No. 23; P-No. 35; any P-No. metal with F-No. 33, 36, or 37 | $\begin{aligned} & 3 \\ & t=3 \text { or less } \end{aligned}$ | $\begin{aligned} & 52.4 \\ & 16 \frac{1}{2} t \end{aligned}$ | $\begin{aligned} & 26.2 \\ & 81 / 4 t \end{aligned}$ | $\begin{aligned} & 60.4 \\ & 18 \frac{1}{2} t+1.6 \end{aligned}$ | $\begin{aligned} & 30.2 \\ & 91 / 4 t+0.8 \end{aligned}$ |
| P-No. 11; P-No. 25 to P-No. 21 or P-No. 22 or P-No. 25 | $\begin{aligned} & 10 \\ & t=10 \text { or less } \end{aligned}$ | $\begin{aligned} & 63.5 \\ & 6 / 3 t \end{aligned}$ | $\begin{aligned} & 31.8 \\ & 31 / 3 t \end{aligned}$ | $\begin{aligned} & 85.8 \\ & 8^{2} / 3 t+3.2 \end{aligned}$ | $\begin{aligned} & 42.9 \\ & 41 / 3 t+1.6 \end{aligned}$ |
| P-No. 51; P-No. 49 | $\begin{aligned} & 10 \\ & t=10 \text { or less } \end{aligned}$ | $\begin{aligned} & 76.2 \\ & 8 t \end{aligned}$ | $\begin{aligned} & 38.1 \\ & 4 t \end{aligned}$ | $\begin{aligned} & 98.4 \\ & 10 t+3.2 \end{aligned}$ | $\begin{aligned} & 49.2 \\ & 5 t+1.6 \end{aligned}$ |
| P-No. 52; P-No. 53; P-No. 61; P-No. 62 | $\begin{aligned} & 10 \\ & t=10 \text { or less } \end{aligned}$ | $\begin{aligned} & 95.2 \\ & 10 t \end{aligned}$ | $\begin{aligned} & 47.6 \\ & 5 t \end{aligned}$ | $\begin{aligned} & 117.5 \\ & 12 t+3.2 \end{aligned}$ | $\begin{aligned} & 58.7 \\ & 6 t+1.6 \end{aligned}$ |
| All others with greater than or equal to $20 \%$ elongation | $\begin{aligned} & 10 \\ & t=10 \text { or less } \end{aligned}$ | $\begin{aligned} & 38.1 \\ & 4 t \end{aligned}$ | $\begin{aligned} & 19.0 \\ & 2 t \end{aligned}$ | $\begin{aligned} & 60.4 \\ & 6 t+3.2 \end{aligned}$ | $\begin{aligned} & 30.2 \\ & 3 t+1.6 \end{aligned}$ |
| All others with less than $20 \%$ elongation | $t=$ (see Note b) | $32^{7} / 8 t$ max. | $\begin{array}{r} 167 / 16 t \\ \max . \end{array}$ | $\begin{gathered} 34^{7} / 8 t+1.6 \\ \max . \end{gathered}$ | $\begin{aligned} & 17^{7} / 16 t+0.8 \\ & \max . \end{aligned}$ |

GENERAL NOTES:
(a) For P-Numbers, see QW/QB-422; for F-Numbers, see QW-432.
(b) The dimensions of the test jig shall be such as to give the bend test specimen a calculated percent outer fiber elongation equal to at least that of the base material with the lower minimum elongation as specified in the base material specification.

$$
\text { percent outer fiber elongation }=\frac{100 t}{A+t}
$$

The following formula is provided for convenience in calculating the bend specimen thickness:

$$
\text { thickness of specimen }(t)=\frac{A \times \text { percent elongation }}{[100-(\text { percent elongation })]}
$$

(c) For guided-bend jig configuration, see QW-466.2, QW-466.3, and QW-466.4.
(d) The weld and heat-affected zone, in the case of a transverse weld bend specimen, shall be completely within the bend portion of the specimen after testing.

QW-466.1 TEST JIG DIMENSIONS (CONT'D)


GENERAL NOTE: See OW-466.1 for jig dimensions and general notes.
NOTES:
(1) Either hardened and greased shoulders or hardened rollers free to rotate shall be used.
(2) The shoulders or rollers shall have a minimum bearing surface of 2 in . ( 50 mm ) for placement of the specimen. The rollers shall be high enough above the bottom of the jig so that the specimens will clear the rollers when the ram is in the low position.
(3) The ram shall be fitted with an appropriate base and provision made for attachment to the testing machine, and shall be of a sufficiently rigid design to prevent deflection and misalignment while making the bend test. The body of the ram may be less than the dimensions shown in column A of QW-466.1.
(4) If desired, either the rollers or the roller supports may be made adjustable in the horizontal direction so that specimens of $t$ thickness may be tested on the same jig.
(5) The roller supports shall be fitted with an appropriate base designed to safeguard against deflection and misalignment and equipped with means for maintaining the rollers centered midpoint and aligned with respect to the ram.

QW-466.2 GUIDED-BEND ROLLER JIG


## GENERAL NOTES:

(a) See QW-466.1 for jig dimensions and other general notes.
(b) Dimensions not shown are the option of the designer. The essential consideration is to have adequate rigidity so that the jig parts will not spring.
(c) The specimen shall be firmly clamped on one end so that there is no sliding of the specimen during the bending operation.
(d) Test specimens shall be removed from the jig when the outer roll has been removed 180 deg from the starting point.

QW-466.3 GUIDED-BEND WRAP AROUND JIG


QW-466.4 STUD-WELD BEND JIG


GENERAL NOTES:
(a) Dimensions are appropriate to the size of the stud.
(b) Threads of the stud shall be clean and free of lubricant other than residual cutting oil.

QW-466.5 TORQUE TESTING ARRANGEMENT FOR STUD WELDS


QW-469.1 BUTT JOINT


QW-466.6 SUGGESTED TYPE TENSILE TEST FIGURE FOR STUD WELDS


QW-469.2 ALTERNATIVE BUTT JOINT

## QW-470 ETCHING - PROCESSES AND REAGENTS

## QW-471 General

The surfaces to be etched should be smoothed by filing, machining, or grinding on metallographic papers. With different alloys and tempers, the etching period will vary from a few seconds to several minutes, and should be continued until the desired contrast is obtained. As a protection from the fumes liberated during the etching process, this work should be done under a hood. After etching, the specimens should be thoroughly rinsed and then dried with a blast of warm air. Coating the surface with a thin clear lacquer will preserve the appearance.

## QW-472 For Ferrous Metals

Etching solutions suitable for carbon and low alloy steels, together with directions for their use, are suggested in QW-472.1 through QW-472.4.

QW-472.1 Hydrochloric Acid. Hydrochloric (muriatic) acid and water, equal parts, by volume. The solution should be kept at or near the boiling temperature during the etching process. The specimens are to be immersed in the solution for a sufficient period of time to reveal all lack of soundness that might exist at their cross-sectional surfaces.

QW-472.2 Ammonium Persulfate. One part of ammonium persulfate to nine parts of water, by weight. The solution should be used at room temperature, and should be applied by vigorously rubbing the surface to be etched with a piece of cotton saturated with the solution. The etching process should be continued until there is a clear definition of the structure in the weld.

QW-472.3 Iodine and Potassium Iodide. One part of powdered iodine (solid form), two parts of powdered potassium iodide, and ten parts of water, all by weight. The solution should be used at room temperature, and brushed on the surface to be etched until there is a clear definition or outline of the weld.

QW-472.4 Nitric Acid. One part of nitric acid and three parts of water, by volume.

CAUTION: Always pour the acid into the water. Nitric acid causes bad stains and severe burns.

The solution may be used at room temperature and applied to the surface to be etched with a glass stirring rod. The specimens may also be placed in a boiling solution of the acid, but the work should be done in a well-ventilated room. The etching process should be continued for a sufficient period of time to reveal all lack of soundness that might exist at the cross-sectional surfaces of the weld.

## QW-473 For Nonferrous Metals

The following etching reagents and directions for their use are suggested for revealing the macrostructure.

## QW-473.1 Aluminum and Aluminum-Base Alloys

| Hydrochloric acid (concentrated) | 15 ml |
| :--- | :--- |
| Hydrofluoric acid (48\%) | 10 ml |
| Water | 85 ml |

This solution is to be used at room temperature, and etching is accomplished by either swabbing or immersing the specimen.

QW-473.2 For Copper and Copper-Base Alloys: Cold Concentrated Nitric Acid. Etching is accomplished by either flooding or immersing the specimen for several seconds under a hood. After rinsing with a flood of water, the process is repeated with a 50-50 solution of concentrated nitric acid and water.

In the case of the silicon bronze alloys, it may be necessary to swab the surface to remove a white $\left(\mathrm{SiO}_{2}\right)$ deposit.

QW-473.3 For Nickel and Nickel-Base Alloys

| Material | Formula |  |
| :---: | :---: | :---: |
| Nickel <br> Low Carbon Nickel <br> Nickel-Copper (400) <br> Nickel-Chromium-Iron <br> (600 and 800) | Nitric Acid or Lepito's Etch Nitric Acid or Lepito's Etch Nitric Acid or Lepito's Etch Aqua Regia or Lepito's Etch |  |
| MAKEUP OF FORMULAS FOR AQUA REGIA AND LEPITO'S ETCH |  |  |
|  | $\begin{gathered} \text { Aqua } \\ \text { Regia } \\ {[(1),(3)]} \end{gathered}$ | $\begin{aligned} & \text { Lepito's } \\ & \text { Etch } \\ & {[(2),(3)]} \end{aligned}$ |
| Nitric Acid, Concentrated $-\mathrm{HNO}_{3}$ | 1 part | 3 ml |
| HCL | 2 parts | 10 ml |
| Ammonium Sulfate $\left(\mathrm{NH}_{4}\right)_{2}\left(\mathrm{SO}_{4}\right)$ |  | 1.5 g |
| Ferric Chloride - $\mathrm{FeCl}_{3}$ | , | 2.5 g |
| Water | . . | 7.5 ml |

NOTES:
(1) Warm the parts for faster action.
(2) Mix solution as follows:
(a) Dissolve $\left(\mathrm{NH}_{4}\right)_{2}\left(\mathrm{SO}_{4}\right)$ in $\mathrm{H}_{2} \mathrm{O}$.
(b) Dissolve powdered $\mathrm{FeCl}_{3}$ in warm HCl .
(c) Mix (a) and (b) above and add $\mathrm{HNO}_{3}$.
(3) Etching is accomplished by either swabbing or immersing the specimen.

## QW-473.4 For Titanium

|  | Kroll's Etch |  |
| :--- | :---: | :---: |
|  | Keller's Etch |  |
| Hydrofluoric acid $(48 \%)$ |  |  |
| Nitric acid (concentrated) | 2 to 6 ml |  |
| Hydrochloric Acid | $\ldots$ | $2 \frac{1}{2} \mathrm{ml}$ |
| $\quad$ (concentrated) |  | $1 \frac{1}{2} \mathrm{ml}$ |
| Water | To make 100 ml | To make 100 ml |

## QW-473.5 For Zirconium

| Hydrofluoric acid | 3 ml |
| :--- | ---: |
| Nitric acid (concentrated) | 22 ml |
| Water | 22 ml |

Apply by swab and rinse in cold water.
These are general purpose etchants which are applied at room temperature by swabbing or immersion of the specimen.

## QW-490 DEFINITIONS <br> QW/QB-491 General

Definitions of the more common terms relating to welding/brazing are defined in QW/QB-492. These are identical to, or substantially in agreement with the definitions of the American Welding Society document, AWS A3.0, Standard Welding Terms and Definitions. There are terms listed that are specific to ASME Section IX and are not presently defined in AWS A3.0. Several definitions have been modified slightly from A3.0 so as to better define the context/intent as used in ASME Section IX.

## 04 QW/QB-492 Definitions

arc seam weld - a seam weld made by an arc welding process
arc spot weld - a spot weld made by an arc welding process
arc strike - any inadvertent discontinuity resulting from an arc, consisting of any localized remelted metal, heataffected metal, or change in the surface profile of any metal object. The arc may be caused by arc welding electrodes, magnetic inspection prods, or frayed electrical cable.
arc welding - a group of welding processes wherein coalescence is produced by heating with an arc or arcs, with or without the application of pressure, and with or without the use of filler metal
as-brazed — adj. pertaining to the condition of brazements after brazing, prior to any subsequent thermal, mechanical, or chemical treatments
as-welded - adj. pertaining to the condition of weld metal, welded joints, and weldments after welding but prior to any subsequent thermal, mechanical, or chemical treatments
backgouging - the removal of weld metal and base metal from the weld root side of a welded joint to facilitate complete fusion and complete joint penetration upon subsequent welding from that side
backhand welding - a welding technique in which the welding torch or gun is directed opposite to the progress of welding
backing - a material placed at the root of a weld joint for the purpose of supporting molten weld metal so as to facilitate complete joint penetration. The material may or may not fuse into the joint. See retainer.
backing gas - a gas, such as argon, helium, nitrogen, or reactive gas, which is employed to exclude oxygen from the root side (opposite from the welding side) of weld joints
base metal - the metal or alloy that is welded, brazed, or cut
bond line (brazing and thermal spraying) - the cross section of the interface between a braze or thermal spray deposit and the substrate
braze - a joint produced by heating an assembly to suitable temperatures and by using a filler metal having a liquidus above $840^{\circ} \mathrm{F}$ and below the solidus of the base materials. The filler metal is distributed between the closely fitted surfaces of the joint by capillary action.
brazer - one who performs a manual or semiautomatic brazing operation
brazing - a group of metal joining processes which produces coalescence of materials by heating them to a suitable temperature, and by using a filler metal having a liquidus above $840^{\circ} \mathrm{F}\left(450^{\circ} \mathrm{C}\right)$ and below the solidus of the base materials. The filler metal is distributed between the closely fitted surfaces of the joint by capillary action.
brazing, automatic - brazing with equipment which performs the brazing operation without constant observation and adjustment by a brazing operator. The equipment may or may not perform the loading and unloading of the work.
brazing, block $(B B)$ - a brazing process that uses heat from heated blocks applied to the joint. This is an obsolete or seldom used process.
brazing, dip $(D B)$ - a brazing process in which the heat required is furnished by a molten chemical or metal bath. When a molten chemical bath is used, the bath may act as a flux; when a molten metal bath is used, the bath provides the filler metal.
brazing, furnace (FB) - a brazing process in which the workpieces are placed in a furnace and heated to the brazing temperature
brazing, induction (IB) - a brazing process that uses heat from the resistance of the workpieces to induced electric current
brazing, machine - brazing with equipment which performs the brazing operation under the constant observation and control of a brazing operator. The equipment may or may not perform the loading and unloading of the work.
brazing, manual - a brazing operation performed and controlled completely by hand. See automatic brazing and machine brazing.
brazing, resistance $(R B)$ - a brazing process that uses heat from the resistance to electric current flow in a circuit of which the workpieces are a part
brazing, semiautomatic - brazing with equipment which controls only the brazing filler metal feed. The advance of the brazing is manually controlled.
brazing, torch (TB) - a brazing process that uses heat from a fuel gas flame
brazing operator - one who operates machine or automatic brazing equipment
brazing temperature - the temperature to which the base metal(s) is heated to enable the filler metal to wet the base metal(s) and form a brazed joint
brazing temperature range - the temperature range within which brazing can be conducted
build-up of base metal/restoration of base metal thickness - this is the application of a weld material to a base metal so as to restore the design thickness and/or structural integrity. This build-up may be with a chemistry different from the base metal chemistry which has been qualified via a standard butt welded test coupon. Also, may be called base metal repair or buildup.
butt joint - a joint between two members aligned approximately in the same plane
buttering - the addition of material, by welding, on one or both faces of a joint, prior to the preparation of the
joint for final welding, for the purpose of providing a suitable transition weld deposit for the subsequent completion of the joint
clad brazing sheet - a metal sheet on which one or both sides are clad with brazing filler metal
coalescence - the growing together or growth into one body of the materials being joined
complete fusion - fusion which has occurred over the entire base material surfaces intended for welding, and between all layers and beads
composite - a material consisting of two or more discrete materials with each material retaining its physical identity
consumable insert - filler metal that is placed at the joint root before welding, and is intended to be completely fused into the root to become part of the weld
contact tube - a device which transfers current to a continuous electrode
corner joint - a joint between two members located approximately at right angles to each other in the form of an $L$
coupon - see test coupon
crack - a fracture-type discontinuity characterized by a sharp tip and high ratio of length and width to opening displacement
defect - a discontinuity or discontinuities that by nature or accumulated effect (for example, total crack length) render a part or product unable to meet minimum applicable acceptance standards or specifications. This term designates rejectability. See also discontinuity and flaw.
direct current electrode negative ( $D C E N$ ) - the arrangement of direct current arc welding leads in which the electrode is the negative pole and the workpiece is the positive pole of the welding arc
direct current electrode positive ( $D C E P$ ) - the arrangement of direct current arc welding leads in which the electrode is the positive pole and the workpiece is the negative pole of the welding arc
discontinuity - an interruption of the typical structure of a material, such as a lack of homogeneity in its mechanical, metallurgical, or physical characteristics. A discontinuity is not necessarily a defect. See also defect and flaw.
double-welded joint - a joint that is welded from both sides
double-welded lap joint - a lap joint in which the overlapped edges of the members to be joined are welded along the edges of both members
$d$ well - the time during which the energy source pauses at any point in each oscillation
electrode, arc welding - a component of the welding circuit through which current is conducted
electrode, bare - a filler metal electrode that has been produced as a wire, strip, or bar with no coating or covering other than that incidental to its manufacture or preservation
electrode, carbon - a nonfiller material electrode used in arc welding and cutting, consisting of a carbon or graphite rod, which may be coated with copper or other materials
electrode, composite - a generic term of multicomponent filler metal electrodes in various physical forms, such as stranded wires, tubes, and covered electrodes
electrode, covered - a composite filler metal electrode consisting of a core of a bare electrode or metal-cored electrode to which a covering sufficient to provide a slag layer on the weld metal has been applied. The covering may contain materials providing such functions as shielding from the atmosphere, deoxidation, and arc stabilization, and can serve as a source of metallic additions to the weld.
electrode, electroslag welding - a filler metal component of the welding circuit through which current is conducted between the electrode guiding member and the molten slag

NOTE: Bare electrodes and composite electrodes as defined under arc welding electrode are used for electroslag welding. A consumable guide may also be used as part of the electroslag welding electrode system.
electrode, emissive - a filler metal electrode consisting of a core of a bare electrode or a composite electrode to which a very light coating has been applied to produce a stable arc
electrode, flux-cored - a composite filler metal electrode consisting of a metal tube or other hollow configuration containing ingredients to provide such functions as shielding atmosphere, deoxidation, arc stabilization, and slag formation. Alloying materials may be included in the core. External shielding may or may not be used.
electrode, lightly coated - a filler metal electrode consisting of a metal wire with a light coating applied subsequent to the drawing operation, primarily for stabilizing the arc
electrode, metal - a filler or nonfiller metal electrode used in arc welding and cutting that consists of a metal wire or rod that has been manufactured by any method and that is either bare or covered
electrode, metal-cored - a composite filler metal electrode consisting of a metal tube or other hollow configuration containing alloying ingredients. Minor amounts of ingredients providing such functions as arc stabilization and fluxing of oxides may be included. External shielding gas may or may not be used.
electrode, resistance welding - the part of a resistance welding machine through which the welding current and, in most cases, force are applied directly to the workpiece. The electrode may be in the form of a rotating wheel, rotating roll, bar, cylinder, plate, clamp, chuck, or modification thereof.
electrode, stranded - a composite filler metal electrode consisting of stranded wires which may mechanically enclose materials to improve properties, stabilize the arc, or provide shielding
electrode, tungsten - a nonfiller metal electrode used in arc welding, arc cutting, and plasma spraying, made principally of tungsten
face feed - the application of filler metal to the face side of a joint
ferrite number - an arbitrary, standardized value designating the ferrite content of an austenitic stainless steel weld metal. It should be used in place of percent ferrite or volume percent ferrite on a direct one-to-one replacement basis. See the latest edition of AWS A4.2, Standard Procedures for Calibrating Magnetic Instruments to Measure the Delta Ferrite Content of Austenitic Stainless Steel Weld Metal.
filler metal - the metal or alloy to be added in making a welded, brazed, or soldered joint
filler metal, brazing - the metal or alloy used as a filler metal in brazing, which has a liquidus above $840^{\circ} \mathrm{F}$ $\left(450^{\circ} \mathrm{C}\right)$ and below the solidus of the base metal
filler metal, powder - filler metal in particle form
filler metal, supplemental - in electroslag welding or in a welding process in which there is an arc between one or more consumable electrodes and the workpiece, a powder, solid, or composite material that is introduced into the weld other than the consumable electrode(s)
fillet weld - a weld of approximately triangular cross section joining two surfaces approximately at right angles
to each other in a lap joint, tee joint, or corner joint
flaw - an undesirable discontinuity. See also defect.
flux (welding/brazing) - a material used to dissolve, prevent, or facilitate the removal of oxides or other undesirable surface substances. It may act to stabilize the arc, shield the molten pool, and may or may not evolve shielding gas by decomposition.
flux, active (SAW) - a flux from which the amount of elements deposited in the weld metal is dependent upon the welding conditions, primarily arc voltage
flux, alloy (SAW) - a flux which provides alloying elements in the weld metal deposit
flux, neutral (SAW) - a flux which will not cause a significant change in the weld metal composition when there is a large change in the arc voltage
flux cover - metal bath dip brazing and dip soldering. A layer of molten flux over the molten filler metal bath.
forehand welding - a welding technique in which the welding torch or gun is directed toward the progress of welding
frequency - the completed number of cycles which the oscillating head makes in 1 min or other specified time increment
fuel gas - a gas such as acetylene, natural gas, hydrogen, propane, stabilized methylacetylene propadiene, and other fuels normally used with oxygen in one of the oxyfuel processes and for heating
fused spray deposit (thermal spraying) - a self-fluxing thermal spray deposit which is subsequently heated to coalescence within itself and with the substrate
fusion (fusion welding) - the melting together of filler metal and base metal, or of base metal only, to produce a weld
fusion face - a surface of the base metal that will be melted during welding
fusion line - a non-standard term for weld interface
gas backing - see backing gas
globular transfer (arc welding) - a type of metal transfer in which molten filler metal is transferred across the arc in large droplets
groove weld - a weld made in a groove formed within a single member or in the groove between two members
to be joined. The standard types of groove weld are as follows:
square groove weld
single-Vee groove weld
single-bevel groove weld
single-U groove weld
single-J groove weld
single-flare-bevel groove weld
single-flare-Vee groove weld
double-Vee groove weld
double-bevel groove weld
double-U groove weld
double-J groove weld
double-flare-bevel groove weld
double-flare-Vee groove weld
heat-affected zone - that portion of the base metal which has not been melted, but whose mechanical properties or microstructures have been altered by the heat of welding or cutting
interpass temperature - the highest temperature in the weld joint immediately prior to welding, or in the case of multiple pass welds, the highest temperature in the section of the previously deposited weld metal, immediately before the next pass is started
joint - the junction of members or the edges of members which are to be joined or have been joined
joint penetration - the distance the weld metal extends from the weld face into a joint, exclusive of weld reinforcement
keyhole welding - a technique in which a concentrated heat source penetrates partially or completely through a workpiece, forming a hole (keyhole) at the leading edge of the weld pool. As the heat source progresses, the molten metal fills in behind the hole to form the weld bead.
lap or overlap - the distance measured between the edges of two plates when overlapping to form the joint
lap joint - a joint between two overlapping members in parallel planes
lower transformation temperature - the temperature at which austenite begins to form during heating
melt-in - a technique of welding in which the intensity of a concentrated heat source is so adjusted that a weld pass can be produced from filler metal added to the leading edge of the molten weld metal
oscillation - for a machine or automatic process, an alternating motion relative to the direction of travel of
welding, brazing, or thermal spray device. See also weave bead.
overlay - a non-standard term, used in Section IX, for surfacing. See hard-facing and corrosion-resistant overlay.
overlay, corrosion-resistant weld metal - deposition of one or more layers of weld metal to the surface of a base material in an effort to improve the corrosion resistance properties of the surface. This would be applied at a level above the minimum design thickness as a nonstructural component of the overall wall thickness.
overlay, hard-facing weld metal - deposition of one or more layers of weld metal to the surface of a material in an effort to improve the wear resistance properties of the surface. This would be applied at a level above the minimum design thickness as a nonstructural component of the overall wall thickness.
pass - a single progression of a welding or surfacing operation along a joint, weld deposit, or substrate. The result of a pass is a weld bead or layer.
pass, cover - a final or cap pass(es) on the face of a weld
pass, wash - pass to correct minor surface aberrations and/or prepare the surface for nondestructive testing
peel test - a destructive method of testing that mechanically separates a lap joint by peeling
peening - the mechanical working of metals using impact blows
performance qualification - the demonstration of a welder's or welding operator's ability to produce welds meeting prescribed standards
plug weld - a weld made in a circular, or other geometrically shaped hole (like a slot weld) in one member of a lap or tee joint, joining that member to the other. The walls of the hole may or may not be parallel, and the hole may be partially or completely filled with weld metal. (A fillet-welded hole or spot weld should not be construed as conforming to this definition.)
polarity, reverse - the arrangement of direct current arc welding leads with the work as the negative pole and the electrode as the positive pole of the welding arc; a synonym for direct current electrode positive
polarity, straight - the arrangement of direct current arc welding leads in which the work is the positive pole and the electrode is the negative pole of the welding arc; a
synonym for direct current electrode negative
postbraze heat treatment - any heat treatment subsequent to brazing
postheating - the application of heat to an assembly after welding, brazing, soldering, thermal spraying, or thermal cutting
postweld heat treatment - any heat treatment subsequent to welding
postweld hydrogen bakeout - holding a completed or partially completed weld at elevated temperature below $800^{\circ} \mathrm{F}\left(425^{\circ} \mathrm{C}\right)$ for the purpose of allowing hydrogen diffusion from the weld
powder - see filler metal, powder
preheat maintenance - practice of maintaining the minimum specified preheat temperature, or some specified higher temperature for some required time interval after welding or thermal spraying is finished or until post weld heat treatment is initiated
preheat temperature - the minimum temperature in the weld joint preparation immediately prior to the welding; or in the case of multiple pass welds, the minimum temperature in the section of the previously deposited weld metal, immediately prior to welding
preheating - the application of heat to the base metal immediately before a welding or cutting operation to achieve a specified minimum preheat temperature
pulsed power welding - any arc welding method in which the power is cyclically programmed to pulse so that effective but short duration values of a parameter can be utilized. Such short duration values are significantly different from the average value of the parameter. Equivalent terms are pulsed voltage or pulsed current welding. See also pulsed spray welding.
pulsed spray welding - an arc welding process variation in which the current is pulsed to utilize the advantages of the spray mode of metal transfer at average currents equal to or less than the globular to spray transition current
rabbet joint - typical design is indicated in figures QB462.1(c), QB-462.4, QB-463.1(c), and QB-463.2(a)
retainer - nonconsumable material, metallic or nonmetallic, which is used to contain or shape molten weld metal. See backing.
seal weld - any weld designed primarily to provide a specific degree of tightness against leakage
seam weld - a continuous weld made between or upon overlapping members in which coalescence may start and occur on the faying surfaces, or may have proceeded from the surface of one member. The continuous weld may consist of a single weld bead or a series of overlapping spot welds. See resistance welding.
short-circuiting transfer (gas metal-arc welding) — metal transfer in which molten metal from a consumable electrode is deposited during repeated short circuits. See also globular transfer and spray transfer.
single-welded joint - a joint welded from one side only
single-welded lap joint - a lap joint in which the overlapped edges of the members to be joined are welded along the edge of one member only
slag inclusion - nonmetallic solid material entrapped in weld metal or between weld metal and base metal
specimen - refer to test specimen
spot weld - a weld made between or upon overlapping members in which coalescence may start and occur on the faying surfaces or may proceed from the outer surface of one member. The weld cross section (plan view) is approximately circular.
spray-fuse - a thermal spraying technique in which the deposit is reheated to fuse the particles and form a metallurgical bond with the substrate
spray transfer (arc welding) - metal transfer in which molten metal from a consumable electrode is propelled axially across the arc in small droplets
stringer bead - a weld bead formed without appreciable weaving
surface temper bead reinforcing layer - a subset of temper bead welding in which one or more layers of weld metal are applied on or above the surface layers of a component and are used to modify the properties of previously deposited weld metal or the heat-affected zone. Surface layer may cover a surface or only the perimeter of the weld.
surfacing - the application by welding, brazing, or thermal spraying of a layer(s) of material to a surface to obtain desired properties or dimensions, as opposed to making a joint
tee joint $(T)$ - a joint between two members located approximately at right angles to each other in the form of a T
temper bead welding - a weld bead placed at a specific location in or at the surface of a weld for the purpose of affecting the metallurgical properties of the heat-affected zone or previously deposited weld metal. The bead may be above, flush with, or below the surrounding base metal surface. If above the base metal surface, the beads may cover all or only part of the weld deposit and may or may not be removed following welding.
test coupon - a weld or braze assembly for procedure or performance qualification testing. The coupon may be any product from plate, pipe, tube, etc., and may be a fillet weld, overlay, deposited weld metal, etc.
test specimen - a sample of a test coupon for specific test. The specimen may be a bend test, tension test, impact test, chemical analysis, macrotest, etc. A specimen may be a complete test coupon, for example, in radiographic testing or small diameter pipe tension testing.
thermal cutting (TC) - a group of cutting processes that severs or removes metal by localized melting, burning, or vaporizing of the workpieces
throat, actual (of fillet) - the shortest distance from the root of a fillet weld to its face
throat, effective (of fillet) - the minimum distance from the fillet face, minus any convexity, to the weld root. In the case of fillet welds combined with a groove weld, the weld root of the groove weld shall be used.
throat, theoretical (of fillet) - the distance from the beginning of the joint root perpendicular to the hypotenuse of the largest right triangle that can be inscribed within the cross-section of a fillet weld. This dimension is based on the assumption that the root opening is equal to zero.
undercut - a groove melted into the base metal adjacent to the weld toe or weld root and left unfilled by weld metal
upper transformation temperature - the temperature at which transformation of the ferrite to austenite is completed during heating
usability - a measure of the relative ease of application of a filler metal to make a sound weld or braze joint
weave bead - for a manual or semiautomatic process, a weld bead formed using weaving. See also oscillation.
weaving - a welding technique in which the energy source is oscillated transversely as it progresses along the weld path
weld - a localized coalescence of metals or nonmetals produced either by heating the materials to the welding
temperature, with or without the application of pressure, or by the application of pressure alone and with or without the use of filler material
weld, autogenous - a fusion weld made without filler metal
weld bead - a weld deposit resulting from a pass. See stringer bead and weave bead.
weld face - the exposed surface of a weld on the side from which welding was done
weld interface - the interface between the weld metal and base metal in a fusion weld
weld metal - metal in a fusion weld consisting of that portion of the base metal and filler metal melted during welding
weld reinforcement - weld metal on the face or root of a groove weld in excess of the metal necessary for the specified weld size
weld size: groove welds - the depth of chamfering plus any penetration beyond the chamfering, resulting in the strength carrying dimension of the weld
weld size: for equal leg fillet welds - the leg lengths of the largest isosceles right triangle which can be inscribed within the fillet weld cross section
weld size: for unequal leg fillet welds - the leg lengths of the largest right triangle which can be inscribed within the fillet weld cross section
welder - one who performs manual or semiautomatic welding
welding, arc stud (SW) - an arc welding process that uses an arc between a metal stud, or similar part, and the other workpiece. The process is used without filler metal, with or without shielding gas or flux, with or without partial shielding from a ceramic or graphite ferrule surrounding the stud, and with the application of pressure after the faying surfaces are sufficiently heated.
welding, automatic - welding with equipment which performs the welding operation without adjustment of the controls by a welding operator. The equipment may or may not perform the loading and unloading of the work. See machine welding.
welding, consumable guide electroslag - an electroslag welding process variation in which filler metal is supplied by an electrode and its guiding member
welding, electrogas ( $E G W$ ) - an arc welding process that uses an arc between a continuous filler metal electrode and the weld pool, employing approximately vertical welding progression with retainers to confine the weld metal. The process is used with or without an externally supplied shielding gas and without the application of pressure. Shielding for use with solid or metal-cored electrodes is obtained from a gas or gas mixture. Shielding for use with flux-cored electrodes may or may not be obtained from an externally supplied gas or gas mixture.
welding, electron beam $(E B W)$ - a welding process that produces coalescence with a concentrated beam composed primarily of high velocity electrons, impinging on the joint. The process is used without shielding gas and without the application of pressure.
welding, electroslag (ESW) - a welding process producing coalescence of metals with molten slag which melts the filler metal and the surfaces of the work to be welded. The molten weld pool is shielded by this slag which moves along the full cross section of the joint as welding progresses. The process is initiated by an arc which heats the slag. The arc is then extinguished and the conductive slag is maintained in a molten condition by its resistance to electric current passing between the electrode and the work. See electroslag welding electrode and consumable guide electroslag welding.
welding, flux-cored arc (FCAW) - a gas metal-arc welding process that uses an arc between a continuous filler metal electrode and the weld pool. The process is used with shielding gas from a flux contained within the tubular electrode, with or without additional shielding from an externally supplied gas, and without the application of pressure.
welding, friction (FRW) - a solid state welding process that produces a weld under compressive force contact of workpieces rotating or moving relative to one another to produce heat and plastically displace material from the faying surfaces
welding, friction, inertia and continuous drive - processes and types of friction welding (solid state welding process) wherein coalescence is produced after heating is obtained from mechanically induced sliding motion between rubbing surfaces held together under pressure. Inertia welding utilizes all of the kinetic energy stored in a revolving flywheel spindle system. Continuous drive friction welding utilizes the energy provided by a continuous drive source such as an electric or hydraulic motor.
welding, gas metal-arc (GMAW) - an arc welding process that uses an arc between a continuous filler metal
electrode and the weld pool. The process is used with shielding from an externally supplied gas and without the application of pressure.
welding, gas metal-arc, pulsed arc (GMAW-P) - a variation of the gas metal-arc welding process in which the current is pulsed. See also pulsed power welding.
welding, gas metal-arc, short-circuiting arc (GMAW$S)$ - a variation of the gas metal-arc welding process in which the consumable electrode is deposited during repeated short circuits. See also short-circuiting transfer.
welding, gas tungsten-arc (GTAW) - an arc welding process which produces coalescence of metals by heating them with an arc between a tungsten (nonconsumable) electrode and the work. Shielding is obtained from a gas or gas mixture. Pressure may or may not be used and filler metal may or may not be used. (This process has sometimes been called TIG welding, a nonpreferred term.)
welding, gas tungsten-arc, pulsed arc (GTAW-P) - a variation of the gas tungsten-arc welding process in which the current is pulsed. See also pulsed power welding.
welding, induction (IW) - a welding process that produces coalescence of metals by the heat obtained from resistance of the workpieces to the flow of induced high frequency welding current with or without the application of pressure. The effect of the high-frequency welding current is to concentrate the welding heat at the desired location.
welding, laser beam (LBW) - a welding process which produces coalescence of materials with the heat obtained from the application of a concentrated coherent light beam impinging upon the members to be joined
welding, machine - welding with equipment that has controls that are manually adjusted by the welding operator in response to visual observation of the welding, with the torch, gun, or electrode holder held by a mechanical device. See welding, automatic.
welding, manual - welding wherein the entire welding operation is performed and controlled by hand
welding, operator - one who operates machine or automatic welding equipment
welding, oxyfuel gas (OFW) - a group of welding processes which produces coalescence by heating materials with an oxyfuel gas flame or flames, with or without the application of pressure, and with or without the use of filler metal
welding, plasma-arc (PAW) - an arc welding process which produces coalescence of metals by heating them with a constricted arc between an electrode and the workpiece (transferred arc), or the electrode and the constricting nozzle (nontransferred arc). Shielding is obtained from the hot, ionized gas issuing from the torch orifice which may be supplemented by an auxiliary source of shielding gas. Shielding gas may be an inert gas or a mixture of gases. Pressure may or may not be used, and filler metal may or may not be supplied.
welding, projection $(P W)$ - a resistance welding process that produces coalescence by the heat obtained from the resistance of the flow of welding current. The resulting welds are localized at predetermined points by projections, embossments, or intersections. The metals to be joined lap over each other.
welding, resistance ( $R W$ ) - a group of welding processes that produces coalescence of the faying surfaces with the heat obtained from resistance of the workpieces to the flow of the welding current in a circuit of which the workpieces are a part, and by the application of pressure welding, resistance seam (RSEW) - a resistance welding process that produces a weld at the faying surfaces of overlapped parts progressively along a length of a joint. The weld may be made with overlapping weld nuggets, a continuous weld nugget, or by forging the joint as it is heated to the welding temperature by resistance to the flow of the welding current.
welding, resistance spot (RSW) - a resistance welding process that produces a weld at the faying surfaces of a joint by the heat obtained from resistance to the flow of welding current through the workpieces from electrodes that serve to concentrate the welding current and pressure at the weld area
welding, resistance stud - a resistance welding process wherein coalescence is produced by the heat obtained from resistance to electric current at the interface between the stud and the workpiece, until the surfaces to be joined are properly heated, when they are brought together under pressure
welding, semiautomatic arc - arc welding with equipment which controls only the filler metal feed. The advance of the welding is manually controlled.
welding, shielded metal-arc (SMAW) - an arc welding process with an arc between a covered electrode and the weld pool. The process is used with shielding from the decomposition of the electrode covering, without the application of pressure, and with filler metal from the electrode
welding, stud - a general term for the joining of a metal stud or similar part to a workpiece. Welding may be accomplished by arc, resistance, friction, or other suitable process with or without external gas shielding.
welding, submerged-arc (SAW) - an arc welding process that uses an arc or arcs between a bare metal electrode or electrodes and the weld pool. The are and molten metal are shielded by a blanket of granular flux on the
workpieces. The process is used without pressure and with filler metal from the electrode and sometimes from a supplemental source (welding rod, flux, or metal granules).
weldment - an assembly whose constituent parts are joined by welding, or parts which contain weld metal overlay

# ARTICLE V STANDARD WELDING PROCEDURE SPECIFICATIONS (SWPSs) 

## QW-500 GENERAL

The SWPSs listed in Appendix E are acceptable for construction in which the requirements of the ASME Boiler and Pressure Vessel Code, Section IX are specified. Any requirements of the applicable Construction Code Section regarding SWPS take precedence over the requirements of Section IX. These SWPSs are not permitted for construction where impact testing of the WPS is required by the Construction Code.

Only SWPSs (including edition) that have been accepted in Appendix E within the 1998 Edition or any later edition of Section IX may be used in accordance with this Article. Adoption of SWPSs (including edition) shall be in accordance with the current edition (see Foreword) and addenda of Section IX.

## QW-510 ADOPTION OF SWPSs

Prior to use, the manufacturer or contractor that will be responsible for and provide operational control over production welding shall comply with the following for each SWPS that it intends to use, except as noted in QW-520.
(a) Enter the name of the manufacturer or contractor on the SWPS.
(b) An employee of that manufacturer or contractor shall sign and date the SWPS.
(c) The applicable Code Section(s) (Section VIII, B31.1, etc.) and/or any other fabrication document (contract, specification, etc.) that must be followed during welding shall be listed on the SWPS.
(d) The manufacturer or contractor shall weld and test one groove weld test coupon following that SWPS. The following information shall be recorded:
(1) the specification, type, and grade of the base metal welded
(2) groove design
(3) initial cleaning method
(4) presence or absence of backing
(5) The ASME or AWS specification and AWS classification of electrode or filler metal used and manufacturer's trade name
(6) size and classification of tungsten electrode for GTAW
(7) size of consumable electrode or filler metal
(8) shielding gas and flow rate for GTAW and GMAW
(9) preheat temperature
(10) position of the groove weld and, if applicable, the progression
(11) if more than one process or electrode type is used, the approximate weld metal deposit thickness for each process or electrode type
(12) maximum interpass temperature
(13) post weld heat treatment used, including holding time and temperature range
(14) visual inspection and mechanical testing results
(15) the results of radiographic examination when permitted as an alternative to mechanical testing by QW-304
(e) The coupon shall be visually examined in accordance with QW-302.4 and mechanically tested in accordance with QW-302.1 or radiographically examined in accordance with QW-302.2. If visual examination, radiographic examination, or any test specimen fails to meet the required acceptance criteria, the test coupon shall be considered as failed and a new test coupon shall be welded before the organization may use the SWPS.

## QW-511 Use of Demonstrated SWPSs

Code Sections or fabrication documents that are required to be referenced by QW-510(c) may be added or deleted from a demonstrated SWPS without further demonstrations.

## QW-520 USE OF SWPSs WITHOUT DISCRETE DEMONSTRATION

Once an SWPS has been demonstrated, additional SWPSs that are similar to the SWPS that was demonstrated may be used without further demonstration. Such additional SWPSs shall be compared to the SWPS that was used for the demonstration, and the following limitations shall not be exceeded:
(a) a change in the welding process.
(b) a change in the P - or S-Number.
(c) a change from the as-welded condition to the heattreated condition. This limitation also applies for SWPSs that allow use in both conditions (e.g., SWPS B2.1-021 allows production welding with or without heat treatment; if the demonstration was performed without heat treatment, production welding with heat treatment is not permitted). Once heat treatment has been demonstrated for any SWPS, this limitation no longer applies.
(d) a change from a gas-shielded flux-cored wire or solid wire to a self-shielded flux-cored wire or vice versa.
(e) a change from spray, globular, or pulsed transfer mode to short-circuiting transfer mode or vice-versa.
$(f)$ a change in the F-Number of the welding electrode.
$(g)$ the addition of preheat above ambient temperature.
$(h)$ a change from an SWPS that is identified as for sheet metal to one that is not and vice versa.

## QW-530 FORMS

A suggested Form QW-485 for documenting the welding conditions and test results of the demonstration is provided in Nonmandatory Appendix B.

## QW-540 PRODUCTION USE OF SWPSs

As with any WPS, welding that is done following an SWPS shall be done in strict accordance with the SWPS.

In addition, the following conditions apply to the use of SWPSs:
(a) The manufacturer or contractor may not deviate from the welding conditions specified on the SWPS.
(b) SWPSs may not be supplemented with PQRs or revised in any manner except for reference to the applicable Code Section or other fabrication documents as provided by QW-511.
(c) Only the welding processes shown on an SWPS shall be used in given production joint. When a multiprocess SWPS is selected, the processes shown on the SWPS shall be used in the order and manner specified on the SWPS.
(d) SWPSs shall not be used in the same production joint together with WPSs qualified by the manufacturer or contractor.
(e) The manufacturer or contractor may supplement an SWPS by attaching additional instructions to provide the welder with further direction for making production welds to Code or other requirements. When SWPSs are supplemented with instructions that address any condition shown on the SWPS, such instructions shall be within the limits of the SWPS. For example, when an SWPS permits use of several electrode sizes, supplemental instructions may direct the welder to use only one electrode size out of those permitted by the SWPS; however, the supplemental instructions may not permit the welder to use a size other than one or more of those permitted by the SWPS.
(f) SWPSs may not be used until the demonstration of QW-510 has been satisfactorily welded, tested, and certified.
$(g)$ The identification number of the Supporting Demonstration shall be noted on each SWPS that it supports prior to using the SWPS.
(h) The certified Supporting Demonstration Record shall be available for review by Authorized Inspector.

## PART QB BRAZING

## ARTICLE XI BRAZING GENERAL REQUIREMENTS

## QB-100 GENERAL

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures that they employ in welding and brazing according to the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. It is divided into two parts: Part QW gives requirements for welding and Part QB contains requirements for brazing.

QB-100.1 The purpose of the Brazing Procedure Specification (BPS) and Procedure Qualification Record (PQR) is to determine that the brazement proposed for construction is capable of providing the required properties for its intended application. It is presupposed that the brazer or brazing operator performing the brazing procedure qualification test is a skilled workman. That is, the brazing procedure qualification test establishes the properties of the brazement, not the skill of the brazer or brazing operator. Briefly, a BPS lists the variables, both essential and nonessential, and the acceptable ranges of these variables when using the BPS. The BPS is intended to provide direction for the brazer or brazing operator. The PQR lists what was used in qualifying the BPS and the test results.

QB-100.2 In performance qualification, the basic criterion established for brazer qualification is to determine the brazer's ability to make a sound brazed joint. The purpose of the performance qualification test for the brazing operator is to determine the operator's mechanical ability to operate the brazing equipment.

QB-100.3 Brazing Procedure Specifications (BPS) written and qualified in accordance with the rules of this Section, and brazers and operators of automatic and machine brazing equipment also qualified in accordance
with these rules may be used in any construction built to the requirements of the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.
However, other Sections of the Code state the conditions under which Section IX requirements are mandatory, in whole or in part, and give additional requirements. The reader is advised to take these provisions into consideration when using this Section.

Brazing Procedure Specifications, Procedure Qualification Records, and Brazer or Brazing Operator Performance Qualifications made in accordance with the requirements of the 1962 Edition or any later Edition of Section IX may be used in any construction built to the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

Brazing Procedure Specifications, Procedure Qualification Records, and Brazer or Brazing Operator Performance Qualifications made in accordance with the requirements of the Editions of Section IX prior to 1962, in which all of the requirements of the 1962 Edition or later Editions are met, may also be used.
Brazing Procedure Specifications and Brazer/Brazing Operator Performance Qualification Records meeting the above requirements do not need to be amended to include any variables required by later Editions and Addenda.
Qualification of new Brazing Procedure Specifications or Brazers/Brazing Operators and requalification of existing Brazing Procedure Specifications or Brazers/Brazing Operators shall be in accordance with the current Edition (see Foreword) and Addenda of Section IX.

QB-101 Scope
The rules in this Section apply to the preparation of Brazing Procedure Specifications, and the qualification
of brazing procedures, brazers, and brazing operators for all types of manual and machine brazing processes permitted in this Section. These rules may also be applied, insofar as they are applicable, to other manual or machine brazing processes, permitted in other Sections.

## QB-102 Terms and Definitions

Some of the more common terms relating to brazing are defined in QW/QB-492. These are in substantial agreement with the definitions of the American Welding Society given in its document, A3.0-89, Standard Welding Terms and Definitions.

Wherever the word pipe is designated, tubes shall also be applicable.

## QB-103 Responsibility

QB-103.1 Brazing. Each manufacturer ${ }^{1}$ or contractor ${ }^{1}$ is responsible for the brazing done by his organization, and shall conduct the tests required in this Section to qualify the brazing procedures he uses in the construction of the brazed assemblies built under this Code and the performance of brazers and brazing operators who apply these procedures.

QB-103.2 Records. Each manufacturer or contractor shall maintain a record of the results obtained in brazing procedure and brazer or brazing operator performance qualifications. These records shall be certified by the manufacturer or contractor and shall be accessible to the Authorized Inspector. Refer to recommended Forms in Nonmandatory Appendix B.

## QB-110 BRAZE ORIENTATION

The orientations of brazes with respect to planes of reference are classified in accordance with figure QB-461.1 into four positions ${ }^{2}$ (A, B, C, and D in column 1), based on the basic flow of brazing filler metal through joints. These positions are flat flow, vertical downflow, vertical upflow, and horizontal flow.

The maximum permitted angular deviation from the specified flow plane is $\pm 45$ deg.

## QB-120 TEST POSITIONS FOR LAP, BUTT, SCARF, OR RABBET JOINTS

Brazed joints may be made in test coupons oriented in any of the positions in figure QB-461.2 and as described

[^3]in the following paragraphs, except that angular deviation from the specified horizontal and vertical flow planes in accordance with column 1 of figure $\mathrm{QB}-461.2$ is permitted during brazing.

## QB-121 Flat-Flow Position

The test coupon joints in position suitable for applying brazing filler metal in rod, strip, or other suitable form under the flat-flow conditions are shown in illustrations (1) through (5) of Line A in figure QB-461.2. The maximum permitted angular deviation from the specified flow plane is $\pm 15$ deg.

## QB-122 Vertical-Downflow Position

The test coupon joints in a position suitable for applying brazing filler metal in rod, strip, or other suitable form under the vertical-downflow conditions are shown in illustrations (1) through (4) of Line B in figure QB-461.2. The brazing filler metal flows by capillary action with the aid of gravity downward into the joint. The maximum permitted angular deviation from the specified flow plane is $\pm 15 \mathrm{deg}$.

## QB-123 Vertical-Upflow Position

The test coupon joints in position suitable for applying brazing filler metal in rod, strip, or other suitable form under the vertical-upflow conditions are shown in illustrations (1) through (4) of Line C in figure QB-461.2. The brazing filler metal flows by capillary action through the joint. The maximum permitted angular deviation from the specified flow plane is $\pm 15 \mathrm{deg}$.

## QB-124 Horizontal-Flow Position

The test coupon joints in a position suitable for applying brazing filler metal in rod, strip, or other suitable form under the horizontal-flow conditions are shown in illustrations (1) and (2) of Line D of figure QB-461.2. The brazing filler metal flows horizontally by capillary action through the joint. The maximum permitted angular deviation from the specified flow plane is $\pm 15$ deg.

## QB-140 TYPES AND PURPOSES OF TESTS AND EXAMINATIONS <br> QB-141 Tests

Tests used in brazing procedure and performance qualifications are specified in QB-141.1 through QB-141.6.

QB-141.1 Tension Tests. Tension tests, as described in QB-150, are used to determine the ultimate strength
of brazed butt, scarf, lap, and rabbet joints.
QB-141.2 Guided-Bend Tests. Guided-bend tests, as described in QB-160, are used to determine the degree of soundness and ductility of butt and scarf joints.

QB-141.3 Peel Tests. Peel tests, as described in QB-170, are used to determine the quality of the bond and the amount of defects in lap joints.

QB-141.4 Sectioning Tests. Sectioning tests, i.e., the sectioning of test coupons, as described in QB-180, are used to determine the soundness of workmanship coupons or test specimens. Sectioning tests are also a substitute for the peel test when the peel test is impractical to perform, e.g., when the strength of brazing filler material is equal to or greater than the strength of the base metals.

QB-141.5 Workmanship Coupons. Workmanship coupons, as described in QB-182, are used to determine the soundness of joints other than the standard butt, scarf, lap, and rabbet joints.

QB-141.6 Visual Examination. Visual examination of brazed joints is used for estimating the soundness by external appearance, such as continuity of the brazing filler metal, size, contour, and wetting of fillet along the joint and, where appropriate, to determine if filler metal flowed through the joint from the side of application to the opposite side.

## QB-150 TENSION TESTS <br> QB-151 Specimens

Tension test specimens shall conform to one of the types illustrated in figures QB-462.1(a) through QB-462.1(f), and shall meet the requirements of QB-153.

QB-151.1 Reduced Section - Plate. Reduced-section specimens conforming to the requirements given in figures QB-462.1(a) and QB-462.1(c) may be used for tension tests on all thicknesses of plate. The specimens may be tested in a support fixture in substantial accordance with figure QB-462.1(f).
(a) For thicknesses up to and including 1 in . ( 25 mm ), a full thickness specimen shall be used for each required tension test.
(b) For plate thicknesses greater than 1 in . ( 25 mm ), full thickness specimens or multiple specimens may be used, provided QB-151.1(c) and QB-151.1(d) are complied with.
(c) When multiple specimens are used in lieu of full thickness specimens, each set shall represent a single tension test of the full plate thickness. Collectively, all of the specimens required to represent the full thickness
of the brazed joint at one location shall comprise a set.
(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QB-153.

QB-151.2 Reduced Section - Pipe. Reduced-section specimens conforming to the requirements given in figure QB-462.1(b) may be used for tension tests on all thicknesses of pipe or tube having an outside diameter greater than 3 in . 75 mm ). The specimens may be tested in a support fixture in substantial accordance with figure QB-462.1(f).
(a) For thicknesses up to and including 1 in. ( 25 mm ), a full thickness specimen shall be used for each required tension test.
(b) For pipe thicknesses greater than 1 in. ( 25 mm ), full thickness specimens or multiple specimens may be used, provided QB-151.2(c) and QB-151.2(d) are complied with.
(c) When multiple specimens are used in lieu of full thickness specimens, each set shall represent a single tension test of the full pipe thickness. Collectively, all of the specimens required to represent the full thickness of the brazed joint at one location shall comprise a set.
(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QB-153.

QB-151.3 Full-Section Specimens for Pipe. Tension specimens conforming to the dimensions given in figure QB-462.1(e) may be used for testing pipe with an outside diameter of 3 in . $(75 \mathrm{~mm})$ or less.

## QB-152 Tension Test Procedure

The tension test specimen shall be ruptured under tensile load. The tensile strength shall be computed by dividing the ultimate total load by the least cross-sectional area of the specimen as measured before the load is applied.

## QB-153 Acceptance Criteria - Tension Tests

QB-153.1 Tensile Strength. Minimum values for procedure qualification are provided under the column heading "Minimum Specified Tensile" of table QW/QB-422. In order to pass the tension test, the specimen shall have a tensile strength that is not less than:
(a) the specified minimum tensile strength of the base metal in the annealed condition; or
(b) the specified minimum tensile strength of the weaker of the two in the annealed condition, if base metals of different specified minimum tensile strengths are used; or
(c) if the specimen breaks in the base metal outside of the braze, the test shall be accepted as meeting the requirements, provided the strength is not more than $5 \%$ below the minimum specified tensile strength of the base metal in the annealed condition.
(d) the specified minimum tensile strength is for full thickness specimens including cladding for Aluminum Alclad materials (P-No. 104 and P-No. 105) less than $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$. For Aluminum Alclad materials $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm})$ and greater, the specified minimum tensile strength is for both full thickness specimens that include cladding and specimens taken from the core.

## QB-160 GUIDED-BEND TESTS <br> QB-161 Specimens

Guided-bend test specimens shall be prepared by cutting the test plate or pipe to form specimens of approximately rectangular cross section. The cut surfaces shall be designated the sides of the specimen. The other two surfaces shall be designated the first and second surfaces. The specimen thickness and bend radius are shown in figures QB-466.1, QB-466.2, and QB-466.3. Guidedbend specimens are of five types, depending on whether the axis of the joint is transverse or parallel to the longitudinal axis of the specimen, and which surface (first or second) is on the convex (outer) side of the bent specimen. The five types are defined as follows (QB-161.1 through QB-161.6).

QB-161.1 Transverse First Surface Bend. The joint is transverse to the longitudinal axis of the specimen, which is bent so that the first surface becomes the convex surface of the bent specimen. In general, the first surface is defined as that surface from which the brazing filler metal is applied and is fed by capillary attraction into the joint. Transverse first surface bend specimens shall conform to the dimensions shown in figure QB-462.2(a). For subsize first surface bends, see QB-161.3.

QB-161.2 Transverse Second Surface Bend. The joint is transverse to the longitudinal axis of the specimen, which is bent so that the second surface becomes the convex surface of the bent specimen. In general, the second surface is defined as the surface opposite to that from which the brazing filler metal is placed or fed, but definitely is the surface opposite to that designated as the first surface, irrespective of how the brazing filler metal is fed. Transverse second surface bend specimens shall
conform to the dimensions shown in figure QB-462.2(a). For subsize first surface bends, see QB-161.3.

QB-161.3 Subsize Transverse Bend. In those cases where the wall thickness of the tube or pipe is less than $3 / 8 \mathrm{in} .(10 \mathrm{~mm})$ and the diameter-to-thickness ratio does not permit the preparation of full-size rectangular guidedbend specimens, the $1 \frac{1}{2} \mathrm{in}$. ( 38 mm ) wide standard guided-bend specimen shown in figure QB-462.2(a) may be replaced by three subsize specimens having a width of $3 / 8 \mathrm{in}$. $(10 \mathrm{~mm})$ or $4 t$, whichever is less.

QB-161.4 Longitudinal-Bend Tests. Longitudinalbend tests may be used in lieu of the transverse-bend tests for testing braze metal or base metal combinations, which differ markedly in bending properties between
(a) the two base metals; or
(b) the braze metal and the base metal.

QB-161.5 Longitudinal First Surface Bend. The joint is parallel to the longitudinal axis of the specimen, which is bent so that the first surface becomes the convex surface of the bent specimen. The definition of first surface is as given in QB-161.1. Longitudinal first surface bend specimens shall conform to the dimensions given in figure QB-462.2(b).

QB-161.6 Longitudinal Second Surface Bend. The joint is parallel to the longitudinal axis of the specimen, which is bent so that the second surface becomes the convex surface of the specimen. The definition of the second surface is given in QB-161.2. Longitudinal second surface bend specimens shall conform to the dimensions given in figure QB-462.2(b).

## QB-162 Guided-Bend Test Procedure

QB-162.1 Jigs. Guided-bend specimens shall be bent in test jigs that are in substantial accordance with QB-466. When using the jigs in accordance with figure QB-466.1 or figure QB-466.2, the side of the specimen turned toward the gap of the jig shall be the first surface for first surface bend specimens (defined in QB-161.1), and the second surface for second surface bend specimens (defined in QB-161.2). The specimen shall be forced into the die by applying load on the plunger until the curvature of the specimen is such that a $1 / 8 \mathrm{in}$. $(3 \mathrm{~mm}$ ) diameter wire cannot be inserted between the specimen and the die of figure QB-466.1, or the specimen is bottom ejected, if the roller type of jig (figure QB-466.2) is used.

When using the wrap around jig (figure QB-466.3) the side of the specimen turned toward the roller shall be the first surface for first surface bend specimens, and the second surface for second surface bend specimens.

## QB-163 Acceptance Criteria - Bend Tests

The joint of a transverse-bend specimen shall be completely within the bent portion of the specimen after testing.

The guided-bend specimens shall have no open discontinuities exceeding $1 / 8 \mathrm{in}$. ( 3 mm ), measured in any direction on the convex surface of the specimen after bending. Cracks occurring on the corners of the specimen during testing shall not be considered, unless there is definite evidence that they result from flux inclusions, voids, or other internal discontinuities.

## QB-170 PEEL TESTS

QB-171 Specimens
The dimensions and preparation of the peel test specimen shall conform to the requirements of figure QB-462.3.

## QB-172 Acceptance Criteria - Peel Test

In order to pass the peel test, the specimens shall show evidence of brazing filler metal along each edge of the joint. Specimens shall be separated or peeled either by clamping Section A and striking Section B with a suitable tool such that the bending occurs at the fulcrum point (see figure QB-462.3), or by clamping Section A and Section B in a machine suitable for separating the sections under tension. The separated faying surfaces of joints shall meet the following criteria:
(a) The total area of discontinuities (unbrazed areas, flux inclusions, etc.) shall not exceed $25 \%$ of the total area of any individual faying surface.
(b) The sum of the lengths of the discontinuities measured on any one line in the direction of the lap shall not exceed $25 \%$ of the lap.
(c) No discontinuity shall extend continuously from one edge of the joint to the other edge, irrespective of its direction.

## QB-180 SECTIONING TESTS AND WORKMANSHIP COUPONS <br> QB-181 Sectioning Test Specimens

The dimensions and configuration of the sectioning test specimens shall conform to the requirements of figure QB-462.4. Each side of the specimen shall be polished and examined with at least a four-power magnifying glass. The sum of the length of unbrazed areas on either side, considered individually, shall not exceed $20 \%$ of the length of the joint overlap.

## QB-182 Workmanship Coupons

The dimensions and configuration of the workmanship coupon shall conform to the nearest approximation of the actual application. Some typical workmanship coupons are shown in figure QB-462.5. Each side of the specimen shall be polished and examined with at least a four-power magnifying glass. The sum of the length of unbrazed areas on either side, considered individually, shall not exceed $20 \%$ of the length of the joint overlap.

# ARTICLE XII BRAZING PROCEDURE QUALIFICATIONS 

## QB-200 GENERAL

QB-200.1 Each manufacturer or contractor shall prepare written Brazing Procedure Specifications, which are defined as follows.
(a) Brazing Procedure Specification (BPS). A BPS is a written qualified brazing procedure prepared to provide direction for making production brazes to Code requirements. The BPS or other documents [see QB-200.1(e)] may be used to provide direction to the brazer or brazing operator to assure compliance with the Code requirements.
(b) Contents of the BPS. The completed BPS shall describe all of the essential and nonessential variables for each brazing process used in the BPS. These variables are listed in QB-250 and are defined in Article XIV, Brazing Data.

The BPS shall reference the supporting Procedure Qualification Record(s) (PQR) described in QB-200.2. The manufacturer or contractor may include any other information in the BPS that may be helpful in making a Code braze.
(c) Changes to the BPS. Changes may be made in the nonessential variables of a BPS to suit production requirements without requalification provided such changes are documented with respect to the essential and nonessential variables for each process. This may be by amendment to the BPS or by use of a new BPS.
Changes in essential variables require requalification of the BPS [new or additional PQRs to support the change in essential variable(s)].
(d) Format of the BPS. The information required to be in the BPS may be in any format, written or tabular, to fit the needs of each manufacturer or contractor, as long as every essential and nonessential variable outlined in QB-250 is included or referenced.

Form QB-482 (see Nonmandatory Appendix B) has been provided as a guide for the BPS. It is only a guide and does not list all required data for all brazing processes.
(e) Availability of the BPS. A BPS used for Code production brazing shall be available for reference and review by the Authorized Inspector (AI) at the fabrication site.

QB-200.2 Each manufacturer or contractor shall be required to prepare a procedure qualification record, which is defined as follows.
(a) Procedure Qualification Record (PQR). A PQR is a record of the brazing data used to braze a test coupon. The $P Q R$ is a record of variables recorded during the brazing of the test coupons. It also contains the test results of the tested specimens. Recorded variables normally fall within a small range of the actual variables that will be used in production brazing.
(b) Contents of the PQR. The completed PQR shall document all essential variables of QB-250 for each brazing process used during the brazing of the test coupon. Nonessential or other variables used during the brazing of the test coupon may be recorded at the manufacturer's or contractor's option. All variables, if recorded, shall be the actual variables (including ranges) used during the brazing of the test coupon. If variables are not monitored during brazing, they shall not be recorded. It is not intended that the full range or the extreme of a given range of variables to be used in production be used during qualification unless required due to a specific essential variable.

The PQR shall be certified accurate by the manufacturer or contractor. The manufacturer or contractor may not subcontract the certification function. This certification is intended to be the manufacturer's or contractor's verification that the information in the PQR is a true record of the variables that were used during the brazing of the test coupon and that the resulting tensile, bend, peel, or section (as required) test results are in compliance with Section IX.
(c) Changes to the PQR. Changes to the PQR are not permitted, except as described below. It is a record of what happened during a particular brazing test. Editorial corrections or addenda to the PQR are permitted. An example of an editorial correction is an incorrect P-Number or F-Number that was assigned to a particular base material or filler metal. An example of an addendum would be a change resulting from a Code change. For example, Section IX may assign a new F-Number to a filler material or adopt a new filler material under an
established F-Number. This may permit, depending on the particular construction Code requirements, a manufacturer or contractor to use other filler metals that fall within that particular F-Number where, prior to the Code revision, the manufacturer or contractor was limited to the particular electrode classification that was used during qualification. Additional information can be incorporated into a PQR at a later date provided the information is substantiated as having been part of the original qualification condition by lab record or similar data.

All changes to a PQR require recertification (including date) by the manufacturer or contractor.
(d) Format of the PQR. Form QB-483 (see Nonmandatory Appendix B) has been provided as a guide for the PQR . The information required to be in the PQR may be in any format, to fit the needs of each manufacturer or contractor, as long as every essential variable, required by QB-250, is included. Also the type of tests, number of tests, and test results shall be listed in the PQR. Additional sketches or information may be attached or referenced to record the required variables.
(e) Availability of the $P Q R$. PQRs used to support BPSs shall be available, upon request, for review by the Authorized Inspector (AI). The PQR need not be available to the brazer or brazing operator.
(f) Multiple BPSs With One PQR/Multiple PQRs With One BPS. Several BPSs may be prepared from the data on a single PQR (e.g., a vertical-upflow pipe PQR may support BPSs for the vertical-upflow and downflow positions on pipe within all other essential variables). A single BPS may cover several essential variable changes as long as a supporting PQR exists for each essential variable.

QB-200.3 To reduce the number of brazing procedure qualifications required, P -Numbers are assigned to base metals dependent on characteristics such as composition, brazability, and mechanical properties, where this can logically be done, and for ferrous and nonferrous metals.

The assignments do not imply that base metals may be indiscriminately substituted for a base metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, postbraze heat treatment, design, mechanical properties, and service requirements. For certain materials permitted by the ASME/ANSI B31 Code for Pressure Piping or by selected Code Cases of the ASME Boiler and Pressure Vessel Code, S-Number groupings are assigned. These groupings are similar to the P-Number groupings of table QW/QB-422. Qualification limits are given in QW-420.2.

QB-200.4 Dissimilar Base Metal Thicknesses. A BPS qualified on test coupons of equal thickness shall be applicable for production brazements between dissimilar
base metal thicknesses provided the thickness of both base metals are within the qualified thickness range permitted by QB-451. A BPS qualified on test coupons of different thicknesses shall be applicable for production brazements between dissimilar base metal thicknesses provided the thickness of each base metal is within the qualified range of thickness (based on each test coupon thickness) permitted by QB-451.

## QB-201 Manufacturer's or Contractor's Responsibility

Each manufacturer or contractor shall list the parameters applicable to brazing that he performs in construction of brazements built in accordance with this Code. These parameters shall be listed in a document known as a Brazing Procedure Specification (BPS).

Each manufacturer or contractor shall qualify the BPS by the brazing of test coupons and the testing of specimens (as required in this Code), and the recording of the brazing data and test results in a document known as a Procedure Qualification Record (PQR). The brazers or brazing operators used to produce brazements to be tested for qualification of procedures shall be under the full supervision and control of the manufacturer or contractor during the production of these test brazements. It is not permissible for the manufacturer or contractor to have the brazing of the test brazements performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test metal for brazing and subsequent work on preparation of test specimens from the completed brazement, performance of nondestructive examination, and mechanical tests, provided the manufacturer or contractor accepts the responsibility for any such work.

The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the brazements to be made in accordance with this Code. If in an organization effective operational control of brazing procedure qualification for two or more companies of different names exists, the companies involved shall describe in their Quality Control system/Quality Assurance Program, the operational control of procedure qualifications. In this case separate brazing procedure qualifications are not required, provided all other requirements of Section IX are met.

A BPS may require the support of more than one PQR , while alternatively, one PQR may support a number of BPSs.

The manufacturer or contractor shall certify that he has qualified each Brazing Procedure Specification, performed the procedure qualification test, and documented
it with the necessary Procedure Qualification Record (PQR).

QB-201.1 The Code recognizes that manufacturers or contractors may maintain effective operational control of PQRs and BPSs under different ownership than existed during the original procedure qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the PQRs and BPSs may be used by the new owner(s) without requalification provided all of the following are met:
(a) the new owner(s) takes responsibility for the BPSs and PQRs
(b) the BPSs reflect the name of the new owner(s)
(c) the Quality Control System/Quality Assurance Program reflects the source of the PQRs as being from the former manufacturer or contractor

## QB-202 Type of Tests Required

QB-202.1 Tests. The type and number of test specimens which shall be tested to qualify a brazing procedure are given in QB-451, and shall be removed in a manner similar to that shown in QB-463. If any test specimen required by QB-451 fails to meet the applicable acceptance criteria, the test coupon shall be considered as failed.

When it can be determined that the cause of failure is not related to brazing parameters, another test coupon may be brazed using identical brazing parameters. Alternatively, if adequate material of the original test coupon exists, additional test specimens may be removed as close as practicable to the original specimen location to replace the failed test specimens.

When it has been determined that the test failure was caused by an essential variable, a new test coupon may be brazed with appropriate changes to the variable(s) that were determined to cause the test failure. If the new test passes, the essential variables shall be documented on the PQR.

When it is determined that the test failure was caused by one or more brazing conditions other than essential variables, a new test coupon may be brazed with the appropriate changes to brazing conditions that were determined to cause the test failure. If the new test passes, the brazing conditions that were determined to cause the previous test failure shall be addressed by the manufacturer to assure that the required properties are achieved in the production brazement.

QB-202.2 Base Metals. The procedure qualification shall encompass the thickness ranges to be used in production for the base metals to be joined or repaired. The range of thickness qualified is given in QB-451.

## QB-203 Limits of Qualified Flow Positions for Procedures (See Figs. QB-461.1 and QB-461.2)

QB-203.1 For plate, qualification in the flat-flow, ver-tical-upflow, or horizontal-flow position shall qualify for the vertical-downflow position. For pipe, qualification in the horizontal-flow or vertical-upflow position shall qualify for the vertical-downflow position.

Qualification in pipe shall qualify for plate, but not vice versa. Horizontal-flow in pipe shall also qualify for flat-flow in plate.

QB-203.2 Special Flow Positions. A fabricator who does production brazing in a special orientation may make the tests for procedure qualification in this specific orientation. Such qualifications are valid only for the flow positions actually tested, except that an angular deviation of $\pm 15 \mathrm{deg}$ is permitted in the inclination of the braze plane, as defined in figures QB-461.1 and QB-461.2.

QB-203.3 The brazing process must be compatible, and the brazing filler metals, such as defined in the specifications of Section II, Part C, must be suitable for their use in specific flow positions. A brazer or brazing operator making and passing the BPS qualification test is thereby qualified for the flow position tested (see QB-301.2).

## QB-210 PREPARATION OF TEST COUPON

## QB-211 Base Metal and Filler Metal

The base metals and filler metals shall be one or more of those listed in the BPS. The dimensions of the test assembly shall be sufficient to provide the required test specimens.

The base metals may consist of either plate, pipe, or other product forms. Qualification in pipe also qualifies for plate brazing, but not vice versa.

## QB-212 Type and Dimension of Joints

The test coupon shall be brazed using a type of joint design proposed in the BPS for use in construction.

QB-250
BRAZING VARIABLES
QB-251 General
QB-251.1 Types of Variables for Brazing Procedure Specification (BPS). Brazing variables (listed for each brazing process in tables QB-252 through QB-257) are subdivided into essential and nonessential variables (QB-401).

QB-251.2 Essential Variables. Essential variables are those in which a change, as described in the specific
variables, is considered to affect the mechanical properties of the brazement, and shall require requalification of the BPS.

QB-251.3 Nonessential Variables. Nonessential variables are those in which a change, as described in the specific variables, may be made in the BPS without requalification.

## 2004 SECTION IX

QB-252
TORCH BRAZING (TB)

|  | 252.1 Essential Variables | 252.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 | . . |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | . . |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | QB-406.3 |
| QB-407 Flow Position | QB-407.1 | . . |
| QB-408 Joint Design | QB-408.2 | . . |
|  | QB-408.4 | . . . |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . . |
|  | QB-409.2 | . . . |
|  | QB-409.3 | . . . |
| QB-410 Technique | . . | QB-410.1 |
|  | . . . | QB-410.2 |
|  | . . | QB-410.3 |
|  | . . | QB-410.4 |
|  | . . | QB-410.5 |

## BRAZING PROCEDURE QUALIFICATIONS

QB-253
FURNACE BRAZING (FB)

|  | 253.1 Essential Variables | 253.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 |  |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | $\cdots$ |
| QB-404 Brazing Temperature | QB-404.1 | $\cdots$ |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | . . |
|  | QB-406.2 | . . |
| QB-407 Flow Position | QB-407.1 | . . |
| QB-408 Joint Design | QB-408.2 | . . |
|  | QB-408.4 | . . . |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . . |
|  | QB-409.2 | . . |
|  | QB-409.3 | . . |
| QB-410 Technique |  | QB-410.1 |
|  | . . | QB-410.2 |

## 2004 SECTION IX

QB-254
INDUCTION BRAZING (IB)

|  | 254.1 Essential Variables | 254.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 |  |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | . . . |
| QB-404 Brazing Temperature | QB-404.1 | . . |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | . $\cdot$ |
| QB-407 Flow Position | QB-407.1 | . . |
| QB-408 Joint Design | QB-408.2 | . |
|  | QB-408.4 | . . . |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . . |
|  | QB-409.2 | . . . |
|  | QB-409.3 | . . . |
| QB-410 Technique | . . | QB-410.1 |
|  |  | QB-410.2 |

## BRAZING PROCEDURE QUALIFICATIONS

QB-255
RESISTANCE BRAZING (RB)

|  | 255.1 Essential Variables | 255.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 | . . |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | . . . |
| QB-404 Brazing Temperature | QB-404.1 | . . |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | . . |
| QB-407 Flow Position | QB-407.1 | . . |
| QB-408 Joint Design | QB-408.2 | . . |
|  | QB-408.4 | . . . |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . . |
|  | QB-409.2 | . . . |
|  | QB-409.3 | . . . |
| QB-410 Technique | . . | QB-410.1 |
|  | . . . | QB-410.2 |

## 2004 SECTION IX

QB-256
DIP BRAZING - SALT OR FLUX BATH (DB)

|  | 256.1 Essential Variables | 256.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 | . . |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | . . |
| QB-404 Brazing Temperature | QB-404.1 | . . |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | $\ldots$ |
| QB-407 Flow Position | QB-407.1 | . . |
| QB-408 Joint Design | QB-408.2 | . . |
|  | QB-408.4 | $\ldots$ |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . . |
|  | QB-409.2 | . . . |
|  | QB-409.3 | . . . |
| QB-410 Technique |  | QB-410.1 |
|  | . | QB-410.2 |

## BRAZING PROCEDURE QUALIFICATIONS

QB-257
DIP BRAZING - MOLTEN METAL BATH (DB)

|  | 257.1 Essential Variables | 257.2 Nonessential Variables |
| :---: | :---: | :---: |
| QB-402 Base Metal | QB-402.1 | . . . |
|  | QB-402.3 | . . |
| QB-403 Brazing Filler Metal | QB-403.1 | . . |
|  | QB-403.2 | . . |
| QB-404 Brazing Temperature | QB-404.1 | . . |
| QB-406 Brazing Flux, Gas, or Atmosphere | QB-406.1 | $\cdots$ |
| QB-407 Flow Position | QB-407.1 | $\ldots$ |
| QB-408 Joint Design | QB-408.2 | . . |
|  | QB-408.4 | . . . |
| QB-409 Postbraze Heat Treatment | QB-409.1 | . |
|  | QB-409.2 | . . . |
|  | QB-409.3 | . . . |
| QB-410 Technique |  | QB-410.1 |
|  | . . . | QB-410.2 |

## ARTICLE XIII BRAZING PERFORMANCE QUALIFICATIONS

## QB-300 GENERAL

QB-300.1 This Article lists the brazing processes separately, with the essential variables which apply to brazer and brazing operator performance qualifications.

The brazer qualification is limited by the essential variables given for each brazing process. These variables are listed in QB-350, and are defined in Article XIV, Brazing Data. The brazing operator qualification is limited by the essential variables given in QB-350 for each brazing process.

## QB-300.2

(a) The basic premises of responsibility in regard to brazing are contained within QB-103 and QB-301.2. These paragraphs require that each manufacturer or contractor shall be responsible for conducting tests to qualify the performance of brazers and brazing operators in accordance with one of his qualified Brazing Procedure Specifications, which his organization employs in the construction of brazements built in accordance with the Code. The purpose of this requirement is to ensure that the manufacturer or contractor has determined that his brazers and brazing operators using his procedures are capable of developing the minimum requirements specified for an acceptable brazement. This responsibility cannot be delegated to another organization.
(b) The brazers or brazing operators used to produce such brazements shall be tested under the full supervision and control of the manufacturer or contractor during the production of these test brazements. It is not permissible for the manufacturer or contractor to have the brazing performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test materials for brazing, subsequent work on the preparation of test specimens from the completed brazement, and performance of nondestructive examination and mechanical tests, provided the manufacturer or contractor accepts full responsibility for any such work.
(c) The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the brazement to be made in accordance with this Code. If in an organization effective
operational control of the brazer performance qualification for two or more companies of different names exists, the companies involved must establish, to the satisfaction of the ASME Boiler and Pressure Vessel Committee, that the necessary controls are applied, in which case requalification of brazers and brazing operators within the companies of such an organization will not be required, provided all other requirements of Section IX are met.
(d) The Code recognizes that manufacturers or contractors may maintain effective operational control of Brazer/Brazing Operator Performance Qualification (BPQ) records under different ownership than existed during the original Brazer or Brazing Operator qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the BPQs may be used by the new owner(s) without requalification, provided all of the following are met:
(1) the new owner(s) takes responsibility for the BPQs
(2) the BPQs reflect the name of the new owner(s)
(3) the Quality Control System/Quality Assurance Program reflects the source of the BPQs as being from the former manufacturer or contractor

QB-300.3 More than one manufacturer or contractor may simultaneously qualify one or more brazers or brazing operators. When simultaneous qualifications are conducted, each participating organization shall be represented by a responsible employee during brazing of the test coupons.
The brazing procedure specifications (BPS) that are followed during simultaneous qualifications shall be compared by the participating organizations. The BPSs shall be identical for all essential variables, except that the flow position, base metal thickness, and overlap lengths need not be identical, but they shall be adequate to permit brazing of the test coupons. Alternatively, the participating organizations shall agree upon the use of a single BPS, provided each participating organization has a $\mathrm{PQR}(\mathrm{s})$ to support the BPS covering the range of variables to be followed in the performance qualification. When a single BPS is to be followed, each participating organization shall review and accept that BPS.

Each participating organization's representative shall positively identify each brazer or brazing operator who is being tested. Each organizational representative shall also verify marking of the test coupon with the brazer's or brazing operator's identification, and marking of the top of the test coupon when the orientation must be known in order to remove test specimens.

Each organizational representative shall complete and sign a Record of Brazer or Brazing Operator Qualification (Form QB-484 or equivalent) for each brazer or brazing operator.

When a brazer or brazing operator changes employers, that new participating organization shall verify that the brazer's continuity of qualifications has been maintained as required by QB-322 by previous employers since his qualification date. If the brazer or brazing operator has had his qualification withdrawn for specific reasons, the employing organization shall notify all participating organizations that the brazer's or brazing operator's qualification(s) has been revoked in accordance with QB-322(b). The new organization shall determine that the brazer or brazing operator can perform satisfactory work in accordance with this Section.

When a brazer's or brazing operator's qualifications are renewed in accordance with the provisions of QB-322, each renewing organization shall be represented by a responsible employee and the testing procedures shall follow the rules of this paragraph.

## QB-301 Tests

QB-301.1 Intent of Tests. The performance qualification tests are intended to determine the ability of brazers and brazing operators to make sound braze joints.

QB-301.2 Qualification Tests. Each manufacturer or contractor shall qualify each brazer or brazing operator for each brazing process to be used in production brazing. The performance qualification test shall be brazed in accordance with one of any of his qualified Brazing Procedure Specifications (BPS).

The brazer or brazing operator who prepares the BPS qualification test coupons is also qualified within the limits of the performance qualifications, listed in QB-304 for brazers and in QB-305 for brazing operators. He is qualified only for the positions tested in the procedure qualification in accordance with QB-407.

The performance test may be terminated at any stage of the testing procedure, whenever it becomes apparent to the supervisor conducting the tests that the brazer or brazing operator does not have the required skill to produce satisfactory results.

QB-301.3 Identification of Brazers and Brazing Operators. Each qualified brazer and brazing operator shall be assigned an identifying number, letter, or symbol by the manufacturer or contractor, which shall be used to identify the work of that brazer or brazing operator.

QB-301.4 Record of Tests. The record of Brazer or Brazing Operator Performance Qualification (BPQ) tests shall include the essential variables (QB-350), the type of tests and the test results, and the ranges qualified in accordance with QB-452 for each brazer and brazing operator. A suggested form for these records is given in Form QB-484 (see Nonmandatory Appendix B).

## QB-302 Type of Test Required

QB-302.1 Test Specimens. The type and number of test specimens required shall be in accordance with QB-452, and shall be removed in a manner similar to that shown in QB-463.

All test specimens shall meet the requirements prescribed in QB-170 or QB-180, as applicable. Tests for brazing operators shall meet the requirements of QB-305.

QB-302.2 Test Coupons in Pipe. For test coupons made in pipe, specimens shall be removed as shown in figure QB-463.2(c) at approximately 180 deg apart.

QB-302.3 Combination of Base Metal Thicknesses. When joints are brazed between two base metals of different thicknesses, a performance qualification shall be made for the applicable combination of thicknesses, even though qualification tests have been made for each of the individual base metals brazed to itself. The range of thickness of each of the base metals shall be determined individually per QB-452.

## QB-303 Limits of Qualified Positions

 (See Figs. QB-461.1 and QB-461.2)QB-303.1 For plate, qualification in the flat-flow, ver-tical-upflow, or horizontal-flow positions shall qualify for the vertical-downflow position.

QB-303.2 For pipe, qualification in either the hori-zontal-flow or vertical-upflow position shall qualify for the vertical-downflow position.

QB-303.3 Qualification in pipe shall qualify for plate, but not vice versa. Horizontal-flow in pipe shall qualify for flat-flow in plate.

QB-303.4 Special Positions. A fabricator who does production brazing in a special orientation may make the tests for performance qualification in this specific orientation. Such qualifications are valid only for the flow positions actually tested, except that an angular deviation
of $\pm 15 \mathrm{deg}$ is permitted in the inclination of the braze plane, as defined in figures QB-461.1 and QB-461.2.

## QB-304 Brazers

Each brazer who brazes under the rules of this Code shall have passed the tests prescribed in QB-302 for performance qualifications.

A brazer qualified to braze in accordance with one qualified BPS is also qualified to braze in accordance with other qualified BPSs, using the same brazing process, within the limits of the essential variables of QB-350.

## QB-305 Brazing Operators

The brazing operator who prepares brazing procedure qualification test specimens meeting requirements of QB-451 is thereby qualified. Alternatively, each brazing operator who brazes on vessels constructed under the rules of this Code shall be qualified for each combination of essential variables under which brazing is performed using semiautomatic or automatic processes (such as the resistance, induction, or furnace processes) as follows:
(a) A typical joint or workmanship coupon embodying the requirements of a qualified brazing procedure shall be brazed and sectioned. Typical joints are shown in figure QB-462.5.
(b) In order to ensure that the operator can carry out the provisions of the brazing procedure, the test sections required in QB-305(a) shall meet the requirements of QB-452.

## QB-310 QUALIFICATION TEST COUPONS

QB-310.1 Test Coupons. The test coupons may be plate, pipe, or other product forms. The dimensions of the test coupon and length of braze shall be sufficient to provide the required test specimens.

QB-310.2 Braze Joint. The dimensions of the braze joint at the test coupon used in making qualification tests shall be the same as those in the Brazing Procedure Specification (BPS).

QB-310.3 Base Metals. When a brazer or brazing operator is to be qualified, the test coupon shall be base metal of the P-Number or P-Numbers to be joined in production brazing.

## QB-320 RETESTS AND RENEWAL OF QUALIFICATION <br> QB-321 Retests

A brazer or brazing operator who fails to meet the requirements for one or more of the test specimens prescribed in QB-452 may be retested under the following conditions.

QB-321.1 Immediate Retest. When an immediate retest is made, the brazer or brazing operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the test requirements.

QB-321.2 Further Training. When the brazer or brazing operator has had further training or practice, a complete retest shall be made for each position on which he failed to meet the requirements.

## QB-322 Renewal of Qualification

Renewal of qualification of a performance qualification is required
(a) when a brazer or brazing operator has not used the specific brazing process for a period of 6 months or more; or
(b) when there is a specific reason to question his ability to make brazes that meet the specification. Renewal of qualification for a specific brazing process under QB-322(a) may be made with specific brazing process by making only one test joint (plate or pipe) with all the essential variables used on any one of the brazer's or brazing operator's previous qualification test joints. This will reestablish the brazer's or brazing operator's qualification for all conditions for which he had previously qualified with the specific brazing process.

## QB-350 BRAZING VARIABLES FOR BRAZERS AND BRAZING OPERATORS

## QB-351 General

A brazer or brazing operator shall be requalified whenever a change is made in one or more of the essential variables for each brazing process, as follows:
(a) Torch Blazing (TB)
(b) Furnace Brazing (FB)
(c) Induction Brazing (IB)
(d) Resistance Brazing (RB)
(e) Dip Brazing (DB)

QB-351.1 Essential Variables - Manual, Semiautomatic, and Machine Brazing

QB-402 Base Metal
QB-402.2
QB-402.3
QB-403 Brazing Filler Metal QB-403.1
QB-403.2
QB-407 Flow Position
QB-407.1

QB-408 Joint Design
QB-408.1
QB-408.3
QB-410 Technique
QB-410.5

QB-351.2 Essential Variables - Automatic
(a) A change from automatic to machine brazing.
(b) A change in brazing process.

# ARTICLE XIV BRAZING DATA 

## QB-400 VARIABLES <br> QB-401 General

QB-401.1 Each brazing variable described in this Article is applicable as an essential or nonessential variable for procedure qualification when referenced in QB-250 for each specific process. Essential variables for performance qualification are referenced in QB-350 for each specific brazing process. A change from one brazing process to another brazing process is an essential variable and requires requalification.

## QB-402 Base Metal

QB-402.1 A change from a base metal listed under one P-Number in table QW/QB-422 to any of the following:
(a) a metal listed under another P-Number
(b) any other base metal not listed in table QW/QB-422
(c) as permitted in QW-420.2 (for S-Numbers)

The brazing of dissimilar metals need not be requalified if each base metal involved is qualified individually for the same brazing filler metal, flux, atmosphere, and process. Similarly, the brazing of dissimilar metals qualifies for the individual base metal brazed to itself and for the same brazing filler metal, flux, atmosphere, and process, provided the requirements of QB-153.1(a) are met.
QB-402.2 A change from a base metal listed under one P-Number in table QW/QB-422 to any of the following:
(a) a metal listed under another P-Number
(b) any other metal not listed in table QW/QB-422
(c) as permitted in QW-420.2 (for S-Numbers)

The brazing of dissimilar metals need not be requalified if each base metal involved is qualified individually for the same brazing filler metal, flux, atmosphere, and process. Similarly, the brazing of dissimilar metals qualifies for the individual base metal brazed to itself and for the same brazing filler metal, flux, atmosphere, and process.
QB-402.3 A change in base metal thickness beyond the range qualified in QB-451 for procedure qualification, or QB-452 for performance qualification.

## QB-403 Brazing Filler Metal

QB-403.1 A change from one F-Number in table QB-432 to any other F-Number, or to any other filler metal not listed in table QB-432.

QB-403.2 A change in filler metal from one product form to another (for example, from preformed ring to paste).

## QB-404 Brazing Temperature

QB-404.1 A change in brazing temperature to a value outside the range specified in the BPS.

## QB-406 Brazing Flux, Fuel Gas, or Atmosphere

QB-406.1 The addition or deletion of brazing flux or a change in AWS classification of the flux. Nominal chemical composition or the trade name of the flux may be used as an alternative to the AWS classification.

QB-406.2 A change in the furnace atmosphere from one basic type to another type. For example:
(a) reducing to inert
(b) carburizing to decarburizing
(c) hydrogen to disassociated ammonia

QB-406.3 A change in the type of fuel gas(es).

## QB-407 Flow Position

QB-407.1 The addition of other brazing positions than those already qualified (see QB-120 through QB-124, QB-203 for procedure, and QB-303 for performance).
(a) If the brazing filler metal is preplaced or facefed from outside the joint, then requalification is required in accordance with the positions defined in figures QB-461.1 and QB-461.2 under the conditions of QB-120 through QB-124.
(b) If the brazing filler metal is preplaced in a joint in a manner that major flow does occur, then requalification is required in accordance with the positions defined in figures QB-461.1 and QB-461.2 under the conditions of QB-120 through QB-124.
(c) If the brazing filler metal is preplaced in a joint so that there is no major flow, then the joint may be brazed in any position without requalification.

## QB-408 Joint Design

QB-408.1 A change in the joint type, i.e., from a butt to a lap or socket, from that qualified. For lap or socket joints, an increase in lap length of more than $25 \%$ from the overlap used on the brazer performance qualification test coupon.

QB-408.2 A change in the joint clearances to a value outside the range specified in the BPS and as recorded in the PQR .

QB-408.3 A change in the joint clearances to a value outside the range specified in the BPS.

QB-408.4 A change in the joint type, e.g., from a butt to a lap or socket, from that qualified. For lap and socket joints, a decrease in overlap length from that qualified.

## QB-409 Postbraze Heat Treatment

QB-409.1 A separate procedure qualification is required for each of the following conditions:
(a) For P-Nos. 101 and 102 materials, the following postbraze heat treatment conditions apply:
(1) no postbraze heat treatment
(2) postbraze heat treatment below the lower transformation temperature
(3) postbraze heat treatment above the upper transformation temperature (e.g., normalizing)
(4) postbraze heat treatment above the upper transformation temperature followed by heat treatment below the lower transformation temperature (e.g., normalizing or quenching followed by tempering)
(5) postbraze heat treatment between the upper and lower transformation temperatures
(b) For all other materials, the following post weld heat treatment conditions apply:
(1) no postbraze heat treatment
(2) postbraze heat treatment within a specified temperature range

QB-409.2 A change in the postbraze heat treatment (see QB-409.1) temperature and time range requires a PQR.

The procedure qualification test shall be subjected to postbraze heat treatment essentially equivalent to that
encountered in the fabrication of production brazements, including at least $80 \%$ of the aggregate time at temperature(s). The postbraze heat treatment total time(s) at temperature(s) may be applied in one heating cycle.

QB-409.3 For a procedure qualification test coupon receiving a postbraze heat treatment in which the upper transformation temperature is exceeded, the maximum qualified thickness for production brazements is 1.1 times the thickness of the test coupon.

## QB-410 Technique

QB-410.1 A change in the method of preparing the base metal, i.e., method of precleaning the joints (for example, from chemical cleaning to cleaning by abrasive or mechanical means).

QB-410.2 A change in the method of postbraze cleaning (for example, from chemical cleaning to cleaning by wire brushing or wiping with a wet rag).

QB-410.3 A change in the nature of the flame (for example, a change from neutral or slightly reducing).

QB-410.4 A change in the brazing tip sizes.
QB-410.5 A change from manual to mechanical torch brazing and vice versa.

## QB-420 P-NUMBERS

(See Part QW, Welding - QW-420)

## QB-430 F-NUMBERS QB-431 General

The following F-Number grouping of brazing filler metals in table QB-432 is based essentially on their usability characteristics, which fundamentally determine the ability of brazers and brazing operators to make satisfactory brazements with a given filler metal. This grouping is made to reduce the number of brazing procedure and performance qualifications, where this can logically be done. The grouping does not imply that filler metals within a group may be indiscriminately substituted for a filler metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, design, mechanical properties, postbraze heat treatment, and service requirements.

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QB-432
F-NUMBERS
Grouping of Brazing Filler Metals for Procedure and Performance Qualification SFA-5.8

| QB | F-No. | AWS Classification No. |
| :---: | :---: | :---: |
| 432.1 | 101 | BAg-1 |
|  |  | BAg-1a |
|  |  | BAg-8 |
|  |  | BAg-8a |
|  |  | BAg-22 |
|  |  | BAg-23 |
|  |  | BVAg-0 |
|  |  | BVAg-8 |
|  |  | BVAg-8b |
|  |  | BVAg-30 |
| 432.2 | 102 | BAg-2 |
|  |  | BAg-2a |
|  |  | BAg-3 |
|  |  | BAg-4 |
|  |  | BAg-5 |
|  |  | BAg-6 |
|  |  | BAg-7 |
|  |  | BAg-9 |
|  |  | BAg-10 |
|  |  | BAg-13 |
|  |  | BAg-13a |
|  |  | BAg-18 |
|  |  | BAg-19 |
|  |  | BAg-20 |
|  |  | BAg-21 |
|  |  | BAg-24 |
|  |  | BAg-26 |
|  |  | BAg-27 |
|  |  | BAg-28 |
|  |  | BAg-33 |
|  |  | BAg-34 |
|  |  | BAg-35 |
|  |  | BAg-36 |
|  |  | BAg-37 |
|  |  | BVAg-6b |
|  |  | BVAg-18 |
|  |  | BVAg-29 |
|  |  | BVAg-31 |
|  |  | BVAg-32 |
| 432.3 | 103 | BCuP-1 |
|  |  | BCuP-2 |
|  |  | BCuP-3 |
|  |  | BCuP-4 |
|  |  | BCuP-5 |
|  |  | BCuP-6 |
|  |  | BCuP-7 |

## BRAZING DATA

QB-432
F-NUMBERS (CONT'D)
Grouping of Brazing Filler Metals for Procedure and Performance Qualification SFA-5.8

| QB | F-No. | AWS Classification No. |
| :---: | :---: | :---: |
| 432.4 | 104 | BAISi-2 |
|  |  | BAISi-3 |
|  |  | BAISi-4 |
|  |  | BAISi-5 |
|  |  | BAISi-7 |
|  |  | BAISi-9 |
|  |  | BAISi-11 |
| 432.5 | 105 | BCu-1 |
|  |  | BVCu-1x |
|  |  | BCu-la |
|  |  | BCu-2 |
| 432.6 | 106 | RBCuZn-A |
|  |  | RBCuZn-B |
|  |  | RBCuZn-C |
|  |  | RBCuZn-D |
| 432.7 | 107 | BNi-1 |
|  |  | BNi-1a |
|  |  | BNi-2 |
|  |  | BNi-3 |
|  |  | BNi-4 |
|  |  | BNi-5 |
|  |  | BNi-5a |
|  |  | BNi-6 |
|  |  | BNi-7 |
|  |  | BNi-8 |
|  |  | BNi-9 |
|  |  | BNi-10 |
|  |  | BNi-11 |
| 432.8 | 108 | BAu-1 |
|  |  | BAu-2 |
|  |  | BAu-3 |
|  |  | BAu-4 |
|  |  | BAu-5 |
|  |  | BAu-6 |
|  |  | BVAu-2 |
|  |  | BVAu-4 |
|  |  | BVAu-7 |
|  |  | BVAu-8 |
| 432.9 | 109 | BMg-1 |
| 432.10 | 110 | BCo-1 |
| 432.11 | 111 | BVPd-1 |

QB-450

## SPECIMENS

QB-451 Procedure Qualification Specimens

QB-451.1
TENSION TESTS AND TRANSVERSE-BEND TESTS - BUTT AND SCARF JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { Tension, QB- } \\ 462.1 \end{gathered}$ | First Surface Bend, QB462.2(a) | Second Surface Bend, QB462.2(a) |
|  | Min. | Max. |  |  |  |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 | 2 | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | 1/16 (1.5) | $2 T$ | 2 | 2 | 2 |
| Over $3 / 8$ (10) | 3/16 (5) | $2 T$ | 2 [Note (1)] | 2 | 2 |

NOTE:
(1) See QB-151 for details on multiple specimens when coupon thicknesses are over 1 in . ( 25 mm ).

QB-451.2
TENSION TESTS AND LONGITUDINAL BEND TESTS - BUTT AND SCARF JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension, QB-462.1 | First <br> Surface <br> Bend | Second Surface Bend, QB-462.2(b) |
|  | Min. | Max. |  | QB-462.2(b) |  |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 | 2 | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | $1 / 16$ (1.5) | $2 T$ | 2 | 2 | 2 |
| Over $3 / 8$ (10) | $3 / 16$ (5) | $2 T$ | 2 [Note (1)] | 2 | 2 |

NOTE:
(1) See QB-151 for details on multiple specimens when coupon thicknesses are over 1 in . ( 25 mm ).

QB-451. 3
TENSION TESTS AND PEEL TESTS - LAP JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension, QB-462.1 | $\begin{gathered} \text { Peel } \\ \text { QB-462.3 } \end{gathered}$ |
|  | Min. | Max. |  | [Notes (1) and (2)] |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | $1 / 16$ (1.5) | $2 T$ | 2 | 2 |
| Over 3/8 (10) | 3/16 (5) | $2 T$ | 2 | 2 |

NOTES:
(1) Sectioning tests may be substituted for peel tests. The specimens shall be sectioned as shown in QB-462.4.
(2) The overlap length must be equal to or greater than the overlap length of the Tension Test specimen.

## BRAZING DATA

QB-451.4
TENSION TESTS AND SECTION TESTS - RABBET JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension, QB-462.1 | $\begin{gathered} \text { Section, } \\ \text { QB-462.4 } \end{gathered}$ |
|  | Min. | Max. |  |  |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | 1/16 (1.5) | $2 T$ | 2 | 2 |
| Over $3 / 8$ (10) | $3 / 16$ (5) | $2 T$ | 2 | 2 |

QB-451.5
SECTION TESTS - WORKMANSHIP COUPON JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required <br> Section, QB-462.5 [Note (1)] |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  | Min. | Max. |  |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | 1/16 (1.5) | $2 T$ | 2 |
| Over $3 / 8$ (10) | 3/16 (5) | $2 T$ | 2 |

## NOTE:

(1) This test in itself does not constitute procedure qualification but must be validated by conductance of tests of butt or lap joints as appropriate. For joints connecting tension members, such as the stay or partition type in QB-462.5, the validation data may be based upon butt joints; for joints connecting members in shear, such as saddle or spud joints, the validation data may be based on lap joints.

04 QB-452 Performance Qualification Specimens

|  | CTION TE | SCAR | OINTS |
| :---: | :---: | :---: | :---: |
| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required |
|  | Min. | Max. | [Note (1)] |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 2 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | 1/16 (1.5) | $2 T$ | 2 |
| Over $3 / 8$ (10) | 3/16 (5) | $2 T$ | 2 |

NOTE:
(1) For a joint brazed with a filler metal having a tensile strength equal to or greater than that of the metal being joined, the specimens shall be sectioned as shown in QB-462.4.

QB-452.2
SECTION TESTS - WORKMANSHIP SPECIMEN JOINTS

| Thickness $T$ of Test Coupon as Brazed, in. (mm) | Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm) |  | Type and Number of Test Specimens Required <br> Section, QB-462.5 |
| :---: | :---: | :---: | :---: |
|  | Min. | Max. |  |
| Less than $1 / 8$ (3) | $0.5 T$ | $2 T$ | 1 |
| $1 / 8$ to $3 / 8$ (3 to 10), incl. | $1 / 16$ (1.5) | $2 T$ | 1 |
| Over $3 / 8$ (10) | $3 / 16$ (5) | $2 T$ | 1 |


(a) $C=$ joint clearance
(b) $L=$ length of lap or thickness

## QB-461.1 FLOW POSITIONS


(a) $C=$ joint clearance
(b) $L=$ length of lap or thickness

QB-461.2 TEST FLOW POSITIONS

## BRAZING DATA



NOTE:
(1) Length may vary to fit testing machine.

QB-462.1(a) TENSION-REDUCED SECTION FOR BUTT AND SCARF JOINTS - PLATE


NOTE:
(1) Length may vary to fit testing machine.

QB-462.1(b) TENSION-REDUCED SECTION FOR BUTT AND SCARF JOINTS - PIPE


NOTES:
(1) Length may vary to fit testing machine.
(2) $A=$ greater of $\frac{1}{4} \mathrm{in}$. ( 6 mm ) or $2 T$
(3) $X=$ test specimen overlap


Alternate for Butt Joints

For Lap Joints

QB-462.1(e) TENSION - FULL SECTION FOR LAP AND BUTT JOINTS - SMALL DIAMETER PIPE


QB-462.1(f) SUPPORT FIXTURE FOR REDUCED-SECTION TENSION SPECIMENS


| $T$, in. $(\mathrm{mm})$ | $y$, in. (mm) |
| :--- | :---: |
|  | All ferrous and nonferrous materials |
| $1 / 16^{-3 / 8}(1.5-10)$ | $T$ |
| $>3 / 8(>10)$ | $3 / 8(10)$ |

GENERAL NOTE: For the first surface bend specimens, machine from the second surface as necessary until the required thickness is obtained. For second surface bend specimens, machine from the first surface as necessary until the required thickness is obtained.

QB-462.2(a) TRANSVERSE FIRST AND SECOND SURFACE BENDS - PLATE AND PIPE


| $T$, in. $(\mathrm{mm})$ | $y$, in. (mm) |
| :--- | :---: |
|  | All ferrous and nonferrous materials |
| $1 / 16^{-3 / 8(1.5-10)}$ | $T$ |
| $>3 / 8(>10)$ | $3 / 8(10)$ |

GENERAL NOTE: For the first surface bend specimens, machine from the second surface as necessary until the required thickness is obtained. For second surface bend specimens, machine from the first surface as necessary until the required thickness is obtained.

QB-462.2(b) LONGITUDINAL FIRST AND SECOND SURFACE BENDS - PLATE

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GENERAL NOTES:
(a) Flange $Y$ may be omitted from Section B when "peeling" is to be accomplished in a suitable tension machine.
(b) Specimen shall be brazed from side marked $Z$.

NOTE:
(1) Length may vary to fit testing machine.

QB-462.3 LAP JOINT PEEL SPECIMEN


(a) Typical Stay or Partition Joint
[Note (1)]

(a) Typical Spud Joint
[Note (2)]

(c) Typical Saddle Joint Sectioned
[Note (2)]

NOTES:
(1) Workmanship coupons shall be $10 \mathrm{in} .(250 \mathrm{~mm}$ ) in length or represent one-half the typical joint, whichever is less.
(2) Circular coupons shall be sectioned in half, and one-half shall be used as the test specimen.

QB-462.5 WORKMANSHIP COUPONS

## QB-463 Order of Removal




## Alternate Butt Joint

QB-463.1(a) PLATES PROCEDURE QUALIFICATION


Alternate Butt Joint

QB-463.1(b) PLATES PROCEDURE QUALIFICATION

| Discard |  | this piece |
| :---: | :---: | :---: | :---: |
| Reduced section |  |  |
| tensile |  |  |$\quad$| specimen |
| :---: |
| Sectioning |



Rabbet Joint
[Note (1)]


Alternate Lap Joint
[Note (2)]


Alternate Lap Joint
[Note (2)]


Alternate Lap Joint
[Note (2)]

NOTES:
(1) Required for rabbet joints.
(2) The sectioning specimen in this view may be used as an alternate to sectioning the peel test specimens of QB-463.1(d) when the peel test cannot be used. This section test specimen should be approximately $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm}$ ) wide.

QB-463.1(c) PLATES PROCEDURE QUALIFICATION

(1) Required when peel test can be used.

QB-463.1(d) PLATES PROCEDURE QUALIFICATION

## BRAZING DATA



## GENERAL NOTES:

(a) Figure shown is for coupons over 3 in. ( 75 mm ) O.D. Locations No. 1 and 2 are for:
(1) second surface specimens for butt and scarf joints
(2) peel or section specimens for lap joints
(3) section specimens for rabbet joints
(b) For coupons $3 \mathrm{in} .(75 \mathrm{~mm}$ ) 0.D. and smaller, two coupons shall be brazed and one specimen shall be removed from each coupon. If brazed in the horizontal flow position, the specimen shall be taken at specimen location No. l. Alternatively, each coupon shall be cut longitudinally and the specimen shall consist of both sides of one half-section of each coupon.
(c) When coupon is brazed in the horizontal flow position, specimens locations shall be as shown relative to the horizontal plane of the coupon, and for half-section specimens, plane of cut shall be oriented as shown relative to the horizontal plane of the coupon.
(d) When both ends of a coupling are brazed, each end is considered a separate test coupon.

> QB-463.1(e) PIPE - PROCEDURE QUALIFICATION

| Discard | this piece |  |
| :---: | :---: | :---: |
| Sectioning | specimen |  |
| Discard | this piece |  |
| Sectioning | specimen |  |
| Discard |  | this piece |



## Alternate Scarf Joint

[Note (2)]


Alternate Butt Joint
[Note (2)]


Alternate Lap Joint
[Note (2)]


Alternate Lap Joint
[Note (2)]


Alternate Lap Joint
[Note (2)]

NOTES:
(1) Required for rabbet joints.
(2) The sectioning specimen in this view may be used as an alternate to sectioning the peel test specimens of QB-463.2 (b) when the peel test cannot be used. This section test specimen should be approximately $1 / 2 \mathrm{in}$. $(13 \mathrm{~mm}$ ) wide.

QB-463.2(a) PLATES PERFORMANCE QUALIFICATION

| Discard |  | this piece |  |
| :---: | :---: | :---: | :---: |
| Peel test |  | specimen |  |
|  |  |  |  |
|  |  | section |  |
|  |  |  |  |
| Peel test |  |  |  |
|  |  |  |  |
| Discard |  |  |  |
|  |  | specimen |  |



NOTE:
(1) Required when peel test can be used.

QB-463.2(b) PLATES PERFORMANCE QUALIFICATION


GENERAL NOTES:
(a) For coupons over 3 in. ( 75 mm ) O.D., one specimen shall be removed from each location shown.
(b) For coupons 3 in. ( 75 mm ) O.D. and smaller, two coupons shall be brazed and one specimen shall be removed from each coupon. If brazed in the horizontal flow position, the specimen shall be taken at specimen location No. 1. Alternatively, each coupon shall be cut longitudinally and the specimen shall be both sides of one half-section of each coupon.
(c) When the coupon is brazed in the horizontal flow position, specimen locations shall be as shown relative to the horizontal plane of the coupon. For half-section specimens, plane of cut shall be oriented as shown relative to the horizontal plane of the coupon.
(d) When both ends of a coupling are brazed, each end is considered a separate test coupon.

QB-463.2(c) PIPE PERFORMANCE QUALIFICATION

## QB-466 <br> Test Jigs



QB-466.1 GUIDED-BEND JIG


GENERAL NOTE: The braze joint in the case of a transverse bend specimen shall be completely within the bend portion of the specimen after testing.

## NOTES:

(1) Either hardened and greased shoulders or hardened rollers free to rotate shall be used.
(2) The shoulders of rollers shall have a minimum bearing surface of $2 \mathrm{in} .(50 \mathrm{~mm})$ for placement of the specimen. The rollers shall be high enough above the bottom of the jig so that the specimens will clear the rollers when the ram is in the low position.
(3) The ram shall be fitted with an appropriate base and provision made for attachment to the testing machine, and shall be of a sufficiently rigid design to prevent deflection and misalignment while making the bend test. The body of the ram may be less than the dimensions shown in column $A$.
(4) If desired, either the rollers or the roller supports may be made adjustable in the horizontal direction so that specimens of $t$ thickness may be tested on the same jig.
(5) The roller supports shall be fitted with an appropriate base designed to safeguard against deflection or misalignment and equipped with means for maintaining the rollers centered midpoint and aligned with respect to the ram.

QB-466.2 GUIDED-BEND ROLLER JIG


| Thickness of Speci- <br> men, in. $(\mathrm{mm})$ | $A$, <br> in. (mm) | $B$, <br> $\frac{1}{3}(10)$ |
| :--- | :--- | :--- |

GENERAL NOTES:
(a) Dimensions not shown are the option of the designer. The essential consideration is to have adequate rigidity so that the jig parts will not spring.
(b) The specimen shall be firmly clamped on one end so that there is no sliding of the specimen during the bending operation.
(c) Test specimens shall be removed from the jig when the outer roll has been removed 180 deg from the starting point.

QB-466.3 GUIDED-BEND WRAP AROUND JIG

# MANDATORY APPENDIX A SUBMITTAL OF TECHNICAL INQUIRIES TO THE BOILER AND PRESSURE VESSEL COMMITTEE 

## A-100

INTRODUCTION
The ASME Boiler and Pressure Vessel Committee and its Subcommittees, Subgroups, and Working Groups meet regularly to consider revisions of the Code rules, new Code rules as dictated by technological development, Code Cases, and Code interpretations. This Appendix provides guidance to Code users for submitting technical inquiries to the Committee. Technical inquiries include requests for revisions or additions to the Code rules, requests for Code Cases, and requests for Code interpretations.

Code Cases may be issued by the Committee when the need is urgent. Code Cases clarify the intent of existing Code requirements or provide alternative requirements. Code Cases are written as a question and a reply and are usually intended to be incorporated into the Code at a later date. Code interpretations provide the meaning of or the intent of existing rules in the Code and are also presented as a question and a reply. Both Code Cases and Code interpretations are published by the Committee.

The Code rules, Code Cases, and Code interpretations established by the Committee are not to be considered as approving, recommending, certifying, or endorsing any proprietary or specific design or as limiting in any way the freedom of manufacturers or constructors to choose any method of design or any form of construction that conforms to the Code rules.

As an alternative to the requirements of this Appendix, members of the Committee and its Subcommittees, Subgroups, and Working Groups may introduce requests for Code revisions or additions, Code Cases, and Code interpretations at their respective Committee meetings or may submit such requests to the secretary of a Subcommittee, Subgroup, or Working Group.
Inquiries that do not comply with the provisions of this Appendix or that do not provide sufficient information for the Committee's full understanding may result in the request being returned to the inquirer with no action.

## INQUIRY FORMAT

Submittals to the Committee shall include:
(a) Scope. Specify one of the following:
(1) revision of present Code rule(s)
(2) new or additional Code rule(s)
(3) Code Case
(4) Code interpretation
(b) Background. Provide the information needed for the Committee's understanding of the inquiry, being sure to include reference to the applicable Code Section, Division, Edition, Addenda, paragraphs, figures, and tables. Preferably, provide a copy of the specific referenced portions of the Code.
(c) Presentations. The inquirer may desire or be asked to attend a meeting of the Committee to make a formal presentation or to answer questions from the Committee members with regard to the inquiry. Attendance at a Committee meeting shall be at the expense of the inquirer. The inquirer's attendance or lack of attendance at a meeting shall not be a basis for acceptance or rejection of the inquiry by the Commitee.

## A-300 <br> CODE REVISIONS OR ADDITIONS

Requests for Code revisions or additions shall provide the following:
(a) Proposed Revision(s) or Addition(s). For revisions, identify the rules of the Code that require revision and submit a copy of the appropriate rules as they appear in the Code marked up with the proposed revision. For additions, provide the recommended wording referenced to the existing Code rules.
(b) Statement of Need. Provide a brief explanation of the need for the revision(s) or addition(s)
(c) Background Information. Provide background information to support the revision(s) or addition(s) including any data or changes in technology that form
the basis for the request that will allow the Committee to adequately evaluate the proposed revision(s) or addition(s). Sketches, tables, figures, and graphs should be submitted as appropriate. When applicable, identify any pertinent paragraph in the Code that would be affected by the revision(s) or addition(s) and paragraphs in the Code that reference the paragraphs that are to be revised or added.

## A-400 CODE CASES

Requests for Code Cases shall provide a Statement of Need and Background Information similar to that defined in A-300(b) and A-300(c), respectively, for Code revisions or additions. The proposed Code Case should identify the Code Section and Division and be written as a Question and a Reply in the same format as existing Code Cases.

## A-500 <br> CODE INTERPRETATIONS

Requests for Code interpretations shall provide the following:
(a) Inquiry. Provide a condensed and precise question, omitting superfluous background information, and, when possible, composed in such a way that a "yes" or a "no" Reply, possibly with brief provisos, is acceptable. The question should be technically and editorially correct.
(b) Reply. Provide a proposed Reply that will clearly and concisely answer the Inquiry question. Preferably, the Reply should be "yes" or "no" with brief provisos.
(c) Background Information. Provide any background information that will assist the Committee in understanding the proposed Inquiry and Reply.

## A-600 SUBMITTALS

Submittals to and responses from the Committee shall meet the following:
(a) Submittal. Inquiries from Code users shall preferably be submitted in typewritten form; however, legible handwritten inquiries will also be considered. They shall include the name, address, telephone number, and a fax number, if available, of the inquirer and be mailed to the following address:

Secretary
ASME Boiler and Pressure Vessel Committee
Three Park Avenue
New York, N.Y. 10016-5990
(b) Response. The Secretary of the ASME Boiler and Pressure Vessel Committee or of the appropriate Subcommittee shall acknowledge receipt of each properly prepared inquiry and shall provide a written response to the inquirer upon completion of the requested action by the Code Committee.

# NONMANDATORY APPENDIX B WELDING AND BRAZING FORMS 

## B-100 FORMS

This Nonmandatory Appendix illustrates sample formats for Welding and Brazing Procedure Specifications, Procedure Qualification Records, and Performance Qualification.

## B-101 <br> Welding

Form QW-482 is a suggested format for Welding Procedure Specifications (WPS); Form QW-483 is a suggested format for Procedure Qualification Records (PQR). These forms are for the shielded metal-arc (SMAW), submerged-arc (SAW), gas metal-arc (GMAW), and gas tungsten-arc (GTAW) welding processes, or a combination of these processes.

Forms for other welding processes may follow the general format of Forms QW-482 and QW-483, as applicable.

Form QW-484 is a suggested format for Welder/Welding Operator/Performance Qualification (WPQ) for groove or fillet welds.

Form QW-485 is a suggested format for Demonstration of Standard Welding Procedure Specifications.

## B-102 Brazing

Form QB-482 is a suggested format for Brazing Procedure Specifications (BPS); Form QB-483 is a suggested format for Procedure Qualifications Records (PQR). These forms are for torch brazing (TB), furnace brazing (FB), induction brazing (IB, resistance brazing (RB), and dip brazing (DB) processes.

Forms for other brazing processes may follow the general format of Forms QB-482 and QB-483, as applicable.

Form QB-484 is a suggested format for Brazer/Brazing Operator/Performance Qualification (BPQ).

| QW-482 SUGGESTED FORMAT FOR WELDING PROCEDURE SPECIFICATIONS (WPS) (See QW-200.1, Section IX, ASME Boiler and Pressure Vessel Code) |  |  |
| :---: | :---: | :---: |
| Company Name ___ By: ___ |  |  |
| Welding Procedure Specification No.___ Date__ Date__ Supporting PQR No.(s)Revision No.__ |  |  |
|  |  |  |
| Welding Process(es) | Type(s) | (Automatic, Manual, Machine, or Semi-Auto.) |
| JOINTS (OW-402) |  | Details |
| Joint Design |  |  |
| Backing (Yes) (No) |  |  |
| Backing Material (Type) |  |  |
| $\square$ Metal $\quad \square$ Nonfusing Metal |  |  |
| $\square$ Nonmetallic $\square$ Other |  |  |
| Sketches, Production Drawings, Weld Symbols or Written Description should show the general arrangement of the parts to be welded. Where applicable, the root spacing and the details of weld groove may be specified. |  |  |
| (At the option of the Mfgr., sketches may be attached to illustrate joint design, weld layers and bead sequence, e.g., for notch toughness procedures, for multiple process procedures, etc.) |  |  |
| *BASE METALS (QW-403) |  |  |
| P-No. $\qquad$ Group No. $\qquad$ to P-No. $\qquad$ Group No. |  |  |
| OR |  |  |
| Specification type and grade |  |  |
| to Specification type and OR |  |  |
|  |  |  |
| Chem. Analysis and Mech. Prop |  |  |
| to Chem. Analysis and Me Thickness Range: |  |  |
|  |  |  |
| Base Metal: Groo |  |  |
| Other |  |  |
| *FILLER METALS (OW-404)Spec. No. (SFA) |  |  |
|  |  |  |
| AWS No. (Class) |  |  |
| F-No. |  |  |
| A-No. |  |  |
| Size of Filler Metals |  |  |
| Weld Metal |  |  |
| Thickness Range: |  |  |
| GrooveFillet |  |  |
| Electrode-Flux (Class) |  |  |
| Flux Trade Name |  |  |
| Consumable Insert |  |  |
| Other |  |  |
| *Each base metal-filler metal combination should be recorded individually. |  |  |
|  | $m$ the Order | ASME, 22 Law Drive, Box 2300, Fa |



## 2004 SECTION IX

## QW-483 SUGGESTED FORMAT FOR PROCEDURE QUALIFICATION RECORDS (POR) (See QW-200.2, Section IX, ASME Boiler and Pressure Vessel Code) Record Actual Conditions Used to Weld Test Coupon.



JOINTS (OW-402)

Groove Design of Test Coupon
(For combination qualifications, the deposited weld metal thickness shall be recorded for each filler metal or process used.)


## NONMANDATORY APPENDIX B



## 2004 SECTION IX

## QW-484A SUGGESTED FORMAT A FOR WELDER PERFORMANCE QUALIFICATIONS (WPQ) (See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)

| Welder's name $\qquad$ Identification No. Test Description |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Identification of WPS followed <br> Specification of base metal(s) |  |  | $\qquad$$\square$ Test coupon Thickness $\qquad$ | $\square$ Production weld |  |
|  |  |  |  |  |
| Testing Conditions and Qualification Limits |  |  |  |  |  |
| Welding Variables (OW-350) |  | Actual Values |  | Range Qualified |  |  |
| Welding process(es) |  |  |  |  |  |
| Type (ie; manual, semi-auto) used |  |  |  |  |  |
| Backing (metal, weld metal, double-welded, etc.) |  |  |  |  |  |
| $\square$ Plate $\square$ Pipe (enter diameter if pipe or tube) |  |  |  |  |  |
| Base metal P- or S-Number to P- or S-Number |  |  |  |  |  |
| Filler metal or electrode specification(s) (SFA) (info. only) |  |  |  |  |  |
| Filler metal or electrode classification(s) (info. only) |  |  |  |  |  |
| Filler metal F-Number(s) |  |  |  |  |  |
| Consumable insert (GTAW or PAW) |  |  |  |  |  |
| Filler type (solid/metal or flux cored/powder) (GTAW or PAW) |  |  |  |  |  |
| Deposit thickness for each process |  |  |  |  |  |
| Process 1: $\square \square 3$ layers minimum $\square$ Yes |  |  |  |  |  |
| Process 2: 3 layers minimum $\square \mathrm{Yes} \square$ No |  |  |  |  |  |
| Position qualified (2G, 6G, 3F, etc.) |  |  |  |  |  |
| Vertical progression (uphill or downhill) |  |  |  |  |  |
| Type of fuel gas (OFW) |  |  |  |  |  |
| Inert gas backing (GTAW, PAW, GMAW) |  |  |  |  |  |
| Transfer mode (spray/globular or pulse to short circuit-GMAW) |  |  |  |  |  |
| GTAW current type/polarity (AC, DCEP, DCEN) |  |  |  |  |  |

## RESULTS

Visual Examination of Completed Weld (OW-302.4)
$\square$ Bend test; $\square$ Transverse root and face [OW-462.3(a); $\square$ Longitudinal root and face [OW-462.3(b); $\square$ Side (OW-462.2);
$\square$ Pipe bend specimen, corrosion-resistant overlay [OW-462.5(c)]; $\square$ Plate bend specimen, corrosion-resistant overlay [OW-462.5(d)]; $\square$ Macro test for fusion [QW-462.5(b)]; $\square$ Macro test for fusion [QW-462.5(e)]

| Type | Result | Type | Result | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  |  |  |  |

Alternative radiographic examination results (OW-191) Fillet weld - fracture test ( $\mathrm{OW}-180$ )
$\qquad$
$\qquad$
gth and percent of defect
$\square$ Macro examination (OW-184) $\qquad$ Fillet size (in x $\qquad$ Concavity/convexity (in.) Other tests $\qquad$
$\qquad$ Company
Film or specimens evaluated by
Mechanical tests conducted by Laboratory test no.
Welding supervised by
$\qquad$

We certify that the statements in this record are correct and that the test coupons were prepared, welded, and tested in accordance with the requirements of Section IX of the ASME Boiler and Pressure Vessel Code.

Organization $\qquad$
Date $\qquad$ By $\qquad$

## NONMANDATORY APPENDIX B

## QW-484B SUGGESTED FORMAT B FOR WELDING OPERATOR PERFORMANCE QUALIFICATIONS (WOPQ) (See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)

| Welding operator's name $\qquad$ Identification no. Test Description (Information On/y) |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Identification of WPS followed $\square \square$ Test coupon $\square$ Production weld |  |  |
| Specification of base metal(s) __ Thickness _ |  |  |
| Base metal P or S-Number $\qquad$ to P or S -Number $\qquad$ Position (2G, 6G, 3F, etc.)$\square$ Plate $\square$ Pipe (enter diameter if pipe or tube): $\qquad$ |  |  |
|  |  |  |
| Filler metal (SFA) specification ___ Filler metal or electrode classification |  |  |
| Testing Conditions and Qualification Limits When Using Automatic Welding Equipment |  |  |
| Welding Variables (QW-361.1) | Actual Values | Range Qualified |
| Type of welding (Automatic) |  |  |
| Welding process |  |  |
| Filler metal (EBW or LBW) |  |  |
| Type of laser for LBW ( $\mathrm{CO}_{2}$ to YAG, etc.) |  |  |
| Continuous drive or inertia welding (FW) |  |  |
| Vacuum or out of vacuum (EBW) |  |  |

Testing Conditions and Qualification Limits When Using Machine Welding Equipment Welding Variables (OW-361.2)
Type of welding (machine)
Welding process
Direct or remote visual control
Automatic arc voltage control (GTAW)
Automatic joint tracking
Position qualified (2G, 6G, 3F, etc.)
Consumable inserts (GTAW or PAW)
Backing (metal, weld metal, etc.)
Single or multiple passes per side

$\qquad$

## RESULTS

Visual Examination of Completed Weld (OW-302.4)
$\square$ Bend test; $\square$ Transverse root and face [QW-462.3(a)] $\square$ Longitudinal root and face [QW-462.3(b)]; $\square$ Side (QW-462.2); $\square$ Pipe bend specimen, corrosion-resistant overlay [QW-462.5(c)]; $\square$ Plate bend specimen, corrosion-resistant overlay [QW-462.5(d)]; $\square$ Macro test for fusion [OW-462.5(b)]; $\square$ Macro test for fusion [OW-462.5(e)]

| Type | Result | Type | Result | Type | Result |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  |  |  |  |


requirements of Section IX of the ASME Code.
Organization

Date $\qquad$ By

## QW-485 SUGGESTED FORMAT FOR DEMONSTRATION OF STANDARD WELDING PROCEDURE SPECIFICATIONS (SWPS) (See Article V)

| Demonstration Welding Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Specification, Type, and Grade of Base Metal(s): to Specification, Type, and Grade of Base Metal(s): |  |  |  |  |  |
| Base Metal P- or S-Number _ to Base Metal P- or S-Number _ Thickness: |  |  |  |  |  |
| Welding Process(es) used: |  |  |  |  |  |
| $\square$ Plate $\square$ Pipe (Enter Diameter of Pipe or Tube): |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Backing (Metal, Weld Metal, Backwelded, etc.): <br> Filler Metal (SFA) Specification: |  |  |  |  |  |
|  |  |  |  |  |  |
| Filler Metal or Electrode Classification: |  |  |  |  |  |
| Filler Metal or Electrode Trade Name: |  |  |  |  |  |
| Tungsten Electrode Type and Size for GTAW: |  |  |  |  |  |
| Consumable Insert Class and Size for GTAW or PAW: |  |  |  |  |  |
| Shielding Gas Composition and Flow Rate for GTAW, PAW, GMAW: |  |  |  |  |  |
| Preheat Temperature ( ${ }^{\circ}$ or ${ }^{\circ} \mathrm{C}$ ): |  |  |  |  |  |
| Position (1G, 2G, etc.) of Weld: |  |  |  |  |  |
| Progression (Uphill or Downhill): |  |  |  |  |  |
| Interpass Cleaning Method: |  |  |  |  |  |
| Measured InterpassTemperature ( ${ }^{\circ} \mathrm{F}$ or ${ }^{\circ} \mathrm{C}$ ): |  |  |  |  |  |
| Approximate Deposit Thickness for Each Filler Metal or Electrode Type (in.): |  |  |  |  |  |
| Current Type/Polarity (AC, DCEP, DECN): |  |  |  |  |  |
| Postweld Heat Treatment Time and Temperature: |  |  |  |  |  |
| Visual Examination of Completed Weld: |  |  |  | Date of Test: |  |
| Bend Test | $\square$ Transverse Root and Face [QW-462.3(a)] |  |  | Side [OW-462.2] |  |
| Type | Result | Type | Result | Type | Result |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Alternative Radiographic Examination Results: |  |  |  |  |  |
| Specimens Evaluated By: $\qquad$ Title: $\qquad$ C |  |  |  |  |  |
| Welding Supervised By: $\qquad$ Title: $\qquad$ Compa |  |  |  |  |  |
| Welder's Name: |  |  |  |  |  |
| We certify that the statements in this record are correct and that the weld described above was prepared, welded, and tested in accordance with the requirements of Section IX of the ASME Boiler and Pressure Vessel Code. |  |  |  |  |  |
| Manufacturer or Contractor: |  |  |  |  |  |
| $\mathrm{By}: \square$ | - | - | Demo | r: |  |

## NONMANDATORY APPENDIX B

| QB-482 SUGGESTED FORMAT FOR BRAZING PROCEDURE SPECIFICATIONS (BPS) (See QB-200.1 , Section IX, ASME Boiler and Pressure Vessel Code) |  |
| :---: | :---: |
| Company Name: $\qquad$ <br> BPS Number: $\qquad$ <br> Supporting PQRs: $\qquad$ <br> Brazing Process(es): $\qquad$ | Revision: $\qquad$ Date Issued: <br> Type(s): |
| Joint Design: Type: $\qquad$ <br> Overlap: <br> Minimum: $\qquad$ | $\qquad$ <br> Joints (QB-408) <br> Clearance: <br> Maximum: |
| Base Metals (OB-402) <br> P/S Number $\qquad$ <br> to P/S Number $\qquad$ <br> Other: $\qquad$ <br> Base Metal Thickness <br> Minimum: $\qquad$ <br> Maximum: $\qquad$ | Filler Metals (QB-403) <br> Specification Number: $\qquad$ <br> AWS Classification: $\qquad$ <br> F-Number: $\qquad$ <br> Filler Form: $\qquad$ $\qquad$ |
| Post Braze Heat Treatment (OB-409) <br> Temperature: $\qquad$ <br> Max. Holding Time: $\qquad$ $\qquad$ <br> Flow Positions (QB-407) <br> Positions Permitted: $\qquad$ <br> Flow Direction: $\qquad$ | Brazing Flux, Fuel Gas, or Atmosphere (QB-406) <br> Flux Type or Trade Name: $\qquad$ <br> Fuel Gas: <br> Flame Type: $\qquad$ <br> Recommended Brazing Temperature: $\qquad$ <br> Other: $\qquad$ |
| Initial Cleaning: - | nique (OB-410) and Other Information |
| Flux Application: $\qquad$ <br> Torch Tip Sizes: $\qquad$ <br> Final Cleaning: $\qquad$ <br> Inspection: $\qquad$ |  |
|  | Manufacturer: By: <br> Title: $\qquad$ Date: $\qquad$ |

## QB-483 SUGGESTED FORMAT FOR BRAZING PROCEDURE QUALIFICATION RECORDS (PQR) (See QB-200.2, Section IX, ASME Boiler and Pressure Vessel Code) Record of Actual Conditions Used to Braze Test Coupon



## Bend Tests

| Type | Results | Type | Results |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  |  |  |  |

## Peel or Section Tests

| Type | Results | Type | Results |
| :---: | :---: | :---: | :---: |
|  | - |  |  |
|  |  |  |  |

Other Tests:
Brazer's Name:
Brazing of Test Coupon Supervised by: __ ID No.:

Test

Test Specimens Evaluated by:
Company:
Laboratory Test Number:
We hereby certify that the statements in this record are correct and that the test welds were prepared, brazed, and tested in accordance with the requirements of Section IX of the ASME Boiler and Pressure Vessel Code.
$\qquad$

## NONMANDATORY APPENDIX B

## QB-484 SUGGESTED FORMAT FOR BRAZER/BRAZING OPERATOR PERFORMANCE QUALIFICATIONS (BPQ) (See QB-301, Section IX, ASME Boiler and Pressure Vessel Code)

 P-NUMBER LISTING

| $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| Steel and Steel Alloys |  |  |  |
| 1 | 1 | SA-36 |  |
| 1 | 1 | SA-53 | Type E, Gr. A |
| 1 | 1 | SA-53 | Type E, Gr. B |
| 1 | 1 | SA-53 | Type F |
| 1 | 1 | SA-53 | Type S, Gr. A |
| 1 | 1 | SA-53 | Type S, Gr. B |
| 1 | 1 | SA-106 | A |
| 1 | 1 | SA-106 | B |
| 1 | 1 | SA-134 | . |
| 1 | 1 | SA-135 | A |
| 1 | 1 | SA-135 | B |
| 1 | 1 | SA-178 | A |
| 1 | 1 | SA-178 | C |
| 1 | 1 | SA-179 | ... |
| 1 | 1 | SA-181 | CI. 60 |
| 1 | 1 | SA-192 | ... |
| 1 | 1 | SA-210 | A-1 |
| 1 | 1 | SA-214 |  |
| 1 | 1 | SA-216 | WCA |
| 1 | 1 | SA-234 | WPB |
| 1 | 1 | SA-283 | A |
| 1 | 1 | SA-283 | B |
| 1 | 1 | SA-283 | C |
| 1 | 1 | SA-283 | D |
| 1 | 1 | SA-285 | A |
| 1 | 1 | SA-285 | B |
| 1 | 1 | SA-285 | C |
| 1 | 1 | SA-333 | 1 |
| 1 | 1 | SA-333 | 6 |
| 1 | 1 | SA-334 | 1 |
| 1 | 1 | SA-334 | 6 |
| 1 | 1 | SA-350 | LFI |
| 1 | 1 | SA-352 | LCA |
| 1 | 1 | SA-352 | LCB |
| 1 | 1 | SA-369 | FPA |
| 1 | 1 | SA-369 | FPB |
| 1 | 1 | SA-372 | A |
| 1 | 1 | SA-414 | A |
| 1 | 1 | SA-414 | B |
| 1 | 1 | SA-414 | C |
| 1 | 1 | SA-414 | D |
| 1 | 1 | SA-414 | E |
| 1 | 1 | SA-420 | WPL6 |
| 1 | 1 | SA-513 | 1008 |


| P- No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| 1 | 1 | SA-513 | 1010 |
| 1 | 1 | SA-513 | 1015 |
| 1 | 1 | SA-515 | 60 |
| 1 | 1 | SA-515 | 65 |
| 1 | 1 | SA-516 | 55 |
| 1 | 1 | SA-516 | 60 |
| 1 | 1 | SA-516 | 65 |
| 1 | 1 | SA-524 | I |
| 1 | 1 | SA-524 | II |
| 1 | 1 | SA-556 | A2 |
| 1 | 1 | SA-556 | B2 |
| 1 | 1 | SA-557 | A2 |
| 1 | 1 | SA-557 | B2 |
| 1 | 1 | SA-562 | $\ldots$ |
| 1 | 1 | SA-587 | $\ldots$ |
| 1 | 1 | SA-660 | WCA |
| 1 | 1 | SA-662 | A |
| 1 | 1 | SA-662 | B |
| 1 | 1 | SA-671 | CA55 |
| 1 | 1 | SA-671 | CB60 |
| 1 | 1 | SA-671 | CB65 |
| 1 | 1 | SA-671 | CC60 |
| 1 | 1 | SA-671 | CC65 |
| 1 | 1 | SA-671 | CE55 |
| 1 | 1 | SA-671 | CE60 |
| 1 | 1 | SA-672 | A45 |
| 1 | 1 | SA-672 | A50 |
| 1 | 1 | SA-672 | A55 |
| 1 | 1 | SA-672 | B55 |
| 1 | 1 | SA-672 | B60 |
| 1 | 1 | SA-672 | B65 |
| 1 | 1 | SA-672 | C55 |
| 1 | 1 | SA-672 | C60 |
| 1 | 1 | SA-672 | C65 |
| 1 | 1 | SA-672 | E55 |
| 1 | 1 | SA-672 | E60 |
| 1 | 1 | SA-675 | 45 |
| 1 | 1 | SA-675 | 50 |
| 1 | 1 | SA-675 | 55 |
| 1 | 1 | SA-675 | 60 |
| 1 | 1 | SA-675 | 65 |
| 1 | 1 | SA-695 | Type B, Gr. 35 |
| 1 | 1 | SA-696 | B |
| 1 | 1 | SA-727 |  |


| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | SA-765 | I | 1 | 2 | SA-691 | CMS-75 |
| 1 | 1 | SA-836 |  | 1 | 2 | SA-691 | CMSH-70 |
| 1 | 1 | SA-1008 | CS Type A | 1 | 2 | SA-695 | Type B, Gr. 40 |
| 1 | 1 | SA-1008 | CS Type B | 1 | 2 | SA-696 | C |
| 1 | 1 | SA/AS | 7-430 | 1 | 2 | SA-737 | B |
|  |  | 1548 |  | 1 | 2 | SA-738 | A |
| 1 | 1 | SA/AS | 7-460 | 1 | 2 | SA-765 | II |
|  |  | 1548 |  | 1 | 2 | SA/AS | 5-490 |
| 1 | 1 | SA/CSA | Gr. 38W |  |  | 1548 |  |
|  |  | G40.21 |  | 1 | 2 | SA/AS | 7-490 |
| 1 | 1 | SA/CSA | Gr. 44W |  |  | 1548 |  |
|  |  | G40.21 |  | 1 | 2 | SA/JIS | SGV480 |
| 1 | 1 | $\begin{aligned} & \text { SA/EN } \\ & \text { 10028-2 } \end{aligned}$ | 295GH |  |  | G3118 |  |
| 1 | 1 | SA/EN | 275 NH | 1 | 3 | SA-333 | 10 |
|  |  | 10028-3 |  | 1 | 3 | SA-537 | CI. 2 |
|  |  |  |  | 1 | 3 | SA-537 | CI. 3 |
| 1 | 2 | SA-105 | . . | 1 | 3 | SA-671 | CD80 |
| 1 | 2 | SA-106 | C | 1 | 3 | SA-672 | D80 |
| 1 | 2 | SA-178 | D | 1 | 3 | SA-691 | CMSH-80 |
| 1 | 2 | SA-181 | CI. 70 | 1 | 3 | SA-737 | C |
| 1 | 2 | SA-210 | C | 1 | 3 | SA-738 | B |
| 1 | 2 | SA-216 | WCB | 1 | 3 | SA-738 | C |
| 1 | 2 | SA-216 | WCC | 1 | 3 | SA-765 | IV |
| 1 | 2 | SA-234 | WPC | 1 | 3 | SA-812 | 65 |
| 1 | 2 | SA-266 | 2 |  |  |  |  |
| 1 | 2 | SA-266 | 3 | 1 | 4 | SA-724 | A |
| 1 | 2 | SA-266 | 4 | 1 | 4 | SA-724 | B |
| 1 | 2 | SA-266 SA-299 | 4 | 1 | 4 | SA-724 | C |
| 1 | 2 | SA-299 | LF2 | 1 | 4 | SA-812 | 80 |
| 1 | 2 | SA-352 | LCC |  |  |  |  |
| 1 | 2 | SA-372 | B | 3 3 | 1 | SA-204 SA-209 | A T1 |
| 1 | 2 | SA-414 | F | 3 | 1 | SA-209 | Tla |
| 1 | 2 | SA-414 | G | 3 | 1 | SA-209 | Tlb |
| 1 | 2 | SA-455 | . . | 3 | 1 | SA-213 | T2 |
| 1 | 2 | SA-487 | Gr. 16, CI. A | 3 | 1 | SA-217 |  |
| 1 | 2 | SA-508 | 1 | 3 | 1 | SA-234 | WP1 |
| 1 | 2 | SA-508 | 1 A | 3 | 1 | SA-250 | T1 |
| 1 | 2 | SA-515 | 70 | 3 | 1 | SA-250 | Tla |
| 1 | 2 | SA-516 | 70 | 3 | 1 | SA-250 | Tlb |
| 1 | 2 | SA-537 | CI. 1 |  |  |  |  |
| 1 | 2 | SA-541 | 1 | 3 | 1 | SA-335 | P1 |
| 1 | 2 | SA-541 | 1 A | 3 | 1 | SA-335 | P2 |
| 1 | 2 | SA-556 | C2 | 3 | 1 | SA-335 | P15 |
| 1 | 2 | SA-557 | C2 | 3 | 1 | SA-352 | LCl |
| 1 | 2 | SA-660 | WCB |  |  |  |  |
| 1 | 2 | SA-660 | WCC | 3 | 1 | SA-369 SA-369 | FP2 |
| 1 | 2 | SA-662 | C | 3 | 1 | SA-387 | Gr. 2, CI. 1 |
| 1 | 2 | SA-671 | CB70 | 3 | 1 | SA-426 | CP1 |
| 1 | 2 | SA-671 | CC70 | 3 | 1 | SA-426 | CP2 |
| 1 | 2 | SA-671 | CD70 | 3 | 1 | SA-426 | CP15 |
| 1 | 2 | SA-671 | CK75 | 3 | 1 | SA-426 SA-672 | LP15 L65 |
| 1 | 2 | SA-672 | B70 | 3 | 1 | SA-691 | $1 / 2 \mathrm{CR}$ |
| 1 | 2 | SA-672 | C70 | 3 | 1 | SA-691 | CM-65 |
| 1 | 2 | SA-672 | D70 |  |  |  |  |
| 1 | 2 | SA-672 | N75 | 3 | 2 | SA-182 | F1 |
| 1 | 2 | SA-675 | 70 | 3 | 2 | SA-182 | F2 |

## 2004 SECTION IX

| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 2 | SA-204 | B | 4 | 1 | SA-335 | Pll |
| 3 | 2 | SA-204 | C | 4 | 1 | SA-335 | P12 |
| 3 | 2 | SA-302 | A | 4 | 1 | SA-336 | Fll, CI. 2 |
| 3 | 2 | SA-336 | Fl | 4 | 1 | SA-336 | Fll, Cl. 3 |
| 3 | 2 | SA-387 | Gr. 2, Cl. 2 | 4 | 1 | SA-336 | Fll, Cl. 1 |
| 3 | 2 | SA-672 | H75 | 4 | 1 | SA-336 | F12 |
| 3 | 2 | SA-672 | L70 | 4 | 1 | SA-369 | FP11 |
| 3 | 2 | SA-672 | L75 | 4 | 1 | SA-369 | FP12 |
| 3 | 2 | SA-691 | $1 / 2 \mathrm{CR}, \mathrm{Cl} .2$ | 4 | 1 | SA-387 | 11, CI. 1 |
| 3 | 2 | SA-691 | CM-70 | 4 | 1 | SA-387 | 11, CI. 2 |
| 3 | 2 | SA-691 | CM-75 | 4 | 1 | SA-387 | 12, CI. 1 |
|  |  |  |  | 4 | 1 | SA-387 | 12, CI. 2 |
| 3 | 3 | SA-302 | B | 4 | 1 | SA-426 | CP11 |
| 3 | 3 | SA-302 | C | 4 | 1 | SA-426 | CP12 |
| 3 | 3 | SA-302 | D | 4 | 1 | SA-541 | 11, CI. 4 |
| 3 | 3 | SA-487 | Gr. 2, CI. A | 4 | 1 | SA-691 | 1 CR |
| 3 | 3 | SA-487 | Gr. 2, CI. B | 4 | 1 | SA-691 | $11 / 4 C R$ |
| 3 | 3 | SA-487 | Gr. 4, CI. A | 4 | 1 | SA-739 | Bll |
| 3 | 3 | SA-508 | 2, CI. 1 | 4 | 2 | SA-333 | 4 |
| 3 | 3 | SA-508 | 2, CI. 2 | 4 | 2 | SA-423 | 1 |
| 3 | 3 | SA-508 | 3, CI. 1 | 4 | 2 | SA-423 | 2 |
| 3 | 3 | SA-508 | 3, CI. 2 |  |  |  |  |
| 3 | 3 | SA-508 | 4N, CI. 3 | 5 A | 1 | SA-182 | F21 |
| 3 | 3 | SA-533 | Type A, Cl. 1 | 5 A | 1 | SA-182 | $\text { F22, CI. } 1$ |
| 3 | 3 | SA-533 | Type A, CI. 2 | 5 A | 1 | SA-182 | $\mathrm{F} 22, \mathrm{Cl} .3$ |
| 3 | 3 | SA-533 | Type B, CI. 1 | 5A | 1 | SA-213 | T21 |
| 3 | 3 | SA-533 | Type B, Cl. 2 | 5 A | 1 | SA-213 | T22 |
| 3 | 3 | SA-533 | Type C, CI. 1 | 5 A | 1 | SA-217 | WC9 |
| 3 | 3 | SA-533 | Type C, CI. 2 | 5 A | 1 | SA-234 | $\text { WP22, CI. } 1$ |
| 3 | 3 | SA-533 | Type D, CI. 1 | 5 A | 1 | SA-250 | T22 |
| 3 | 3 | SA-533 | Type D, CI. 2 | 5 A | 1 | SA-335 | P21 |
| 3 | 3 | SA-541 | 2, Cl. 1 | 5 A | 1 | SA-335 | P22 |
| 3 | 3 | SA-541 | 2, CI. 2 | 5A | 1 | SA-336 | F21, CI. 3 |
| 3 | 3 | SA-541 | 3, CI. 1 | 5 A | 1 | SA-336 | F21, CI. 1 |
| 3 | 3 | SA-541 | 3, CI. 2 | 5 A | 1 | SA-336 | F22, CI. 3 |
| 3 | 3 | SA-543 | B Cl. 3 | 5 A | 1 | SA-336 | F22, CI. 1 |
| 3 | 3 | SA-543 | C Cl. 3 | 5 A | 1 | SA-369 | FP21 |
| 3 | 3 | SA-672 | H80 | 5 A | 1 | SA-369 | FP22 |
| 3 | 3 | SA-672 | J80 | 5 A | 1 | SA-387 | 21, Cl. 1 |
| 3 | 3 | SA-672 | J90 | 5 A | 1 | SA-387 | 21, CI. 2 |
| 3 | 3 | SA-672 | J90 | 5 A | 1 | SA-387 | 22, CI. 1 |
| 4 | 1 | SA-182 | Fll, CI. 1 | 5 A | 1 | SA-387 | 22, CI. 2 |
| 4 | 1 | SA-182 | Fll, CI. 2 | 5 A | 1 | SA-426 | CP21 |
| 4 | 1 | SA-182 | Fll, CI. 3 | 5 A | 1 | SA-426 | CP22 |
| 4 | 1 | SA-182 | F12, CI. 1 | 5 A | 1 | SA-691 | $21 / 4 \mathrm{CR}$ |
| 4 | 1 | SA-182 | F12, CI. 2 | 5 A | 1 | SA-691 | 3CR |
|  |  |  |  | 5 A | 1 | SA-739 | B22 |
| 4 | 1 | SA-202 | A |  |  |  |  |
| 4 | 1 | SA-202 | B | 5B | 1 | SA-182 | F5 |
| 4 | 1 | SA-213 | Tll | 5B | 1 | SA-182 | F5a |
| 4 | 1 | SA-213 | T12 | 5B | 1 | SA-182 | F9 |
| 4 | 1 | SA-217 | WC4 | 5B | 1 | SA-213 | T5 |
| 4 | 1 | SA-217 | WC5 | 5B | 1 | SA-213 | T5b |
| 4 | 1 | SA-217 | WC6 | 5B | 1 | SA-213 | T5c |
| 4 | 1 | SA-234 | WP11, CI. 1 | 5B | 1 | SA-213 | T9 |
| 4 | 1 | SA-234 | WP12, CI. 1 | 5B | 1 | SA-217 | C5 |
| 4 | 1 | SA-250 | Tll | 5B | 1 | SA-217 | Cl 2 |


| P- No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| 5B | 1 | SA-234 | WP5 |
| 5B | 1 | SA-234 | WP9 |
| 5B | 1 | SA-335 | P5 |
| 5B | 1 | SA-335 | P5b |
| 5B | 1 | SA-335 | P5c |
| 5B | 1 | SA-335 | P9 |
| 5B | 1 | SA-336 | F5 |
| 5B | 1 | SA-336 | F5A |
| 5B | 1 | SA-336 | F9 |
| 5B | 1 | SA-369 | FP5 |
| 5B | 1 | SA-369 | FP9 |
| 5B | 1 | SA-387 | 5, Cl. 1 |
| 5B | 1 | SA-387 | 5, Cl. 2 |
| 5B | 1 | SA-426 | CP5 |
| 5B | 1 | SA-426 | CP5b |
| 5B | 1 | SA-426 | CP9 |
| 5B | 1 | SA-691 | 5CR |
| 5B | 2 | SA-182 | F91 |
| 5B | 2 | SA-213 | T91 |
| 5B | 2 | SA-234 | WP91 |
| 5B | 2 | SA-335 | P91 |
| 5B | 2 | SA-336 | F91 |
| 5B | 2 | SA-369 | FP91 |
| 5B | 2 | SA-387 | Gr. 91, CI. 2 |
| 5 C | 1 | SA-182 | F3V |
| 5 C | 1 | SA-182 | F22V |
| 5 C | 1 | SA-336 | F3V |
| 5 C | 1 | SA-336 | F22V |
| 5 C | 1 | SA-487 | Gr. 8 Cl . A |
| 5 C | 1 | SA-508 | 3 V |
| 5 C | 1 | SA-508 | 22, CI. 3 |
| 5 C | 1 | SA-541 | 3 V |
| 5 C | 1 | SA-541 | 22 V |
| 5 C | 1 | SA-541 | 22, CI. 3 |
| 5 C | 1 | SA-542 | A, Cl. 4 |
| 5 C | 1 | SA-542 | A, CI. 4a |
| 5 C | 1 | SA-542 | B, CI. 4 |
| 5 C | 1 | SA-542 | B, CI. 4a |
| 5 C | 1 | SA-542 | C, Cl. 4 |
| 5 C | 1 | SA-542 | C, CI. 4a |
| 5 C | 1 | SA-542 | D, CI. 4a |
| 5 C | 1 | SA-832 | 21 V |
| 5 C | 1 | SA-832 | 22 V |
| 5 C | 3 | SA-542 | A, CI. 3 |
| 5 C | 3 | SA-542 | B, Cl. 3 |
| 5 C | 3 | SA-542 | C, Cl. 3 |
| 5 C | 4 | SA-487 | Gr. 8 Cl . B |
| 5 C | 4 | SA-487 | Gr. 8 Cl . C |
| 5 C | 4 | SA-541 | 22, CI. 4 |
| 5 C | 4 | SA-542 | A, Cl. 1 |
| 5 C | 4 | SA-542 | B, CI. 1 |
| 5 C | 4 | SA-542 | C, Cl. 1 |
| 5 C | 5 | SA-541 | 22, CI. 5 |


| $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| 5 C | 5 | SA-542 | A, Cl. 2 |
| 5 C | 5 | SA-542 | B, Cl. 2 |
| 5 C | 5 | SA-542 | C, Cl. 2 |
| 6 | 1 | SA-182 | F6a, Cl. 1 |
| 6 | 1 | SA-240 | 410 |
| 6 | 1 | SA-268 | TP410 |
| 6 | 1 | SA-479 | 403 |
| 6 | 1 | SA-479 | 410 |
| 6 | 2 | SA-182 | F429 |
| 6 | 2 | SA-240 | 429 |
| 6 | 2 | SA-268 | TP429 |
| 6 | 3 | SA-182 | F6a, Cl. 2 |
| 6 | 3 | SA-182 | F6b |
| 6 | 3 | SA-217 | CAl5 |
| 6 | 3 | SA-336 | F6 |
| 6 | 3 | SA-426 | CPCAl5 |
| 6 | 3 | SA-487 | CAl5 CI. B |
| 6 | 3 | SA-487 | CAl5 CI. C |
| 6 | 3 | SA-487 | CA15 CI. D |
| 6 | 3 | SA-487 | CA15M CI. A |
| 6 | 4 | SA-182 | F6NM |
| 6 | 4 | SA-240 | S41500 |
| 6 | 4 | SA-268 | S41500 |
| 6 | 4 | SA-352 | CA6NM |
| 6 | 4 | SA-479 | 414 |
| 6 | 4 | SA-479 | S41500 |
| 6 | 4 | SA-487 | CA6NM CI. A |
| 6 | 4 | SA-487 | CA6NM CI. B |
| 6 | 4 | SA-731 | S41500 |
| 6 | 4 | SA-815 | S41500 |
| 7 | 1 | SA-240 | Type 405 |
| 7 | 1 | SA-240 | Type 409 |
| 7 | 1 | SA-240 | Type 410S |
| 7 | 1 | SA-268 | S40800 |
| 7 | 1 | SA-268 | TP405 |
| 7 | 1 | SA-268 | TP409 |
| 7 | 1 | SA-268 | TP430Ti |
| 7 | 1 | SA-479 | 405 |
| 7 | 2 | SA-182 | F430 |
| 7 | 2 | SA-240 | S44400 |
| 7 | 2 | SA-240 | Type 430 |
| 7 | 2 | SA-240 | Type 439 |
| 7 | 2 | SA-268 | $18 \mathrm{Cr}-2 \mathrm{Mo}$ |
| 7 | 2 | SA-268 | TP430 |
| 7 | 2 | SA-268 | TP439 |
| 7 | 2 | SA-479 | 430 |
| 7 | 2 | SA-479 | 439 |
| 7 | 2 | SA-479 | S44400 |
| 7 | 2 | SA-731 | 18Cr-2Mo |
| 7 | 2 | SA-731 | TP439 |
| 7 | 2 | SA-803 | TP439 |
| 8 | 1 | SA-182 | S30600 |


| $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. | $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. <br> No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 1 | SA-182 | F304 | 8 | 1 | SA-240 | Type 347 |
| 8 | 1 | SA-182 | F304H | 8 | 1 | SA-240 | Type 347H |
| 8 | 1 | SA-182 | F304L | 8 | 1 | SA-240 | Type 348 |
| 8 | 1 | SA-182 | F304LN | 8 | 1 | SA-240 | Type 348H |
| 8 | 1 | SA-182 | F304N | 8 | 1 | SA-240 | Type XM-15 |
| 8 | 1 | SA-182 | F316 | 8 | 1 | SA-240 | Type XM-21 |
| 8 | 1 | SA-182 | F316H | 8 | 1 | SA-249 | TP304 |
| 8 | 1 | SA-182 | F316L | 8 | 1 | SA-249 | TP304H |
| 8 | 1 | SA-182 | F316LN | 8 | 1 | SA-249 | TP304L |
| 8 | 1 | SA-182 | F316 | 8 | 1 | SA-249 | TP304LN |
| 8 | 1 | SA-182 | F317 | 8 | 1 | SA-249 | TP304N |
| 8 | 1 | SA-182 | F317L | 8 | 1 | SA-249 | TP316 |
| 8 | 1 | SA-182 | F321 | 8 | 1 | SA-249 | TP316H |
| 8 | 1 | SA-182 | F321H | 8 | 1 | SA-249 | TP316L |
| 8 | 1 | SA-182 | F347 | 8 | 1 | SA-249 | TP316LN |
| 8 | 1 | SA-182 | F347H | 8 | 1 | SA-249 | TP316N |
| 8 | 1 | SA-182 | F348 | 8 | 1 | SA-249 | TP317 |
| 8 | 1 | SA-182 | F348H | 8 | 1 | SA-249 | TP317L |
| 8 | 1 | SA-213 | TP304 | 8 | 1 | SA-249 | TP321 |
| 8 | 1 | SA-213 | TP304H | 8 | 1 | SA-249 | TP321H |
| 8 | 1 | SA-213 | TP304L | 8 | 1 | SA-249 | TP347 |
| 8 | 1 | SA-213 | TP304LN | 8 | 1 | SA-249 | TP347H |
| 8 | 1 | SA-213 | TP304N | 8 | 1 | SA-249 | TP348 |
| 8 | 1 | SA-213 | TP316 | 8 | 1 | SA-249 | TP348H |
| 8 | 1 | SA-213 | TP316H | 8 | 1 | SA-249 | TP XM-15 |
| 8 | 1 | SA-213 | TP316L | 8 | 1 | SA-312 | S30600 |
| 8 | 1 | SA-213 | TP316LN | 8 | 1 | SA-312 | TP304 |
| 8 | 1 | SA-213 | TP316N | 8 | 1 | SA-312 | TP304H |
| 8 | 1 | SA-213 | TP321 | 8 | 1 | SA-312 | TP304L |
| 8 | 1 | SA-213 | TP321H | 8 | 1 | SA-312 | TP304LN |
| 8 | 1 | SA-213 | TP347 | 8 | 1 | SA-312 | TP304N |
| 8 | 1 | SA-213 | TP347H | 8 | 1 | SA-312 | TP316 |
| 8 | 1 | SA-213 | TP347HFG | 8 | 1 | SA-312 | TP316H |
| 8 | 1 | SA-213 | TP348 | 8 | 1 | SA-312 | TP316L |
| 8 | 1 | SA-213 | TP348H | 8 | 1 | SA-312 | TP316LN |
| 8 | 1 | SA-213 | XM-15 | 8 | 1 | SA-312 | TP316N |
| 8 | 1 | SA-240 | S30500 | 8 | 1 | SA-312 | TP317 |
| 8 | 1 | SA-240 | S30600 | 8 | 1 | SA-312 | TP317L |
| 8 | 1 | SA-240 | S31753 | 8 | 1 | SA-312 | TP321 |
| 8 | 1 | SA-240 | Type 302 | 8 | 1 | SA-312 | TP321H |
| 8 | 1 | SA-240 | Type 304 | 8 | 1 | SA-312 | TP347 |
| 8 | 1 | SA-240 | Type 304H | 8 | 1 | SA-312 | TP347H |
| 8 | 1 | SA-240 | Type 304L | 8 | 1 | SA-312 | TP348 |
| 8 | 1 | SA-240 | Type 304LN | 8 | 1 | SA-312 | TP348H |
| 8 | 1 | SA-240 | Type 304N | 8 | 1 | SA-312 | TP XM-15 |
| 8 | 1 | SA-240 | Type 316 | 8 | 1 | SA-336 | F304 |
| 8 | 1 | SA-240 | Type 316Cb | 8 | 1 | SA-336 | F304H |
| 8 | 1 | SA-240 | Type 316H | 8 | 1 | SA-336 | F304L |
| 8 | 1 | SA-240 | Type 316L | 8 | 1 | SA-336 | F304LN |
| 8 | 1 | SA-240 | Type 316LN | 8 | 1 | SA-336 | F304N |
| 8 | 1 | SA-240 | Type 316N | 8 | 1 | SA-336 | F316 |
| 8 | 1 | SA-240 | Type 316Ti | 8 | 1 | SA-336 | F316H |
| 8 | 1 | SA-240 | Type 317 | 8 | 1 | SA-336 | F316L |
| 8 | 1 | SA-240 | Type 317L | 8 | 1 | SA-336 | F316LN |
| 8 | 1 | SA-240 | Type 321 | 8 | 1 | SA-336 | F316N |
| 8 | 1 | SA-240 | Type 321H | 8 | 1 | SA-336 | F321 |


| P- <br> No. | Grp. <br> No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 1 | SA-336 | F321H | 8 | 1 | SA-403 | WP321H |
| 8 | 1 | SA-336 | F347 | 8 | 1 | SA-403 | WP347 |
| 8 | 1 | SA-336 | F347H | 8 | 1 | SA-403 | WP347H |
| 8 | 1 | SA-336 | F348 | 8 | 1 | SA-403 | WP348 |
| 8 | 1 | SA-336 | F348H | 8 | 1 | SA-403 | WP348H |
| 8 | 1 | SA-351 | CF3 | 8 | 1 | SA-409 | TP304 |
| 8 | 1 | SA-351 | CF3A | 8 | 1 | SA-409 | TP304L |
| 8 | 1 | SA-351 | CF3M | 8 | 1 | SA-409 | TP316 |
| 8 | 1 | SA-351 | CF8 | 8 | 1 | SA-409 | TP316L |
| 8 | 1 | SA-351 | CF8A | 8 | 1 | SA-409 | TP317 |
| 8 | 1 | SA-351 | CF8C | 8 | 1 | SA-409 | TP321 |
| 8 | 1 | SA-351 | CF8M | 8 | 1 | SA-409 | TP347 |
| 8 | 1 | SA-351 | CF10 | 8 | 1 | SA-409 | TP348 |
| 8 | 1 | SA-351 | CF10M | 8 | 1 | SA-430 | FP304 |
| 8 | 1 | SA-351 | CG8M | 8 | 1 | SA-430 | FP304H |
| 8 | 1 | SA-358 | 304 | 8 | 1 | SA-430 | FP304N |
| 8 | 1 | SA-358 | 304H | 8 | 1 | SA-430 | FP316 |
| 8 | 1 | SA-358 | 304L | 8 | 1 | SA-430 | FP316H |
| 8 | 1 | SA-358 | 304LN | 8 | 1 | SA-430 | FP316N |
| 8 | 1 | SA-358 | 304 N | 8 | 1 | SA-430 | FP321 |
| 8 | 1 | SA-358 | 316 | 8 | 1 | SA-430 | FP321H |
| 8 | 1 | SA-358 | 316 H | 8 | 1 | SA-430 | FP347 |
| 8 | 1 | SA-358 | 316L | 8 | 1 | SA-430 | FP347 H |
| 8 | 1 | SA-358 | 316 LN | 8 | 1 | SA-430 | FP16-8-2 H |
| 8 | 1 | SA-358 | 316 N | 8 | 1 | SA-451 | CPF3 |
| 8 | 1 | SA-358 | 321 | 8 | 1 | SA-451 | CPF3A |
| 8 | 1 | SA-358 | 347 | 8 | 1 | SA-451 | CPF3M |
| 8 | 1 | SA-358 | 348 | 8 | 1 | SA-451 | CPF8 |
| 8 | 1 | SA-376 | 16-8-2 H | 8 | 1 | SA-451 | CPF8A |
| 8 | 1 | SA-376 | TP304 | 8 | 1 | SA-451 | CPF8C |
| 8 | 1 | SA-376 | TP304H | 8 | 1 | SA-451 | CPF8M |
| 8 | 1 | SA-376 | TP304LN | 8 | 1 | SA-479 | 302 |
| 8 | 1 | SA-376 | TP304N | 8 | 1 | SA-479 | 304 |
| 8 | 1 | SA-376 | TP316 | 8 | 1 | SA-479 | 304H |
| 8 | 1 | SA-376 | TP316H | 8 | 1 | SA-479 | 304L |
| 8 | 1 | SA-376 | TP316LN | 8 | 1 | SA-479 | 304LN |
| 8 | 1 | SA-376 | TP316N | 8 | 1 | SA-479 | 304 N |
| 8 | 1 | SA-376 | TP321 | 8 | 1 | SA-479 | 316 |
| 8 | 1 | SA-376 | TP321H | 8 | 1 | SA-479 | $316 \mathrm{Cb}$ |
| 8 | 1 | SA-376 | TP347 | 8 | 1 | SA-479 | 316 H |
| 8 | 1 | SA-376 | TP347H | 8 | 1 | SA-479 | 316 L |
| 8 | 1 | SA-376 | TP348 | 8 | 1 | SA-479 | 316 LN |
| 8 | 1 | SA-376 | 16-8-2 H | 8 | 1 | SA-479 | $316 \mathrm{~N}$ |
| 8 | 1 | SA-403 | WP304 | 8 | 1 | SA-479 | $316 \mathrm{Ti}$ |
| 8 | 1 | SA-403 | WP304H | 8 | 1 | SA-479 | 321 |
| 8 | 1 | SA-403 | WP304L | 8 | 1 | SA-479 | 321 H |
| 8 | 1 | SA-403 | WP304LN | 8 | 1 | SA-479 | 347 |
| 8 | 1 | SA-403 | WP304N | 8 | 1 | SA-479 | $347 \mathrm{H}$ |
| 8 | 1 | SA-403 | WP316 | 8 | 1 | SA-479 | 348 |
| 8 | 1 | SA-403 | WP316H | 8 | 1 | SA-479 | 348 H |
| 8 | 1 | SA-403 | WP316L | 8 | 1 | SA-479 | S30600 |
| 8 | 1 | SA-403 | WP316LN | 8 | 1 | SA-666 | 302 |
| 8 | 1 | SA-403 | WP316N | 8 | 1 | SA-666 | 304 |
| 8 | 1 | SA-403 | WP317 | 8 | 1 | SA-666 | 304L |
| 8 | 1 | SA-403 | WP317L | 8 | 1 | SA-666 | 304LN |
| 8 | 1 | SA-403 | WP321 | 8 | 1 | SA-666 | 304 N |

## 2004 SECTION IX

| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 1 | SA-666 | 316 | 8 | 2 | SA-213 | TP309S |
| 8 | 1 | SA-666 | 316 L | 8 | 2 | SA-213 | TP310Cb |
| 8 | 1 | SA-666 | 316 N | 8 | 2 | SA-213 | TP310S |
| 8 | 1 | SA-688 | TP304 | 8 | 2 | SA-213 | TP309HCb |
| 8 | 1 | SA-688 | TP304L | 8 | 2 | SA-213 | TP310H |
| 8 | 1 | SA-688 | TP304LN | 8 | 2 | SA-213 | TP310MoLN |
| 8 | 1 | SA-688 | TP304N | 8 | 2 | SA-213 | TP310 HCb |
| 8 | 1 | SA-688 | TP316 | 8 | 2 | SA-240 | S30815 |
| 8 | 1 | SA-688 | TP316L | 8 | 2 | SA-240 | Type 309Cb |
| 8 | 1 | SA-688 | TP316LN | 8 | 2 | SA-240 | Type 309H |
| 8 | 1 | SA-688 | TP316N | 8 | 2 | SA-240 | Type 309HCb |
| 8 | 1 | SA-813 | TP304 | 8 | 2 | SA-240 | Type 309S |
| 8 | 1 | SA-813 | TP304H | 8 | 2 | SA-240 | Type 310Cb |
| 8 | 1 | SA-813 | TP304L | 8 | 2 | SA-240 | Type 310HCb |
| 8 | 1 | SA-813 | TP304LN | 8 | 2 | SA-240 | Type 310 MoLN |
| 8 | 1 | SA-813 | TP304N | 8 | 2 | SA-240 | Type 310S |
| 8 | 1 | SA-813 | TP316 | 8 | 2 | SA-249 | S30815 |
| 8 | 1 | SA-813 | TP316H | 8 | 2 | SA-249 | TP309Cb |
| 8 | 1 | SA-813 | TP316L | 8 | 2 | SA-249 | TP309H |
| 8 | 1 | SA-813 | TP316LN | 8 | 2 | SA-249 | TP309HCb |
| 8 | 1 | SA-813 | TP316N | 8 | 2 | SA-249 | TP309S |
| 8 | 1 | SA-813 | TP317 | 8 | 2 | SA-249 | TP310Cb |
| 8 | 1 | SA-813 | TP317L | 8 | 2 | SA-249 | TP310H |
| 8 | 1 | SA-813 | TP321 | 8 | 2 | SA-249 | TP310S |
| 8 | 1 | SA-813 | TP321H | 8 | 2 | SA-249 | TP310MoLN |
| 8 | 1 | SA-813 | TP347 | 8 | 2 | SA-312 | S30815 |
| 8 | 1 | SA-813 | TP347 H | 8 | 2 | SA-312 | TP309Cb |
| 8 | 1 | SA-813 | TP348 | 8 | 2 | SA-312 | TP309H |
| 8 | 1 | SA-813 | TP348H | 8 | 2 | SA-312 | TP309HCb |
| 8 | 1 | SA-813 | TPXM-15 | 8 | 2 | SA-312 | TP309S |
| 8 | 1 | SA-814 | TP304 | 8 | 2 | SA-312 | TP310Cb |
| 8 | 1 | SA-814 | TP304H | 8 | 2 | SA-312 | TP310H |
| 8 | 1 | SA-814 | TP304L | 8 | 2 | SA-312 | TP310HCb |
| 8 | 1 | SA-814 | TP304LN | 8 | 2 | SA-312 | TP310S |
| 8 | 1 | SA-814 | TP304N | 8 | 2 | SA-312 | TP310MoLN |
| 8 | 1 | SA-814 | TP316 | 8 | 2 | SA-336 | F310 |
| 8 | 1 | SA-814 | TP316H | 8 | 2 | SA-351 | CH8 |
| 8 | 1 | SA-814 | TP316L | 8 | 2 | SA-351 | CH20 |
| 8 | 1 | SA-814 | TP316LN | 8 | 2 | SA-351 | CK20 |
| 8 | 1 | SA-814 | TP316N | 8 | 2 | SA-358 | 309 |
| 8 | 1 | SA-814 | TP317 | 8 | 2 | SA-358 | 309 Cb |
| 8 | 1 | SA-814 | TP317L | 8 | 2 | SA-358 | 309S |
| 8 | 1 | SA-814 | TP321 | 8 | 2 | SA-358 | 310 Cb |
| 8 | 1 | SA-814 | TP321H | 8 | 2 | SA-358 | 310 S |
| 8 | 1 | SA-814 | TP347 | 8 | 2 | SA-358 | S30815 |
| 8 | 1 | SA-814 | TP347 H | 8 | 2 | SA-403 | WP309 |
| 8 | 1 | SA-814 | TP348 | 8 | 2 | SA-403 | WP310 |
| 8 | 1 | SA-814 | TP348H | 8 | 2 | SA-409 | S30815 |
| 8 | 1 | SA-814 | TPXM-15 | 8 | 2 | SA-409 | TP309Cb |
|  |  |  |  | 8 | 2 | SA-409 | TP309S |
| 8 | 2 | SA-182 | F10 | 8 | 2 | SA-409 | TP310Cb |
| 8 | 2 | SA-182 | F45 | 8 | 2 | SA-409 | TP310S |
| 8 | 2 | SA-182 | F310 | 8 | 2 | SA-451 | CPH8 |
| 8 | 2 | SA-213 | S30815 | 8 | 2 | SA-451 | CPH20 |
| 8 | 2 | SA-213 | TP309Cb | 8 | 2 | SA-451 | CPK20 |
| 8 | 2 | SA-213 | TP309H | 8 | 2 | SA-479 | 309Cb |


| $\begin{aligned} & \text { P- } \\ & \text { No. } \end{aligned}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| 8 | 2 | SA-479 | 3095 |
| 8 | 2 | SA-479 | 310 Cb |
| 8 | 2 | SA-479 | 310 S |
| 8 | 2 | SA-479 | S30815 |
| 8 | 2 | SA-813 | S30815 |
| 8 | 2 | SA-813 | TP309Cb |
| 8 | 2 | SA-813 | TP309S |
| 8 | 2 | SA-813 | TP310Cb |
| 8 | 2 | SA-813 | TP310S |
| 8 | 2 | SA-814 | S30815 |
| 8 | 2 | SA-814 | TP309Cb |
| 8 | 2 | SA-814 | TP309S |
| 8 | 2 | SA-814 | TP310Cb |
| 8 | 2 | SA-814 | TP310S |
| 8 | 3 | SA-182 | FXM-11 |
| 8 | 3 | SA-182 | FXM-19 |
| 8 | 3 | SA-213 | TP201 |
| 8 | 3 | SA-213 | TP202 |
| 8 | 3 | SA-213 | XM-19 |
| 8 | 3 | SA-240 | S20100 |
| 8 | 3 | SA-240 | S21800 |
| 8 | 3 | SA-240 | S20100 |
| 8 | 3 | SA-240 | S20153 |
| 8 | 3 | SA-240 | Type 202 |
| 8 | 3 | SA-240 | S20400 |
| 8 | 3 | SA-240 | Type XM-17 |
| 8 | 3 | SA-240 | Type XM-18 |
| 8 | 3 | SA-240 | Type XM-19 |
| 8 | 3 | SA-240 | Type XM-29 |
| 8 | 3 | SA-249 | TP201 |
| 8 | 3 | SA-249 | TP202 |
| 8 | 3 | SA-249 | TPXM-19 |
| 8 | 3 | SA-249 | TPXM-29 |
| 8 | 3 | SA-312 | TPXM-11 |
| 8 | 3 | SA-312 | TPXM-19 |
| 8 | 3 | SA-312 | TPXM-29 |
| 8 | 3 | SA-336 | FXM-11 |
| 8 | 3 | SA-336 | FXM-19 |
| 8 | 3 | SA-351 | CG6MMN |
| 8 | 3 | SA-358 | XM-19 |
| 8 | 3 | SA-358 | XM-29 |
| 8 | 3 | SA-403 | WPXM-19 |
| 8 | 3 | SA-479 | S21800 |
| 8 | 3 | SA-479 | XM-11 |
| 8 | 3 | SA-479 | XM-17 |
| 8 | 3 | SA-479 | XM-18 |
| 8 | 3 | SA-479 | XM-19 |
| 8 | 3 | SA-479 | XM-29 |
| 8 | 3 | SA-666 | 201 |
| 8 | 3 | SA-666 | XM-11 |
| 8 | 3 | SA-688 | XM-29 |
| 8 | 3 | SA-813 | TPXM-11 |
| 8 | 3 | SA-813 | TPXM-19 |
| 8 | 3 | SA-813 | TPXM-29 |
| 8 | 3 | SA-814 | TPXM-11 |
| 8 | 3 | SA-814 | TPXM-19 |


| $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: |
| 8 | 3 | SA-814 | TPXM-29 |
| 8 | 4 | SA-182 | F44 |
| 8 | 4 | SA-213 | S31725 |
| 8 | 4 | SA-213 | S31726 |
| 8 | 4 | SA-240 | S31254 |
| 8 | 4 | SA-240 | S31725 |
| 8 | 4 | SA-240 | S31726 |
| 8 | 4 | SA-249 | S31254 |
| 8 | 4 | SA-249 | S31725 |
| 8 | 4 | SA-249 | S31726 |
| 8 | 4 | SA-312 | S31254 |
| 8 | 4 | SA-312 | S31725 |
| 8 | 4 | SA-312 | S31726 |
| 8 | 4 | SA-336 | F46 |
| 8 | 4 | SA-351 | J93254 |
| 8 | 4 | SA-358 | S31254 |
| 8 | 4 | SA-358 | S31725 |
| 8 | 4 | SA-358 | S31726 |
| 8 | 4 | SA-376 | S31725 |
| 8 | 4 | SA-376 | S31726 |
| 8 | 4 | SA-403 | S31254 |
| 8 | 4 | SA-409 | S31254 |
| 8 | 4 | SA-409 | S31725 |
| 8 | 4 | SA-409 | S31726 |
| 8 | 4 | SA-479 | S31254 |
| 8 | 4 | SA-479 | S31725 |
| 8 | 4 | SA-479 | S31726 |
| 8 | 4 | SA-813 | S31254 |
| 8 | 4 | SA-814 | S31254 |
| 9A | 1 | SA-182 | FR |
| 9A | 1 | SA-203 | A |
| 9A | 1 | SA-203 | B |
| 9A | 1 | SA-234 | WPR |
| 9A | 1 | SA-333 | 7 |
| 9A | 1 | SA-333 | 9 |
| 9A | 1 | SA-334 | 7 |
| 9A | 1 | SA-334 | 9 |
| 9A | 1 | SA-350 | LF5, CI. 1 |
| 9A | 1 | SA-350 | LF5, Cl. 2 |
| 9A | 1 | SA-350 | LF9 |
| 9A | 1 | SA-352 | LC2 |
| 9A | 1 | SA-420 | WPL9 |
| 9 B | 1 | SA-203 | D |
| 9B | 1 | SA-203 | E |
| 9B | 1 | SA-203 | F |
| 9B | 1 | SA-333 | 3 |
| 9B | 1 | SA-334 | 3 |
| 9B | 1 | SA-350 | LF3, CI. 2 |
| 9B | 1 | SA-352 | LC3 |
| 9B | 1 | SA-420 | WPL3 |
| 9B | 1 | SA-765 | III |
| 9 C | 1 | SA-352 | LC4 |

## 2004 SECTION IX

| $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. | $\begin{gathered} \text { P- } \\ \text { No. } \end{gathered}$ | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10A | 1 | SA-225 | C | 10J | 1 | SA-479 | S44700 |
| 10A | 1 | SA-225 | D | 10J | 1 | SA-731 | S44700 |
| 10A | 1 | SA-487 | Gr. 1, CI. A |  |  |  |  |
| 10 A | 1 | SA-487 | Gr. 1, Cl. B | 10K | 1 | SA-240 | S44660 |
|  |  |  |  | 10K | 1 | SA-240 | S44800 |
| 10 B | 1 | SA-213 | T17 | 10K | 1 | SA-268 | S44660 |
|  |  |  |  | 10K | 1 | SA-268 | S44800 |
| 10 C | 1 | SA-612 |  | 10K | 1 | SA-479 | S44800 |
| 10H | 1 | SA-182 | F50 | 10K | 1 | SA-731 | S44660 |
| 10 H | 1 | SA-182 | F51 | 10K | 1 | SA-731 | S44800 |
| 10 H | 1 | SA-240 | S31200 | 10K | 1 | SA-803 | S44660 |
| 10 H | 1 | SA-240 | S31260 | 11 A | 1 |  |  |
| 10 H | 1 | SA-240 | S31803 | 11A | 1 | SA-333 SA-334 | 8 |
| 10 H | 1 | SA-240 | S32550 | 11 A | 1 | SA-353 | . . |
| 10 H | 1 | SA-240 | S32950 | 11 A | 1 | SA-420 | WPL8 |
| 10 H | 1 | SA-240 | Type 329 | 11 A | 1 | SA-522 | Type I |
| 10 H | 1 | SA-479 | S32550 |  |  |  |  |
| 10 H | 1 | SA-479 | S31803 | 11 A | 1 | SA-522 | Type II |
| 10H | 1 | SA-789 | S31200 | 11 A | 1 | SA-553 | Type I |
| 10H | 1 | SA-789 | S31260 | 11 A | 1 | SA-553 | Type II |
| 10 H | 1 | SA-789 | S31500 |  |  |  |  |
| 10 H | 1 | SA-789 | S31803 | 11 A | 2 | SA-645 | $\ldots$ |
| 10 H | 1 | SA-789 | S32304 |  |  |  |  |
| 10 H | 1 | SA-789 | S32550 | 11 A | 3 3 | SA-487 SA-487 | Gr. 4, CI. E |
| 10 H | 1 | SA-789 | S32750 |  |  |  |  |
| 10 H | 1 | SA-789 | S32900 | 11 A | 4 | SA-533 | Type A, CI. 3 |
| 10 H | 1 | SA-789 | S32950 | 11 A | 4 | SA-533 | Type B, CI. 3 |
| 10 H | 1 | SA-790 | S31200 | 11 A | 4 | SA-533 | Type C, CI. 3 |
| 10 H | 1 | SA-790 | S31260 | 11 A | 4 | SA-533 | Type D, CI. 3 |
| 10 H | 1 | SA-790 | S31500 | 11 A | 4 | SA-672 | J100 |
| 10 H | 1 | SA-790 | S31803 | 11 A | 5 | SA-352 | LC2-1 |
| 10H | 1 | SA-790 | S32304 | 11 A | 5 | SA-508 | 4N, Cl. 1 |
| 10 H | 1 | SA-790 | S32550 | 11 A | 5 | SA-508 | 5, Cl. 1 |
| 10 H | 1 | SA-790 | S32750 | 11 A | 5 | SA-543 | B Cl. 1 |
| 10 H | 1 | SA-790 | S32900 | 11 A | 5 | SA-543 | C Cl. 1 |
| 10 H | 1 | SA-790 | S32950 |  |  |  |  |
| 10 H | 1 | SA-815 | S31803 | 11 B | 1 | SA-517 | A |
| 10 H | 1 | SA-995 | 1 A | 11 B | 1 | SA-592 | A |
| 10 H | 1 | SA-995 | 1 B |  |  |  |  |
|  |  |  |  | 11B | 2 | SA-517 | E |
| 10 I | 1 | SA-182 | FXM-27Cb | 11 B | 2 | SA-592 | E |
| 10I | 1 | SA-240 | S44635 |  |  |  |  |
| 101 | 1 | SA-240 | Type XM-27 | 11 B | 3 | SA-517 | F |
| 10 I | 1 | SA-240 | Type XM-33 | 11 B | 3 | SA-592 | F |
| 10I | 1 | SA-268 | 25-4-4 |  |  |  |  |
| 10I | 1 | SA-268 | TP446-1 | 11 B | 4 | SA-517 | B |
| 10I | 1 | SA-268 | TP446-2 | 11 B | 6 | SA-517 | J |
| 10 I | 1 | SA-268 | TPXM-27 | 11 | 6 | SA 517 | J |
| 10 I | 1 | SA-268 | TPXM-33 | 11 B | 8 | SA-517 | P |
| 10I | 1 | SA-336 | FXM-27Cb | 11B | 8 | SA-517 | P |
| 101 | 1 | SA-479 | XM-27 | 11B | 10 | SA-508 | 4N, Cl. 2 |
| 10 I | 1 | SA-731 | TPXM-27 | 11 B | 10 | SA-508 | 5, Cl. 2 |
| 10 I | 1 | SA-731 | TPXM-33 | 11 B | 10 | SA-543 | B Cl. 2 |
|  |  |  |  | 11B | 10 | SA-543 | C CI. 2 |
| 10J | 1 | SA-240 | S44700 |  |  |  |  |
| 10J | 1 | SA-268 | S44700 | Aluminum and Aluminum-Base Alloys |  |  |  |
| 10J | 1 | SA-268 | S44735 | 21 |  | SB-209 | A91060 |

NONMANDATORY APPENDIX D

| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 |  | SB-209 | A91100 | 31 |  | SB-75 | C10200 |
| 21 |  | SB-209 | A93003 | 31 |  | SB-75 | C12000 |
| 21 |  | SB-210 | A91060 |  |  |  |  |
| 21 |  | SB-210 | A93003 | 31 |  | SB-75 | C12200 |
|  |  |  |  | 31 |  | SB-75 | C14200 |
| 21 |  | SB-221 | A91060 | 31 |  | SB-111 | C10200 |
| 21 |  | SB-221 | A91100 | 31 |  | SB-111 | C12000 |
| 21 |  | SB-221 | A93003 | 31 |  | SB-111 | C12200 |
| 21 |  | SB-234 | A91060 |  |  |  |  |
| 21 |  | SB-234 | A93003 | 31 |  | SB-111 | C14200 |
|  |  |  |  | 31 |  | SB-111 | C19200 |
| 21 |  | SB-241 | A91060 | 31 |  | SB-152 | C10200 |
| 21 |  | SB-241 | A91100 | 31 |  | SB-152 | C10400 |
| 21 |  | SB-241 | A93003 |  |  |  |  |
| 21 |  | SB-247 | A93003 | 31 |  | SB-152 | C10500 |
|  |  |  |  | 31 |  | SB-152 | C10700 |
| 22 |  | SB-209 | A93004 | 31 |  | SB-152 | C11000 |
| 22 |  | SB-209 | A95052 | 31 |  | SB-152 | C12200 |
| 22 |  | SB-209 | A95154 | 31 |  | SB-152 | C12300 |
| 22 |  | SB-209 | A95254 | 31 |  | SB-152 | C12500 |
| 22 |  | SB-209 | A95454 |  |  |  |  |
|  |  |  |  | 31 |  | SB-152 | C14200 |
| 22 |  | SB-209 | A95652 | 31 |  | SB-187 | C10200 |
| 22 |  | SB-210 | A95052 | 31 |  | SB-187 | C11000 |
| 22 |  | SB-210 | A95154 | 31 |  | SB-359 | C10200 |
| 22 |  | SB-221 | A95154 | 31 |  | SB-359 | C12000 |
| 22 |  | SB-221 | A95454 | 31 |  | SB-359 | C12200 |
|  |  |  |  | 31 |  | SB-359 | C14200 |
| 22 |  | SB-234 | A95052 |  |  |  |  |
| 22 |  | SB-234 | A95454 | 31 |  | SB-359 | C19200 |
| 22 |  | SB-241 | A95052 | 31 |  | SB-395 | C10200 |
| 22 |  | SB-241 | A95454 | 31 |  | SB-395 | C12000 |
|  |  |  |  | 31 |  | SB-395 | C12200 |
| 23 |  | SB-209 | A96061 | 31 |  | SB-395 | C14200 |
| 23 |  | SB-210 | A96061 |  |  |  |  |
| 23 |  | SB-210 | A96063 | 31 |  | SB-395 | C19200 |
| 23 |  | SB-211 | A96061 | 31 |  | SB-543 | C12200 |
| 23 |  | SB-221 | A96061 | 31 |  | SB-543 | C19400 |
| 23 |  | SB-221 | A96063 | 32 |  | SB-43 | C23000 |
| 23 |  | SB-234 | A96061 | 32 |  | SB-111 | C23000 |
| 23 |  | SB-241 | A96061 | 32 |  | SB-111 | C28000 |
| 23 |  | SB-241 | A96063 | 32 |  | SB-111 | C44300 |
| 23 |  | SB-247 | A96061 | 32 |  | SB-111 | C44400 |
| 23 |  | SB-308 | A96061 | 32 |  | SB-111 | C44500 |
| 25 |  | SB-209 | A95083 | 32 |  | SB-111 | C68700 |
| 25 |  | SB-209 | A95086 | 32 |  | SB-135 | C23000 |
| 25 |  | SB-209 | A95456 | 32 |  | SB-171 | C36500 |
| 25 |  | SB-221 | A95083 | 32 |  | SB-171 | C44300 |
|  |  |  |  | 32 |  | SB-171 | C44400 |
| 25 |  | SB-221 | A95456 | 32 |  | SB-171 | C44500 |
| 25 |  | SB-241 | A95083 |  |  |  |  |
| 25 |  | SB-241 | A95086 | 32 |  | SB-171 | C46400 |
| 25 |  | SB-241 | A95456 | 32 |  | SB-171 | C46500 |
| 25 |  | SB-247 | A95083 | 32 |  | SB-359 | C23000 |
| Copper and Copper-Base Alloys |  |  |  | 32 |  | SB-359 | C44300 |
| 31 |  | SB-42 | C10200 | 32 |  | SB-359 | C44400 |
| 31 |  | SB-42 | C12000 | 32 |  | SB-359 | C44500 |
| 31 |  | SB-42 | C12200 | 32 |  | SB-359 | C68700 |

## 2004 SECTION IX

| P- No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 32 |  | SB-395 | C23000 | 35 |  | SB-271 | C95200 |
| 32 |  | SB-395 | C44300 | 35 |  | SB-271 | C95400 |
| 32 |  | SB-395 | C44400 | 35 |  | SB-359 | C60800 |
| 32 |  | SB-395 | C44500 | 35 |  | SB-395 | C60800 |
| 32 |  | SB-395 | C68700 | 35 |  | SB-505 | C95200 |
| 32 |  | SB-543 | C23000 |  |  |  |  |
|  |  |  |  | Nickel and Nickel-Base Alloys |  |  |  |
| 32 |  | SB-543 | C44300 | 41 |  | SB-160 | N02200 |
| 32 |  | SB-543 | C44400 | 41 |  | SB-160 | N02201 |
| 32 |  | SB-543 | C44500 | 41 |  | SB-161 | N02200 |
| 32 |  | SB-543 | C68700 | 41 |  | SB-161 | N02201 |
|  |  |  |  | 41 |  | SB-162 | N02200 |
| 33 |  | SB-96 | C65500 |  |  |  |  |
| 33 |  | SB-98 | C65100 | 41 |  | SB-162 | N02201 |
| 33 |  | SB-98 | C65500 | 41 |  | SB-163 | N02200 |
| 33 |  | SB-98 | C66100 | 41 |  | SB-163 | N02201 |
| 33 |  | SB-315 | C65500 | 41 |  | SB-366 | N02200 |
|  |  |  |  | 41 |  | SB-366 | N02201 |
| 34 |  | SB-111 | C70400 |  |  |  |  |
| 34 |  | SB-111 | C70600 | 42 |  | SB-127 | N04400 |
| 34 |  | SB-111 | C71000 | 42 |  | SB-163 | N04400 |
| 34 |  | SB-111 | C71500 | 42 |  | SB-164 | N04400 |
| 34 |  | SB-111 | C71640 | 42 |  | SB-164 | N04405 |
|  |  |  |  | 42 |  | SB-165 | N04400 |
| 34 |  | SB-111 | C72200 | 42 |  | SB-366 | N04400 |
| 34 |  | SB-151 | C70600 | 42 |  | SB-564 | N04400 |
| 34 |  | SB-171 | C70600 |  |  |  |  |
| 34 |  | SB-171 | C71500 | 43 |  | SB-163 | N06600 |
| 34 |  | SB-359 | C70400 | 43 |  | SB-163 | N06690 |
|  |  |  |  | 43 |  | SB-166 | N06600 |
| 34 |  | SB-359 | C70600 | 43 |  | SB-166 | N06617 |
| 34 |  | SB-359 | C71000 | 43 |  | SB-166 | N06690 |
| 34 |  | SB-359 | C71500 |  |  |  |  |
| 34 |  | SB-369 | C96200 | 43 |  | SB-167 | N06600 |
| 34 |  | SB-395 | C70600 | 43 |  | SB-167 | N06617 |
|  |  |  |  | 43 |  | SB-167 | N06690 |
| 34 |  | SB-395 | C71000 | 43 |  | SB-168 | N06600 |
| 34 |  | SB-395 | C71500 | 43 |  | SB-168 | N06617 |
| 34 |  | SB-466 | C70600 | 43 |  | SB-168 | N06690 |
| 34 |  | SB-466 | C71000 |  |  |  |  |
| 34 |  | SB-466 | C71500 | 43 |  | SB-366 | N06002 |
|  |  |  |  | 43 |  | SB-366 | N06022 |
| 34 |  | SB-467 | C70600 | 43 |  | SB-366 | N06059 |
| 34 |  | SB-467 | C71500 | 43 |  | SB-366 | N06200 |
| 34 |  | SB-543 | C70400 | 43 |  | SB-366 | N06230 |
| 34 |  | SB-543 | C70600 | 43 |  | SB-366 | N06455 |
| 34 |  | SB-543 | C71500 |  |  |  |  |
|  |  |  |  | 43 |  | SB-366 | N06600 |
| 34 |  | SB-543 | C71640 | 43 |  | SB-366 | N06625 |
|  |  |  |  | 43 |  | SB-366 | N10276 |
| 35 |  | SB-111 | C60800 | 43 |  | SB-435 | N06002 |
| 35 |  | SB-148 | C95200 | 43 |  | SB-435 | N06230 |
| 35 |  | SB-148 | C95400 |  |  |  |  |
| 35 |  | SB-150 | C61400 | 43 |  | SB-443 | N06625 |
| 35 |  | SB-150 | C62300 | 43 |  | SB-444 | N06625 |
|  |  |  |  | 43 |  | SB-446 | N06625 |
| 35 |  | SB-150 | C63000 | 43 |  | SB-462 | N06022 |
| 35 |  | SB-150 | C64200 | 43 |  | SB-462 | N06200 |
| 35 |  | SB-169 | C61400 | 43 |  | SB-462 | N10276 |
| 35 |  | SB-171 | C61400 | 43 |  | SA-494 | N26022 |
| 35 |  | SB-171 | C63000 | 43 |  | SB-516 | N06600 |


| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 43 |  | SB-517 | N06600 | 44 |  | SB-333 | N10675 |
|  |  |  |  | 44 |  | SB-335 | N10001 |
| 43 |  | SB-564 | N06022 | 44 |  | SB-335 | N10629 |
| 43 |  | SB-564 | N06059 | 44 |  | SB-335 | N10665 |
| 43 |  | SB-564 | N06200 | 44 |  | SB-335 | N10675 |
| 43 |  | SB-564 | N06230 |  |  |  |  |
| 43 |  | SB-564 | N06600 | 44 |  | SB-366 | N10001 |
| 43 |  | SB-564 | N06617 | 44 |  | SB-366 | N10003 |
|  |  |  |  | 44 |  | SB-366 | N10629 |
| 43 |  | SB-564 | N06625 | 44 |  | SB-366 | N10665 |
| 43 |  | SB-564 | N06686 | 44 |  | SB-366 | N10675 |
| 43 |  | SB-564 | N06690 | 44 |  | SB-434 | N10003 |
| 43 |  | SB-564 | N10276 | 44 |  | SB-462 | N10665 |
| 43 |  | SB-572 | N06002 | 44 |  | SB-462 | N10675 |
| 43 |  | SB-572 | N06230 | 44 |  | SB-564 | N10629 |
|  |  |  |  | 44 |  | SB-564 | N10675 |
| 43 |  | SB-574 | N06022 | 44 |  | SB-573 | N10003 |
| 43 |  | SB-574 | N06059 |  |  |  |  |
| 43 |  | SB-574 | N06200 | 44 |  | SB-619 | N10001 |
| 43 |  | SB-574 | N06455 | 44 |  | SB-619 | N10629 |
| 43 |  | SB-574 | N06686 | 44 |  | SB-619 | N10665 |
| 43 |  | SB-574 | N10276 | 44 |  | SB-619 | N10675 |
| 43 |  | SB-575 | N06022 | 44 |  | SB-622 | N10001 |
| 43 |  | SB-575 | N06059 | 44 |  | SB-622 | N10629 |
| 43 |  | SB-575 | N06200 | 44 |  | SB-622 | N10665 |
| 43 |  | SB-575 | N06455 | 44 |  | SB-622 | N10675 |
| 43 |  | SB-575 | N06686 | 44 |  | SB-626 | N10001 |
| 43 |  | SB-575 | N10276 | 44 |  | SB-626 | N10629 |
|  |  |  |  | 44 |  | SB-626 | N10665 |
| 43 |  | SB-619 | N06002 | 44 |  | SB-626 | N10675 |
| 43 |  | SB-619 | N06022 |  |  |  |  |
| 43 |  | SB-619 | N06059 | 45 |  | SB-163 | N08800 |
| 43 |  | SB-619 | N06200 | 45 |  | SB-163 | N08810 |
| 43 |  | SB-619 | N06230 | 45 |  | SB-163 | N08811 |
| 43 |  | SB-619 | N06455 | 45 |  | SB-163 | N08825 |
| 43 |  | SB-619 | N06686 | 4545 |  | SA-351 | CN3MN |
| 43 |  | SB-619 | N10276 |  |  | SA-351 |  |
|  |  |  |  | 45 |  | SA-351 | N08151 |
| 43 43 |  | SB-622 SB-622 | N06002 N06022 | 45 |  | SB-366 | N06007 |
| 43 43 |  | SB-622 SB-622 | N06022 | 45 |  | SB-366 | N06030 |
| 43 |  | SB-622 | N06200 | 45 |  | SB-366 | N06985 |
| 43 |  | SB-622 | N06230 | 45 |  | SB-366 | N08020 |
| 43 |  | SB-622 | N06455 | 45 |  | SB-366 | N08031 |
| 43 |  | SB-622 | N06686 | 45 |  | SB-366 | N08367 |
| 43 |  | SB-622 | N10276 | 45 |  | SB-366 | N08800 |
|  |  |  |  | 45 |  | SB-366 | N08825 |
| 43 |  | SB-626 | N06002 | 45 |  | SB-366 | N08925 |
| 43 |  | SB-626 | N06022 | 45 |  | SB-366 | R20033 |
| 43 |  | SB-626 | N06059 | 45 |  | SB-407 | N08800 |
| 43 |  | SB-626 | N06200 | 45 |  | SB-407 | N08810 |
| 43 |  | SB-626 | N06230 | 45 |  | SB-407 | N08811 |
| 43 |  | SB-626 | N06455 |  |  |  |  |
| 43 |  | SB-626 | N06686 | 45 |  | SB-408 |  |
| 43 |  | SB-626 | N10276 | 45 |  | SB-408 SB-408 | N08810 N08811 |
| 43 |  | SB-704 | N06625 | 45 |  | SB-408 | N08811 |
| 43 |  | SB-705 | N06625 | 45 45 |  | $\begin{aligned} & \text { SB-409 } \\ & \text { SB-409 } \end{aligned}$ | $\begin{aligned} & \text { N08800 } \\ & \text { N08810 } \end{aligned}$ |
| 44 |  | SB-333 | N10001 | 45 |  | SB-409 | N08811 |
| 44 |  | SB-333 | N10629 | 45 |  | SB-423 | N08825 |
| 44 |  | SB-333 | N10665 | 45 |  | SB-424 | N08825 |

## 2004 SECTION IX

| P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. | P- <br> No. | Grp. No. | Spec. No. | Type, Grade, or UNS No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 |  | SB-425 | N08825 | 45 |  | SB-625 | N08031 |
| 45 |  | SB-435 | R30556 | 45 |  | SB-625 | N08904 |
| 45 |  | SB-462 | N06030 | 45 |  | SB-625 | N08925 |
| 45 |  | SB-462 | N08020 | 45 |  | SB-625 | R20033 |
| 45 |  | SB-462 | N08367 | 45 |  | SB-626 | N06007 |
| 45 |  | SB-463 | N08020 | 45 |  | SB-626 | N06030 |
| 45 |  | SB-463 | N08024 | 45 |  | SB-626 | N06975 |
| 45 |  | SB-463 | N08026 | 45 |  | SB-626 | N06985 |
| 45 |  | SB-464 | N08020 | 45 |  | SB-626 | N08031 |
| 45 |  | SB-464 | N08024 | 45 |  | SB-626 | N08320 |
| 45 |  | SB-464 | N08026 | 45 |  | SB-626 | R20033 |
| 45 |  | SB-468 | N08020 | 45 |  | SB-626 | R30556 |
| 45 |  | SB-468 | N08024 | 45 |  | SB-649 | N08904 |
| 45 |  | SB-468 | N08026 | 45 |  | SB-649 | N08925 |
| 45 |  | SB-473 | N08020 | 45 |  | SB-649 | R20033 |
| 45 |  | SB-514 | N08800 | 45 |  | SB-668 | N08028 |
| 45 |  | SB-514 | N08810 | 45 |  | SB-672 | N08700 |
| 45 |  | SB-515 | N08800 | 45 |  | SB-673 | N08904 |
| 45 |  | SB-515 | N08810 | 45 |  | SB-673 | N08925 |
| 45 |  | SB-515 | N08811 | 45 |  | SB-674 | N08904 |
| 45 |  | SB-564 | N08031 | 45 |  | SB-674 | N08925 |
| 45 |  | SB-564 | N08367 | 45 |  | SB-675 | N08367 |
| 45 |  | SB-564 | N08800 | 45 |  | SB-676 | N08367 |
| 45 |  | SB-564 | N08810 | 45 |  | SB-677 | N08904 |
| 45 |  | SB-564 | N08811 | 45 |  | SB-677 | N08925 |
| 45 |  | SB-564 | N08825 | 45 |  | SB-688 | N08367 |
| 45 |  | SB-564 | R20033 |  |  |  |  |
| 45 |  | SB-572 | R30556 | 45 |  | SB-690 | N08367 |
| 45 |  | SB-581 | N06007 | 45 |  | SB-691 | N08367 |
| 45 |  | SB-581 | N06030 | 45 |  | SB-704 | N08825 |
| 45 |  | SB-581 | N06975 | 45 |  | SB-705 | N08825 |
| 45 |  | SB-581 | N06985 | 45 |  | SB-709 | N08028 |
| 45 |  | SB-581 | N08031 | 45 |  | SB-729 | N08020 |
| 45 |  | SB-582 | N06007 | 46 |  | SB-166 | N06045 |
| 45 |  | SB-582 | N06030 | 46 |  | SB-167 | N06045 |
| 45 |  | SB-582 | N06975 | 46 |  | SB-168 | N06045 |
| 45 |  | SB-582 | N06985 | 46 |  | SB-366 | N06045 |
| 45 |  | SB-599 | N08700 | 46 |  | SB-366 | N08330 |
| 45 |  | SB-619 | N06007 | 46 |  | SB-366 | N12160 |
| 45 |  | SB-619 | N06030 | 46 |  | SB-435 | N12160 |
| 45 |  | SB-619 | N06975 | 46 |  | SB-511 | N08330 |
| 45 |  | SB-619 | N06985 | 46 |  | SB-516 | N06045 |
| 45 |  | SB-619 | N08031 | 46 |  | SB-517 | N06045 |
| 45 |  | SB-619 | N08320 | 46 |  | SB-535 | N08330 |
| 45 |  | SB-619 | R20033 | 46 |  | SB-536 | N08330 |
| 45 |  | SB-619 | R30556 | 46 |  | SB-564 | N06045 |
| 45 |  | SB-620 | N08320 | 46 |  | SB-564 | N12160 |
| 45 |  | SB-621 | N08320 | 46 |  | SB-572 | N12160 |
| 45 |  | SB-622 | N06007 | 46 |  | SB-619 | N12160 |
| 45 |  | SB-622 | N06030 | 46 |  | SB-622 | N12160 |
| 45 |  | SB-622 | N06975 | 46 |  | SB-626 | N12160 |
| 45 |  | SB-622 | N06985 | 46 |  | SB-710 | N08330 |
| 45 |  | SB-622 | N08031 |  |  |  |  |
| 45 |  | SB-622 | N08320 | 49 |  | SB-815 | R31233 |
| 45 |  | SB-622 | R20033 | 49 |  | SB-818 | R31233 |
| 45 |  | SB-622 | R30556 |  |  |  |  |

NONMANDATORY APPENDIX D

| P- Grp.  <br> No. No. Spec. No. |  |  |
| :--- | :---: | :---: |
| Titanium and Titanium-Base Alloys | Type, Grade, or <br> UNS No. |  |
| 51 | SB-265 |  |
| 51 | SB-265 | R50250 |
| 51 | SB-265 | R50400 |
| 51 | SB-265 | R52250 |
| 51 | SB-265 | R52252 |
| 51 | SB-265 | R52254 |
| 51 | SB-265 | R52400 |
| 51 | SB-265 | R52402 |
| 51 | SB-338 | R52404 |
| 51 | SB-338 | R50250 |
| 51 | SB-338 | R50400 |
| 51 | SB-388 | R52400 |
| 51 | SB-388 | R5202 |
| 51 | SB-348 | R5204 |
| 51 | SB-348 | R50250 |
| 51 | SB-348 | R50400 |
| 51 | SB-348 | R50402 |
| 51 | SB-348 | R52400 |
| 51 | SB-363 | R52404 |
| 51 | SB-363 | R50250 |
| 51 | SB-363 | R50400 |
| 51 | SB-363 | R52400 |
| 51 | SB-367 | R52404 |
| 51 | SB-381 | R50400 |
| 51 | SB-381 | SB-862 |

\(\left.$$
\begin{array}{ccc}\hline \text { P- } & \text { Grp. } & \\
\text { No. } & \text { No. } & \text { Spec. No. }\end{array}
$$ \begin{array}{c}Type, Grade, or <br>

UNS No.\end{array}\right]\)| 52 | SB-265 | R50550 |
| :--- | :--- | :--- |
| 52 | SB-265 | R53400 |
| 52 | SB-338 | R50550 |
| 52 | SB-338 | R50550 |
| 52 | SB-348 | R53400 |
| 52 | SB-348 | R50550 |
| 52 | SB-363 | R53400 |
| 52 | SB-363 | R50550 |
| 52 | SB-367 | R50550 |
| 52 | SB-381 | R53400 |
| 52 | SB-381 | R50550 |
| 52 | SB-861 | R53400 |
| 52 | SB-861 | R50550 |
| 52 | SB-862 | R53400 |
| 52 | SB-862 |  |
| 53 |  | R56320 |
| 52 | SB-658 | R56320 |
| 53 |  | SB-338 |

# MANDATORY APPENDIX E PERMITTED SWPSs 

The following Standard Welding Procedure Specifications may be used under the conditions given in Article V.

| Specification | Designation |
| :---: | :---: |
| Carbon Steel |  |
| Shielded Metal Arc Welding |  |
| Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, E7018, As-Welded or PWHT Condition | B2.1-1-016-94 |
| Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), $1 / 8$ through $\mathrm{I}^{1} / 2$ inch Thick, E6010, As-Welded or PWHT Condition | B2.1-1-017-94 |
| Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, E6010 (Vertical Uphill) Followed by E7018, As-Welded or PWHT Condition | B2.1-1-022-94 |
| Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, E6010 (Vertical Downhill) Followed by E7018, As-Welded or PWHT Condition | B2.1-1-026-94 |
| Combination GTAW and SMAW |  |
| Standard Welding Procedure Specification for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, ER70S-2 and E7018, As-Welded or PWHT Condition | B2.1-1-021-94 |
| Flux Cored Arc Welding |  |
| Standard Welding Procedure Specification (WPS) for $\mathrm{CO}_{2}$ Shielded Flux Cored Arc Welding of Carbon Steel (M-1/ P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, E70T-1 and E71T-1, As-Welded Condition | B2.1-1-019-94 |
| Standard Welding Procedure Specification (WPS) for $75 \% \mathrm{Ar} / 25 \% \mathrm{CO}_{2}$ Shielded Flux Cored Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 / 2$ inch Thick, E70T-1 and E71T-1, As-Welded or PWHT Condition | B2.1-1-020-94 |
| Carbon Steel - Primarily Pipe Applications |  |
| Shielded Metal Arc Welding |  |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $3 / 4$ inch Thick, E6010 (Vertical Uphill) Followed by E7018 (Vertical Uphill), AsWelded Condition, Primarily Pipe Applications | B2.1-1-201-96 |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $3 / 4$ inch Thick, E6010 (Vertical Downhill) Followed by E7018 (Vertical Uphill), AsWelded Condition, Primarily Pipe Applications | B2.1-1-202-96 |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $3 / 4$ inch Thick, E6010 (Vertical Uphill), As-Welded Condition, Primarily Pipe Applications | B2.1-1-203-96 |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $3 / 4$ inch Thick, E6010 (Vertical Downhill Root with the Balance Vertical Uphill), AsWelded Condition, Primarily Pipe Applications | B2.1-1-204-96 |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 / 2$ inch Thick, E6010 (Vertical Uphill) Followed by E7018 (Vertical Uphill), AsWelded or PWHT Condition, Primarily Pipe Applications | B2.1-1-205-96 |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), $1 / 8$ through $1 / 2$ inch Thick, E6010 (Vertical Downhill) Followed by E7018 (Vertical Uphill), AsWelded or PWHT Condition, Primarily Pipe Applications | B2.1-1-206-96 |

## MANDATORY APPENDIX E

| Specification | Designation |
| :---: | :---: |
| Carbon Steel - Primarily Pipe Applications (CONT'D) |  |
| Shielded Metal Arc Welding (CONT'D) |  |
| Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 / 2$ inch Thick, E7018, As-Welded or PWHT Condition, Primarily Pipe Applications | B2.1-1-208-96 |
| Gas Tungsten Arc Welding |  |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 / 2$ inch Thick, ER70S-2, As-Welded or PWHT Condition, Primarily Pipe Applications | B2.1-1-207-96 |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), $1 / 8$ through $1 / 2$ inch Thick, INMs-1 and ER70S-2, As-Welded or PWHT Condition, Primarily Pipe Applications | $\begin{gathered} \text { B2.1-1-210: } \\ 2001 \end{gathered}$ |
| Combination GTAW and SMAW |  |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, ER70S-2 and E7018, AsWelded or PWHT Condition, Primarily Pipe Applications | B2.1-1-209-96 |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root followed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2 ), $1 / 8$ through $1 / \frac{1}{2}$ inch Thick, INMs-1, ER70S-2, and E7018, As-Welded or PWHT Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1-211: } \\ & 2001 \end{aligned}$ |


| Austenitic Stainless Steel Plate and Pipe |
| :--- |
| Shielded Metal Arc Welding |
| Standard Welding Procedure Specification for Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/ |
| S-8, Group 1), $1 / 8$ through $1 / 2$ inch Thick, As-Welded Condition |
| Gas Tungsten Arc Welding |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Austenitic Stainless Steel (M-8/ |
| P-8/S-8, Group 1), $1 / 16$ through $1 / 2$ inch Thick, ER3XX, As-Welded Condition, Primarily Plate and Structural |
| Applications |
| Combination GTAW and SMAW |
| Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding followed by Shielded Metal Arc |
| Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1 ), $1 / 8$ through $1 / 2$ inch Thick, ER3XX and 3XX-XX, |
| As-Welded Condition, Primarily Plate and Structural Applications |

## Austenitic Stainless Steel Primarily Pipe Applications

## Shielded Metal Arc Welding

Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Austenitic Stainless Steel (M-
B2.1-8-213-97
8/P-8/S-8, Group 1), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, E3XX-XX, As-Welded Condition, Primarily Pipe Applications

## Gas Tungsten Arc Welding

Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Austenitic Stainless Steel (M-8/ P-8/S-8, Group 1), $1 / 16$ through $1 / 2$ inch Thick, ER3XX, As-Welded Condition, Primarily Pipe Applications
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, IN3XX and ER3XX, As-Welded Condition, Primarily Pipe Applications

## Combination GTAW and SMAW

Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding followed by Shielded Metal Arc
B2.1-8-214: Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), $1 / 8$ through $1 \frac{1}{2}$ inch Thick, ER3XX and E3XX-XX, 2001 As-Welded Condition, Primarily Pipe Applications
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root fol-B2.1-8-216: lowed by Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), $1 / 8$ through $1 / 2$ inch

B2.1-8-215: 2001 Thick, IN3XX, ER3XXX, and E3XX-XX, As-Welded Condition, Primarily Pipe Applications

## 2004 SECTION IX

| Specification | Designation |
| :---: | :---: |
| Carbon Steel to Austenitic Stainless Steel |  |
| Gas Tungsten Arc Welding |  |
| Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1), $1 / 16$ through $1 \frac{1}{2}$ inch Thick, ER309(L), As-Welded Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1/8- } \\ & \text { 227: } 2002 \end{aligned}$ |
| Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding with Consumable Insert Root of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Gruops 1 and 2 Welded to M-8/P-8/S-8, Group 1), 1/16 through $1 \frac{1}{2}$ inch Thick, IN309 and R309(L), As-Welded Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1/8- } \\ & \text { 230: } 2002 \end{aligned}$ |
| Shielded Metal Arc Welding |  |
| Standard Welding Procedure Specification (SWPS) for Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Groups 1 and 2 Welded to $\mathrm{M}-8 / \mathrm{P}-8 / \mathrm{S}-8$, Group 1), $1 / 8$ through $1 / 2$ inch Thick, E309(L)-15, -16, or -17, As-Welded Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1/8- } \\ & \text { 228: } 2002 \end{aligned}$ |
| Combination GTAW and SMAW |  |
| Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1 Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1), $1 / 8$ through $1 / 1 / 2$ inch Thick, ER309(L) and E309(L)-15, -16 , or -17 , As-Welded Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1/8- } \\ & \text { 229: } 2002 \end{aligned}$ |
| Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding with Consumable Insert Root, Followed by Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1 Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1) $1 / 8$ through $1 \frac{1}{2}$ inch Thick, IN309, ER309(L), and E309(L)-15, -16, -17, As-Welded Condition, Primarily Pipe Applications | $\begin{aligned} & \text { B2.1-1/8- } \\ & \text { 231: } 2002 \end{aligned}$ |

# MANDATORY APPENDIX F STANDARD UNITS FOR USE IN EQUATIONS 

TABLE F-100
STANDARD UNITS FOR USE IN EQUATIONS

| Quantity | U.S. Customary Units | SI Units |
| :---: | :---: | :---: |
| Linear dimensions (e.g., length, height, thickness, radius, diameter) | inches (in.) | millimeters (mm) |
| Area | square inches (in. ${ }^{2}$ ) | square millimeters ( $\mathrm{mm}^{2}$ ) |
| Volume | cubic inches (in. ${ }^{3}$ ) | cubic millimeters ( $\mathrm{mm}^{3}$ ) |
| Section modulus | cubic inches (in. ${ }^{3}$ ) | cubic millimeters ( $\mathrm{mm}^{3}$ ) |
| Moment of inertia of section | inches ${ }^{4}$ (in. ${ }^{4}$ ) | millimeters ${ }^{4}\left(\mathrm{~mm}^{4}\right)$ |
| Mass (weight) | pounds mass (lbm) | kilograms (kg) |
| Force (load) | pounds force (lbf) | newtons (N) |
| Bending moment | inch-pounds (in.-lb) | newton-millimeters ( $\mathrm{N} \cdot \mathrm{mm}$ ) |
| Pressure, stress, stress intensity, and modulus of elasticity | pounds per square inch (psi) | megapascals ( MPa ) |
| Energy (e.g., Charpy impact values) | foot-pounds (ft-lb) | joules (J) |
| Temperature | degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) | degrees Celsius ( ${ }^{\circ} \mathrm{C}$ ) |
| Absolute temperature | Rankine (R) | kelvin (K) |
| Fracture toughness | ksi square root inches (ksi $\sqrt{\text { in. }}$ ) | MPa square root meters ( $\mathrm{MPa} \sqrt{\mathrm{m}}$ ) |
| Angle | degrees or radians | degrees or radians |
| Boiler capacity | Btu/hr | watts (W) |

## G-100 USE OF UNITS IN EQUATIONS

The equations in this Nonmandatory Appendix are suitable for use only with either the U.S. Customary or the SI units provided in Mandatory Appendix F, or with the units provided in the nomenclature associated with that equation. It is the responsibility of the individual and organization performing the calculations to ensure that appropriate units are used. Either U.S. Customary or SI units may be used as a consistent set. When SI units are selected, U.S. Customary values in referenced specifications may be converted to SI values to at least three significant figures for use in calculations and other aspects of construction.

## G-200 GUIDELINES USED TO DEVELOP SI EQUIVALENTS

The following guidelines were used to develop SI equivalents:
(a) SI units are placed in parentheses after the U.S. Customary units in the text.
(b) In general, separate SI tables are provided if interpolation is expected. The table designation (e.g., table number) is the same for both the U.S. Customary and SI tables, with the addition of suffix " M " to the designator for the SI table, if a separate table is provided. In the text, references to a table use only the primary table number (i.e., without the " M "). For some small tables, where interpolation is not required, SI units are placed in parentheses after the U.S. Customary unit.
(c) Separate SI versions of graphical information (charts) are provided, except that if both axes are dimensionless, a single figure (chart) is used.
(d) In most cases, conversions of units in the text were done using hard SI conversion practices, with some soft conversions on a case-by-case basis, as appropriate. This was implemented by rounding the SI values to the number
of significant figures of implied precision in the existing U.S. Customary units. For example, 3,000 psi has an implied precision of one significant figure. Therefore, the conversion to SI units would typically be to 20000 kPa . This is a difference of about $3 \%$ from the "exact" or soft conversion of 20684.27 kPa . However, the precision of the conversion was determined by the Committee on a case-by-case basis. More significant digits were included in the SI equivalent if there was any question. The values of allowable stress in Section II, Part D generally include three significant figures.
(e) Minimum thickness and radius values that are expressed in fractions of an inch were generally converted according to the following table:

| Fraction, in. | Proposed <br> $1 / 32$ | SI Conversion, mm |
| :---: | :---: | :---: |
| $3 / 64$ | 0.8 | Difference, $\%$ <br> $1 / 16$ |
| $3 / 32$ | 1.2 | -0.8 |
| $1 / 8$ | 1.5 | -0.8 |
| $5 / 32$ | 2.5 | 5.5 |
| $3 / 16$ | 3 | -5.0 |
| $7 / 32$ | 4 | 5.5 |
| $1 / 4$ | 5 | -0.8 |
| $5 / 16$ | 5.5 | -5.0 |
| $3 / 8$ | 6 | 1.0 |
| $7 / 16$ | 8 | 5.5 |
| $1 / 2$ | 10 | -0.8 |
| $9 / 16$ | 11 | -5.0 |
| $5 / 8$ | 13 | 1.0 |
| $11 / 16$ | 14 | -2.4 |
| $3 / 4$ | 16 | 2.0 |
| $7 / 8$ | 17 | -0.8 |
| 1 | 19 | 2.6 |
|  | 22 | 0.3 |
|  | 25 | 1.0 |
|  |  | 1.6 |

(f) For nominal sizes that are in even increments of inches, even multiples of 25 mm were generally used. Intermediate values were interpolated rather than converting and rounding to the nearest mm . See examples in the following table. [Note that this table does not apply
to nominal pipe sizes (NPS), which are covered below.]

| Size, in. | Size, mm |
| :---: | :---: |
| 1 | 25 |
| $1^{1 / 8}$ | 29 |
| $1^{1 / 4}$ | 32 |
| $1^{1 / 2}$ | 38 |
| 2 | 50 |
| $2^{1 / 4}$ | 57 |
| $2^{1 / 2}$ | 64 |
| 3 | 75 |
| $3^{1 / 2}$ | 89 |
| 4 | 100 |
| $4^{1 / 2}$ | 114 |
| 5 | 125 |
| 6 | 150 |
| 8 | 200 |
| 12 | 300 |
| 18 | 450 |
| 20 | 500 |
| 24 | 600 |
| 36 | 900 |
| 40 | 1000 |
| 54 | 1350 |
| 60 | 1500 |
| 72 | 1800 |
|  |  |
| Size or Length, ft | Size or Length, m |
| 3 | 1 |
| 5 | 1.5 |
| 200 | 60 |

(g) For nominal pipe sizes, the following relationships were used:

| U.S. <br> Customary |  | $\begin{gathered} \text { U.S. } \\ \text { Customary } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: |
| Practice | $\underline{\text { SI Practice }}$ | Practice | $\underline{\text { SI Practice }}$ |
| NPS 1/8 | DN 6 | NPS 20 | DN 500 |
| NPS 1/4 | DN 8 | NPS 22 | DN 550 |
| NPS 3/8 | DN 10 | NPS 24 | DN 600 |
| NPS 1/2 | DN 15 | NPS 26 | DN 650 |
| NPS 3/4 | DN 20 | NPS 28 | DN 700 |
| NPS 1 | DN 25 | NPS 30 | DN 750 |
| NPS 11/4 | DN 32 | NPS 32 | DN 800 |
| NPS 11⁄2 | DN 40 | NPS 34 | DN 850 |
| NPS 2 | DN 50 | NPS 36 | DN 900 |
| NPS $21 / 2$ | DN 65 | NPS 38 | DN 950 |
| NPS 3 | DN 80 | NPS 40 | DN 1000 |
| NPS 31/2 | DN 90 | NPS 42 | DN 1050 |
| NPS 4 | DN 100 | NPS 44 | DN 1100 |
| NPS 5 | DN 125 | NPS 46 | DN 1150 |
| NPS 6 | DN 150 | NPS 48 | DN 1200 |
| NPS 8 | DN 200 | NPS 50 | DN 1250 |
| NPS 10 | DN 250 | NPS 52 | DN 1300 |
| NPS 12 | DN 300 | NPS 54 | DN 1350 |
| NPS 14 | DN 350 | NPS 56 | DN 1400 |
| NPS 16 | DN 400 | NPS 58 | DN 1450 |
| NPS 18 | DN 450 | NPS 60 | DN 1500 |

(h) Areas in square inches (in. ${ }^{2}$ ) were converted to square $\mathrm{mm}\left(\mathrm{mm}^{2}\right)$ and areas in square feet $\left(\mathrm{ft}^{2}\right)$ were converted to square meters $\left(\mathrm{m}^{2}\right)$. See examples in the following table:

| Area (U.S. Customary) |  |
| :---: | :---: |
| $1 \mathrm{in.}^{2}$ |  |
| $6 \mathrm{in.}^{2}$ | $650 \mathrm{~mm}^{2}$ |
| $10 \mathrm{in.}^{2}$ | $4000 \mathrm{~mm}^{2}$ |
| $5 \mathrm{ft}^{2}$ | $6500 \mathrm{~mm}^{2}$ |
|  | $0.5 \mathrm{~m}^{2}$ |

(i) Volumes in cubic inches (in. ${ }^{3}$ ) were converted to cubic $\mathrm{mm}\left(\mathrm{mm}^{3}\right)$ and volumes in cubic feet $\left(\mathrm{ft}^{3}\right)$ were converted to cubic meters $\left(\mathrm{m}^{3}\right)$. See examples in the following table:

| Volume (U.S. Customary) | Volume (SI) |
| :---: | :---: |
| $1 \mathrm{in}^{3}$ | $16000 \mathrm{~mm}^{3}$ |
| 6 in. ${ }^{3}$ | $100000 \mathrm{~mm}^{3}$ |
| 10 in. ${ }^{3}$ | $160000 \mathrm{~mm}^{3}$ |
| $5 \mathrm{ft}^{3}$ | $0.14 \mathrm{~m}^{3}$ |

(j) Although the pressure should always be in MPa for calculations, there are cases where other units are used in the text. For example, kPa is used for small pressures. Also, rounding was to one significant figure (two at the most) in most cases. See examples in the following table. (Note that 14.7 psi converts to 101 kPa , while 15 psi converts to 100 kPa . While this may seem at first glance to be an anomaly, it is consistent with the rounding philosophy.)

| Pressure (U.S. Customary) |  | Pressure (SI) |
| :---: | :---: | :---: |
| 0.5 psi |  | 3 kPa |
| 2 psi |  | 15 kPa |
| 3 psi |  | 20 kPa |
| 10 psi |  | 70 kPa |
| 14.7 psi |  | 101 kPa |
| 15 psi |  | 200 kPa |
| 30 psi | 350 kPa |  |
| 50 psi | 700 kPa |  |
| 100 psi | 1 MPa |  |
| 150 psi | 1.5 MPa |  |
| 200 psi | 1.7 MPa |  |
| 250 psi | 2 MPa |  |
| 300 psi | 2.5 MPa |  |
| 350 psi | 3 MPa |  |
| 400 psi | 3.5 MPa |  |
| 500 psi | 4 MPa |  |
| 600 psi | 8 MPa |  |
| $1,200 \mathrm{psi}$ | 10 MPa |  |
| $1,500 \mathrm{psi}$ |  |  |

(k) Material properties that are expressed in psi or ksi (e.g., allowable stress, yield and tensile strength, elastic modulus) were generally converted to MPa to three significant figures. See example in the following table:
$\frac{\text { Strength (U.S. Customary) }}{95,000 \mathrm{psi}} \quad \frac{\text { Strength (SI) }}{655 \mathrm{MPa}}$
(l) In most cases, temperatures (e.g., for PWHT) were rounded to the nearest $5^{\circ} \mathrm{C}$. Depending on the implied precision of the temperature, some were rounded to the nearest $1^{\circ} \mathrm{C}$ or $10^{\circ} \mathrm{C}$ or even $25^{\circ} \mathrm{C}$. Temperatures colder than $0^{\circ} \mathrm{F}$ (negative values) were generally rounded to the nearest $1^{\circ} \mathrm{C}$. The examples in the table below were created by rounding to the nearest $5^{\circ} \mathrm{C}$, with one exception:

| Temperature, ${ }^{\circ} \mathrm{F}$ | Temperature, ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: |
| 70 | 20 |
| 100 | 38 |
| 120 | 50 |
| 150 | 65 |
| 200 | 95 |
| 250 | 120 |
| 300 | 150 |
| 350 | 175 |
| 400 | 205 |
| 450 | 230 |
| 500 | 260 |
| 550 | 290 |
| 600 | 315 |
| 650 | 345 |
| 700 | 370 |
| 750 | 400 |
| 800 | 425 |
| 850 | 455 |
| 900 | 480 |
| 925 | 495 |
| 950 | 510 |
| 1,000 | 540 |
| 1,050 | 565 |
| 1,100 | 595 |
| 1,150 | 620 |
| 1,200 | 650 |
| 1,250 | 675 |
| 1,800 | 1040 |
| 1,900 | 1095 |
| 2,000 | 1120 |
| 2,050 |  |
|  | 20 |

## G-300 CHECKING EQUATIONS

When a single equation is provided, it has been checked using dimensional analysis to verify that the results obtained by using either the U.S. Customary or SI units provided are equivalent. When constants used in these equations are not dimensionless, different constants are provided for each system of units. Otherwise, a U.S. Customary and an SI version of the equation are provided. However, in all cases, the Code user should check the equation for dimensional consistency.

## G-400 EXAMPLES OF DIMENSIONAL ANALYSIS

(a) This example illustrates the concept of dimensional analysis.
(1) Equation and Nomenclature

$$
S=\frac{P r}{t}
$$

where

$$
\begin{aligned}
& S=\text { stress, psi (MPa) } \\
& P=\text { pressure, psi }(\mathrm{MPa}) \\
& r=\text { radius, inches }(\mathrm{mm}) \\
& t=\text { thickness, inches }(\mathrm{mm}) \\
& \text { (2) Dimensional Analysis } \\
& S\left[\frac{\text { pounds }}{\text { (inches)(inches) }}\right]=\frac{P\left[\frac{\text { pounds }}{(\text { inches })(\text { inches })}\right] r \text { (inches) }}{t(\text { inches })}
\end{aligned}
$$

(b) Note that in the above equation, it is necessary that the dimensions of the radius, $r$, and the thickness, $t$, be the same, since they must cancel out. The dimensions of the pressure, $P$, and the stress, $S$, must also be the same. For this particular equation, $r$ and $t$ could be in U.S. Customary units and $P$ and $S$ in SI units, and the result would still be acceptable. Further, any consistent units could be used for the radius and the thickness (e.g., feet, miles, meters, light years) and the result would be the same. Similarly, the units of pressure and stress can be any legitimate pressure or stress unit (e.g., psi, ksi, $\mathrm{kPa}, \mathrm{MPa}$ ), as long as they are the same.
(c) When the equation is converted to SI units,

$$
S(\mathrm{MPa})=\frac{P(\mathrm{MPa}) r(\mathrm{~mm})}{t(\mathrm{~mm})}
$$

(d) However, more complex equations present special challenges, e.g., it is necessary to add the stress from an axial load acting on a cylinder to the stress that results from pressure.

## (1) Equation and Nomenclature

$$
S_{t}=\frac{P r}{2 t}+\frac{L}{2 \pi r t}
$$

where

$$
\begin{aligned}
S_{t} & =\text { total stress, } \mathrm{psi}(\mathrm{MPa}) \\
P & =\text { pressure, psi }(\mathrm{MPa}) \\
L & =\text { load, pounds }(\mathrm{N}) \\
r & =\text { radius, inches }(\mathrm{mm}) \\
t & =\text { thickness, inches }(\mathrm{mm})
\end{aligned}
$$

(2) Dimensional Analysis

$$
\begin{aligned}
S_{t}\left[\frac{\text { pounds }}{(\text { inches })(\text { inches })}\right]= & \frac{P\left[\frac{\text { pounds }}{(\text { (inches })(\text { inches })}\right] r(\text { inches })}{2 t(\text { inches })} \\
& +\frac{L(\text { pounds })}{2 \pi r(\text { inches }) t(\text { inches })}
\end{aligned}
$$

(e) Note that in the above equation, it is necessary that the pressure, load, and length dimensions be consistent, because quantities cannot be added unless they have the same units. Although the first part of the equation is similar to the first example, where the length and pressure units could be in different systems, the second example requires that if the pressure and stress units are in pounds per square inch, the load must be in pounds and the radius and thickness must be in inches. Note that the load could be in kips and the pressure in ksi. This is why we should permit any consistent system of units to be used. However, the equations should be checked only for the "standard" units.
(f) When the equation is converted to SI units,

$$
S_{t}(\mathrm{MPa})=\frac{P(\mathrm{MPa}) r(\mathrm{~mm})}{2 t(\mathrm{~mm})}+\frac{L(\mathrm{~N})}{2 \pi r(\mathrm{~mm}) t(\mathrm{~mm})}
$$

Note that $1 \mathrm{MPa}=1 \mathrm{~N} / \mathrm{mm}^{2}$, so

$$
S_{t}\left[\frac{\mathrm{~N}}{(\mathrm{~mm})(\mathrm{mm})}\right]=\frac{P\left[\frac{\mathrm{~N}}{(\mathrm{~mm})(\mathrm{mm})}\right] r(\mathrm{~mm})}{2 t(\mathrm{~mm})}+\frac{L(\mathrm{~N})}{2 \pi r(\mathrm{~mm}) t(\mathrm{~mm})}
$$

which reduces to

$$
S_{t}\left[\frac{\mathrm{~N}}{(\mathrm{~mm})(\mathrm{mm})}\right]=\frac{P(\mathrm{~N}) r(\mathrm{~mm})}{(\mathrm{mm})(\mathrm{mm}) 2 t(\mathrm{~mm})}+\frac{L(\mathrm{~N})}{2 \pi r(\mathrm{~mm}) t(\mathrm{~mm})}
$$

$(g)$ Therefore, the units in the above equation are consistent. However, this is not always the case. For example, the bolted joint design rules define an effective gasket seating width as a function of the actual width using an equation of the form below.
(1) Equation and Nomenclature

$$
b_{e}=\sqrt{b_{a}}
$$

where
$b_{e}=$ effective gasket seating width
$b_{a}=$ actual gasket seating width
(2) Dimensional Analysis

$$
b_{e}(\text { inches })=\sqrt{b_{a}(\text { inches })}
$$

(h) Obviously, the equation above is not dimensionally consistent; therefore, a constant is needed if it is to be used with SI units. The constant can be calculated by converting the SI unit (mm) to the U.S. Customary unit
(in.) for the calculation, then converting back to get the result in mm as follows:

$$
b_{e}(\mathrm{~mm})=25.4(\mathrm{~mm} / \mathrm{inch}) \sqrt{\frac{b_{a}(\mathrm{~mm})}{25.4(\mathrm{~mm} / \mathrm{inch})}}
$$

which can be reduced to

$$
b_{e}(\mathrm{~mm})=5.04 \sqrt{b_{a}(\mathrm{~mm})}
$$

## G-500 SOFT CONVERSION FACTORS

The following table of "soft" conversion factors is provided for convenience. Multiply the U.S. Customary value by the factor given to obtain the SI value. Similarly, divide the SI value by the factor given to obtain the U.S. Customary value. In most cases it is appropriate to round the answer to three significant figures.

| U.S. <br> Customary | SI | Factor | Notes |
| :---: | :---: | :---: | :---: |
| in. | mm | 25.4 |  |
| ft | m | 0.3048 |  |
| in. ${ }^{2}$ | $\mathrm{mm}^{2}$ | 645.16 |  |
| $\mathrm{ft}^{2}$ | $\mathrm{m}^{2}$ | 0.09290304 | $\ldots$ |
| in. ${ }^{3}$ | $\mathrm{mm}^{3}$ | 16,387.064 |  |
| $\mathrm{ft}^{3}$ | $\mathrm{m}^{3}$ | 0.02831685 |  |
| U.S. gal | $\mathrm{m}^{3}$ | 0.003785412 | $\ldots$ |
| U.S. gal | liters | 3.785412 |  |
| psi | MPa | 0.0068948 | Used exclusively in equations |
| psi | kPa | 6.894757 | Used only in text and for nameplate |
| ft -lb | J | 1.355818 |  |
| ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | $5 / 9 \times\left({ }^{\circ} \mathrm{F}-32\right)$ | Not for temperature difference |
| ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | $5 / 9 \times{ }^{\circ} \mathrm{F}$ | For temperature differences only |
| R | K | 5/9 | Absolute temperature |
| lbm | kg | 0.4535924 |  |
| lbf | N | 4.448222 |  |
| in.-lb | $\mathrm{N} \cdot \mathrm{mm}$ | 112.98484 | Use exclusively in equations |
| ft -lb | $\mathrm{N} \cdot \mathrm{m}$ | 1.3558181 | Use only in text |
| $\mathrm{ksi} \sqrt{\text { in. }}$ | $\mathrm{MPa} \sqrt{\mathrm{m}}$ | 1.0988434 |  |
| Btu/hr | W | 0.2928104 | Use for boiler rating and heat transfer |
| $\mathrm{lb} / \mathrm{ft}^{3}$ | $\mathrm{kg} / \mathrm{m}^{3}$ | 16.018463 |  |

## G-600 SPECIAL REQUIREMENTS FOR POSTWELD HEAT TREAT TIMES

In general, PWHT times in hours per inch of thickness were converted to minutes per millimeter of thickness as follows:
(a) $1 \mathrm{hr} / \mathrm{in} .=2 \mathrm{~min} / \mathrm{mm}$. Although this results in heat treatment for only 51 min for a 25.4 mm thick section, this is considered to be within the range of intended precision of the U.S. Customary requirement.
(b) $15 \mathrm{~min} / \mathrm{in}$. $=0.5 \mathrm{~min} / \mathrm{mm}$. Although converting and rounding would give $0.6 \mathrm{~min} / \mathrm{mm}$, it was necessary to use 0.5 to be consistent with the rounding for $1 \mathrm{hr} / \mathrm{in}$.

## G-700 NOTES ON CONVERSIONS IN SECTION II, PARTS A, B, AND C

The conversions provided by ASTM and AWS were used for consistency with those documents.

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[^0]:    ${ }^{1}$ Construction, as used in this Foreword, is an all-inclusive term comprising materials, design, fabrication, examination, inspection, testing, certification, and pressure relief.

[^1]:    ${ }^{1}$ Wherever these words are used in Section IX, they shall include installer or assembler.

[^2]:    (1) The following variables further restrict the limits shown in this table when they are referenced in QW-250 for the process under consideration: QW-403.9, QW-403.10, QW-404.32, and QW-407.4. Also, QW-202.2, QW-202.3, and QW-202.4 provide exemptions that supersede the limits of this table.
    (2) (2) For combination of welding procedures, see QW-200.4
    (4) See QW-151.1, QW-151.2, and QW-151.3 for details on multiple specimens when coupon thicknesses are over 1 in . ( 25 mm ). (5) Four side-bend tests may be substituted for the required face- and root-bend tests, when thickness $T$ is $3 / 8 \mathrm{in}$. ( 10 mm ) and over.

[^3]:    ${ }^{1}$ Wherever these words are used in Section IX, they shall include installer or assembler.
    ${ }^{2}$ In the following paragraphs the word position is synonymous with flow position.

