

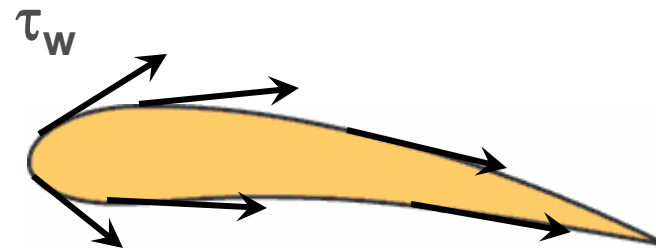
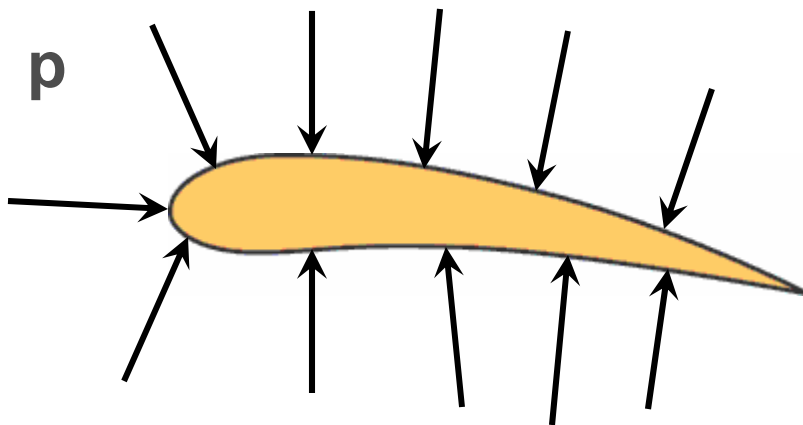
Reading: Chapter 4

Recall: Aerodynamic Forces

- “Theoretical and experimental aerodynamicists labor to calculate and measure flow fields of many types.”
- ... because “the aerodynamic force exerted by the airflow on the surface of an airplane, missile, *etc.*, stems from only two simple natural sources:

Pressure distribution on the surface (normal to surface)

Shear stress (friction) on the surface (tangential to surface)



Fundamental Principles

- Conservation of mass
⇒ Continuity equation (§§ 4.1-4.2)
- Newton's second law ($F = ma$)
⇒ Euler's equation & Bernoulli's equation (§§ 4.3-4.4)
- Conservation of energy
⇒ Energy equation (§§ 4.5-4.7)

First: Buoyancy

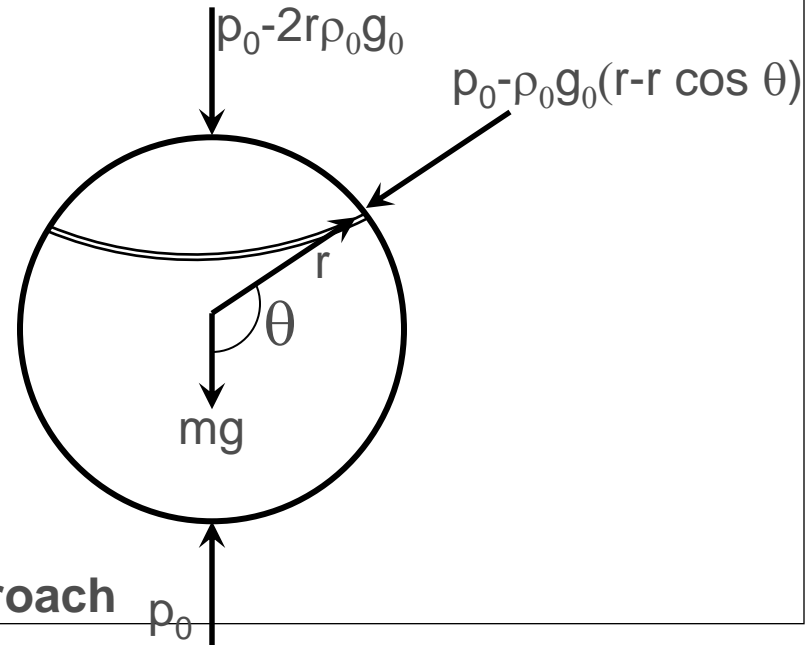
- One way to get lift is through Archimedes' principle of buoyancy
- The buoyancy force acting on an object in a fluid is equal to the weight of the volume of fluid displaced by the object

- Requires integral
(assume ρ_0 is constant)
 $\rho = \rho_0 - \rho_0 g_0 (r - r \cos \theta)$

Force is

$$p \, dA = [\rho_0 - \rho_0 g_0 (r - r \cos \theta)] \, dA$$

$$dA = 2 \pi r^2 \sin \theta \, d\theta$$



Integrate using “shell element” approach

Buoyancy: Integration Over Surface of Sphere

- Each shell element is a ring with radius $r \sin \theta$, and width $r d\theta$

Thus the differential area of an element is

$$dA = 2 \pi r^2 \sin \theta d\theta$$

- Pressure at each point on an element is

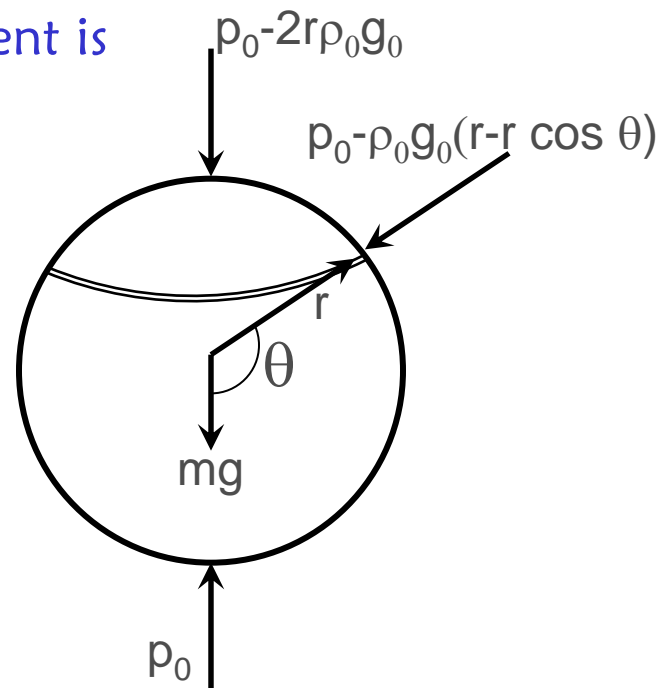
$$p = p_0 - \rho_0 g_0 (r - r \cos \theta)$$

- Force is pressure times area

$$dF = p dA = [p_0 - \rho_0 g_0 (r - r \cos \theta)] dA$$

- Vertical pressure force is

$$dF \cos \theta = p dA \cos \theta = [p_0 - \rho_0 g_0 (r - r \cos \theta)] \cos \theta dA$$



↑ Increasing altitude

Buoyancy: Integration Over Surface of Sphere (continued)

- Total vertical pressure force is found by integrating from $\theta = 0$ to $\theta = \pi$:

$$F_{vp} = 2\pi r^2 \int [\rho_0 - \rho_0 g_0 (r - r \cos \theta)] \cos \theta \sin \theta d\theta$$

- Some useful identities:

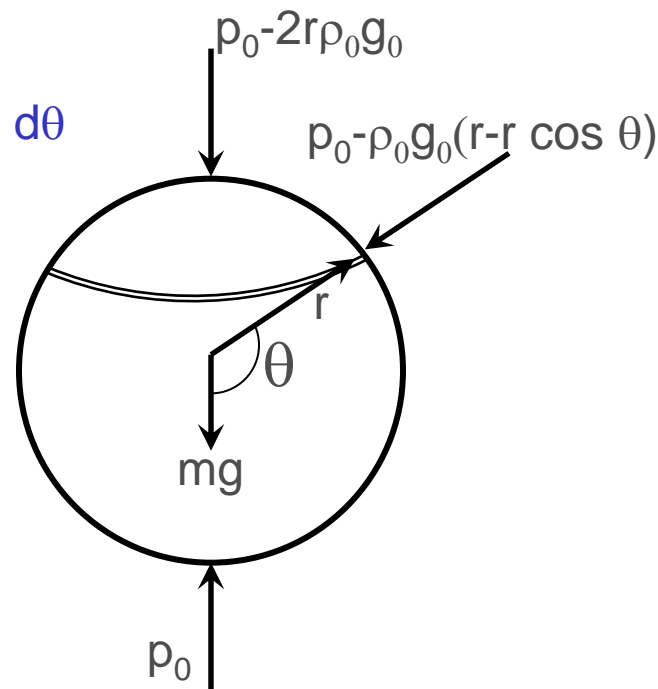
$$\int \cos \theta \sin \theta d\theta = \frac{1}{2} \sin^2 \theta$$

$$\int \cos^2 \theta \sin \theta d\theta = -\frac{1}{3} \cos^3 \theta$$

- Put them together to get

$$F_{vp} = \frac{4}{3} \pi r^3 \cdot \rho_0 \cdot g_0$$

- The first bit is the volume of the sphere; multiplying by density gives mass of fluid displaced; multiplying by gravity gives weight of fluid displaced



Increasing altitude

Buoyancy: Forces on a Sphere (continued)

- Total vertical pressure force is

$$F_{vp} = \frac{4}{3}\pi r^3 \cdot \rho_0 \cdot g_0$$

or

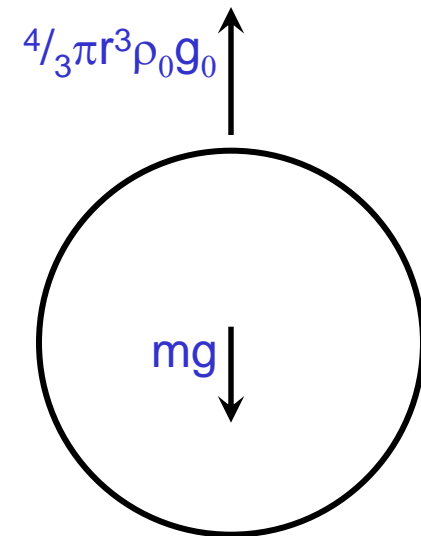
$$F_{vp} = W_v \text{ (weight of volume of fluid)}$$

- Thus the total vertical force on the sphere is

$$F_v = W_v - W_s$$

where $W_s = mg$ is the weight of the sphere

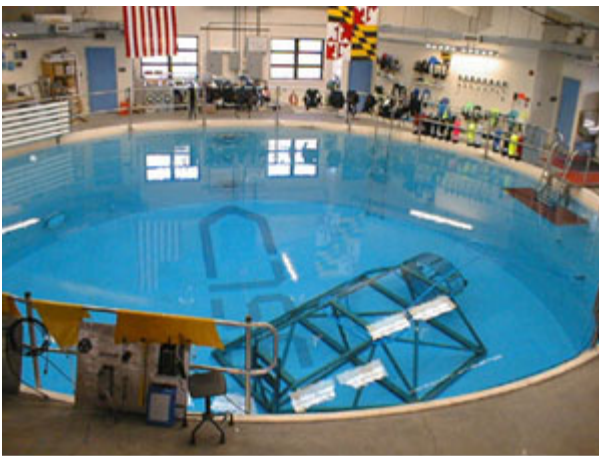
- If $W_v > W_s$, then the net force is a positive “Lift”
- If $W_v < W_s$, then the net force is a negative “Lift”
- If $W_v = W_s$, then the sphere is said to be “neutrally buoyant”



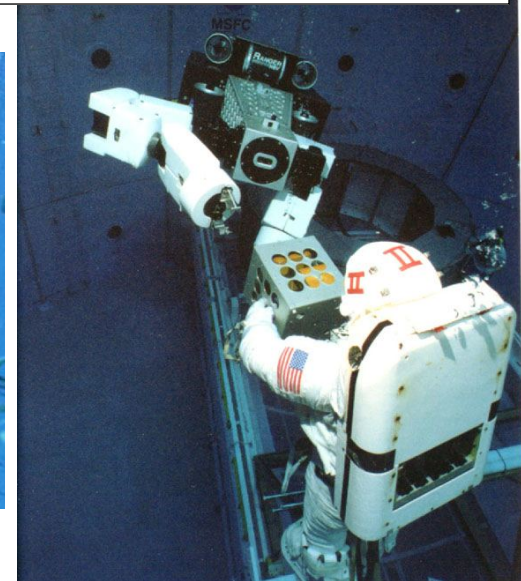
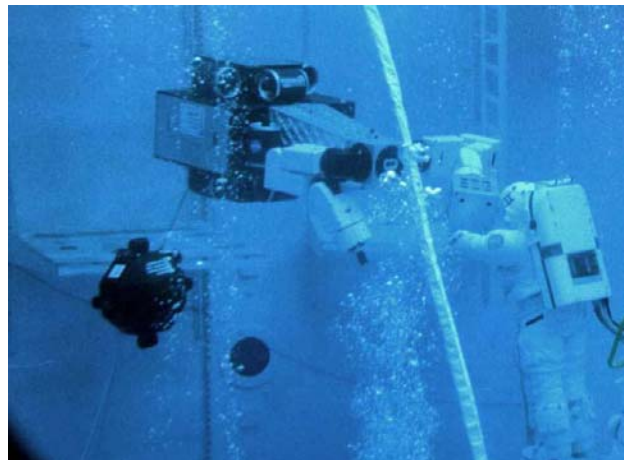
Increasing altitude

Neutral Buoyancy Tanks

- Neutral buoyancy is useful for simulating the freefall environment experienced by astronauts
- NASA's Marshall Space Flight Center has a Neutral Buoyancy Simulator
<http://www1.msfc.nasa.gov/NEWSROOM/background/facts/nbs.htm>
- University of Maryland has a Neutral Buoyancy Tank
<http://www.ssl.umd.edu/facilities/facilities.html>



The deck area of the neutral buoyancy tank. In the water is a mockup of an International Space Station truss.



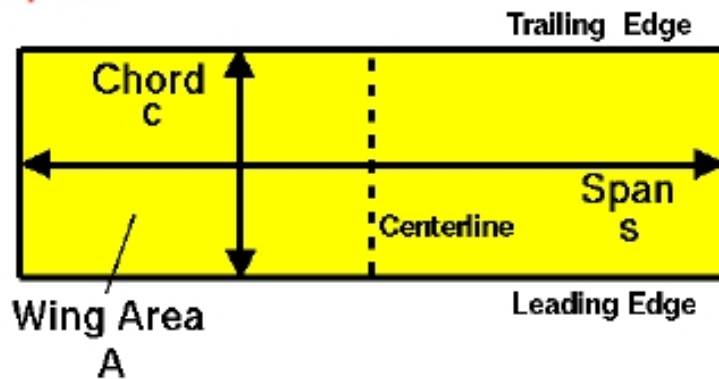
What's In Our Toolbox So Far?

- Four aerodynamic quantities, flow field
- Steady vs unsteady flow
- Streamlines
- Two sources of all aerodynamic forces
- Equation of state for perfect gas
- Standard atmosphere: six different altitudes
- Hydrostatic equation
- Linear interpolation, local approximation
- Lift due to buoyancy
- Viscous vs inviscid flow

Lift from Fluid Motion

- First: Airplane wing geometry
- Span, Chord, Area, Planform, Aspect Ratio, Camber, Leading and Trailing Edges

Top View



Aspect Ratio = AR

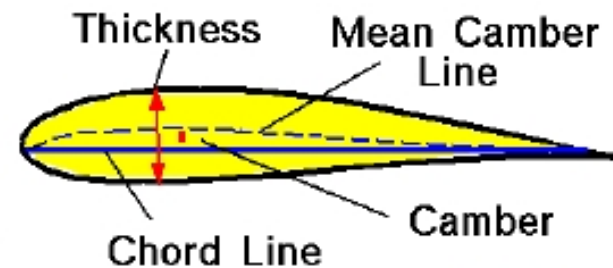
$$AR = \frac{s^2}{A} = \frac{s}{c}$$



Symmetric Airfoil

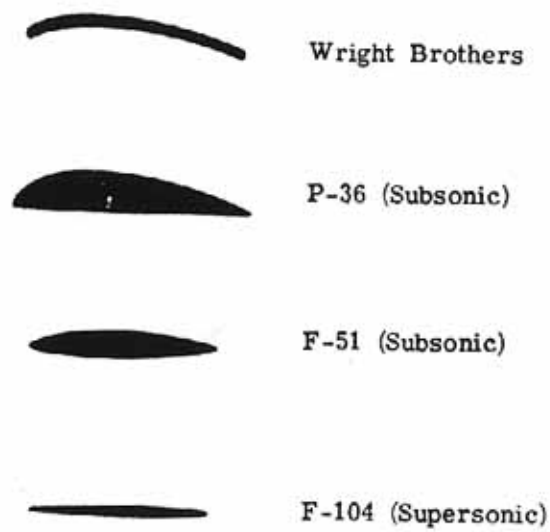
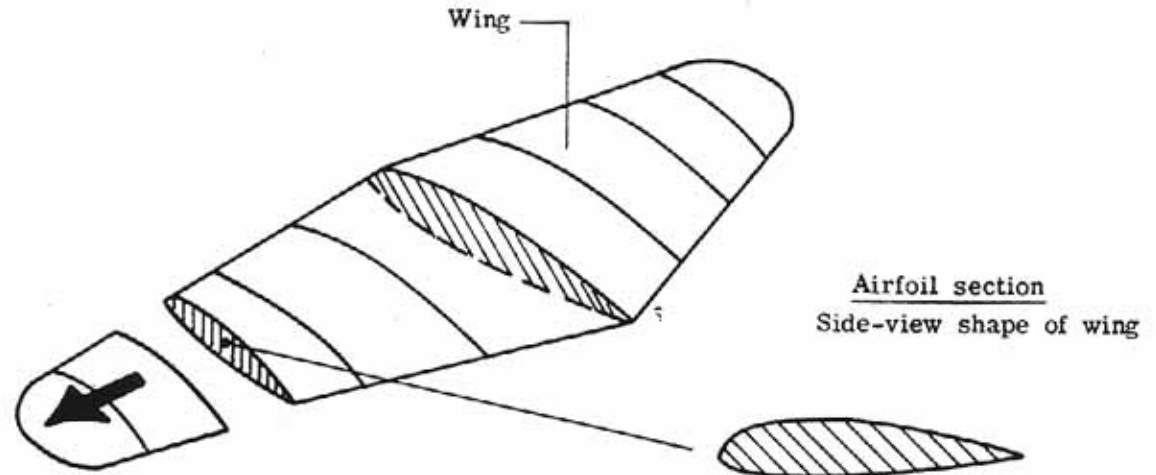
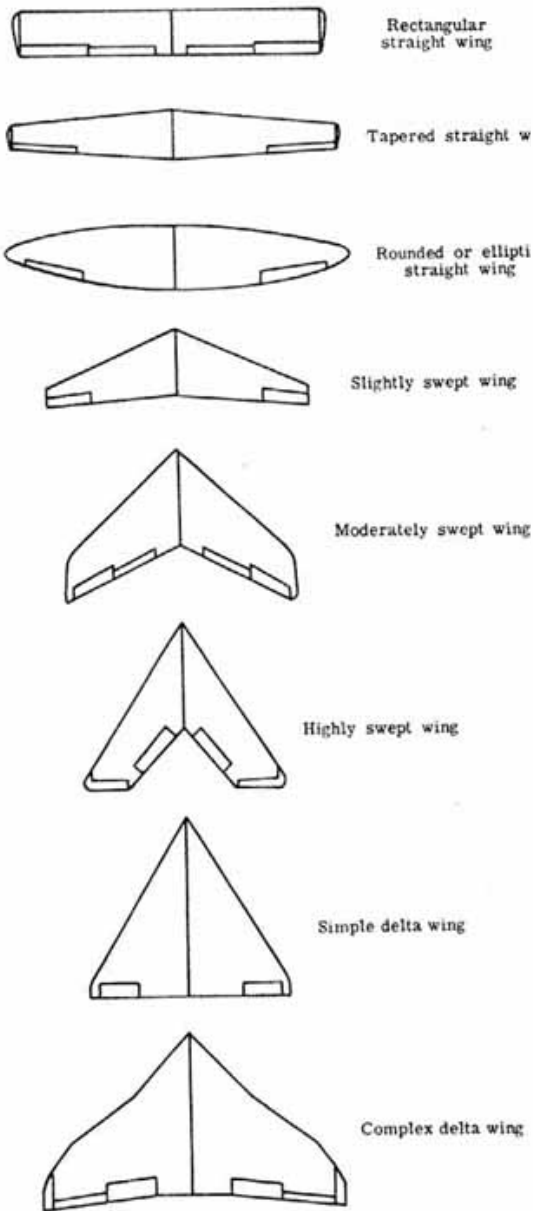
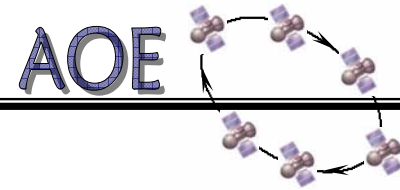


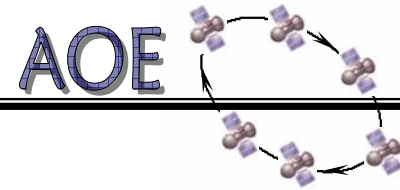
Front View



Side View

Some Wing Shapes

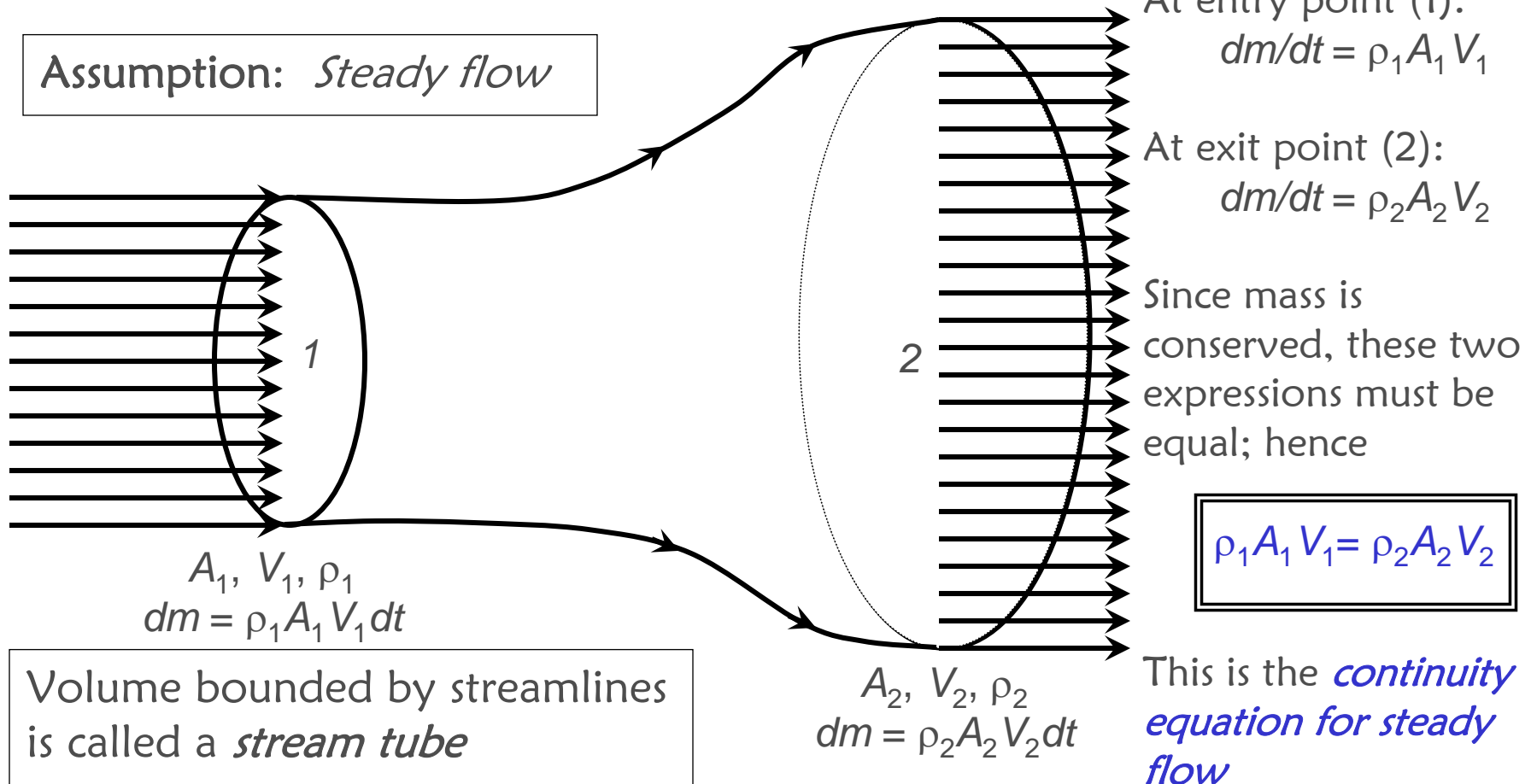




Continuity

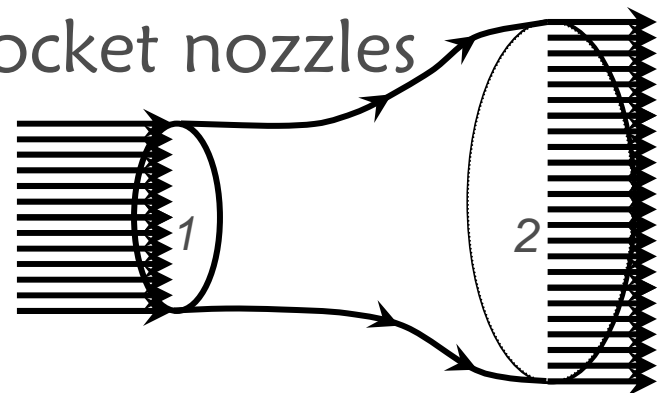
Physical principle: Mass can be neither created nor destroyed.

Assumption: *Steady flow*

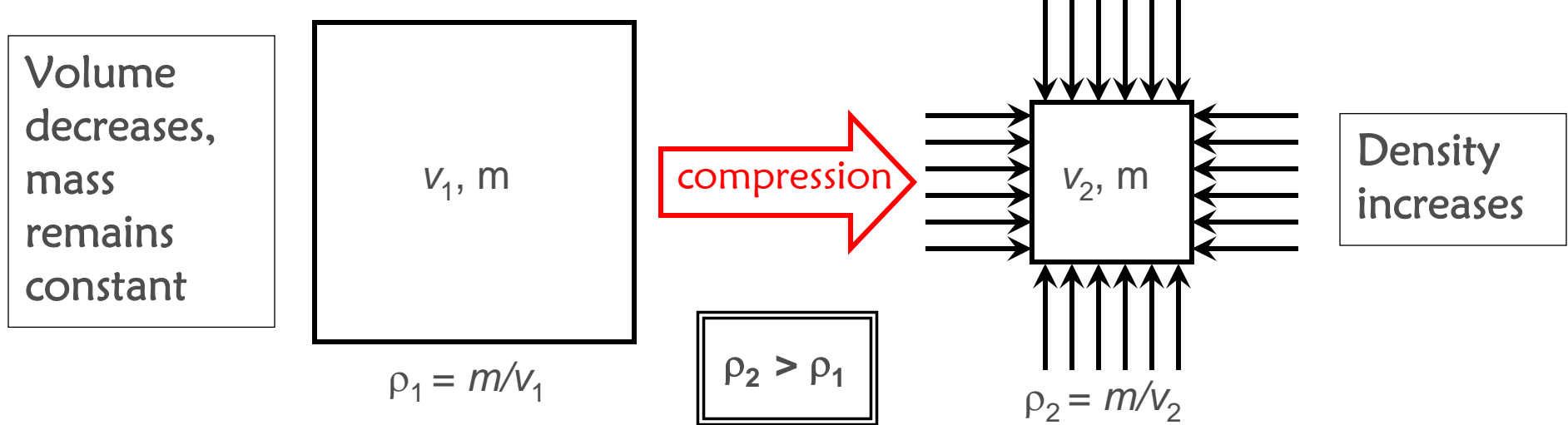


Remarks on Continuity

- In the stream tube figure, the velocities and densities at points 1 and 2 are assumed to be uniform across the cross-sectional areas
- In reality, V and ρ do vary across the area and the values represent mean values
- The continuity equation is used for flow calculations in many applications such as wind tunnels and rocket nozzles
- Stream tubes do not have to represent physical flow boundaries



Compressible vs Incompressible



- **Compressible flow:** flow in which the density of the fluid changes from point to point
 - In reality, all flows are compressible, but $\Delta\rho$ may be negligible
- **Incompressible flow:** flow in which the density of the fluid is constant
 - Continuity equation becomes $A_1 V_1 = A_2 V_2$

Compressible vs Incompressible

- Incompressible flow does not exist in reality
- However, many flows are “incompressible enough” so that the assumption is useful
- Incompressibility is an excellent model for
 - Flow of liquids such as water and oil
 - Low-speed aerodynamics (<100 m/s or <225 mph)
- For incompressible flow, the continuity equation can be written as $V_2 = A_1 V_1 / A_2$
- Thus if $A_1 > A_2$ then $V_1 < V_2$

Example 4.1

Consider a convergent duct with an inlet area $A_1 = 5 \text{ m}^2$. Air enters this duct with velocity $V_1 = 10 \text{ m/s}$ and leaves the duct exit with a velocity $V_2 = 30 \text{ m/s}$. What is the area of the duct exit?

First, check that the velocities involved are $< 100 \text{ m/s}$, which implies *incompressible flow*.

Then use

$$A_2 = A_1 V_1 / V_2 = (5 \text{ m}^2)(10)/(30) = 1.67 \text{ m}^2$$

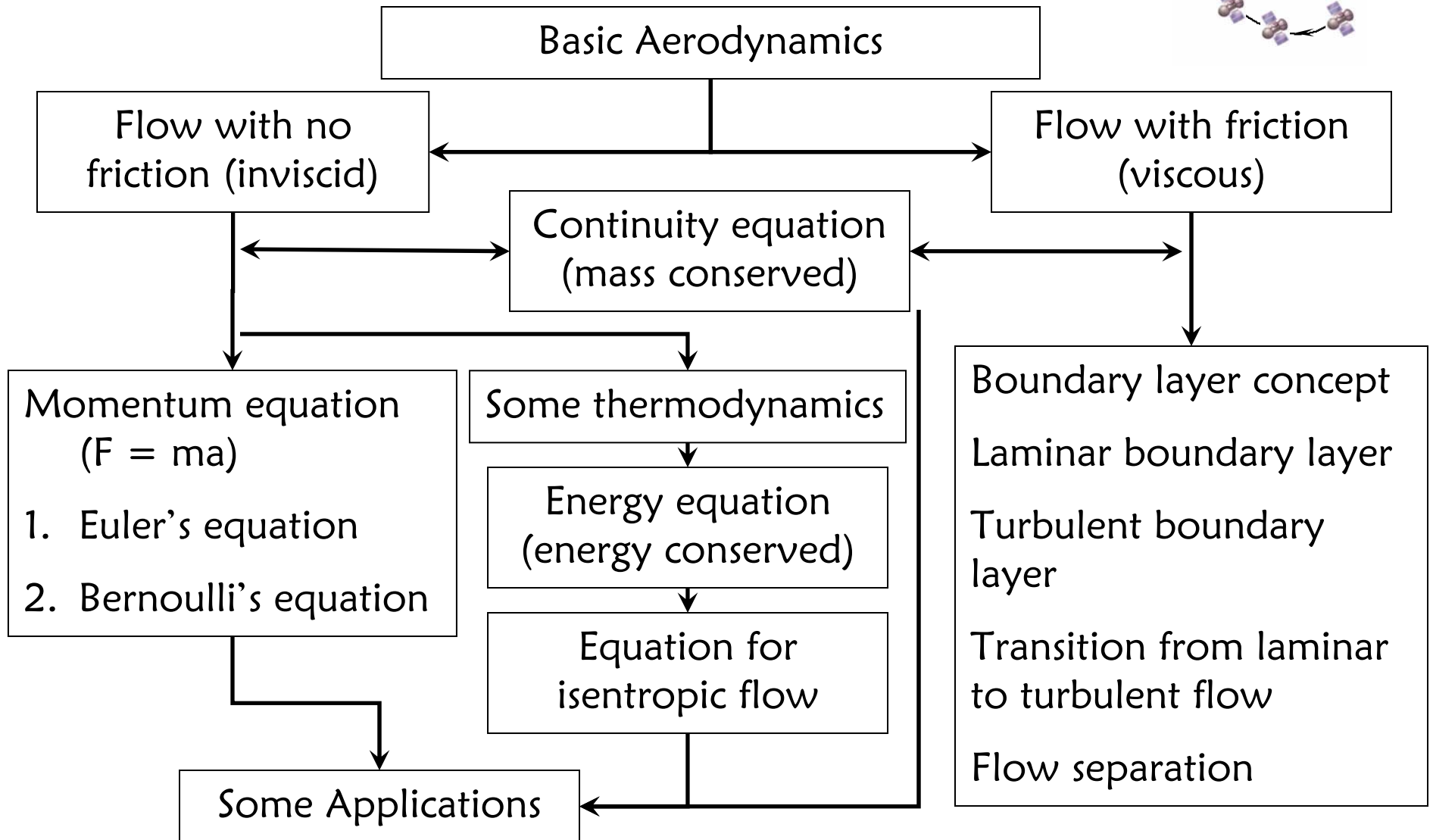
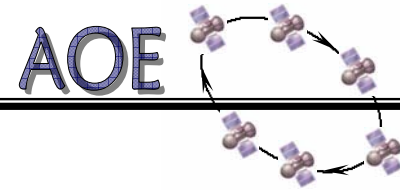
Example 4.2

Consider a convergent duct with an inlet area $A_1 = 3 \text{ ft}^2$ and an exit area $A_2 = 2.57 \text{ ft}^2$. Air enters this duct with velocity $V_1 = 700 \text{ ft/s}$ and a density $\rho_1 = 0.002 \text{ slug/ft}^3$, and leaves the duct exit with a velocity $V_2 = 1070 \text{ ft/s}$. What is the density of the air at the duct exit?

First, check that the velocities involved are $> 300 \text{ ft/s}$, which implies *compressible flow*.

Then use

$$\rho_2 = \rho_1 A_1 V_1 / (A_2 V_2) = 0.00153 \text{ slug/ft}^3$$



Reading: Chapter 4

Momentum Equation

- Continuity equation does not involve pressure
- Pressure \Rightarrow Force \Rightarrow Change in momentum
 \Rightarrow Change in velocity

Force = $d(\text{momentum})/dt$ What Newton said

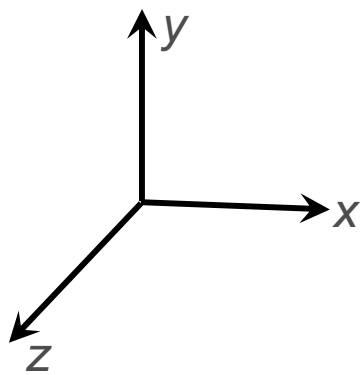
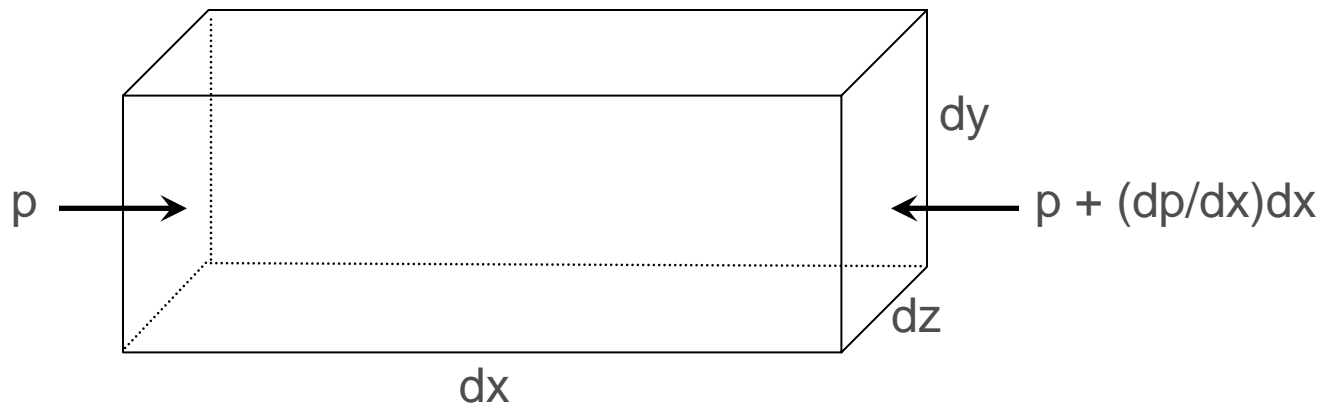
Force = $d(mv)/dt$ but only applies if $m=\text{const}$

$$F = m \, dv/dt$$

$$F = ma$$

- We apply $F = ma$ to the fluid by summing the forces acting on a single infinitesimally small particle of fluid

Free-Body Diagram



- Assume element is moving in x direction
- Force on element has three sources:
 - Normal pressure distribution: p
 - Shear stress distribution: τ_w
 - Gravity: $\rho dx dy dz g$
- Ignore gravity, smaller than other forces
- Consider force balance in x direction
- Force = Pressure \times Area

Force Balance

- Force on left face: $F_L = p \, dy \, dz$
- Force on right face: $F_R = (p + [dp/dx]dx) \, dy \, dz$
 $F = F_L - F_R = p \, dy \, dz - (p + [dp/dx]dx) \, dy \, dz$
 $F = -(dp/dx) \, dx \, dy \, dz$
- Mass of the fluid element is
 $m = \rho \, dx \, dy \, dz$
- Acceleration of the fluid element
 $a = dV/dt = (dV/dx)(dx/dt) = (dV/dx)V$
- Newton's second law
 $F = ma \Rightarrow \boxed{dp = -\rho \, V \, dV}$ Euler's Equation
- Also referred to as the Momentum Equation
 - Keep in mind that we assumed steady flow and ignored gravity and friction, thus this is the momentum equation for *steady, inviscid flow*
 - However, Euler's equation applies to compressible and incompressible flows

Incompressible Flow

- If the flow is incompressible, then ρ is constant

- The momentum equation can be written as

$$dp + \rho V dV = 0$$

- Integrating along a streamline between two points 1 and 2 gives

$$p_2 - p_1 + \rho (V_2^2 - V_1^2)/2 = 0$$

- Which can be rewritten as

$$p_2 + \rho V_2^2/2 = p_1 + \rho V_1^2/2$$

Or

$$p + \rho V^2/2 = \text{constant along a streamline}$$

- This equation is known as Bernoulli's equation

Euler's and Bernoulli's Equations

- Bernoulli's equation

$$p_2 + \rho V_2^2/2 = p_1 + \rho V_1^2/2$$

- Holds for inviscid, incompressible flow
- Relates properties of different points along a streamline

- Euler's equation

$$dp = -\rho V dV$$

- Holds for inviscid flow, compressible or incompressible

- These equations represent Newton's Second Law applied to fluid flow, and relate pressure, density, and velocity

Euler's and Bernoulli's Equations

- Bernoulli's equation

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- Holds for inviscid flow, compressible or incompressible

- These equations represent Newton's Second Law applied to fluid flow, and relate pressure, density, and velocity

Example 4.3

Consider an airfoil in a flow of air, where far ahead (upstream) of the airfoil, the pressure, velocity, and density are 2116 lb/ft², 100 mi/h, and 0.002377 slug/ft³, respectively. At a given point A on the airfoil, the pressure is 2070 lb/ft². What is the velocity at point A?

First, we must use consistent units. Using the fact that 60 mi/h \approx 88 ft/s, we find that $V = 100 \text{ mi/h} = 146.7 \text{ ft/s}$. This flow is slow enough that we can assume it is incompressible, so we can use Bernoulli's equation:

$$p_1 + \rho V_1^2/2 = p_A + \rho V_A^2/2$$

Where “1” is the far upstream condition, and “A” is the point on the airfoil. Solving for velocity at A gives

$$V_A = 245.4 \text{ ft/s}$$

Example 4.4

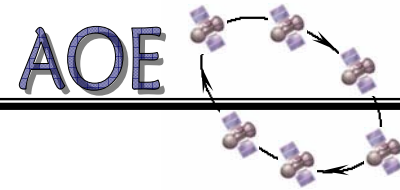
Consider a convergent duct with an inlet area $A_1 = 5 \text{ m}^2$. Air enters this duct with velocity $V_1 = 10 \text{ m/s}$ and leaves the duct exit with a velocity $V_2 = 30 \text{ m/s}$. If the air pressure and temperature at the inlet are $p_1 = 1.2 \times 10^5 \text{ N/m}^2$ and $T_1 = 330\text{K}$, respectively, calculate the pressure at the exit.

First, compute density at inlet using equation of state:

$$\rho_1 = p_1 / (R T_1) = 1.27 \text{ kg/m}^3$$

Assuming compressible flow, use Bernoulli's equation to solve for p_2 :

$$p_2 = p_1 + \rho(V_1^2 - V_2^2)/2 = 1.195 \times 10^5 \text{ N/m}^2$$

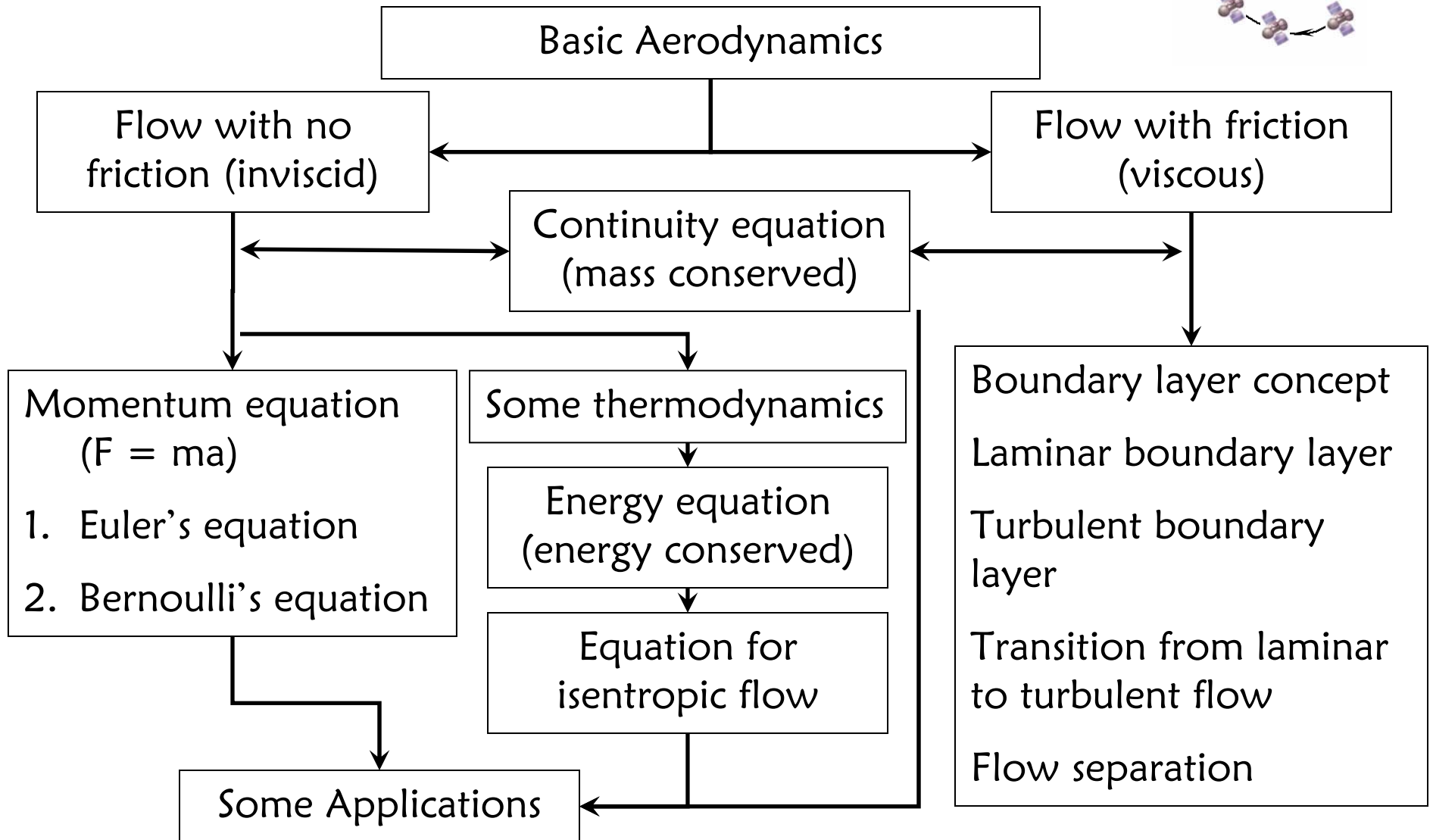
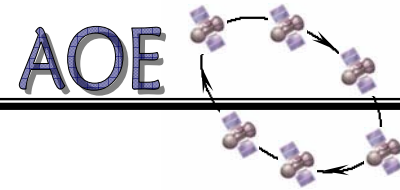


Example 4.5

Consider a long dowel with semicircular cross section

...

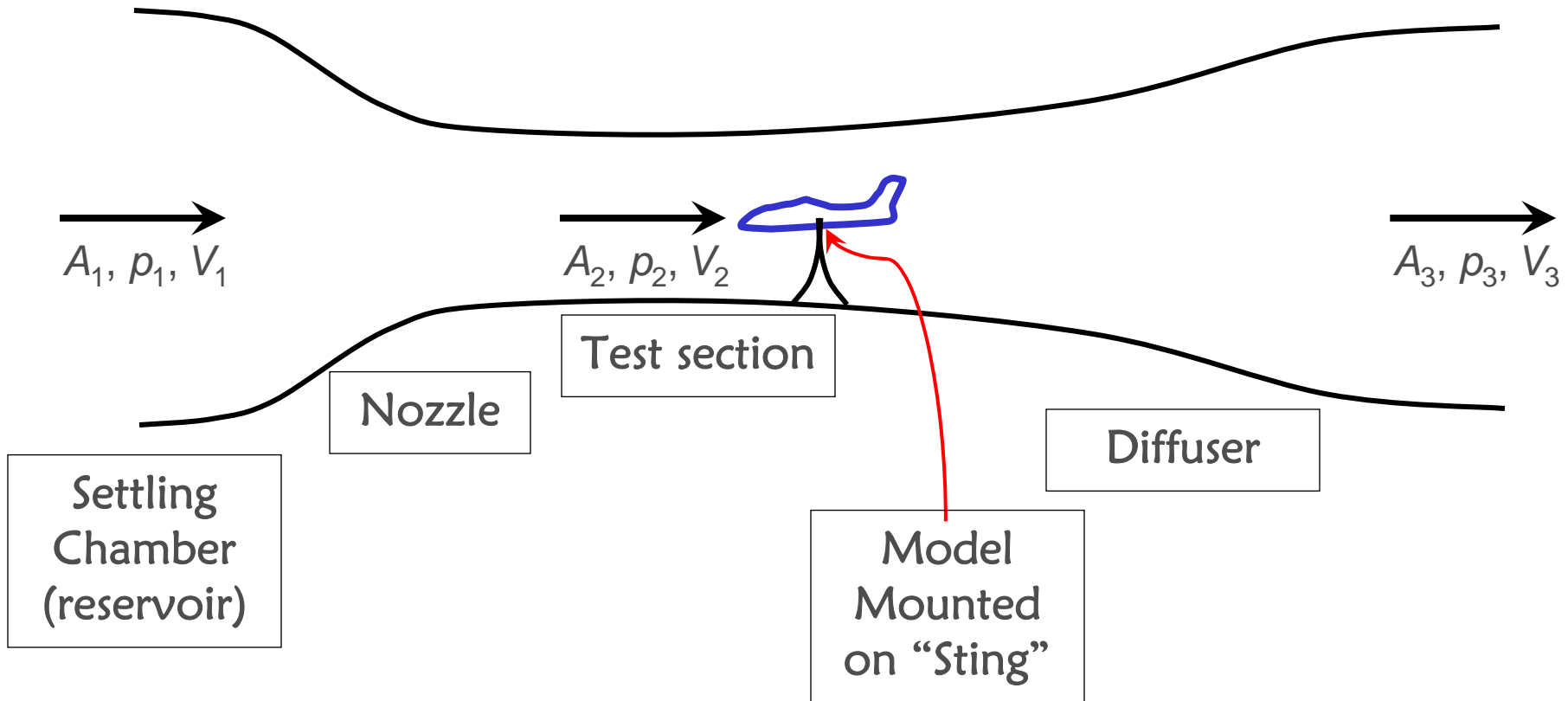
See pages 135-141 in text



Reading: Chapter 4

§4.10: Low-Speed Subsonic Wind Tunnels

Assumption: *Steady incompressible flow*



Continuity and Bernoulli's Equation apply

Wind Tunnel Calculations

$$\text{Continuity} \Rightarrow V_1 = (A_2/A_1)V_2$$

$$\text{Bernoulli} \Rightarrow V_2^2 = 2(p_1 - p_2)/\rho + V_1^2$$

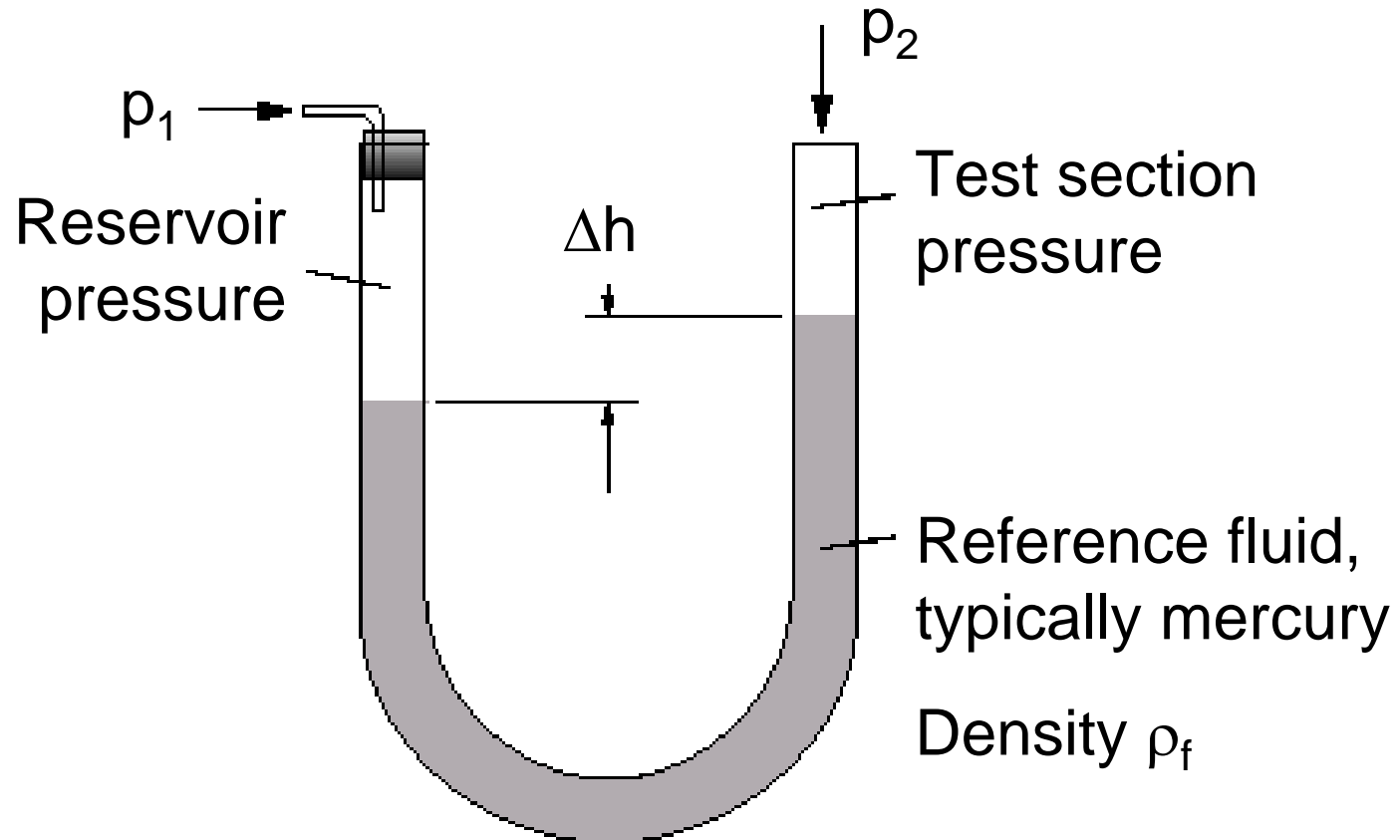
Combine to get

$$V_2 = \{ 2(p_1 - p_2) / [\rho(1 - (A_2/A_1)^2)] \}^{1/2}$$

The ratio A_2/A_1 is fixed for a given wind tunnel, and the density ρ is constant for low-speed tunnels, so the “control” is $p_1 - p_2$

How to determine $p_1 - p_2$?

Manometer



$$p_1 A = p_2 A + w A \Delta h, \quad w = \rho_f g$$

$$p_1 - p_2 = w \Delta h, \quad \text{So} \quad \Delta h \Rightarrow V_2$$

Example 4.13

In a low-speed subsonic wind tunnel, one side of a mercury manometer is connected to the reservoir and the other side is connected to the test section. The contraction ratio of the nozzle $A_2/A_1 = 1/15$. The reservoir pressure and temperature are $p_1 = 1.1 \text{ atm}$ and $T_1 = 300 \text{ K}$. When the tunnel is running the height difference between the two columns of mercury is 10 cm . The density of liquid mercury is $1.36 \times 10^4 \text{ kg/m}^3$. Calculate the airflow velocity V_2 in the test section.

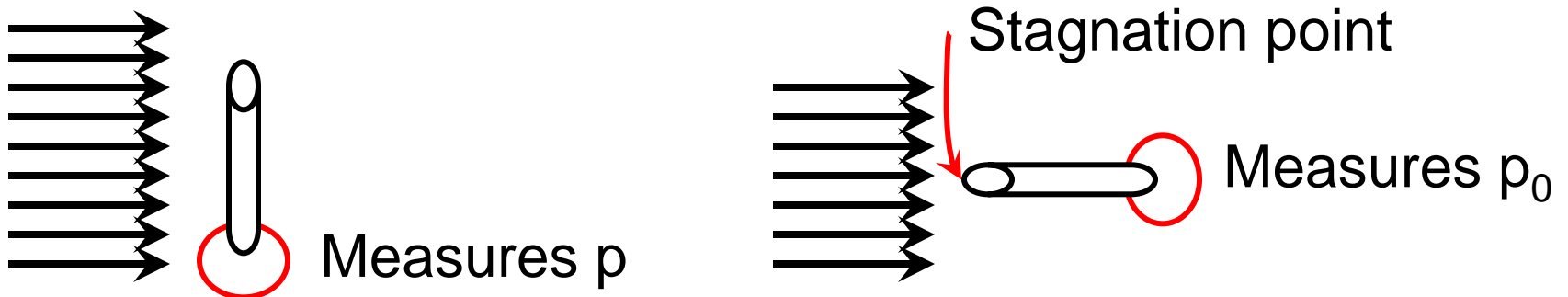
§4.11: Measurement of Airspeed

- **Total pressure** *vs* **static pressure**
- Static pressure is the pressure we've been using all along, and is the pressure you'd feel if you were moving along with the fluid
- Total pressure includes the static pressure, but also includes the “pressure” due to the fluid's velocity, the so-called **dynamic pressure**
- Imagine a hollow tube with an opening at one end and a **pressure sensor** at the other, and imagine inserting it into a flow in two different ways



Pitot Tube

- This device is called a Pitot Tube (after Henri Pitot, who invented it in 1732; see §4. 23)
- The orientation on the left measures the static pressure (the pressure in all our calculations so far)
- The orientation on the right measures the total pressure, or the pressure if the flow is reduced to zero velocity



Pitot Tube for Incompressible Flow

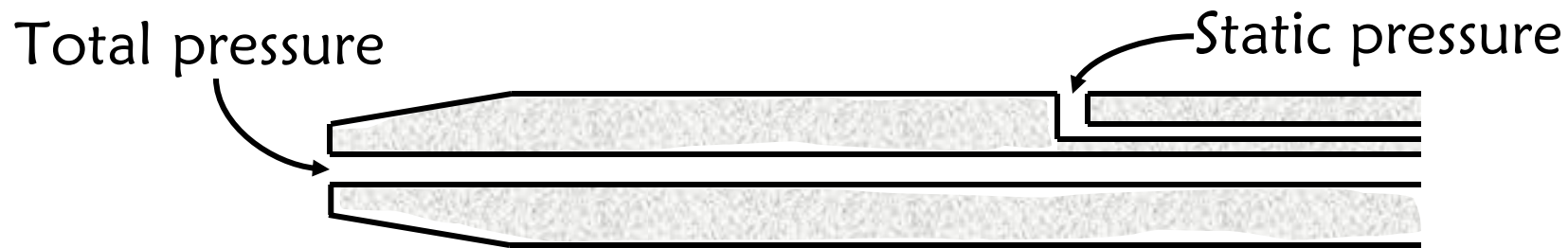
- The two tube orientations are used together
- One measures static pressure p , and the other measures total pressure p_0
- Since the total pressure is measured by removing all the velocity, and we're assuming incompressible flow, we can apply Bernoulli's equation to see that

$$p + \rho V^2/2 = p_0$$

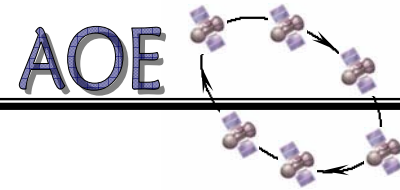
Static pressure + Dynamic Pressure = Total Pressure

- Dynamic pressure, the $\rho V^2/2$ term, is frequently denoted by $q = \rho V^2/2$

Using the Pitot-static Probe



- The two pressures are measured by a pressure transducer
- Bernoulli's equation (incompressible flow only!) can be written as
$$p_0 = p + q \quad (q = \rho V^2/2)$$
- Solve for velocity
$$V = [2(p_0 - p)/\rho]^{1/2}$$
- A Pitot-static tube provides an airspeed measurement



Example 4.16

The altimeter on a low-speed Cessna 150 reads 5000 ft. The outside temperature is $T = 505^{\circ}\text{R}$. If a Pitot tube on the wingtip measures $p = 1818$ lb/ft², what is the true velocity of the airplane? What is the equivalent airspeed?

Overview of the “Rest” of Aerodynamics

- We will not cover the remainder of Ch. 4, but here are some highlights
- First Law of Thermodynamics leads to relationships between **energy**, **temperature**, **heat**, **enthalpy**, and **specific heat**
- Energy has units of Joules
- Enthalpy has units of Joules but also accounts for temperature
- **Adiabatic** \Rightarrow no heat is added or removed
- **Reversible** \Rightarrow no frictional losses
- **Isentropic** \Rightarrow adiabatic and reversible