#### ADDENDUM NO. 01

DATE: Tuesday June 21, 2016

PROJECT: City of Sugar Hill EpiCenter

**CPL PROJECT NO.: 13886.00** 

FROM: Clark Patterson Lee

3011 Sutton Gate Drive

Suite 130

Suwanee, GA 30024

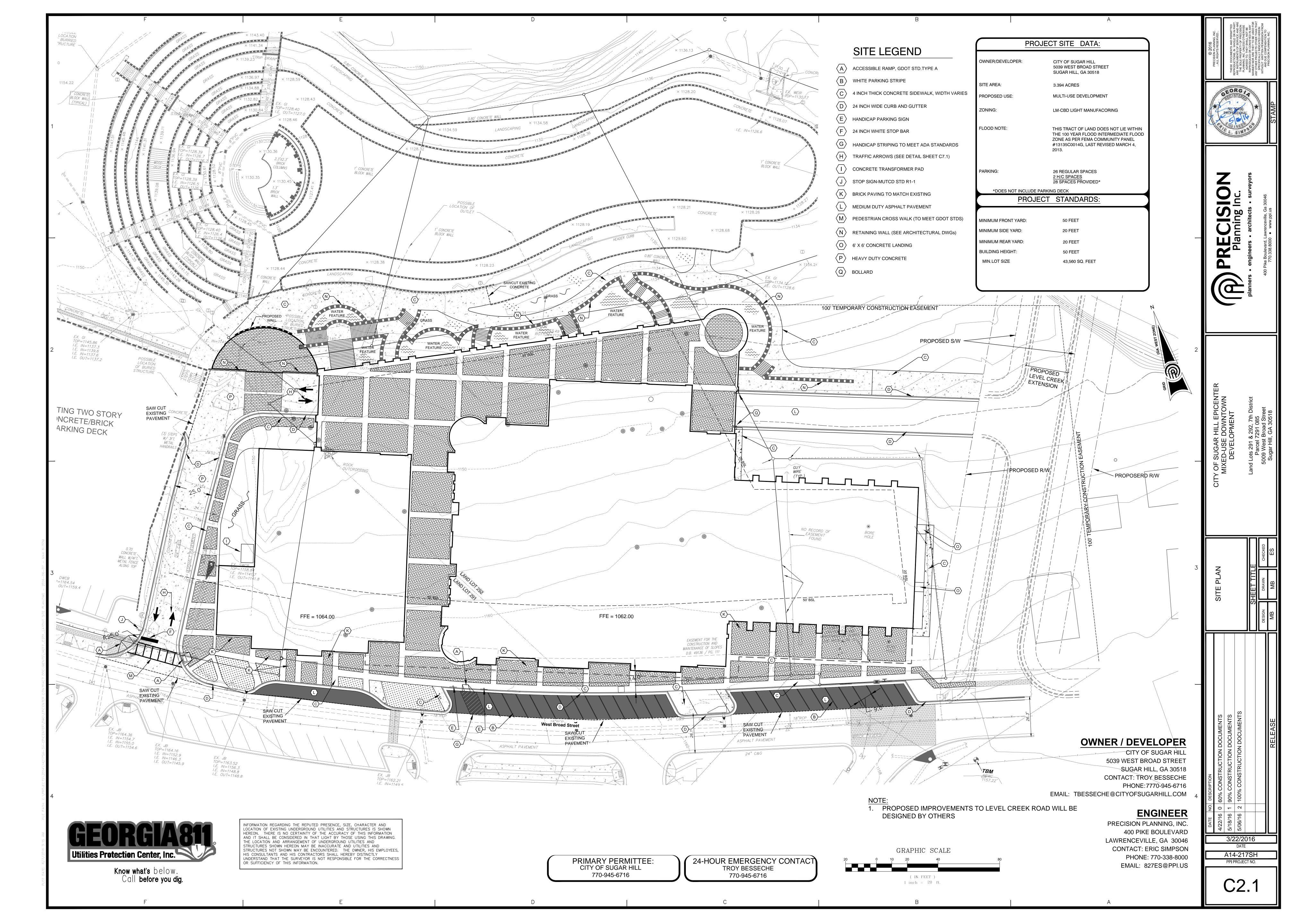
TO: Prospective Proposers

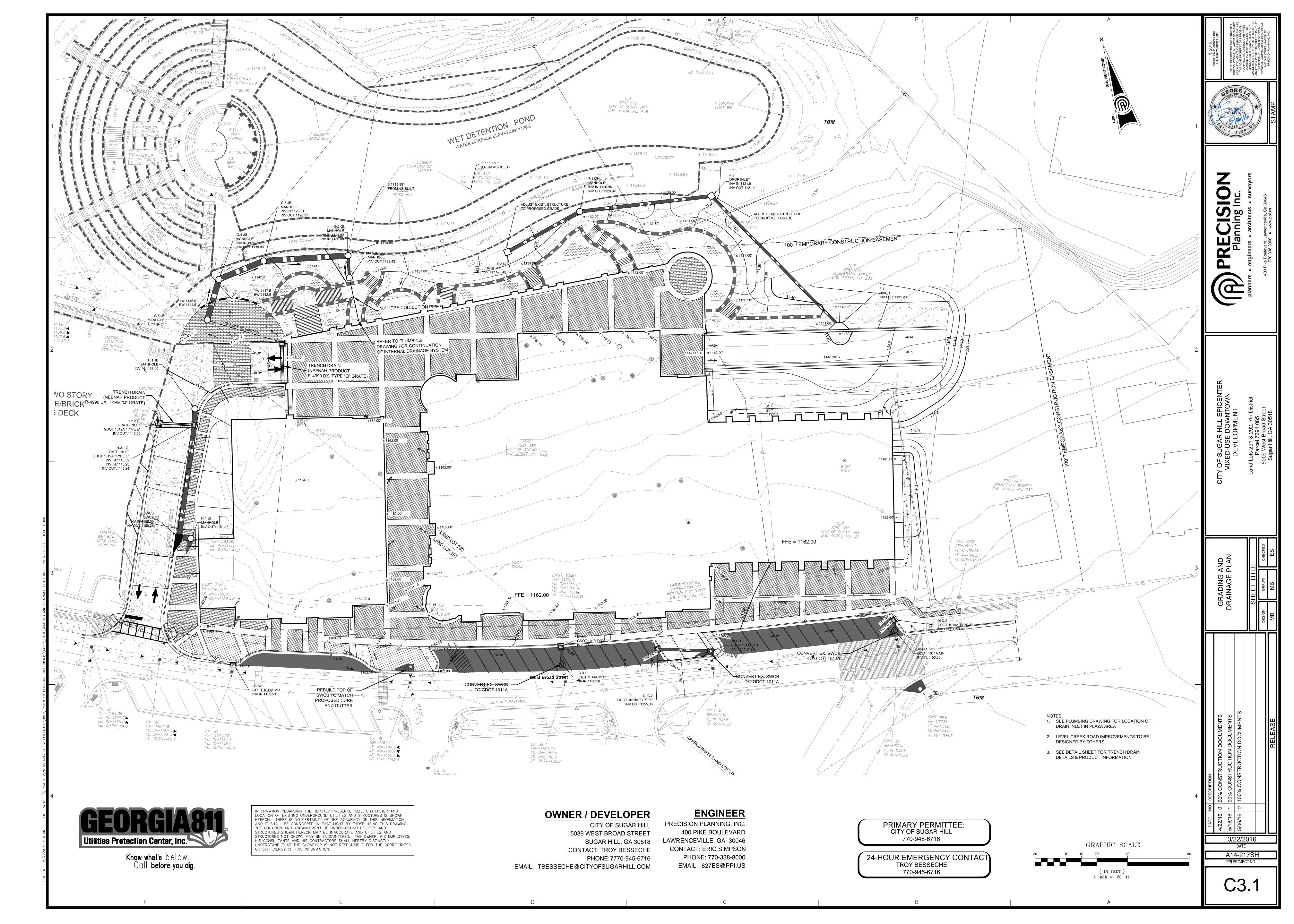
This Addendum supplements portions of the original Request for Proposal, the extent of which shall remain, except for the additional information provided herein to assist in preparation of proposals;

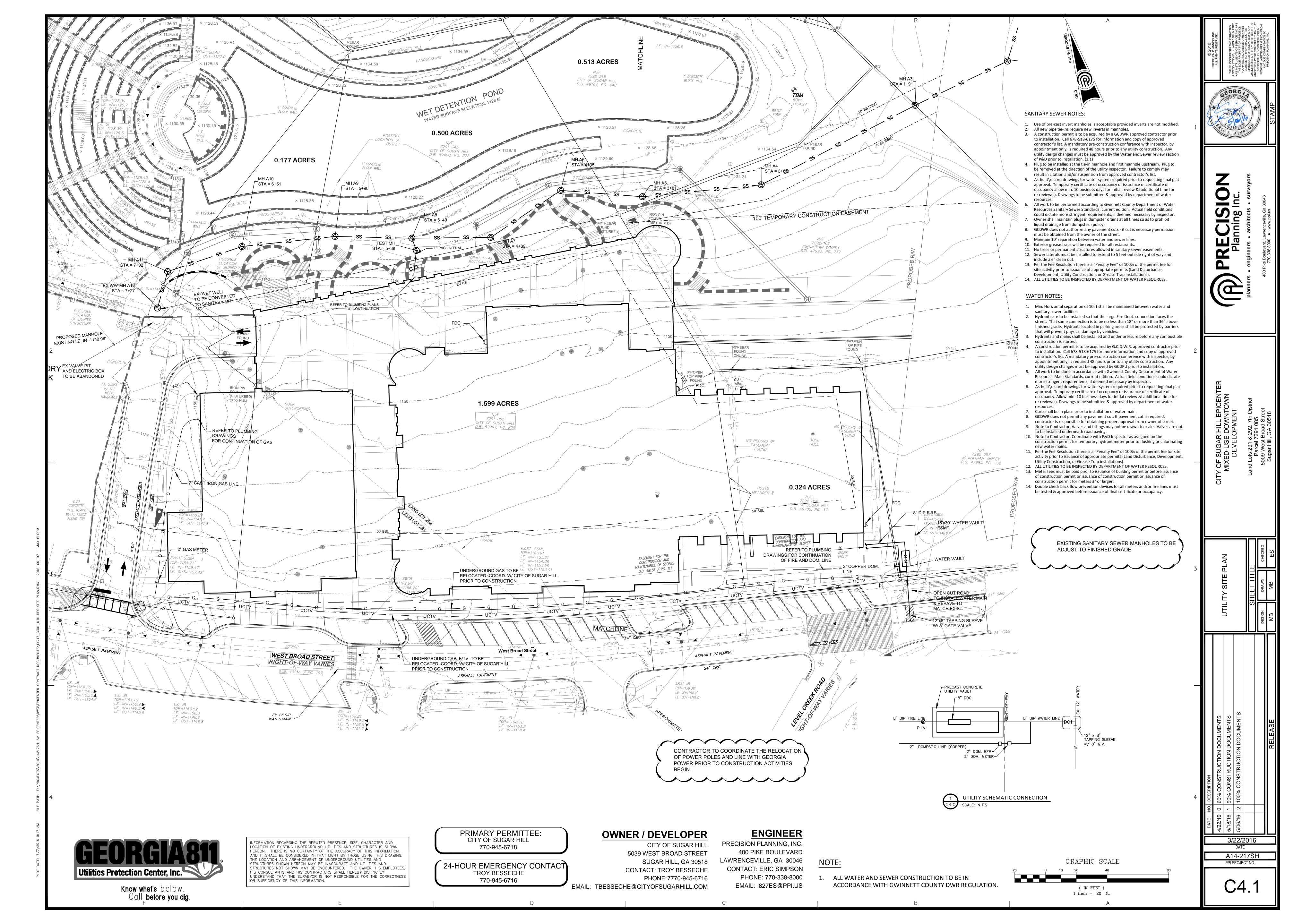
- 1. C2.1 Site Plan
- 2. C3.1 Grading Plan
- 3. C4.1 Utility Site Plan
- 4. C4.2 Utility Site Plan
- 5. Geotechnical report

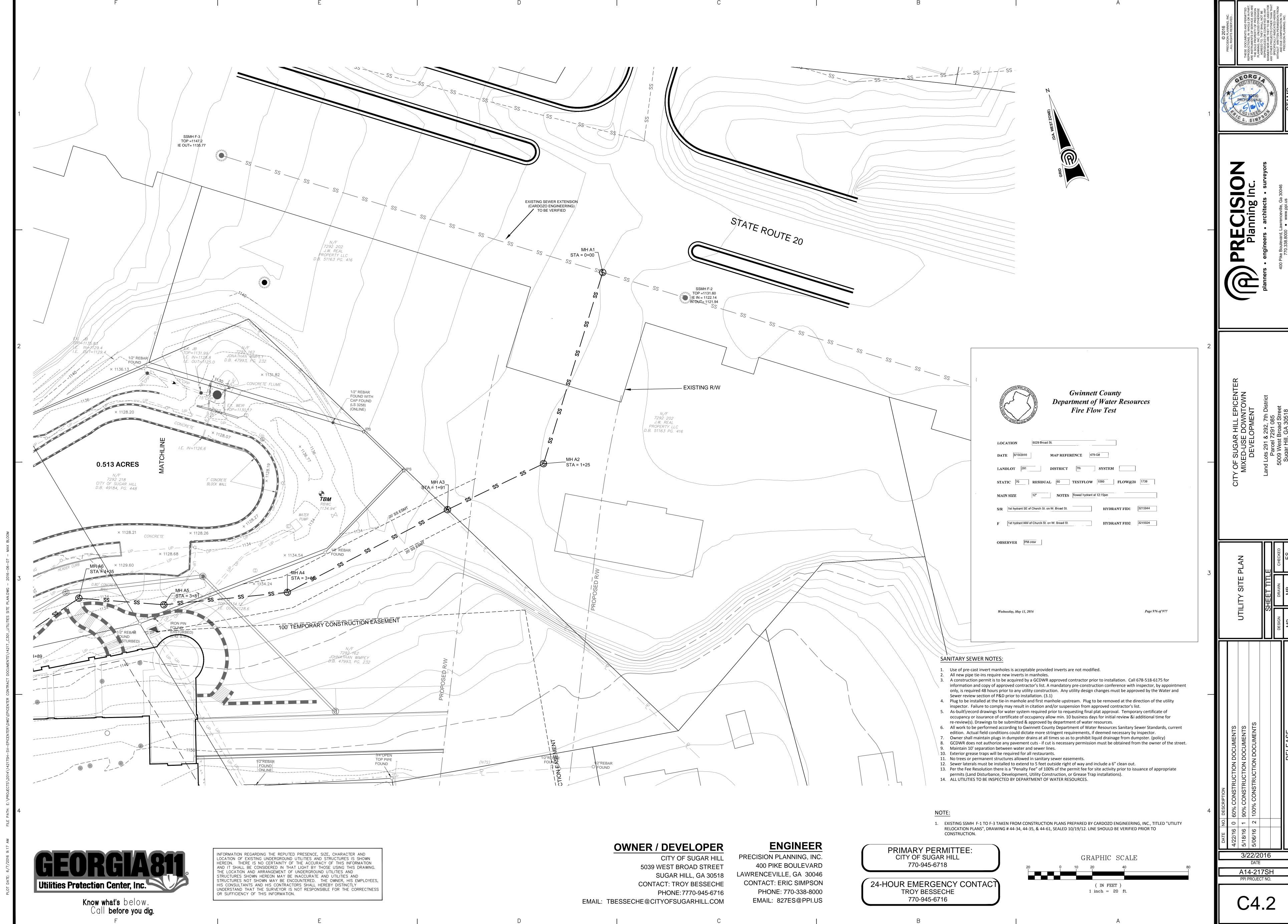
Should you have any questions or concerns please do not hesitate to contact us.

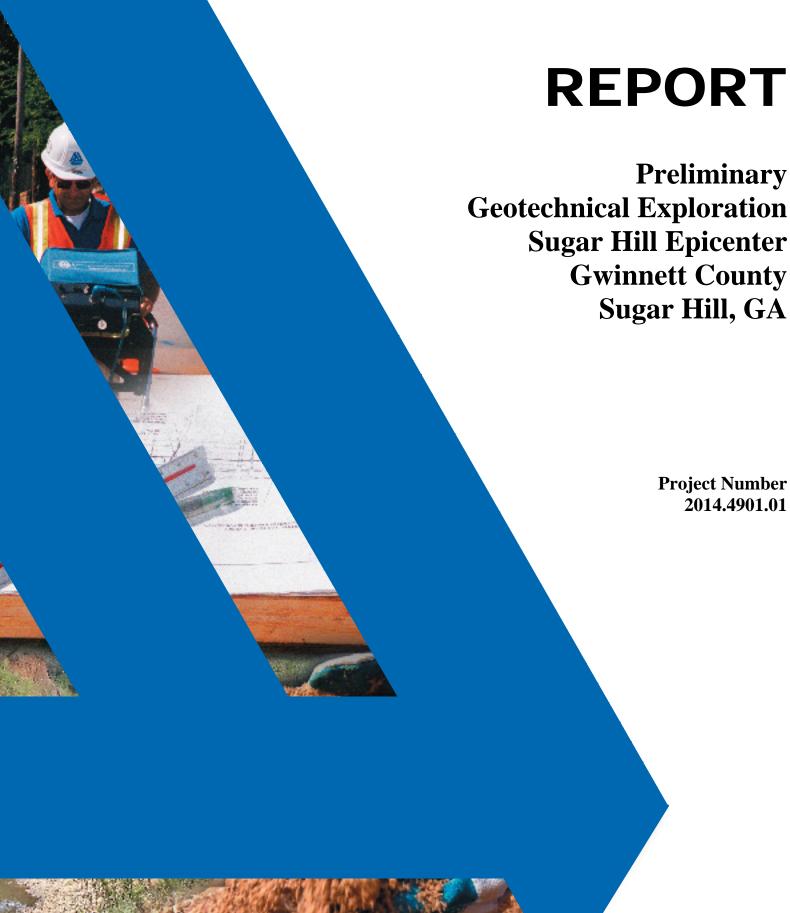
END OF ADDENDUM NO. 01











**September 16, 2014** 





September 16, 2014

Mr. Troy Besseche City of Sugar Hill 5039 West Broad Street Sugar Hill, Georgia, 30518

Via E-mail: tbesseche@cityofsugarhill.com

RE: Report of Preliminary Geotechnical Exploration

> Sugar Hill Epicenter 5009 West Broad Street

Sugar Hill, Gwinnett County, Georgia

Project No. 2014.4901.01

Dear Mr. Besseche:

United Consulting is pleased to submit this report of our Preliminary Geotechnical Exploration for the above-referenced project. We appreciate the opportunity to assist you with this project. Please contact us if you have any questions or if we can be of further assistance.

Sincerely,

UNITED CONSULTING

Kheibar Khanidokht, P.E.

Senior Geotechnical Engineer

Chris L. Roberds, P.G.

Senior Executive Vice President

Donald E. Hill, P.E. Chief Engineer

CJC/KK/CLR/DEH/nj

ucblade10/sites/geotechenv/10327/2014.4901.01/Environmental Documents/Geotechnical/2014.4901.01.suger hill pre. geo.doc

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#### **FIGURE**

Figure 1 - Boring Location Plan

#### **APPENDIX**

General Notes/Narrative of Drilling Operations Boring Logs (8)





#### **EXECUTIVE SUMMARY**

United Consulting has completed a Preliminary Geotechnical Exploration on the **Sugar Hill Epicenter** tract located in Gwinnett County, Sugar Hill, Georgia. The results from this investigation are briefly summarized below. The text of the report should be reviewed for a discussion of these items.

- 1. The borings encountered fill soils to depths of 3 to 13 feet. The fill was highly variable and included occasional topsoil and rock fragments were noted in the fill. As is the case with any previously graded site, undocumented fill can contain soft soils, or buried trash, topsoil, boulders, or other unsuitable materials. Unsuitable materials, if encountered in the fill soils, shall be removed and replaced and/or stabilized per the geotechnical engineer's recommendations.
- 2. Partially Weathered Rock (PWR) was encountered in borings B-2 and B-6 at depths of about 49 feet and 44 feet below the existing grade. Auger refusal occurred in borings B-2 and B-6 at depths 56 feet and 71 feet, respectively. We do not generally envision significant excavation difficulties associated with massive PWR or rock for this project.
- 3. We envision that lightly loaded structures (timber framed structures with column loads not exceeding 150 kips and wall loads not exceeding 6 klf) can be supported on conventional shallow foundations. Due to the presence of variable condition existing fill, some excavation and replacement of soft or otherwise unsuitable soils from below the planned foundation bearing locations should be anticipated and budgeted for.
- 4. United Consulting believes that more heavily loaded (concrete or steel framed) multistory residential structures and the concrete parking deck will likely require a deep foundation system (piles) or a shallow foundations constructed over compacted aggregate piers (Geopiers or Vibropiers). Preliminary recommendations for these foundation options are included in the text.
- 5. Groundwater was encountered in borings B-2 and B-6 at depths 35 and 37 feet at the time of boring. The influence of groundwater on the proposed development will depend on the finalized grading plan. The contractor should be prepared to remove groundwater or perched water, if encountered.
- 6. United Consulting recommends that a seismic site classification of "Site Class D" per Chapter 16 of the 2006 International Building Code (IBC) be utilized for the site.
- 7. Once final grades, finished floor elevations and foundation loads are determined, the preliminary recommendations in this report should be re-evaluated and, and additional geotechnical exploration be conducted.





#### SITE AND PROJECT INFORMATION

The project site is located on the northeast quadrant of the intersection between West Broad Street and Lee Street in Sugar Hill, Georgia. The client provided a site plan via e-mail dated September 9, 2014, prepared by Precision Planning, Inc., showing the client's desired boring locations. This site plan was used as a guide to locate the boundaries of the project site during this exploration. The locations of the borings are shown on the attached Boring Location Plan (Figure 1).

At the time of our visit, the site was accessed via West Broad Street to the southeast of the project site. The site consisted of 2 parcels totaling approximately 1.9 acres of land and contained one residential structure. The remainder of the site consisted of sparse landscaped areas around the residential structure and partially wooded land. The northeastern portion of the site contained a few parked trucks. These trucks appear to be associated with an off-site facility. The adjoining properties consisted of commercial and local government buildings.

At the time of completion of this report, no topographic information was provided. Based on our visual observation, the site generally slopes down to the north and east from higher areas in the south and west. Total relief across the site is approximately 10 feet.

We understand that the project is at the preliminary stage of design and the proposed development will consist of a mixed-use development that includes a gymnasium, a swimming pool, parking deck and other amenities. The existing structures within the proposed development will be demolished prior to the new construction.

No information on the building structural loads, grading plan, or finished ground floor elevations for the proposed structures was available at the time of this report.

The recommendations herein should be considered preliminary. Once the grading plans and proposed structural loads have been finalized, a final geotechnical exploration should be performed in order to finalize our recommendations.

#### **PURPOSE**

The purpose of this preliminary exploration was to determine the general type and condition of the subsurface materials at the project site, and to provide preliminary recommendations regarding potential foundation types and general information regarding soil types, fill availability and suitability, depth to groundwater and rock, and other geotechnical considerations that may impact site development plans.





#### SCOPE

The scope of our Preliminary Geotechnical Exploration has included the following items:

- 1. A visual reconnaissance of the site from a geotechnical standpoint;
- 2. Drilling eight (8) Standard Penetration Test (SPT) borings to determine the nature and condition of the subsurface soils;
- 3. Evaluation of soil samples obtained during our field exploration program for further identification and classification;
- 4. Determine IBC seismic site class based on average N-values;
- 5. Analyzing subsurface conditions with respect to the proposed construction; and
- 6. Preparing this report to document the results of our fieldwork program, general information regarding soil types, provide preliminary recommendations for site work, seismic site class, and foundation design for conceptual development based on subsurface soil exploration.

#### **EXPLORATION PROCEDURES**

Eight Standard Penetration Test (SPT) borings (designated as B-1 through B-8) were drilled at the approximate locations shown on the attached Boring Location Plan (Figure 1). Soil samples obtained using the split spoon sampler were examined by the Geotechnical Engineer and classified according to the visual-manual procedure described in ASTM D 2488-00. Soil test borings were performed in general accordance with ASTM D 1586. A narrative of field operations is included in The Appendix.

Boring locations were determined in the field by the Geotechnical Engineer who measured distances and estimated angles with the aid of a hand held compass, a measuring tape and existing site features. Therefore, the boring locations shown on the attached boring plan should be considered approximate. A topographic plan of the site was not available at the time of completion of the report, therefore, ground elevations are not provided on the boring logs.

#### SUBSURFACE CONDITIONS

The borings initially encountered 3 inches of topsoil. The borings encountered fill below the topsoil to depths 3 to 13 feet. The soils generally consisted of firm to very stiff sandy silt with traces of rock fragments, clay and mica with the N-values ranging from 5 to 16 blows per foot (bpf).





Below the fill soils, residual soils typical of the Piedmont Physiographic Region were encountered. The residual soils generally consisted of stiff to hard sandy silt or firm to dense silty sand with varying amounts of mica and rock fragments, and traces of clay with the N-values in the residual soils ranging from 11 to 49 bpf.

Partially Weathered Rock (PWR) was encountered in borings B-2 and B-6 at depths ranging from 50 to 70 feet below existing grade. PWR is a term for the residuum that can be penetrated by soil drilling techniques and has standard penetration resistance values (N-values) in excess of 100 bpf.

Auger refusal occurred in borings B-2 and B-6 at depths of 56 feet and 71 feet, respectively. Auger refusal indicates the depth at which the boring cannot be drilled further using soil drillings tools and techniques. Auger refusal levels may represent the top of massive bedrock, a boulder or other obstruction.

Groundwater was encountered in borings B-2 and B-6 at depths 35 feet and 37 feet at the time of drilling. No groundwater was encountered in the remaining borings. Groundwater levels should be anticipated to fluctuate with the change of seasons, during periods of very low or high precipitation, or due to changes in the floodplain or watershed upstream from the area.

For a more precise description of the conditions encountered within the soil test borings, we refer you to the Boring Logs included in The Appendix.

#### DISCUSSION AND PRELIMINARY RECOMMENDATIONS

The following preliminary recommendations are based on our understanding of the proposed construction, the data obtained from our soil test borings and our experience with soils and subsurface conditions similar to those encountered at this site.

Since finished floor elevation (FFE) and structural loads have not been finalized the following information and recommendations should be considered preliminary. Once the design drawings are finalized, additional subsurface exploration and engineering analyses will be required to finalize our preliminary recommendations.

#### **Existing Fill Consideration**

Below the topsoil, the borings encountered fill to depths ranging from 3 to 13 feet. The fill generally appeared to be relatively clean and moderately compacted.

As is the case with any previously graded site, undocumented fill can contain soft soils, or buried trash, topsoil, boulders, or other unsuitable materials. For construction on an undocumented fill, the owner must assume the risk of greater than normal settlement due to the possible presence of soft soils or unsuitable materials within the fill. SPT borings alone are not well suited to evaluate existing fill.





We recommend excavating test pits to further evaluate the condition and lateral extent of the fill. If not removed during mass grading, some excavation of soft or otherwise unsuitable fill should be anticipated and budgeted for.

#### **Excavation Conditions**

Partially Weathered Rock (PWR) was encountered in borings B-2 and B-6 a depth of about 49 feet and 44 feet below the existing grade. Auger refusal occurred in borings B-2 and B-6 at depths 56 feet and 71 feet, respectively. We do not generally envision significant excavation difficulties associated with massive PWR or rock for this project.

Due to the geology of the area, depth to bedrock can vary significantly over short horizontal distances. Therefore, it is not uncommon to encountered PWR and rock at shallower depths than those encountered in the borings. Pinnacles, boulders or lenses of PWR or rock could therefore be present at higher elevations, between or away from the areas explored.

Conventional scrapers and loaders can generally excavate soils. PWR typically requires loosening by ripping with large dozers pulling single tooth rippers in mass excavation or the use of jackhammers or light blasting in confined (trench) excavation. Relatively sound, massive, rock typically requires blasting for removal in mass or trench excavation.

#### **Caving Considerations**

Due to the presence of existing fill and low-cohesive soil, some caving of excavations should be anticipated. Flattening of the excavation sidewalls and/or the use of bracing may be needed to maintain stability. All excavations must be performed in accordance with OSHA excavation safety standards.

#### **Groundwater Conditions**

Groundwater was encountered in borings B-2 and B-6 at depths 35 feet and 37 feet at the time of drilling. Due to presence of up to 13 feet of highly variable fill and silt, the site is also susceptible to formation of perched water. The contactor should be prepared to remove perched or groundwater as needed.

Overall, the actual impact of the groundwater on the planned development will depend greatly on the final grading plan, utility profiles, and building FFEs.

#### **Preliminary Foundation Design**

The most appropriate foundation system for the project will depend on the actual building/structure types, locations, FFEs, building loads, and settlement tolerances. Once this information becomes available we welcome the opportunity to assist you in developing final foundation recommendations for the project. We offer the following preliminary foundation recommendations for the project.





#### Lightly Loaded Structures - Conventional Shallow Foundations

We envision that lightly loaded structures (timber framed structures with column loads not exceeding 150 kips and wall loads not exceeding 6 klf) can be supported on conventional shallow foundations. Foundation area preparation will be dependent on the final grading plan and building FFEs. However, if existing fill is to remain below the proposed foundation areas, some excavation and replacement of the existing fill should be anticipated and budgeted for in order for shallow foundations to be feasible.

#### More Heavily Loaded Structures and Parking Deck

For the concrete parking deck and other more heavily loaded structures (concrete or steel framed structures with column loads exceeding 150 kips and wall loads exceeding 6 klf) we envision that shallow foundations will not likely be feasible due to the variability of the subsurface conditions across the site, and the potential for excessive settlements. United Consulting believes that a deep foundation system (auger cast piles) or possibly, a shallow foundation underlain by a ground improvement system (such as compacted aggregate columns) would most likely be required for support of the more heavily loaded structures. United Consulting offers the following preliminary discussions regarding possible foundation types for the project.

#### Deep Foundation - Auger-Cast Piles

An allowable pile capacity in the range of 70 to 150 tons per pile is typically available for 14 to 18-inch auger-cast piles installed to practical refusal or sufficient embedment into very dense PWR. We note that continuous PWR was encountered at depths ranging from 44 feet to 48 feet and rock was encountered at a depth of 56 and 71 feet in borings B-2 and B-6. As such auger-cast piles for the project could be designed as friction piles embedded into very dense PWR. Higher capacities might be available if piles are extended through the PWR to practical refusal in competent rock.

#### Deep Foundation – Ground Improvement (Compacted Stone Piers)

We envision that a properly designed and installed compacted stone pier system (Geopiers or Vibropiers) would also be suitable to improve soils such that the proposed structures could be supported on conventional shallow foundations underlain by stone piers.

The bearing capacity and settlement of the compacted stone piers are a function of the on-site soils, the strength (modulus) of the compacted aggregate within the stone columns, the length of the columns, and the percentage of the foundation bearing area that is directly supported by the stone piers. Typically, a conventional shallow foundation system bearing on a properly designed and installed compacted stone column system may be designed for an allowable bearing pressure in the range of 4,000 to 6,000 psf.

Additional subsurface exploration and engineering evaluation based on the actual planned building structural loads and FFEs will be required to further assess the feasibility of using compacted stone columns for support of the multi-story structures.





#### **Seismic Site Class**

The seismic design is covered by the provisions of Chapter 16 of the International Building Code (IBC). The site categories referenced in the IBC are defined in terms of the average shear wave velocity ( $V_s$ ) in the top 100 ft of the profile. In absence of shear wave velocities, geotechnical parameters such as standard penetration resistance (N) and the undrained shear strength ( $S_u$ ) can be utilized.

United Consulting utilized available geotechnical information (N-values) and our experience with the similar soil conditions to provide a seismic site class for the site. United Consulting recommends that a seismic site classification of "Site Class D" be utilized for the site. Based on published data, the liquefaction potential of the on-site soils is considered low.

A site class determination based on the average N values is necessarily conservative. A site-specific geophysical study acquiring soil shear wave velocity data may or may not demonstrate sufficient stiffness to allow a higher site class. Shear wave velocity measurements were beyond our authorized scope of work. United Consulting will be pleased to provide the additional seismic services, if requested.

#### **Earthwork**

The soils encountered at the project site should be generally suitable for re-use as engineered fill. Existing fill containing excessive boulders, topsoil, or other unsuitable materials, if encountered, would not be considered suitable. Again, test pits are recommended to further evaluate the extent and condition of the existing fill.

#### **Final Geotechnical Exploration**

The subsurface data gathered in this preliminary geotechnical exploration should be used to plan the site development, layout and earthwork so that difficult excavation and ground improvement requirements can be considered. Once the building FFEs, and foundation loads are finalized, additional borings with rock coring and test pits should be preformed to develop final geotechnical recommendations specific to the actual planned construction. The information provided in this preliminary geotechnical exploration report should be used to develop the scope the finial Geotechnical Exploration.

#### LIMITATIONS

This report is for the exclusive use of **City of Sugar Hill** and the designers of the project described herein, and may only be applied to this specific project. Our conclusions and preliminary recommendations have been prepared using generally accepted standards of Geotechnical Engineering practice in the State of Georgia. No other warranty is expressed or implied. Our firm is not responsible for conclusions, opinions or recommendations of others.





The right to rely upon this report and the data within may not be assigned without UNITED CONSULTING'S written permission.

The scope of this geotechnical evaluation was limited to an evaluation of the load-carrying capabilities and stability of the subsoils. Oil, hazardous waste, radioactivity, irritants, pollutants, molds, or other dangerous substance and conditions were not the subject of this study. Their presence and/or absence is not implied or suggested by this report, and should not be inferred.

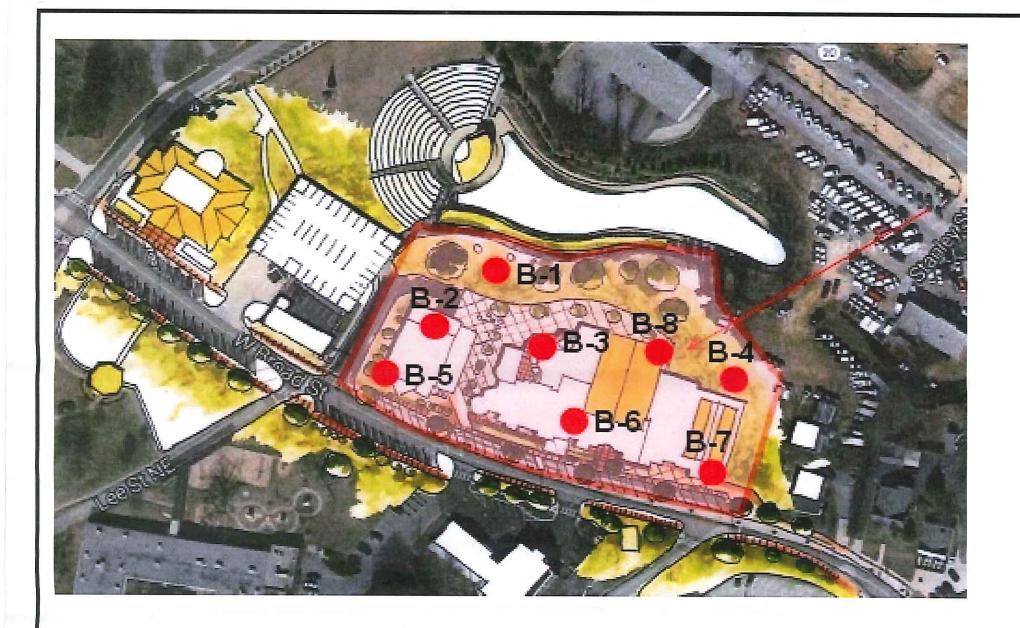
Our conclusions and recommendations are based upon design information furnished us, data obtained from the previously described exploration and testing program and our experience. They do not reflect variations in subsurface conditions that may exist intermediate of our borings and in unexplored areas of the site. Should such variations become apparent during construction, it will be necessary to re-evaluate our conclusions and recommendations based upon "on-site" observations of the conditions.

If the design or location of the project is changed, the preliminary recommendations contained herein must be considered invalid, unless our firm reviews the changes and our recommendations are either verified or modified in writing. When design is complete, we should be given the opportunity to review the foundation plan, grading plan, and applicable portions of the specifications to see if they are consistent with the intent of our recommendations.

#### **UNITED CONSULTING**







Notes:





Scale:	NTS
Prepared:	KN
Checked:	KK
Project No.:	2014.4901.01

	•	
Client:	City of Sugar Hill	Г
Site:	Sugar Hill Epicenter	
Title:	Boring Location Plan	

FIG.1

#### **APPENDIX**

General Notes/Narrative of Drilling Operations Boring Logs (8)

#### **GENERAL NOTES**

The soil classifications noted on the Boring Logs are visual classifications unless otherwise noted. Minor constituents of a soil sample are termed as follows:

0 - 10%
11 - 35%
36 - 49%

#### **LEGEND**

	Split Spoon Sample obtained during Standard Penetration Testing
$\boxtimes$	Relatively Undisturbed Shelby Tube Sample
	Groundwater Level at Time of Boring Completion
<u>_</u>	Groundwater Level at 24 hours (or as noted) after Termination of Boring
w	Natural Moisture Content
LL PL PI	Liquid Limit Plastic Limit Atterberg Limits Plasticity Index
PF	Percent Fines (Percent Passing #200 Sieve)
8 d 8 m 8 sat	Dry Unit Weight (Pounds per Cubic Foot or PCF Moist or In-Situ Unit Weight (PCF) Saturated Unit Weight (PCF)

#### BORING LOG DATA AND NARRATIVE OF DRILLING OPERATIONS

The test borings were made by mechanically advancing helical hollow stem augers into the ground. Samples were covered at regular intervals in each of the borings following established procedures for performing the Standard Penetration Test in accordance with ASTM Specification D-1586. Soil samples were obtained with a standard 1.4" I.D. x 2.0" O.D. split barrel sampler. The sampler is first seated 6" to penetrate any loose cuttings and then driven an additional foot with the blows of a 140 pound hammer freely falling a distance of 30". The number of blows required to drive the sampler each six inches is recorded on the Boring Logs. The total number of blows required to drive the sampler the final foot is designated the "standard penetration resistance." This driving resistance, known as the "N" value, is a measure of the relative density of granular soils and is an indication of the consistency of cohesive deposits.

The Following table describes soil consistencies and relative densities based on standard-penetration resistance values (N) determined by the Standard Penetration Test.

	"N"	Consistency
Clay and Silt	0-2 3-4 5-8 9-15 16-30 Over 31	Very Soft Soft Firm Stiff Very Stiff Hard
	"N"	Relative Density
Sand	0-4 5-10 11-19 20-29 30-49 50+	Very Loose Loose Firm Medium Dense Dense Very Dense



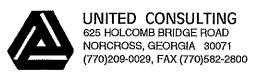
CONTRACTED WITH: CITY OF SUGAR HILL

PROJECT NAME: SUGAR HILL EPICENTER

DATE: 09/10/2014

JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55 LOGGED BY: KN

ELEV.	DESCRIPTION	DEPTH in			SAMPLES			NOTES
	3" TOPSOIL	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w	
	Silt-sandy, trace clay; firm; brown	0	1		2-3-5	14		
	(Fill)				2-3-3	14		•
	0174 4 4 60 4 60 4 60 4 60 4 60 4 60 4 60 4 60 4 60 4 60 -		1					
	Silt-sandy, some mica; very stiff; tan (Residual)	5	2		10-12-12	10		
		5						
	-tan	10	3		6-7-11	18		
	-some sand							
-		15	4		6-7-9	18		No Groundwater encountered at
	BORING TERMINATION AT 15'							the time of drilling
		20						
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		25						
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		30						
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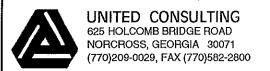
 CONTRACTED WITH: CITY OF SUGAR HILL

 PROJECT NAME: SUGAR HILL EPICENTER
 DATE: 09/10/2014

 JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55
 LOGGED BY: KN

Doucment Control # 3000-2030; Rev:0

	1	DEPTH	Γ		SAMPLES			
ELEV.	DESCRIPTION	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w	NOTES
	3" TOPSOIL .	0						
	Silt-sandy, trace clay; firm; dark		1		2-2-4	18		
	brown (Fill)							-
	-stiff	_	2		4-5-6	13		
		5				,		
			İ					
	-some mica					<u> </u>		
		10	3		5-6-8	18		
	Silt-sandy, some mica; very stiff; tan							,
	(Residual)	15	4		7-10-12	18		ļ
		10						
	The state of the s							
	-trace sand; stiff		5		5-5-7	18		
		20	5		3-3-7	18		
	-							
				ŀ				,
	-very stiff	25	6		7-10-13	12		
		20						
			İ					
	-trace clay; stiff		7		3-5-6	18		
		30			2-3-0	10		
	-very stiff; brown	85	8		4-5-11	18		
		\$5	ľ					Groundwater encountered at
					:			depth 35' at the time of drilling
	Sand-trace silt; firm; light brown		9		5-7-7	18		
	_	40			J-1-1			
L								



Doucment Control # 3000-2030; Rev:0

#### **BORING LOG**

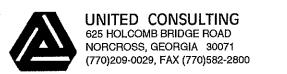
CONTRACTED WITH: CITY OF SUGAR HILL

PROJECT NAME: SUGAR HILL EPICENTER

DATE: 09/10/2014

JOB NO.: KN DRILLER: BILLY/KILMAN RIG: CME 55 LOGGED BY: KN

Γ			DEPTH	<u> </u>		SAMPLES			1
	ELEV.	DESCRIPTION	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w	NOTES
ŀ			FEET	IVO.	TIFE	BLOWS/G	RECOV.	"	<del> </del>
			ļ						l i
١				ļ					
		-some silt and mica; medium dense		<u> </u>					-
		-some sitt and inica, medium dense		10		6-12-14	18		REPARAMENT OF THE PARAMENT OF
			45						·
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·		Partially Weathered Rock sampled	50	11		5-14-50/3	8		
	l	as Sand-some silt and mica; very	50						***************************************
-		dense; white-brown							
1									
1									
							-		
			55	12		50/2	6		
	I		35						
ı	ŀ	ALICED DEFLICAT AT 52							
		AUGER REFUSAL AT 56'							
1									
			60						
	1								
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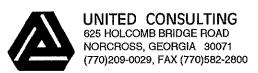
BORING NO.: B-3

 CONTRACTED WITH: CITY OF SUGAR HILL

 PROJECT NAME: SUGAR HILL EPICENTER
 DATE: 09/10/2014

 JOB NO.: 2014.4901.01
 DRILLER: BILLY/KILMAN RIG: CME 55
 LOGGED BY: KN

		DEPTH	Γ		SAMPLES			
LEV.	DESCRIPTION	in FEET		TYPE	BLOWS/6"	RECOV.	W	NOTES
	3" TOPSOIL	0						
Ī	Silt-sandy, trace clay; firm; dark		1		2-3-5	18		
	brown (Fill)		Ľ		2.5.5			
	Silt-sandy, some mica; very stiff;							
	dark brown (Residual)	5	2		11-13-15	18		
		<u></u>						
	*							
	1 1							
	-hard	10	3		14-20-20	18		
		10						
	-trace sand; very stiff; dark tan	15	4		11-12-18	12		
l	BORING TERMINATION AT 15'	15						No Groundwater encountered a
1		-						the time of drilling
ŀ								
		20						
		25						
		30						
		35						
		<u>                                     </u>						
			1					
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Doucment Control # 3000-2030; Rev:0

#### **BORING LOG**

CONTRACTED WITH: CITY OF SUGAR HILL

BORING NO.: \_ B-4

PROJECT NAME: SUGAR HILL EPICENTER

DATE: \_\_\_\_\_09/10/2014

JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55 LOGGED BY: KN

		DEPTH			SAMPLES			NOTEO
ELEV.	DESCRIPTION	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	W	NOTES
	3" TOPSOIL	0						
	Silt-sandy, trace clay and mica and		1		4-7-6	18		
	rock fragments; stiff; brown (Fill)		<u> </u>			<del>                                     </del>		
		5	2		4-6-6	18		
	Sand-silty, some mica and rock		ļ					
	fragments; dense; brown (Residual)	10	3		15-22-27	18		
	-firm		<u> </u>			ļ.,		
		15	4		4-6-7	18		
	BORING TERMINATION AT 15'			İ				No Groundwater encountered at the time of drilling
								the time of drining
		20						
						****		
						***************************************		
		25						
						}		
		30						
			,					
		<u> </u>						
		35						
		40		-				
			L			<u></u>		



CONTRACTED WITH: CITY OF SUGAR HILL

BORING NO.: B-5

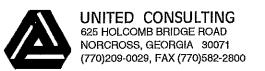
PROJECT NAME: SUGAR HILL EPICENTER

DATE: <u>09/10/2014</u>

JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55

LOGGED BY: KN

D NO	2014.4901.01 DRILLER: BILLY	. / [ ] [ ] [ ]	14 11 1	_ '''		ME 33		_ LOGGED BY:KN
ELEV.	DESCRIPTION	DEPTH			SAMPLES			NOTES
ELEV.		in FEET	NO.	TYPE	BLOWS/6"	RECOV.	W	NOTES
	3" TOPSOIL	0						
	Silt-sandy, some mica, trace clay;		1		5-5-9	12		
	stiff; brown (Fill)		<u> </u>		3-3-9	12		
	, ,		ł					
		ļ	-					
	Sand-some silt; medium dense; tan				0.12.15	4.4		
	(Residual)	5	2		8-12-15	14		
			l					
			1					
			-					
	-dense		3		15-15-15	18		
		10			13-13-13	10		
			1			***		
				<u> </u>				
	-silty; medium dense		4		8-11-13	18		
		15						
			ļ					
								·
I	Silt-sandy, some mica; very stiff; tan		<u> </u>					
1	, ,		5		7-7-10	18		
ŀ	BORING TERMINATION AT 20'	20						No Groundwater at the time of
	BORING TERMINATION AT 20							drilling
						TO STATE OFFI		
		25						
			ł					
		30						
		ļ						
		35						
I		40						
		L	L					



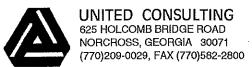
CONTRACTED WITH: CITY OF SUGAR HILL

PROJECT NAME: SUGAR HILL EPICENTER

DATE: 09/10/2014

JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55 LOGGED BY: KN

ELEV.	DESCRIPTION	DEPTH in			SAMPLES	· -	, ,	NOTES
		in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w	
	3" TOPSOIL	0					-	
l	Silt-sandy, trace clay and rock		1		1-2-3	18		
	fragments; dark brown; firm (Fill)							
ļ	Silt-trace sand; very stiff; brown						٠	
	(Residual)	5	2		4-9-9	18		
ŀ	Sand-some mica, trace silt; brown;	ļ						
	dense	<u> </u>	3		13-15-15	18		
		10						
ĺ								
						İ		
	-medium dense		4		12-13-16	18		
		15	4		12"13"10	10		
Ì								
							ν.	
	Silt-sandy; trace mica; very stiff							1
		20	5		10-11-11	18		
						·		
,								
	Anna							
	-tan	05	6		10-15-15	18		
		25						
				1				
-	_							
			_					
	-trace sand and mica; dark tan		7		10-10-11	18		
		30						r.
		$\vdash \vdash \mid$						<i>(</i>
ď								
	-some mica		8		3-8-8	18		
		35	0		7.0.0	10		
		<u> </u>						
1		<u> </u>						
								Groundwater encountered at
	-hard							depth 37' at the time of drilling
		40	9		12-25-24	18		

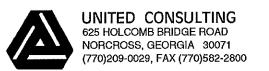


Doucment Control # 3000-2030; Rev:0

#### **BORING LOG**

CONTRACTED	WITH: 0	CITY OF SUGA	AR HILL			BORING NO.	: <u>B-6</u>
PROJECT NAM	E: SUGA	AR HILL EPIC	ENTER			DATE:	09/10/2014
JOB NO.:	KN	_ DRILLER:	BILLY/KILMAN	RIG:	CME 55	LOGGED BY:	KN

ELEV.	DESCRIPTION	DEPTH in	<u></u>	T	SAMPLES		NOTES .	
		in FEET	NO.	TYPE	BLOWS/6"	RECOV.	W	
								,
			10		26-50/5	18		
	Partially Weathered Rock sampled	45	10		20*30/3	10	,	
1	as Silt-some mica, trace sand; hard; gray							
1	gruy							
,	,							
	-sandy		11		50/5	12		
		50	11		30/3	12		
								,
	-some sand		40		50/0	40		
		55	12		50/3	12		
								·
					•			
			<u> </u>					
		60	13		23-50/2	12		
								ı
	-brown							
	·	65	14		33-38-50/6	18		
		-						
		70	15		29-50/4	12		
		1.0						
AUGER REFUSAL AT	AUGER REFUSAL AT 71'							
								;
		75						
		10						
l	-							
		80						
- 1	•							

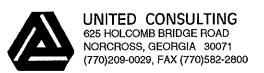


BORING NO.: B-7 CONTRACTED WITH: CITY OF SUGAR HILL 
 PROJECT NAME: SUGAR HILL EPICENTER
 DATE: 09/10/2014

 JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55
 LOGGED BY: KN

ELEV.		I in	┗	SAMPLES			NOTES	
	DESCRIPTION	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	W	NOILO
	3" TOPSOIL	0						
	Silt-sandy, trace clay and rock		1		6-9-7	18		
	fragments; very stiff; brown (Fill)		$\vdash$					
_		<u> </u>						
i.	Silt-sandy, some mica and rock fragments; very stiff; brown	<u> </u>	2		3-9-7	18		
	(Residual)	5	<u> </u>		3-9-7	10		
	(	<u> </u>						
	-stiff		3		3-5-6	18		
		10						
								ļ
		45	4		3-6-6	18		
		15						***
	tunga gandi yawi gtiffi huayin		ļ					
	-trace sand; very stiff; brown	20	5		6-8-12	6		
	AUGER REFUSAL AT 20'							No Groundwater encountered at
								the time of drilling
				:				
		25						
		30						
		35						
		40						

Doucment Control # 3000-2030; Rev:0



Doucment Control # 3000-2030; Rev:0

#### **BORING LOG**

CONTRACTED WITH: CITY OF SUGAR HILL

BORING NO.: B-8

PROJECT NAME: SUGAR HILL EPICENTER

DATE: 09/10/2014 JOB NO.: 2014.4901.01 DRILLER: BILLY/KILMAN RIG: CME 55 LOGGED BY: KN

ELEV.	DESCRIPTION	DEPTH in			SAMPLES	T	NOTES	
			NO.	TYPE	BLOWS/6"	RECOV.	W	
	3" TOPSOIL	0						
	Silt-sandy, trace clay; stiff; dark brown (Fill)		1		4-5-9	9		
	brown (Fin)							
	Silt-sandy, trace clay; very stiff; tan		2		11-11-16	10		
	(Residual)	5			11-11-10	18		
	-tan							
		10	3		8-11-16	18		
	-trace sand; gray							
	, 67	15	4		8-11-15	18		
	-hard					ļ		
	nara	20	5		15-18-23	18		
l	BORING TERMINATION AT 20'	INATION AT 20'						No Groundwater encountered a
								the time of drilling
		25						
		1,0						
		30						
		35						
		- 55						
,								
		40				-		
		40					-	

# **Important Information About Your**

# Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

The following information is provided to help you manage your risks.

#### Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared *solely* for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you —* should apply the report for any purpose or project except the one originally contemplated.

#### **Read the Full Report**

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

#### A Geotechnical Engineering Report Is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you.
- not prepared for your project,
- not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

 the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

#### **Subsurface Conditions Can Change**

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

#### Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

#### A Report's Recommendations Are *Not* Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

subsurface conditions revealed during construction. The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.

### A Geotechnical Engineering Report Is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineering report. Reduce that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

#### Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk*.

#### Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. Be sure contractors have sufficient time to perform additional study. Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

#### **Read Responsibility Provisions Closely**

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

#### **Geoenvironmental Concerns Are Not Covered**

The equipment, techniques, and personnel used to perform a *geoenvironmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else*.

#### **Obtain Professional Assistance To Deal with Mold**

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

## Rely, on Your ASFE-Member Geotechncial Engineer for Additional Assistance

Membership in ASFE/The Best People on Earth exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you ASFE-member geotechnical engineer for more information.



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