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**Addendum No. 1
Technical Memorandum
Remedial Design Sampling Activities**

**Ace Services
Colby, Kansas**

December 21, 2000

Prepared for:
USEPA Region VII

176

Prepared by:
Black & Veatch Special Projects Corp.

EPA Contract No.: 68-W5-0004
EPA Work Assignment Number: 039-RDRD-07GE
BVSPC Project No.: 46118

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SUPERFUND RECORDS

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1.0 Introduction

The U.S. Environmental Protection Agency (USEPA) has initiated remedial design (RD) efforts for groundwater contamination at the Ace Services site near Colby, Kansas. The RD process is the methodology that the Superfund program has established for remediating risks posed by uncontrolled hazardous waste sites. Documents detailing the methodology for preliminary RD activities at the Ace Services site consist of a work plan (WP) (BVSPC, 1999a and 1999f), a field sampling plan (FSP) (BVSPC, 1999b and 2000a), a site management plan (SMP) (BVSPC, 1999e), a quality assurance project plan (QAPP) (BVSPC, 1999c and 2000b), and a health and safety plan (HSP) (BVSPC, 1999d and 2000c).

This Addendum No. 1 to the RD sampling activities technical memorandum presents a description of field activities performed in July, August, and September 2000, as preliminary RD activities at the Ace Services site. It describes the following items:

- Installation and development of groundwater extraction and observation wells.
- Survey of newly installed extraction and observation wells.
- Analytical results of existing groundwater monitoring wells, recovery wells, water supply wells, and residential wells (September 2000).
- Description of the sampling methodologies for the various media.
- Procedures for managing derived wastes.
- Nature and extent of groundwater contamination.
- Pump test results of contaminated aquifer zones.
- Groundwater flow modeling results and extraction well field design.

The previous RD sampling activities technical memorandum (BVSPC, 2000d) presents a description of activities performed in October 1999 (Phase 1) and February 2000 (Phase 2) and should be referred to for supplemental information. Comments provided by EPA and KDHE were incorporated into the document and are included in Appendix J. The previous RD Sampling Activities Technical Memorandum describes the following items:

- Installation, development, and sampling of new groundwater wells.
- Analytical results of existing groundwater monitoring wells, recovery wells, water supply wells, and residential wells (October 1999 and February 2000).
- Descriptions of the sampling methodologies for the various media.
- Procedures for managing derived wastes.
- Evaluation of subsurface soils in historical lagoon area.
- Nature and extent of groundwater contamination.

- Survey of new monitoring wells.

1.1 Site Location and History

The Ace Services site is located near the east edge of Colby, Kansas, at 345 Convesse Street in Thomas County. The geographic coordinates for the site are approximately 100°02'10" West Longitude and 39° 23' 47" North Latitude. The site lies in the southeast quarter of Section 31, Township 7 South, Range 33 West. The facility is next to the Thomas County Mental Health Center and a hardware store. The Thomas County courthouse is approximately 2-1/2 blocks west of the site. The surrounding property is primarily light industrial and commercial, although there are some residential properties within 2 blocks of the site. A railroad right-of-way, aligned north-south, is approximately 1 block west of the site.

Northwest Manufacturing Company operated a chromium plating facility at the site from 1954 to 1969, when Ace Services was formed and began operating an electroplating facility. Ace Services operated the facility until 1989 when it forfeited its corporate status and abandoned the facility.

1.2 Purpose and Scope

The purpose and scope of this report is to describe the results of the preliminary RD investigation activities and describe revised proposed activities based on the results.

2.0 Investigation Objectives

The objective of the preliminary RD sampling efforts was to complete characterization of the chromium groundwater plume and complete characterization of aquifer characteristics. The data acquired during the preliminary RD activities will be used for design of groundwater remediation systems. The scope of the preliminary RD activities included:

- Installing and sampling new monitoring wells.
- Sampling existing monitoring wells.
- Sampling existing recovery and water supply wells.
- Sampling residential wells.
- Installing groundwater extraction and observation wells.
- Evaluation of subsurface soils in historical lagoon area.
- Survey of newly installed groundwater monitoring wells.
- Performing pumping tests of contaminated aquifer zones and measuring groundwater levels.
- Collecting subsurface soil samples for geotechnical evaluation.
- Performing a ground survey to develop a base map for design drawings.

The objectives identified above have been completed at the time of this memorandum except for the objectives listed below:

- Installing and sampling monitoring wells.
- Collecting subsurface soil samples for geotechnical evaluation.
- Performing a ground survey to develop a base map for design drawings.

Two additional groundwater monitoring well nests consisting of shallow and intermediate depth wells are to be installed south of the railroad tracks near monitoring well nests MW-11 and MW-12. Final locations of the wells will be controlled by property access restrictions and technical adequacy.

Additional subsurface soil samples may need to be collected and evaluated for geotechnical properties. The existing onsite machine shop is to be used to house the treatment system, therefore, a separate building will not be constructed. However, geotechnical information concerning the site may be needed for other structures.

The ground survey for the base map will be performed after property access has been granted by all required property owners. The base map will be provided under separate cover.

3.0 Investigation Activities

Field investigation activities for the preliminary RD efforts are discussed in this section. The following subtasks are discussed:

- Well Installation.
- Groundwater Sampling Locations and Analyses.
- Groundwater Sampling Procedures.
- Decontamination Procedures.
- Treatability Study Groundwater Sampling.
- Aquifer Pump Test.
- Numerical Computer Modeling of Groundwater Flow.

A site map illustrating the locations of all wells is presented as Figure 3-1. Final well locations were agreed to by EPA, KDHE, and the City of Colby.

The RD investigation activities discussed in this memorandum were conducted in July, August, and September 2000. Well nests EX-2, OB-1, and OB-2 were installed and developed during July 10, 2000 to July 19, 2000. Pump tests for the shallow, intermediate, and deep aquifer zones were conducted from July 31, 2000 to August 10, 2000. Groundwater sampling activities were conducted from September 18, 2000 to September 22, 2000.

3.1 Well Installation

The groundwater well construction details are described in this section. The drilling and well installation was conducted by Woofter Pump and Well, Inc., of Hoxie, Kansas, a drilling subcontractor licensed in the State of Kansas. The wells installed as part of the Phase 2 remedial design sampling activities are listed in Table 3-1. At all times during the progress of the work, precautions were used to prevent tampering with the well or the entrance of foreign material into the well. Runoff was prevented from entering the well during construction. The completed wells have a sanitary seal to prevent material from entering the wells.

Table 3-1
Wells Installed as part of the Phase 3 Remedial Design Sampling Activities
Ace Services Site
Remedial Design

Well Number

OB-1-S

OB-1-I

OB-1-D

OB-2-S

OB-2-I

OB-2-D

EX-2-S

EX-2-I

EX-2-D

Note: EX = Extraction Well
OB = Observation Well
S = Shallow
I = Intermediate
D = Deep

3.1.1 Observation Wells

Observation wells installed for the preliminary RD efforts are listed in Table 3-1. The observation wells were constructed using 4 inch diameter, polyvinyl chloride (PVC) riser pipe and screen. The riser pipe was Schedule 40 PVC. The well screens were 20-foot-long, Schedule 40 PVC with 0.020-inch slots.

Observation wells were installed in a nested fashion and consist of three wells at various depths to respectively evaluate shallow (110 to 130 feet), intermediate (172 to 195 foot) and deep (215 to 235 feet) aquifer zones. The water table ranged in depth from approximately 108 to 113 feet below ground surface (bgs) and impermeable shale bedrock (Pierre Shale Formation) was encountered at approximately 235 feet bgs.

A test hole for each well nest was drilled from the ground surface to bedrock and logged by the onsite geologist. The lithologic information was used to select the specific screen depth for each water bearing zone and monitoring well. Screen lengths for the wells were field determined and each well was installed within the selected water bearing zone at each well nest location.

Wells within the well nest were installed so that the shallow well is upgradient of the intermediate well and the intermediate well is upgradient of the deep well. Individual wells were installed approximately 15 feet apart.

The annular space around well screens was backfilled with a silica sand filter pack that conformed to screen gradation analysis requirements of not less than 95 percent of the sand passing US Standard Sieve No. 10 and not more than 5 percent passing US Standard Sieve No. 20. The filter pack extended from the bottom of the borehole to a minimum of 3 feet above the top of the screen. The annular space above the filter pack was backfilled with a minimum of 5 feet of bentonite chips. The annular space above the bentonite chips to the surface was backfilled with cement/bentonite grout tremied into place. A locking above ground or, where required, flush mount cover was installed to secure the well head.

3.1.2 Extraction Wells

Extraction wells installed for the preliminary RD efforts are listed in Table 3-1. Extraction well EX-2-S was constructed using 6 inch diameter PVC riser pipe and screen. Extraction wells EX-2-I and EX-2-D were constructed using 8 inch diameter PVC riser pipe and screen. The riser pipe was Schedule 40 PVC. The well screen was constructed of Schedule 40 PVC with 0.032-inch slots.

Extraction wells were installed in a nested fashion and consist of a maximum of three wells at various depths to respectively extract contaminated groundwater at shallow (100 to 130 feet), intermediate (145 to 190 foot) and deep (195 to 235 feet) aquifer zones. Results from the plume characterization study were used to determine which aquifer zones are contaminated.

A test hole for the well nest was drilled first and logged by the onsite geologist. The boring log information was used to select the specific screen depth for each extraction well. Screen length for the wells was field determined and installed within the selected water bearing zone at each extraction well location.

Wells within the well nest were installed with the shallow well upgradient of the intermediate well and the intermediate well, upgradient of the deep well. Individual wells were installed approximately 15 feet apart. A detailed location map for observation well nests OB-1 and OB-2 and extraction well nest EX-2 is presented in Figure 3-2.

The annular space around the screen was backfilled with No. 1 Fine Washed Silica Sand filter pack. The filter pack extended from the bottom of the borehole to a minimum of 3 feet above the top of the screen. The annular space above the filter pack was backfilled with a minimum of 5 feet of bentonite chips. Remaining annular space about the bentonite seal was backfilled to the ground surface with bentonite grout. A locking flush mount cover was installed to secure the well head.

3.1.3 Boring Logs and Well Construction Logs

Boring logs and well construction logs for wells listed in Table 3-1 are provided in Appendix A and Appendix B, respectively.

3.1.4 Well Development

Well development consisted of surging and pumping the well using an electric submersible pump. The temperature, pH, specific conductivity, turbidity, dissolved oxygen (DO), and oxidation reduction potential (ORP) was monitored during pumping. Well development data was recorded in the field data sheets (Appendix C). Pumping continued until the field parameters stabilized and the water was clear and free of fines.

In all cases, care was taken not to collapse well screens during development activities, and at least half as much water as was introduced during drilling was removed during development and construction of each well. Development fluids (fluids recovered from the wells during development) were collected and managed as described in Section 4.0.

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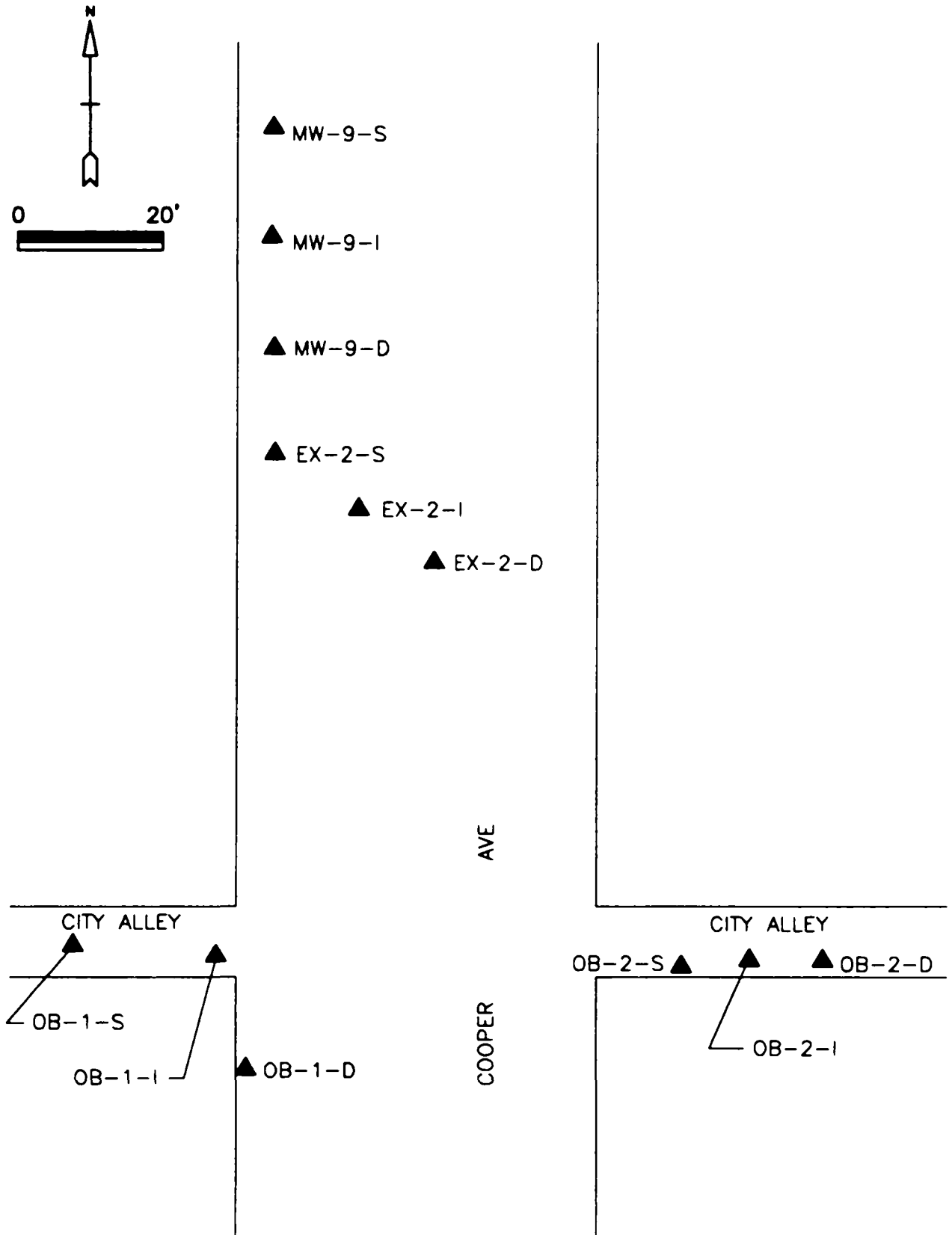


FIGURE 3-2
WELL LOCATIONS FOR
MW-9, EX-2, OB-1
AND OB-2
ACE SERVICES SITE

3.2 Sampling Locations and Analyses

The scope of the preliminary RD investigation included groundwater sampling and analysis for newly installed wells (Table 3-1) and currently existing wells (Table 3-2). The locations of the wells are shown on Figure 3-1. Groundwater samples were analyzed for total chromium (Cr). Samples from wells representative of extracted groundwater were analyzed for total chromium and hexavalent chromium. Groundwater samples were collected separately for treatability study purposes from wells EX-2-S, EX-2-I, EX-2-D, RW-6, and a composite sample from several monitoring wells. The treatability study samples were analyzed for several wet chemistry and metals parameters. Results of the samples will be discussed in the treatability study report. All samples were unfiltered.

Analytical parameters, analytical methods, sample container requirements, preservation methods, and holding times are summarized by sample media in Table 3-3. The total number of samples collected during the investigation including duplicates, blanks, and other quality control samples are summarized by sample media in Table 3-4.

3.3 Groundwater and Soil Sampling Procedures

The following general procedures were practiced when sampling:

- A clean pair of new, disposable surgical gloves were worn each time a sample was collected and equipment was decontaminated or replaced with new material between each sample.
- During the course of the field investigation, all samples were properly documented, as described in the FSP (BVSPC, 1999b), FSP Addendum (BVSPC, 2000a), QAPP (BVSPC, 1999c), and QAPP Addendum (BVSPC, 2000b). Documentation included completion of chain of custody (COC) forms, field logbook documentation, and sample labels for sample containers.
- Samples were immediately sealed, kept out of the sun, and kept cool by ice after collection.
- All samples for hexavalent chromium analysis were shipped "Next Day Air-Early A.M." by UPS for 7:30 A.M. delivery to meet the 24 hour holding time.

3.3.1 Water Level Measurement

Water levels for existing wells were measured prior to any intrusive work. The water level, time of measurement, and date were recorded.

Table 3-2
Existing Wells Sampled as part of the Remedial Design (September 2000)
Ace Services Site
Remedial Design

Well Number	Well Number
MW-1-S	MW-9-D
MW-1-I	MW-10-P
MW-1-D	MW-11-S
MW-2-S	MW-11-I
MW-2-I	MW-11-D
MW-2-D	MW-12-S
MW-3-D	MW-12-I
MW-4-S	MW-12-D
MW-4-I	Ace Recovery Well-S (ACE-R-S)
MW-4-D	Ace Recovery Well-I (ACE-R-I)
MW-5-S	Ace Recovery Well-D (ACE-R-D)
MW-5-I	PWS #8
MW-5-D	RW-1
MW-6-S	RW-2
MW-6-I	RW-3
MW-6-D	RW-4
MW-7-S	RW-5
MW-7-I	RW-6
MW-7-D	RW-8
MW-8-S	RW-9
MW-8-I	HPMW-6-S
MW-8-D	HPMW-9-S
MW-9-S	Ion Exchange Treatability Study Samples
MW-9-I	
Notes MW = Monitoring Well PWS = Public Water Supply RW = Residential Well P = Perched HPMW = Hi-Plains Coop Monitoring Well S = Shallow I = Intermediate D = Deep	

Table 3-3
 Analytical Parameters and Methods,
 Containers, Preservatives, and Holding Times
 Ace Services Site
 Remedial Design

Parameter	Method ¹		Container Requirements	Preservative	Holding Time	
	Extraction	Analysis			Extraction	Analysis
Water						
Cr. total	--	6010	120 ml Poly	HNO ₃ , 4°C	6 months	6 months
Cr VI	--	7196A	120 ml Poly	4°C	24 hours	24 hours
Soil						
Cr. total	3050	6010	2 oz glass jar	4°C	6 months	6 months
Note 1 - Level III data packages						

Table 3-4
 Sample Summary
 Ace Services Site
 Remedial Design

Parameter	Number of Primary Samples	Number of Duplicates	Number of Rinsates	Number of Matrix Spikes ¹	Number of Matrix Spike Duplicates ¹	Total Number of Samples
<u>Water</u>						
Cr, total	54	6	4	[3]	[3]	64
Cr VI	11	1	1	[1]	[1]	13
<u>Soil</u>						
Cr, total	3	0	0	0	0	3
Note 1: MS/MSD samples are additional volume only.						

3.3.2 Well Purging/Development and Groundwater Sample Collection

Before sampling, the depth to water was measured and recorded. Using information from the well construction logs, the total volume of water in the well casing was determined. The subcontractor (Woofter Pump and Well, Inc., Hoxie, Kansas) purged the wells prior to collecting groundwater samples. The monitoring wells and the Ace Recovery Well were purged and sampled using a submersible pump and Public Water Supply Well No. 8 was sampled using its dedicated turbine pump. A water truck was used to store and transport the purge water so it could be discharged to the City of Colby's sanitary sewer system.

In addition to the collection of primary samples, quality assurance/quality control (QA/QC) samples such as equipment rinsate blanks, duplicate samples, and matrix spike (MS), and matrix spike duplicate (MSD) samples were collected.

Monitoring well purging/development data sheets were completed for each well that was developed or sampled and are provided in Appendix C.

3.3.2.1 Existing Monitoring Well Purging and Sample Collection. Most of the existing monitoring wells were purged using a high capacity (~15 gpm) submersible pump.

The remaining existing monitoring wells and the three screened intervals of the Ace Recovery Well were micropurged. The wells were micropurged at a rate less than the recharge rate of the well. The water level in the well was monitored for drawdown during micropurging. Micropurging was performed at a rate so that minimal drawdown occurred. Micropurging was performed at approximately one liter per minute (0.26 gallons per minute). The wells were micropurged from the midpoint of the screened intervals.

Field parameters (temperature, pH, specific conductivity, ORP, turbidity, and DO) were measured and recorded during both purging processes. Measurements were recorded periodically until stabilization occurred at which time purging was complete and the sample collected.

3.3.2.2 Public Supply Well No. 8 Purging and Sample Collection

The subcontractor (Woofter Pump and Well, Inc.) purged the well prior to collecting groundwater samples. The public water supply well was sampled using its dedicated turbine pump. Field parameters (temperature, pH, specific conductivity, ORP, DO, and turbidity) were measured and recorded during the purging process.

3.3.2.3 Residential Well Purging and Sample Collection. The residential wells sampled during the groundwater sampling activity are listed in Table 3-2. Addresses for the residential wells are provided on Table 3-5. The residential wells are equipped with dedicated pumps. The samples were collected from an outside tap prior to any water treatment system. Purging and sample collection procedure for the residential wells was as follows:

- (1) The tap was opened and allowed to flow prior to sample collection. The field parameters (temperature, pH, specific conductivity, ORP, turbidity, and DO) were measured periodically. Purging was considered complete when the field parameters stabilized.
- (2) Following the purging procedure, the flow from the tap was reduced for sample collection in order to minimize agitation and aeration.
- (3) The sampler donned a clean pair of surgical gloves.
- (4) At the end of the purging interval, the sample containers were filled directly from the tap.
- (5) Following sample collection, sample documentation (i.e., sample number, chain-of-custody record) was completed and noted in the field logbook.
- (6) The samples were placed in a cooler on ice.

3.3.3 Subsurface Soil Sampling

Soil samples were collected from drill cuttings for IDW characterization as discussed in Section 4.0. The samples were analyzed for total chromium.

3.3.4 Equipment Rinsate Blanks

Rinsate blanks were used to measure the effectiveness of pump decontamination procedures. Equipment rinsate blanks were prepared from the submersible pumps after the pumps had been decontaminated. The rinsate blanks were identified with a sample identification number. The rinsate blank number, time, and date of collection was documented in the field logbook.

3.3.5 Duplicate Samples

The purpose of duplicate samples is to assess laboratory QA/QC. Duplicate samples were collected in the field by alternately filling appropriate sample containers for the primary

Table 3-5
Residential Well Sample Codes
Ace Services Site
Remedial Design

Code	Residential Well Description
RW-1	175 Thompson
RW-2	1655 E. 4th
RW-3	1765 E. 4th
RW-4	1795 E. 4th
RW-5	1680 E. 4th
RW-6	1940 E. 4th
RW-7	2040 E. 4th
RW-8	1888 County Road 21
RW-9	2580 E. 4th

and duplicate samples. The primary sample and the duplicate samples were placed in identical containers, preserved in the same manner, and submitted for the same analyses. The duplicate groundwater samples were identified with a sample identification number. The sample location, number, and date and time of collection was documented in the field logbook.

3.3.6 Matrix Spike/Matrix Spike Duplicates

The purpose of MS/MSD samples is to evaluate effects of the sample matrix on the accuracy of the analysis. MS/MSD samples were collected in the field by alternately filling appropriate sample containers for the primary, MS, and MSD sample from the discharge hose of the pump. The primary sample, the MS sample, and the MSD samples were placed in identical containers, preserved in the same manner, and submitted for the same analyses. The MS/MSD samples were identified with a sample identification number. The sample location, number, and date and time of collection was documented in the field logbook.

3.4 Sample Numbering System

A sample numbering system was used to identify each sample submitted for chemical analysis. The purpose of the numbering system was to provide a tracking system for retrieval of information on each sample. The sample identification numbers allocated for all sampling efforts were used on sample labels, chain-of-custody records, and all other applicable documentation used during the sampling activity. A listing of all sample identification numbers was maintained in the field logbook by the field team representative.

Sample identification numbers consist of four components: a media code, a well code, the date, and the sample characteristic code. The following is an example of a completely numbered sample, with each component identified:

W-MW-1-S-091900-P.

where

W = water

MW = well type code (i.e., monitoring well),

1 = well number code

S = well interval code (shallow)

091900 = sample date code (month, day, and year sample was collected), and

P = sample characteristic code (i.e., primary).

The media codes consist of W for water or S for subsurface soil. The well type code identifies the well type: MW for monitoring well, PWS for public water supply, RW for residential well, ACE for Ace recovery well, EX for extraction wells, OB for observation wells, and HPMW for HI-Plains Coop monitoring wells. The well number code identifies the well number. The well interval code identifies the aquifer zone monitored: P for perched, S for shallow, I for intermediate, and D for deep. The sample date code identifies the data the sample was collected: 091900 is September 19, 2000. The sample characteristic code indicates whether the sample is a primary sample (P), an equipment rinsate blank (R), duplicate (D), a matrix spike (MS), or a matrix spike duplicate (MSD) sample.

3.5 Documentation

Documentation was a vital aspect of the site investigation. This section discusses pertinent documentation activities.

3.5.1 Field Logbook

Bound field logbooks were maintained by the sampling team to provide a detailed record of significant events, observations, and measurements taken during the field investigation. The field log books are intended to provide sufficient data and observations to enable the field team to reconstruct events that occurred during the project. Copies of the field logbooks kept by field personnel are presented in Appendix D.

3.5.2 Sample Labels

An adhesive sample label was placed on each sample container submitted for chemical analysis. The following information was included on each sample label:

- Site name.
- Sample number.
- Name of sampler.
- Sample collection date and time.
- Analysis requested and preservatives added.

3.5.3 Chain-of-Custody Record

Chain-of-custody procedures were employed to maintain and document continuous sample possession. A sample was considered under a person's custody if it was in that

person's physical possession, within visual sight of that person after taking physical possession, secured by that person so that the sample could not be tampered with, or secured by that person in an area that was restricted from unauthorized personnel.

A chain-of-custody record was completed for each sample shipment. Standard laboratory chain-of-custody records were used. After completion of the chain-of-custody-record, one carbonless copy of the chain-of-custody record was retained by the field crew and the remaining copies and the original were enclosed in a sealable plastic bag and secured to the inside of the shipping container lid. A separate chain-of-custody record was completed for each shipping container. Shipping containers were secured, and custody seals were placed across the container openings. The chain-of-custody record was sealed inside the shipping container, and the custody seals remained intact; therefore, the commercial carrier was not required to sign the chain-of-custody record. Copies of the chain-of-custody records are included in Appendix E.

3.5.4 Custody Seals

Custody seals were used to ensure the integrity of the samples when they remained unattended or when they were relinquished to the delivery service until they were opened by the laboratory. All samples were shipped in an insulated shipping container, and each shipping container was sealed with at least two custody seals. The seals were affixed to each shipping container so that it was necessary to break the seals to open the shipping container.

3.5.5 Airbills

An airbill was completed for each sample shipment. Priority 7:30 a.m. overnight delivery was used for samples collected in the morning and late morning delivery was used for samples collected in the afternoon to achieve the analytical holding time (24 hours) for hexavalent chromium analysis. Copies of the completed airbills are included in Appendix F.

3.6 Decontamination Procedures

Procedures for equipment decontamination were implemented to avoid cross-contamination of subsurface strata and samples of various media that are to be submitted for chemical analysis. Sampling equipment was thoroughly cleaned and decontaminated before initial use and between sample locations.

3.6.1 Initial Decontamination

Initial decontamination of the drill rig, sampling equipment, and electric pump before any wells were purged and sampled included the following:

- (1) Steam clean with potable water.
- (2) Circulate and rinse pump with potable water.
- (3) Rinse pump with distilled water.

Initial decontamination of the split-spoon sampler includedalconox wash followed by potable and distilled water rinses.

3.6.2 Intermediate Decontamination

Intermediate decontamination of the sampling equipment was required between sampling attempts. The intermediate decontamination procedures for sampling equipment was the same as those outlined in the initial decontamination.

3.6.3 Final Decontamination

Final decontamination was performed on all equipment used to drill, purge, or sample wells. The procedures used during initial decontamination were utilized during final contamination.

3.7 Site Survey Data

A location survey was conducted by Zerr Engineering of Colby, Kansas, as part of the preliminary RD investigation. Items surveyed included newly installed monitoring wells. At monitoring well locations, top of casing (TOC) elevations were measured to the closest 0.01 foot using the notched reference point for monitoring wells. Ground elevations were measured to the closest 0.01 foot. Location coordinates were also determined for the wells and are referenced to the State Plane Coordinate System. Elevations are referenced to mean sea level (msl), specifically to the National Geodetic Vertical Datum of 1929. Survey data for the wells are presented in Appendix G.

A survey of the site will be performed after all wells are installed and the site area is defined. A site map will be developed from the survey data. The site map will include locations of the wells, utilities, cultural features, and topography which will be used as a base map for engineering drawings.

3.8 Data Validation

Samples collected in October 1999 and February 2000 were sent to Analytical Management Laboratories, Inc. of Olathe, Kansas, for analyses. Once samples were received at the lab, the specified analyses were performed, and results in the form of raw laboratory data were generated. Data validation and evaluation was then performed on the raw laboratory data in accordance with EPA Contract Laboratory Program (CLP) National Functional Guidelines by Heartland Environmental Services, Inc. of St. Charles, Missouri.

Samples collected in September 2000 were sent to Southwest Laboratories of Oklahoma in Broken Arrow, Oklahoma. Once samples were received at the lab, the specified analyses were performed, and results in the form of raw laboratory data were generated. Data validation and evaluation was then performed on the raw laboratory data in accordance with EPA Contract Laboratory Program (CLP) National Functional Guidelines by Validata Chemical Services, Inc. of Lilburn, Georgia.

The objective of the data validation was to review analytical laboratory procedures and QC results to evaluate whether the data met project data quality objectives (DQOs) established in the site specific QAPP (BVSPC, 1999c and 2000b).

Results of the laboratory data assessment for the samples collected in October 1999 and February 2000 are presented in the *Data Validation Report* dated January 10, 2000 and April 20, 2000 (BVSPC, 2000e and 2000f) and the *PARCC's Report and Data Evaluation Technical Memorandum* dated June 28, 2000 (BVSPC, 2000g).

Results of the laboratory data assessment for the samples collected in September 2000 are presented in the *Data Validation Report* dated December 12, 2000 (BVSPC 2000h) and the *PARCC's Report and Data Evaluation Technical Memorandum* dated December 18, 2000 (BVSPC 2000i).

Results of the data validation and evaluation process have determined the data are defensible, were collected in accordance with the site specific QAPP and FSP, and are useable for the intended purposes.

3.9 Aquifer Pump Test

An objective of the preliminary RD efforts was to perform pump tests within the three aquifer zones. Hydrogeologic data for the pump tests were used to develop a computer flow model of groundwater flow of the site. The model results were used to estimate the number, location, and extraction rates necessary to achieve remedial action objectives.

Three pump tests were performed in July and August 2000, and evaluated in September 2000. Pump test procedures and results are discussed in the *Pump Test Results Ace Services Site Memorandum*, November 13, 2000, which is presented in Appendix H.

3.10 Groundwater Modeling

An objective of the preliminary RD efforts was to develop a numerical computer model of groundwater flow of the site. The model results were used to estimate the number, location, and extraction rates necessary to achieve remedial action objectives.

Numerical computer modeling efforts of groundwater flow of the site was performed in October and November 2000. Modeling procedures and results are discussed in the *Groundwater Modeling Activities Ace Services Site Memorandum*, December 14, 2000, which is presented in Appendix I.

4.0 Investigation Derived Waste

Investigation derived wastes (IDW) included decontamination fluids, groundwater removed from monitoring wells, drill cuttings, fluids, plastic sheeting, and personal protective equipment.

4.1 Liquids

Purging fluids, development water, and decontamination solution and rinses were collected and stored in a water tank. The fluids were then transported and discharged into the City of Colby's sanitary sewer system.

4.2 Personal Protective Equipment

All personal protective equipment (PPE) such as surgical gloves, paper towels, plastic sheeting, etc., was double bagged and disposed of as solid waste.

4.3 Drill Cuttings

Drill cuttings were placed in containment structures for characterization prior to disposal. Care was taken to exclude or remove any free liquid. A composite drill-cuttings sample was collected from the cuttings of each well nest and analyzed for total chromium for hazardous waste determination purposes. Results of the soil cuttings analyses are summarized in Table 4-1.

Analytical results determined the cuttings to be non-hazardous (i.e., less than 100 mg/kg total chromium). Once results indicated the soils were non-hazardous, the soil cuttings were spread to the ground per agreement with KDHE Bureau of Waste Management-Solid Waste Section.

Table 4-1
IDW Analytical Results
Ace Services Site
Remedial Design

Well Nest No.	Sample No.	Total Cr (mg/kg)
OB-1	S-IDW-OB-1-071300	2.4
OB-2	S-IDW-OB-2-071400	3.7
EX-2	S-IDW-EX-2-071200	3.2

5.0 Remedial Design Investigation Results

This section presents, evaluates, and interprets data collected during the preliminary RD efforts performed from July 2000 to September 2000.

5.1 Water Level Data

The Ogallala Formation is an unconfined aquifer in the Colby area. The Ogallala aquifer is the sole source of potable water for the City of Colby.

Water level data for the monitoring wells are presented in Tables 5-1 and 5-2. The groundwater elevations were determined using location survey data and water level data collected during previous RI and RD investigation activities. The predominant groundwater flow direction for September 22, 2000, for the shallow, intermediate, and deep zones is illustrated on Figures 5-1 through 5-3 respectively. Depth to groundwater in the site area is approximately 100 to 120 feet bgs. Plots of the groundwater elevation data on site maps indicate the groundwater flow direction in the three zones in the site area is predominantly to the east-southeast. Detailed hydrogeologic data are presented in Appendices H and I.

5.2 Geochemical and Biochemical Groundwater Data

Basic water quality parameters were analyzed or measured on groundwater samples to evaluate the geochemical and biochemical quality of the groundwater. The geochemical and biochemical data will be used in the design of the groundwater treatment process. Results of field parameters are presented in Table 5-3. Analytical results of samples collected specifically for design criteria will be discussed in the Treatability Study Report which will be prepared as part of the RD efforts.

5.3 Nature and Extent of Groundwater Contamination

The nature and extent of contamination in groundwater at the site was evaluated from 54 primary groundwater samples. A list of the wells sampled and the analytical results are presented in Table 5-3. Results for the duplicate samples are also included.

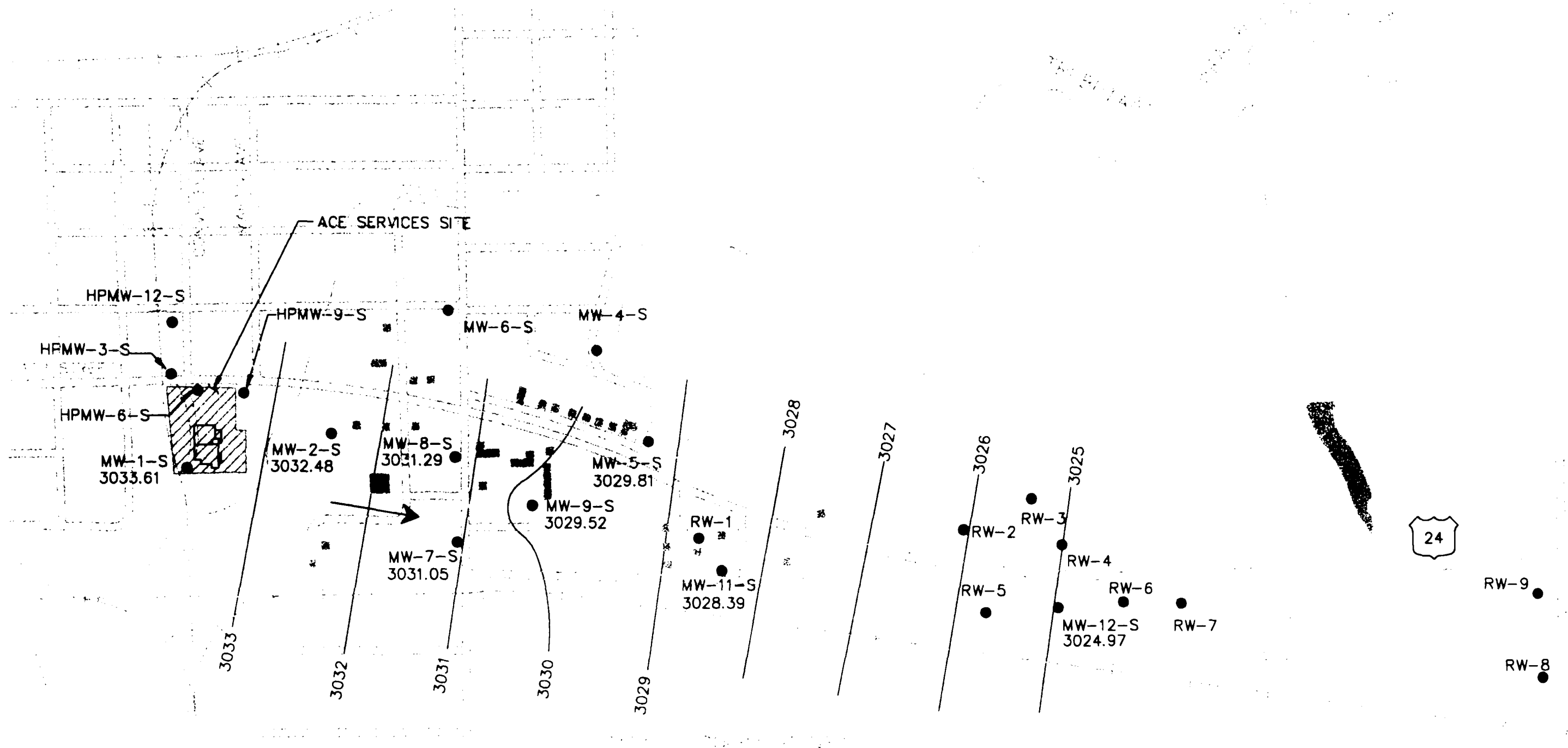
Table 5-1
Groundwater Elevation Data
September 18-22, 2000
Ace Services Site
Remedial Design

Well	Top of Casing Elevation (ft)	Depth to Water from Top of Casing (ft)	Groundwater Elevation (ft MSL)
MW-1-S	3140 53	107 00	3033 53
MW-2-S	3134 99	102 49	3032 5
MW-4-S	3126 62	96 02	3030 6
MW-5-S	3130 57	100 59	3029 98
MW-6-S	3136 55	104 73	3031 82
MW-7-S	3147 87	116 85	3031 02
MW-8-S	3139 57	108 28	3031 29
MW-9-S	3142 47	111 98	3030 49
MW-11-S	3148 20	119 66	3028 54
MW-12-S	3168 21	143 07	3025 14
HPMW-3-S	3138 65	105 01	3033 64
HPMW-6-S	3139 23	105 41	3033 82
HPMW-9-S	3136 61	103 37	3033 24
HPMW-12-S	3136 03	102 41	3033 62
OB-1-S	3142 71	112 08	3030 63
OB-2-S	3139 59	109 30	3030 29
EX-2-S	3142 13	111 67	3030 46
MW-1-I	3140 56	107 07	3033 49
MW-2-I	3134 90	102 80	3032 1
MW-4-I	3126 98	96 50	3030 48
MW-5-I	3130 44	100 56	3029 88
MW-6-I	3136 64	105 00	3031 64
MW-7-I	3147 70	116 65	3031 05
MW-8-I	3139 00	107 75	3031 25
MW-9-I	3142 35	111 79	3030 56
MW-11-I	3148 60	120 05	3028 55
MW-12-I	3168 29	143 42	3024 87
OB-1-I	3142 31	112 17	3030 14
OB-2-I	3138 63	108 15	3030 48
EX-2-I	3141 30	110 89	3030 41
MW-1-D	3140 10	106 56	3033 54
MW-2-D	3136 56	105 31	3031 25
MW-3-D	3137 00	104 91	3032 09
MW-4-D	3127 18	98 68	3028 5
MW-5-D	3131 07	103 20	3027 87
MW-6-D	3136 83	106 17	3030 66
MW-7-D	3147 49	117 71	3029 78
MW-8-D	3138 66	107 76	3030 9
MW-9-D	3142 13	113 32	3028 81
MW-11-D	3149 08	122 37	3026 71
MW-12-D	3168 10	144 87	3023 23
OB-1-D	3141 98	113 22	3028 76
OB-2-D	3138 11	109 56	3028 55
EX-2-D	3140 50	111 54	3028 96
MW-10-P	3123 37	dry	dry

Table 5-2
Groundwater Elevation Data
September 22, 2000
Ace Services Site
Remedial Design

Well	Top of Casing Elevation (ft)	Depth to Water from Top of Casing (ft)	Groundwater Elevation (ft MSL)
MW-1-S	3140.53	106.92	3033.61
MW-2-S	3134.99	102.51	3032.48
MW-4-S	3126.62	NA	NA
MW-5-S	3130.57	100.76	3029.81
MW-6-S	3136.55	NA	NA
MW-7-S	3147.87	116.82	3031.05
MW-8-S	3139.57	108.28	3031.29
MW-9-S	3142.47	112.95	3029.52
MW-11-S	3148.20	119.81	3028.39
MW-12-S	3168.21	143.24	3024.97
HPMW-3-S	3138.65	NA	NA
HPMW-6-S	3139.23	NA	NA
HPMW-9-S	3136.61	NA	NA
HPMW-12-S	3136.03	NA	NA
MW-1-I	3140.56	106.98	3033.58
MW-2-I	3134.90	102.78	3032.12
MW-4-I	3126.98	NA	NA
MW-5-I	3130.44	100.65	3029.79
MW-6-I	3136.64	NA	NA
MW-7-I	3147.70	116.66	3031.04
MW-8-I	3139.00	107.80	3031.2
MW-9-I	3142.35	111.81	3030.54
MW-11-I	3148.60	120.16	3028.44
MW-12-I	3168.29	143.57	3024.72
MW-1-D	3140.10	106.49	3033.61
MW-2-D	3136.56	104.99	3031.57
MW-3-D	3137.00	NA	NA
MW-4-D	3127.18	NA	NA
MW-5-D	3131.07	103.28	3027.79
MW-6-D	3136.83	NA	NA
MW-7-D	3147.49	117.67	3029.82
MW-8-D	3138.66	107.89	3030.77
MW-9-D	3142.13	113.29	3028.84
MW-11-D	3149.08	122.49	3026.59
MW-12-D	3168.10	144.65	3023.45
MW-10-P	3123.37	NA	NA

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LEGEND

- MW-1-S 3025.60 EXISTING WELL LOCATION WITH IDENTIFICATION AND GROUNDWATER ELEVATION (MSL) (09-22-00)
- 3032 GROUNDWATER ELEVATION CONTOUR (MSL)
- PREDOMINANT GROUNDWATER FLOW DIRECTION

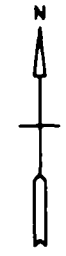
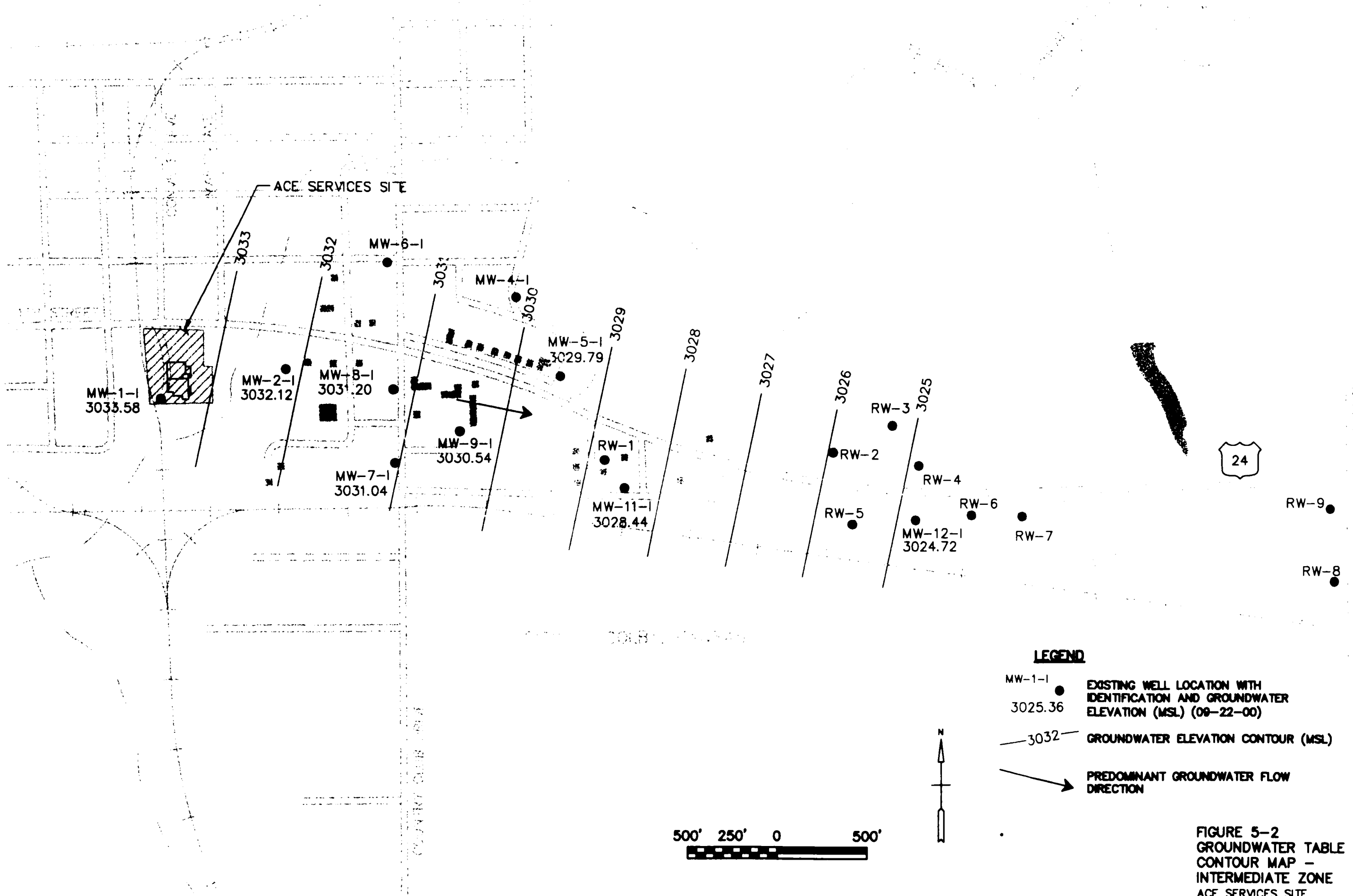


FIGURE 5-1
GROUNDWATER TABLE
CONTOUR MAP -
SHALLOW ZONE
ACE SERVICES SITE

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LEGEND

- MW-1-1 ● EXISTING WELL LOCATION WITH IDENTIFICATION AND GROUNDWATER ELEVATION (MSL) (09-22-00)
- 3032 — GROUNDWATER ELEVATION CONTOUR (MSL)
- PREDOMINANT GROUNDWATER FLOW DIRECTION

FIGURE 5-2
GROUNDWATER TABLE
CONTOUR MAP -
INTERMEDIATE ZONE
ACE SERVICES SITE

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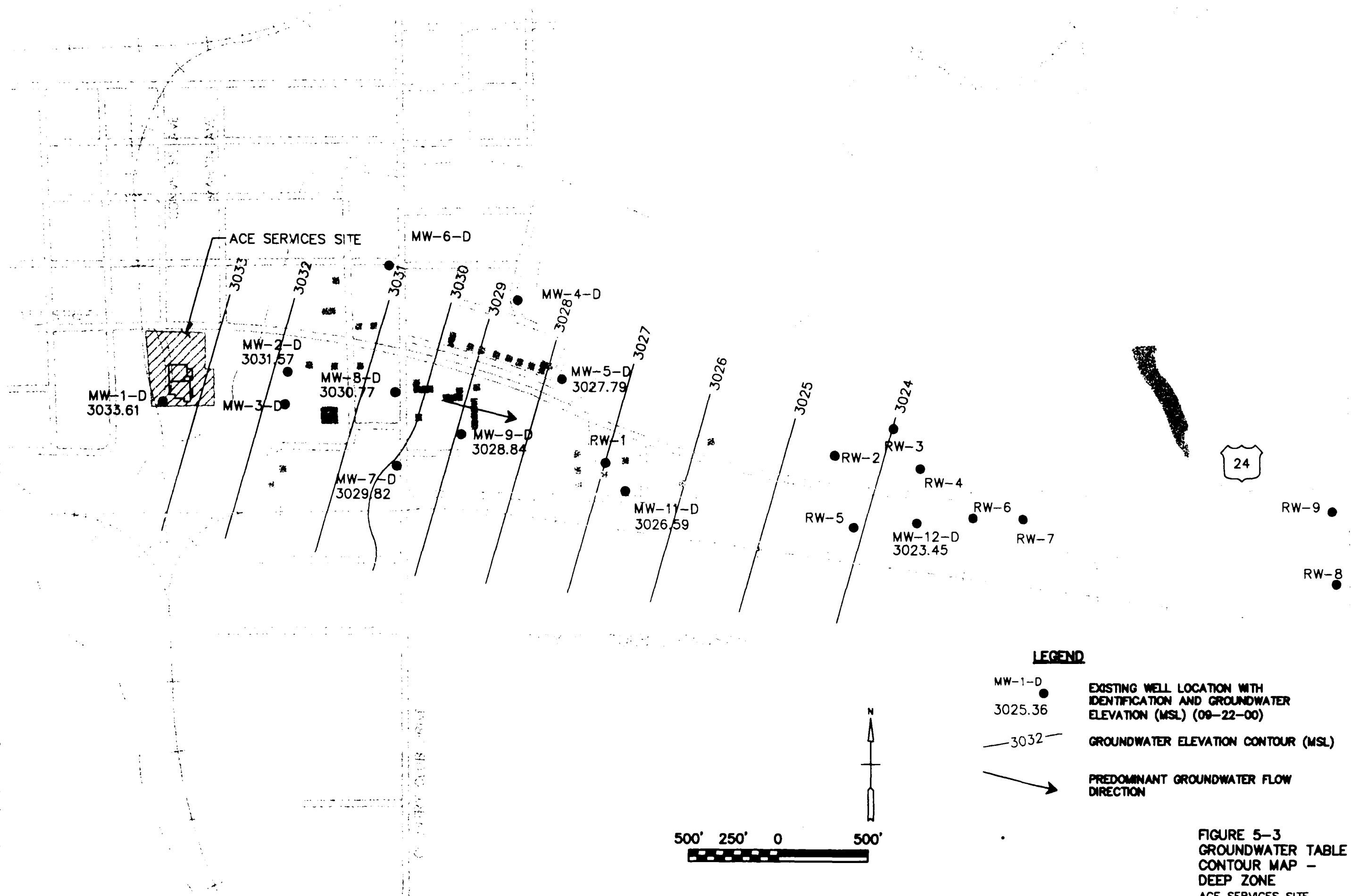


FIGURE 5-3
 GROUNDWATER TABLE
 CONTOUR MAP -
 DEEP ZONE
 ACE SERVICES SITE

Table 5-3
 Data Summary (September 2000)
 Ace Services Site
 Remedial Design

Well	Total Cr (ug/L)	Hexavalent Cr (ug/L)	pH (units)	SC (umhos/cm)	Temp. (C)	DO (mg/L)	Turbidity (NTUs)	ORP (mV)
Groundwater								
MW 1 S	14		6.8	1248	20	1.1	3	77
MW 2 S	118		6.9	754	19	5.2	12	83
MW 4 S	22		6.5	1013	19	7.3	4	105
MW 5 S	3 U (3 U)		7.3	733	15	6.9	0	219
MW 6 S	66		7.4	544	20	7.6	17	70
MW 7 S	94		7.2	576	14	6.9	0	222
MW 8 S	10 U		7.2	606	15	6.4	0	212
MW 9 S	259 (300)		7.3	632	15	7.5	0	214
MW 11 S	162	170	7.2	665	15	7.2	0	220
MW 12 S	92	30	7.1	700	20	7.0	7	51
EX 2 S	532		7.3	649	15	6.9	0	216
OB 1 S	483		7.1	916	20	5.6	20	64
OB 2 S	356		7.2	940	18	6.6	6	97
HPMW 6 S	3 U		7.2	940	18	6.6	6	97
HPMW 9 S	374		6.8	950	16	0.8	0	192
ACE R S	358		6.9	1015	17	0.7	12	103
MW 1 I	6		6.7	1111	19	0.3	1	63

Table 5-3
 Data Summary (September 2000)
 Ace Services Site
 Remedial Design

Well	Total Cr (ug/L)	Hexavalent Cr (ug/L)	pH (units)	SC (umhos/cm)	Temp. (C)	DO (mg/L)	Turbidity (NTUs)	ORP (mV)
MW 2 I	1,780	1,800	5.0	660	18	2.2	7	157
MW 4 I	35		6.6	853	19	6.1	3	115
MW 5 I	33	50 U	6.1	551	19	7.3	4	113
	[5]		7.3	480	15	7.7	0	226
MW 6 I	64		7.1	754	18	5.8	8	81
MW 7 I	36	50 U	6.9	566	20	5.6	11	61
MW 8 I	1,020		7.2	624	15	3.8	0	211
MW 9 I	4,170		7.2	592	15	4.5	1	214
MW 11 I	117 (114)	120 (120)	7.2	629	15	6.6	0	204
MW 12 I	182	180	7.4	442	15	7.5	0	192
EX 2 I	2,360	3,000	7.2	571	15	5.2	0	209
OB 1 I	197		7.3	652	18	5.6	7	54
OB 2 I	630		6.7	692	19	4.9	9	117
ACE R I	151		6.9	756	17	4.1	6	199
MW 1 D	22		7.4	428	18	7.9	3	94
MW 2 D	214	220	7.3	450	16	7.1	0	212
MW 3 D	60		7.4	410	15	7.2	0	210
MW 4 D	44		7.0	446	18	8.0	8	121
MW 5 D	4		7.4	422	16	8.0	0	199

Table 5-3
 Data Summary (September 2000)
 Ace Services Site
 Remedial Design

Well	Total Cr (ug/L)	Hexavalent Cr (ug/L)	pH (units)	SC (umhos/cm)	Temp. (C)	DO (mg/L)	Turbidity (NTUs)	ORP (mV)
MW 6 D	211		7.4	551	17	6.7	5	75
MW 7 D	84 (80)		7.5	388	15	7.7	0	227
MW 8 D	1,630 (1610)		7.3	532	15	5.1	0	232
MW 9 D	2,040		7.4	555	15	4.4	0	217
MW 11 D	114		7.4	466	15	7.3	0	213
MW 12 D	7 U (7 U)		7.6	373	15	7.8	0	215
EX 2 D	1,920	1,930	7.1	559	15	4.9	0	48
OB 1 D	210		7.4	437	16	7.0	0	225
OB 2 D	1,120		7.1	657	19	5.6	13	61
ACE R D	61		7.2	621	17	6.3	3	87
PWS 8	2,900	3,000	7.5	587	15	6.9	4	231
Residential Wells								
RW 1	40		7.2	784	15	7.6	0	273
RW 2	3 U		7.7	410	16	8.7	0	212
RW 3	3 U		7.7	400	15	8.4	1	383
RW 4	7 U		7.7	428	15	8.5	0	274
RW 5	9 U		7.6	456	16	7.9	0	248

Table 5-3
Data Summary (September 2000)
Ace Services Site
Remedial Design

Well	Total Cr (ug/L)	Hexavalent Cr (ug/L)	pH (units)	SC (umhos/cm)	Temp. (C)	DO (mg/L)	Turbidity (NTUs)	ORP (mV)
RW 6	132		7.5	484	15	9.0	1	220
RW 8	31 U		7.4	537	16	8.4	1	274
RW 9	3 U		7.7	381	15	8.5	0	262
Rinsates								
MW R I	3 U							
MW 11 S	3 U	50 U						
OB 1 D	3 U							
OB 2 S	4							
IDW (mg/kg)								
OB 1	2							
OB 2	4							
EX 2	3							

Duplicate results in parentheses

Re-sampling in brackets

Cr = chromium

ug/L = microgram per liter

Cr VI = hexavalent chromium

SC = specific conductance

umhos/cm = micromhos per centimeter

Temp = temperature

C = Celsius

DO = dissolved oxygen

mg/L = milligram per liter

NTUs = nephelometric turbidity units

ORP = oxidation/reduction potential

mV = millivolt

MW = monitoring well

P = perched

S = shallow

I = intermediate

D = deep

ND = nondetect (detection limit)

U = qualified as nondetect

J = estimated

ARW = Ace recovery well

PWS = Public Water Supply

R = residential well

mg/kg = milligram per kilogram

IDW = investigation derived waste

Analytical results of the groundwater samples indicate the presence of chromium in groundwater. Comparing results of the total chromium and hexavalent chromium analyses indicates that most or all of the total chromium is in the hexavalent state. Hexavalent chromium (Cr (VI)) typically occurs in the dissolved state while trivalent chromium (Cr (III)) typically occurs as a precipitate or solid. The detected concentration of hexavalent chromium may exceed the total chromium concentration because the parameters were analyzed using two different methods. Data validation procedures have determined that results for both methods are within acceptable ranges of the methodologies.

The total chromium concentrations have been contoured on Figures 5-4 through 5-6 to illustrate the horizontal extent of total chromium in the aquifer in the shallow, intermediate, and deep zones. The vertical extent of hexavalent chromium in the groundwater is illustrated in Figure 5-7.

Historical results for total chromium are presented in Table 5-4.

5.4 Remaining Preliminary RD Activities

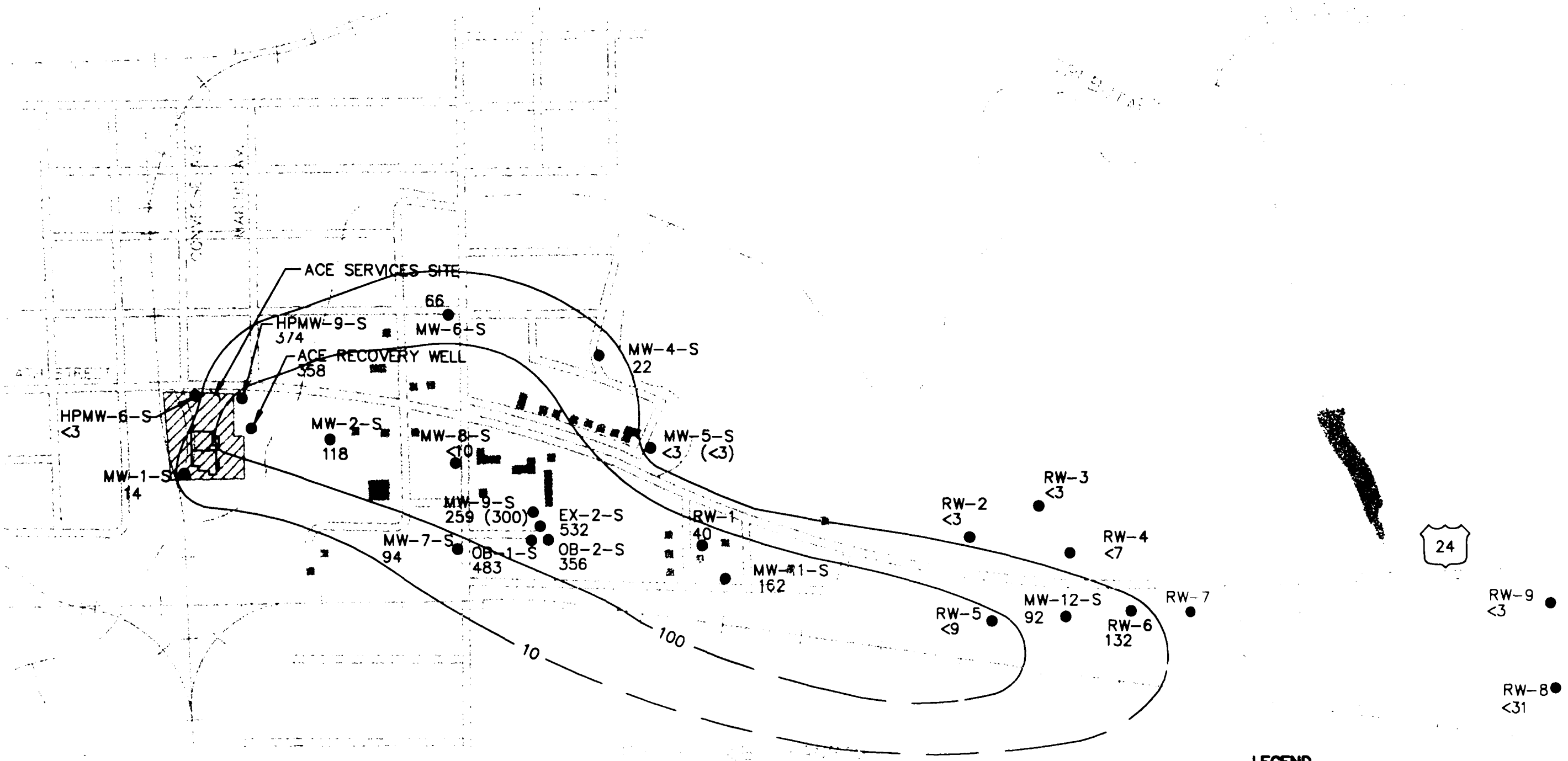
Efforts for completing preliminary RD objectives are described in the RD WP (BVSPC, 1999a; 1999f), FSP (BVSPC, 1999b; 2000a), and QAPP (BVSPC 1999c; 2000b). Initial efforts were planned using information and site data available at that time. Completion in October 1999 of Phase 1 of the preliminary RD activities indicated additional monitoring wells were needed to complete characterization of the nature and extent of contamination. Completion in February 2000 of Phase 2 activities also indicated additional monitoring wells were needed to complete objectives. Phase 3 of the preliminary RD activities was completed in November 2000, results of which are discussed in this report. However, two additional monitoring well nests remain to be installed pending property access.

Phase 3 investigation activities have provided additional and more complete information concerning site characteristics and the nature and extent of contamination. The remaining preliminary RD activities include:

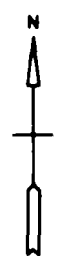
- Installation of two monitoring well nests; and
- Geotechnical borings
- Survey of site area to develop a base map for engineering design drawings.

Two additional monitoring well nests are to be installed to confirm the downgradient extent of the chromium plume (MW-13 and MW-14). Each monitoring well nest will consist of a shallow and intermediate well. The well nests will be installed south of the railroad tracks. Proposed locations for the two well nests are illustrated on Figure 5-8. Final locations of the wells were selected with consideration to property access restrictions.

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NOTES:
 WELL CONSTRUCTION DATA NOT AVAILABLE FOR RESIDENTIAL WELLS (RW). RW DATA ARE PRESENTED FOR REFERENCE ONLY AND ARE NOT CONTOURED.

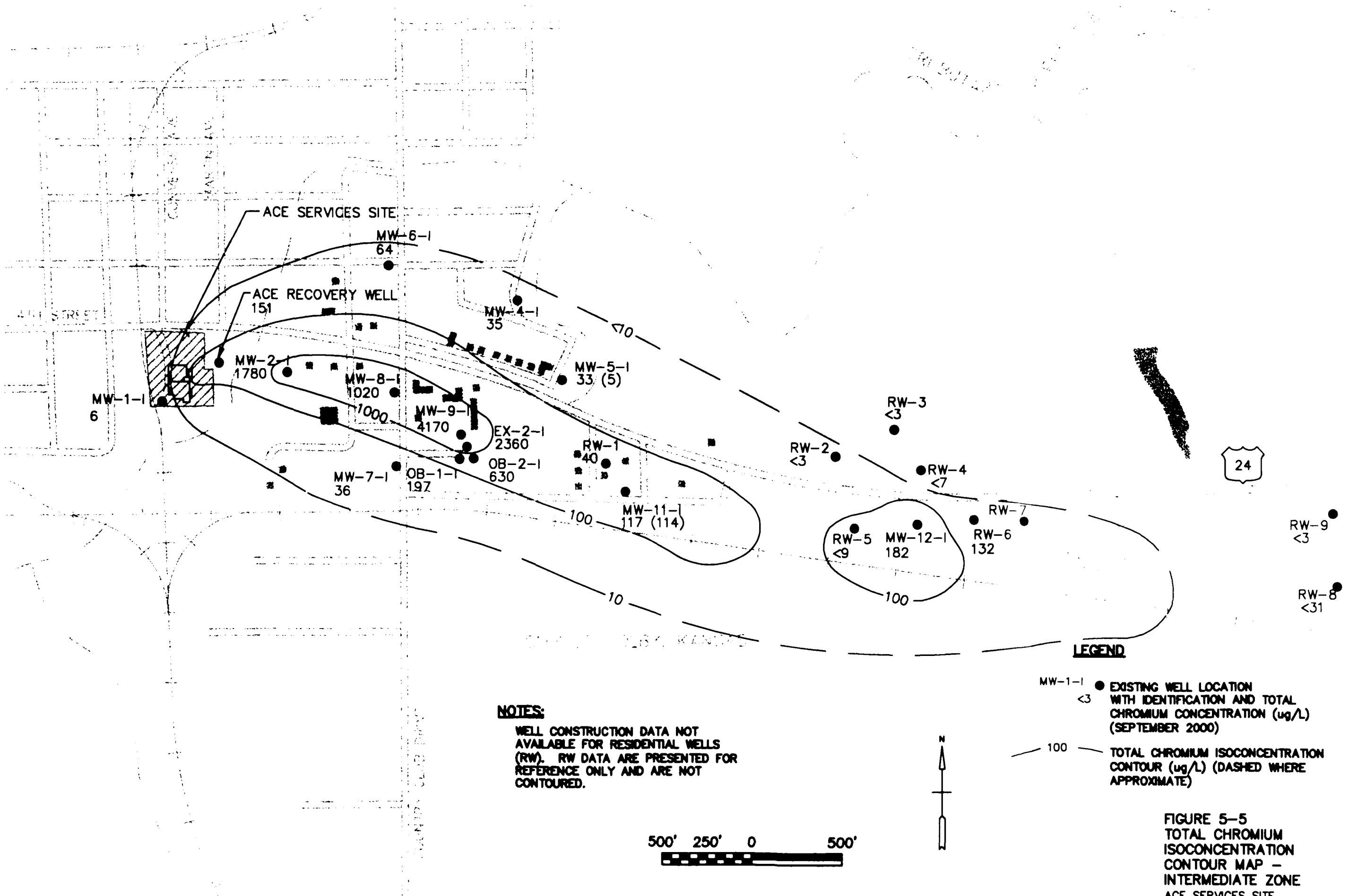


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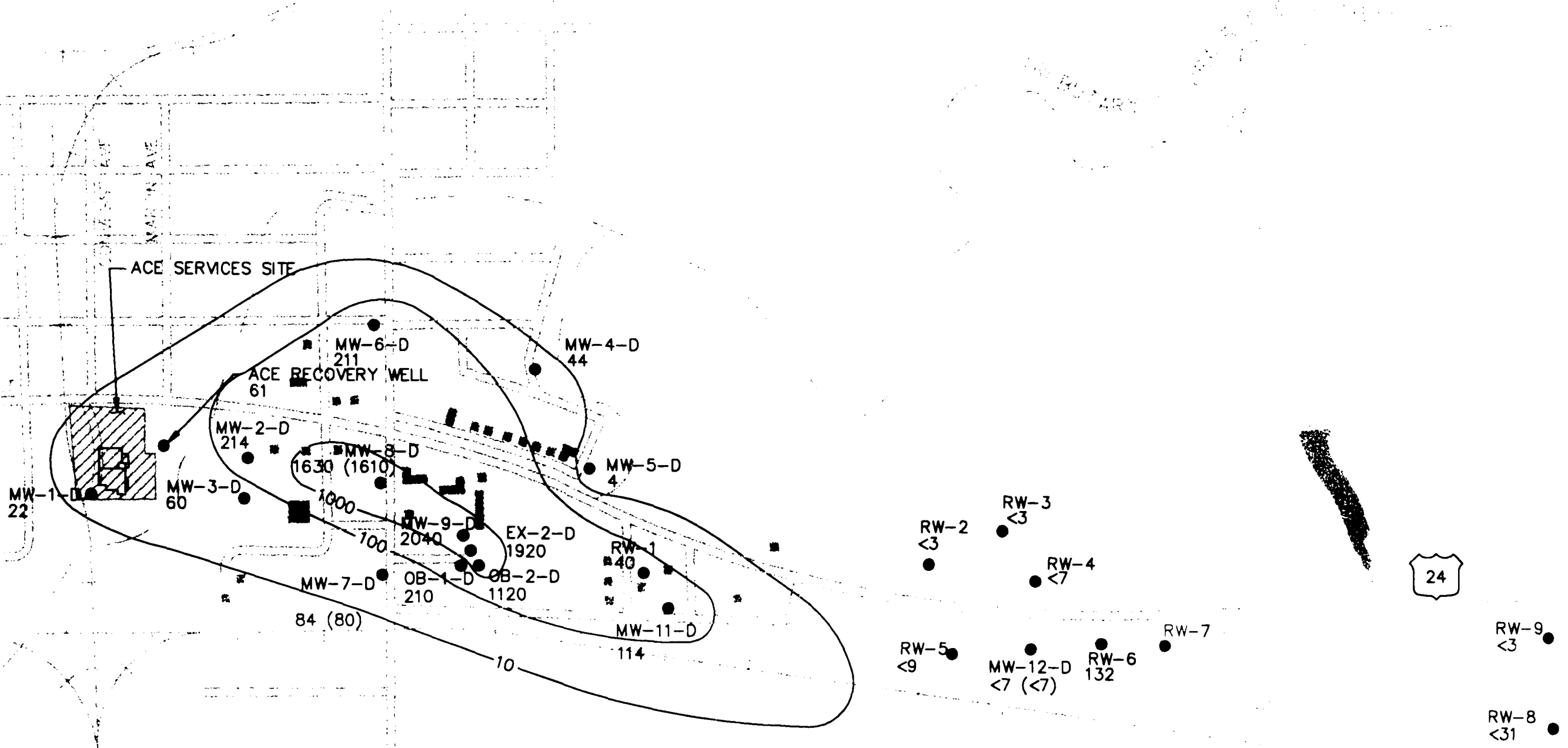
- MW-1-S ● EXISTING WELL LOCATION WITH IDENTIFICATION AND TOTAL CHROMIUM CONCENTRATION (ug/L) (SEPTEMBER 2000)
- 100 ——— TOTAL CHROMIUM ISOCONCENTRATION CONTOUR (ug/L) (DASHED WHERE APPROXIMATE)

FIGURE 5-4
 TOTAL CHROMIUM ISOCONCENTRATION CONTOUR MAP - SHALLOW ZONE ACE SERVICES SITE

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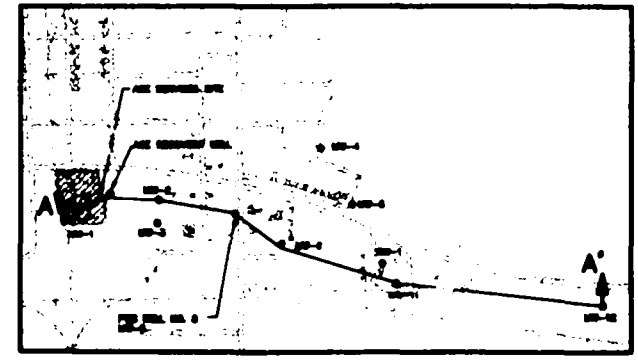
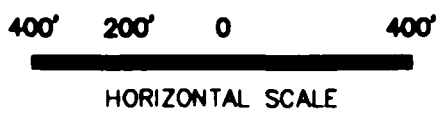
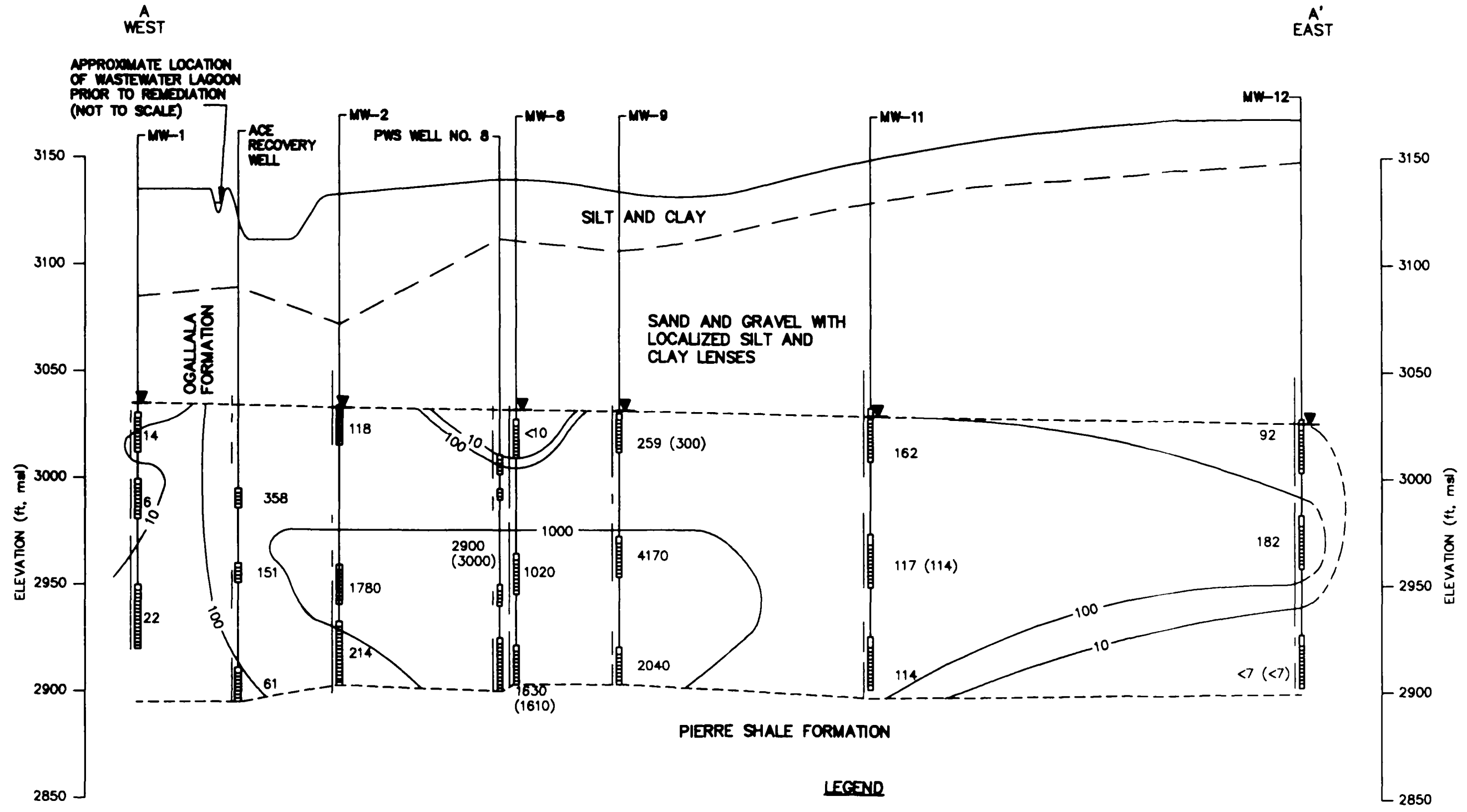
NOTES:
 WELL CONSTRUCTION DATA NOT AVAILABLE FOR RESIDENTIAL WELLS (RW). RW DATA ARE PRESENTED FOR REFERENCE ONLY AND ARE NOT CONTOURED.

LEGEND

- MW-1-D ● EXISTING WELL LOCATION WITH IDENTIFICATION AND TOTAL CHROMIUM CONCENTRATION (ug/L) (SEPTEMBER 2000)
- 100 ——— TOTAL CHROMIUM ISOCONCENTRATION CONTOUR (ug/L) (DASHED WHERE APPROXIMATE)

FIGURE 5-6
 TOTAL CHROMIUM ISOCONCENTRATION CONTOUR MAP - DEEP ZONE ACE SERVICES SITE

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CROSS SECTION LOCATION

LEGEND

- 1000J (990J)
- SCREEN PORTION OF WELL, TOTAL CHROMIUM CONCENTRATION (ug/L), AND DUPLICATE (SEPTEMBER 2000)
- GROUNDWATER ELEVATION FOR SHALLOW ZONE (FEBRUARY 2000)
- TOTAL CHROMIUM ISOCONCENTRATION CONTOUR (ug/L) (DASHED WHERE APPROXIMATE)
- SAND PORTION OF AQUIFER BELOW WATER TABLE

FIGURE 5-7
VERTICAL EXTENT OF
TOTAL CHROMIUM
ACE SERVICES SITE

**Table 5-4
Summary of Historical Analytical Results
Total Chromium in Groundwater (ug/L, unfiltered)
Ace Services Site**

Well Name	1980	1981	1982	1983	1984	1985	1986	1987	1988	6/13-15/89	4/5/90	11/9/90	12/20/90	5/23/91	12/21/94	12/12/95-1/10/96	9/23/25/96	11/1-6/97	10/99	2/00	9/00	
MW-1-D												ND-9	ND			ND	2.9 J	ND(10)	82		22	
MW-2-D													40-118	1910		345	2,610(2,680)		1180(1240)		214	
MW-3-D												ND-7	ND			53	[2,447]	1,200(1,200)				
MW-4-S																	20.2	ND(10)	105		60	
MW-5-S																		ND(10)	92		22	
Ace Recovery Well																		ND(10)	94		ND(3) (ND(1))	
Ace Recovery Well (Shallow Screen)																			870	1130	158	
Ace Recovery Well (Intermediate Screen)																			250	471	151	
Ace Recovery Well (Deep Screen)																			60	160	61	
Colby PWS Well No. 8	112-357	240	480-710	870	1400	9,915	4,985	610-714	410	95-284				135		242	283					
Hi-Plans HPMW-6-S															ND(10)					73	ND(3)	
Hi-Plans HPMW-9-S															1800					501	374	
Residential Well #5										17	17					18	27.5	20	11		ND(9)	
Residential Well #6																24	32.2	60	122	104(101)	132	
Residential Well #1																	43.4	40	37	36	40	
Residential Well #2																ND		ND(10)	ND(10)		ND(3)	
Residential Well #3										ND	ND					ND		ND(10)	22		ND(3)	
Residential Well #4																ND		ND(10)	ND(10)		ND(7)	
Colby Wrecking Co. Well																ND						
Residential Well #7																	14					
Residential Well #8																					ND(11)	
Colby Implement Co. Well																						
Meadowlark Inn Well	20	20	ND			3-14	ND-4100			ND											Plugged	
Cobblestone Inn Well	ND	ND		10	ND-6	4-7	ND-12															Plugged

J = Estimated
 ND(10) = Chromium not detected at identified detection limit
 a = Duplicate sample result in parentheses
 b = KDHE split sample result in brackets
 c = Hi-Plans Co-op Report, February 21, 1995
 112-357 = Minimum-maximum range of total chromium during sampling period
 MCL for Chromium = 100 ug/L.
 Source = KDHE 1989, KDHE 1996

The site survey base map will include the area identified as part of the site. The site survey base map will include areas where additional extraction well nests may need to be installed to achieve the active remediation goal defined in the ROD for the site.

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**Appendix A
Boring Logs**



BLACK & VEATCH

LOG OF BORING

BORING NO. OB-1-S
SHEET 1 OF 1

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9380.08607' E 10308.46867'	ELEVATION (DATUM) 3142.71' (msl)	TOTAL DEPTH 13.3 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Feikner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							1			Undifferentiated Overburden (See boring log for OB-1-D).	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid.	
							2					
							3					
							4					
							5					
							6					
							7					
							8					
							9					
							10					
							11					
							12					
							13					
							14				Bottom of boring @ 133'. Water level not recorded.	
							15					
							16				Monitoring well installed on 7/12/00.	
							17					
							18					
							19					
							20					
							21					
							22					
							23					
							24					
							25					
							26					
							27					
							28					
							29					



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LOG OF BORING

BORING NO. OB-1-I
SHEET 1 OF 1

CLIENT USEPA		PROJECT Ace Services		PROJECT NO 46118	
PROJECT LOCATION Colby, Kansas		COORDINATES N 9378.57019' E 10328.25223'		ELEVATION (DATUM) 3142.31' (msl)	TOTAL DEPTH 19.8 FEET
SURFACE CONDITIONS Grassy			LOGGED BY G. Felkner		DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 8 INCHES	2ND 8 INCHES	3RD 8 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							1			Undifferentiated Overburden (See boring log for OB-1-D).	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid.
							2				
							3				
							4				
							5				
							6				
							7				
							8				
							9				
							10				
							11				
							12				
							13				
							14				
							15				
							16				
							17				
							18				
							19				
							20				
							21				
							22				
							23				
							24				
							25				
							26				
							27				
							28				
							29				

Bottom of boring @ 198'.
Water level not recorded.
Monitoring well installed on 7/13/00.



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LOG OF BORING

BORING NO. 0B-1-D
SHEET 1 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9382.48239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Felkner	DATE FINISH 7/12/00

SAMPLING								CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS	
CORING								DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							1			GRAVEL.	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid. Lithology logged from cuttings.	
							2			Clayey SILT, brown, non-plastic, (Loess).		
							3					
							4					
							5					
							6					
							7					
							8					
							9					
							10					
							11					
							12					
							13					
							14					
							15					
							16					
							17					
							18					
							19					
							20			Silty CLAY, brown.		
							21					
							22					
							23					
							24					
							25					
							26					
							27					
							28					
							29					



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LOG OF BORING

BORING NO. OB-1-D
SHEET 2 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO 48118	
PROJECT LOCATION Colby, Kansas		COORDINATES N 9382.49239' E 10332.46531'		ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Feikner		DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							31			Gravelly SAND, brown, medium grained.	
							32				
							33				
							34				
							35				
							36				
							37				
							38				
							39				
							40				
							41				
							42				
							43			Sandy CLAY, brown.	
							44				
							45				
							46				
							47				
							48				
							49				
							50			Silty CLAY, brown.	
							51				
							52				
							53			Sandy CLAY, brown.	
							54				
							55				
							56				
							57				
							58				
							59				



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LOG OF BORING

BORING NO. OB-1-D
SHEET 3 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9362.49239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Feikner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 0 INCHES	2ND 0 INCHES	3RD 0 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							81				
							82				
							83				
							84				
							85				
							86				
							87				
							88				
							89				



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LOG OF BORING

BORING NO. 0B-1-D
SHEET 4 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9362.49239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Felkner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							91			Clayey SAND, brown.	
							92			Sandy CLAY, brown.	
							93				
							94				
							95				
							96				
							97				
							98				
							99				
							100				
							101			Silty SAND, brown.	
							102				
							103				
							104				
							105				
							106				
							107				
							108				
							109			Gravelly SAND, brown, medium grained w/some clay.	
							110				
							111				
							112				
							113				
							114				
							115				
							116				
							117				
							118				
							119				



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LOG OF BORING

BORING NO. OB-1-D
SHEET 5 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9382.49239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Felkner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							121					
							122					
							123					
							124					
							125					
							126					
							127					
							128					
							129					
							130					
							131					
							132					
							133					
							134					
							135					
							136					
							137					
							138					
							139					
							140					
							141					
							142					
							143					
							144					
							145					
							146					
							147					
							148					
							149					



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LOG OF BORING

BORING NO. OB-1-D
SHEET 6 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4818	
PROJECT LOCATION Colby, Kansas		COORDINATES N 9382.49239' E 10332.46531'		ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel			LOGGED BY G. Felkner		DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							151			Clayey SAND, brown, fine to medium grained.	
							152				
							153				
							154				
							155				
							156				
							157				
							158				
							159				
							160				
							161				
							162				
							163				
							164				
							165				
							166				
							167				
							168				
							169				
							170				
							171				
							172				
							173				
							174				
							175				
							176				
							177				
							178				
							179			Gravelly SAND, brown.	



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LOG OF BORING

BORING NO. OB-1-D
SHEET 7 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4818
PROJECT LOCATION Colby, Kansas		COORDINATES N 9382.49239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Felkner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 0 INCHES	2ND 0 INCHES	3RD 0 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							181				
							182				
							183				
							184				
							185				
							186				
							187				
							188				
							189				
							190				
							191				
							192				
							193				
							194				
							195				
							196				
							197			Silty CLAY.	
							198				
							199				
							200				
							201				
							202				
							203				
							204				
							205				
							206			Clayey SAND, brown, medium grained.	
							207				
							208				
							209				



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LOG OF BORING

BORING NO. OB-1-D
SHEET 8 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9362.49239' E 10332.46531'	ELEVATION (DATUM) 3141.98' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Gravel.			LOGGED BY G. Feikner	DATE FINISH 7/12/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							211				
							212				
							213				
							214				
							215				
							216				
							217				
							218				
							219				
							220			CLAY, brown.	
							221				
							222				
							223				
							224				
							225			Gravelly SAND, brown.	
							226				
							227				
							228				
							229				
							230				
							231				
							232				
							233				
							234				
							235			SHALE, grayish-green, thin bedded. (Pierre Shale Fm).	
							236				
							237				
							238				
							239				

-4000 gallons water used during drilling.
Bottom of boring @ 240'.
Water level not recorded. Extraction well installed 7/12/00.



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LOG OF BORING

BORING NO. OB-2-S
SHEET 1 OF 1

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.06295' E 10392.88955'	ELEVATION (DATUM) 3159.59' (msl)	TOTAL DEPTH 13.3 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/14/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							1			Undifferentiated Overburden (See boring log for OB-2-D).	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid.
							2				
							3				
							4				
							5				
							6				
							7				
							8				
							9				
							10				
							11				
							12				
							13				
							14			Bottom of boring @ 133'. Water level not recorded. Monitoring well installed on 7/14/00.	
							15				
							16				
							17				
							18				
							19				
							20				
							21				
							22				
							23				
							24				
							25				
							26				
							27				
							28				
							29				



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LOG OF BORING

BORING NO. OB-2-I
SHEET 1 OF 1

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.94194' E 10402.35013'	ELEVATION (DATUM) 3138.63' (msl)	TOTAL DEPTH 196 FEET
SURFACE CONDITIONS Grassy			LOGGED BY G. Felkner	DATE START 7/14/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							1			Undifferentiated Overburden (See boring log for OB-2-D).	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid.
							2				
							3				
							4				
							5				
							6				
							7				
							8				
							9				
							10				
							11				
							12				
							13				
							14				
							15				
							16				
							17				
							18				
							19				
							20			Bottom of boring @ 196'.	
							21			Water level not recorded.	
							22			Monitoring well installed on 7/14/00.	
							23				
							24				
							25				
							26				
							27				
							28				
							29				



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LOG OF BORING

BORING NO. OB-2-D
SHEET 1 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4818
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/13/00

SAMPLING								CHECKED BY		APPROVED BY		REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET	2ND 6 INCHES	3RD 6 INCHES	N	VALUE	SAMPLE RECOVERY	B. Smith		B. Smith		
CORING								DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD	ROD					CLASSIFICATION OF MATERIAL
								1			TOPSOIL	Boring advanced using rotary wash methods w/5-3/8" OD drag bit. Reamed boring w/8" OD drag bit using water as drilling fluid. Lithology logged from cuttings.
								2			Clayey SILT, brown. (Loess).	
								3				
								4				
								5				
								6				
								7				
								8				
								9				
								10				
								11				
								12				
								13				
								14				
								15				
								16				
								17				
								18				
								19				
								20			CLAY, brown.	
								21				
								22				
								23				
								24				
								25				
								26				
								27				
								28				
								29				



CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4818	
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'		ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner		DATE FINISH 7/13/00

SAMPLING						CHECKED BY B. Smith		APPROVED BY B. Smith	
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG

CORING							DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					

							31		Clayey SAND, brown.	
							32			
							33			
							34			
							35			
							36			
							37			
							38			
							39			
							40			
							41			
							42			
							43			
							44			
							45			
							46			
							47			
							48			
							49			
							50			
							51			
							52			
							53			
							54			
							55			
							56			
							57			
							58			
							59			



BLACK & VEATCH

LOG OF BORING

BORING NO. OB-2-D
SHEET 3 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							81					
							82					
							83					
							84					
							85					
							86					
							87					
							88					
							89					
							81					
							82					
							83					
							84					
							85					
							86					
							87					
							88					
							89					
							81					
							82					
							83					
							84					
							85					
							86					
							87					
							88					
							89					

Sandy CLAY, brown.

Clayey SAND, brown, medium grained.



BLACK & VEATCH

LOG OF BORING

BORING NO. 08-2-D
SHEET 4 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith	APPROVED BY B. Smith
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY		

CORING							DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					

							91				
							92				
							93			Sandy CLAY, brown.	
							94				
							95				
							96				
							97				
							98			Clayey SAND, brown, medium grained.	
							99				
							100				
							101				
							102				
							103				
							104				
							105				
							106				
							107				
							108				
							109				
							110				
							111				
							112				
							113				
							114				
							115				
							116				
							117				
							118				
							119				



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LOG OF BORING

BORING NO. 0B-2-D
SHEET 5 OF 8

CLIENT USEPA	PROJECT Ace Services	PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas	COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)
SURFACE CONDITIONS Grassy.	TOTAL DEPTH 240 FEET	DATE START 7/13/00
	LOGGED BY G. Feikner	DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 0 INCHES	2ND 0 INCHES	3RD 0 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING							DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							121					
							122					
							123					
							124					
							125					
							126					
							127					
							128					
							129					
							130					
							131					
							132					
							133					
							134					
							135					
							136					
							137					
							138					
							139					
							140					
							141					
							142					
							143					
							144					
							145					
							146					
							147					
							148					
							149					

Sandy CLAY, brown.



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LOG OF BORING

BORING NO. OB-2-D
SHEET 6 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy			LOGGED BY G. Feikner	DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							151			Clayey SAND, brown.	
							152				
							153				
							154				
							155				
							156				
							157				
							158				
							159				
							160				
							161				
							162				
							163				
							164				
							165			Gravelly SAND, brown.	
							166				
							167				
							168				
							169				
							170				
							171				
							172				
							173			Sandy CLAY, brown, w/trace gravel.	
							174				
							175				
							176				
							177				
							178				
							179				



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LOG OF BORING

BORING NO. OB-2-D
SHEET 7 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Feikner	DATE FINISH 7/13/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 0 INCHES	2ND 0 INCHES	3RD 0 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							181					
							182					
							183				Clayey SAND, brown.	
							184					
							185					
							186					
							187					
							188					
							189					
							190					
							191					
							192					
							193					
							194					
							195					
							196					
							197					
							198					
							199					
							200					
							201					
							202					
							203					
							204					
							205					
							206					
							207					
							208					
							209					



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LOG OF BORING

BORING NO. OB-2-D
SHEET 8 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9377.88098' E 10412.45754'	ELEVATION (DATUM) 3138.11' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/13/00

SAMPLING								CHECKED BY B. Smith			APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS		
CORING								DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS	
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD							
							211						
							212						
							213						
							214						
							215			CLAY, brown.			
							216						
							217						
							218						
							219						
							220			Gravelly SAND, brown.			
							221						
							222						
							223						
							224						
							225						
							226						
							227						
							228						
							229						
							230						
							231						
							232						
							233						
							234			SHALE, greenish-gray, thin bedded, (Pierre Shale Fm).			
							235						
							236						
							237						
							238						
							239						

-4000 gallons water used during drilling
Bottom of boring @ 240'.
Water level not recorded. Extraction well installed 7/13/00.



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LOG OF BORING

BORING NO. EX-2-S
SHEET 1 OF 1

CLIENT USEPA	PROJECT Ace Services	PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas	COORDINATES N 9449.78932' E 10338.29564'	ELEVATION (DATUM) 3142.13' (msl)
TOTAL DEPTH 135 FEET		DATE START 7/11/00
SURFACE CONDITIONS Grassy.		LOGGED BY G. Felkner
		DATE FINISH 7/11/00

SAMPLING								CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT. (x10)	SAMPLE TYPE	GRAPHIC LOG				
CORING													
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD							
							1			Undifferentiated Overburden (See boring log for EX-2-D).	Boring advanced using rotary wash methods w/7 1/2" OD drag bit. Reamed boring w/10" OD drag bit using water as drilling fluid.		
							2						
							3						
							4						
							5						
							6						
							7						
							8						
							9						
							10						
							11						
							12				~4,000 gallons of water used during drilling.		
							13						
							14				Bottom of boring @ 135'.		
							15				Water level not recorded.		
							16				Monitoring well installed on 7/11/00.		
							17						
							18						
							19						
							20						
							21						
							22						
							23						
							24						
							25						
							26						
							27						
							28						
							29						



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LOG OF BORING

BORING NO. EX-2-I
SHEET 1 OF 1

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9441.91718' E 10347.99760'	ELEVATION (DATUM) 3141.30' (msl)	TOTAL DEPTH 200 FEET
SURFACE CONDITIONS Gravel/Asphalt Road			LOGGED BY G. Felkner	DATE FINISH 7/11/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							1		Undifferentiated Overburden (See boring log for EX-2-0)	Boring advanced using rotary wash methods w/7 1/2" OD drag bit. Reamed boring w/12" OD drag bit using Bentonite/water as drilling fluid.	
							2				
							3				
							4				
							5				
							6				
							7				
							8				
							9				
							10				
							11				
							12				
							13				
							14				
							15				
							16				
							17				
							18				
							19				
							20				
							21				
							22				
							23				
							24				
							25				
							26				
							27				
							28				
							29				
										Bottom of boring @ 200'. Water level not recorded. Monitoring well installed on 7/11/00.	



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LOG OF BORING

BORING NO. EX-2-D
SHEET 1 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118	
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31823' E 10358.43995'		ELEVATION (DATUM) 3140.50' (msl)	
SURFACE CONDITIONS Grassy.		LOGGED BY G. Felkner		TOTAL DEPTH 240 FEET	
		APPROVED BY B. Smith		DATE START 7/10/00	
				DATE FINISH 7/10/00	

SAMPLING								CHECKED BY B. Smith		APPROVED BY B. Smith	
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							1			TOPSOIL.	Boring advanced using rotary wash methods w/7 1/2" OD drag bit. Reamed boring w/12" OD drag bit using Bentonite/water as drilling fluid. Lithology logged from cuttings.
							2			Clayey SILT, brown, non-plastic, (Loess).	
							3				
							4				
							5				
							6				
							7				
							8				
							9				
							10				
							11				
							12				
							13				
							14				
							15				
							16				
							17				
							18				
							19				
							20			Silty CLAY, brown.	
							21				
							22				
							23				
							24				
							25				
							26				
							27				
							28				
							29				



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LOG OF BORING

BORING NO. EX-2-D
SHEET 2 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4818
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31623' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy			LOGGED BY G. Felkner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	
CORING							DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
							31			Gravelly SAND, brown, medium grained, some clay.	
							32				
							33				
							34				
							35				
							36				
							37				
							38				
							39				
							40				
							41				
							42				
							43			Sandy CLAY, brown.	
							44				
							45				
							46				
							47				
							48				
							49				
							50				
							51				
							52				
							53				
							54				
							55				
							56				
							57				
							58				
							59				



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LOG OF BORING

BORING NO. EX-2-D
SHEET 3 OF 8

CLIENT USEPA	PROJECT Ace Services	PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas	COORDINATES N 9434.31823' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)
SURFACE CONDITIONS Grassy.	TOTAL DEPTH 240 FEET	DATE START 7/10/00
	LOGGED BY G. Felkner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	
CORING	CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY					
							81		Gravelly SAND, brown, medium grained.		
							82				
							83				
							84			Sandy CLAY, brown.	
							85				
							86				
							87				
							88				
							89				
							81				
							82				
							83				
							84				
							85				
							86				
							87				
							88				
							89				



BLACK & VEATCH

LOG OF BORING

BORING NO. EX-2-D
SHEET 4 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31623' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy			LOGGED BY G. Felkner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 8 INCHES	2ND 8 INCHES	3RD 8 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING							DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROO RECOVERY	PERCENT RECOVERY	ROO					
							91				
							92				
							93				
							94				
							95				
							96				
							97				
							98				
							99				
							100				
							101				
							102				
							103				
							104				
							105				
							106			Gravelly SAND, brown, medium grained, some clay.	
							107				
							108				
							109				
							110				
							111				
							112				
							113				
							114				
							115				
							116				
							117				
							118				
							119				



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LOG OF BORING

BORING NO. EX-2-D
SHEET 5 OF 8

CLIENT USEPA	PROJECT Ace Services	PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas	COORDINATES N 9434.31823' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)
SURFACE CONDITIONS Grassy.	TOTAL DEPTH 240 FEET	DATE START 7/10/00
	LOGGED BY G Feikner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							121				
							122				
							123				
							124				
							125				
							126				
							127				
							128				
							129				
							130				
							131			Sandy CLAY, brown.	
							132				
							133				
							134				
							135				
							136			Clayey SAND, brown, medium grained.	
							137				
							138				
							139				
							140			Sandy CLAY, brown.	
							141				
							142				
							143				
							144				
							145				
							146			Clayey SAND, brown, medium grained.	
							147				
							148				
							149				



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LOG OF BORING

BORING NO. EX-2-D
SHEET 6 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 4618
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31823' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET Ø INCHES	2ND Ø INCHES	3RD Ø INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							151					
							152					
							153					
							154					
							155					
							156					
							157					
							158					
							159					
							160					
							161					
							162					
							163					
							164					
							165					
							166					
							167					
							168					
							169					
							170					
							171					
							172					
							173					
							174					
							175					
							176					
							177					
							178					
							179					



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LOG OF BORING

BORING NO. EX-2-D
SHEET 7 OF 8

CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 48118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31823' E 10358.43895'	ELEVATION (DATUM) 3140.50' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/10/00

SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		CLASSIFICATION OF MATERIAL	REMARKS
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FEET	SAMPLE TYPE	GRAPHIC LOG			
CORING												
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD						
							181					
							182					
							183					
							184					
							185				SAND, brown, medium grained.	
							186					
							187					
							188					
							189					
							190					
							191				Clayey SAND, brown, medium grained.	
							192					
							193					
							194					
							195					
							196					
							197					
							198					
							199					
							200					
							201					
							202					
							203					
							204					
							205					
							206					
							207					
							208					
							209					



CLIENT USEPA		PROJECT Ace Services		PROJECT NO. 46118
PROJECT LOCATION Colby, Kansas		COORDINATES N 9434.31623' E 10358.43995'	ELEVATION (DATUM) 3140.50' (msl)	TOTAL DEPTH 240 FEET
SURFACE CONDITIONS Grassy.			LOGGED BY G. Felkner	DATE FINISH 7/10/00

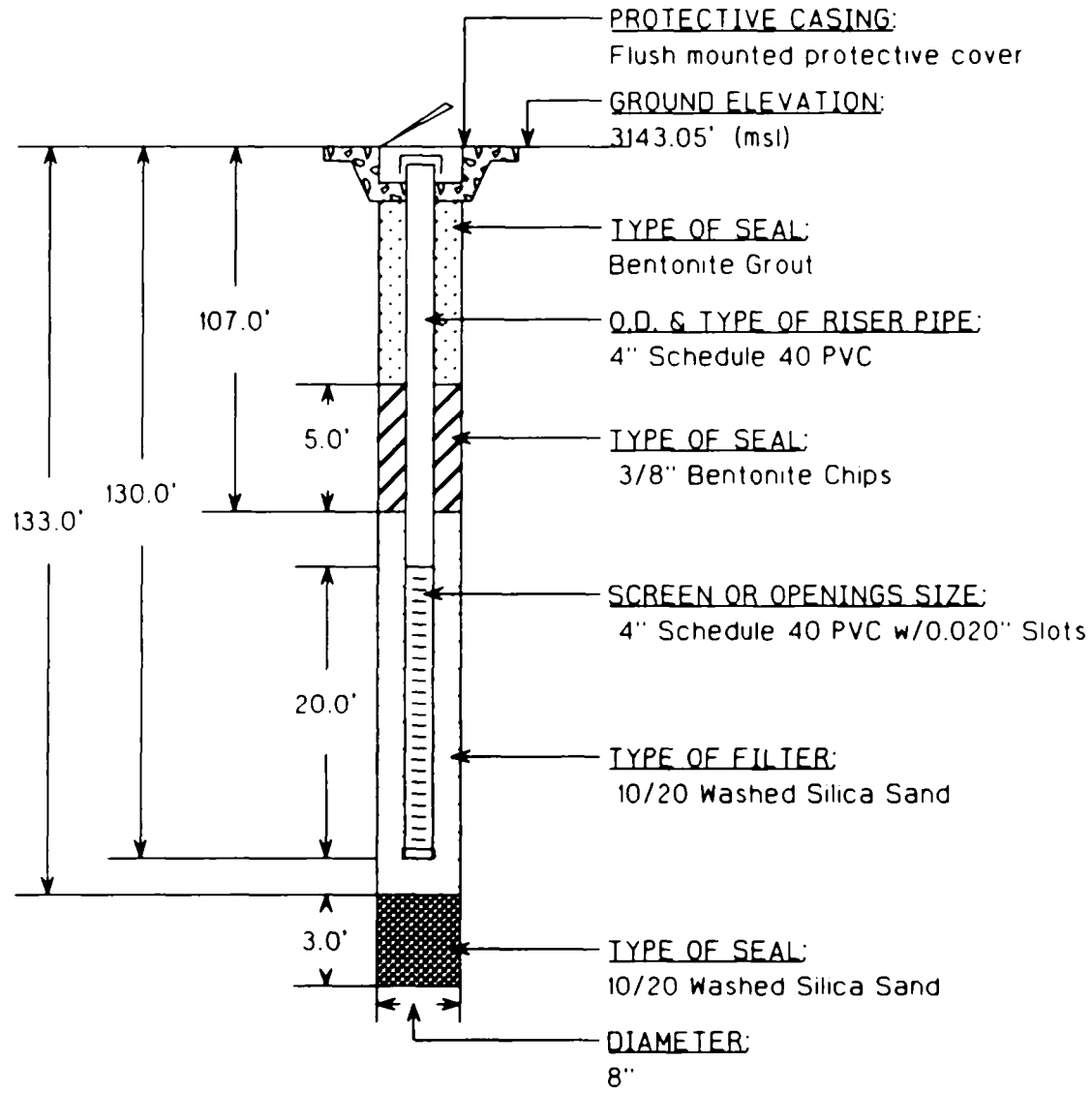
SAMPLING							CHECKED BY B. Smith		APPROVED BY B. Smith		
SAMPLE TYPE	SAMPLE NUMBER	SET 6 INCHES	2ND 6 INCHES	3RD 6 INCHES	N VALUE	SAMPLE RECOVERY	DEPTH IN FT (x10)	SAMPLE TYPE	GRAPHIC LOG	CLASSIFICATION OF MATERIAL	REMARKS
CORING											
CORE SIZE	RUN NUMBER	RUN LENGTH	RUN RECOVERY	ROD RECOVERY	PERCENT RECOVERY	ROD					
							211				
							212				
							213				
							214				
							215				
							216				
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							218				
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							220				
							221				
							222				
							223			Gravelly SAND, brown, medium grained.	
							224				
							225				
							226				
							227				
							228				
							229				
							230				
							231				
							232				
							233				
							234			SHALE, greenish-gray, thin bedded, (Pierre Shale Fm).	
							235				
							236				
							237				
							238				
							239				

~4000 gallons water used during drilling.
Bottom of boring @ 240'. Water level not recorded. Extraction well installed 7/10/00.

Appendix B
Well Construction Logs



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 46118
PROJECT LOCATION Colby, KS	COORDINATES N 9380.08607' E 10308.46867'	TOP OF RISER ELEVATION (DATUM) 3142.71' (msl)	DATE 7/12/00
STRATUM MONITORED Gravelly SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	



METHOD OF INSTALLATION.

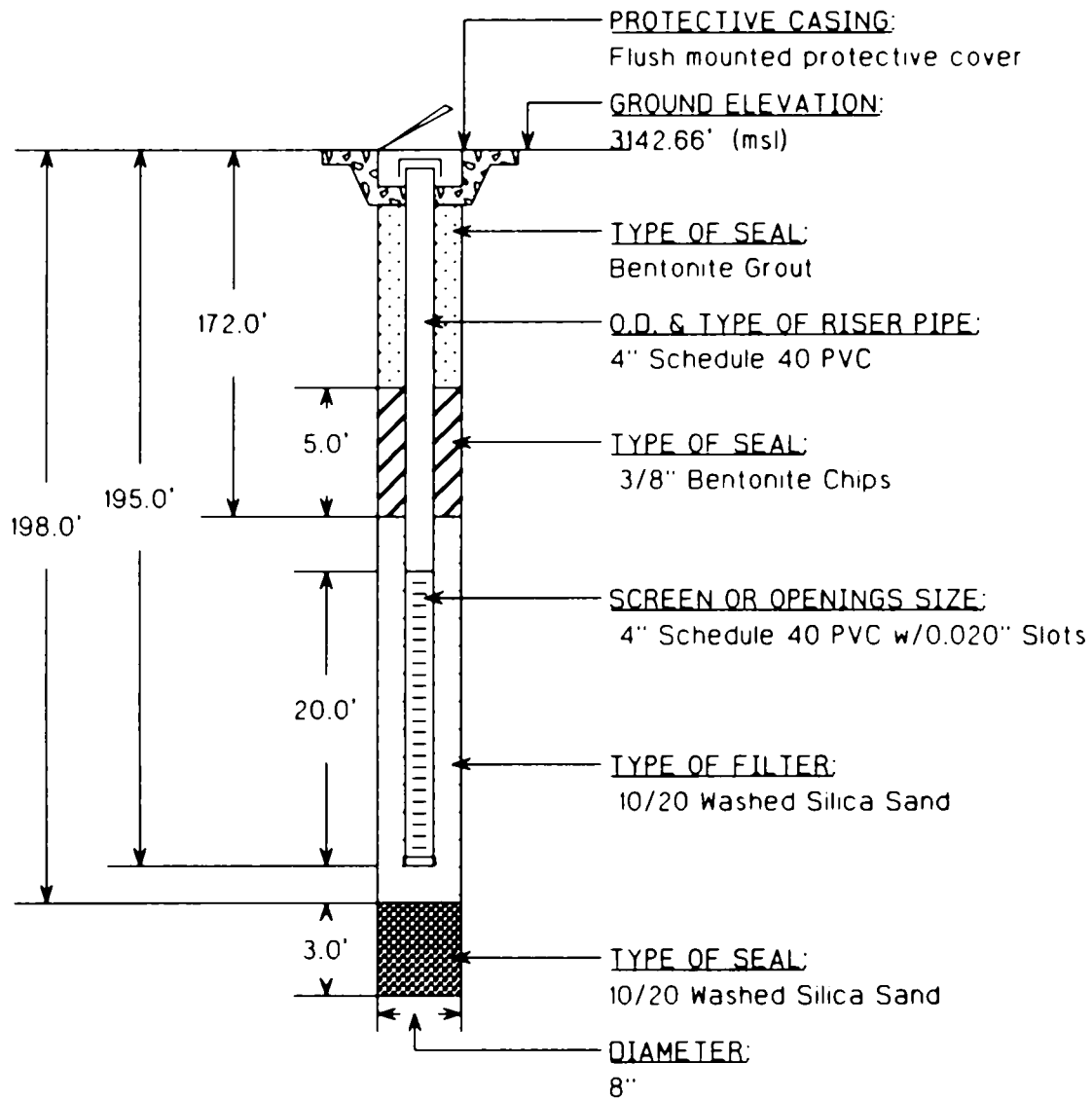
Boring drilled to completion, set riser pipe & screen; placed filter & seal. Grouted to 2' below ground surface.

REMARKS

Well developed by pumping ~2,525 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 48118
PROJECT LOCATION Colby, KS	COORDINATES N 9378.57019' E 10328.25223'	TOP OF RISER ELEVATION (DATUM) 3142.31' (msl)	DATE 7/13/00
STRATUM MONITORED Clayey SAND, Gravelly SAND		LOGGED BY G Felkner	
CHECKED BY B Smith		APPROVED BY B Smith	

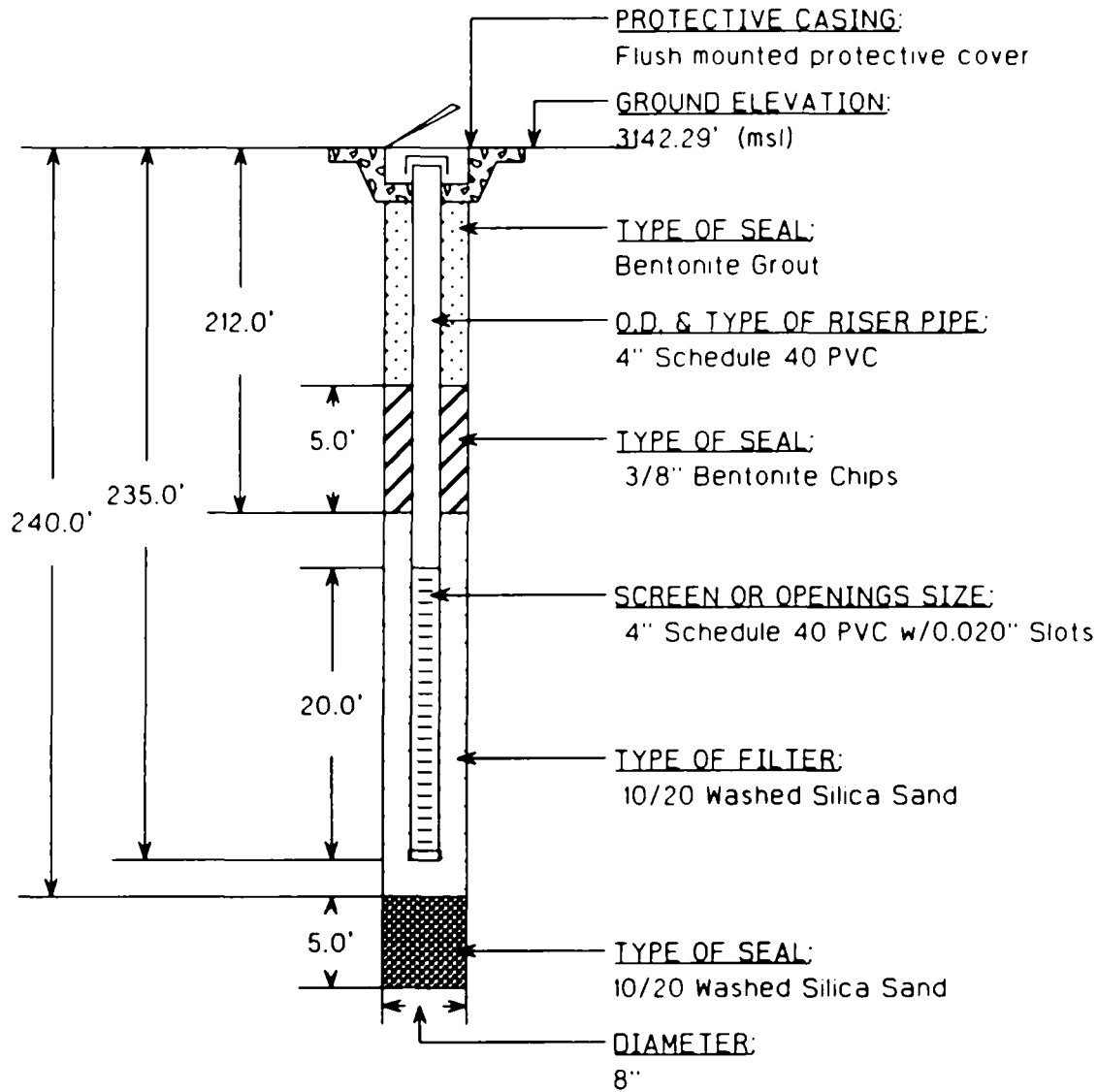


METHOD OF INSTALLATION.
Boring drilled to completion, set riser pipe & screen, placed filter & seal. Grouted to 2' below ground surface.

REMARKS.
Well developed by pumping ~5,115 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 46118
PROJECT LOCATION Colby, KS	COORDINATES N 9362.49239' E 10332.46531'	TOP OF RISER ELEVATION (DATUM) 3141.98' (msl)	DATE 7/12/00
STRATUM MONITORED Clayey SAND, CLAY, Gravelly SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	

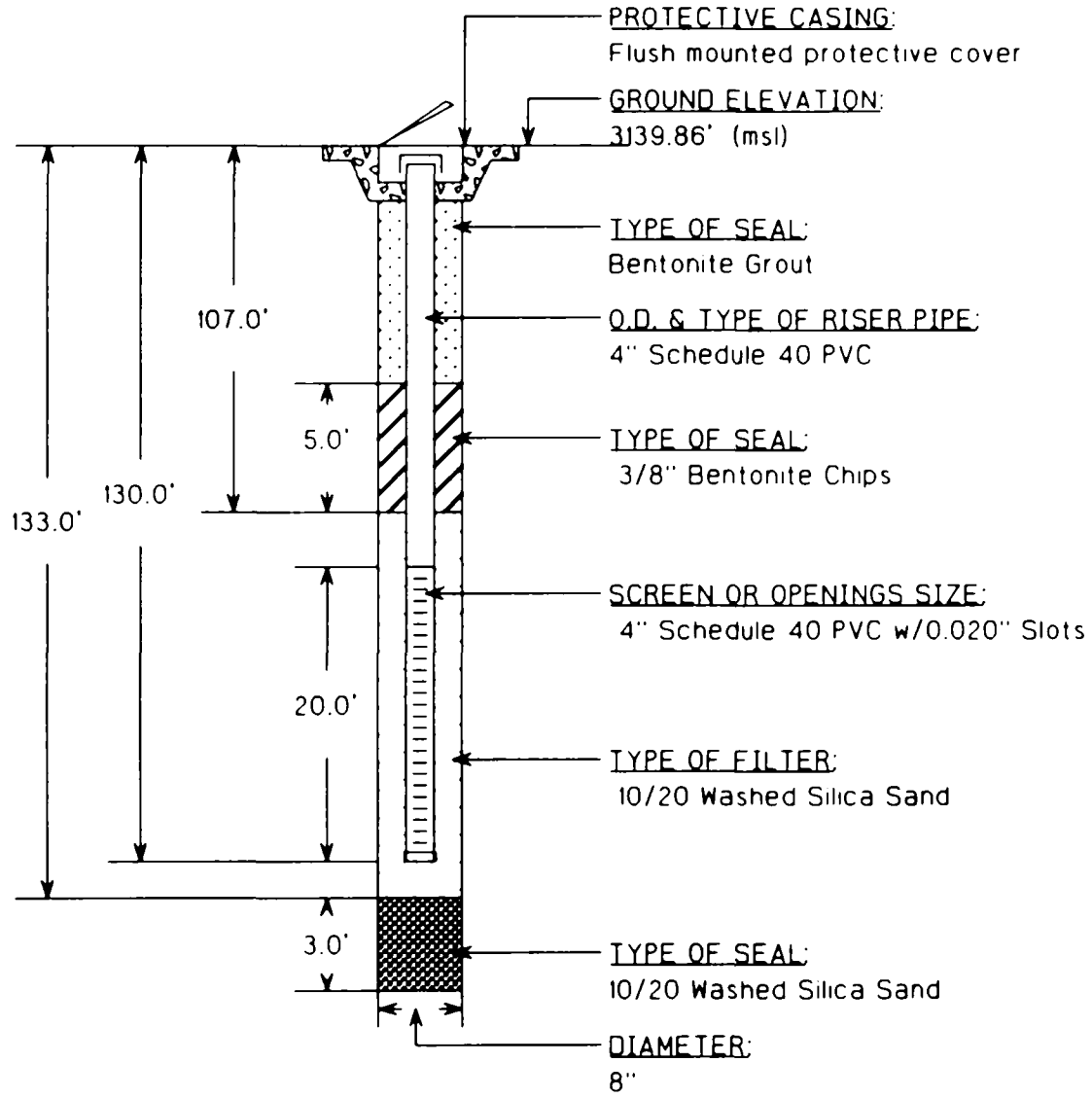


METHOD OF INSTALLATION:
Boring drilled to completion; set riser pipe & screen; placed filter & seal. Grouted to 2' below ground surface.

REMARKS:
Well developed by pumping ~5,500 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 48118
PROJECT LOCATION Colby, KS	COORDINATES N 9377.06295' E 10392.88955'	TOP OF RISER ELEVATION (DATUM) 3139.59' (msl)	DATE 7/14/00
STRATUM MONITORED Clayey SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	

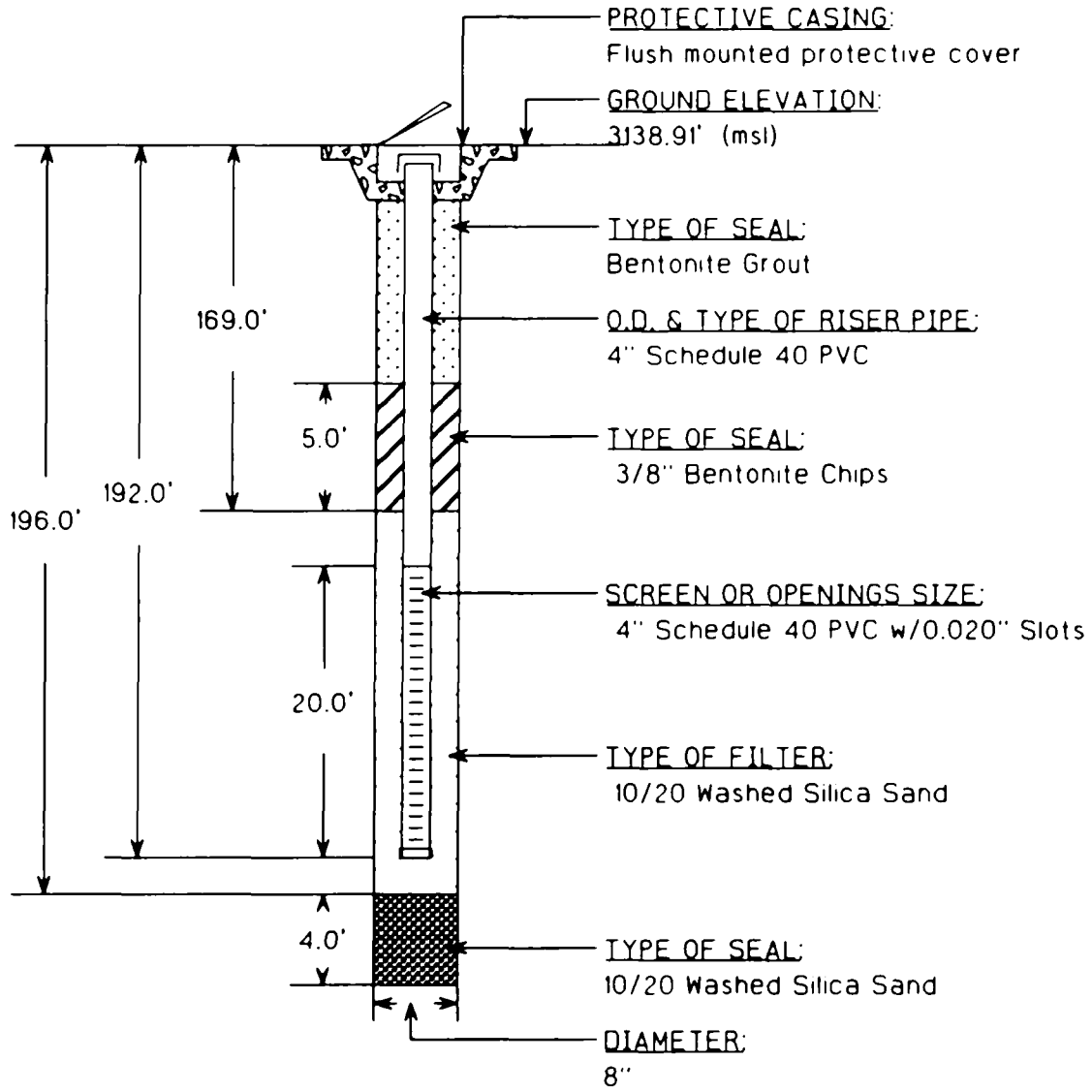


METHOD OF INSTALLATION:
Boring drilled to completion, set riser pipe & screen, placed filter & seal. Grouted to 2' below ground surface.

REMARKS:
Well developed by pumping ~2,900 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 46118
PROJECT LOCATION Colby, KS	COORDINATES N 9377.94194' E 10402.35013'	TOP OF RISER ELEVATION (DATUM) 3138.63' (msl)	DATE 7/14/00
STRATUM MONITORED Sandy CLAY, Clayey SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	

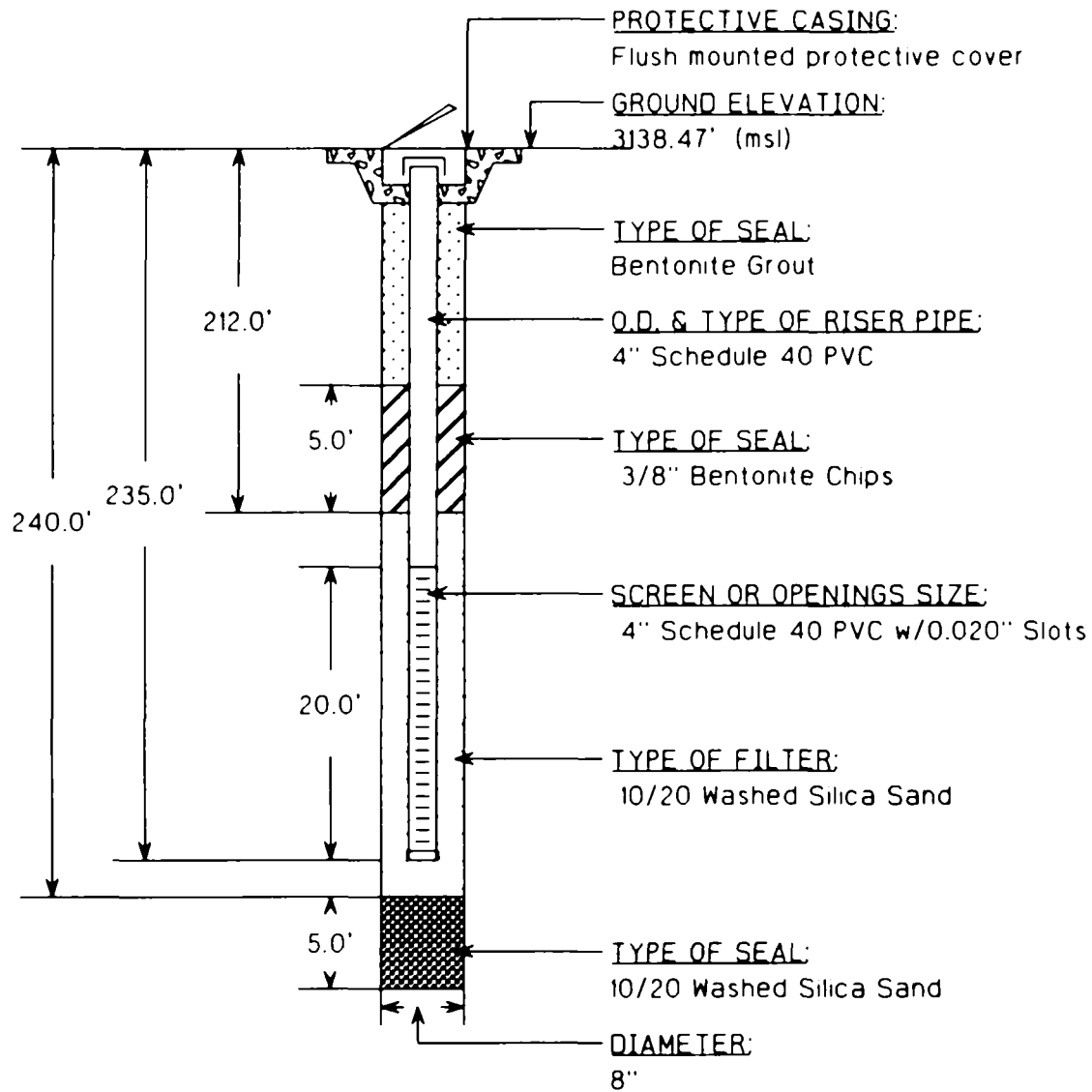


METHOD OF INSTALLATION.
Boring drilled to completion, set riser pipe & screen; placed filter & seal. Grouted to 2' below ground surface.

REMARKS.
Well developed by pumping ~8,500 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 46118
PROJECT LOCATION Colby, KS	COORDINATES N 9377.88098' E 10412.45754'	TOP OF RISER ELEVATION (DATUM) 3138.11' (msl)	DATE 7/13/00
STRATUM MONITORED CLAY, Gravelly SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	

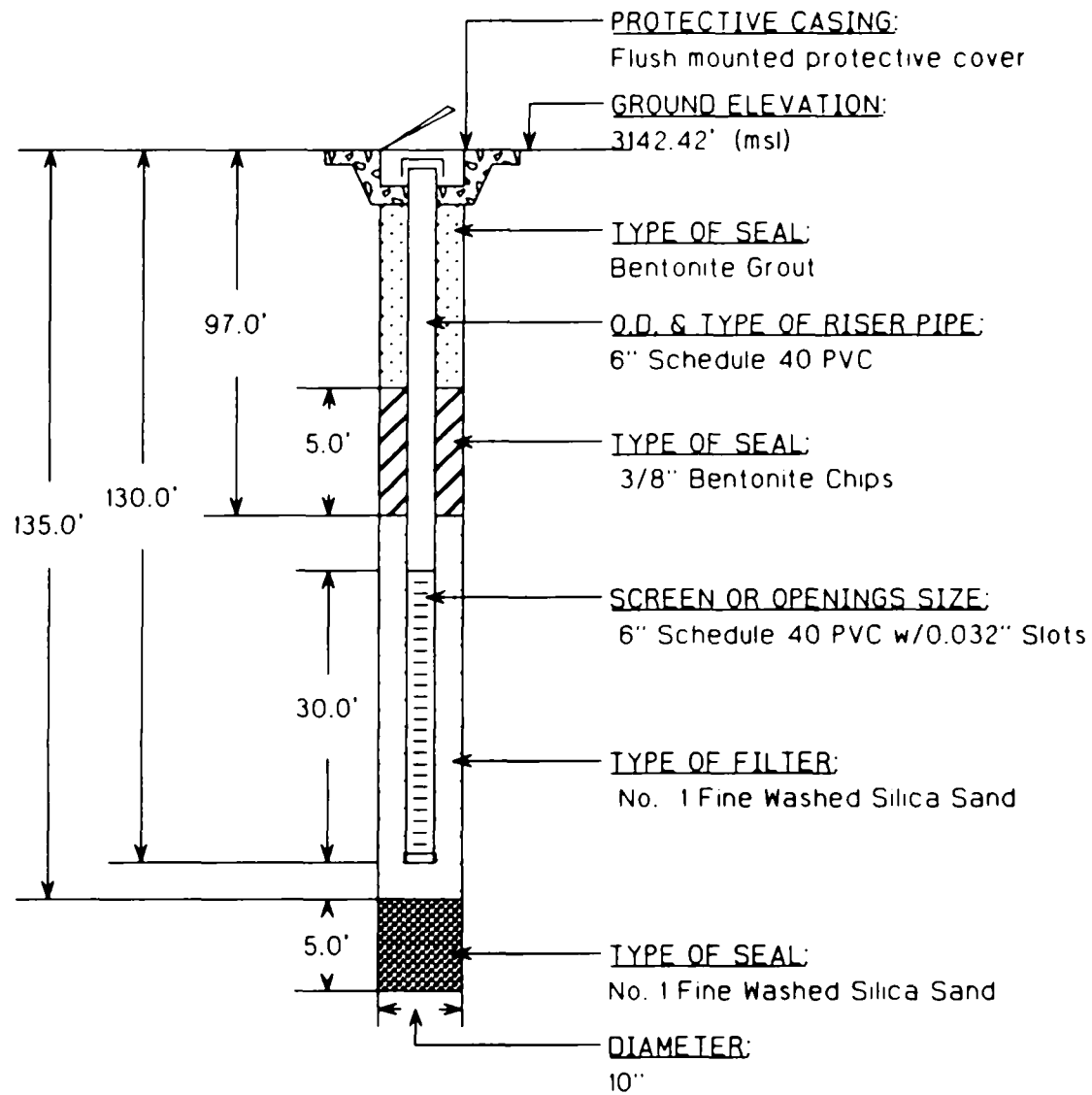


METHOD OF INSTALLATION:
Boring drilled to completion, set riser pipe & screen, placed filter & seal. Grouted to 2' below ground surface.

REMARKS:
Well developed by pumping ~4,680 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 46118
PROJECT LOCATION Colby, KS	COORDINATES N 9449.78932' E 10336.29564'	TOP OF RISER ELEVATION (DATUM) 3142.13' (msl)	DATE 7/11/00
STRATUM MONITORED Gravelly SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	



METHOD OF INSTALLATION.

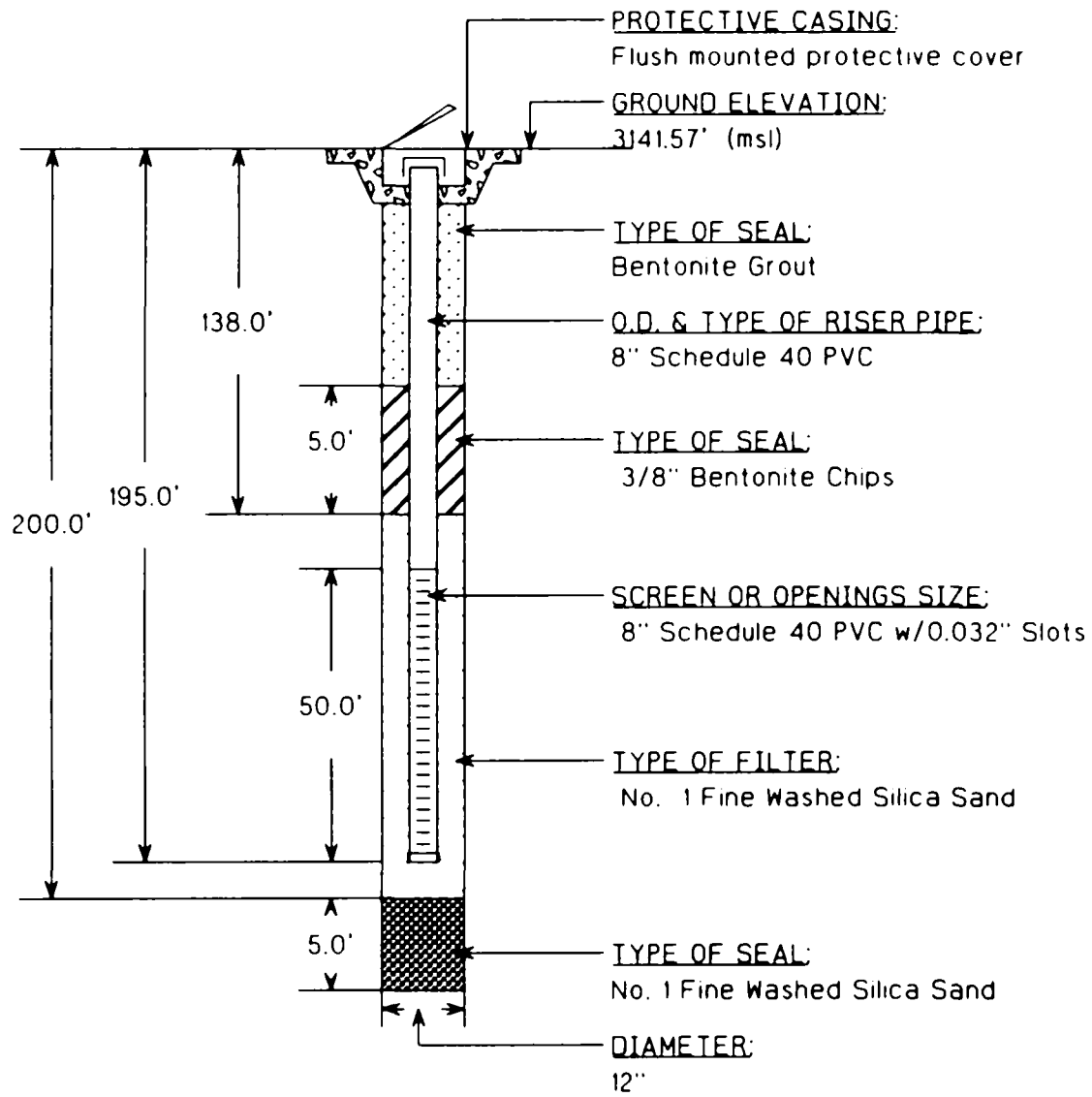
Boring drilled to completion, set riser pipe & screen, placed filter & seal. Grouted to 2' below ground surface.

REMARKS.

Well developed by pumping ~3,260 gallons of water from well & surging.



CLIENT USEPA - Region VII		PROJECT Ace Services Site	PROJECT NO. 4818
PROJECT LOCATION Colby, KS	COORDINATES N 9441.91718' E 10347.99760'	TOP OF RISER ELEVATION (DATUM) 3141.30' (msl)	DATE 7/11/00
STRATUM MONITORED Clayey SAND		LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith	



METHOD OF INSTALLATION.

Boring drilled to completion, set riser pipe & screen, placed filter & seal. Grouted to 2' below ground surface.

REMARKS.

Well developed by pumping ~12,375 gallons of water from well & surging.

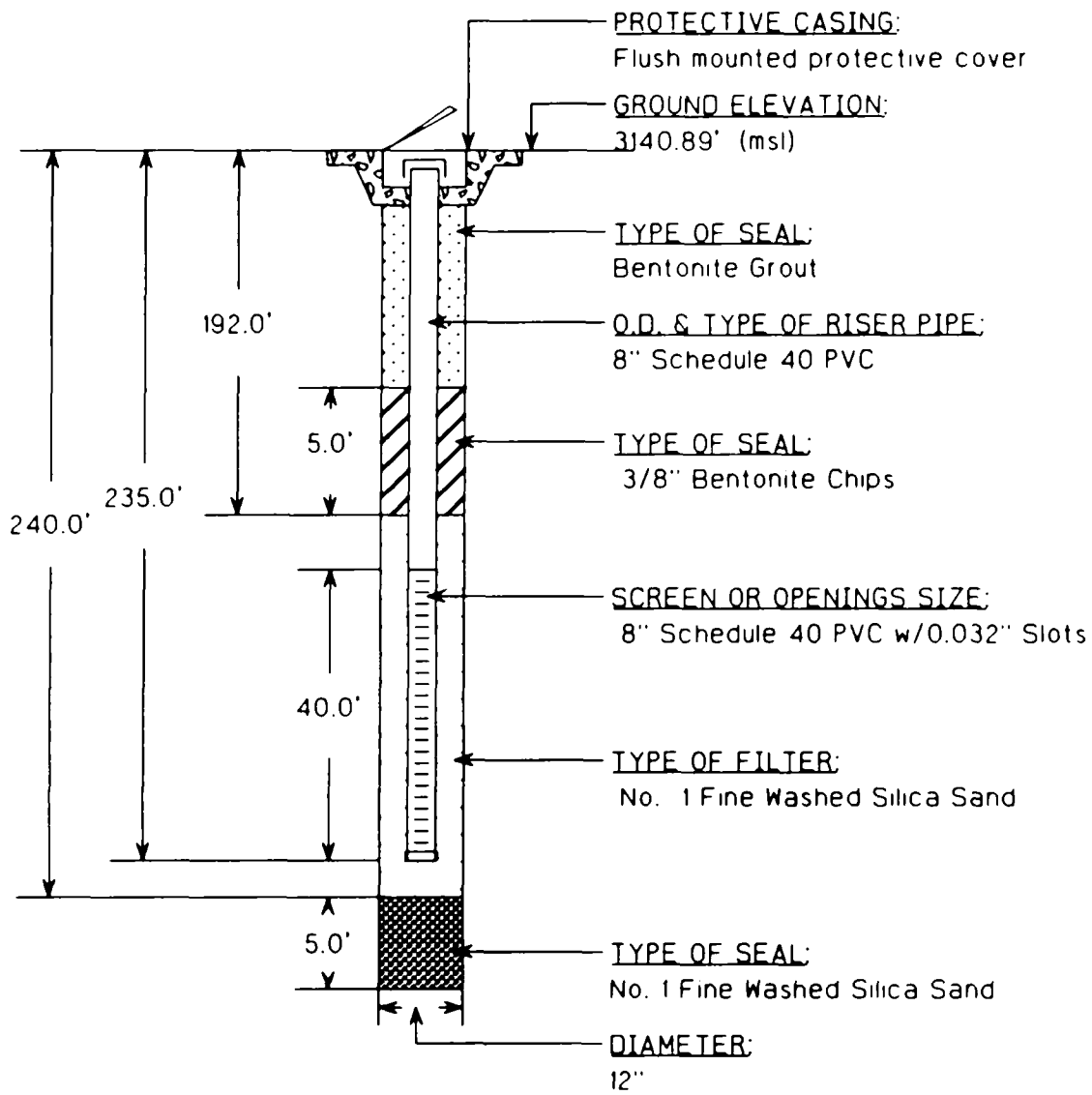


BLACK & VEATCH

WELL INSTALLATION LOG

NO. EX-2-D

CLIENT USEPA - Region VII		PROJECT Ace Services Site		PROJECT NO. 4818
PROJECT LOCATION Colby, KS		COORDINATES N 9434.31623' E 10358.43995'	TOP OF RISER ELEVATION (DATUM) 3140.50' (msl)	DATE 7/10/00
STRATUM MONITORED Clayey SAND, Gravelly SAND			LOGGED BY G. Felkner	
CHECKED BY B. Smith		APPROVED BY B. Smith		



METHOD OF INSTALLATION:
Boring drilled to completion, set riser pipe & screen; placed filter & seal. Grouted to 2' below ground surface.

REMARKS:
Well developed by pumping ~19,500 gallons of water from well & surging.

Appendix C
Well Development/Purging Data Sheets

Black & Veatch Special Projects Corp. MONITORING WELL DEVELOPMENT/BURGING DATA		Page <u>1</u> of <u>1</u>																																																																																																																								
Project Number <u>46118.123</u>	Project Name <u>Acc Services</u>	Date <u>7-18-00</u>																																																																																																																								
Monitor Well Number <u>OB-1-S</u>	Field Investigator(s) <u>G. Felker</u>																																																																																																																									
WELL DATA INITIAL DEPTH <u>112.2'</u> <u>630</u> Total Depth <u>130'</u> Well Diameter <u>4"</u>		Water Column Height <u>17.8'</u> Well Volume (gals) <u>-12</u> (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"																																																																																																																								
METHOD OF WELL DEVELOPMENT <input checked="" type="checkbox"/> Pumping <input type="checkbox"/> Air Lift <input checked="" type="checkbox"/> Surging <input type="checkbox"/> Bailing		PHOTOGRAPH IDENTIFICATION NO.																																																																																																																								
WATER SAMPLING DATA Method of Water Removal <u>submersible pump</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>																																																																																																																										
Well Volumes <u>36</u> gals		Amount of Water Removed from Well <u>2525</u> gals																																																																																																																								
FINAL FIELD ANALYSIS Water Temp _____ °C Specific Conductance _____ microhohes pH _____ Turbidity _____ Physical Appearance <u>slight greenish tint</u>																																																																																																																										
Remarks <u>High range Hexi Co field test kit = 450 ppb</u>																																																																																																																										
<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>TIME</th> <th>Temp °C</th> <th>Conductivity</th> <th>pH</th> <th>NTU</th> <th>WL</th> <th>In. tid Removed x10</th> <th>Flow Rate</th> <th>DO</th> <th>ORP</th> </tr> </thead> <tbody> <tr> <td><u>1300</u></td> <td><u>Start</u></td> <td><u>pumping</u></td> <td><u>-</u></td> <td><u>turbid</u></td> <td><u>112.2</u></td> <td><u>0</u></td> <td><u>25 gpm</u></td> <td><u>-</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1330</u></td> <td><u>15.5</u></td> <td><u>717</u></td> <td><u>6.8</u></td> <td><u>44</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>"</u></td> <td><u>10.1</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1340</u></td> <td><u>15.6</u></td> <td><u>722</u></td> <td><u>7.0</u></td> <td><u>20</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>"</u></td> <td><u>10.0</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1355</u></td> <td><u>15.5</u></td> <td><u>726</u></td> <td><u>6.9</u></td> <td><u>21</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>"</u></td> <td><u>10.1</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1410</u></td> <td><u>15.6</u></td> <td><u>729</u></td> <td><u>6.9</u></td> <td><u>6</u></td> <td><u>-</u></td> <td><u>-1750</u></td> <td><u>"</u></td> <td><u>10.4</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1415</u></td> <td><u>15.6</u></td> <td><u>729</u></td> <td><u>6.9</u></td> <td><u>7</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>"</u></td> <td><u>10.1</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1417</u></td> <td><u>Surge</u></td> <td><u>well</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1430</u></td> <td><u>15.6</u></td> <td><u>743</u></td> <td><u>6.8</u></td> <td><u>29</u></td> <td><u>-</u></td> <td><u>-2250</u></td> <td><u>"</u></td> <td><u>10.3</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1435</u></td> <td><u>15.6</u></td> <td><u>740</u></td> <td><u>6.9</u></td> <td><u>9</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>"</u></td> <td><u>10.4</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1440</u></td> <td><u>15.6</u></td> <td><u>740</u></td> <td><u>6.9</u></td> <td><u>7</u></td> <td><u>-</u></td> <td><u>-2525</u></td> <td><u>"</u></td> <td><u>10.4</u></td> <td><u>-</u></td> </tr> <tr> <td><u>1441</u></td> <td><u>Stop</u></td> <td><u>pumping</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> <td><u>-</u></td> </tr> </tbody> </table>			TIME	Temp °C	Conductivity	pH	NTU	WL	In. tid Removed x10	Flow Rate	DO	ORP	<u>1300</u>	<u>Start</u>	<u>pumping</u>	<u>-</u>	<u>turbid</u>	<u>112.2</u>	<u>0</u>	<u>25 gpm</u>	<u>-</u>	<u>-</u>	<u>1330</u>	<u>15.5</u>	<u>717</u>	<u>6.8</u>	<u>44</u>	<u>-</u>	<u>-</u>	<u>"</u>	<u>10.1</u>	<u>-</u>	<u>1340</u>	<u>15.6</u>	<u>722</u>	<u>7.0</u>	<u>20</u>	<u>-</u>	<u>-</u>	<u>"</u>	<u>10.0</u>	<u>-</u>	<u>1355</u>	<u>15.5</u>	<u>726</u>	<u>6.9</u>	<u>21</u>	<u>-</u>	<u>-</u>	<u>"</u>	<u>10.1</u>	<u>-</u>	<u>1410</u>	<u>15.6</u>	<u>729</u>	<u>6.9</u>	<u>6</u>	<u>-</u>	<u>-1750</u>	<u>"</u>	<u>10.4</u>	<u>-</u>	<u>1415</u>	<u>15.6</u>	<u>729</u>	<u>6.9</u>	<u>7</u>	<u>-</u>	<u>-</u>	<u>"</u>	<u>10.1</u>	<u>-</u>	<u>1417</u>	<u>Surge</u>	<u>well</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>1430</u>	<u>15.6</u>	<u>743</u>	<u>6.8</u>	<u>29</u>	<u>-</u>	<u>-2250</u>	<u>"</u>	<u>10.3</u>	<u>-</u>	<u>1435</u>	<u>15.6</u>	<u>740</u>	<u>6.9</u>	<u>9</u>	<u>-</u>	<u>-</u>	<u>"</u>	<u>10.4</u>	<u>-</u>	<u>1440</u>	<u>15.6</u>	<u>740</u>	<u>6.9</u>	<u>7</u>	<u>-</u>	<u>-2525</u>	<u>"</u>	<u>10.4</u>	<u>-</u>	<u>1441</u>	<u>Stop</u>	<u>pumping</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>
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WATER SAMPLING DATA Method of Water Removal <u>submersible pump</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> Well Volume <u>165</u> gals Amount of Water Removed from Well <u>~5115</u> gals																																																																																																																																				
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WELL DATA INITIAL DEPTH <u>113.82' bgs</u> Total Depth <u>225'</u> Well Diameter <u>4"</u>		Water Column Height <u>121.18'</u> Well Volume (gals) <u>80 gals</u> (x)(height) x=.163 gal/ft @ 2", x=.655 gal/ft @ 4"																																																																																																																																		
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Monitor Well Number <u>OB-2-5</u>	Field Investigator(s) <u>G. Felker</u>																																																																																																													
WELL DATA INITIAL DEPTH <u>108.8'</u> Total Depth <u>130.0'</u> Well Diameter <u>4"</u>		Water Column Height <u>21.2'</u> Well Volume (gals) <u>~14</u> (x)(height) x=.163 gal/ft @ 2". x=.633 gal/ft @ 4"																																																																																																												
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<u>1645</u>	<u>Stop Pump</u>					<u>-12,375</u>																																																																																																																				
NTU = Nephelometric turbidity units WL = Water level																																																																																																																										
Checked By <u>Af</u>	Date <u>8-3-00</u>																																																																																																																									

Black & Veatch Special Projects Corp.		Page 1 of 4																																																																																																																																																																
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Project Number 446118.123	Project Name Hex Services	Date 7-14-00																																																																																																																																																																
Monitor Well Number EX-2-D	Field Investigator(s) G. Felkner																																																																																																																																																																	
WELL DATA INITIAL DEPTH <u>110.35' bgs</u> Total Depth <u>235.0'</u> Well Diameter <u>8"</u>		Water Column Height <u>124.65'</u> Well Volume (gals) (x)(height) x=.163 gal/ft @ 2". x=.653 gal/ft @ 4"																																																																																																																																																																
METHOD OF WELL DEVELOPMENT <input checked="" type="checkbox"/> Pumping <input type="checkbox"/> Air Lift <input checked="" type="checkbox"/> Surging <input type="checkbox"/> Bailing		PHOTOGRAPH IDENTIFICATION NO.																																																																																																																																																																
WATER SAMPLING DATA Method of Water Removal <u>submersible pump</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>																																																																																																																																																																		
Well Volumes _____ gals		Amount of Water Removed from Well <u>19,500</u> gals																																																																																																																																																																
FINAL FIELD ANALYSIS Water Temp <u>15</u> °C Specific Conductance <u>472</u> micromhos pH <u>7.2</u> Turbidity <u>0.5</u> Physical Appearance <u>Greenish Tint, Hex Co. field test kit = 1.5 mg/L C.</u>																																																																																																																																																																		
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Checked By A+	Date 8-3-00																																																																																																																																																																	

MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Acc Services Date 09-19-00

Monitor Well Number MW-1-S Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH 10200' Water Column Height 18'
 Total Depth 125' Well Volume (gals) ~12 gals
 Well Diameter 4" (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purge
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes NA gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS
 Water Temp 19.86 °C Specific Conductance 1248 micromhos pH 6.80 Turbidity 2.5
 Physical Appearance Normal

Remarks Micro purge

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1030	measured	depth to water	at	107.00					
1040	pumping	started and flow	adjusted to	~10 L/min				3.67	146.0
1051	18.39	1155	6.67	4.4	107.06			3.67	146.0
1057	19.64	1231	6.72	4.3	107.06			2.8	143
1103	19.96	1252	6.75	3.0	107.06			1.7	95.6
1110	19.76	1244	6.73	2.6	107.07			1.53	89.8
1118	19.64	1242	6.72	1.8	107.06			1.21	89.4
1127	19.86	1248	6.80	2.5	107.07			1.14	76.8
1129	Sampled water w/ MW-1-S-091900-P (total Cr)								

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AF Date 9-26-00

Black & Veatch Special Projects Corp.		Page 1 of 1																																																																																																																																		
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Monitor Well Number MW-1-I MW-1-I	Field Investigator(s) Kyle Madden																																																																																																																																			
WELL DATA INITIAL DEPTH <u>107.07'</u> Water Column Height _____ Total Depth <u>162'</u> Well Volume (gals) _____ (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4" Well Diameter <u>4"</u>																																																																																																																																				
METHOD OF WELL DEVELOPMENT <input checked="" type="checkbox"/> Pumping <input type="checkbox"/> Air Lift <input type="checkbox"/> Surging <input type="checkbox"/> Bailing																																																																																																																																				
WATER SAMPLING DATA <u>Micro-Purge</u> Method of Water Removal <u>Pumping</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> 3 Well Volumes <u>NA</u> gals Amount of Water Removed from Well <u>NA</u> gals																																																																																																																																				
FINAL FIELD ANALYSIS Water Temp <u>19.10</u> °C Specific Conductance <u>1111</u> micromhos pH <u>6.73</u> Turbidity <u>0.9</u> Physical Appearance <u>Normal</u>																																																																																																																																				
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Checked By <u>AF</u>	Date <u>9-26-00</u>																																																																																																																																			

**MONITORING WELL
DEVELOPMENT/PURGING DATA**

Project Number 11/0118 Project Name Ace Services Date 09-19-00

Monitor Well Number MW-1-D Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH 106.56 Water Column Height _____
 Total Depth 220 Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 5"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping _____ Air Lift _____
 Surging _____ Bailing _____

WATER SAMPLING DATA Micro-Purge
 Method of Water Removal pumping Was Well Pumped Dry? Yes No

3 Well Volumes _____ gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS
 Water Temp 17.62 °C Specific Conductance 428 micromhos pH 7.38 Turbidity 2.8
 Physical Appearance Normal

Remarks None

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>0910</u>	<u>16.53</u>	<u>418</u>	<u>7.15</u>	<u>6.3</u>	<u>106.56</u>	<u>PI</u>			
<u>0918</u>	<u>17.84</u>	<u>430</u>	<u>7.27</u>	<u>5.2</u>	<u>106.79</u>			<u>7.88</u>	<u>183.8</u>
<u>0925</u>	<u>17.69</u>	<u>429</u>	<u>7.27</u>	<u>4.3</u>	<u>106.79</u>			<u>7.76</u>	<u>122.4</u>
<u>0929</u>	<u>17.64</u>	<u>430</u>	<u>7.29</u>	<u>3.1</u>	<u>106.80</u>			<u>7.79</u>	<u>116.0</u>
<u>0937</u>	<u>17.70</u>	<u>429</u>	<u>7.29</u>	<u>2.3</u>	<u>106.79</u>			<u>7.80</u>	<u>102.0</u>
<u>0944</u>	<u>17.62</u>	<u>428</u>	<u>7.38</u>	<u>2.8</u>	<u>106.81</u>			<u>7.82</u>	<u>96.5</u>
<u>0952</u>								<u>7.93</u>	<u>93.6</u>
<u>0953</u>	<u>Sampled water w-MW-1-D-091900-P (total C)</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By DS Date 9-26-00

Black & Veatch Special Projects Corp.		Page (of (
MONITORING WELL DEVELOPMENT/PURGING DATA																																																																																																																										
Project Number <u>46118</u>	Project Name <u>Ace Services</u>	Date <u>9-22-00</u>																																																																																																																								
Monitor Well Number <u>MW-2-S</u>	Field Investigator(s) <u>Kyle Madden</u>																																																																																																																									
WELL DATA INITIAL DEPTH <u>102.49</u> Water Column Height _____ Total Depth <u>123</u> Well Volume (gals) _____ (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4" Well Diameter <u>4"</u>																																																																																																																										
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Black & Veatch Special Projects Corp. Page 1 of 1

MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ace Services Date 09/18/00

Monitor Well Number MW-2-I Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH 102.80' Water Column Height _____
 Total Depth 193' Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping _____ Air Lift _____
 Surging _____ Bailing _____

WATER SAMPLING DATA Micro-Purge
 Method of Water Removal Pumping Was Well Pumped Dry? Yes No

3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance Green in color

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1600	depth to water initially measured at				102.80				
1606	- starting	pumping - adjusted	flow rate to 1.0 L/min						
1614	19.72	751	5.48	8.7	102.82			2.10	309.5
1622	19.53	725	5.40	13.7	102.82			1.86	215.6
1629	18.92	693	5.42	8.0	102.82			2.10	73.8
1636	18.39	680	5.93	5.3	102.84			2.35	93.8
1644	17.64	660	4.96	1.9	102.84			2.19	157.1
1646	Samples collected W-MW-2-I-091800-P (1 total Cr, 1 Cr ⁶⁺)								
1649	15 Gallons collected for treatability study								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AF Date 9-26-00

Black & Veatch Special Projects Corp. MONITORING WELL DEVELOPMENT/PURGING DATA		Page <u>1</u> of <u>1</u>																																																																																																																																		
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**MONITORING WELL
DEVELOPMENT/PURGING DATA**

Project Number
46118

Project Name
Ace Services

Date
9-22-00

Monitor Well Number
mw-3-D

Field Investigator(s)
G. Felton

WELL DATA

INITIAL DEPTH 104.91' STOC

Water Column Height ~115'

Total Depth 220'

Well Volume (gals) ~117.3 gal

Well Diameter 5"

(x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
y=1.02 gal/ft @ 5"

METHOD OF WELL DEVELOPMENT

PHOTOGRAPH IDENTIFICATION NO.

Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA

Method of Water Removal Submersible Pump Was Well Pumped Dry? Yes No

3 Well Volumes ~352 gals Amount of Water Removed from Well 465 gals

FINAL FIELD ANALYSIS

Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____

Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1116	Initial	W.L.			104.91'				
1140	Started	pumping					15.5 gpm		
1151	14.9	408	7.4	0				7.33	212
1155	14.9	409	7.4	0				7.23	212
1200	14.9	409	7.4	0				7.23	211
1203	14.9	410	7.4	0				7.22	211
1206	14.9	410	7.4	0				7.21	210
1209	14.9	410	7.4	0		465 gal.		7.21	210
1210	Collect	sample							

NTU = Nephelometric turbidity units
WL = Water level

Checked By JS

Date 9-26-00

Black & Veatch Special Projects Corp.		Page 1 of 1																																																																																																																																		
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**MONITORING WELL
DEVELOPMENT (PURGING DATA)**

Project Number 46118 Project Name Ace Services Date 09-19-00

Monitor Well Number MW-4-D Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH 98.68 Water Column Height _____
 Total Depth 229 Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA micro-purge
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance normal

Remarks None

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1359					98.68'				
1420						1.0 L/min	1.0 L/min		
1426	17.37	424	7.18	8.9	99.67			7.72	196.3
1435	16.78	419	7.14	11.5	98.70			7.72	193.0
1445	17.49	431	7.13	14.8	98.69			7.61	144.8
1454	17.88	436	7.09	7.3	98.68			7.64	114.1
1501	18.11	440	7.02	6.3	98.67			7.60	111.2
1509	18.07	442	6.89	7.2	98.66			7.56	124.4
1515	18.36	446	6.97	7.9	98.66			7.95	121.4
1516									

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AS Date 9-26-00

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Method of Water Removal <u>Submersible Pump</u>	Was Well Pumped Dry?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>																																																																																																																																		
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1411	Initial	W.L.	—	—	100.59'	—	—	—	—																																																																																																																											
1440	Start	Pumping	—	—	—	—	15 gpm	—	—																																																																																																																											
1450	15.3	720	7.3	45	(air in with, reduce flow)	—	—	6.28	233																																																																																																																											
1455	15.3	—	—	—	—	—	↓	—	—																																																																																																																											
1500	15.5	722	7.3	1.1	—	300 gals	5.6 gpm	6.98	225																																																																																																																											
1505	15.5	736	7.3	3.1	—	—	↓	6.91	222																																																																																																																											
1507	15.4	735	7.3	1.6	—	—	↓	6.88	221																																																																																																																											
1508	15.4	733	7.3	0	—	356 gals	↓	6.87	219																																																																																																																											
1510	Collected sample and duplicate	—	—	—	—	—	—	—	—																																																																																																																											
NTU = Nephelometric turbidity units WL = Water level																																																																																																																																				
Checked By <u>AS</u>	Date <u>9-26-00</u>																																																																																																																																			

**MONITORING WELL
DEVELOPMENT/PURGING DATA**

Project Number 46118	Project Name Ace Services	Date 09-18-00
Monitor Well Number MW-5-I	Field Investigator(s) Kyle Madden	

WELL DATA

INITIAL DEPTH 100.56' Water Column Height _____
 Total Depth 185' Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT **PHOTOGRAPH IDENTIFICATION NO.**

Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purging

Method of Water Removal Pumping Was Well Pumped Dry? Yes No

3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS

Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____

Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
131400		<u>measured water depth at 100.56 feet</u>							
1407		<u>started pumping well - adjusted Flow to 1.0 L/min</u>							
1413	<u>20.67</u>	<u>570.00</u>	<u>6.72</u>	<u>6.3</u>				<u>7.43</u>	<u>198.6</u>
1419	<u>19.98</u>	<u>567.0</u>	<u>6.56</u>	<u>10.5</u>				<u>7.33</u>	<u>156.3</u>
1425	<u>22.6</u>	<u>602</u>	<u>6.78</u>	<u>8.7</u>	<u>100.56</u>			<u>7.24</u>	<u>143.3</u>
1431	<u>24.7</u>	<u>630</u>	<u>6.92</u>	<u>7.6</u>	<u>100.56</u>			<u>7.15</u>	<u>144.1</u>
1433-1440	<u>Pump lost prime - restart & adjust to 1.0 L/min</u>								
1445	<u>20.38</u>	<u>577.0</u>	<u>6.43</u>	<u>15.3</u>	<u>100.58</u>			<u>7.22</u>	<u>71.5</u>
1450	<u>20.03</u>	<u>571.00</u>	<u>6.37</u>	<u>13.2</u>	<u>100.60</u>			<u>7.25</u>	<u>81.3</u>
1456	<u>19.16</u>	<u>559</u>	<u>6.23</u>	<u>8.5</u>	<u>100.60</u>			<u>7.30</u>	<u>102.5</u>
1500	<u>18.66</u>	<u>551</u>	<u>6.12</u>	<u>4.4</u>	<u>100.60</u>			<u>7.33</u>	<u>112.5</u>
1503	<u>collected W-MW-5-I-091800-P (2 bottles - 1 Cr6, 1 total Cr)</u>								
1505	<u>started collecting 30 gallons for treatability study</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AS Date 9-26-00

Black & Veatch Special Projects Corp. Page 1 of 1

MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118	Project Name Ace Services	Date 9-21-00
Monitor Well Number mw-5-D mw-5-D	Field Investigator(s) G. Felker	

WELL DATA
 INITIAL DEPTH 103.20' Water Column Height 127'
 Total Depth 230' Well Volume (gals) 83 gals
 (x)(height) x=.163 gal/ft @ 2', x=.653 gal/ft @ 4'
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal Pumping Was Well Pumped Dry? Yes No
 3 Well Volumes 250 gals Amount of Water Removed from Well 465 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1120	Initial	W.L.	—	—	103.20	—	—	—	—
1131	Start	Pumping	—	—	—	—	14.1 gpm	—	—
1146	15.5	409	7.44	0	—	—	—	8.0	203
1145	15.5	416	7.44	0	—	—	—	8.0	202
1150	15.5	419	7.44	0	—	—	—	8.0	200
1155	15.5	420	7.44	0	—	—	—	8.0	199
1200	15.5	421	7.44	0	—	—	—	8.0	199
1204	15.5	422	7.44	0	—	465 gal	↓	7.98	199
1205	Collected	sample	—	—	—	—	—	—	—

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AF Date 9-26-00

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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ace Services Date 09/20/00

Monitor Well Number MW-6-S Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH ~~106.73~~ 104.73 Water Column Height _____
 Total Depth 132 Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purging
 Method of Water Removal Pumping Was Well Pumped Dry? Yes No

3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance Slightly colored

Remarks Lots of PVC shavings coming up into monitor - turbidity measured in drinking water (Culligan water) as ~0.8

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1222	Initial measurement of depth to water = <u>104.73</u>				<u>106.73</u>				
1237	Started pumping - adjusted flow rate to <u>1.0 L/min</u>				<u>104.73</u>		<u>1.0 L/min</u>		
1249	<u>17.32</u>	<u>517</u>	<u>7.30</u>	<u>64.7</u>	<u>104.87</u>			<u>7.50</u>	<u>130.1</u>
1257	<u>18.03</u>	<u>519</u>	<u>7.30</u>	<u>57.8</u>	<u>104.86</u>			<u>7.58</u>	<u>126.7</u>
1308	<u>20.41</u>	<u>546</u>	<u>7.39</u>	<u>40.8</u>	<u>104.88</u>			<u>7.71</u>	<u>77.0</u>
1314	<u>20.54</u>	<u>549</u>	<u>7.42</u>	<u>34.9</u>	<u>104.90</u>			<u>7.65</u>	<u>67.3</u>
1323	<u>20.33</u>	<u>547</u>	<u>7.44</u>	<u>24.6</u>	<u>104.90</u>			<u>7.71</u>	<u>63.1</u>
1332	<u>20.17</u>	<u>549</u>	<u>7.41</u>	<u>18.5</u>	<u>104.90</u>			<u>7.60</u>	<u>66.8</u>
1338	<u>19.77</u>	<u>544</u>	<u>7.39</u>	<u>17.1</u>	<u>104.89</u>			<u>7.62</u>	<u>69.6</u>
1340	Sample collected w-MW-6-S-092000-P								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By DM Date 9-26-00

MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number <u>4618</u>	Project Name <u>Ace Services</u>	Date <u>09-20-00</u>
Monitor Well Number <u>MW-6-I</u>	Field Investigator(s) <u>Kyle Madden</u>	

WELL DATA

INITIAL DEPTH 105.00 Water Column Height _____
 Total Depth 190 Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2". x=.653 gal/ft @ 4"

Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____

Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro Purging

Method of Water Removal pumping Was Well Pumped Dry? Yes No

3 Well Volumes _____ gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS

Water Temp 17.84 °C Specific Conductance 754 microhos pH 7.11 Turbidity 8.2

Physical Appearance Normal

Remarks none

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>0848</u>	<u>initial measurement depth to water</u>				<u>105.00</u>				
<u>0900</u>	<u>starting pumping - adjusted flow to</u>				<u>1.0 L/min</u>		<u>1.0 L/min</u>		
<u>0941</u>	<u>16.87</u>	<u>764</u>	<u>7.09</u>	<u>7.2</u>	<u>105.05</u>			<u>5.73</u>	<u>110.0</u>
<u>0949</u>	<u>17.03</u>	<u>766</u>	<u>7.09</u>	<u>7.6</u>	<u>105.08</u>			<u>5.69</u>	<u>109.6</u>
<u>0957</u>	<u>16.96</u>	<u>756</u>	<u>7.10</u>	<u>7.2</u>	<u>105.02</u>			<u>5.65</u>	<u>92.9</u>
<u>1006</u>	<u>17.17</u>	<u>754</u>	<u>7.10</u>	<u>8.2</u>	<u>105.02</u>			<u>5.85</u>	<u>84.7</u>
<u>1017</u>	<u>17.61</u>	<u>754</u>	<u>7.11</u>	<u>9.2</u>	<u>105.01</u>			<u>5.86</u>	<u>81.0</u>
<u>1022</u>	<u>17.70</u>	<u>754</u>	<u>7.11</u>	<u>8.0</u>	<u>105.01</u>			<u>5.74</u>	<u>81.0</u>
<u>1026</u>	<u>17.84</u>	<u>754</u>	<u>7.11</u>	<u>8.2</u>	<u>105.01</u>			<u>5.76</u>	<u>80.6</u>
<u>1028</u>	<u>1 sample collected W-MW-6-I-051600-P (Total Cr)</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AX Date 9-26-00

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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number <u>46118</u>	Project Name <u>Ace Services</u>	Date <u>09/06/00</u>
Monitor Well Number <u>MW-6-D</u>	Field Investigator(s) <u>Kyle Madden</u>	

WELL DATA

INITIAL DEPTH 106.17' Water Column Height _____
 Total Depth 237' Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2". x=.653 gal/ft @ 4"

Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____

Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purging

Method of Water Removal Pumping Was Well Pumped Dry? Yes No

3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS

Water Temp 17.04 °C Specific Conductance 551 micromhos pH 7.41 Turbidity 4.9

Physical Appearance Normal

Remarks None

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>1101042</u>	<u>Initial Depth to water =</u>				<u>106.17</u>				
<u>1050</u>	<u>Started pumping - flow rate adjusted to ~1.0 g/min</u>						<u>~1.04/min</u>		
<u>1108</u>	<u>15.42</u>	<u>474</u>	<u>7.33</u>	<u>9.2</u>	<u>106.15</u>			<u>7.02</u>	<u>121.7</u>
<u>1113</u>	<u>16.46</u>	<u>489</u>	<u>7.36</u>	<u>15.3</u>	<u>106.16</u>			<u>6.90</u>	<u>101.9</u>
<u>1118</u>	<u>17.27</u>	<u>520</u>	<u>7.39</u>	<u>11.4</u>	<u>106.14</u>			<u>6.79</u>	<u>85.8</u>
<u>1124</u>	<u>17.11</u>	<u>556</u>	<u>7.36</u>	<u>8.3</u>	<u>106.15</u>			<u>6.60</u>	<u>78.0</u>
<u>1131</u>	<u>17.05</u>	<u>554</u>	<u>7.35</u>	<u>6.2</u>	<u>106.17</u>			<u>6.62</u>	<u>77.7</u>
<u>1136</u>	<u>17.17</u>	<u>554</u>	<u>7.35</u>	<u>5.5</u>	<u>106.16</u>			<u>6.63</u>	<u>77.8</u>
<u>1140</u>	<u>17.04</u>	<u>551</u>	<u>7.41</u>	<u>4.9</u>	<u>106.17</u>			<u>6.70</u>	<u>75.4</u>
<u>1141</u>	<u>collected W-MW-6-D-092000-P (total cr)</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AS Date 7-26-00

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Monitor Well Number MU-7-S	Field Investigator(s) G. Felton																																																																																																																																													
WELL DATA INITIAL DEPTH <u>116.85'</u> Water Column Height <u>23'</u> Total Depth <u>140'</u> Well Volume (gals) <u>-15 gals</u> Well Diameter <u>4"</u> (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"																																																																																																																																														
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WATER SAMPLING DATA Method of Water Removal <u>Submersible pump</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> 3 Well Volumes <u>-45</u> gals Amount of Water Removed from Well <u>480</u> gals																																																																																																																																														
FINAL FIELD ANALYSIS Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____ Physical Appearance _____ Remarks _____																																																																																																																																														
<table border="1" style="width:100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>TIME</th> <th>Temp °C</th> <th>Conductivity</th> <th>pH</th> <th>NTUs</th> <th>WL</th> <th>Removed</th> <th>Flow Rate</th> <th>DO</th> <th>ORP</th> </tr> </thead> <tbody> <tr> <td>1005</td> <td>Initial</td> <td>water level</td> <td>—</td> <td>—</td> <td>116.85'</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>1017</td> <td>Start</td> <td>pumping</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>15 gpm</td> <td>—</td> <td>—</td> </tr> <tr> <td>1032</td> <td>14.4</td> <td>578</td> <td>7.2</td> <td>0</td> <td>—</td> <td>—</td> <td>↓</td> <td>8.61</td> <td>221</td> </tr> <tr> <td>1035</td> <td>14.4</td> <td>577</td> <td>7.2</td> <td>0</td> <td>—</td> <td>—</td> <td>↓</td> <td>7.27</td> <td>222</td> </tr> <tr> <td>1038</td> <td>14.3</td> <td>576</td> <td>7.2</td> <td>0</td> <td>—</td> <td>—</td> <td>↓</td> <td>7.04</td> <td>222</td> </tr> <tr> <td>1042</td> <td>14.4</td> <td>577</td> <td>7.2</td> <td>0</td> <td>—</td> <td>—</td> <td>↓</td> <td>6.93</td> <td>221</td> </tr> <tr> <td>1047</td> <td>14.3</td> <td>576</td> <td>7.2</td> <td>0</td> <td>—</td> <td>—</td> <td>↓</td> <td>6.91</td> <td>221</td> </tr> <tr> <td>1049</td> <td>14.3</td> <td>576</td> <td>7.2</td> <td>0</td> <td>—</td> <td>480 gal</td> <td>—</td> <td>6.91</td> <td>222</td> </tr> <tr> <td>1050</td> <td>Collected</td> <td>sample</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>			TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP	1005	Initial	water level	—	—	116.85'	—	—	—	—	1017	Start	pumping	—	—	—	—	15 gpm	—	—	1032	14.4	578	7.2	0	—	—	↓	8.61	221	1035	14.4	577	7.2	0	—	—	↓	7.27	222	1038	14.3	576	7.2	0	—	—	↓	7.04	222	1042	14.4	577	7.2	0	—	—	↓	6.93	221	1047	14.3	576	7.2	0	—	—	↓	6.91	221	1049	14.3	576	7.2	0	—	480 gal	—	6.91	222	1050	Collected	sample	—	—	—	—	—	—	—																																								
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WATER SAMPLING DATA <u>Micro-Purgings</u> Method of Water Removal <u>pumping</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>																																																																																																																																																																												
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FINAL FIELD ANALYSIS Water Temp <u>20.02</u> °C Specific Conductance <u>566</u> micromhos pH <u>6.9</u> Turbidity <u>11.1</u> Physical Appearance <u>Normal</u>																																																																																																																																																																												
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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Aire Services Date 9-21-00

Monitor Well Number MW-8-D Field Investigator(s) G. Felker

WELL DATA
 INITIAL DEPTH ~~107.76~~ 107.76' Water Column Height ~131
 Total Depth 239 Well Volume (gals) ~86
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes ~250 gals Amount of Water Removed from Well 650 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance Greenish tint

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
0800	Initial	W.L.	—	—	107.76'	—	—	—	—
0820	Start	pumping	—	—	—	—	14.5 gpm	—	—
0827	15.1	532	7.0	0	—	—	↓	5.02	233
0859	15.1	532	7.2	0	—	—	↓	4.93	232
0901	15.1	532	7.3	0	—	—	↓	5.03	231
0903	15.1	532	7.3	0	—	—	↓	5.08	232
0904	15.1	532	7.3	0	—	~650 gals	↓	5.08	232
0905	Collect	Sample + Duplicate	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AS Date 9-26-00

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WELL DATA INITIAL DEPTH <u>111.98'</u> Water Column Height <u>-20'</u> Total Depth <u>132'</u> Well Volume (gals) <u>13 gal</u> Well Diameter <u>4"</u> (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"																																																																																																																										
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WATER SAMPLING DATA Method of Water Removal <u>pumping</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> 3 Well Volumes <u>39</u> gals Amount of Water Removed from Well <u>438</u> gals																																																																																																																										
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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number: 46118 Project Name: Acc Services Date: 9-19-00

Monitor Well Number: MW-9-I Field Investigator(s): G. Falkner

WELL DATA
 INITIAL DEPTH: 111.79' Water Column Height: ~80'
 Total Depth: 190 Well Volume (gals): -53
 Well Diameter: 4" (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

METHOD OF WELL DEVELOPMENT
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal: Pumping Was Well Pumped Dry? Yes No
 3 Well Volumes: -160 gals Amount of Water Removed from Well: ~480 gals

FINAL FIELD ANALYSIS
 Water Temp: _____ °C Specific Conductance: _____ micromhos pH: _____ Turbidity: _____
 Physical Appearance: Greenish tint

Remarks: _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	25 sec Removed	Flow Rate	DO	ORP
1600					111.79'				
1615	start	Pumping					12 gpm		
1640	15.3	591	7.4	2.1				4.71	204
1645	15.3	592	7.2	4.1				4.6	209
1647	15.2	592	7.2	6.9				4.6	211
1650	15.3	592	7.2	5.1				4.5	212
1653	15.3	592	7.2	0.9				4.5	214
1655	collected	sample				~480 gals			

NTU = Nephelometric turbidity units
 WL = Water level

Checked By: AS Date: 9-26-00

Project Number 46118 Project Name Ace Services Date 9-20-00

Monitor Well Number MW-9-D Field Investigator(s) G Folkner

WELL DATA
 INITIAL DEPTH 113.32' Water Column Height -123'
 Total Depth 236 Well Volume (gals) -81 gal
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes ~243 gals Amount of Water Removed from Well ~476 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance Greenish Tint

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
0820	Initial	W.L.	—	—	113.32'	—	—	—	—
0835	Start	pumping	—	—	—	—	13.6 gal	—	—
0857	15.3	552	7.2	0	—	—	—	4.4	220
0903	15.3	554	7.3	0	—	—	—	4.4	216
0906	15.3	554	7.3	0	—	—	—	4.4	217
0909	15.3	555	7.4	0	—	~476	—	4.4	217
0910	Collect	sample	—	—	—	—	—	—	—

NTU = Nephelometric turbidity units
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Checked By AF Date 9-26-00

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WELL DATA INITIAL DEPTH <u>119.66'</u> Total Depth <u>140</u> Well Diameter <u>4"</u>		Water Column Height <u>~20</u> Well Volume (gals) <u>13</u> (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"																																																																																																																																		
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Project Number 46118 Project Name Ace Services Date 9-21-00

Monitor Well Number MW-11-D Field Investigator(s) G. Felker

WELL DATA
 INITIAL DEPTH 122.37' Water Column Height 127'
 Total Depth -249 Well Volume (gals) ~83 gal
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes ~250 gals Amount of Water Removed from Well ~400 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____

Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL ^{16 sec.}	Removed	Flow Rate	DO	ORP
0944	Initial	Water Level			122.37'				
1000	Start	pumping					11.5 gpm		
1018	15.3	466	7.4	0				7.4	207
1025	15.3	466	7.5	0				7.26	211
1027	15.3	466	7.4	0				7.26	211
1030	15.4	466	7.4	0				7.26	212
1034	15.4	466	7.4	0		~400 gal		7.25	213
1035	Collected	sample							

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AF Date 9-26-00

Black & Veatch Special Projects Corp.		Page 1 of 1																																																																																																														
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Project Number 46118 Project Name ACE Services Date 9/18/00

Monitor Well Number MW12-I Field Investigator(s) Madden / Felkner

WELL DATA
 INITIAL DEPTH 143.42' Water Column Height 113.42 68'
 Total Depth 211' Well Volume (gals) 44.4
 Well Diameter 4" (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes 133 gals Amount of Water Removed from Well 540 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
0830	In. J. d	W.L. 143.42'			143.42'				
0835	Start	pumping				0	12 gpm		
0935	15.1	437	7.2	0				8.32	234
0940	15.2	439	7.3	0				7.6	221
0951	15.2	440	7.3	0				7.6	194
0900	15.2	440	7.4	0					
1010	15.2	442	7.4	0		540 gals	12 gpm	7.5	192
1010	Collected	sample							

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AS Date 9-26-00

Black & Veatch Special Projects Corp.		Page 1 of 1																																																																																																																																																																
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<p>WELL DATA</p> <p>INITIAL DEPTH <u>144.87'</u> Water Column Height <u>~118'</u> Total Depth <u>263'</u> Well Volume (gals) <u>~78'</u> Well Diameter <u>4"</u> (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"</p> <p>METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.</p> <p><input checked="" type="checkbox"/> Pumping <input type="checkbox"/> Air Lift <input type="checkbox"/> Surging <input type="checkbox"/> Bailing</p> <p>WATER SAMPLING DATA</p> <p>Method of Water Removal <u>Pumping</u> Was Well Pumped Dry? Yes <u>No</u></p> <p>3 Well Volumes <u>~234</u> gals Amount of Water Removed from Well <u>~350</u> gals</p> <p>FINAL FIELD ANALYSIS</p> <p>Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____</p> <p>Physical Appearance <u>Clear</u></p> <p>Remarks _____</p>																																																																																																																																																																		
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Black & Veatch Special Projects Corp.		Page 1 of 1							
MONITORING WELL DEVELOPMENT/PURGING DATA									
Project Number 46118	Project Name Ace Services	Date 09-20-00							
Monitor Well Number ACE-R-5	Field Investigator(s) Kyle Madden								
WELL DATA									
INITIAL DEPTH <u>103.99</u> ^{water malfunction at 8.5'}	Water Column Height _____								
Total Depth <u>125-135 (shallow screen)</u>	Well Volume (gals) _____ (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"								
Well Diameter <u>5"</u>									
METHOD OF WELL DEVELOPMENT									
<input checked="" type="checkbox"/> Pumping	<input type="checkbox"/> Air Lift	PHOTOGRAPH IDENTIFICATION NO. _____							
<input type="checkbox"/> Surging	<input type="checkbox"/> Bailing								
WATER SAMPLING DATA <u>Micro-Purging</u>									
Method of Water Removal <u>pumping</u>	Was Well Pumped Dry?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>							
3 Well Volumes <u>NA</u> gals	Amount of Water Removed from Well <u>NA</u> gals								
FINAL FIELD ANALYSIS									
Water Temp <u>16.98</u> °C	Specific Conductance <u>1015</u> microhos	pH <u>6.83</u> Turbidity <u>11.6</u>							
Physical Appearance <u>slightly green</u>									
Remarks <u>Some bubbles (pump cavitation?) periodically</u>									
TIME									
<u>1645</u>	<u>Temp °C</u>	<u>Conductivity</u>	<u>pH</u>	<u>NTUs</u>	<u>WL</u>	<u>Removed</u>	<u>Flow Rate</u>	<u>DO</u>	<u>ORP</u>
<u>Initial</u>	<u>depth to water measured at</u>				<u>103.99</u>				
<u>1652</u>	<u>pumping started - flow rate adjusted to 1.04/min.</u>						<u>~1.04/min.</u>		
<u>1702</u>	<u>16.96</u>	<u>964</u>	<u>6.85</u>	<u>15.9</u>	<u>103.99</u>		<u>~1.04/min.</u>	<u>0.85</u>	<u>180.1</u>
<u>1708</u>	<u>16.96</u>	<u>991</u>	<u>6.83</u>	<u>16.2</u>	<u>104.00</u>		<u>~1.04/min.</u>	<u>0.71</u>	<u>153.4</u>
<u>1715</u>	<u>17.12</u>	<u>1059</u>	<u>6.82</u>	<u>13.7</u>	<u>104.00</u>		<u>~1.04/min.</u>	<u>5.81</u>	<u>29.7</u>
<u>1722</u>	<u>6.86</u>	<u>1057</u>	<u>6.84</u>	<u>10.4</u>	<u>104.00</u>		<u>~1.04/min.</u>	<u>2.27</u>	<u>45.2</u>
<u>1727</u>	<u>16.89</u>	<u>1048</u>	<u>6.84</u>	<u>16.2</u>	<u>103.99</u>		<u>~1.04/min.</u>	<u>0.70</u>	<u>111.2</u>
<u>1732</u>	<u>16.81</u>	<u>1030</u>	<u>6.86</u>	<u>9.4</u>	<u>104.00</u>		<u>~1.04/min.</u>	<u>1.60</u>	<u>106.7</u>
<u>1737</u>	<u>16.98</u>	<u>1015</u>	<u>6.88</u>	<u>11.6</u>	<u>104.00</u>		<u>~1.04/min.</u>	<u>0.73</u>	<u>103.2</u>
<u>1738</u>	<u>collected 1 total cr sample - W-ACE-R-5-092000-P</u>								
NTU = Nephelometric turbidity units									
WL = Water level									
Checked By <u>JS</u>							Date <u>9-26-00</u>		

Project Number 76118 Project Name Ace Services Date 09-20-00

Monitor Well Number ACE-R-I Field Investigator(s) Kyle Mueller

WELL DATA
 INITIAL DEPTH 104.03 (From ground level) Water Column Height _____
 Total Depth 161-171 (intermediate screen) Well Volume (gals) _____
 Well Diameter 5" (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purging
 Method of Water Removal Pumping Was Well Pumped Dry? Yes No
 3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>1525</u>	<u>10.1</u>	<u>depth to water (From ground level)</u>	<u>measured as</u>	<u>104.03</u>					
<u>1530</u>		<u>pumping started - flow rate</u>	<u>adjusted to 104/m</u>				<u>1.24/m</u>		
<u>1541</u>	<u>16.24</u>	<u>830</u>	<u>6.84</u>	<u>31.3</u>	<u>104.03</u>			<u>2.87</u>	<u>135.1</u>
<u>1556</u>	<u>17.11</u>	<u>718</u>	<u>6.92</u>	<u>10.7</u>	<u>104.03</u>			<u>4.46</u>	<u>171.2</u>
<u>1603</u>	<u>17.12</u>	<u>748</u>	<u>6.94</u>	<u>7.2</u>	<u>104.03</u>		<u>1.04/m</u>	<u>3.99</u>	<u>145.1</u>
<u>1608</u>	<u>17.06</u>	<u>728</u>	<u>6.98</u>	<u>9.6</u>	<u>104.01</u>			<u>4.44</u>	<u>126.0</u>
<u>1617</u>	<u>17.07</u>	<u>721</u>	<u>6.99</u>	<u>8.4</u>	<u>104.01</u>			<u>4.35</u>	<u>106.3</u>
<u>1624</u>	<u>17.15</u>	<u>725</u>	<u>7.00</u>	<u>7.2</u>	<u>104.01</u>			<u>4.36</u>	<u>100.9</u>
<u>1630</u>	<u>17.29</u>	<u>756</u>	<u>6.85</u>	<u>5.8</u>	<u>104.00</u>			<u>4.05</u>	<u>191.0</u>
<u>1631</u>		<u>collected 1 total Cr sample to MWD</u>			<u>W-ACE-R-I-092000-P</u>				

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AF Date 9-26-00

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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number <u>46118</u>	Project Name <u>Ace Services</u>	Date <u>09-21-00</u>
Monitor Well Number <u>ACE-R-D</u>	Field Investigator(s) <u>Kyle Malde</u>	

WELL DATA
 INITIAL DEPTH 84.20' Water Column Height _____
 Total Depth 209.225 (screen Depth) Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 5"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Micro-Purging
 Method of Water Removal pumping Was Well Pumped Dry? Yes No

3 Well Volumes NA gals Amount of Water Removed from Well NA gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance green color

Remarks water level higher than yesterday by ~20' - yesterday's levels at this well may be irregular?

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
0900	<u>Initial depth to water measured at</u>				<u>84.00</u>				
0910	<u>Pumping started - flow rate adjusted to ~1.0 L/min</u>						<u>~1.0 L/min</u>		
0938	<u>16.73</u>	<u>691</u>	<u>6.65</u>	<u>9.4</u>	<u>84.96</u>		<u>~1.0 L/min</u>	<u>552</u>	<u>177.4</u>
0947	<u>16.61</u>	<u>650</u>	<u>7.17</u>	<u>5.0</u>	<u>83.95'</u>		<u>~1.0 L/min</u>	<u>593</u>	<u>113.5</u>
0957	<u>16.54</u>	<u>624</u>	<u>7.21</u>	<u>3.0</u>	<u>83.95</u>		<u>~1.0 L/min</u>	<u>6.24</u>	<u>99.3</u>
1003	<u>16.37</u>	<u>619</u>	<u>7.21</u>	<u>3.5</u>	<u>83.95</u>		<u>~1.0 L/min</u>	<u>6.33</u>	<u>102.0</u>
1008	<u>16.13</u>	<u>614</u>	<u>7.20</u>	<u>6.3</u>	<u>83.95</u>		<u>~1.0 L/min</u>	<u>6.34</u>	<u>93.0</u>
1013	<u>16.82</u>	<u>623</u>	<u>7.20</u>	<u>5.2</u>	<u>83.96</u>		<u>~1.0 L/min</u>	<u>6.28</u>	<u>87.0</u>
1020	<u>16.71</u>	<u>621</u>	<u>7.20</u>	<u>3.0</u>	<u>83.95</u>		<u>~1.0 L/min</u>	<u>6.33</u>	<u>86.7</u>
1022	<u>collected 1 total Cr Sample - ^{for 3000} W-ACE-R-D-092100-P</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By AS Date 9-26-00

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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number <u>46118</u>	Project Name <u>Acc Services</u>	Date <u>9-19-00</u>
Monitor Well Number <u>EX-2-I</u>	Field Investigator(s) <u>G. Felker</u>	

WELL DATA
 INITIAL DEPTH 110.89' Water Column Height 85'
 Total Depth 195' Well Volume (gals) -222
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter 8" 8" = 2.6" gal/ft

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA Placed pump at screen interval
 Method of Water Removal pumping Was Well Pumped Dry? Yes No
 3 Well Volumes -666 gals Amount of Water Removed from Well -455 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance Greenish Tint

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>0845</u>	<u>Initial</u>				<u>110.89'</u>				
<u>0920</u>	<u>Start pumping</u>						<u>13 gpm</u>	<u>6.21</u>	<u>220</u>
<u>0925</u>	<u>15.1</u>	<u>547</u>	<u>7.1</u>	<u>0.3</u>			<u>"</u>	<u>6.21</u>	<u>220</u>
<u>0931</u>	<u>15.1</u>	<u>561</u>	<u>7.2</u>	<u>0</u>				<u>5.51</u>	<u>213</u>
<u>0942</u>	<u>15.1</u>	<u>566</u>	<u>7.2</u>	<u>0</u>				<u>5.25</u>	<u>210</u>
<u>0949</u>	<u>15.1</u>	<u>568</u>	<u>7.2</u>	<u>0</u>				<u>5.70</u>	<u>208</u>
<u>0951</u>	<u>15.1</u>	<u>569</u>	<u>7.2</u>	<u>0</u>				<u>5.20</u>	<u>209</u>
<u>0953</u>	<u>15.1</u>	<u>571</u>	<u>7.2</u>	<u>0</u>				<u>5.16</u>	<u>209</u>
<u>0954</u>	<u>15.1</u>	<u>571</u>	<u>7.2</u>	<u>0</u>		<u>-455 gals</u>		<u>5.17</u>	<u>209</u>
<u>0955</u>	<u>collected sample</u>								

NTU = Nephelometric turbidity units
 WL = Water level

Checked By JS Date 9-26-00

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Monitor Well Number <u>EX-2-D</u>	Field Investigator(s) <u>G. Felker</u>																																																																																																																																			
WELL DATA INITIAL DEPTH <u>111.54'</u> Total Depth <u>235'</u> Well Diameter <u>8"</u>	Water Column Height <u>123.5'</u> Well Volume (gals) <u>~322 gal</u> (x)(height) x=.163 gal/ft @ 2", x= 653 gal/ft @ 4" <u>8" = 2.611 gal/ft</u>																																																																																																																																			
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WATER SAMPLING DATA Method of Water Removal <u>pumping</u> Was Well Pumped Dry? Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>Pump at top of water column</u>																																																																																																																																			
Well Volume <u>~966</u> gals	Amount of Water Removed from Well <u>~653</u> gals																																																																																																																																			
FINAL FIELD ANALYSIS Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____ Physical Appearance <u>Greenish Tint</u>																																																																																																																																				
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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ice Services Date 9-21-00

Monitor Well Number OB-1-D Field Investigator(s) G. Felker

WELL DATA
 INITIAL DEPTH 113.22' Water Column Height 122'
 Total Depth 235' Well Volume (gals) ~80 gal
(x)(height) x=.163 gal/ft @ 2". x=.653 gal/ft @ 4"
 Well Diameter 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal Submersible Pump Was Well Pumped Dry? Yes No
 3 Well Volumes ~240 gals Amount of Water Removed from Well ~510 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>1600</u>	<u>Inter. tidal</u>	<u>W.L.</u>	—	—	<u>113.22'</u>	—	—	—	—
<u>1616</u>	<u>Start</u>	<u>Pumping</u>	—	—	—	—	<u>15 gpm</u>	—	—
<u>1630</u>	<u>15.5</u>	<u>429</u>	<u>7.46</u>	<u>0</u>	—	—	—	<u>7.2</u>	<u>228</u>
<u>1633</u>	<u>15.5</u>	<u>431</u>	<u>7.45</u>	<u>0</u>	—	—	—	<u>7.1</u>	<u>228</u>
<u>1636</u>	<u>15.5</u>	<u>433</u>	<u>7.45</u>	<u>0</u>	—	—	—	<u>7.0</u>	<u>227</u>
<u>1639</u>	<u>15.5</u>	<u>435</u>	<u>7.44</u>	<u>0</u>	—	—	—	<u>7.0</u>	<u>227</u>
<u>1642</u>	<u>15.5</u>	<u>436</u>	<u>7.44</u>	<u>1.6</u>	—	—	—	<u>6.99</u>	<u>226</u>
<u>1646</u>	<u>15.5</u>	<u>436</u>	<u>7.44</u>	<u>1.4</u>	—	—	—	<u>6.98</u>	<u>226</u>
<u>1649</u>	15.5	437	<u>7.44</u>	<u>0</u>	—	<u>~510 gal</u>	—	<u>6.97</u>	<u>225</u>
<u>1650</u>	<u>Collect sample</u>	—	—	—	—	—	—	—	—

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AS Date 9-26-00

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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ace Services Date 9-19-00

Monitor Well Number PWS-8 Field Investigator(s) G. Felkner

WELL DATA
 INITIAL DEPTH ? Water Column Height _____
 Total Depth 240' Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter _____

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping _____ Air Lift _____
 Surging _____ Bailing _____

WATER SAMPLING DATA
 Method of Water Removal dedicated turbine pump Was Well Pumped Dry? Yes No
 3 Well Volumes NA gals Amount of Water Removed from Well 10,200 gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance greenish tint

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1018	Start	Pumping	—	—	?	—	—	—	—
1019	15.29	551	7.5	29	—	2400 gal	4 in	6.66	199
1022	15.19	582	7.4	14	—	3 tanks	850 gpm	6.19	204
1046	—	—	—	—	—	—	—	—	—
1049	15.2	592	7.7	10	—	—	850 gpm	6.96	218
1050	15.3	584	7.4	5	—	—	—	6.90	224
1108	—	—	—	—	—	—	850 gpm	—	—
1110	15.3	592	7.6	9	—	—	—	6.37	227
1111	15.3	587	7.5	3.6	—	—	—	6.89	231
1111	Collect sample	—	—	—	—	10,200 gals	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—

NTU = Nephelometric turbidity units
 WL = Water level

Checked By 7401 10,200 Date _____

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WATER SAMPLING DATA Method of Water Removal <u>Pumping</u> Was Well Pumped Dry? Yes No <input checked="" type="radio"/> 3 Well Volumes <u>~39</u> gals Amount of Water Removed from Well <u>~600</u> gals																																																																																																																																				
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MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ace Services Date 9-20-00

Monitor Well Number HPMW-9-S Field Investigator(s) G. Felton

WELL DATA
 INITIAL DEPTH 103.37' Water Column Height ~ 22'
 Total Depth 125' Well Volume (gals) ~ 14
 Well Diameter 4" (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO. _____
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal Pumping Was Well Pumped Dry? Yes No
 3 Well Volumes ~ 43' gals Amount of Water Removed from Well ~ 470 gal gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed ^{2.5 in @ 4"}	Flow Rate ^{gpm}	DO	ORP
1315	Initial	WL	—	—	103.37'	—	—	—	—
1322	Start	Purging	—	—	—	—	10.9 gpm	—	—
1338	15.5	939	6.89	2.2	—	—	↓	1.3	191
1344	15.5	943	6.81	0.3	—	—	↓	0.88	191
1356	15.5	948	6.80	0	—	—	↓	1.12	192
1359	15.5	950	6.8	0	—	—	↓	0.75	192
1402	15.5	950	6.8	0	—	—	↓	0.72	192
1404	15.5	950	6.8	—	—	~ 470 gal	↓	0.75	192
1405	Collect	sample	—	—	—	—	—	—	—

NTU = Nephelometric turbidity units
 WL = Water level

Checked By DF Date 9-26-00

Project Number 46118 Project Name Ace Services Date 9-22-00

Monitor Well Number RW-2 Field Investigator(s) G. Felker

WELL DATA
 INITIAL DEPTH Residential Water Column Height _____
 Total Depth _____ Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter _____

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal _____ Was Well Pumped Dry? Yes No
 3 Well Volumes _____ gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1449	Start	Purging	—	—	—	—	—	—	—
1455	16.2	414	7.78	0	—	—	—	8.75	212
1500	15.9	413	7.64	0	—	—	—	8.75	213
1505	15.8	411	7.74	0	—	—	—	8.73	214
1509	15.8	410	7.74	0	—	—	—	8.72	212
1510	Collect	sample	—	—	—	—	—	—	—

NTU - Nephelometric turbidity units
 WL - Water level

Checked By DF Date 9-26-00

Project Number 46118 Project Name Acc Services Date 9-22-00

Monitor Well Number RW-4 Field Investigator(s) G. Fellner

WELL DATA
 INITIAL DEPTH Residence Water Column Height _____
 Total Depth _____ Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"
 Well Diameter _____

METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal _____ Was Well Pumped Dry? Yes No
 3 Well Volumes _____ gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ microhos pH _____ Turbidity _____
 Physical Appearance _____

Remarks _____

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
<u>1557</u>	<u>Start</u>	<u>purging</u>	—	—	—	—	—	—	—
<u>1603</u>	<u>16.8</u>	<u>442</u>	<u>7.73</u>	<u>0.6</u>	—	—	—	<u>8.04</u>	<u>278</u>
<u>1607</u>	<u>15.5</u>	<u>429</u>	<u>7.72</u>	<u>0</u>	—	—	—	<u>8.49</u>	<u>271</u>
<u>1611</u>	<u>15.5</u>	<u>432</u>	<u>7.73</u>	<u>0</u>	—	—	—	<u>8.13</u>	<u>273</u>
<u>1617</u>	<u>15.2</u>	<u>429</u>	<u>7.82</u>	<u>0</u>	—	—	—	<u>8.5</u>	<u>273</u>
<u>1619</u>	<u>15.2</u>	<u>428</u>	<u>7.7</u>	<u>0</u>	—	—	—	<u>8.5</u>	<u>274</u>
<u>1620</u>	<u>Collect</u>	<u>sample</u>	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—

NTU - Nephelometric turbidity units
 WL - Water level

Checked By AS Date 9-26-00

MONITORING WELL DEVELOPMENT/PURGING DATA

Project Number 46118 Project Name Ace Services Date 09-22-00

Monitor Well Number 1940 E. 4th - RW 06 Field Investigator(s) Kyle Madden

WELL DATA
 INITIAL DEPTH Residence Water Column Height _____
 Total Depth _____ Well Volume (gals) _____
 (x)(height) x=.163 gal/ft @ 2", x=.653 gal/ft @ 4"

Well Diameter _____
 METHOD OF WELL DEVELOPMENT PHOTOGRAPH IDENTIFICATION NO.
 Pumping Air Lift
 Surging Bailing

WATER SAMPLING DATA
 Method of Water Removal _____ Was Well Pumped Dry? Yes No
 3 Well Volumes _____ gals Amount of Water Removed from Well _____ gals

FINAL FIELD ANALYSIS
 Water Temp _____ °C Specific Conductance _____ micromhos pH _____ Turbidity _____
 Physical Appearance Clear

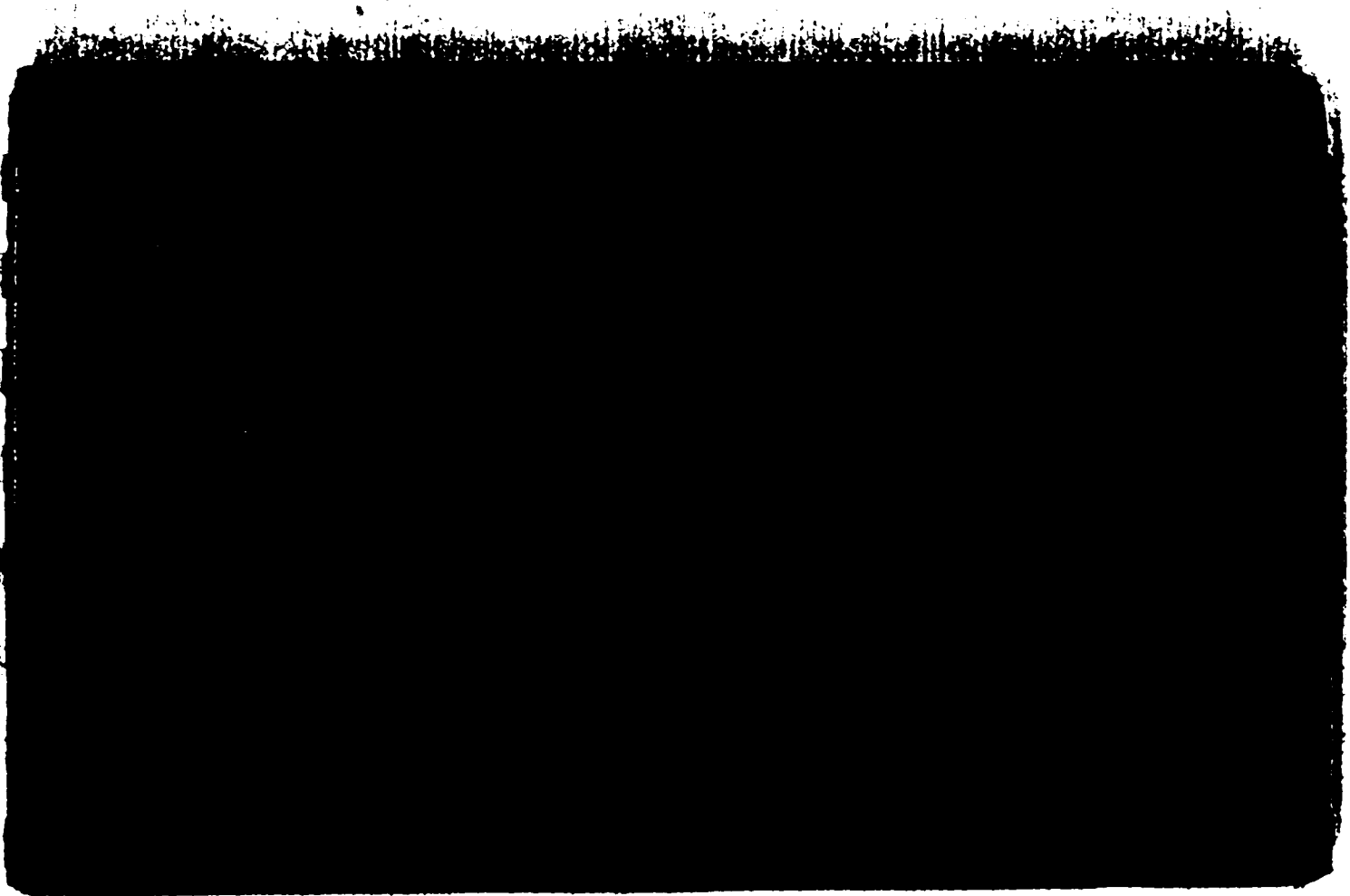
Remarks 1940 East 4th - metzler Residence

TIME	Temp °C	Conductivity	pH	NTUs	WL	Removed	Flow Rate	DO	ORP
1445	Started								
1450	16.34	496	7.47	11.3				10.30	184.5
1455	15.95	491	7.43	4.4				8.96	191.6
1500	15.49	485	7.48	2.9				9.04	206.9
1505	15.35	479	7.47	0.3				9.18	216.2
1510	15.35	484	7.47	0.6				8.97	220.3
1510	Collected	1 total Gr Sample - W-RW-06-092200-P							

NTU = Nephelometric turbidity units
 WL = Water level

Checked By DF Date 9-26-00

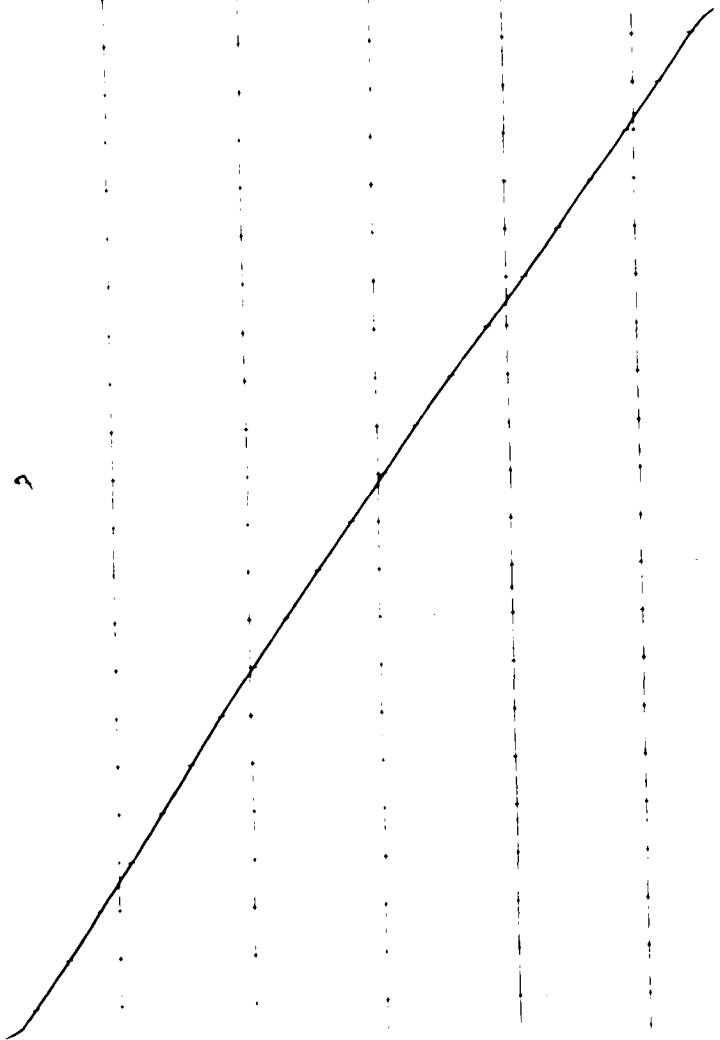
Appendix D
Field Logbooks



Walt Wafta

2/24/00

UNITED Parcel fee shipment back to Vendor. ALL Worker levels are recorded on separate work level sheet.



July 10th

7-10-00

Weather: Sunny 70°-90°s, wind from NNW
0750 Arrive site. Alley marker still up. I set well location survey flags.

0858 Drill crew:

John Mosier

Kerry Bentley

Mark Carter

Mike Newman

Crew move site. Utilities

out marking utilities.

Drill crew prepare to drill.

1040 Have dug mud pit for EX-2-D. We will drill EX-2-D first. Local pit.

1059 Conduct safety meeting. Highlights:

include:

- hard hats

- PPE to prevent contact w/ groundwater (+3000 45/c hr)

- Drink water

1105 Begin drilling EX-2-D.

1400 Reach total depth @ EX-2-D @

240' Shale @ 233'

1600 Finish reaming boring to 12" dia.

1640 Still flushing grout from boring.

July 10th 7-10-00

94. Aug 10 7-10-00

1825 Still flushing boring and thinning drilling fluid.

1830 Starting to rain.

1940 Lowering casing @ EX-2-D.

2010 Screen on casing set to 235' ~~222'~~

Begin placing sand filter pack

2050 Have placed bentonite chip seal. Begin grouting.

2130 Have placed 3 lbs grout hydrant quit to rig

2132 Secure site w/ caution tape and surround pit w/ rags also.

2135 Drill crew & myself to site.

~~Aug 10~~
~~7-10-00~~

Aug 11 7-11-00

Weather Sunny 70's - 90's

0728 Arrive site. Drill crew

preparing for day. Will finish

getting EX-2-Dent drill

EX-2-I.

0805 While excavating circulation pit for EX-2-I a phone line is hit. (damaged)

Drill crew to phone company. Local businesses still have power. Phone co. says they will call if problem.

0857 Pull rig with EX-2-I. Have excavated pit for circulation.

0930 Begin drilling @ EX-2-I.

1124 Have reached @ EX-2-I w/ 7 1/2" OD bit. Begin to run to 12" OD.

1250 Go by Dougherty's Implement to see about moving two combines blocking access to well locations. Meet w/ Jay Wodtke. Jim Dougherty said he could move them in next two days.

1330 Go by Max Embree's house at G+E Farms to see about access to the farm field for wells 114-1314

Aug 11 7-11-00

98

A. J. Allen 7-12-00

begin to set screen +
vise.

1730

Finish setting screen + vise
to total depth @ OB-1-S.

1736

Relinquish soil sample to
U.P.S.

1800

Finish placing screen filter
pack, seal, + grout @ OB-1-S.
Move rig onto OB-1-I.
Driller repairing return hose
on water pump.

1919

Have secured site. Locked
wells. All in site.

Diagonal scribble
A. J. Allen
7-12-00

A. J. Allen 7-13-00

Weather: Sunny 70's - 90's

0745 Arrive site. Driller onsite. We will
drill ~~at~~ OB-1-I today.

0815 Call Bob Stewart. Update on
progress.

1003 Ken total depth @ OB-1-I w/
3" bit. Flushing boring.

1028 Finish flushing boring. begin lowering
casing @ OB-1-I.

1130 Finish grouting well OB-1-I. Rig goes
to deck.

1212 Finish decommissioning. Pull rig onto
OB-2-D.

1258 Begin drilling OB-2-D.

1350 Collect:

S-IDWQBI-071300

1351 Ken Wirth (btt) arrives site
I show Ken around site.

1500 Meet w/ Gerry Bickel (colby)
to discuss rounded design.

Also discuss project w/ Gordon
Armstrong.

1630 Go to county court house to get
city maps.

1700 Driller has set OB-2-D, TD 240
A. J. Allen 7-13-00

100 Jimmy Fallon 7-13-00

1735 Deliv. sample to UPS for shipment

1807 Rig moved over to OB-2-I. Site secured. All in site.

~~Jimmy Fallon 7-13-00~~

Jimmy Fallon 7-14-00 101

Weather Sunny 70-90°
0740 Arrive site w/ Ken Lynch, D. Han
doubts OB-2-I and OB-2-S.
0801 Go to Ace Services building for
inspect for use in treatment
plant.

0930 Rig one shored up to lot as
in Machine shop. Use time
outside measurements and logs.

1010 Calibrate YSE meter (pH + ~~ORP~~ ^{ORP})

1023 110.25' water level EX-2 @

EX-2-D.

We set up to develop EX-2-D.

D. Han setting pipe @ OB-2-I.

1229 Finish setting OB-2-I. Rig pulls over
to OB-2-S.

133 Start pumping EX-2-D @ 75 gpm

1512 Finish developing EX-2-D

1520 Receive soil results for IDW

See EX-2. Results = 37 mg/kg total

Cr which is less than 100 mg/kg so

soil will be spread to ground.

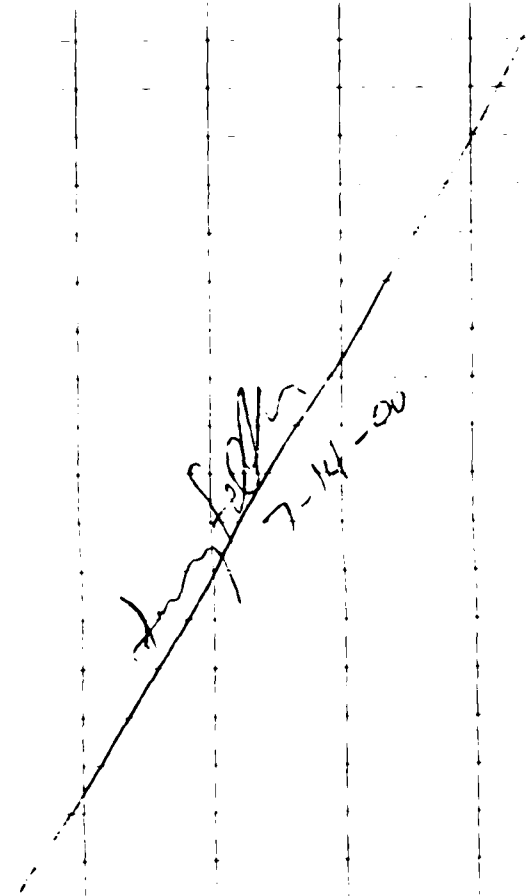
1550 D. Han finish setting and grouting

OB-2-S (10')

1554 Collect S-IDW OB2-071400

102 Aug 14 7-14-00

1620 110.8' ^{165'} WL @ EX-2-S prior
 to pumps
 1640 Begin pumping EX-2-S.
 1800 Stop pumping for day. Secure site.



103 Aug 15 7-15-00

0820 Arrive site. D. then start
 pumping EX-2-S @ 0810.
 Also setting up to pump OB-2-D.
 0850 Calibrate pit. Verify conductivity
 calibration.
 0913 Start developing OB-2-D.

Well	Water Level	Notes	ID
OB-1-S	112.15'	BCG	130
OB-1-I	111.45'		195'
OB-1-D	113.82'		235'
OB-2-S	108.80'		130
OB-2-I	107.90'		192
OB-2-D		pumps pipe in 4" dia 235'	
EX-2-S	116.50'	pumps @ 15.7 gpm	
EX-2-I	110.95'		195'
EX-2-D	112.65'		235'

1034 Stop pump EX-2-S
 1325 Start developing EX-2-I
 1520 ~~Stop~~ Finish development @ OB-2-D
 1645 Finish development @ EX-2-I
 1705 Site secured, all leave site.

Aug 15 7-15-00

104

Angell 7-17-00
Weather: cloudy/rainy 60-70°

- 0740 Arrive site. Will clean pipe then develop next well. Driller pulling pipe from EX-2-I.
- 0850 Set up to develop OB-2-I. ~~Check~~ Check calibration of YSI meter (pH). Raining hard.
- 0920 start pumping @ OB-2-I.
- 1055 Finish developing OB-2-I. Driller pull pump.
- 1130 It's been raining hard all morning. Rig is stuck, quite a bit of runoff starting to develop. Will secure site and quit for day.
- 1157 Quit for day due to rain.

Angell
7-17-00

Angell 7-18-00

105

- Weather: Sunny 60-70°
- 0740 Arrive site. Rig still stuck. Driller trying to pull out of other trucks.
- 0815 Get rig out and pull out OB-1-D.
- 0830 Calibrate SC and verify pH calibration.
- 0915 Begin pumping (developing) OB-1-D.
- 1126 Finish developing OB-1-D. Driller go down and set-up on OB-1-S.
- 1300 Start pumping @ OB-1-S.
- 1441 Finish developing OB-1-S. Driller breakdown to go down.
- 1520 Rig pulls onto OB-2-S to develop.
- 1540 Start pumping OB-2-S.
- 1737 Finish developing OB-2-S.
- 1806 Secure site. All in for day.

Angell
7-18-00

106

July 19th 7-19-00

Weather: Cloudy 60-70's. Rain
hard last night.

0740 Arrive site. Driller getting
ready to develop well OB-1-I.

0840 Verify sc + pH calibration.

0910 Start pumps OB-1-I.

1100 Fin in developing OB-1-I.

* 1231 Site secured. Cottages test
non-hazardous. Driller will proceed
to ground. Lu. STP for K.C.

~~July 19th 7-19-00~~

July 31st

7-31-00 107

1600 Arrive site w/ Dustin
Marlow (B+V). Remind Dustin
Marlow to remain in exclusion
zone.

Ron. Shipler w/ Woffa Pump
onsite. Review site procedure w/
Ron. Dustin + I set up
to perform pump test.

2213 Have set transducers in
well EX-2 w/ M.V.-9.
Recorder is running.
Have measured lengths for
transducers in wells
OB-1 and OB-2.

I go to get supplies.
2330 Dustin lvs site. I
remain to oversee equipment
while collecting steady state
data.

2400 Continued 8-1-00

~~July 31st 7-31-00~~

108 Aug 1st 8-1-00

0000 Onsite to oversee recorder measuring steady state data at wells EX-2 and MW-9

0235 Colby Police stop by. I inform them what we are doing and that Gerry Becker knows that we are performing pump tests. The police say OK and leave site.

0651 Dustin arrives site. Continue setting up other channel box. Check recorder which is running.

0754 Ron Spay (Wolfe) arrives site.
0954 Have finished setting up transit recorder and start stop test.

1400 Begin pumping EX-2-D @ 100.

1605 Return to hotel to program background Levelogger

1807 MW-7-D
W.L. 120.01 ft below TCC

Aug 1st 8-1-00

Aug 1st 8-1-00 109

1818 MW-6-D
WL = 106.42' TCC

1825 Lower Levelogger probe to 110' TCC @ MW-6-D

1904 Check flow rate @ EX-2-D = 108 gpm
Lv. site for day.
Dustin will be gone till 23:00.
Wolfe pump watch 23:00 - 7:00

~~Aug 1st 8-1-00~~

110 Amy Lell 8-2-00

0700 Arrive site. Darren at
Woolta pump onsite. He said

growth OK.
0710 EX-2-D pumping @ 105 gpm

0927 EX-2-D pump rate @ 105 gpm

1029 EX-2-D pump rate @ 105 gpm

1100 Discuss additional sample collection
for treatability study w/ Ken
Wyatt.

1130 Talk to SW Labs about
analyses. FAX parameter request
to Randy Stagg @ SW Labs.

1200 Return to site w/ Darren. Ron
w/ Woolta onsite from 1100 to 1200.

1416 W.L. @ MW-6-D
= 106.71' b70C

1425 W.L. @ MW-7-D
= 120.19' b70C

1454 EX-2-D pump rate @
105 gpm

1531 Call Bob Stewart (EPA) and
update on progress.

1900 Lv. site for day. Darren @
site

~~8-2-00~~
8-2-00

Amy Lell 8-3-00

Weather P.H. Cloudy - Sunny 60°-90°

0654 Arrive site. Darren w/ Woolta
Pump & Well onsite. Light rain last night.

0701 EX-2-D pumping @ 105 gpm

0830 EX-2-D pumping @ 105 gpm

1045 EX-2-D pumping @ 105 gpm

1156 Dustin Maibou (Bob) arrives
site.

1450 Lv. site. Dustin onsite.

1857 Arrive site. Relieve Dustin
from exercise.

1930 Call Jay Woolta. Arrange schedule
for tomorrow.

2006 EX-2-D pumping @ 105 gpm

2250 Darren at Woolta Pump arrive
site. I lv.

~~Amy Lell~~
~~8-3-00~~

112 Amy Fell 8-4-00

0755 Arrive site. Dust on site

0800 Collect sample
GW-EX2-D-080400-F

high range Cr⁶⁺ field test
= \rightarrow 1.5 mg/L

1042 Arrive RW-6 (Metzler)

Begin pumping.

1100 Collect
GW-RW6-080400-P

1200 Weather pump arrive to pull
pump and set in EX-2-I.

1529 WL @ MW-6-D
106.13' btop

~~Move Levelogger to
MW-6-I~~

1536 WL @ MW-6-I
= 104.54' btop

1600 Move & set Levelogger to
MW-6-I

2032 Pumping EX-2-I @
185 gpm

2305 Lv. site after Danes
arrives

~~Amy Fell
8-4-00~~

Amystall 8-5-00 113

1155 Arrive site. Dust on site.

1259 Measure WL @ MW-6-I
= 104.74' btop

1500 Dust on lv. site

1510 Pumping @ EX-2-I @
185 gpm

1709 Pumping @ EX-2-I @
185 gpm

1830 Pumping @ EX-2-I @
185 gpm

2150 Pumping @ EX-2-I @
185 gpm

2300 Lv. site after weather pump +
Well employee arrives.

~~Amy Fell
8-5-00~~

114

Arry Lell 8-6-00

1200 Arrive site, Dustin onsite

1316 W.L. @ MW-6-I =
104.73' bToc

1600 Dustin lv. site.

1744 Pumping @ EX-2-I @

185 gpm

2057 Pumping @ EX-2-I @

185 gpm

2300 Darren / Wootter Pump +
Well arrives. I lv. site.

~~Arry Lell
8-6-00~~

Arry Lell

8-7-00

115

1120 Arrive site, Dustin onsite

1130 Collect sample
GW-EX2-I-080000-P

Field test kit for C¹⁴
= >4.5 mg/L (w/ dilution)

1300 Relinquish sample to hotel for
Fed. Ex. pick-up.

1332 W.L. @ MW-6-I =

104.67'

1350 Wootter Pump (Ron supply + labor)
arrive site to pull well from
EX-2-I and set different
pump in EX-2-S.

1600 Begin test pump @ 30 gpm

1630 Reduce flow to 20 gpm

1700 Dustin lv. site.

2335 Darren arrives site, I lv.

~~Arry Lell
8-7-00~~

116

Aug 8-00

Aug 9-00

~~116~~ 8-9-00 117

1200 Arrive site Duston is onsite.

1230 Talk w/ Sellers Tractor (Mike (785) 462-2321 Johnson) about supplying water. They said OK. Will call more tomorrow.

1405 Pick-up Fed Ex package.

1430 Discuss shipping equipment w/ UPS.

1700 Duston lvs site.

2240 Lvs site after Daman from Weather Pump and site.

1200 Arrive site. Duston onsite.

1330 WL @ MW-6-I = 104.74'

1730 Duston lvs site.

2240 Daman arrives site. I leave.

~~Aug 8-00~~

~~Aug 9-00~~

118

Andy Sell 8-10-00

- 0802 Arrive site. Duston onsite.
- 0805 Wait Wraith (bV) arrives site.
- 0810 Collect
GW-EX2-S-081000-P
Field Cr⁶⁺ measurement =
0.8 mg/L (2x dilution)
- 1140 W.L. @ MW-6-I =
104.77'
- 1200 Pull Level Logger
Site cleaned and wells
secured. Drop off boxes for
shipment @ Comfort Inn
for shipment via UPS.
- 1330 Call Bob Stewart of EPA
and update on progress.
- 1345 Call Siv laboratory to confirm
sample receipt. Sample received OK.
- 1400 Head to KC, MO

Andy Sell 8-10-00

119

Andy Sell 9-18-00

- 0750 Arrive hotel station w/
Ede, Mr. Aden, & Tapa. Arrive
- 0840 Pumping @ MW-12-S
MW-12-I. Mr. Aden, Mr. Aden
arrive site. Conduct H+S meeting.
- 0930 Crew #1 pump for MW-12-I
Crew #2 pump for MW-12-S
- 1010 Collect
W-MW-12-I-091800-P
- 1025 Crew #1 pull pipe so deep
- 1100 W.L. MW-11-I = 120.05'
Crew #1 @ MW-11-I
- 1151 Collect
W-MW-11-I-091800-P
W-MW-11-I-091800-D
D.H. crew pull pump to so deep
- 1235 Collect Rinstate
W-MW-11-S-091800-R
- 1300 Working @ MW-11-S
Crew #2 @ MW-7-I &
MW-5-I
- 1355 Collect
W-MW-11-S-091800-P
D.H. crew so deep
- 1415 W.L. @ MW-2-D

Andy Sell 9-18-00

120

Andy Sellen 9-18-00

1458 Pumping @ MW-2-D @

1540 Collect

W-MW-2-D-091800-P

1600 Crew #1 pulling pipe & going to decon

1606 Crew #2 pull onto MW-2-I

1654 Start pump @ EX-2-D

1800 Relinquish sample to UPS

1900 Finish collect cleanup of site, getting supplies, and prepare for tomorrow

~~Andy Sellen 9-18-00~~

121

Andy Sellen 9-19-00

0750 Arrive PWS #8, prepare for day

0805 Calibrate conductivity & pH

0825 City not here yet. Crews #1 & #2 ready to go. Call city. They forgot and are on way.

0835 City realizes power meter is blown out and will have to replace. We sample EX-2-I and will return to PWS-8 later.

0845 Arrive @ EX-2-I. W.L. = 110.89'

0955 Collect W-EX-2-I-091900-P

1012 Return to PWS-8

1111 Collect W-PWS-8-091900-P

Driller decon
1208 Tilted W.L. @ EX-2-S = 111.67'

1315 Collect W-EX-2-S-091900-P

Driller go decon
1350 W.L. @ MW-9-S = 111.98'

Andy Sellen 9-19-00

122 Amy Sells 9-19-00

1415 Start pumping MW-9-S

1450 Collect
 W-MW-9-S-091900-P
 W-MW-9-S-091900-D

1510 Start filling 6 15 gal
 drums for shipment to
 Samco Tech for Ion Exchange
 treatability st. day.

1600 Collect
 W-IX-TS-1-091900-P

1615 Start pumping MW-9-I

1626 IX-TS sample is
 650 mg/L Cr⁺⁶ field test

1655 Collect
 W-MW-9-I-091900-P

1800 Relinquish sample to UPS

1815 Secure site.

Sells
 9-19-00

Amade 9-20-00 123

40-60" Rain last night

0800 Arrive site. Prepare for day.

0830 113.32 W.L. @ MW-9-B

0850 Verify calibration of pH
 and conductivity Update Sub Start (EM)

0910 Collect
 W-MW-9-D-092000-P

Driller go decon.

0949 W.L. @ MW-12-D = 144.87

1045 Collect
 W-MW-12-D-092000-P
 W-MW-12-D-092000-D

Driller go decon.

1125 W.L. @ HPMW-6-S = 105.41

1140 Start pumping HPMW-6-S

1144 W.L. @ HPMW-3-S = 105.01

1152 W.L. @ HPMW-12-S = 107.41

1225 Collect
 W-HPMW-6-S-092000-P
 " " -MS
 " " -MSD

Driller go decon.

~~1447 W.L. @ MW-8-S = 108.28~~

1405 Collect
 W-HPMW-9-S-092000-P

Amy 9-20-00

124 Aug 19 9-20-00
 1430 ~~1430~~ Well MW-10-P
 is DRY
 1447 W.L. @ MW-8-S = 108.28
 1505 Collect
 W-ACE-R-I-092000-R
 (Kinsate from Gen #2)
 1540 Collect
 W-MW-8-S-092000-P
 Driller down
 1606 W.L. @ MW-8-I = 107.75'
 1655 Collect
 W-MW-8-I-092000-P
 Driller down
 Begin sample management
 1800 Relinquish sample to US
 for shipment.
 1847 Finish securing site w/ getting
 supplies.

~~1430~~
 9-20-00

Aug 19 9-21-00 125
 0755 Arrive site
 0800 W.L. @ MW-8-D = 107.76
 0820 Calibrate meter for conduct
 and pH. Cal #2 low also
 0905 Collect
 W-MW-8-D-092100-P
 W-MW-8-D-092100-D
 Driller down
 0944 W.L. @ ~~MW-8~~ MW-11-D
 = 122.37'
 1035 Collect
 W-MW-11-D-092100-P
 Driller go down
 1120 W.L. @ MW-5-D = 103.20'
 1205 Collect
~~1240~~
 W-MW-5-D-092100-P
 Driller down
 1240 W.L. @ MW-5-I = 100.49'
 1350 Collect
 W-MW-5-I-092100-P
 Driller go down
 1411 W.L. @ MW-5-S = 100.51'
 1440 Start pumping MW-5-S
 Aug 19 9-21-00

126 9-21-00

1510 Collect
W-MW-5-S-092100-P
W-MW-5-S-092100-D

Driller deco
1600 W.L. @ OB-1-D = 113.22'

1650 Collect
~~W-OB-1-D-092100-P~~

Driller deco
1715 Collect

W-OB-1-D-092100-R

1800 Relinquish sample to
VPS Site secured.

Driller
9-21-00

127 9-22-00

0755 Aqueous ...

0905 Pump #2 ...

0915 Verify conductivity + pH
calibration

0835 W.L. @ MW-7-D =
117.71'

0925 Collect
W-MW-7-D-092200-P
W-MW-7-D-092200-D, driller deco

1050 Collect
W-MW-7-S-092200-P, driller deco

1116 W.L. @ MW-3-D = 104.91'

1210 Collect
W-MW-3-D-092200-P

1336 Calibrate water level meters to
read the same

1340 Collect water levels

1450 Annie Vap residence (KW-2)
and start pumping Mus. Vap says
house next door (to east) on same
well. 1745 E 4th (Ketchum)

1510 Collect W-RW-2-092200-P

9-22-00

128

Jimmy Sells 9-22-00

29

1538

Spoke w/ person @ Sowers residence on phone. Person said Mr. Sowers would return on Sunday and could talk w/ him then. But could not give permission now.

1545

Collect
W-RW-3-092200-P

1600

At RW-4 (1795 E 4th)

1620

Collect

1635

W-RW-4-092200-P
Arrive RW-8. Mr. Smith said to go ahead and sample other property also.
RW-9 (3580 E. 4th)

owner { Mr. + Mrs. Mike Smith
1888 County Road 21
Colby, KS 67701

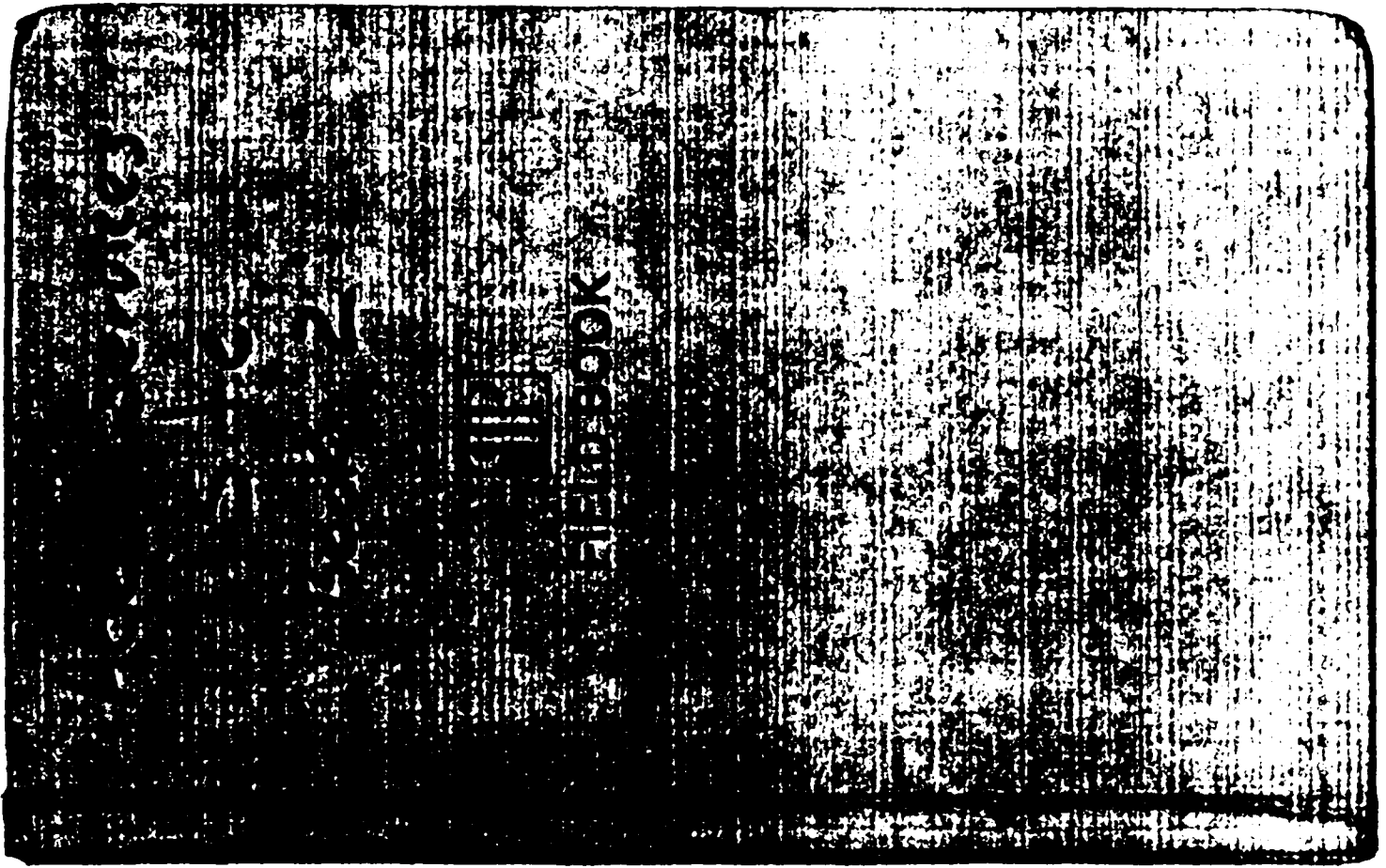
1650

Collect

1800

W-RW-9-092200-P
Relinquish sample to UPS.

~~Jimmy Sells
9-22-00~~



84

July 21, 2000 Sat. Hot slight breeze
D. Merlou

1:00 AM @ 12:20 PM
Check equipment transducers MW 2
(11-10psi, 1 20psi)

4:00 PM meet w/ Driller - Discuss plans for pumping test

Well	Depth	Return
MW-9-S	111.40	113.2
MW-9-I	111.25	
MW-9-D	110.87	
EX-2-S	111.75	
EX-2-I	111.37	
EX-2-D	110.11	
EX-2-S	108.75	
EX-2-I	107.71	
EX-2-D	109.42	
EX-2-S	111.10	
EX-2-I	110.33	
EX-2-D	110.0	

FT ↓
NEAR RETURN 2 LITS
↓

4:30 PM meet w/ Driller - Discuss plans for pumping test

5:00 PM Measure and mark all transducer cables and install transducers in MW-9-S, MW-9-I, MW-9-D, EX-2-S and EX-2-I

85

10psi Transducer = max depth + 28 ft

Well	Transducer Depth	Ref Return = TOC
MW-9-S	120'	5052
MW-9-I	134'	5072
MW-9-D	136'	6957
EX-2-S	125'	5416
EX-2-I	133'	6963

8:00 PM start Recorder to monitor water table fluctuations from pumping test = Measure 1 min intervals

Recorder: Hiram 201
SN 45418

Well	Input Port
MW-9-S	#1
MW-9-I	#2
MW-9-D	#3
EX-2-S	#4
EX-2-I	#5
EX-2-D	#6

10:00 PM Finish preliminary report
Appear from static water table there is a slight correlation of difference to all wells. Intermediate-shallow and Deep Wells (<2')

D. Merlou

TRANSFORMER S/N	RANGE	SCALE	Linearity	COEFF
5082	10psi	9.9661	0.0097	0.0519
5092	10psi	9.9179	0.0222	0.0000
6859	10psi	10.0011	0.0197	0.1171
5416	10psi	9.9456	0.0232	0.0000
5057	10psi	10.0225	0.0178	0.0107
5057	10psi	9.9316	0.025	0.0000

VALUES

Pressure 2500
6000
Range A Site
Temperature and humidity

Well	Temp	Scale	Linearity	COEFF
20-1-S	5251	10psi	0.0103	0.0000
20-1-I	5415	10psi	0.0236	0.0000
20-1-D	5415	10psi	0.0242	0.1109
20-2-S	5430	10psi	0.0103	0.0000
20-2-I	5437	10psi	0.0103	0.0000
20-2-D	6902	10psi	0.0103	0.0000

Pressure 10psi

730-

Well	Scale	Linearity	COEFF
20-1-S	111.42		
20-1-I	111.29		
20-1-D	115.13		
20-2-S	111.12		
20-2-I	112.36		

Pressure ± 0.001

4DA

Sept 45418

Hermit 45457 EXN

TRDUT

- #1 08-1-S
- #2 08-1-I
- #3 08-1-D
- #4 08-2-S
- #5 08-2-I
- #6 08-2-D

7:55 start pump
 Pump running LA 11

8:00 stop pump
 No. 100
 8:15 start pump
 No. 100

8:30 stop pump
 No. 100
 8:45 start pump
 No. 100
 9:00 stop pump
 No. 100

	<u>RATE</u>	<u>DRAWL. (ft)</u>
11:01		46.2
↓		
11:22	70 gpm	43.6 - 30.4'
↓		
11:37	100 gpm	39.8 - 29.2'
↓		
11:50	120 gpm	29.7 - 39.3'
↓		
12:01 p		20.4 - 45.6'

Start test
 100 gpm = 22.2' DEW

Stop 100 gpm = 29.2'

Start 120 gpm = 39.3'

Stop 120 gpm = 45.6'

Start 100 gpm = 29.2'

Stop 100 gpm = 39.8'

Start 70 gpm = 30.4'

Stop 70 gpm = 43.6'

Start 100 gpm = 29.2'

Stop 100 gpm = 39.8'

Start 120 gpm = 39.3'

Stop 120 gpm = 45.6'

5:30p
 Check flow rate = 100 gpm
 D. Malow

10

EX-2-D

10.20	-1.805				
	14.4	0.08	1.3	21.0	29.7
	14.6	0.34	1.3	21.0	29.9
	13.7	0.2	1.2	21.0	29.7
	11.4	0.1	1.2	21.0	30.0
	7.0	0.4	1.2	21.0	30.1
	2.0	1.0	1.24	21.1	29.8
	6.7	1.2	1.2	21.0	30.1
	6.1	1.2	1.2	21.1	29.7
	6.8	1.2	1.2	21.1	36.0
	6.7	1.3	1.2	21.2	38.6
11.21	12.8	1.3	1.2	21.5	37.3
	15.2	1.3	1.2	21.7	37.6
	16.5	1.3	1.2	21.7	37.7
	16.7	1.3	(12.01)	21.1	37.8
	17.3	1.3	1.3	21.2	37.9
	17.2	1.3	1.3	21.1	37.6
	16.9	1.3	1.3	21.1	37.3
	17.0	1.3	1.3	21.2	40.1
	16.9	1.3	1.3	21.4	36.5
	16.8	1.3	1.3	21.1	35.0
	17.1	1.3	20.8	29.9	40.0
	17.2	1.3	20.8	29.5	40.1
	17.2	1.3	20.9	29.5	40.6
11.14	0.5	1.3	20.9		41.7

11

46.5	2.9	2.1
45.6	3.2	2.2
44.1	3.2	2.2
43.0	3.0	2.2
42.0	3.0	2.1
41.5	2.9	2.1
41.4	2.8	2.1
41.5	2.8	2.1
41.3	2.7	2.1
41.5	2.6	2.0
41.5	2.6	2.0
41.4	2.6	2.0
41.4	2.5	2.0
41.5	2.5	2.0
41.3	2.4	2.0
41.3	2.4	2.0
41.2 (12.15)	2.4	2.0
41.1	2.4	2.0
41.0	2.3	2.0
40.9	2.3	2.0
40.8	2.3	2.0
40.7	2.3	1.9
40.6	2.3	1.9
40.5	2.2	1.9 (14:07)

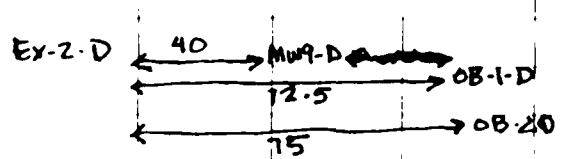
D. Marley

0.003	0.030	0.064	0.097	0.129	0.158	23.98	0.184	.204	.232	.255	.329
0.006	0.032	0.065	0.098	0.130	0.156		.184	.207	.230	.255 +A	.327
0.006	0.033	0.067	0.1	0.132	0.158		.185	.207	.232	.255	.329
0.006	0.035	0.068	0.101	0.133	0.159		.185	.208	.234	.256	.326
0.007	0.036	0.069	0.103	0.135	0.161		.187	.208	.234	.255	.321
0.009	0.038	0.071	0.104	0.136	0.162		.188	.21	.234	.256	.314
0.009	0.039	0.072	0.106	0.137	0.162		.190	.211	.236	.258	.304
0.010	0.041	0.073	0.106	0.137	0.164		.190	.211	.237	.259 SA	.291
0.012	0.042	0.075	0.107	0.139	0.165		.192	.213	.237	100A .261	.276
0.012	0.042	0.077	0.109	0.140	0.165		.192	.214	.239	100A .266	.261
0.013	0.043	0.078	0.110	0.142	0.166		.194	.214	.240	↓ .274	.246
0.014	0.045	0.078	0.111	0.143	0.168		.194	.216	.242	.281	.23
0.014	0.046	0.081	0.113	0.145	0.168		.195	.217	.242	.287	.22
0.016	0.048	0.082	0.114	0.145	0.169		.195	.219	.242	.292 6A	.198
0.017	0.049	0.084	0.116	0.146	0.171		.197	.219	.243	200A .297	.184
0.019	0.051	0.084	0.119	0.146	0.171		.198	.220	.243	.302	.17
0.020	0.052	0.084	0.119	0.148	0.172		.198	.220	.247	.310	.15
0.022	0.054	0.085	0.120	0.149	0.174		.198	.221	.246	.313	.14
0.022	0.055	0.087	0.122	0.151	0.175		.201	.224	.246	.317	.13
0.022	0.056	0.088	0.122	0.151	.178		.201	.224	.249	3:00A .320 7A	.114
0.025	0.058	0.090	0.124	0.152	.178		.201	.226	.247	L → .323	.101
0.026	0.059	0.090	0.124	0.153	.179		.203	.227	.250	.324	.093
0.027	0.061	0.093	0.126	0.155	.181		.203	.229	.252	.326	.084
0.027	0.062	0.094	0.126	0.155	.181	8/1100	.204	.229	.252	.327	.78
0.029	0.064	0.096	0.127	0.156	.182	12:01A	.204	.229	.253	.329	.78

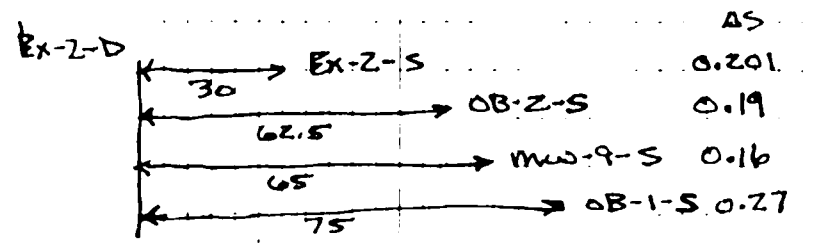
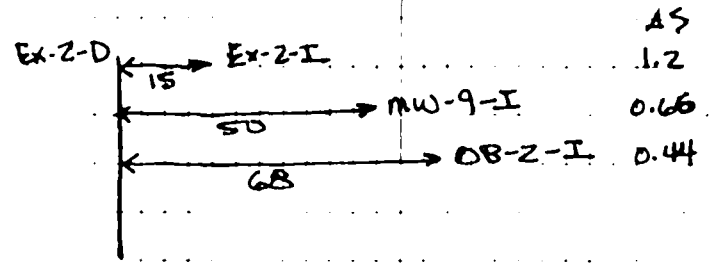
D. Marlow

BA 0.084
 0.088
 0.094
 0.106
 0.111
 0.113

	#		ex. Dist. FT
800 P	2100		
MW 9-S	2100	0.161	65
MW 9-I	2200	0.656	50
MW 9-D	4400	8.118	40
Ex-2-S	1300	0.201	30
Ex-2-I		1.119	15
Ex-2-D		46.445	0
OB-1-S		0.272	75
OB-1-D		6.692	72.5
OB-2-S		0.186	62.5
OB-2-I		0.436	68
OB-2-D		6.188	75



AS
 8.1
 6.7
 6.2



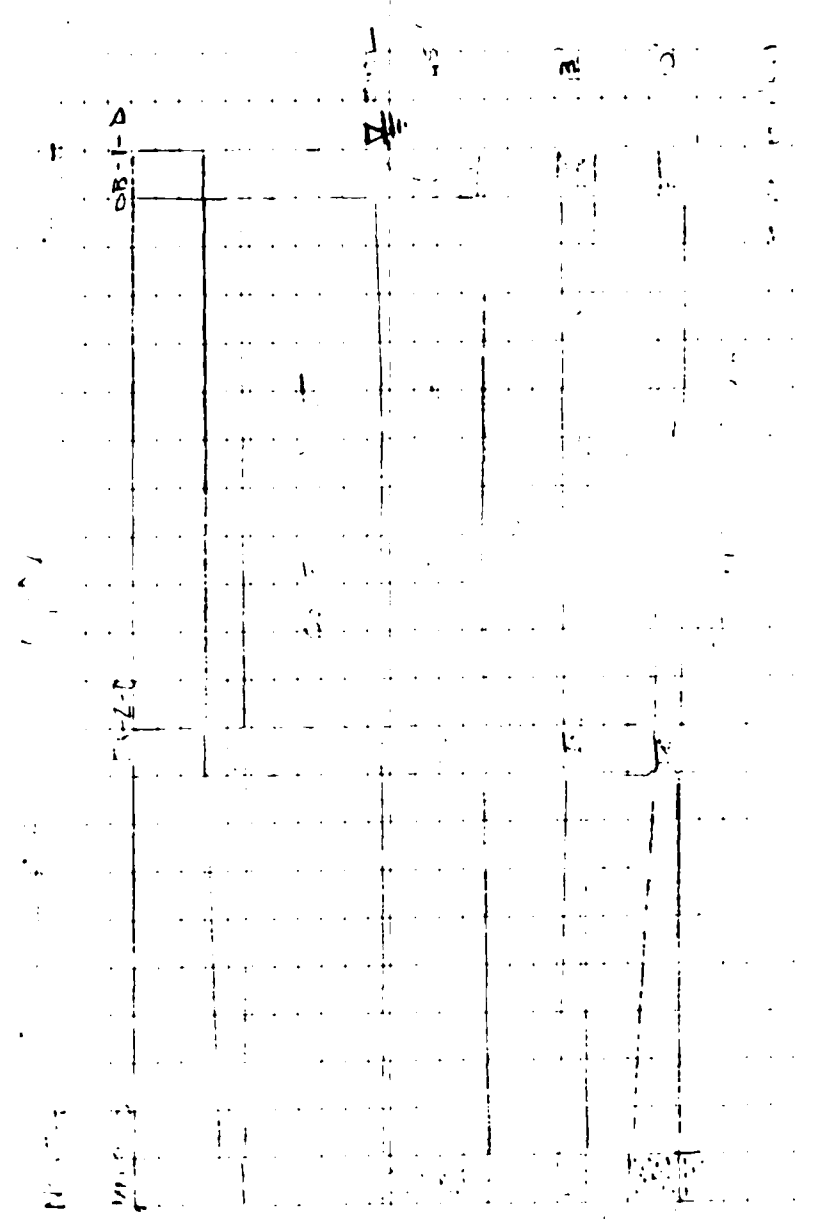
15 hrs
 10:00
 8:00-11:00 plot Tankage
 11:00 to 1:00

Point	Dist.	Value
Ex-2-D	75	45.6
MW 9-D	72.5	116.75
OB-1-D	72.5	
OB-2-D	75	

gals

Handwritten notes on the left side of the page, including:

- 1. ...*
- 2. ...*
- 3. ...*
- 4. ...*
- 5. ...*
- 6. ...*
- 7. ...*
- 8. ...*
- 9. ...*
- 10. ...*
- 11. ...*
- 12. ...*
- 13. ...*
- 14. ...*
- 15. ...*
- 16. ...*
- 17. ...*
- 18. ...*
- 19. ...*
- 20. ...*



Handwritten text at the bottom right of the page:

(1) #107

D. Marlow

10:00	10.0
10:15	10.0
10:30	10.0
10:45	10.0
11:00	10.0
11:15	10.0
11:30	10.0
11:45	10.0
12:00	10.0
12:15	10.0
12:30	10.0
12:45	10.0
13:00	10.0

Rate 106 gpm

12 hrs

Sunny and hot

6:45A Arrive at site

pumping Rate 106 gpm

7:00A Ex-2-D 46.7 ft

7:48A TAKE water samples for analysis

8:00A pump turned off

let Reservoir fill 12:00p

move pump to Ex-2-I

10 hrs = 600 min

16 hrs 40 min = 1000 min

5 hrs = 300 min

1 hr = 60 min

will try to use log scale on

Ex-2-I pump test. Largest interval @ 1000 min

Need to switch Transducers

in Ex-2-D & Ex-2-I

SWL

SWL

110.0

110.33

Turn off pump

2:00p in hole Ex-2-I w/ pump

Probe 5 - Ex-2-D

Probe 6 - Ex-2-I

Start Hermit

Ex-2-S 13.7'

45 gal (18 gal)

Start pump @ 2:25p
50 gpm/min

P. Marlow

2:25p 50 gal/min D 5
69 13.7

↓
2:40p 100 gal/min 60.2 13.5

2:55p 150 103 11

Hum. T 37.1 #1 75 0.5
454/19 #2 91 6.0
#3 80 0.4
#4 EX25 0.77
#5 WED 1.93
#6 EX24 335

4:00p EX-2-I 180 ppm

5:15p Pumping Rate = 186

75 0.6
95 0.09
100 0.42
110 0.91
120 2.05
130 3.05

140 4.05

14H 35

175 2.10

180 2.05

but a amount of water being pumped
pumping rate = 180 ppm
Collect in a few days of treatment

11:00a R-186 ppm

~~186~~

D. Marlow

3:30p leave site

3:30p - 6:30p Plot up time

~~6:30p~~ 8:30p at site review DATA 14 hrs
August 6, 2000

ar.
6:45p ARRIVE at site
Q = 186 gpm

11:31a pull 1 Dr. Ex-2-I
will plot later

leave site @ 1:00p

4:30 - 7:30p

Plot Data for Ex-2-I
New Plots for Deep Aquifer

13 hrs

Aug 7, 2000
ARRIVED site @ 6:30a

Q = 184 gpm

11:31a pull 1 Dr.
11:32p pull 1 Dr.

George 577-121

Start Recovery
12:00p 1 hour of water level
water level, Ex-2-I with recovery
1.2 ft above original

1:30p 1 hour of water level
1:59p 1 hour of water level
2:16p 1 hour of water level

1:45p 1 hour of water level

2:00p pull pump 1
1:50p pull pump 2

3:00p install 1 Dr. set up
Recovery 1.2 ft

D. Maulow

107

4:30 - 4:55, 215, 216

4:55

Q = 20

5:00, 11-20, 11-21

5:20, 11-22

6:00 - 1:00

12:15

1:00

6:15, 11-23

6:30, 11-24

All well locations

9:15A Survey Complete

9:30A

10:00

108

10:00

Compute Distances

11:00

11:15

11:30

11:45

5:00 p. 11-25, 11-26, 11-27

5:20, 11-28

6:00 - 10:00 Plot in 11-29

11:00

14:15

D. Manley

6:45 AM Aug 2, 2000 at site
 Q = 20 gpm
 L = 7.457

Preliminary 1
 2.5 hrs
 1.5 hrs
 1.5 hrs

1:15 PM at the site
 W = 20 gpm
 L = 7.457

2:45 PM 20 gpm
 6:27 PM at site

11:00 AM at site
 Lead Hand
 Pump out
 13 hrs

6:45 AM
 $y = (2716.1(x)) + 7.713$ $x = .000045$ EP-1-I

7:05 AM
 $y = (25104.1(x)) + 0.2225$ $x = .178$ OB-2-I

7:25 AM
 $y = (24400.1(x)) + 2.445$ $x = .0045$ MW-7-I

1:00 PM
 1:15 PM
 1:26 PM

1:50 PM

1:26 PM 45,891 Not correct
 to be

$$x = \frac{T_{10}}{9710} = 0.0002$$

Aug 2, 2000

at site

1:55 PM
 2:00 PM
 2:05 PM

10:15p K. M. G. - 12
K. M. G.

Logger 95119
15457
Ex. well #
1111 or 1112
061111

11:30A Return to site K. M. G.
Logger, Turbidity etc

100p L. M. G. site

8:20 - 11:00
13420

D. M. G.

Calibrated Ph to 70 Solution
Calibrated conductivity to 1000 μ S/cm Solution

07:20 on site at well site MW-12
08:20 MW12-I depth 143.42
09:00 MW12-S depth 143.07
10:12 started pumping
10:19 water rate = 1.1 L/min
10:54 W-MW-12-S-091800-P collected for
total Cr and Cr VI
11:05 15 gal collected and placed into
large collection vessel for treatability
11:25 - arrived at well MW-7-I
depth to water = 116.65
11:34 started pumping water - rate adjusted
to 1.1 L/min
12:18 collected water samples
W-MW-7-I-091800-P } 1 bottle = Cr6
W-MW-7-I-091800-MS } 1 bottle =
total Cr
W-MW-7-I-091800-MSD
12:20 - 12:48 - collected 30 gallons
placed in large collection vessel for
treatability study
Well # MW-5-I @ 1350
1400 measured well at 100.56 feet
1407 started pumping - adjusted
to 1.0 L/min
1416 - starting monitoring water depth
was 100.56
K. M. G.
D. M. G.

1433 - ~1440 Lost prime on pump
 restarted & adjusted to 1 L/min
 1503 collected 2 (Cr6 & total Cr) samples
 labeled W-MW-5-I-091800-P
 1505-1516 collected 30 gallons for
 treatability study
 1600 - MW2-I - tested
 for depth of water @ 102.80
 1606 - started pumping, adjusted
 to ~1.0 L/min
 1614 - started to take readings
 1646 - collected 2 water samples
 W-MW-2-I-091800-P - (Cr total), 1 Cr6
 1740 preparation of log/shipping
 1750 - to Shipping/UPS

end of day
 1746
 09/18/08

0815 Calibrated pH probe with pH 7 solution
 Calibrated conductivity probe with 1000µS/cm solution
 09-19-08 0800 on site - waiting for crew
 0830 - crew got distilled water perm
 0845 on site at wells MW-1-D
 0900 - Depth to water at 106.56
 0910 - pumping started - flow adjusted
 to 1.0 L/min
 0918 readings started
 0953 collected 1 water sample
 W-MW-1-D-091900-P (total Cr)
 1030 set up on well MW-1-S
 depth to water = 107.00 feet
 1040 - started pumping - adjusted to ~1.0 L/min
 1051 - started monitoring
 1129 collected 1 water sample
 W-MW-1-S-091900-P (total Cr)
 1140 - measured Depth to water at 107.07 for
 well MW-1-I
 1147 - Pumping started - flow rate adjusted to 1.0 L/min
 1151 monitoring started
 1234 water sample collected W-MW-1-I-091900-P
 (total Cr)
 1240 - 30 gallons collected for treatability study
 1312 - lunch - also got DI water from well
 1350 - at site/well MW-4-D
 059 - initial depth to water 98.68'
 1420 - started pumping - adjusted flow to 1.0 L/min

K. Madden
 09/19/08

- 1426 - started monitoring
- 1516 collected 1 Sample W-MW-4-D-091900-P (total Cr) deconed equipment
- 1526 Well MW-4-I - depth to water = 96.50 feet
- 1537 - started pumping - Flow adjusted to 1.0 L/min
- 1617 collected 1 water sample W-MW-4-I-091900-P (total Cr)
- 1632 Well MW-4-S - initial depth to water = 96.02
- 1644 - left well to dump wastewater
- 1656 - started pumping - flow adjusted to ~1.0 L/min
- 1702 started monitoring
- 1730 collected 1 total Cr Sample # W-MW-4-S-091900 deconed - 1745
- 1800 - Shipping samples

end of day
091900
J.K. Madden

Note: Calibrated of meters at -0330 (pH=7) (cont = 1ms/cm) 09-21-00

- 09-20-00
- 0800 - on meeting site
- 0820 - at culligan getting water for decon
- 0840 At well site MW-6-I
- 0848 - took initial measurement of depth to water = 105.00'
- 0900 starting pumping - some problems with pumping - flow achieved and adjusted to 1.0 L/min at - 0939
- 0949 - started monitoring
- 1028 1 Sample collected W-MW-6-I-092000-P
- 1042 - initial ^{depth} sample measurement of depth to water = 106.1' For well MW-6-D
- 1050: started pumping adjust flow rate to 1.0 L/min
- 1108 - started monitoring
- 1141 - collected 1 water sample W-MW-6-D-092000-P
- 1222 - initial measurement of depth to water well MW-6-S
- 1257 1245 pumping started - flow rate adjusted to 1.0 L/min
- 1335 - conductivity OK - turbidity high - lots of PVC shavings coming up and in monitoring chamber - use of "I" button to clean turbidity probe - probe tested at ~1300 in culligan drinking water and turbidity was ~0.8
K. Madden

- 1340 Sample collected - total Cr - W-MW-6-S-092000-P
- 1415 Lunch after decon - also emptied waste water and did water depth on well behind Ace site - no water in well at bottom of ~ 32 feet
- 1525 - measured initial depth to water ^(?) of ACE-R-S,I,D well, at 104.03 from ground level (west side of casing)
- 1530 pumping started - adjusted flow rate to ~10 L/min
- 1541 - started monitoring of ACE-R-I - pump set to depth of 167' (screen depth 161-171) from ground level.
- 1631 - collected W-ACE-R-I-092000-P (total Cr)
- 1645 - after decon - measured depth to water @ 103.99' from ground level - set pump at 130' from ground level
- 1652 - started pumping - flow rate set to ~10 L/min
- 1715 - noticed air bubbles flowing into monitor possible pump cavitation? - bubbles periodic
- 1730 - collected sample W-ACE-R-S-092000-P
- 1815 - all decon completed - samples logged and sent to UPS

~~end of Day~~
 7/16/11
 092000

09-21-00

- 0800 - met crew on worksite
- 0835 - arrived at well ACE-R-D and calibrated meter - 2 pt ph calibration (pH4, pH7) and 1000 μ m for conductivity
- 0845 - at site for well ACE-R-D
- Depth meter appears to be malfunctioning ^{probably conduct} get other meter -
- 0900 - depth to water measured at 104.00' ^{probably correct} note: much higher water level than yesterday
- 0910 - pumping started water level adjusted to 10 L/min
- 0920 - fixed other water meter
- 0935 - started monitoring
- 1022 - collected 1 total Cr sample - W-ACE-R-D-092000-P
- 1024 - began decon - also dumped waste water
- 1104 - arrived at OB-1 cluster - started OB-1-I
- 1112 - initial depth to water at 112.17'
- 1120 - pumping started - flow adjusted to 10 L/min
- 1131 - started monitoring
- 1200 - collected W-OB-1-I-092000-P (total chrome)
- 1225 - decon
- 1235 - move to OB-1-S
- 1240 - Initial ^{depth} sample of OB-1-S at 112.08'
- 1300 - started pumping - adjusted flow to 10 L/min
- 1355 - collected W-OB-1-S-092000-P (total Cr)

K. Madden

1430 initial measure - depth to water at 109.56
 for OB-2-D
 1440 - started pumping - flow rate adjusted
 to ~1.0 L/min
 1506 started monitoring
 1554 collected total Cr sample W-10B-2 0.092001
 1612 well OB-2-I initial depth to
 water measured 108.15
 1622 - pumping - flow set at 1.0 L/min
 1635 - sample / mon for
 1717 - W-OB-2-I-092100-P collected
 1800 - sample & treatability water
 left at UPS
 1810 - end of day

W. Madden
 and of Day
 092100
 092100

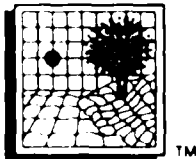
09-22-00
 0800 - at ido site
 0825 - calibration of monitoring probes
 Ph = 2 point - soln for pH 4 & pH 7
 conductivity = soln 1000 μ S/cm
 0830 - power problem with monitoring
 module - tested AC converter finally
 switched to car AC supply
 0851 - at well OB-2-S - well initially
 measured to water at 109.30 feet
 - micropurge pump lowered to 120 feet
 0910 - started pumping
 0917 - flow rate adjusted to ~1.0 L/min
 0921 - monitoring started
 1016 - sample W-OB-2-S-092200-P
 collected
 1022 - Rinse sample collected
 1046 at side of well MW-2-S
 1051 - depth to water 102.49 feet
 1102 flow rate set at 1.0 L/min
 1107 - started monitoring
 1202 - took sample W-MW-2-S-092200-P
 1204 - down - final
 1240 - lunch
 1310 - met to prepare for simultaneous
 reading of well depths

well	depth readings	time or reading
MW-8-S	108.28	1340
MW-8-I	107.80	1337
MW-8-O	107.89 / 107.89	1332
	Gary F's meter	K. Madden meter
MW-9-S	112.95	1349
MW-9-I	111.81	1352
MW-9-O	113.29	1354
MW-11-S	119.81	1402
MW-11-I	120.16	1404
MW-11-O	122.49	1406
MW-12-S	143.24	1419
MW-12-I	143.57	1416
MW-12-O	144.65	1414

Personal Well monitoring
 1445 arrived 1940 E. 4th (metzger house) RW-06
 1450 - started monitoring
 1510 - took last monitoring reading and collected 1 total Cr sample w- RW-06-092200-P
 1516 - arrived at 1650 E. 4th (Havel Residence) well RW-05
 1516 - started tap through hose
 1521 - started monitoring
 1537 - took 3 total Cr samples w- RW-05-092200-P, w- RW-05-092200-MS and w- RW-05-092200-MSD

1541 - arrived at 175 thompson Dr. at Leopold Residence - RW-01 well
 1546 - started monitoring
 1606 - last monitoring
 1603 - collected 1 total Cr w- RW-01-092200-P
 1630 - Arrived at Smith residence RW-08 started well water running through garden hose
 1641 - started monitoring
 1702 - collected sample w- RW-08-092200-P
 1720 - decommissioning equipment, getting materials ready to ship

Appendix E
Chain-of-Custody Records



CHAIN OF CUSTODY RECORD

SOUTHWEST LABORATORY OF OKLAHOMA, INC.

1700 W. Albany • Broken Arrow, Oklahoma 74012-1421
Office: 918-251-2858 • Fax 918-251-2599

SAMPLING FIRM
Fletcher Vachek

CLIENT CONTACT
Craig Fisk

PHONE NUMBER
918-2459 6583

P.O. or PROPOSAL NUMBER
46118.124

PROJECT NAME
Are Services

SAMPLER (Signature)
[Signature]

ANALYTICAL TESTS REQUESTED									
<i>Total Cr</i>	<i>Hex Cr</i>								

SAMPLE NO	DATE	TIME	COMP	GRAB	LOCATION	MATRIX	NUMBER OF CONTAINERS	REMARKS												
	7-18-00	1010		X	W-MW-12-I-091800-P	W	2	1	1											
	7-18-00	1054		X	W-MW-12-S-091800-P	W	2	1	1											
	9-18-00	1151		X	W-MW-11-I-091800-P	W	2	1	1											
	9-18-00	1151		X	W-MW-11-I-091800-D	W	2	1	1											
	9-18-00	1210		X	W-MW-7-I-091800-P	W	6	3	3											
	9-18-00	1235		X	W-MW-11-S-091800-R	W	2	1	1											
	9-18-00	1355		Y	W-MW-11-S-091800-P	W	2	1	1											
	9-18-00	1503		X	W-MW-5-S-091800-P	W	2	1	1											
	9-18-00	1540		X	W-MW-2-D-091800-P	W	2	1	1											
	9-18-00	1646		X	W-MW-2-I-091800-P	W	2	1	1											
	9-18-00	1745		X	W-MW-2-D-091800-P	W	2	1	1											

*Duplicate (R)
Include ms/ms volume
Remade (R)*

RELINQUISHED BY (Signature) <i>[Signature]</i>	DATE 7-18-00	TIME 1800	RECEIVED BY (Signature) <i>UPS</i>
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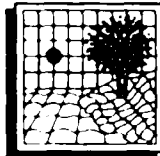
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RELINQUISHED BY (Signature)	DATE	TIME	RECEIVED FOR LABORATORY BY (Signature)
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RELINQUISHED BY (Signature)	DATE	TIME	RECEIVED BY (Signature)
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REMARKS



CHAIN OF CUSTODY RECORD

SOUTHWEST LABORATORY OF OKLAHOMA, INC.

1700 W. Albany • Broken Arrow, Oklahoma 74012-1421
Office: 918-231-2858 • Fax 918-231-2999

SAMPLING FIRM
Chil + Vach

CLIENT CONTACT
Gee, Farkas

PHONE NUMBER
918-231-6583

P.O. or PROPOSAL NUMBER
40118.124

PROJECT NAME
Aco Services

SAMPLER (Signature)
[Signature]

ANALYTICAL TESTS REQUESTED

SAMPLE NO	DATE	TIME	COMP	GRAB	LOCATION	MATRIX	NUMBER OF CONTAINERS	ANALYTICAL TESTS REQUESTED										REMARKS						
								Total C	H2S C	①	②	TOC	Ammonia	Sulfide										
	7-11-00	0955		X	W-EX-2-I-09100	P/W	2	1	1															
	7-11-00	1111		X	W-PWS-8-01100	P/W	2	1	1															
	7-19-00	1315		X	W-EX-2-S-01100	P/W	1	1																
	7-19-00	1450		X	W-MW-9-S-09100	P/W	1	1																
	7-19-00	1450		X	W-MW-9-S-09100	D/W	1	1																
	7-17-00	1600	100	X	W-IX-TS-1-01100	P/W	6	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
	7-17-00	1655		X	W-MW-9-I-01100	P/W	1																	
	7-17-00	1700		X	W-1-D-01100	P/W	1	1																
	7-17-00	1700		X	W-MW-1-S-09100	P/W	1	1																
	07-11-00	1239		X	W-MW-1-I-09100	P/W	1	1																
	07-11-00	1516		X	W-MW-4-D-09100	P/W	1	1																
	07-11-00	1617		X	W-MW-4-I-09100	P/W	1	1																
	07-19-00	1730		X	W-MW-4-S-09100	P/W	1	1																

① Al, Cl, F, NO₃, NO₂, SO₄, TDS, BTSS, TC, S. bic, orthophosphate, bicarbonate

② Al, Ca, Fe, Mg, Mn, K, Na, Sr, Ba

RELINQUISHED BY (Signature) *[Signature]* DATE 7-17-00 TIME 1400 RECEIVED BY (Signature) UPS 125E810W211000 0069

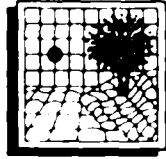
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RELINQUISHED BY (Signature) DATE TIME RECEIVED BY (Signature)

RELINQUISHED BY (Signature) DATE TIME RECEIVED FOR LABORATORY BY (Signature)

RELINQUISHED BY (Signature) DATE TIME RECEIVED BY (Signature)

REMARKS



CHAIN OF CUSTODY RECORD

SOUTHWEST LABORATORY OF OKLAHOMA, INC.

1700 W. Albany • Broken Arrow, Oklahoma 74012-1421
Office: 918-251-2898 • Fax: 918-251-2999

SAMPLING FIRM SVE	CLIENT CONTACT Guy [unclear]	PHONE NUMBER [unclear]
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P.O. or PROPOSAL NUMBER 48-H-124	PROJECT NAME [unclear]
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SAMPLER (Signature): *[Signature]*

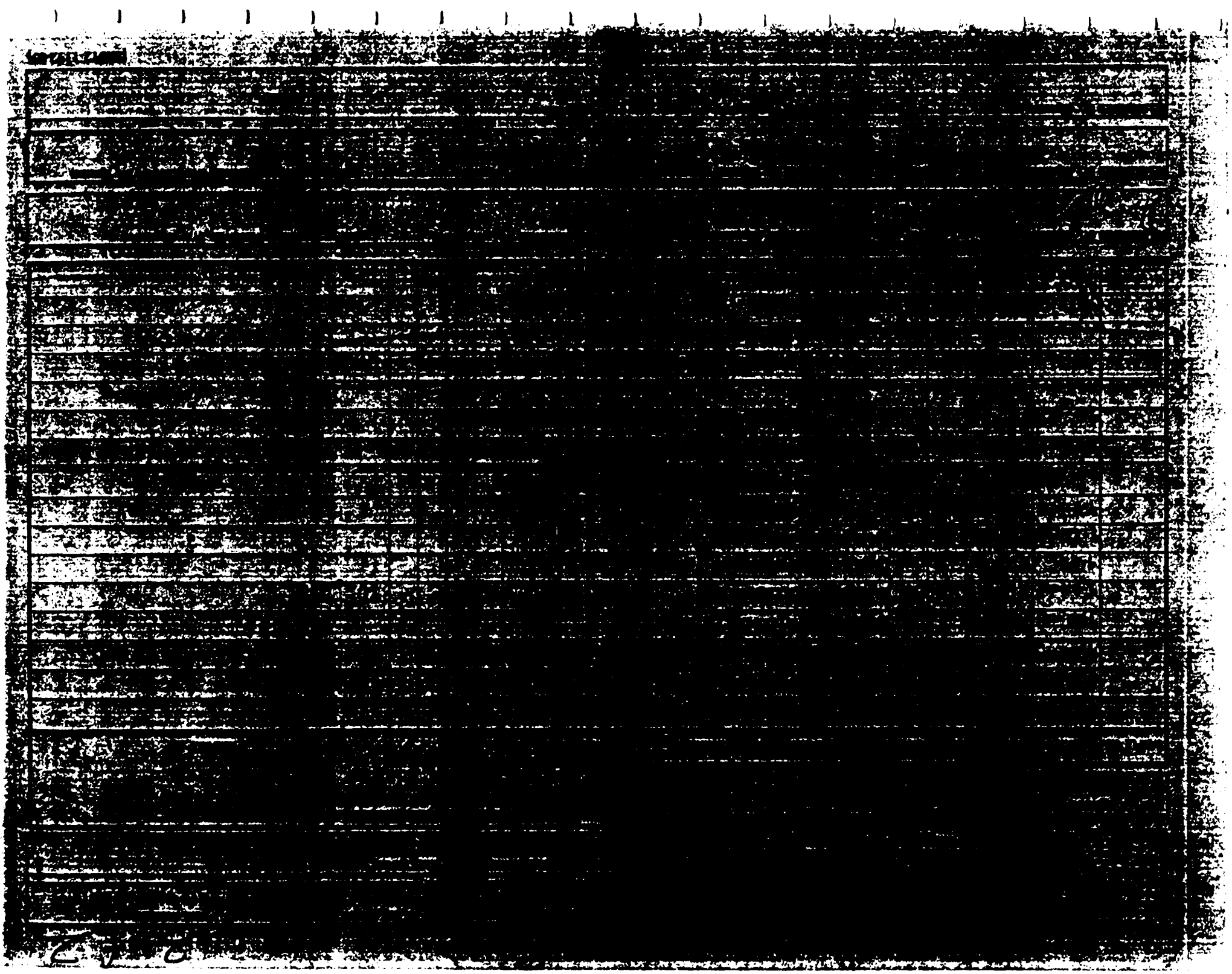
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1	2	3	4	5	6	7	8	9	10	
<i>[Diagonal lines]</i>										

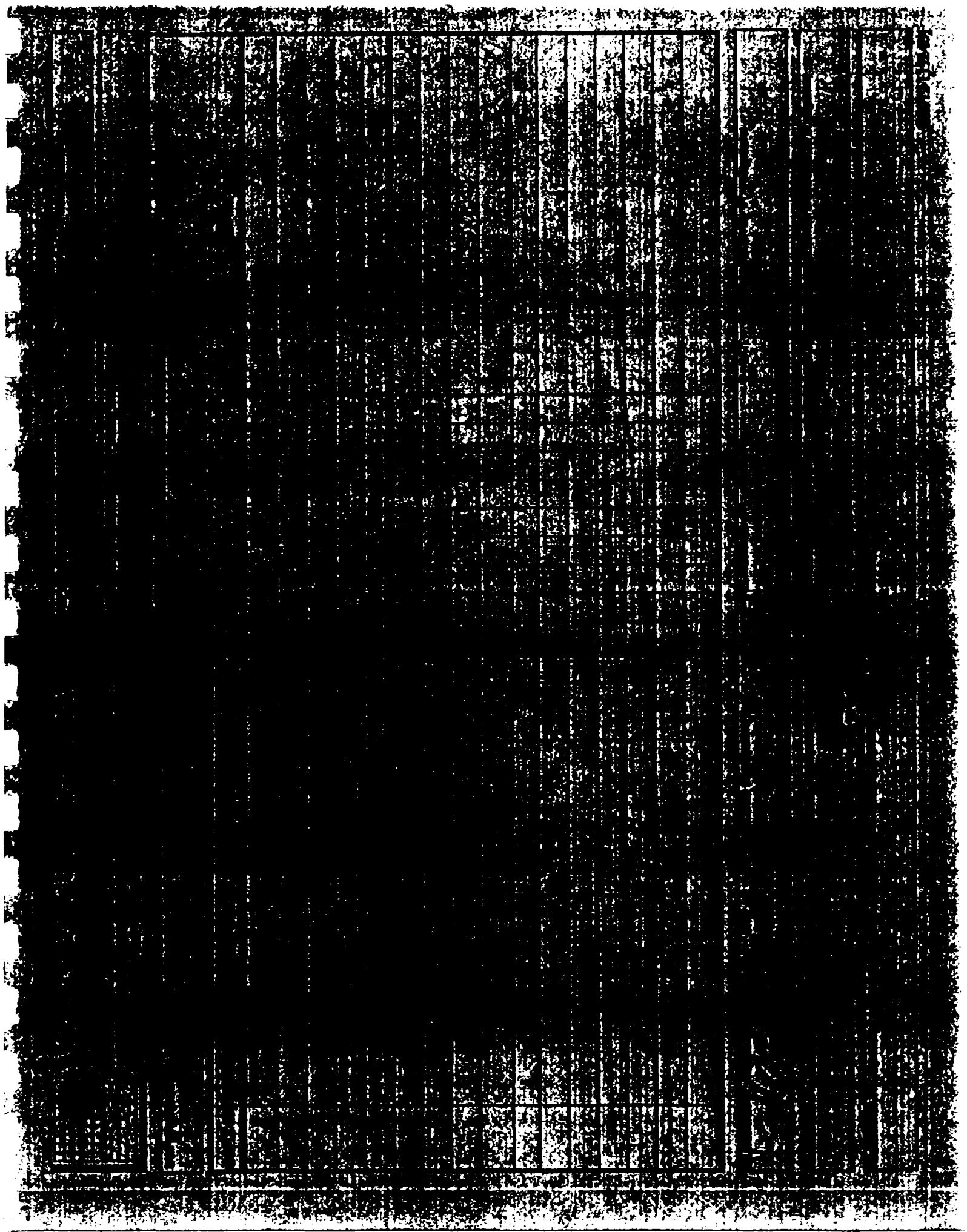
SAMPLE NO	DATE	TIME	COMP	GRAB	LOCATION	MATRIX	NUMBER OF CONTAINERS	1	2	3	4	5	6	7	8	9	10	REMARKS
	9-20-00	0910		X	W-MW-9-D-092000-PW		1	1										
	9-20-00	1045		X	W-MW-12-D-092000-PW		1	1										
	9-20-00	1045		X	W-MW-12-D-092000-DW		1	1										Indicate
	9-20-00	1225		X	W-HPMW-6-S-092000-PW		3	3										m/m/d volume
	9-20-00	1405		X	W-HPMW-9-S-092000-PW		1	1										
	9-20-00	1505		X	W-ACE-R-092000-RW		1	1										Rate
	9-20-00	1540x		X	W-MW-8-S-092000-PW		1	1										
	9-20-00	1655		X	W-MW-8-I-092000-PW		1	1										
	9-20-00	1028		X	W-MW-6-I-092000-PW		1	1										
	9-20-00	1740		X	W-MW-6-S-092000-PW		1	1										
	9-20-00	1141		X	W-MW-6-S-092000-PW		1	1										
	9-20-00	1631		X	W-ACE-R-I-092000-PW		1	1										
	9-20-00	1758		X	W-ACE-R-S-092000-PW		1	1										
<i>[Handwritten signature and date]</i>																		

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Appendix F
Airbills

ups **UPS Next Day Air**
UPS Worldwide Express
Shipping Document

See instructions on back. Call 1-800-PICK-UPS (800-742-5877) for additional information.

TRACKING NUMBER **1Z OE8 10W 22 1000 067 4**

SHIPMENT FROM
SHIPPER'S UPS ACCOUNT NO **0 E 8 1 0 W**

REFERENCE NUMBER
0461180123

NAME **Gary Felkner** TELEPHONE **913-458-2000**

COMPANY
BLACK & VEATCH SPEC PROJ CORP

STREET ADDRESS
6601 COLLEGE BLVD

CITY AND STATE **OVERLAND PARK KS** ZIP CODE **66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Dave LeMaster** TELEPHONE **(918) 251-2858**

COMPANY
SW Labs

STREET ADDRESS **1700 W. Albany** DEPT./FLOOR

CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow, OK** ZIP CODE **74012**



3	WEIGHT ENTER LTR IF FEET	DIMENSIONAL WEIGHT If Applicable	SHIPPER'S COPY
4	TYPE OF SERVICE <input checked="" type="checkbox"/> NEXT DAY AIR <input type="checkbox"/> WORLDWIDE EXPRESS (INTERNATIONAL)		CHARGES
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7	METHOD OF PAYMENT <input checked="" type="checkbox"/> BILL SHIPPER <input type="checkbox"/> BILL RECEIVER <input type="checkbox"/> BILL THIRD PARTY <input type="checkbox"/> CREDIT CARD <input type="checkbox"/> American Express <input type="checkbox"/> Diner's Club <input type="checkbox"/> MasterCard <input type="checkbox"/> Visa		

8) RECEIVERS / THIRD PARTYS UPS ACCT NO OR MAJOR CREDIT CARD NO EXPIRATION DATE

THIRD PARTY'S COMPANY NAME

STREET ADDRESS

CITY AND STATE ZIP CODE

9) SHIPPER'S SIGNATURE **X Gary Felkner**

DATE OF SHIPMENT **7/12/00**
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ups **UPS Next Day Air**
UPS Worldwide Express
Shipping Document

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TRACKING NUMBER **1Z OE8 10W 22 1000 073 6**

SHIPMENT FROM
SHIPPER'S UPS ACCOUNT NO **0 E 8 1 0 W**

REFERENCE NUMBER
0461180123

NAME **Gary Felkner** TELEPHONE **913-458-2000**

COMPANY
BLACK & VEATCH SPEC PROJ CORP

STREET ADDRESS
6601 COLLEGE BLVD

CITY AND STATE **OVERLAND PARK KS** ZIP CODE **66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Randy Staggs** TELEPHONE **(918) 251-2858**

COMPANY
SW Laboratory

STREET ADDRESS **1700 W. Albany** DEPT./FLOOR

CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow, OK** ZIP CODE **74012**



3	WEIGHT ENTER LTR IF FEET	DIMENSIONAL WEIGHT If Applicable	SHIPPER'S COPY
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8) RECEIVERS / THIRD PARTYS UPS ACCT NO OR MAJOR CREDIT CARD NO EXPIRATION DATE

THIRD PARTY'S COMPANY NAME

STREET ADDRESS

CITY AND STATE ZIP CODE

9) SHIPPER'S SIGNATURE **X Randy Staggs**

DATE OF SHIPMENT **7/13/00**

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TRACKING NUMBER **1Z 0E8 10W 22 1000 072 7**

SHIPMENT FROM
SHIPPER'S UPS ACCOUNT NO **0E810W**

REFERENCE NUMBER **0461180123**

NAME **Gary Felkner** TELEPHONE **913-458-2000**

COMPANY **BLACK & VEATCH SPEC PROJ CORP**

STREET ADDRESS **6601 COLLEGE BLVD**
CITY AND STATE **OVERLAND PARK KS** ZIP CODE **66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Randy Stagg** TELEPHONE **(918) 251-2858**

COMPANY **SW Labs**

STREET ADDRESS **1700 W. Albany**

CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow, OK** ZIP CODE **74012**



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TRACKING NUMBER **1Z 0E8 10W 21 1000 022 9**

SHIPMENT FROM
SHIPPER'S UPS ACCOUNT NO **0E810W**

REFERENCE NUMBER **0461180123**

NAME **Gary Felkner** TELEPHONE **913-458-2171**

COMPANY **BLACK & VEATCH**

STREET ADDRESS **6601 COLLEGE BLVD**
CITY AND STATE **OVERLAND PARK KS** ZIP CODE **66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Randy Stagg** TELEPHONE **(918) 251-2858**

COMPANY **SW Lab of OK**

STREET ADDRESS **1700 West Albany**

CITY AND STATE **Broken Arrow, OK** ZIP CODE **74012**

3 EARLIEST DELIVERY TIME

7:00

3	WEIGHT ENTER LTR IF LETTER	DIMENSIONAL WEIGHT * Applicable	SHIPPER'S COPY
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6	ADDITIONAL HANDLING CHARGE		
7	TOTAL CHARGES		
8	METHOD OF PAYMENT <input checked="" type="checkbox"/> BILL SHIPPER <input type="checkbox"/> BILL RECEIVER <input type="checkbox"/> BILL THIRD PARTY <input type="checkbox"/> CREDIT CARD <input type="checkbox"/> American Express <input type="checkbox"/> Discover <input type="checkbox"/> MasterCard <input type="checkbox"/> Visa <input type="checkbox"/> CHECK		
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			0101911202609 2/99 M

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7	SHIPPER'S SIGNATURE X Gary Felkner	DATE OF SHIPMENT 9/18/00	

ups Next Day Air[®] Early A.M.
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TRACKING NUMBER **1Z 0E8 10W 21 1000 006 9**

SHIPMENT FROM
UPS ACCOUNT NO
0E810W

REFERENCE NUMBER
0461180123

NAME **Gary Felkner** TELEPHONE **913-458-2171**
COMPANY

BLACK & VEATCH
STREET ADDRESS
6601 COLLEGE BLVD
CITY AND STATE **OVERLAND PARK** ZIP CODE **KS 66211 1504**

EXTREMELY URGENT DELIVERY TO
NAME **Randy Staggs** TELEPHONE **(918) 251-2858**
COMPANY
SW Lab of OK
STREET ADDRESS **1700 W. Albany** DEPT./FLR
CITY AND STATE **Broken Arrow OK** ZIP CODE **74012**

EARLIEST DELIVERY TIME **7:00**

0201811288008 8/28 W

WEIGHT **3915** DIMENSIONAL WEIGHT **104** SHIPPER'S COPY

TYPE OF SERVICE
 SATURDAY PICKUP SATURDAY DELIVERY
 DECLARED VALUE C.O.D.
 VERBAL CONFIRMATION OF DELIVERY

ADDITIONAL HANDLING CHARGE
 An Additional Handling Charge applies for certain items. See instructions.

TOTAL CHARGES

METHOD OF PAYMENT
 Bill Shipper Bill Receiver Bill Third Party Credit Card American Express Check

RECEIVERS / THIRD PARTY'S UPS ACCT NO OR MAJOR CREDIT CARD NO EXPIRATION DATE

THIRD PARTY'S COMPANY NAME

STREET ADDRESS

CITY AND STATE ZIP CODE

SHIPPER'S SIGNATURE **X Gary Felkner** DATE OF SHIPMENT **9/19/00**

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TRACKING NUMBER **1Z 0E8 10W 22 1001 149 3**

SHIPMENT FROM
UPS ACCOUNT NO
0E810W

REFERENCE NUMBER
0461180123

NAME **GARY FELKNER** TELEPHONE **913-458-6583**
COMPANY

BLACK & VEATCH SPEC PROJ CORP
STREET ADDRESS
6601 COLLEGE BLVD
CITY AND STATE **OVERLAND PARK** ZIP CODE **KS 66211**

EXTREMELY URGENT DELIVERY TO
NAME **Randy Staggs** TELEPHONE **(918) 251-2858**
COMPANY
SW Lab of OK
STREET ADDRESS **1700 West Albany** DEPT./FLR
CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow OK** ZIP CODE **74012**

WEIGHT **30** DIMENSIONAL WEIGHT **104** SHIPPER'S COPY

TYPE OF SERVICE
 NEXT DAY AIR EXPRESS (INTL)
FOR WORLDWIDE EXPRESS SHIPMENTS
 SATURDAY PICKUP SATURDAY DELIVERY
 INSURED VALUE C.O.D.
 An Additional Handling Charge applies for certain items. See instructions.

ADDITIONAL HANDLING CHARGE
 An Additional Handling Charge applies for certain items. See instructions.

TOTAL CHARGES

METHOD OF PAYMENT
 Bill Shipper Bill Receiver Bill Third Party Credit Card American Express Check

RECEIVERS / THIRD PARTY'S UPS ACCT NO OR MAJOR CREDIT CARD NO EXPIRATION DATE

THIRD PARTY'S COMPANY NAME

STREET ADDRESS

CITY AND STATE ZIP CODE

SHIPPER'S SIGNATURE **X Gary Felkner** DATE OF SHIPMENT **9/20/00**

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Shipping Document

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TRACKING NUMBER **1Z 0E8 10W 22 1000 096 9**

1 SHIPMENT FROM

SHIPPER'S UPS ACCOUNT NO
0 E 8 1 0 W

REFERENCE NUMBER
0461180123

NAME **Gary Felkner** TELEPHONE **913-458-2000**

COMPANY **BLACK & VEATCH SPEC PROJ CORP**

STREET ADDRESS
6601 COLLEGE BLVD

CITY AND STATE **OVERLAND PARK** ZIP CODE **KS 66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Randy Staggs** TELEPHONE **(918)251-2858**

COMPANY **SW Lab of OK**

STREET ADDRESS **1700 W. Albany** DEPT/FLOOR

CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow, OK** ZIP CODE **74012**



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TRACKING NUMBER **1Z 0E8 10W 22 1000 097 8**

1 SHIPMENT FROM

SHIPPER'S UPS ACCOUNT NO
0 E 8 1 0 W

REFERENCE NUMBER
0461180123

NAME **Gary Felkner** TELEPHONE **913-458-2000**

COMPANY **BLACK & VEATCH SPEC PROJ CORP**

STREET ADDRESS
6601 COLLEGE BLVD

CITY AND STATE **OVERLAND PARK** ZIP CODE **KS 66211 1504**

2 EXTREMELY URGENT DELIVERY TO

NAME **Randy Staggs** TELEPHONE **(918)251-2858**

COMPANY **SW Lab of OK**

STREET ADDRESS **1700 W. Albany** DEPT/FLOOR

CITY AND STATE (INCLUDE COUNTRY IF INTERNATIONAL) **Broken Arrow OK** ZIP CODE **74012**



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7	TOTAL CHARGES		
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6	ADDITIONAL HANDLING CHARGE		
7	TOTAL CHARGES		
8	RECEIVERS / THIRD PARTYS UPS ACCT NO OR MAJOR CREDIT CARD NO		EXPIRATION DATE
9	SHIPPER'S SIGNATURE <i>X Gary Felkner</i>		DATE OF SHIPMENT 9/22/00

**Appendix G
Survey Data**

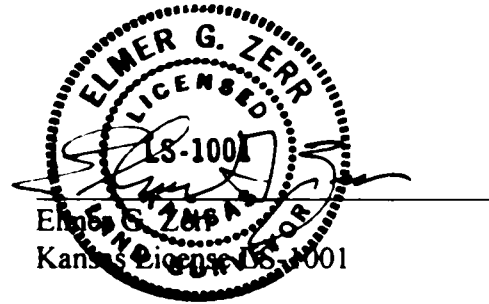
ACE SERVICES
Colby, Kansas

Well Designation	Coordinates *		Elevation	
	North	East	Top of Casing	Top of North Side of Flush Mount Ring
OB 1S	9380.08607	10308.46867	3142.71	3143.05
OB 1I	9378.57019	10328.25223	3142.31	3142.66
OB 1D	9362.49239	10332.46531	3141.98	3142.29
OB 2S	9377.06295	10392.88955	3139.59	3139.86
OB 2I	9377.94194	10402.35013	3138.63	3138.91
OB 2D	9377.88098	10412.45754	3138.11	3138.47
EX 2S	9449.78932	10336.29564	3142.13	3142.42
EX 2I	9441.91718	10347.99760	3141.30	3141.57
EX 2D	9434.31623	10358.43995	3140.50	3140.89

* Assumes the Coordinates of the SW Corner of 32-07-33 to be N = 9079.96000, E = 10000.00000

ACE SERVICES
Colby, Kansas

Well Designation	Distance From SW Corner of 32-07-33		2.5 Acre Tract Location
	North	East	
OB 1S	300	308	SW SW SW SW
OB 1I	299	328	SW SW SW SW
OB 1D	283	332	SW SW SW SW
OB 2S	297	393	SW SW SW SW
OB 2I	298	402	SW SW SW SW
OB 2D	298	412	SW SW SW SW
EX 2S	370	336	NE SW SW SW
EX 2I	362	348	NE SW SW SW
EX 2D	354	358	NE SW SW SW



Appendix H
Pump Test Results

TECHNICAL MEMORANDUM

USEPA
Ace Services Site
Pump Test Results

BVSPC Project 46118.126
BVSPC File D.3 ✓
November 13, 2000

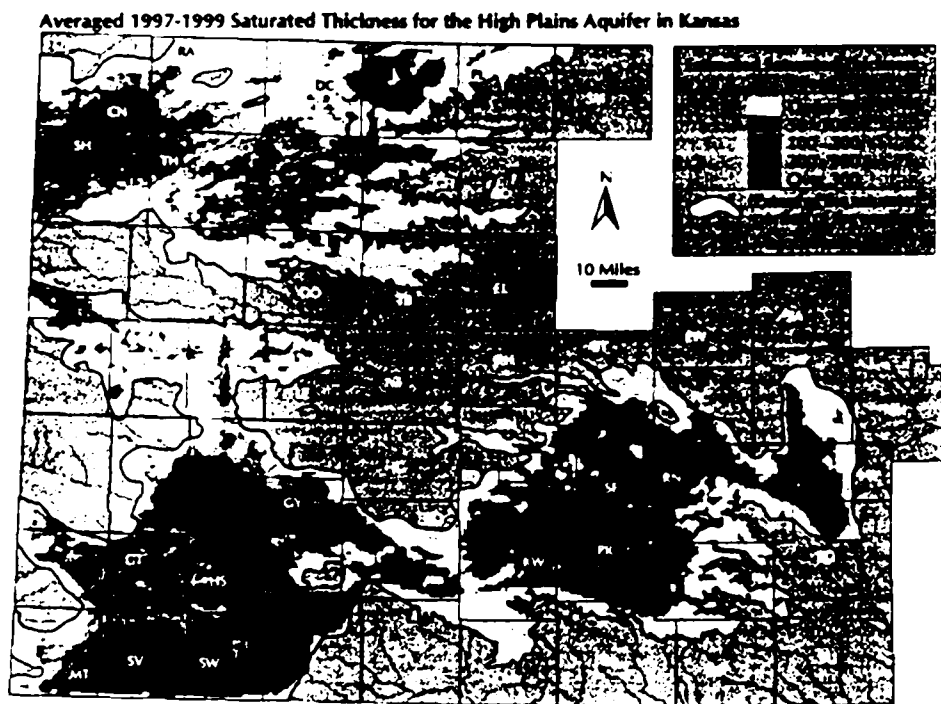
INTRODUCTION

In August 2000, a pump test was conducted at the Ace Services site in Colby, Kansas. The purpose of the pump test was to characterize the High Plains aquifer in the vicinity of the Ace Services site. Results of the pumping test will be used to model the hydraulic properties of the aquifer and to develop a design for a pump and treat remedial alternative for the Ace Services site. Three 72-hour pumping tests were conducted at three separate hydrologic zones within the aquifer to determine the transmissivity and hydraulic conductivity of the aquifer.

The City of Colby, Kansas relies upon the High Plains aquifer for its source of potable water (Figure 1). The High Plains aquifer is the principal source of water for the High Plains region. The High Plains aquifer consists primarily of sediments within the Ogallala Formation of Miocene age. The Ogallala consists of unconsolidated gravel, sand, silt, and clay. Locally, it also includes caliche, which is deposited as thin, discontinuous, layers within the upper portions of the formation. The Ogallala Formation was deposited by an extensive eastward flowing system of braided streams that drained the eastern slopes of the Rocky Mountains during the late Tertiary Period.

Unconsolidated deposits of Quaternary age overlie the Ogallala Formation. These deposits consist of gravel, sand, silt, and clay, much of which is reworked material that was derived from the Ogallala Formation. Deposits of loess overlie the Ogallala Formation or the unconsolidated Quaternary sediments at some locations.

FIGURE 1



Modified from U.S.G.S., 1997

SITE GEOLOGIC CONDITIONS:

The lithology of the unconsolidated sediments, determined from soil samples collected during the drilling of the extraction and observation wells, indicates a highly stratified aquifer consisting of sand, gravelly sand, silt, and clay. The thickness of the unconsolidated sediments (Ogallala Formation) was approximately 230 feet thick. Multicolored shale of the Pierre Shale Formation underlies the unconsolidated sediments at 230 feet. The site subsurface stratigraphy is generalized by the following:

Depth (ft)	Lithology	Remarks
0 - 30	Silt, Sandy Silt (Loess)	Dry
30 - 57	Sand and Silty Clay	Dry
57 - 105	Silt, Clay, and Sand	Dry to moist
105 - 135	Sand, some gravel w/ Silty Clay layers	Shallow Aquifer Zone
135 - 145	Sand and Clay (w/ interbedded caliche)	Shallow Aquifer Zone
145 - 190	Gravelly Sand w/ thin clay lenses	Intermediate Aquifer Zone
190 - 207	Clay and Silty Clay	Semi-Confining Unit
207 - 230	Gravelly Sand w/ thin clay lenses	Deep Aquifer Zone
230 +	230 +	Bedrock (Pierre Shale)

REGIONAL HYDROGEOLOGY

The average saturated thickness of the High Plains aquifer in Kansas is approximately 90 feet. Water in the High Plains aquifer generally is under unconfined conditions. However, in some locations, water levels in wells completed in portions of the aquifer may rise or fall slightly in relation to the regional water table because of artesian pressure created by local confining beds. Generally the ground water gradient within the aquifer is from west to east. Water moves in response to the slope of the water table, which typically averages between 10 to 15 feet per mile. On the basis of these average gradients and aquifer hydraulic properties, the regional velocity of water that moves through the aquifer is estimated to average about 1 foot per day. Regional transmissivity values typically range from 40,000 to 60,000 gallons per day/ft with storage coefficients ranging from 0.14 to 0.27 (Miller and Appel, U.S.G.S. Ground Water Atlas, 1997).

SITE HYDROGEOLOGY

Water levels measured during the remedial investigation indicate a slightly downward gradient within the aquifer surrounding the Ace Services site. Locally ground water flows to the east-southeast at horizontal gradients ranging from 0.0022 - 0.0032 ft/ft. Continuous water level monitoring prior to the pump test activities indicated that the shallow and intermediate zones within the aquifer function as a typical unconfined aquifer. However, monitoring data from the deep zone, collected prior to the pumping activities suggest that this lower zone acts as a semi-confined unit. Diurnal fluctuations in hydraulic head prior to the pump test occurred only in observation wells screened in the deep zone. These fluctuations suggest significant lateral influence by water supply wells pumping from the deep zone portion of the aquifer.

PUMPING TESTS

Pumping tests were conducted at the Ace Services site within the Ogallala aquifer in Colby, Kansas from July 31 to August 10, 2000. Three 72-hour pump tests were conducted within each hydrologic interval. Changes in water levels within the three extraction wells and nine observation wells were measured during pumping tests using pressure transducers attached to a Hermit 3000 data recording device. An atmospheric transducer was also installed near the surface in one of the wells (MW-6) to monitor atmospheric pressure changes during the test. The data recorders were programmed to take readings at 1-minute intervals during the duration of the tests.

The extraction wells were screened at three different intervals: shallow, intermediate, and deep zones within the aquifer. The observation wells consisted of three well nests of three wells per nest. Each nest of wells contained a well screened in the shallow, intermediate, and deep zones of the aquifer. A plan of the extraction wells and observation wells is shown in Figure 2. The following table gives well numbers, locations, elevation of top of casing, depth to static water level, and the screened interval.

Table 1

<u>Well Number</u>	<u>Northing</u>	<u>Easting</u>	<u>Elevation TOC Ft.</u>	<u>Static W.L. Depth in Ft. bgs</u>	<u>Screen Interval Ft. bgs</u>
Extraction Wells:					
EX-2-S	9449.79	10336.29	3142.13	111.10	110-130
EX-2-I	9441.92	10348.0	3141.30	110.33	145-195
EX-2-D	9434.32	10358.44	3140.50	110.0	195-235
Observation Wells:					
MW-9-S	9495.90	10336.04	3142.47	111.40	112-132
MW-9-I	9480.50	10335.85	3142.35	111.25	170-190
MW-9-D	9464.69	10336.19	3142.13	113.09	216-236
OB-1-S	9380.09	10308.47	3142.71	111.75	110-130
OB-1-I	9378.57	10328.25	3142.31	111.37	175-195
OB-1-D	9362.49	10332.46	3141.98	113.11	215-235
OB-2-S	9377.06	10392.89	3139.59	108.75	110-130
OB-2-I	9377.94	10402.35	3138.63	107.91	172-192
OB-2-D	9377.88	10412.46	3138.11	109.43	215-235

A 1.5-horsepower submersible pump was used to conduct the shallow zone pump test while a 20-horse power pump was used to conduct the pump tests in the intermediate and deep zones. A flow meter was installed at the well head to monitor the discharge rate. The discharge water was piped approximately 50 feet to a sanitary sewer manhole for disposal, as per permission by the City of Colby public works department.

TEST ACTIVITIES

The deep zone pump test was conducted from August 1 to August 4, 2000 at a pumping rate of 105 gallons per minute (gpm). The test lasted for 68 hours and drawdown data from the deep zone monitoring wells initially indicated that this zone behaved like a semi-confined aquifer (larger drawdowns over time). However, some drawdown was measured in the shallow extraction well EX-2-S (0.25 ft) and the intermediate extraction well EX-2I, (1.1 ft) immediately adjacent to the deep zone extraction well indicating significant vertical leakage from the overlying intervals.

The intermediate zone pump test was conducted from August 4 to August 7, 2000 at a pumping rate of 187 gpm. The test was conducted for 69 hours and up to 6.6 feet of drawdown was measured in the observation wells within the intermediate zone. Lesser amounts of drawdown were measured in EX-2S (2.2 ft) and EX-2D (2.4 ft), immediately adjacent to the intermediate pumping well. Negligible drawdowns were measured in the shallow observation wells and were not used in the pump test analysis because of the difficulty of filtering out the background aquifer fluctuations and atmospheric effects.

The shallow zone pump test was conducted from August 7 to August 10, 2000 at a rate of 30 gpm for 63 hours. Due to the limited zone of saturation within the upper portion of the aquifer, little to no drawdown was measurable in the observation and non-pumping extraction wells.

TEST LIMITATIONS

The tests were limited by several factors; the pumping rate for each test could not exceed 150-200 gpm, the pumping tests were limited to a maximum of 72 hours, and the wells were constructed in the three distinct zones (partial penetration) because of analytical/treatment considerations. Also, difficulties occurred at the beginning of each test with relation to establishing a constant pumping rate that would yield sufficient drawdowns in the adjacent observation wells. As a result, the intermediate and deep zones may not have been stressed sufficiently and/or may not have been pumped long enough to generate a cone of depression that would yield precise estimates of transmissivity and specific yield. To compensate for uncertainties in early time data, the late time data was used to perform curve matching. Overall, late time data is considered more accurate in unconfined aquifers for estimating transmissivities and storage coefficients.

ANALYSES

Several methods of analysis were used to determine solutions that most closely matched the conditions within the aquifer at the Ace Services site. The aquifer is generally considered to be under unconfined flow conditions. As a result, the Neuman (1975) method is thought to best analyze pumping test data within unconfined aquifers. The Neuman method was implemented during analysis of the intermediate pump test data. The Neuman method assumes that:

- The aquifer is unconfined and has an "apparent infinite extent"
- The aquifer is homogeneous, isotropic, and of uniform thickness
- The well is pumped at a constant rate
- Well diameter is small, so well storage is negligible
- Flow is unsteady to the pumping well
- The well penetrates the entire aquifer

Several factors involved with the pump tests at the Ace Services site could cause significant variations with relation to evaluation of the data by the Neuman method. The biggest factor is that the pumping wells did not fully penetrate the aquifer. There are also large portions of the aquifer that are not homogeneous and isotropic.

The Moench method, derived from Neuman's solution, may be better suited to the testing conditions that occurred at the Ace Services site. The Moench method is an analysis used when partially penetrating conditions occur. The Moench method was also implemented during analysis of the data and assumes that:

- The aquifer is unconfined and has an "apparent infinite extent"
- The aquifer is homogeneous and isotropic
- The well is pumped at a constant rate
- Well diameter is small, so well storage is negligible
- Drawdown is small relative to saturated thickness

This method appeared to best suit the conditions of the pump test within the intermediate and deep zones.

However, due to the geologic conditions, mainly the presence of a clay layer that separated the intermediate and deep zones, the deep zone data was also analyzed by traditional methods typically applicable to confined or leaky confined aquifers (Cooper-Jacob method and the Hantush-Jacob method).

The traditional methods of time vs. drawdown and distance vs. drawdown assume:

- The aquifer is confined and has an "apparent" infinite extent
- The aquifer is homogeneous, isotropic, and of uniform thickness
- The well is pumped at a constant rate
- The well is fully penetrating
- Water removed from storage is discharged instantaneously with decline in head

- Well diameter is small, so well storage is negligible
- The values of μ are small (rule of thumb $\mu < 0.01$)

TEST RESULTS

The deep zone pump test data were analyzed by the Cooper & Jacob time/drawdown, the Hantush & Jacob, and Moench methods. Results from the Cooper & Jacob method (Figure 3) yielded a transmissivity of 1,900 Ft²/day, the Hantush & Jacob method (Figure 4) yielded a transmissivity of 1,310 Ft²/day, and the Moench method (Figure 5) yielded a transmissivity of 1,610 Ft²/day. Horizontal hydraulic conductivities ranged from 10.4 to 15.4 ft/day.

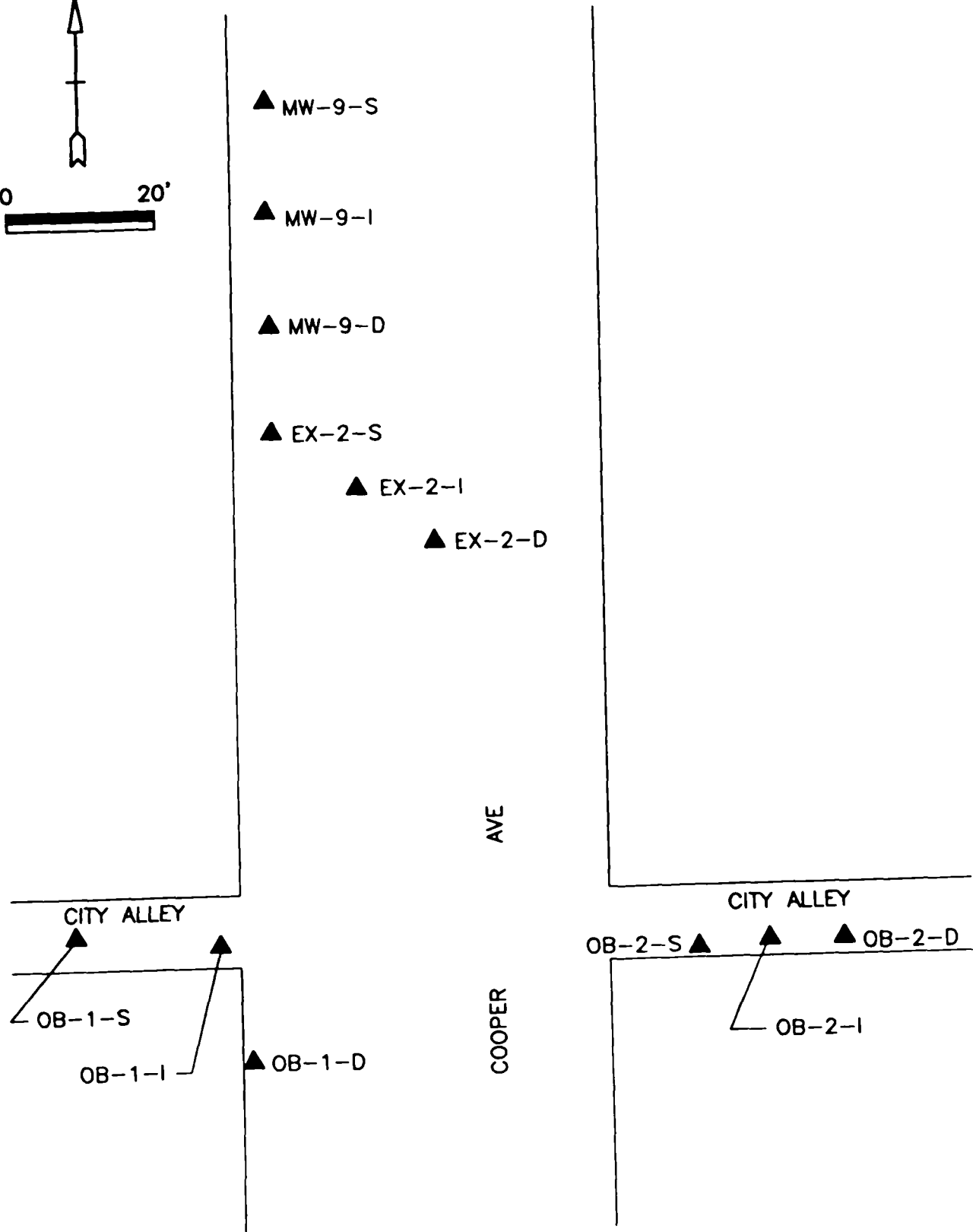
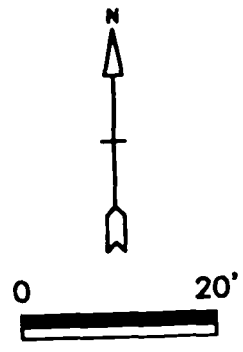
The Intermediate zone pump test data was analyzed by the Moench and Newman methods. Intermediate zone pump test data from shallow and intermediate observation wells, analyzed by the Moench method yielded transmissivities of 4,520 – 6,090 Ft²/day with storage coefficients of 0.11 to 0.20. Horizontal hydraulic conductivities ranged from 53.1 to 71.7 ft/day. Late time drawdown data from the shallow extraction well EX-2-S were used in the Moench analysis plots as illustrated in Figures 6, 7, and 8. This well was selected because it showed evidence of the delayed yield effects that were expected within the shallow zone during the test. The intermediate observation wells did not show any significant effects of delayed yield. Analysis of the late time data for the intermediate observation wells using the Neuman method, Figures 9 and 10, resulted in values of transmissivity and specific yield that were significantly lower than expected and much lower than published values for the aquifer.

The Neuman method of analysis was used for the intermediate zone pump test using shallow well drawdown data from EX -2S and MW-9S. The late-time data were graphically matched to the type curves and yielded a transmissivity of 2,940 Ft²/day. Horizontal hydraulic conductivities ranged from 17.9 to 34.6 ft/day. Neuman analysis of the intermediate observation well data yielded transmissivities of only 1,520 Ft²/day, significantly lower than expected. The values for the storage coefficient were not considered because the wells were partially penetrating.

Table 2
Transmissivity Summary Table

Aquifer Zone	Solution Method (Transmissivity, Ft ² /day)			Hydraulic Conductivity (Ft/day)	Combined Transmissivity
	Neuman	Cooper Jacob	Hantush Jacob		
Intermediate	2,940 1,520			4,520 – 6,090	6,682
Deep		1,900	1,310	1,610	

The aquifer pump tests were conducted at the Ace Services site under the assumption that there existed three distinct zones within the aquifer. However, results of the pump test analyses indicate that the High Plains aquifer at the Ace Services site may function as two distinct hydrologic zones, an upper zone (shallow and intermediate) and a lower (deep) zone. The fine grained clay-silty clay unit that separates the intermediate and deep zones appears to function as a leaky aquitard. Combining the average transmissivities of the upper (from Moench analysis) and lower zones arithmetically yields a value of approximately 6,682 Ft²/day (50,000 gpd/ft). This is consistent with published transmissivity values for this region of the High Plains Aquifer. The combined transmissivity and hydraulic conductivity values



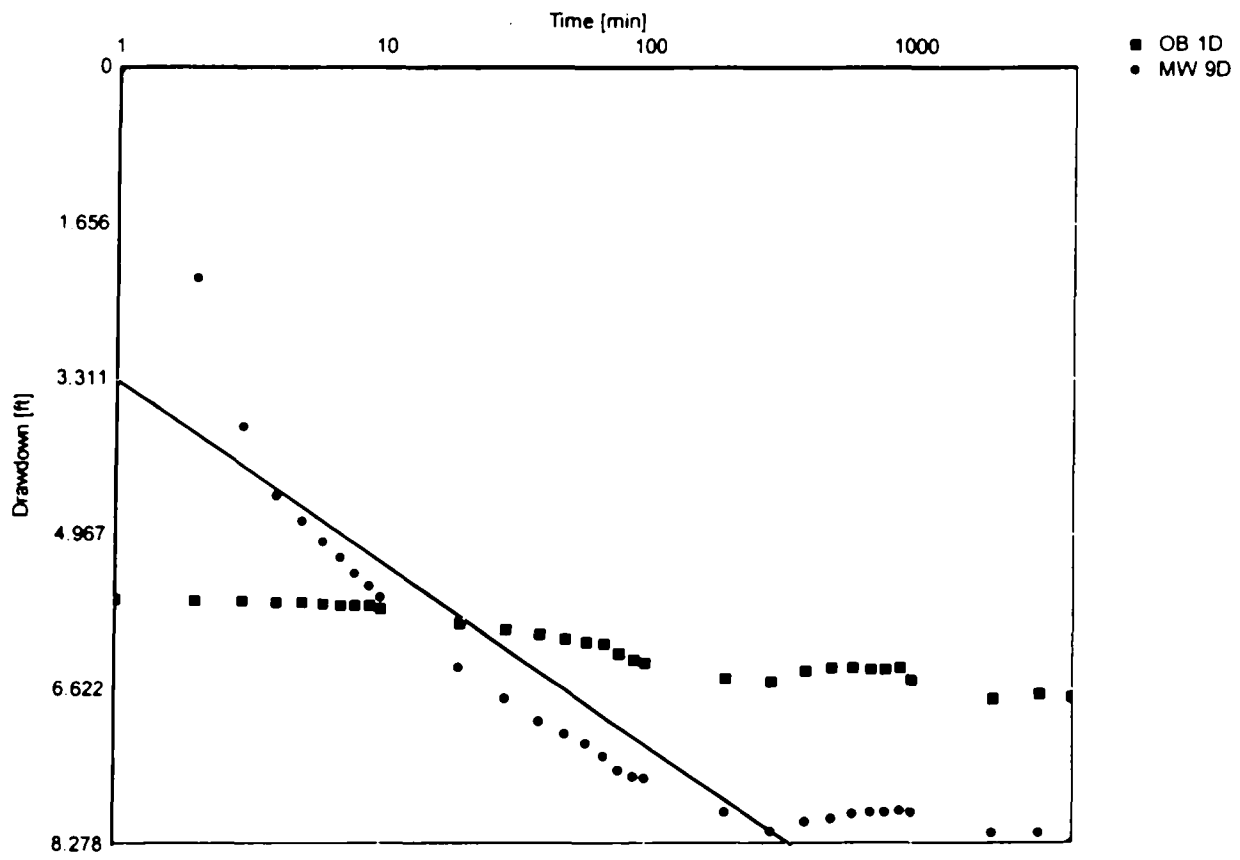
40116.128
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FIGURE 2
WELL LOCATIONS FOR
MW-9, EX-2, OB-1
AND OB-2
ACE SERVICES SITE

Location: Colby, KS	Pumping test: Deep Zone Test	Pumping well: EX 2D
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Test performed by: Dustin Marlow	Evaluated by: Brian Smith
Test date: 8/30/00	Evaluation date: 9/11/00

Analysis method: COOPER & JACOB Time-Drawdown	Aquifer thickness: 123
	Discharge rate: 105 [U.S. gal/min]



Transmissivity: 1.90×10^{-3} [ft²/d]
 Conductivity: 1.55×10^{-1} [ft/d]

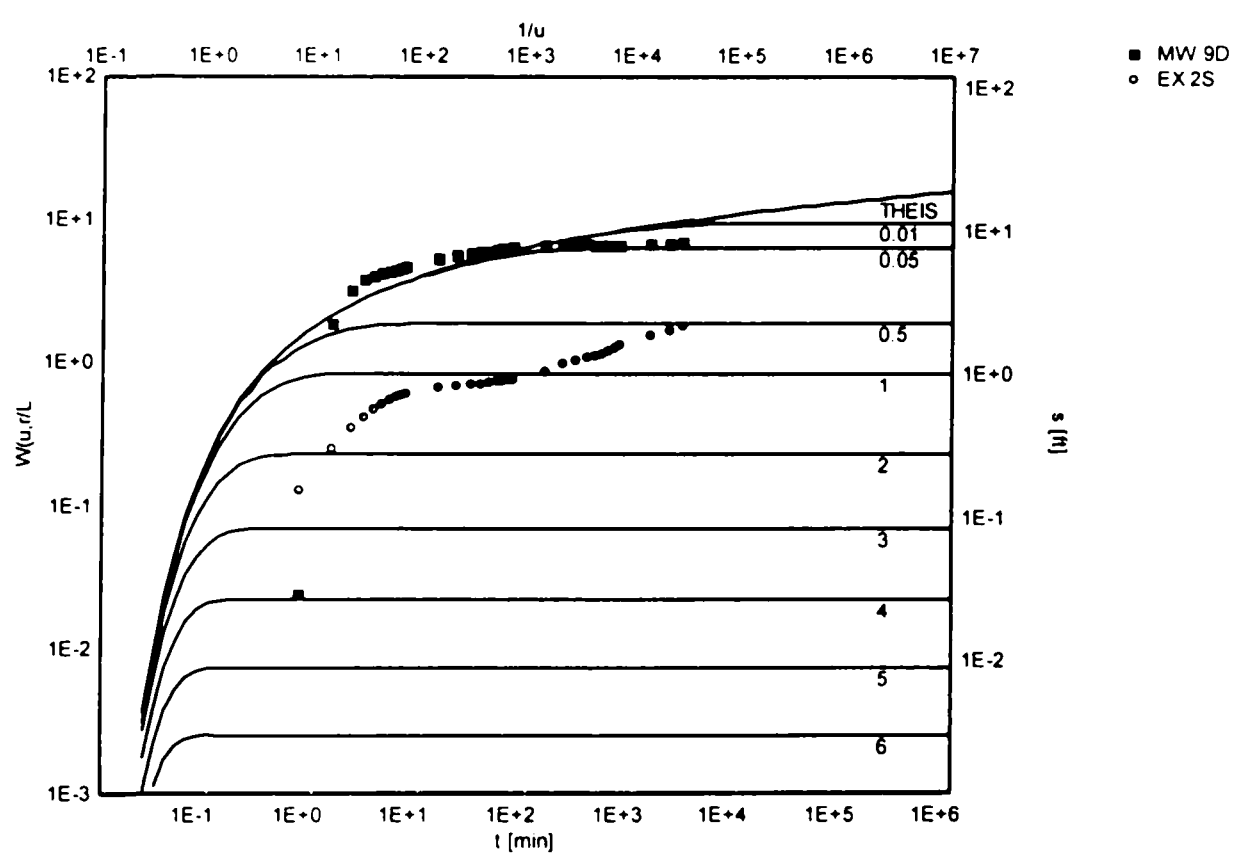
** Graphically Matched Curve

FIGURE 3

Location: Colby, KS Pumping test: Deep ZoneTest Pumping well: EX 2D

Test performed by: Dustin Marlow Evaluated by: Brian Smith
 Test date: 8/30/00 Evaluation date: 9/1/00

Analysis method: Hantush and Jacob Aquifer thickness: 123
 Discharge rate: 105 [U.S. gal/min]



Transmissivity: 1.31×10^3 [ft²/d]
 Conductivity: 1.07×10^1 [ft/d]
 Storativity: 3.56×10^{-4}
 c: 1.55×10^7 [min]

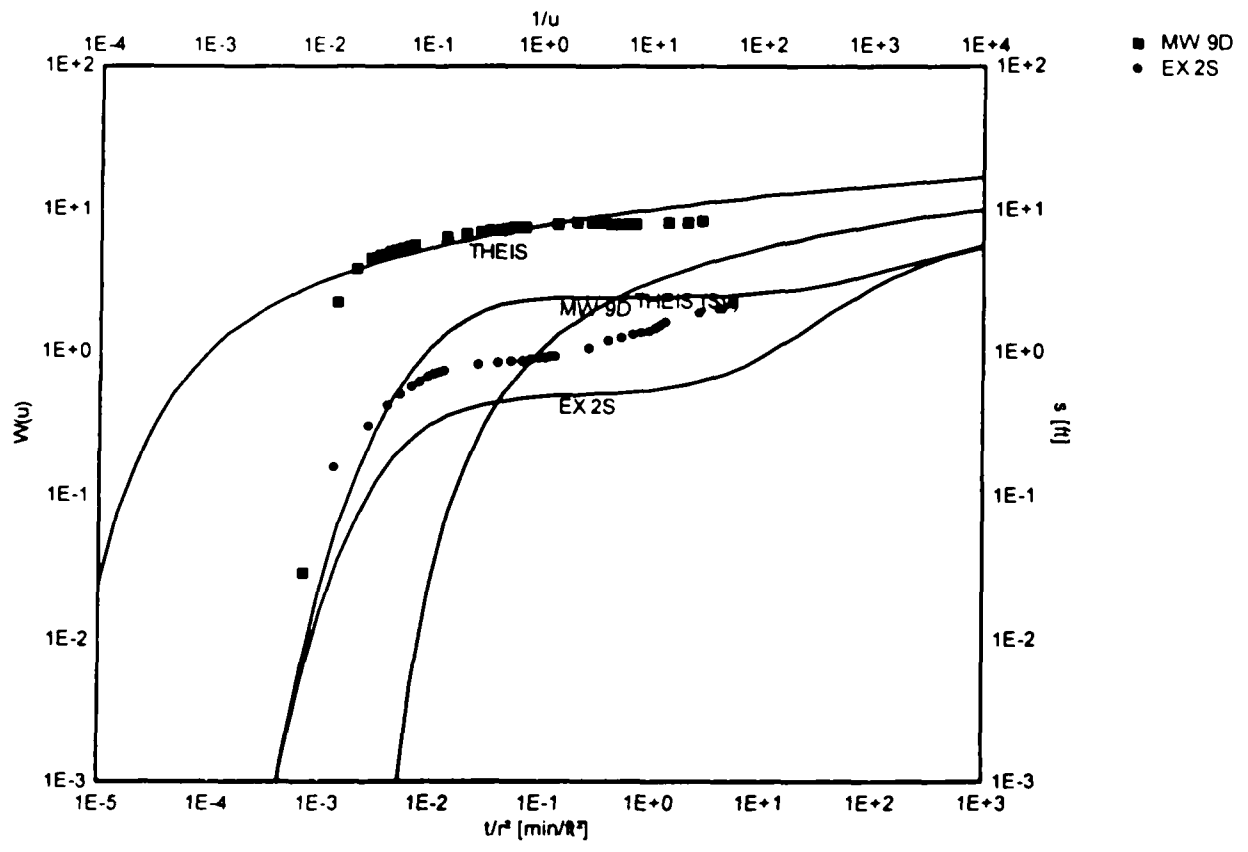
** Graphical Matched Curve

FIGURE 4

Location: Colby, KS Pumping test: Deep Zone Test Pumping well: EX 2D

Test performed by: Dustin Marlow Evaluated by: Brian Smith
 Test date: 8/30/00 Evaluation date: 8/31/00

Analysis method: MOENCH Aquifer thickness: 123
 Discharge rate: 105 [U.S. gal/min]



Transmissivity: 1.61×10^3 [ft^2/d]
 Conductivity: 1.31×10^1 [ft/d]
 Storativity: 1.12×10^{-1}
 Conductivity vertical: 1.31×10^{-1} [ft/d]

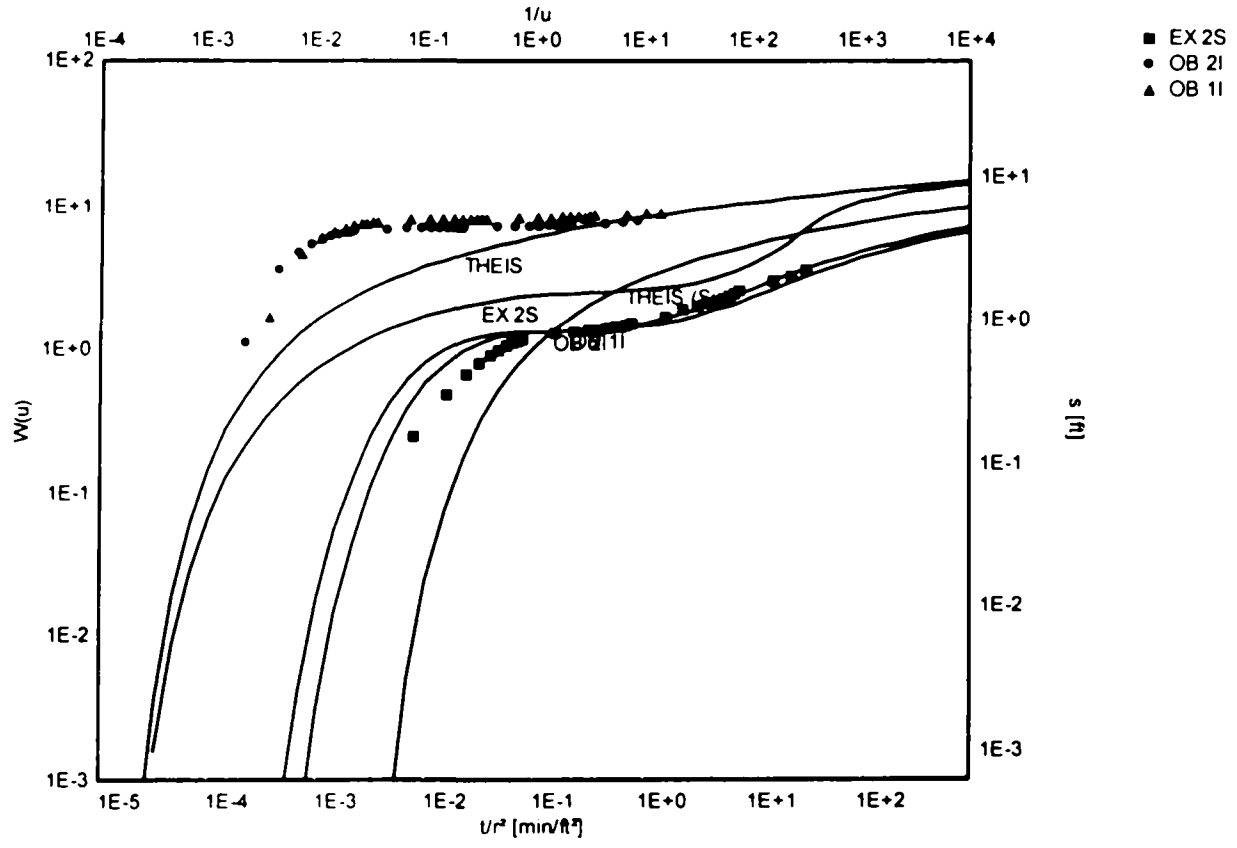
** Computer Matched with "automatic fit"

FIGURE 5

Location: Colby, KS Pumping test: Intermediate Zone Pumping well: EX 21

Test performed by: G Felkner Evaluated by: Brian Smith
 Test date: 8/7/00 Evaluation date: 8/30/00

Analysis method: MOENCH Aquifer thickness: 85 [ft]
 Discharge rate: 186 [U.S. gal/min]



Transmissivity: 4.52×10^3 [ft²/d]
 Conductivity: 5.31×10^1 [ft/d]
 Storativity: 2.02×10^{-1}
 Conductivity vertical: 5.31×10^{-1} [ft/d]

** Graphically Matched Curve Using Late-time Data

FIGURE 6



BLACK & VEATCH
SPECIAL PROJECTS CORP

Black & Veatch Special Projects

6601 College Blvd
Overland Park KS
Phone (913) 458-2000

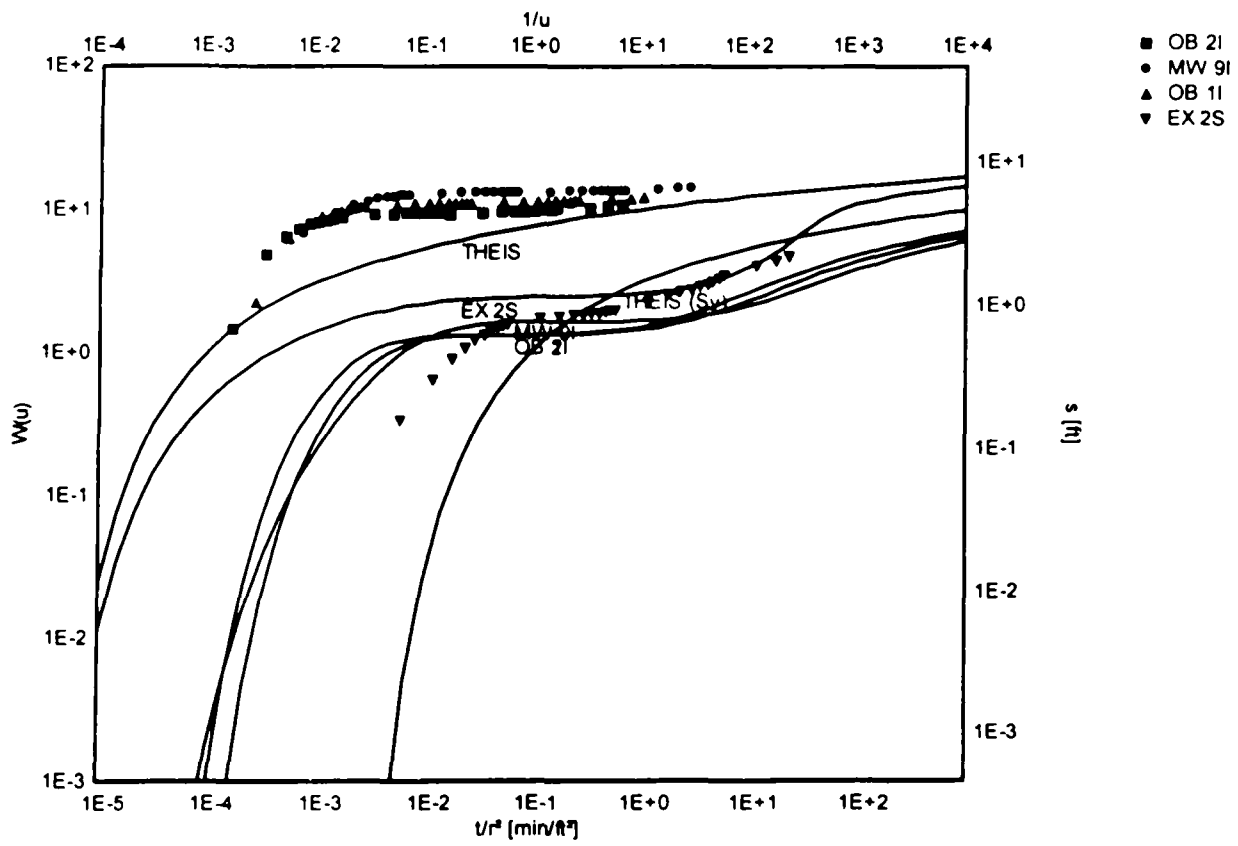
Pumping test analysis

No: 46118.126
Project: Ace Services
Client: USEPA

Location: Colby, KS Pumping test: Intermediate Zone Pumping well: EX 2I

Test performed by: G Felkner Evaluated by: Brian Smith
Test date: 8/7/00 Evaluation date: 8/29/00

Analysis method: MOENCH Aquifer thickness: 85 [ft]
Discharge rate: 186 [U.S. gal/min]



Transmissivity: 6.09×10^3 [ft²/d]

Conductivity: 7.17×10^1 [ft/d]

Storativity: 3.52×10^{-1}

Conductivity vertical: 7.17×10^{-1} [ft/d]

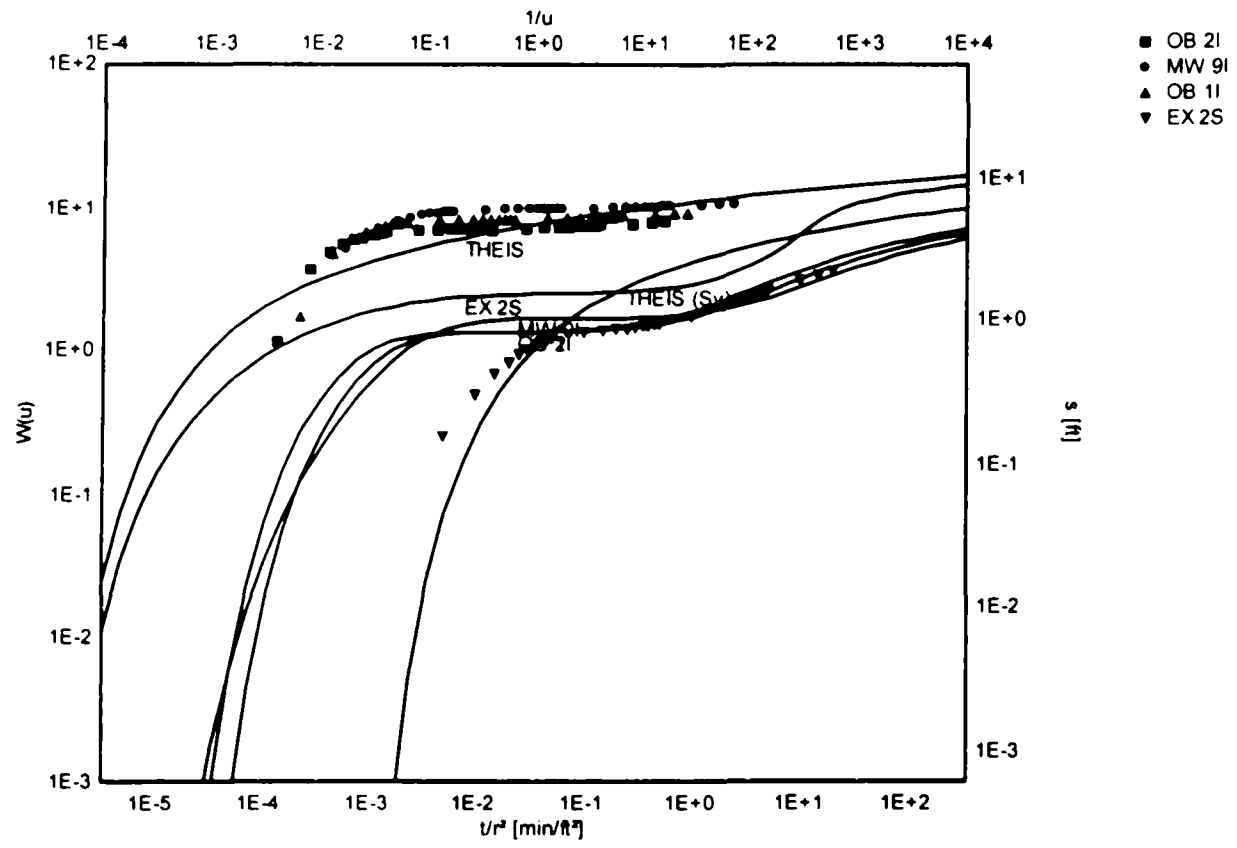
** Graphically Matched Curve Using Late-time Data

FIGURE 7

Location: Colby, KS Pumping test: Intermediate Zone Pumping well: EX 21

Test performed by: G Felkner Evaluated by: Brian Smith
 Test date: 8/7/00 Evaluation date: 8/29/00


Analysis method: MOENCH Aquifer thickness: 85 [ft]
 Discharge rate: 186 [U.S. gal/min]

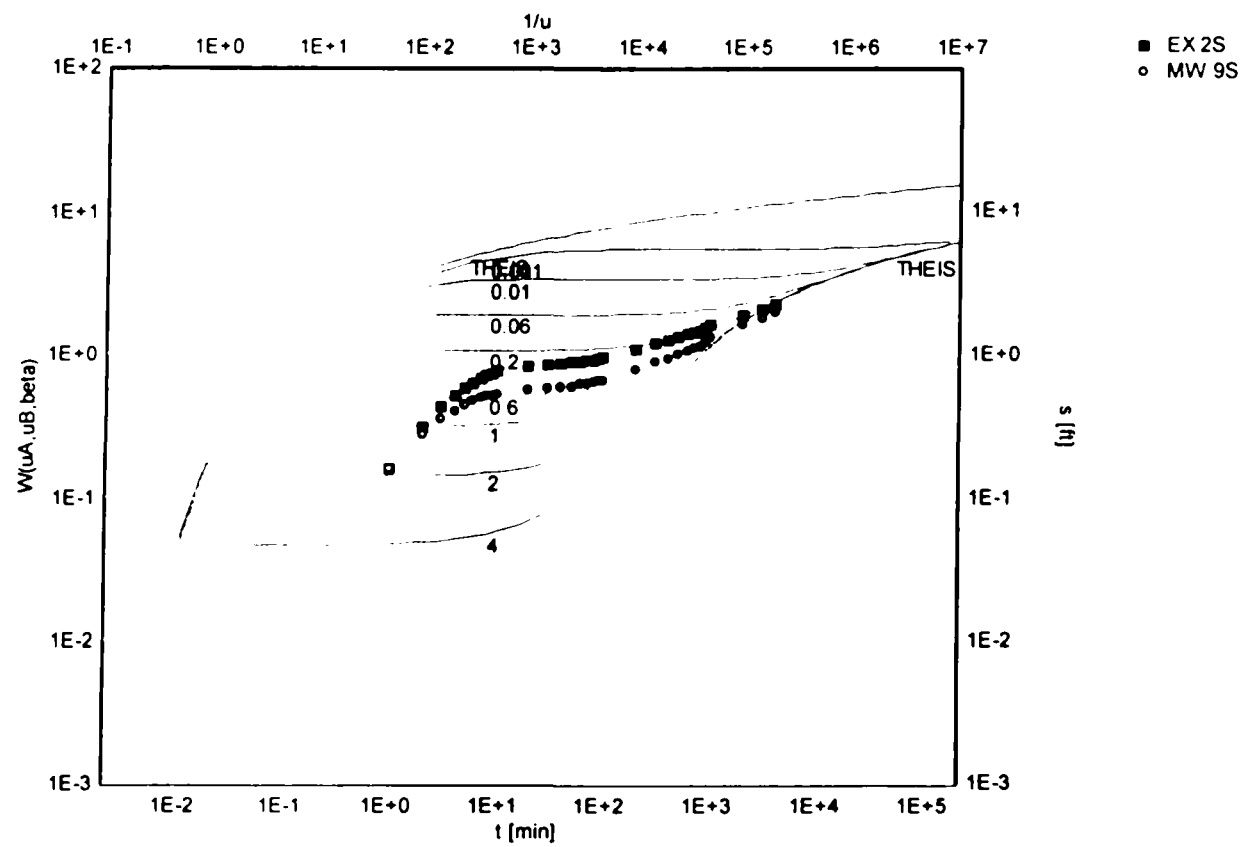


Transmissivity: 4.62×10^3 [ft²/d]
 Conductivity: 5.44×10^1 [ft/d]
 Storativity: 1.14×10^{-1}
 Conductivity vertical: 5.44×10^{-1} [ft/d]

** Graphically Matched Curve Using Late-time Data

FIGURE 8

 BLACK & VEATCH SPECIAL PROJECTS CORP	Black & Veatch Special Projects 6601 College Blvd Overland Park KS Phone (913) 458-2000	Pumping test analysis No: 46118.126 Project: Ace Services Client: USEPA
	Location: Colby, KS Pumping test: Intermediate Zone Pumping well: EX 2I	Test performed by: G. Felkner Test date: 8/7/00 Analysis method: NEUMAN



Transmissivity: 2.94×10^3 [ft²/d]
 Conductivity: 3.46×10^1 [ft/d]
 Storativity: 5.64×10^{-5}
 Specific yield: 5.64×10^{-1}

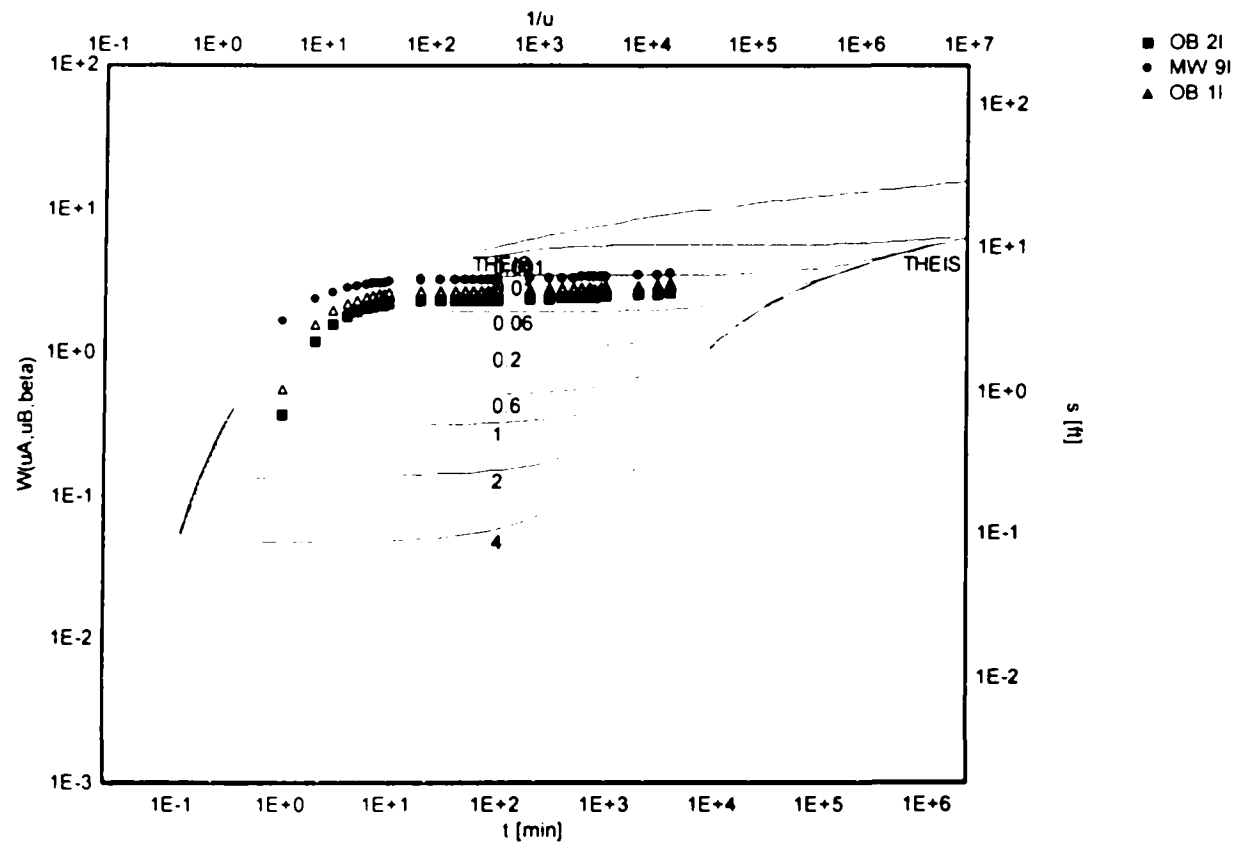
** Graphically Matched Curve Using Late-time Data

FIGURE 9

Location: Colby, KS Pumping test: Intermediate Zone Pumping well: EX 21

Test performed by: G Felkner Evaluated by: Brian Smith
 Test date: 8/7/00 Evaluation date: 8/29/00

Analysis method: NEUMAN Aquifer thickness: 85 [ft]
 Discharge rate: 186 [U.S. gal/min]



Transmissivity: 1.52×10^3 [ft²/d]
 Conductivity: 1.79×10^1 [ft/d]
 Storativity: 1.37×10^{-4}
 Specific yield: 1.37×10^0

** Computer Matched using "Automatic Fit"

FIGURE 10

from this analysis will be implemented into a finite difference ground water model to aid in the design of an optimum active remediation pump and treat system for the Ace Services site.

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Cooper, H.H. and C.E. Jacob, 1946, A Generalized Graphical Method for Evaluation Formation Constants and Summarizing Well Field History, Am. Geophys. Union Trans., vol. 27, pp. 526-534.

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Miller, J.A., and Appel, C.L., 1997, Ground Water Atlas of the United States, Kansas, Missouri, Nebraska, U.S. Geological Survey Hydrologic Atlas 730-D.

Moench, A.F., 1995, Combining the Neuman and Boulton Models for Flow to a Well in an Unconfined Aquifer. Ground Water, vol. 33, No. 3, pp.378-384.

Appendix I
Groundwater Modeling Results

Original
File D.3
46118

TECHNICAL MEMORANDUM

USEPA
Ace Services
Ground Water Modeling Activities

BVSPC Project 46118.126 ✓
BVSPC File D.3
December 14, 2000

INTRODUCTION

A record of decision (ROD) for the Ace Services site was signed on May 5, 1999 stipulating an active remediation pump and treat system be installed based on a ground water model developed in 1998. Following completion of this ROD, an additional phase of investigation work was conducted in late 1999 and this new data indicates that a larger and more vertically complex plume of chromium contamination is present at the Ace Services site. To investigate this new information and provide a more accurate design basis for the pump and treat remediation system, vertically stratified pumping tests within the observed contaminated water column were performed in August 2000. These pumping tests confirm that the aquifer system exhibits a large amount of vertical heterogeneity and that the ground water contamination at the Ace Services site is vertically distributed. Therefore as part of the required modifications to the original ROD, a new ground water model was constructed to more accurately simulate the vertical flow component within the aquifer system at the site and provide input for evaluating potential remedial designs for capturing and remediating the chromium plume. The primary objectives of this new modeling effort were the following:

- Develop a ground water flow model capable of simulating the observed vertically stratified flow within the aquifer.
- Incorporate the recently collected pumping test data into the ground water flow model and calibrate this model using the pumping test results.
- Determine an effective extraction well configuration to capture the observed chromium plume.
- Determine an effective pumping rate for the selected extraction well configuration.
- Estimate the potential duration of the pump and treat remediation effort.

To accomplish these objectives, MODFLOW, a three-dimensional finite difference ground water flow model was used to simulate ground water flow and estimate the aquifer response to various ground water remediation strategies. MODPATH, a three dimensional advective particle transport program was used in combination with MODFLOW to more accurately estimate extraction well capture zones by tracking individual particles within the simulated flow field. GMS, Ground Water Modeling Software, originally developed by the Department of Defense, was utilized as a pre- and post-processor to expedite model runs and to generate ground water contour maps showing modeling results and well field configurations.

REGIONAL HYDROGEOLOGY

The average saturated thickness of the High Plains aquifer in Kansas is approximately 90 feet. Water in the High Plains aquifer generally is under unconfined conditions. However, in some locations, water levels in wells completed in portions of the aquifer may rise or fall slightly in relation to the regional water table because of artesian pressure created by local confining beds. Generally the ground water gradient within the aquifer is from west to east. Water moves in response to the gradient of the water table, which typically averages between 10 to 15 feet per mile. On the basis of these average gradients and aquifer hydraulic properties, the regional velocity at which water moves through the aquifer is estimated to average about 1 foot per day. Transmissivity values within the High Plains aquifer typically range from 40,000 to 60,000 gallons per day/ft with storage coefficients ranging from 0.14 to 0.27 (Miller and Appel, U.S.G.S Ground Water Atlas, 1997).

SITE HYDROGEOLOGY

Aquifer testing was conducted at the Ace Services site under the assumption that three distinct water bearing zones were present. However, based on the results of the pumping tests performed at the site

(Pumping Test Technical Memorandum, BVSPC, October 2000), the High Plains aquifer at the Ace Services site appears to function as two distinct hydrologic zones, an upper zone consisting of shallow and intermediate ground water and a lower zone consisting of deep ground water. A fine grained clay/silty clay unit that separates the upper and lower zones and appears to function as a leaky aquitard. Water levels recorded during the remedial investigation indicate a slightly downward vertical gradient within the aquifer surrounding the Ace Services site. Locally, ground water flows to the east-southeast at horizontal gradients ranging from 0.0022 – 0.0032 ft/ft. Continuous water level monitoring conducted prior to the pumping test activities indicates that the upper zone within the aquifer follows typical unconfined aquifer behavior. However, continuous ground water monitoring data collected from the lower zone suggests that this zone behaves as a semi-confined aquifer. This is demonstrated by observed diurnal fluctuations in hydraulic head in the deep zone wells due to the hydraulic influence of water supply wells in the vicinity of the Ace Services site. Diurnal fluctuations in hydraulic head were not observed in nested shallow and intermediate wells.

MODEL ASSUMPTIONS

Ground water modeling requires a set of assumptions to simplify the modeling effort in order to approximate the complexities associated with ground water flow. Simplifying some of the uncertainties of the system allows for the model to come to an accurate solution. The following assumptions were used to develop the Ace Services site ground water flow model:

- Water level data collected from nested monitoring wells at the site indicate ground water flow to the east-southeast. The data also indicate that a downward vertical gradient exists across the site. The geology within the saturated and contaminated portion of the aquifer consists of interbedded zones of sands, silty sands, gravels and a relatively consistent silty clay layer that separates the intermediate and deep water bearing zones. These hydrogeologic conditions were approximated by four model layers. Layer 1 represented the shallow zone. Layer 2 represented the intermediate zone. Layer 3 represented the silty clay leaky confining layer. Layer 4 represented the deep zone. Representing the site hydrogeology with four model layers allowed for the simulation of a vertical gradient and the stratification of aquifer properties and ground water extraction.
- Hydraulic conductivities used in the model were based on the pumping test data conducted in August, 2000. However the hydrologic data calculated from the shallow zone pumping test was determined to be unrepresentative of site conditions and was not used in the model. The small magnitudes of drawdown observed during the shallow zone test did not allow for accurate curve matching to derive an accurate solution for transmissivity. Also, the analytical solutions derived from data collected from the deep zone pump test appeared low in relation to published values. As a result, the horizontal hydraulic conductivity value from the intermediate test was used as a starting value and the values for the upper and lower layers were estimated as a percentage thereof based on lithology and well yields from the shallow and deep extraction wells. Hydraulic conductivity values of 37 ft/day (layer 1), 62 ft/day (layer 2), and 43 ft/day (layer 4) were used to simulate flow within the shallow, intermediate, and deep zones respectively. Vertical hydraulic conductivity values were estimated as $K_v/10$. Layer 3 was simulated as a leaky-confining unit and the hydraulic conductivities of this layer were determined during model calibration. The leaky-confining unit was modeled over the entire domain of the model but may only be present in the vicinity of the site. To test the validity of these model assumptions, the model was calibrated in both steady-state and transient mode.
- The aerial and vertical extent of the contamination was assumed to be that which is defined in the technical memorandum for remedial design activities, (BVSPC, March 29, 2000). However, the actual downgradient extent of the plume and the extent of the 100 ug/L contour line representing the MCL for chromium has not been completely defined along the southern plume boundary or at the downgradient edge of the plume due to property access constraints.
- It has been assumed that proposed new nested monitoring wells installed along the southern plume boundary and at the downgradient plume edge will not show high (>500 ppb Cr) levels of contamination.
- It has been assumed that no additional source areas exist downgradient of the site.

MODEL DOMAIN AND BOUNDARY CONDITIONS

The model domain is approximately 5 miles by 4 miles with the long axis (parallel to ground water flow direction) oriented approximately 104 degrees from north. The model boundaries were extended far from the site to ensure that the boundary conditions had negligible impact on the model simulations. Figure 1 shows the model domain in relation to the Ace Services site. The model grid consists of 110 columns and 85 rows with 4 layers. Grid spacing near extraction well locations was set at 10 ft by 10 ft and expanded outward in increments of 1.5 to a maximum of 1000 feet in the x-direction and to a maximum of 500 feet in the y-direction. Constant head values were assigned at the northwest and southeast boundaries to simulate ground water entering and discharging from the model domain. No-flow boundaries were assigned to the northern and southern boundaries because ground water flow is essentially parallel to these boundaries. Ground water recharge from leakage through the overlying strata was input to the top of layer 1. A value of 0.05 in/year was assigned to the model based on published recharge data for the High Plains aquifer.

MODEL CALIBRATION

The model was calibrated in two steps through both steady-state and transient simulation. In the first step, appropriate head values were input for each constant head boundary and the model was run under steady-state conditions. The modeled heads were then compared to the observed head values collected from monitoring wells at the site prior to the pump test in August 2000. Figure 2 shows the modeled simulated ground water contours with no wells pumping. Hydrogeologic parameters (constant head, recharge, horizontal and vertical hydraulic conductivity) were adjusted until the calibration error was minimal. Table 1 shows the results of the steady-state model calibration. This first part of the calibration resulted in a ground water gradient of 0.0023. Figure 3 shows a comparison between observed heads and modeled residual values (the difference between the measured heads and the modeled heads). The residual head values show that the recharge and hydraulic conductivity values (calculated from the pumping test data) used in the calibration process are representative of site conditions and did not have to be adjusted during calibration.

A trend was observed during the steady-state calibration: the modeled heads on the north and western sides of the site were lower than the observed heads and the modeled heads on the far downgradient side of the site (the labeled wells) and were significantly higher than the observed heads. The magnitude of the error appeared to be skewed by the differences in head within the deep wells (layer 4) along the eastern end of the site. One explanation might be changes in lithology, which might influence the hydraulic conductivity within and between the intermediate (layer 2) and deep (layer 4) zones of the aquifer. However, subsurface geological data does not indicate significant changes in aquifer material across the site. Another possible explanation is the position of the well screens of the monitoring wells on the western side of the site. The intermediate and deep monitoring wells at well nests at MW-2 are screened very close together and have the smallest vertical hydraulic gradient. The intermediate and deep wells at well nest MW-1 are screened at higher elevations so the wells may in fact be screened in the same hydrologic zone (intermediate). These differences in head do not significantly impact the flow model.

The second part of the calibration involved inputting calibrated steady-state head values into a transient simulation identical to the 72-hour pumping tests that were conducted within the intermediate and deep water bearing zones in August 2000. During this part of the calibration, the coefficient of storage and specific yield values were adjusted within those layers to best match the observed aquifer response during each pumping test. The transient calibration data confirm that the hydraulic conductivity and recharge values used in the model accurately simulated flow within the aquifer. Table 2 shows the results of the transient calibrations.

Figure 3

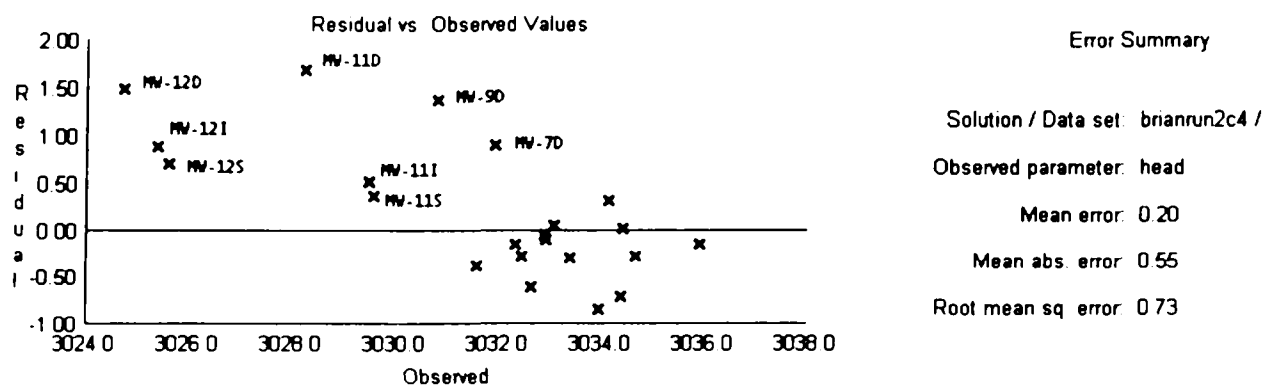


Table 1
MODFLOW Calibration Results

WELL	MODEL HEAD	OBSERVED HEAD	RESIDUAL HEAD	RESIDUAL SQUARED
MW-1S	3035.8	3035.9	-0.10	0.01
MW-2S	3034.4	3034.7	-0.3	0.09
MW-2I	3034.4	3034.41	0.01	0.0001
MW-2D	3034.4	3034.1	0.3	0.09
MW-4S	3032.0	3032.6	-0.6	0.36
MW-6S	3033.7	3034.4	-0.7	0.49
MW-7S	3032.8	3032.9	-0.1	0.01
MW-7I	3032.8	3032.9	-0.1	0.01
MW-7D	3032.8	3031.9	0.9	0.81
MW-8S	3033.1	3033.9	-0.8	0.64
MW-8I	3033.1	3033.4	-0.3	0.09
MW-8D	3033.1	3033.14	0.04	0.0016
MW-9S	3032.2	3032.3	-0.01	0.01
MW9I	3032.1	3032.4	-0.03	0.09
MW-9D	3032.1	3030.8	1.3	1.69
MW-11S	3030.0	3029.5	0.5	0.25
MW-11I	3029.9	3029.6	0.3	0.09
MW-11D	3029.9	3028.2	1.7	2.89
MW-12S	3026.3	3025.6	0.7	0.49
MW-12I	3026.2	3025.4	0.8	0.64
MW-12D	3026.2	3024.7	1.5	2.25

Table 2
Transient Calibration Results

WELL	MODEL HEAD	OBSERVED HEAD	RESIDUAL HEAD	RESIDUAL SQUARED
OB-2I	3027.19	3026.96	0.231	0.053
OB-1I	3027.36	3026.36	1.0	1.0
MW-9I	3024.73	3025.46	-0.72	0.518
OB-1D	3025.98	3025.37	0.617	0.38
OB-2D	3025.65	3025.56	0.098	0.0096
MW-9D	3023.67	3023.77	0.10	0.01

SENSITIVITY ANALYSIS

After the model was calibrated, a sensitivity analysis was conducted to evaluate the model uncertainty. Hydraulic conductivity and aquifer recharge were both increased and decreased by factors of 25 and 50 percent, and the residual sum of squares (difference or residual between the measured and the modeled head values squared) was calculated. The results of the sensitivity analysis are shown on Table 3. These results indicate that the calibrated model has the best match. The sensitivity results also indicate that the model is most sensitive to changes in hydraulic conductivity.

Table 3
Model Sensitivity Analysis

	RESIDUAL SUM OF SQUARES (FT ²)
Calibrated Model	0.69
Hydraulic Conductivity +/- 25%	0.88
Hydraulic Conductivity +/- 50%	1.18
Recharge +/- 25%	0.78
Recharge +/- 50%	0.80

EXTRACTION WELLFIELD DESIGN EVALUATION

Following calibration of the MODFLOW model, an active ground water extraction scheme was developed for containment and remediation of the contamination at and down gradient from the Ace Services site. Well locations were selected by incorporating property access considerations, position within the known extent of contamination, and pumping rate required to actively remediate the contamination. Property access was a major factor in extraction well location selection to minimize cost and property agreement delays.

Both MODFLOW and MODPATH programs were used to optimize extraction well locations and pumping rates. Ground water pumping rates were simulated at different locations within the different model layers using the calibrated steady-state heads to generate ground water contour plots for each layer. A set of optimal pumping scenarios were developed and used by the MODPATH particle tracking program to

further define extraction well positions and pumping rates. Particle travel times of 3 years were used as a benchmark when considering the well locations for active contaminant removal. The three year time period was used because most of the extraction well locations simulate capture of the edges of the 100 ug/L plume in less than 2 years. However, certain well locations require a minimum of 3 years to capture ground water from the edges of the 100 ug/L contour, indicating that it will require approximately 3 years to remove one pore volume within the area encompassed by the plume.

As outlined in the Technical Memorandum for Remedial Design (BVSPC, March, 2000), three distinct zones of contamination were identified through the sampling activities. The largest aerial extent of chromium contamination occurs within the intermediate zone of the aquifer. This zone will also require the greatest number of extraction wells to capture the contamination. The shallow zone and the deep zone will require a fewer number of extraction wells. The proposed total combined pumping rate and the proposed number of extraction wells differs significantly from the original FS modeling study due primarily to the large increase in the vertical and lateral extent of the plume.

Simulations within the shallow zone (layer 1) resulted in three optimal pumping scenarios that would sufficiently capture the maximum extent of contamination in an acceptable time frame. One limitation within the upper most portion of the aquifer is saturated thickness. Within the upper zone (layer 1) there exists only 30-35 feet of saturation. As a result, ground water extraction rates are limited to the 20 to 30 gpm range in order to maintain a steady pumping rate. These lower extraction rates limit the cone of influence generated by the extraction wells. Figures 4, 5, and 6 show the optimum well configurations and pumping rates predicted within the shallow zone of the aquifer. It should be noted however that these scenarios, simulated by extracting water from the shallow zone (layer 1), will be accomplished in the field by extraction wells screened within both the shallow and intermediate zones. The total pumping rate expected to capture and contain the shallow zone contamination is expected to be 65 – 85 gpm. It should be noted that the 25 gpm that is simulated at the PWS-8 well location may vary because the actual discharge from the upper zone during pumping at PWS-8 has not been determined.

Four optimal pumping scenarios were developed for the intermediate zone (layer 2) remediation. The intermediate zone is the most transmissive interval within the aquifer in the vicinity of the site. Figures 7, 8, 9, and 10 show the well configurations and pumping rates that most efficiently capture the contamination within the intermediate zone. A series of 5 or 6 extraction wells was used to maximize the area of capture and minimize the time required for treatment of the entire plume. The extraction well east of the plume, as shown in Figures 7, 8, and 9, is not located within the 100 ug/L contour. This additional well was simulated because of data from the residential wells indicates the presence of contamination, but the vertical distribution of the contamination in this area is not known because the residential wells are screened within multiple zones. Extraction well discharge rates vary from 35 gpm to 100 gpm depending upon the zone of capture. The predicted total discharge from the intermediate zone scenarios ranges from 285- 335 gpm. It also should be noted that the discharge of 50 gpm that is simulated from the intermediate zone of PWS-8 may vary due to the lack of information on that multi-screened well. The majority of the contaminant load for the treatment plant will come from the intermediate zone.

The simulated extent of capture within the deep zone (layer 4) is illustrated in Figures 11 and 12. Pumping rates vary from 35 to 100 gpm depending upon the position within the plume. Cones of influence are much larger within this zone because it behaves as a semi-confined zone within the aquifer. Estimated total discharge expected to actively remediate the deep zone range from 185 to 300 gpm. The discharge from the lower screen zone within PWS-8 was estimated and contributes to the uncertainty of the actual pumping rates that will be required within the deep zone.

EXTRACTION WELLFIELD DESIGN RECOMMENDATIONS

The well configuration shown on Figure 13 illustrates the optimal shallow zone pumping scheme. Extraction wells EX-2S and PWS-8 have already been installed, therefore shallow wells EX-3S and EX-4S will need to be installed.

The optimal extraction well scheme for the intermediate zone is shown on Figure 14. This scheme incorporates 6 wells pumping at a combined total of 335 gpm. Wells EX-2I and PWS-8 were installed during the remedial design investigation and pumping test activities. Wells EX-1I, EX-3I, EX-4I, and EX-5I will need to be installed in the intermediate zone with an option for a seventh well. This optional well may be installed east of EX-5I if additional analytical data indicate that the extent of the plume is further east than presently indicated.

Figure 15 shows wells EX-1D, PWS-8, EX-2D, and EX-3D pumping a total of 260 gpm for complete capture of the deep zone contamination. Well EX-1D and EX-3D will need to be installed. Wells EX-2D and PWS-8 are already installed.

The proposed configuration for all of the extraction wells is illustrated on Figure 16, assuming property access is granted for each location. Proposed extraction well design specifications are presented in Table 4. This report estimates a total extraction rate of approximately 690 gpm. At this pumping rate it is expected that one pore volume of the aquifer will be removed approximately every 3 years. However, it is common to require flushing several (3 to 5) pore volumes through contaminated media to reduce contaminant concentrations to cleanup goals. The total time to actively remediate the chromium contamination to acceptable levels is estimated to be approximately 12 years. Due to the variability within the multi-layered aquifer with respect to both the horizontal and vertical distribution of contaminants, it is recommended that the final plant design influent rate incorporate some flexibility to allow for a 15% to 20% increase in flow. Should the results of this modeling study be incorporated into a final design, 8 additional extraction wells at four different locations (2 shallow, 4 intermediate, and 2 deep) will be needed to satisfy the active remediation goals. Additional nested monitoring wells will also be needed to be installed to ensure that contaminant capture is occurring and to monitor contamination reduction. The total number and final pumping rates of the extraction wells required to meet the site remediation objectives may differ from the predictions presented in this report.

REFERENCES

Black & Veatch, October, 2000, Pumping Test Memorandum, Ace Services, Colby, Kansas, USEPA Technical Memorandum.

Black & Veatch, March 29, 2000, Remedial Design Sampling Activities, Ace Services, Colby, Kansas, USEPA Technical Memorandum.

Miller, J.A., and Appel, C.L., 1997, Ground Water Atlas of the United States, Kansas, Missouri, Nebraska, U.S. Geological Survey Hydrologic Atlas 730-D.

Table 4
Proposed Extraction Well Design Specifications

Extraction Well	Screened Interval (bgs) (aquifer zone)	Pumping Rate (gpm)	Well Diameter (inches)
EX-1I	165' – 195' intermediate	35 gpm	8"
EX-1D	210' – 235' deep	35 gpm	8"
PWS-8	128' – 138' shallow 145' – 150' intermediate 190' – 200' intermediate 215' – 240' deep	145 gpm	12"
EX-2S	100' – 130' shallow	25 gpm	6"
EX-2I	145' – 195' intermediate	100 gpm	8"
EX-2D	195' – 235' deep	100 gpm	8"
EX-3S	120' – 140' shallow	25 gpm	6"
EX-3I	150' – 200' intermediate	50 gpm	8"
EX-3D	210' – 230' Deep	50 gpm	8"
EX-4S	110' – 140' shallow	25 gpm	6"
EX-4I	180' – 200' intermediate	50 gpm	8"
EX-5I	170' – 200' intermediate	50 gpm	8"
Total Well Field Pumping Rate		690 gpm	



Constant Head Cells

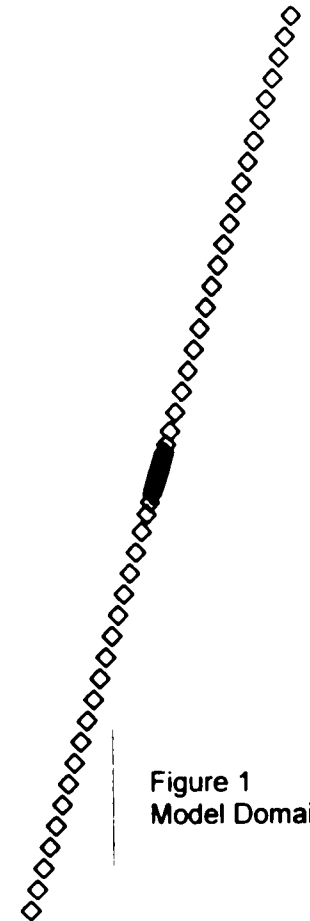
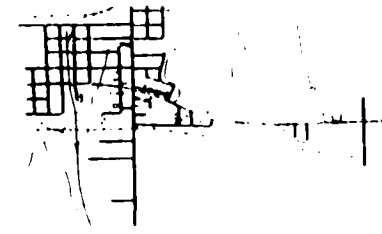


Figure 1
Model Domain

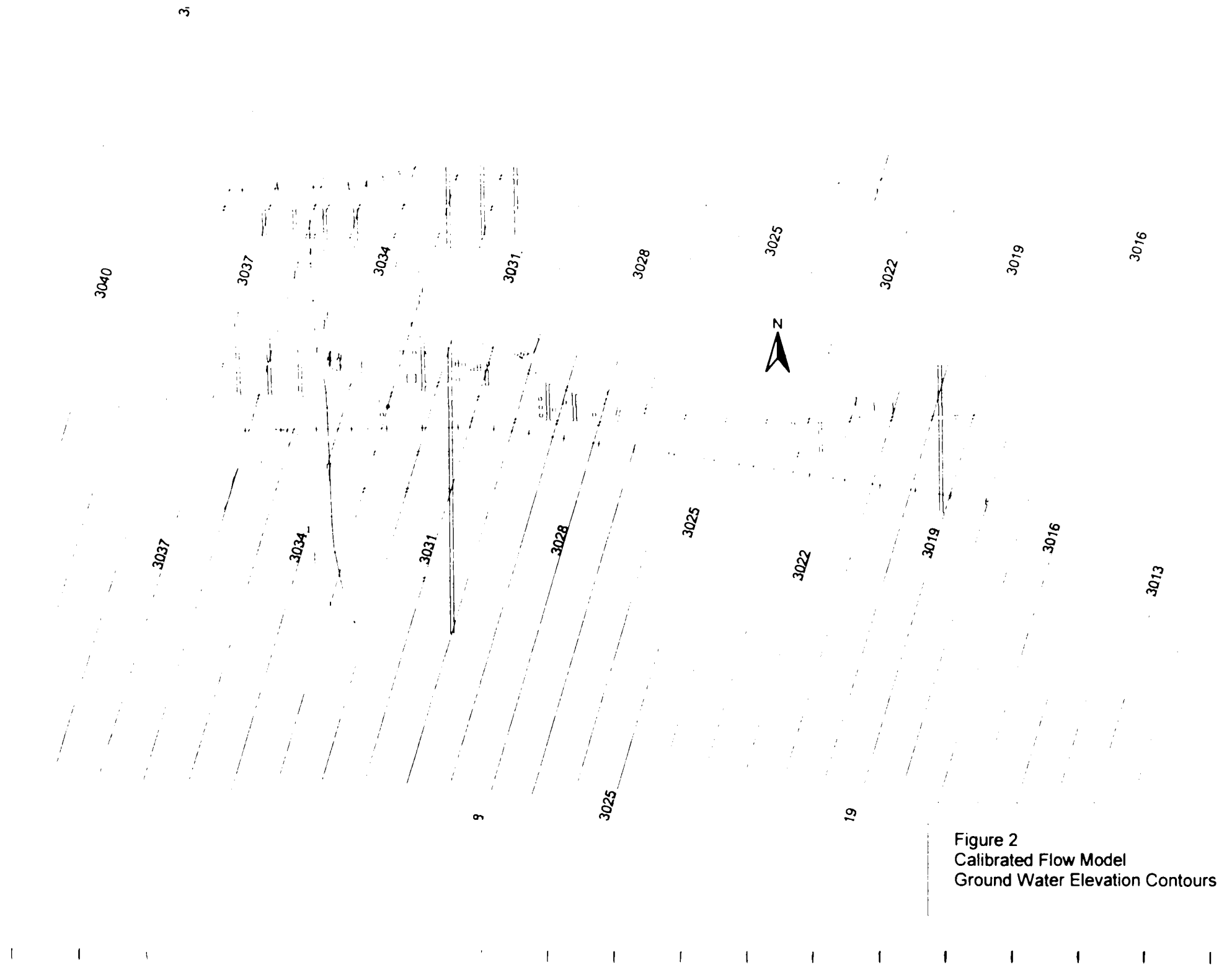


Figure 2
Calibrated Flow Model
Ground Water Elevation Contours

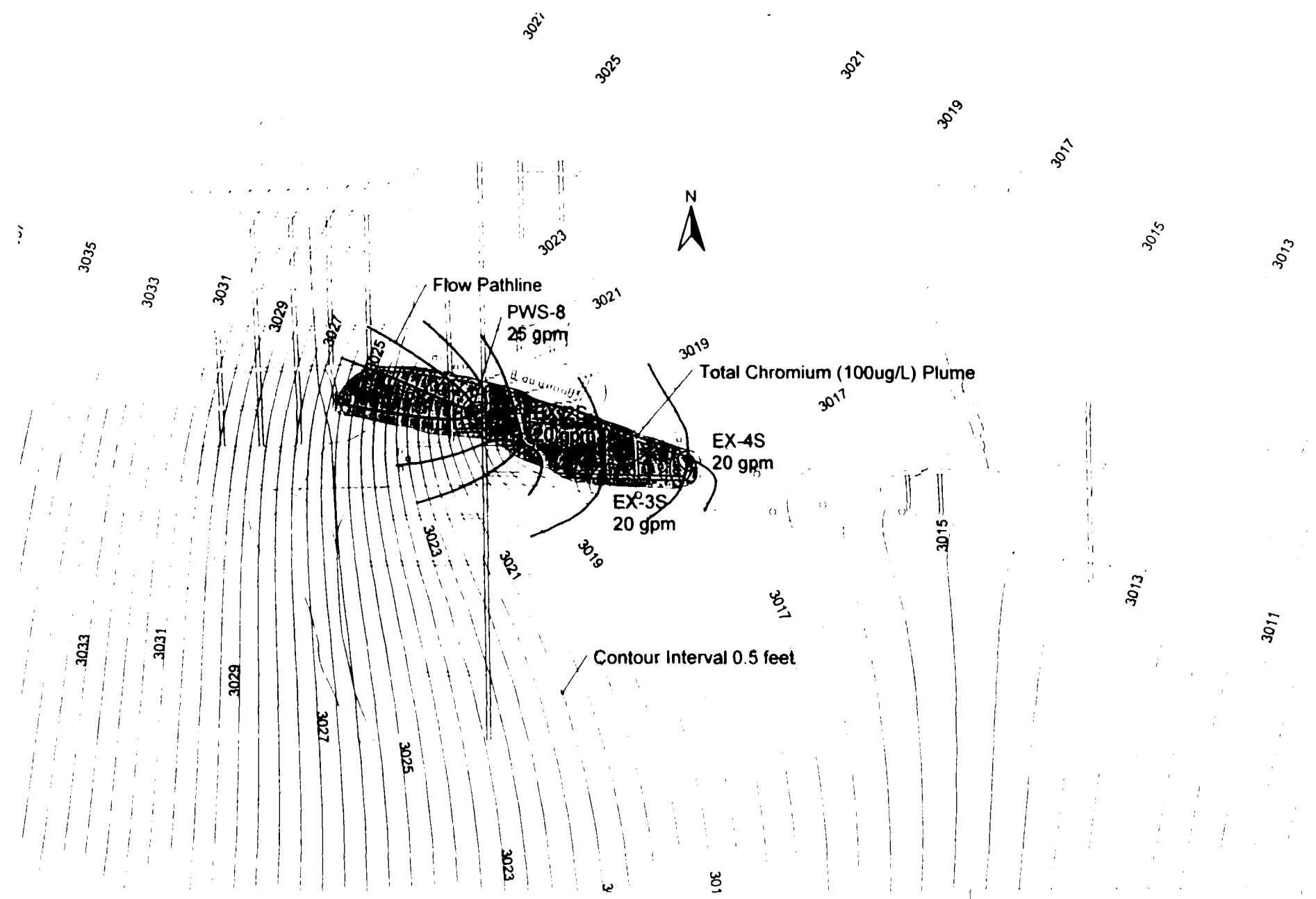


Figure 4
 Shallow Zone
 Total Discharge 85 gpm
 3-yr Contaminant Capture Zone

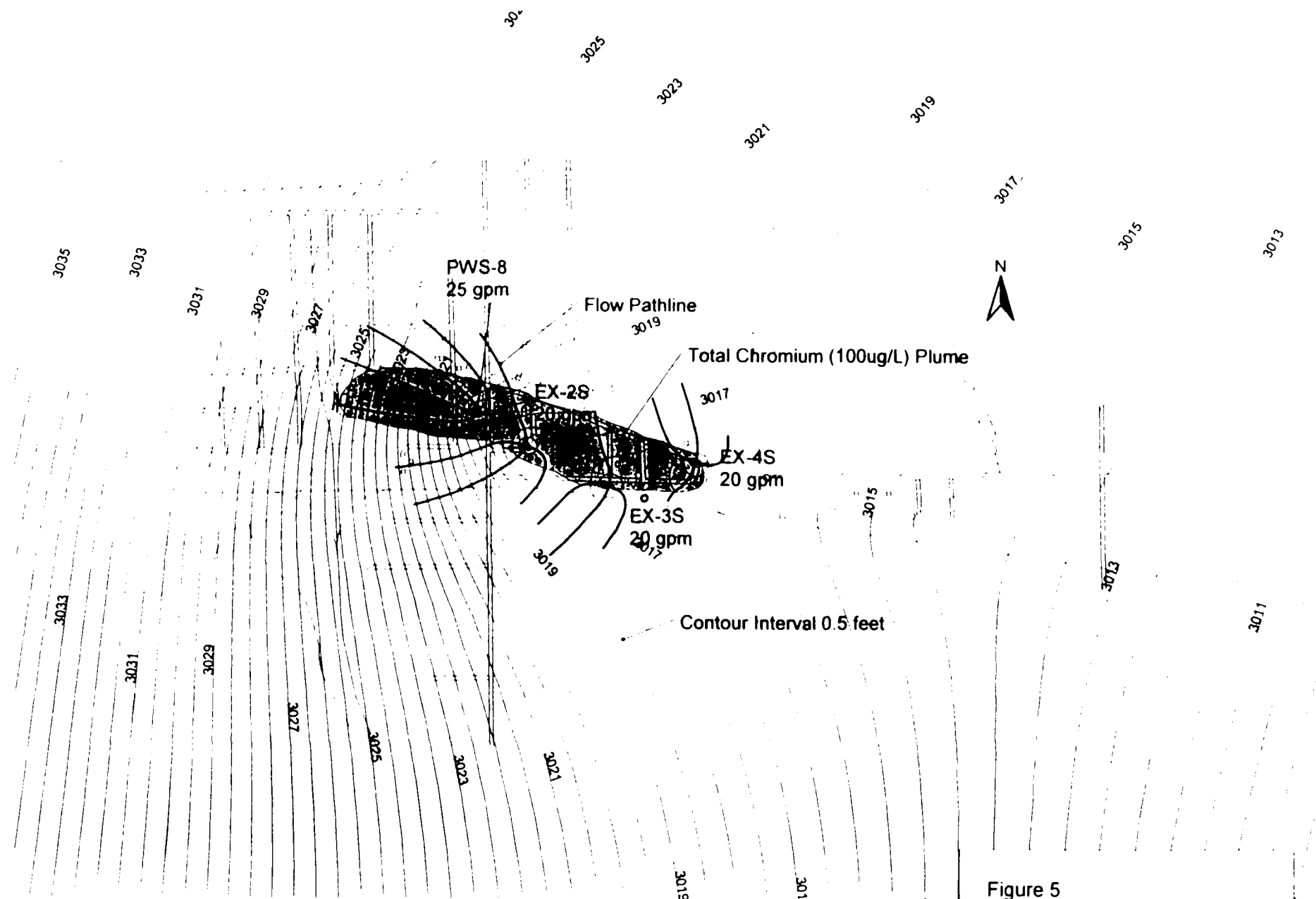


Figure 5
 Shallow Zone
 Total Discharge 85 gpm
 3-yr Contaminant Capture Zone

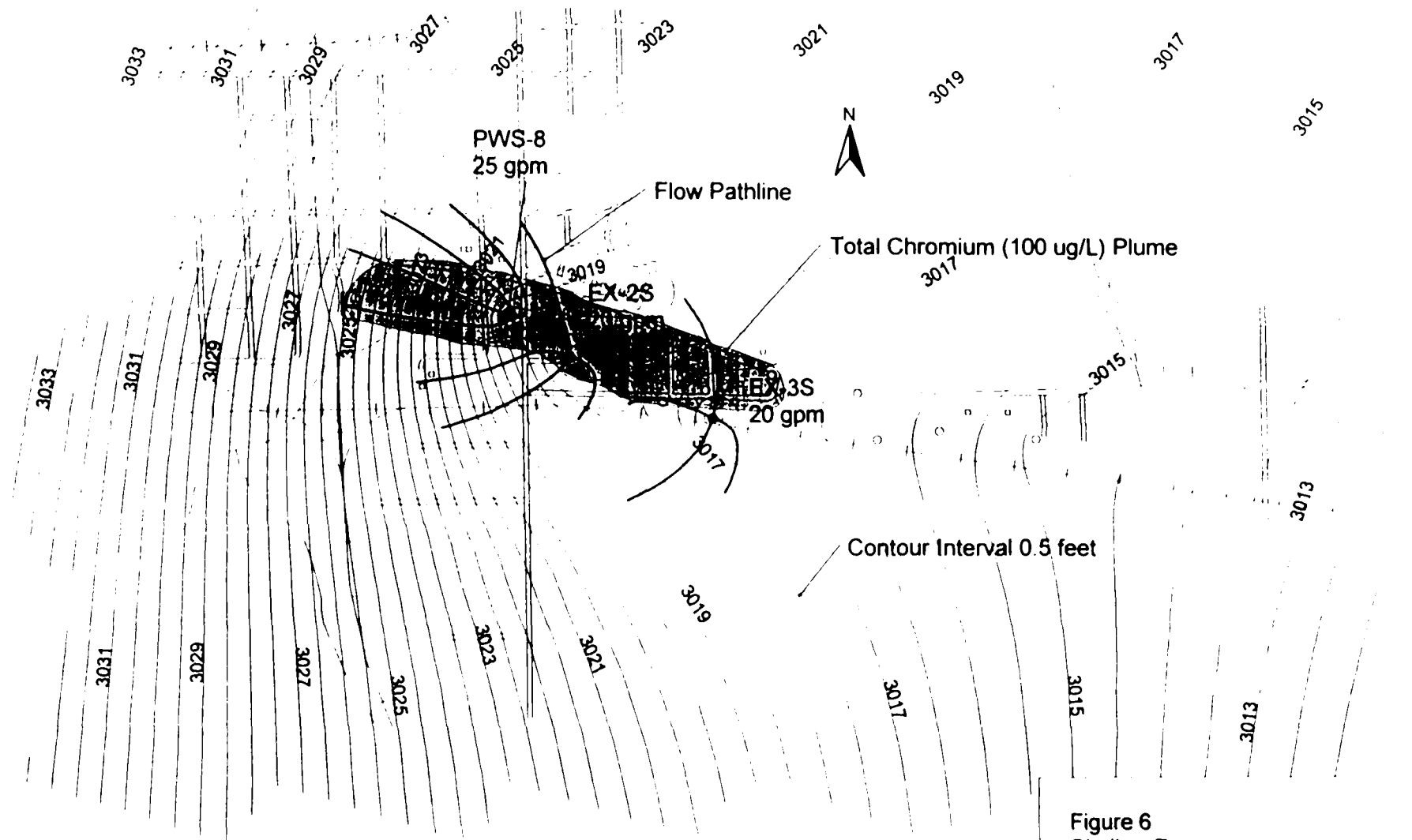


Figure 6
 Shallow Zone
 Total Discharge 65 gpm
 3-yr Contaminant Capture Zone

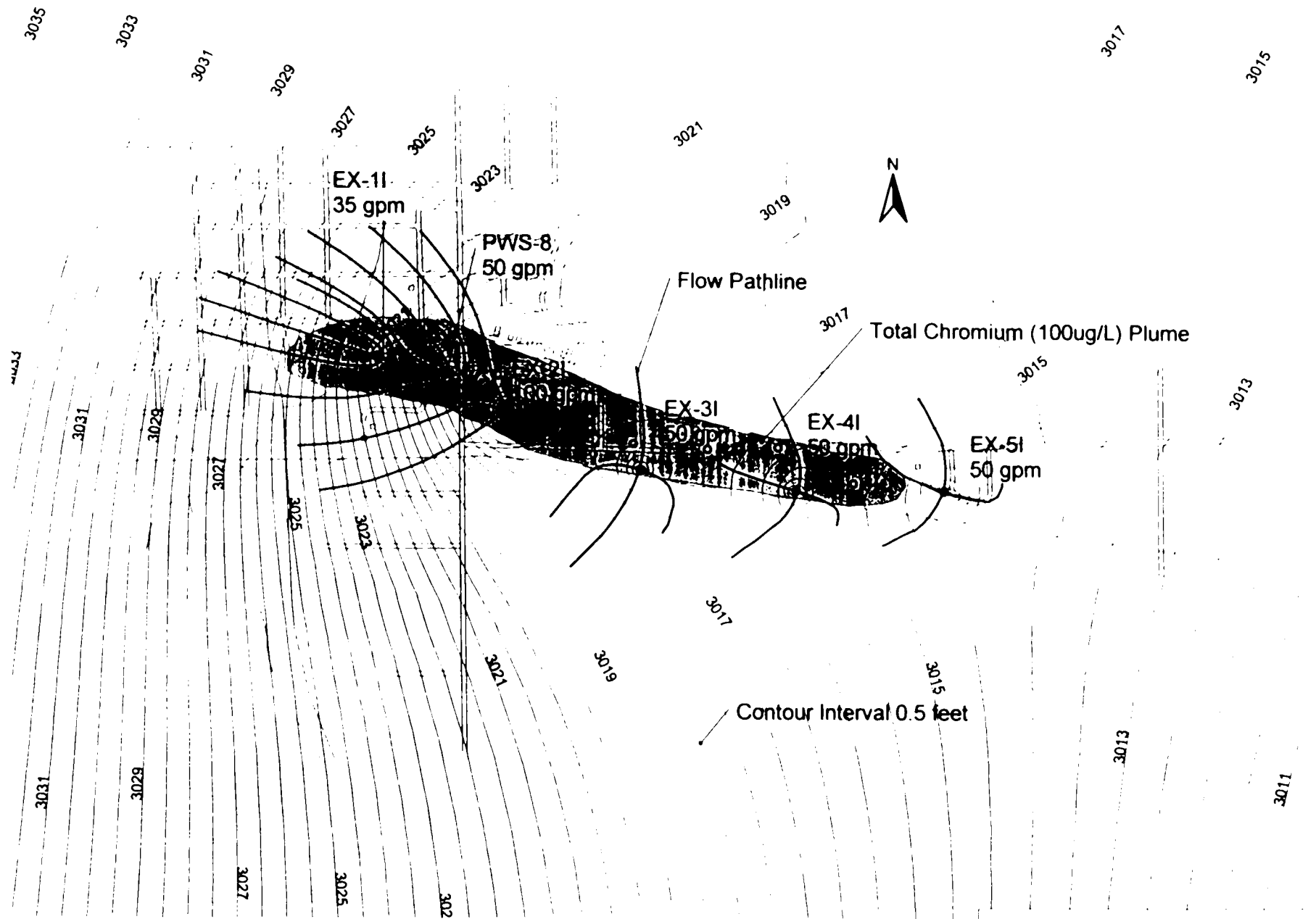


Figure 7
 Intermediate Zone
 Total Discharge 335 gpm
 3-yr Contaminant Capture Zone

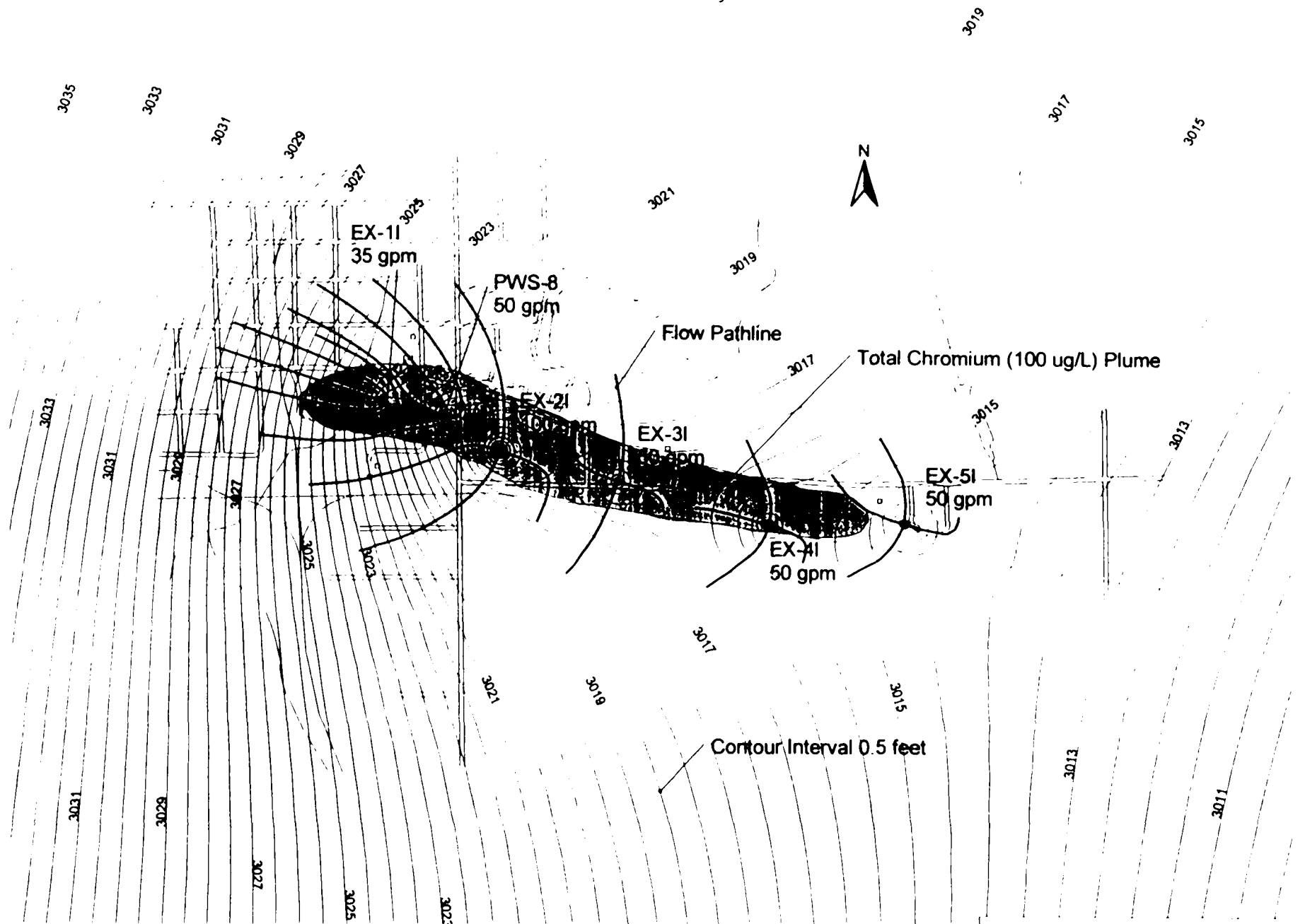


Figure 8
 Intermediate Zone
 Total Discharge 335 gpm
 3-yr Contaminant Capture Zone

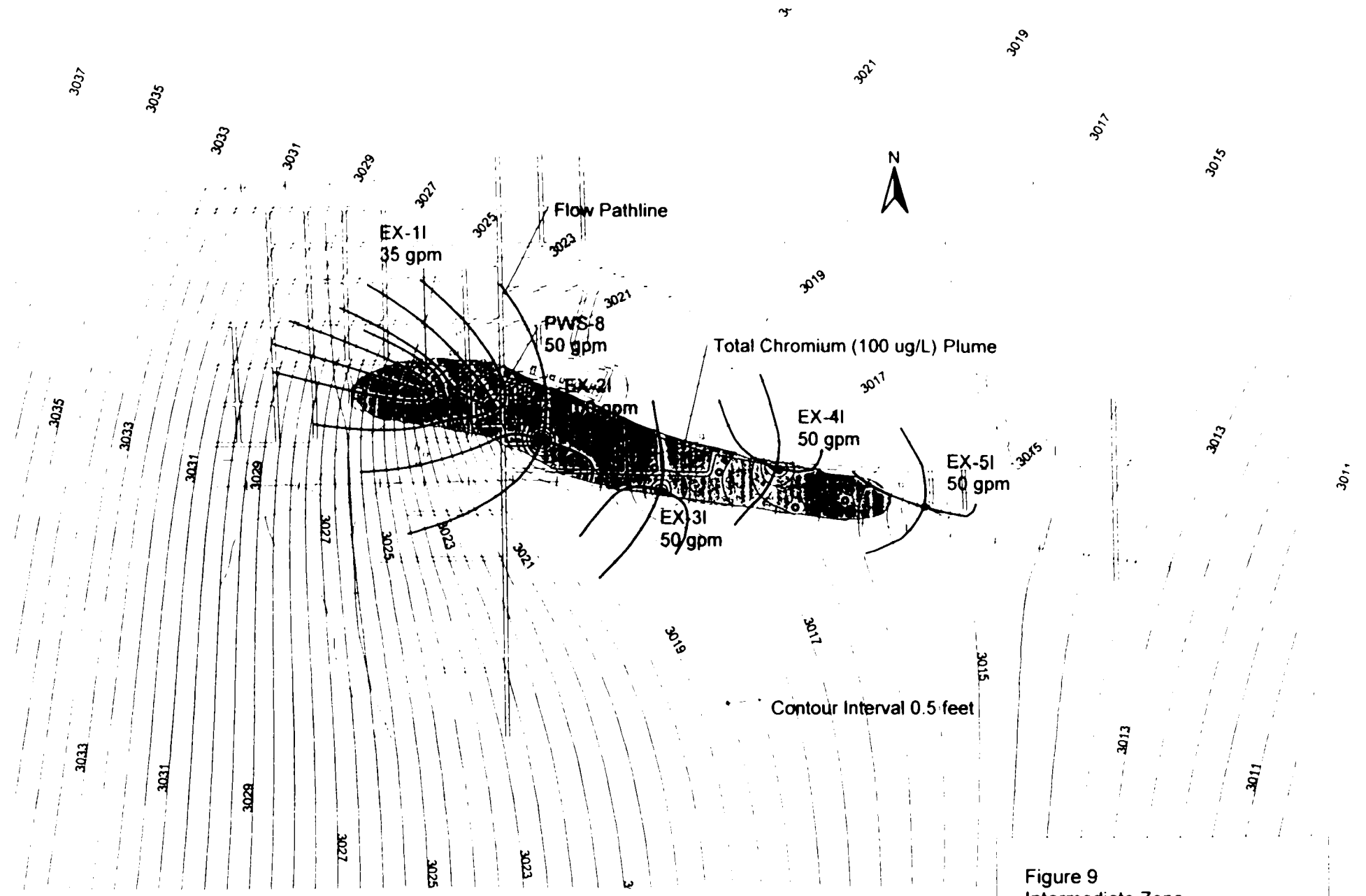


Figure 9
 Intermediate Zone
 Total Discharge 335 gpm
 3-yr Contaminant Capture Zone

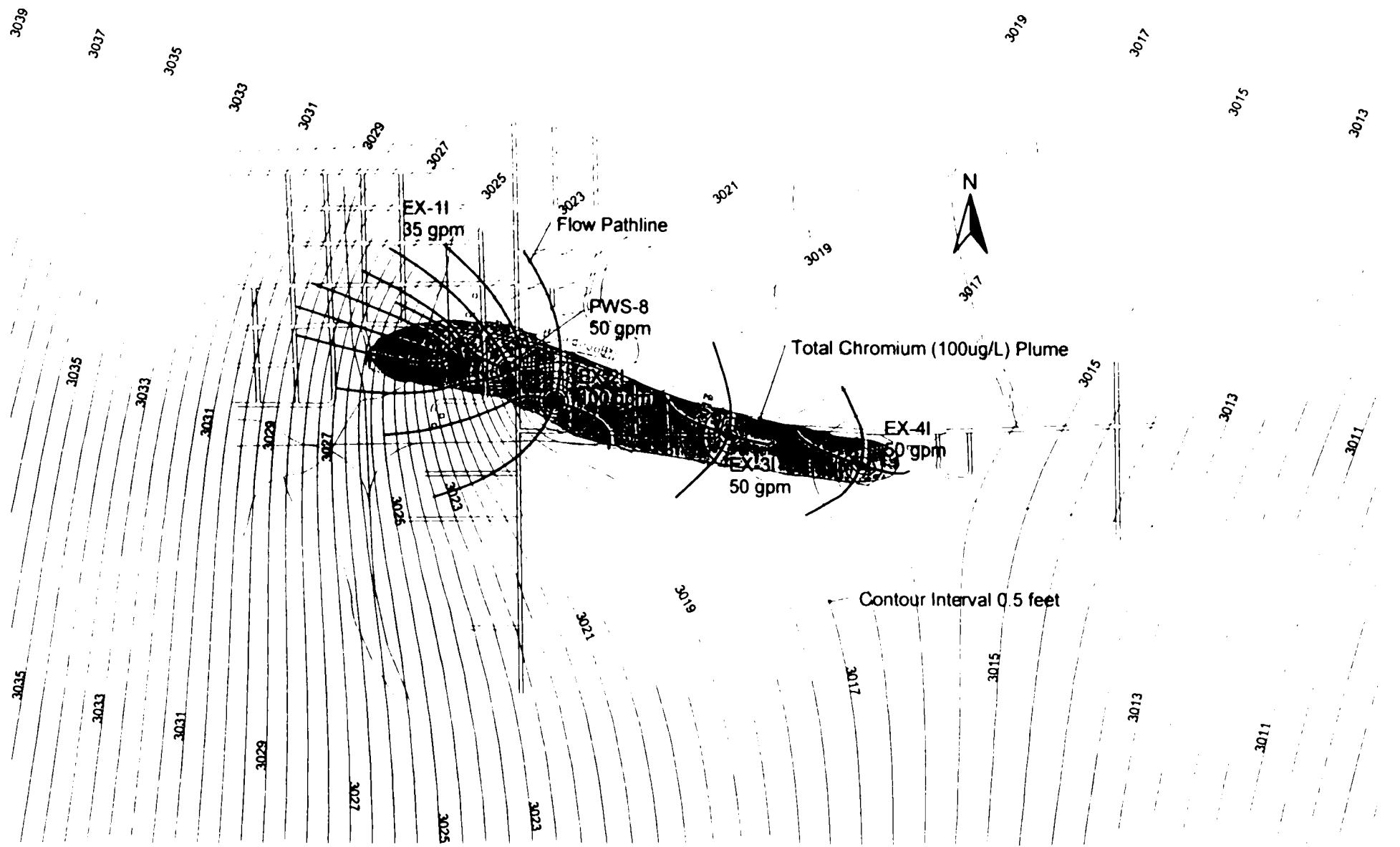


Figure 10
 Intermediate Zone
 Total Discharge 285 gpm
 3-yr Contaminant Capture Zone

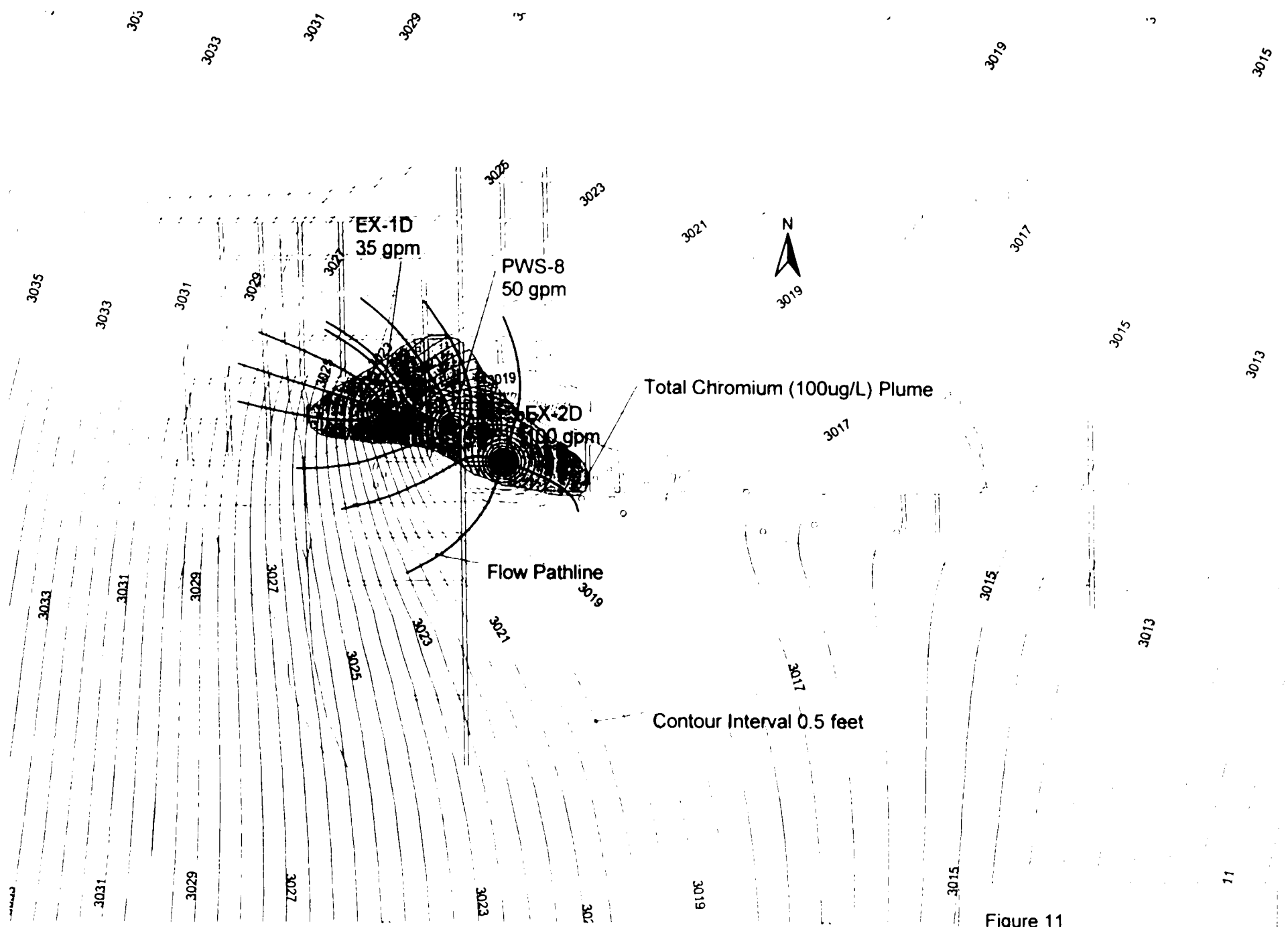


Figure 11
 Deep Zone
 Total Discharge 185 gpm
 3-yr Contaminant Capture Zone

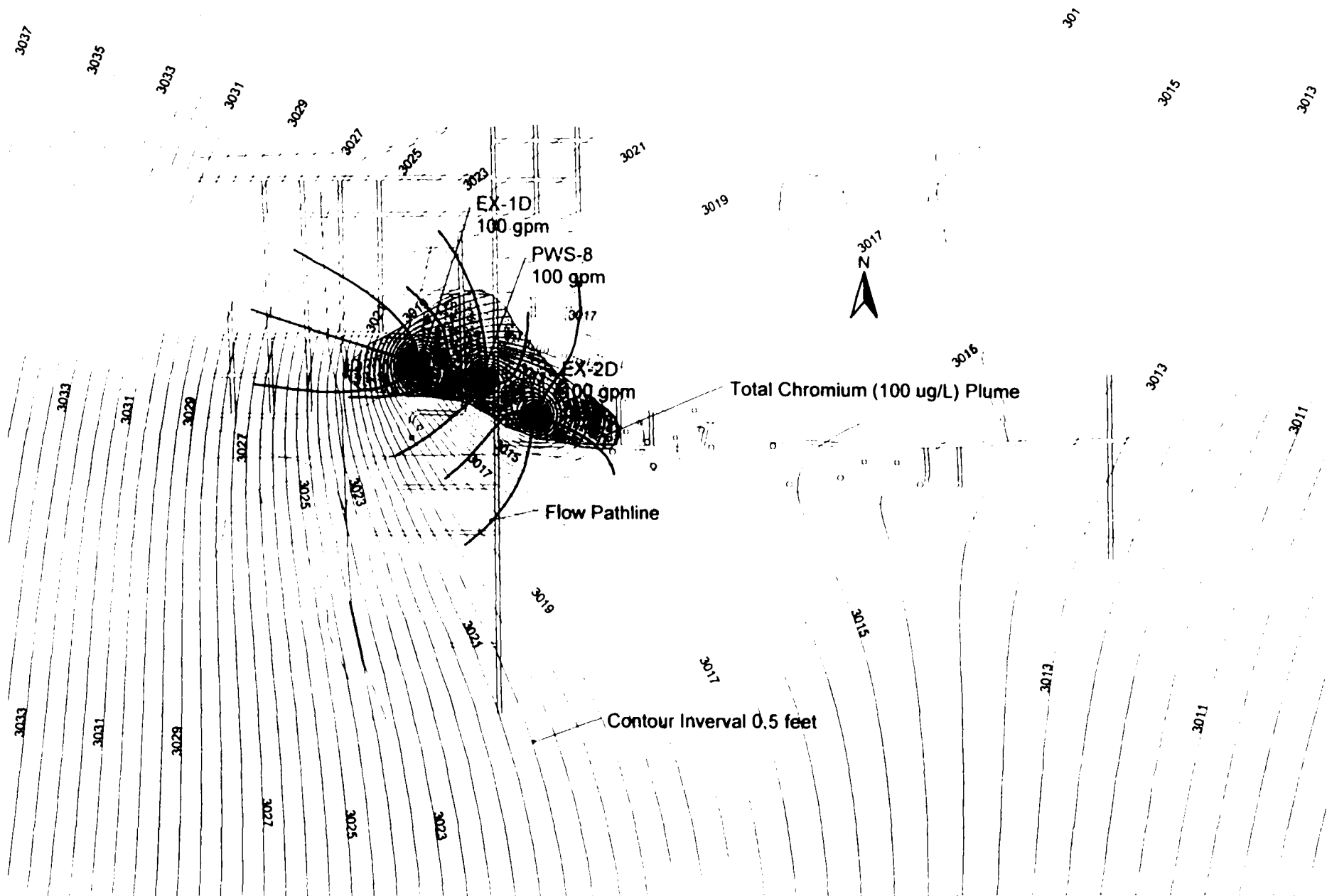


Figure 12
 Deep Zone
 Total Discharge 300 gpm
 3-yr Contaminant Capture Zone

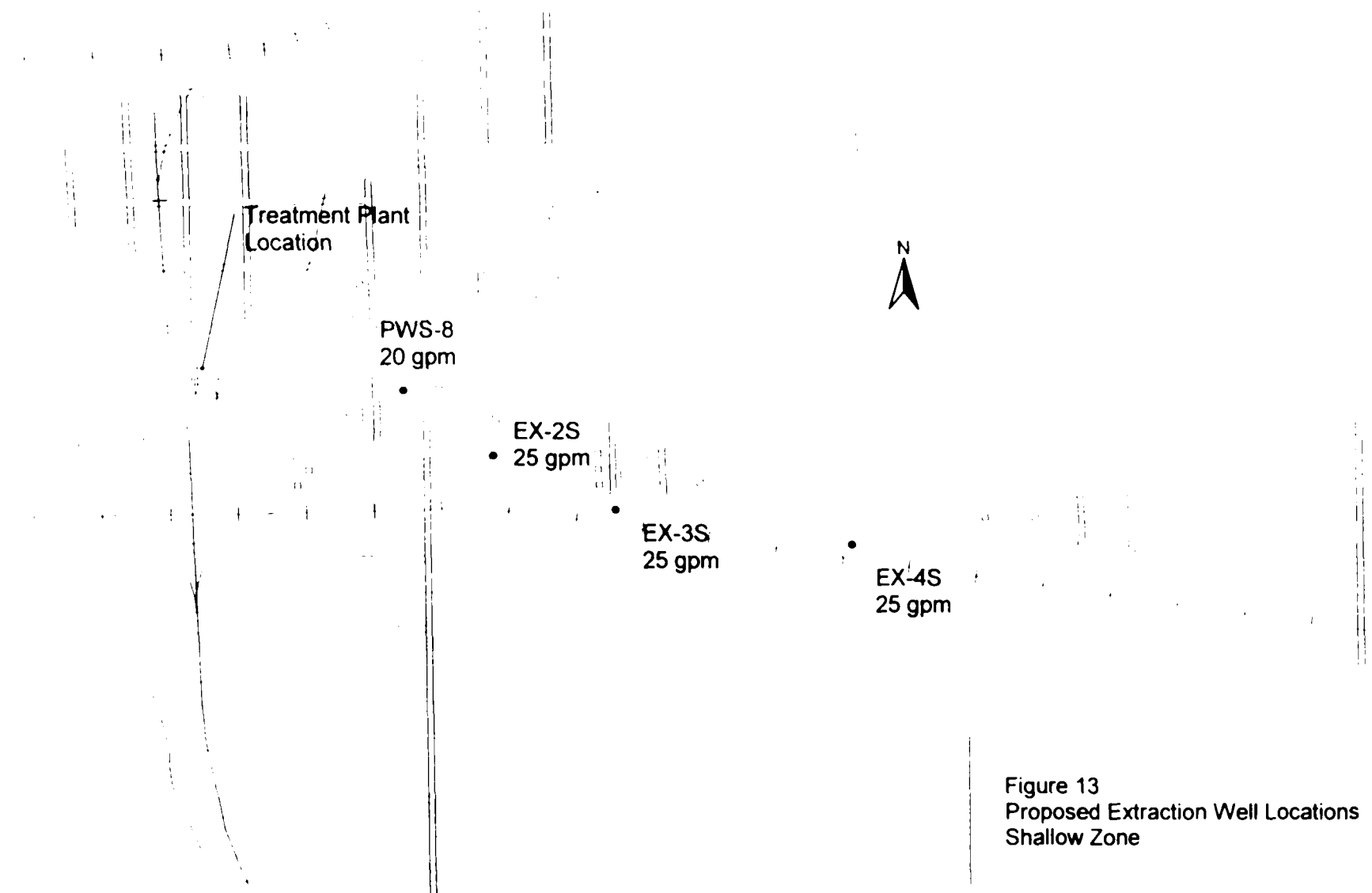


Figure 13
Proposed Extraction Well Locations
Shallow Zone

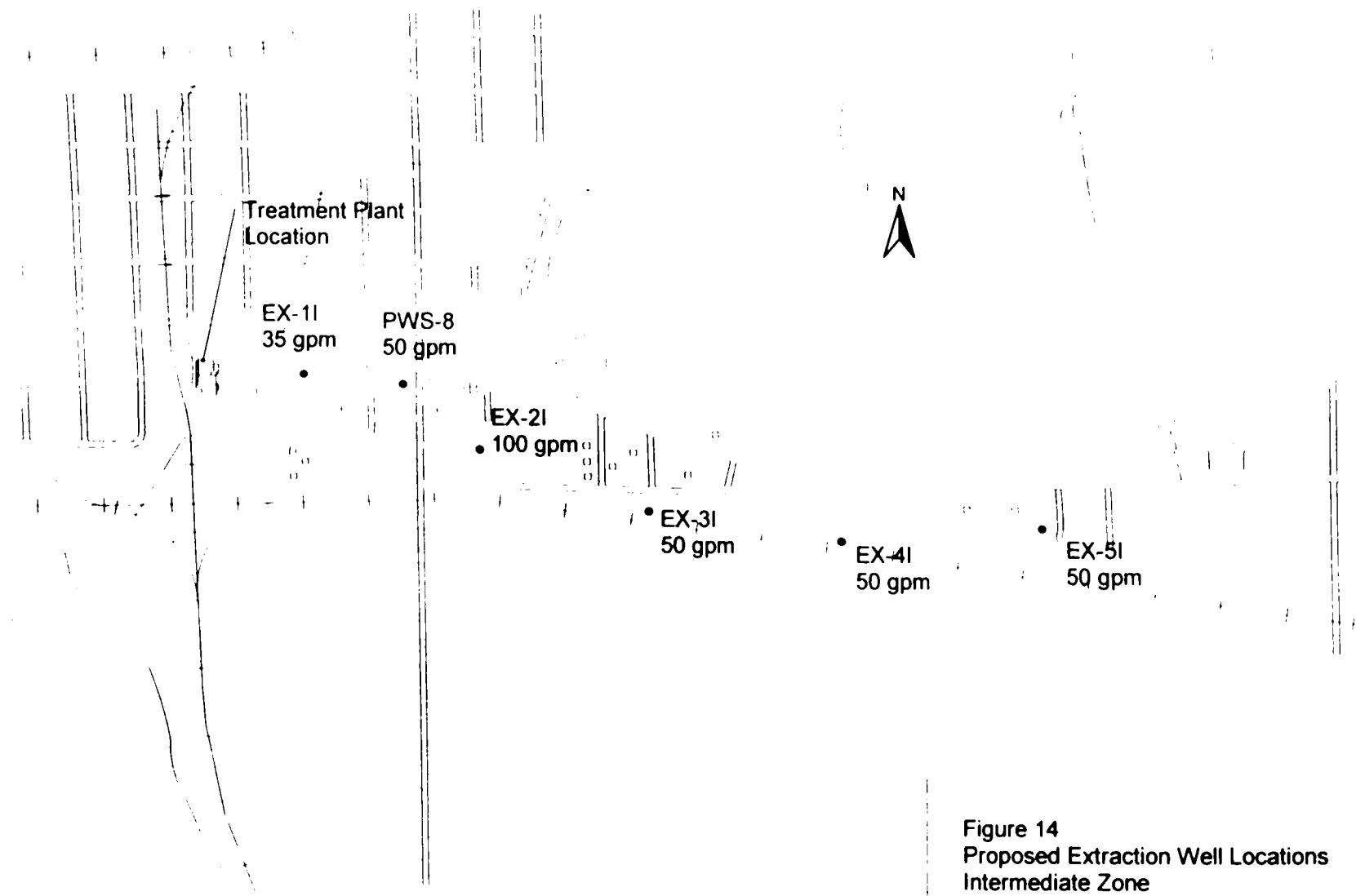


Figure 14
Proposed Extraction Well Locations
Intermediate Zone

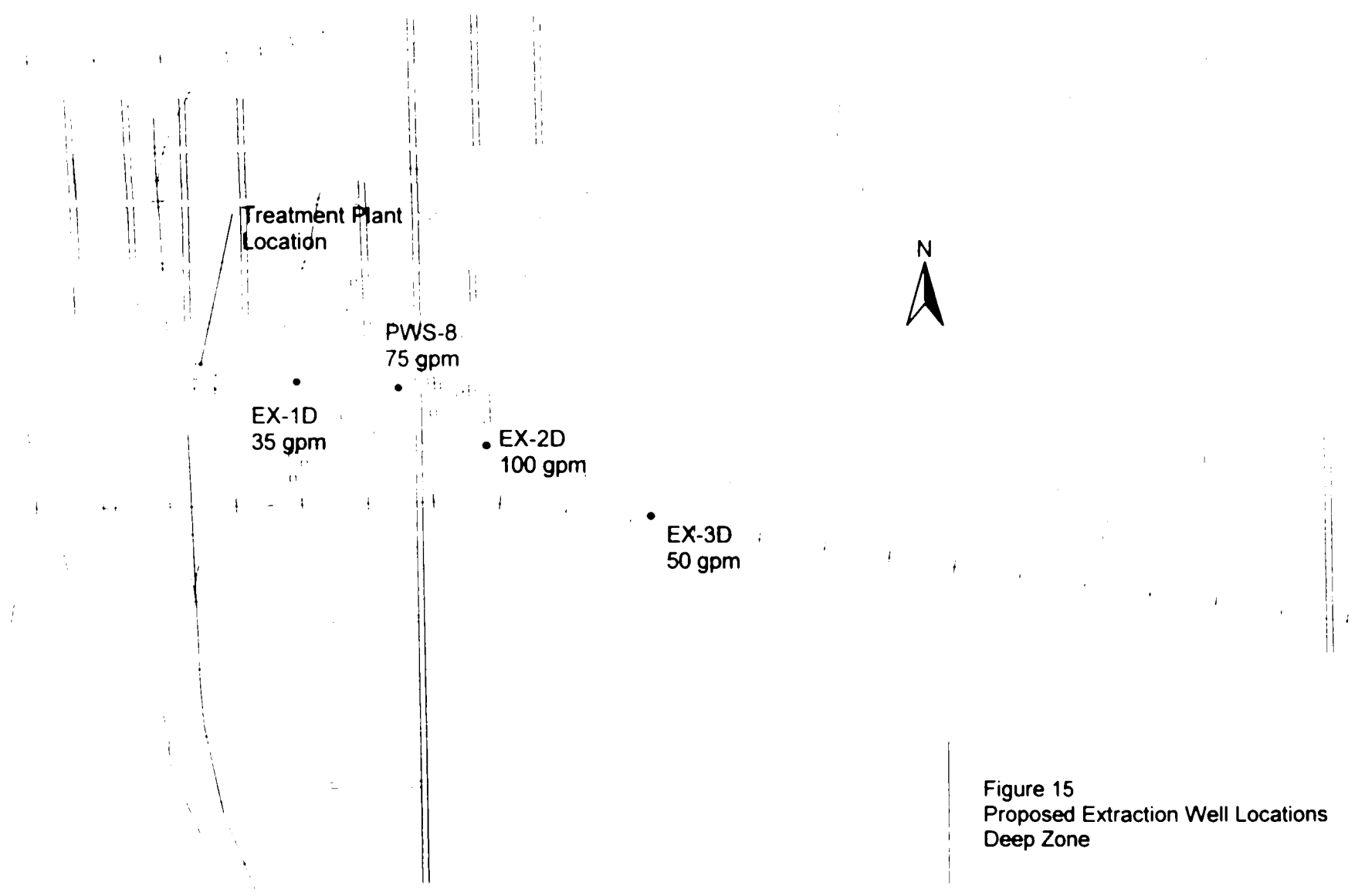


Figure 15
Proposed Extraction Well Locations
Deep Zone

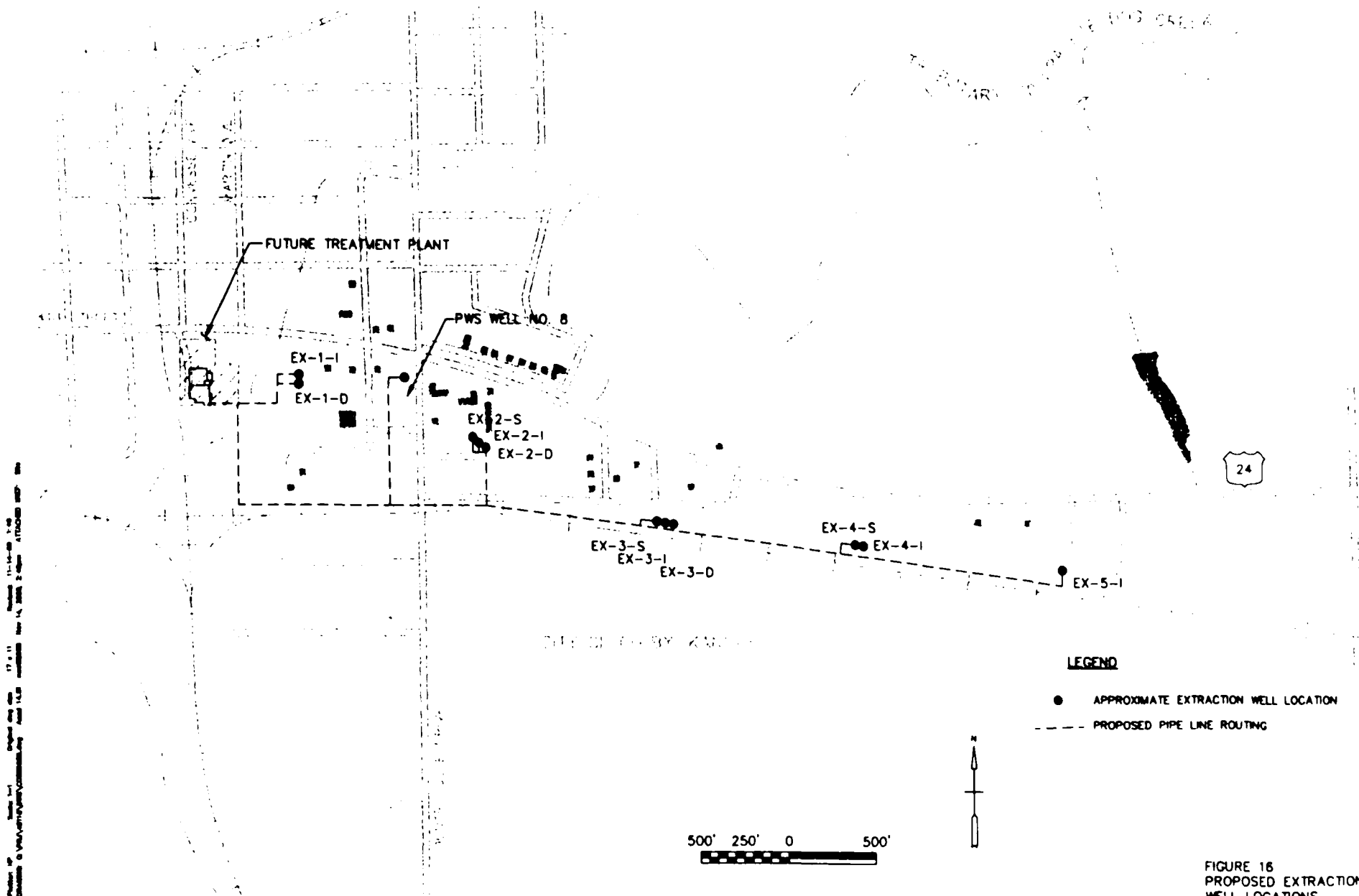


FIGURE 16
 PROPOSED EXTRACTION
 WELL LOCATIONS
 ACF SERVICES SITE

Appendix J

EPA and KDHE Comments and Responses on *Technical Memorandum Remedial Design Sampling Activities, Ace Services Site, Colby, Kansas, March 29, 2000.*



BLACK & VEATCH

6601 College Boulevard
Overland Park, Kansas 66211 USA

Tel (913) 458-2900

Black & Veatch Special Projects Corp.

File L. >
46118

USEPA Region VII
Ace Services Site

BVSPC Project 46118.126 ✓
BVSPC File 2
May 12, 2000

Mr. Bob Stewart
USEPA Region VII
901 N. 5th Street
Kansas City, Kansas 66101

Subject: EPA Contract No. 68-W5-0004
W.A. No. 034-RDRD-07GE
Responses to KDHE
Review Comments for *Technical
Memorandum Remedial Design Sampling
Activities, Ace Services Site, Colby, Kansas*

Dear Mr. Stewart:

The following are responses to review comments for the *Technical Memorandum Remedial Design Sampling Activities, Ace Services Site, Colby, Kansas (March 29, 2000)*. The comments were provided by the Kansas Department of Health and Environment (KDHE), April 18, 2000. The review comments are restated in italics, followed by responses from Black & Veatch Special Projects Corp. (BVSPC).

1. *KDHE/BER requests an electronic copy of the site map when it is completed.*

An electronic copy of the site map will be forwarded to KDHE when the survey is final.

2. *Pages 3-5 and 3-9, Sections 3.1.5 and 3.3.2. Newly installed wells were sampled immediately after the wells were developed. The well development procedure, however, only removed "at least half as much water as was introduced during drilling". From the discussion in the report, there appears to be the potential that samples from the new wells may not be representative of aquifer conditions. Is data from the new wells consistent with the old wells? For example, consider the results from MW-8-D (89 mg/L total Cr) compared to PWS well No. 8 (1930 mg/L total Cr) which is immediately adjacent. The report should discuss the implications of the well development procedure relative to any theoretical effects on the quality of the samples.*

Well development consisted of surging and pumping the well using an electric

Mr. Bob Stewart

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May 12, 2000

submersible pump. The temperature, pH, specific conductivity, turbidity, dissolved oxygen (DO), and oxidation reduction potential (ORP) was monitored during pumping. Pumping continued until the field parameters stabilized and the water was clear and free of fines at which time the samples were collected.

Additional water was also removed during well construction. Approximately 400 gallons of water was displaced and collected from each boring during installation of the well casing, filter packs, bentonite seal, and bentonite grout. This information will be included in the report.

This same development/sampling method was used for all newly installed wells. Analytical results of total chromium in groundwater samples ranged from non-detect to 2740 ug/L, indicating dilution of groundwater by introducing drilling fluid (potable water) was not significant and that the samples are representative of groundwater quality.

All wells will be sampled again during the final stages of the remedial design. Analytical results of the two rounds of sampling will be compared and, if necessary, extraction well locations could be relocated to accommodate changes in concentrations and limits of the plume.

3. *Page 5-1, Section 5-2, last sentence. Conclusive evidence has not been gathered to show that leaching of residual chromium from the unsaturated zone to groundwater is no longer occurring. Showing that chromium concentrations in the unsaturated zone decrease with depth only shows the depths of chromium contamination in the unsaturated zone. Migration of chromium to groundwater does not occur through movement of the mass of chromium downward through the unsaturated zone, but rather by dissolution of chromium as water percolates downward to the water table. Chromium concentrations in groundwater 200 to 500 feet downgradient of Ace Services still range from 500 to 1130 mg/L. During the removal of chromium sludge in 1994, it was recognized that the bottom of the soil contamination had not been reached even after digging 20 feet below the floor of the Ace Services building (EPA Site Progress Report, July 13, 1994). If the source has been significantly reduced, then with time chromium concentrations in groundwater near the source area should diminish while higher concentrations continue to exist downgradient. Enough time may not have passed to see such a trend, however, since remediation of groundwater will not be successful without significant source reduction, further analysis should be conducted to assess whether or not the source area continues to be active.*

Ceasing discharge of wastewater and the excavation of contaminated sludge and soils has removed the primary sources of groundwater contamination. It is not evident that the remaining contaminants will migrate significantly to the groundwater.

Elevated chromium levels in the surface soil of the lagoon area was addressed when the surface soil was remediated to cleanup levels (1500 mg/kg total chromium and 500 mg/kg lead) during the 1994 removal action. A monitoring well (MW-10-P) was installed near the former lagoon and screened at a depth of 30 feet (BVSPC 1999) to evaluate the possibility of a contaminated perched groundwater zone. Well MW-10-P has been dry on every water level measurement event indicating the perched groundwater zone is no longer present.

As described in comment #6 of the Responsiveness Summary of the ROD, EPA will conduct further investigation of the subsurface soil. Initial efforts including subsurface soil sampling and installation of well MW-10-P has been performed. Additional efforts will continue up to and after the groundwater extraction program has begun. This will allow EPA to judge the effectiveness of the extraction and then determine if the soils have a continuing source impact on the groundwater quality. A decision concerning further remedial action of the soil will be made before or during the 5-year review

Further evaluation of significant leaching of contaminants from the lagoon area soils will be made by sampling groundwater from each of the three screened intervals of the Ace Recovery well. The groundwater sampling will be performed quarterly for the first year as part of the remedial action as described in the ROD or more frequently as necessary to evaluate contaminant trends in the groundwater. Analytical results from groundwater samples collected from the Ace Recovery well will identify any trends in contaminant leaching. It is estimated that the contaminant concentrations will decrease with time. In addition, well MW-10-P will be monitored to verify that the perched groundwater condition is still no longer present.

4. *Figures 5-7 and 5-8. The extent of chromium contamination above the Maximum Contaminant Level (MCL) within shallow and intermediate depths of the groundwater aquifer has not been defined. The extent needs to be known to determine if the plume can be captured by the proposed extraction wells and to determine if additional receptors, such as wells R-7 and R-8, might be at risk. KDHE/BER recommends installation of additional wells*

Mr. Bob Stewart

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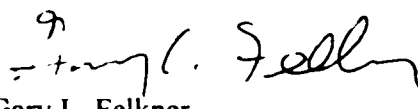
east of MW-12 to define the downgradient extent of chromium contamination. KDHE/BER also recommends installation of additional wells south of the railroad line because the direction of groundwater flow indicates that the chromium plume should be oriented in a more southeasterly direction from the source area. Most receptors to the plume are located along either side of Highway 24, which led us to position monitor wells along the same east-west directional trend. This has resulted in a picture of the plume that follows the highway, rather than the groundwater gradient. To determine if the plume will be captured by the extraction wells, the spatial distribution of the plume needs to be known. See enclosures 1 and 2 for the areas where additional wells should be located.

Current data have delineated the plume extent and concentration for the purposes of remedial design. However, to further ensure optimization of the placement of extraction wells additional monitoring wells will be installed as KDHE requests. It is proposed that two additional groundwater monitoring well nests consisting of shallow and intermediate depth wells be installed south of the railroad tracks. Proposed locations for the two well nests are illustrated on the attached figure. Final locations of the wells will be limited to property access restrictions.

If you have any questions or require any additional information, please call me at (913) 458-6583.

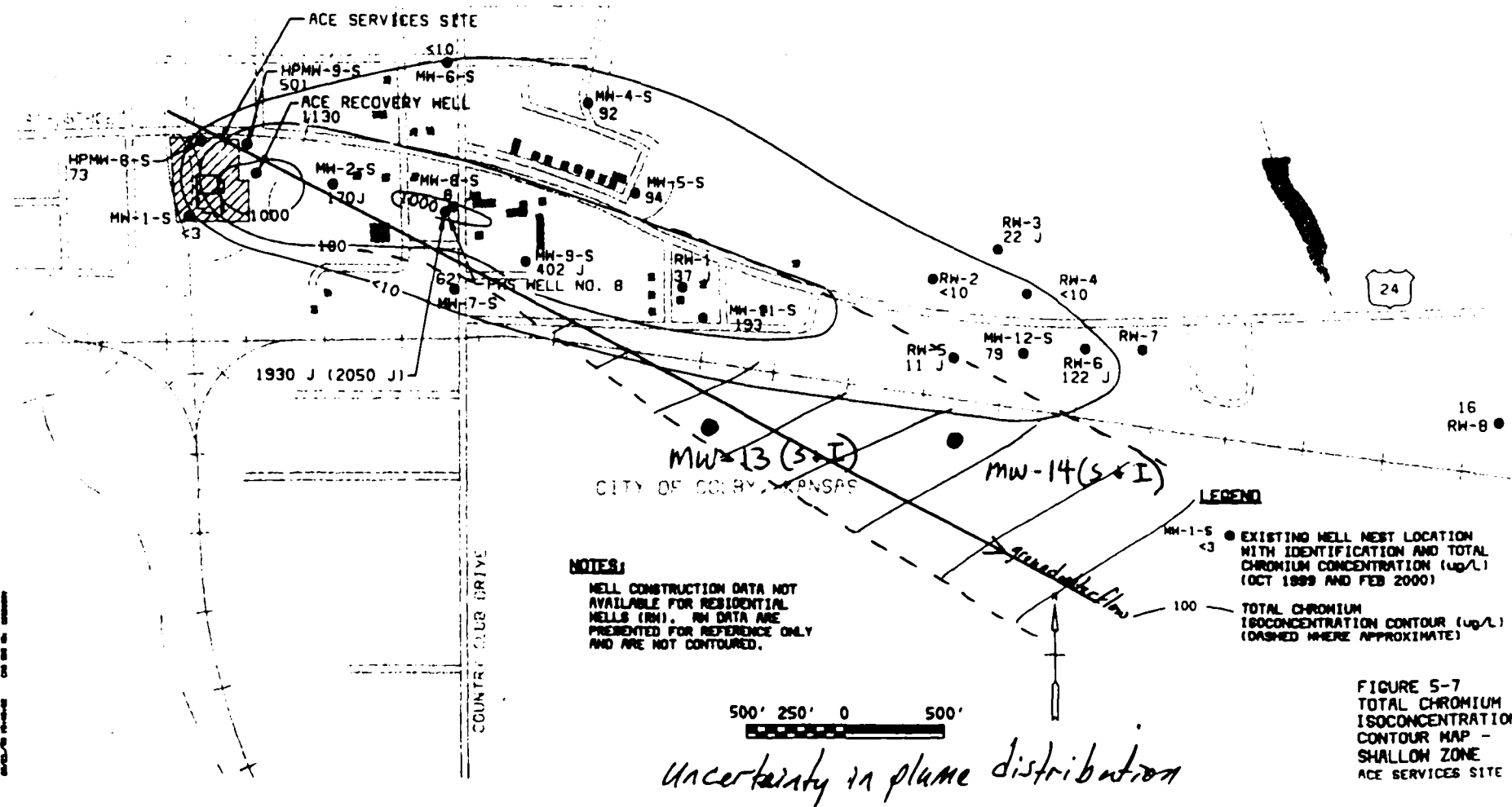
Sincerely,

BLACK & VEATCH SPECIAL PROJECTS
CORP.


Gary L. Felkner
Site Manager

cc: Randy Carlson, KDHE
File

Enclosure 1
 proposed area of additional well
 ● MW-13(S+I)
 Proposed Well Location



NOTES:
 WELL CONSTRUCTION DATA NOT AVAILABLE FOR RESIDENTIAL WELLS (RW). RW DATA ARE PRESENTED FOR REFERENCE ONLY AND ARE NOT CONTOURED.

LEGEND

● MW-1-S <3 ● EXISTING WELL NEAR LOCATION WITH IDENTIFICATION AND TOTAL CHROMIUM CONCENTRATION (ug/L) (OCT 1999 AND FEB 2000)

100 TOTAL CHROMIUM ISOCONCENTRATION CONTOUR (ug/L) (DASHED WHERE APPROXIMATE)

FIGURE 5-7
 TOTAL CHROMIUM ISOCONCENTRATION CONTOUR MAP - SHALLOW ZONE ACE SERVICES SITE