

BASIC THEORY OF THE MOLLIER'S CHART

1. What is Mollier's chart?

- the tool for determining of isobaric psychrometric processes of moist air
- suitable for steady conditions
- similar to psychrometric chart used mainly in Anglo-Saxon literature
- each chart is determined for specific pressure

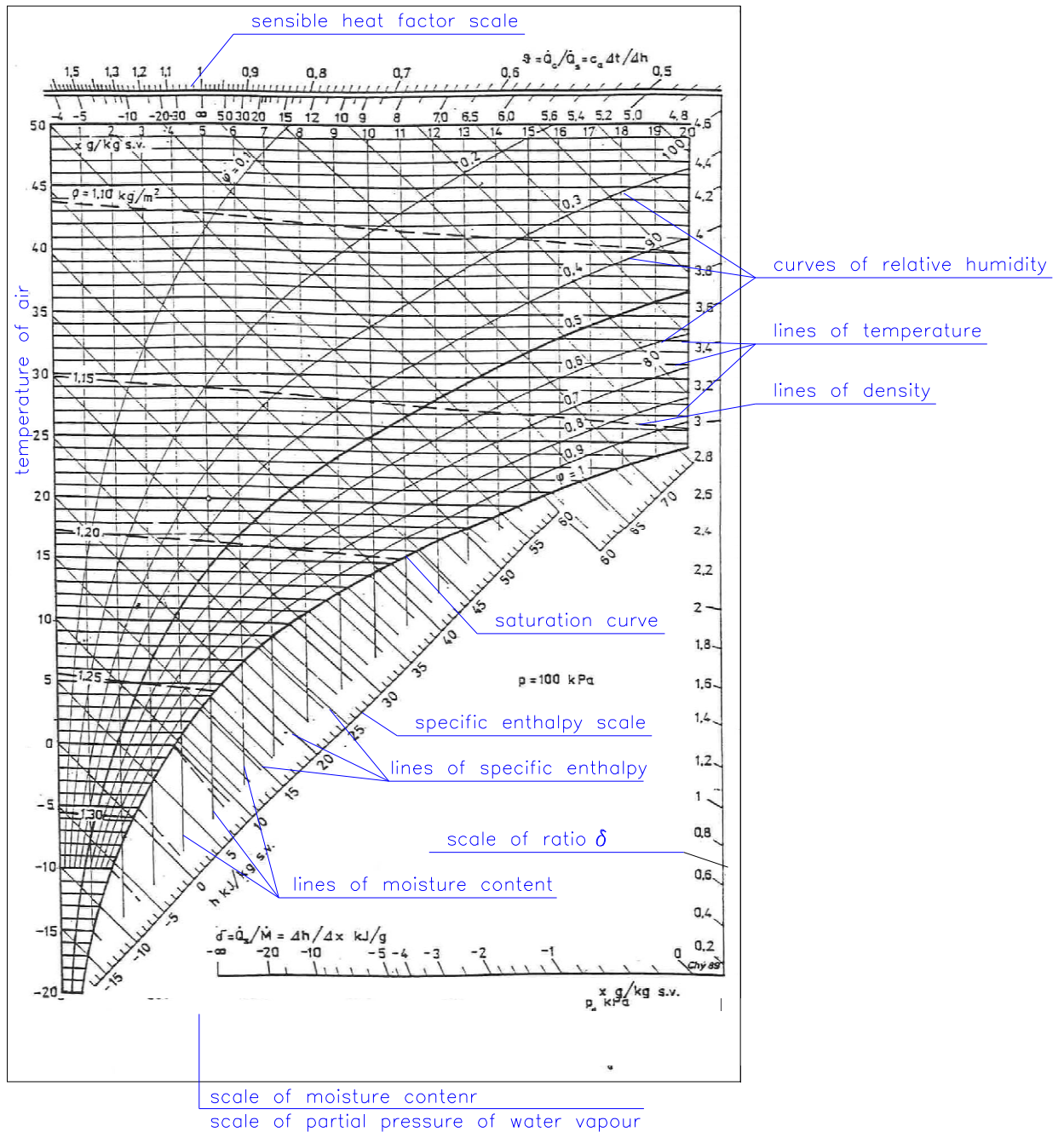


Figure 1- Description of Mollier's chart

Determination of the dew point temperature and the wet-bulb temperature

- **dew point temperature t_d :**

The temperature of moist air saturated at the same pressure p and with the same moisture content x as the given state of moist air.

- **thermodynamic wet-bulb temperature t_w :**

The temperature at which water evaporating into moist air, can bring air to the adiabatic saturation. The lowest temperature of adiabatic cooling of air.

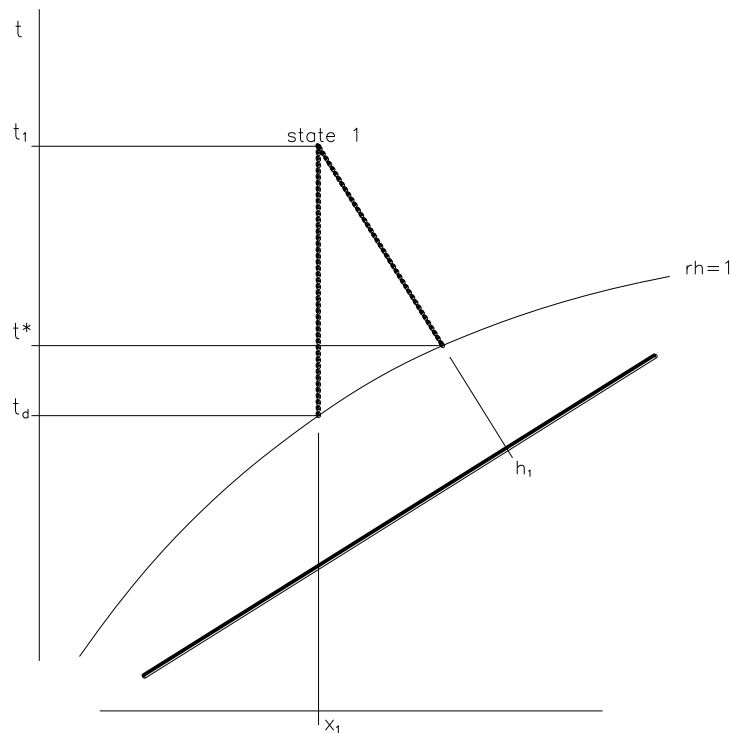


Figure 2 - Determination of the dew point temperature and the wet-bulb temperature

Training example for diagram use

<p>Air state: dry-bulb temperature $t = 15^\circ\text{C}$ moisture content $x = 7,8 \text{ g/kg d.a.}$ barometric pressure $p = 100 \text{ kPa}$</p>	<p>Find other moist air properties: specific enthalpy, relative humidity, dew point temperature, wet-bulb temperature</p>
<p>Results: specific enthalpy $h = 35 \text{ kJ/kg}$, relative humidity $rh = 73 \%$, dew point temperature $t_d = 10^\circ\text{C}$, wet-bulb temperature $t_w = 12,5^\circ\text{C}$</p>	

<p>Air state: specific enthalpy $h = 55 \text{ kJ/kg}$ relative humidity $rh = 45 \%$ barometric pressure $p = 100 \text{ kPa}$</p>	<p>Find other moist air properties: dry-bulb temperature, moisture content, dew point temperature, wet-bulb temperature</p>
<p>Results: dry-bulb temperature $t_d = 28^\circ\text{C}$, moisture content $x = 10,6 \text{ g/kg d.a.}$, dew point temperature $t_d = 15^\circ\text{C}$, wet-bulb temperature $t_w = 19^\circ\text{C}$</p>	

2. Basic psychrometric processes

3.1 Introduction

- any process has two heat components

- sensible heat S – moisture is constant
- latent heat L – temperature is constant

1 – 2 is any process in Mollier's chart

total heat $Q = L + S$

where:

- latent heat component
 $L = m_a \cdot (h_2 - h_1)$
- sensible heat component
 $S = m_a \cdot (h_{1'} - h_1)$

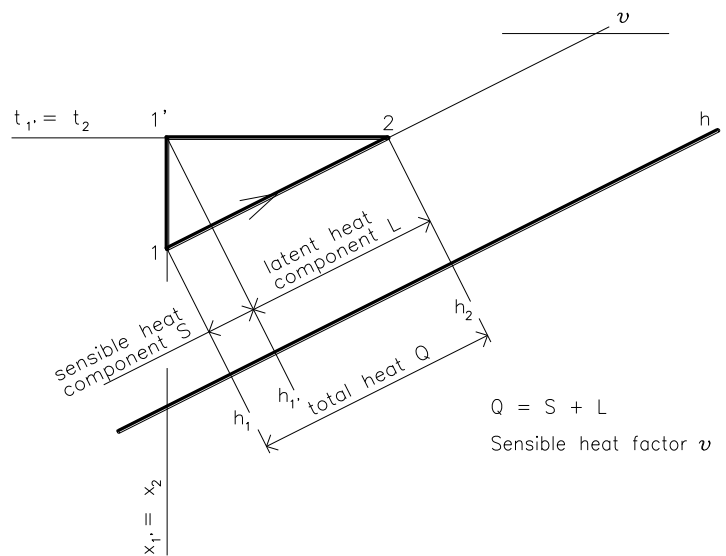


Figure 3 - Components of any process

sensible heat factor u :

- ratio of sensible heat component included in total heat

$$g = \frac{S}{Q} = \frac{c \cdot \Delta t}{\Delta h}$$

2.2. Sensible heating and cooling

- the process with no changes of moisture content x

- the sensible cooling and the sensible heating are reversed processes

- in the case of sensible cooling the surface temperature of cooler must be higher than the dew point temperature of moist air

Properties of states:

$x_1 = x_2$

- sensible cooling

$$\begin{aligned} t_2 < t_1 \\ rh_2 > rh_1 \\ h_2 < h_1 \end{aligned}$$

- heating

$$\begin{aligned} t_2 > t_1 \\ rh_2 < rh_1 \\ h_2 > h_1 \end{aligned}$$

The heat required for the process:

- sensible cooling

$$Q = m_a \cdot (h_1 - h_2) = m_a \cdot c_d \cdot (t_1 - t_2) \quad [\text{kW}]$$

- heating

$$Q = m_a \cdot (h_2 - h_1) = m_a \cdot c_d \cdot (t_2 - t_1) \quad [\text{kW}]$$

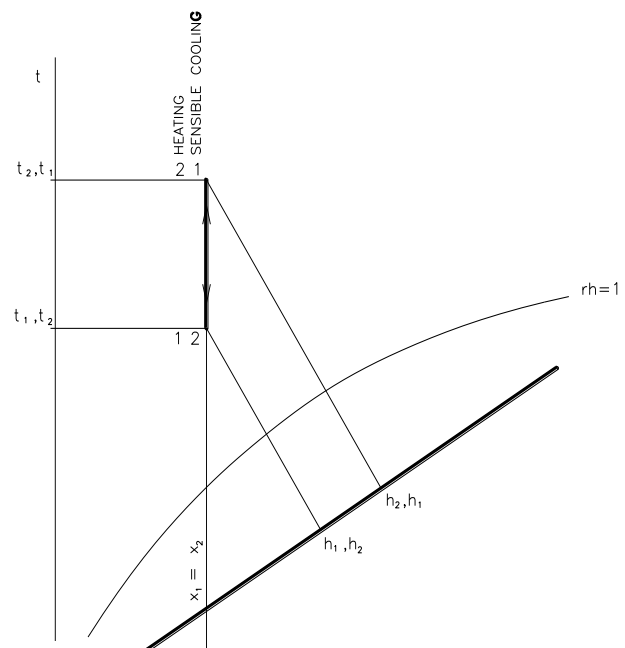


Figure 4- Sensible heating and cooling

2.3. Cooling

- the process with change of moisture content x
- the surface temperature of cooler is lower than the dew point temperature of moist air
→ the condensation occurs

Properties of states:

$$x_1 > x_2$$

$$t_2 < t_1$$

$$rh_2 > rh_1$$

$$h_2 < h_1$$

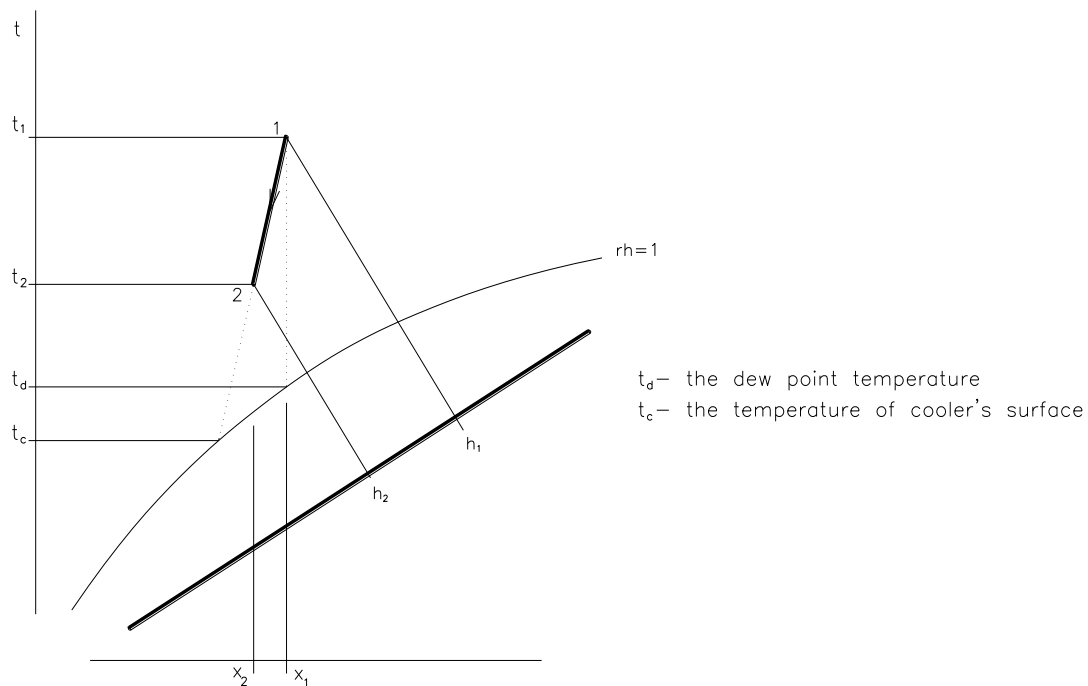


Figure 5 - Cooling process

The heat required for the process:

$$Q = m_a \cdot (h_1 - h_2) \text{ [kW]}$$

The rate of condensing moisture:

$$m_w = m_a \cdot (x_1 - x_2) \text{ [kg/s]}$$

2.4. The different between sensible cooling and cooling

- while the cooler's surface temperature is lower than the dew point temperature condensation of water vapour occurs.
→ a part of total heat is used for change from gaseous state to liquid state

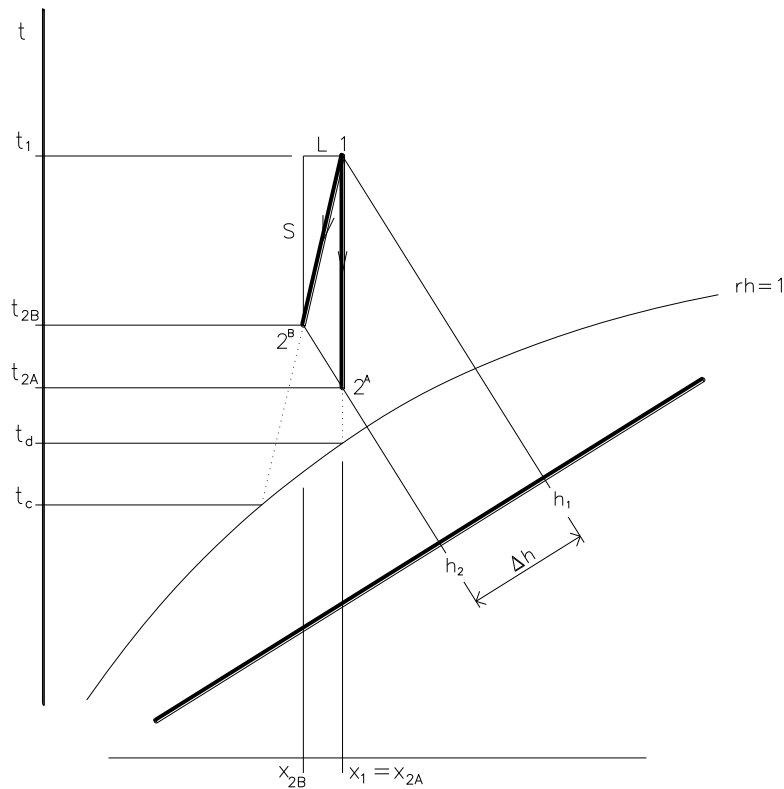


Figure 6 - The different between sensible cooling and cooling

$$Q = m \cdot \Delta h; \Delta h = h_1 - h_2$$

A) $Q = S + L; L = 0$

B) $Q = S + L; L \neq 0 \Rightarrow S_B < S_A \rightarrow t_{2B} > t_{2A}$

2.5. Humidification

- the moisture content can be increased in two ways

- the direct injection of steam into the air stream
- passing the air through a spray chamber containing small water droplets

2.5.1. Steam injection

Definition

the mass balance: $m_{a1} = m_{a2} = m_a$

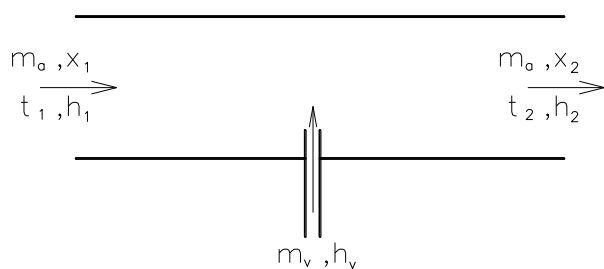
steady-flow energy equations:

$$m_a \cdot x_1 + m_v = m_a \cdot x_2$$

$$m_a \cdot h_1 + m_v \cdot h_v = m_a \cdot h_2$$

$$\Rightarrow m_v \cdot h_v = m_a \cdot (h_2 - h_1)$$

$$m_v = m_a \cdot (x_2 - x_1)$$



$$\rightarrow \frac{h_2 - h_1}{x_2 - x_1} = h_v = q_{12} \rightarrow \text{specific heat of the proces}$$

Properties of states:

$$x_1 < x_2$$

$$t_2 = t_1$$

$$rh_2 > rh_1$$

$$h_2 > h_1$$

Mollier's chart:

ratio d

$$\delta = \frac{\Delta h}{\Delta x} = h_v$$

where:

h_v – specific enthalpy of injected steam (or any liquid)

h_v varies about 2,6 kJ/kg

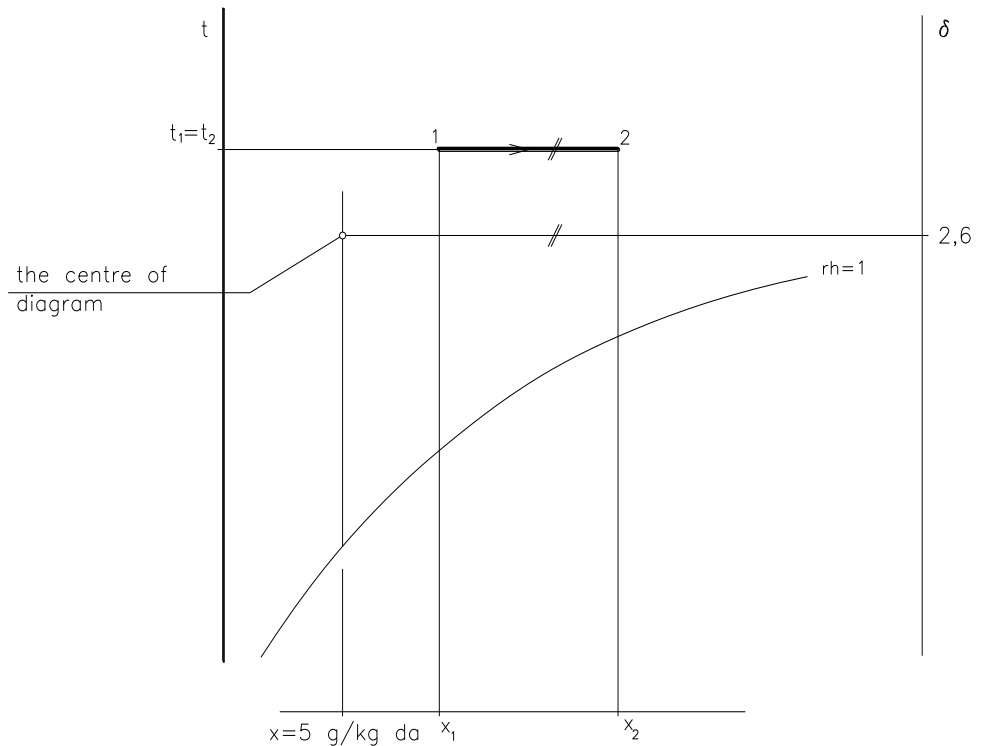
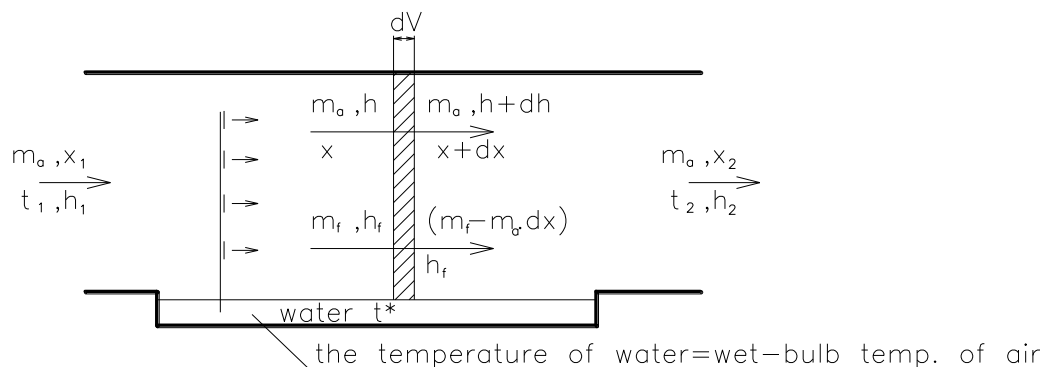


Figure 7 - Steam humidification

The process of steam injection in the air stream is taken with reasonable accuracy as isothermal.

2.5.2. b) Humidification in spray chamber

Definition



Energy balance:

$$m_a \cdot dh = m_a \cdot dx \cdot h_f$$

$$m_a \cdot dh = m_a \cdot dx \cdot h_f \rightarrow \frac{dh}{dx} = h_f; \text{the same equation as in the steam injection humidification}$$

h_f of water at temperature 10 to 15 °C varies between 0 to 0,42 kJ/kg

Properties of states:

- $x_1 < x_2$
- $t_2 < t_1$
- $rh_2 > rh_1$
- $h_2 = h_1$

Equations:

$$m_w = m_a \cdot (x_2 - x_1) \text{ [kg/s]}$$

m_w - the rate of water transported into the air stream

Humidification with water in spray chamber is taken with reasonable precision as adiabatic \Rightarrow specific enthalpy is constant

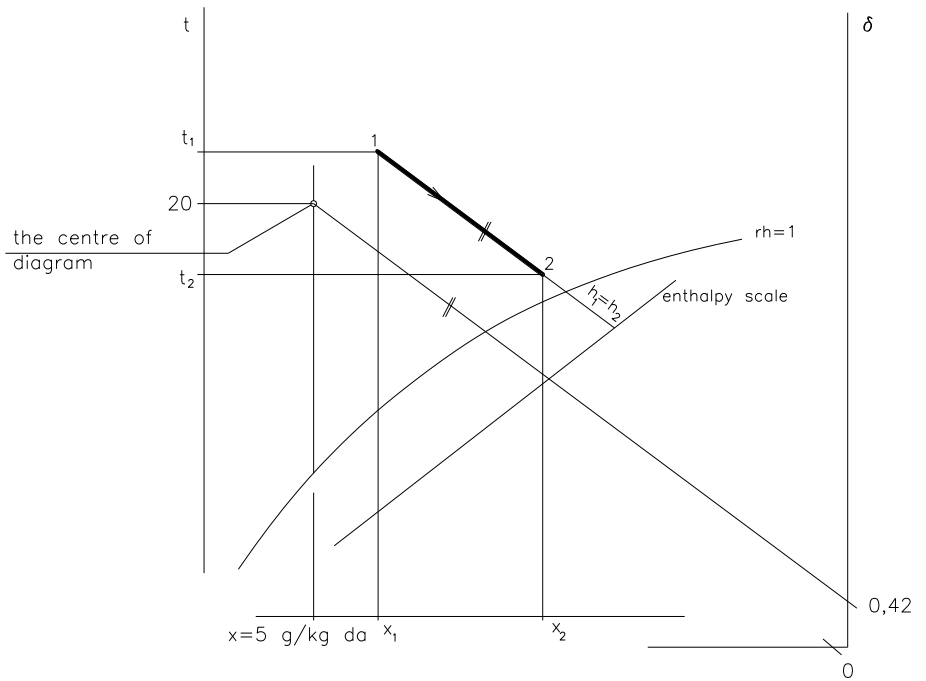


Figure 8 - Humidification with water in spray chamber

2.6. Mixing

Definition

- mix of two air streams

steady-flow energy equation:

$$m_{a1} \cdot h_1 + m_{a2} \cdot h_2 = m_{a3} \cdot h_3$$

mass balance equation:

$$m_{a1} + m_{a2} = m_{a3} \text{ for dry air}$$

$$m_{a1} \cdot x_1 + m_{a2} \cdot x_2 = m_{a3} \cdot x_3 \text{ for water vapour}$$

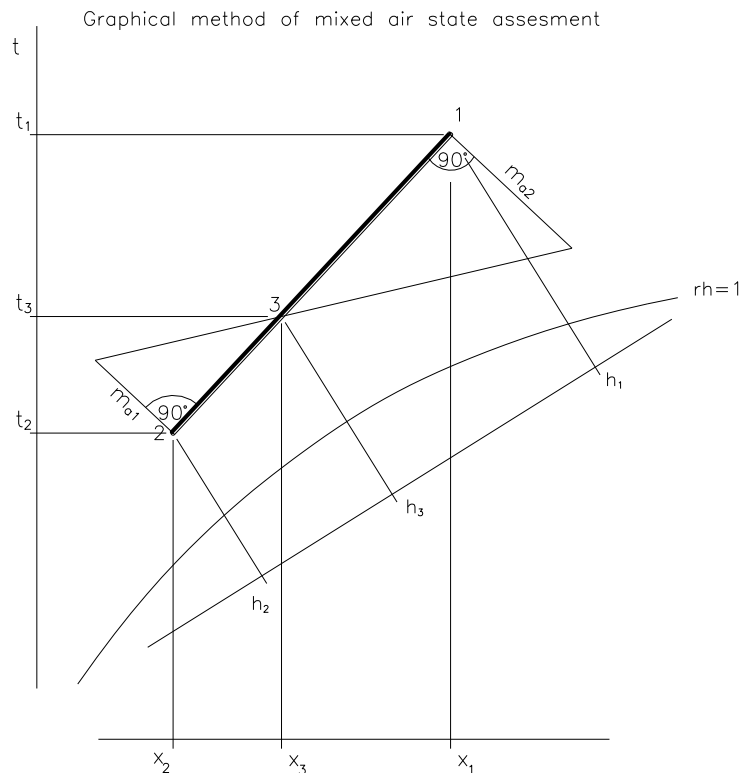


Figure 9- Mixing

from the equations ensues:

$$\frac{m_{a1}}{m_{a2}} = \frac{h_3 - h_2}{h_1 - h_3} = \frac{x_3 - x_2}{x_1 - x_3} \Rightarrow \frac{h_3 - h_2}{x_3 - x_2} = \frac{h_1 - h_3}{x_1 - x_3} = \delta_{13} = \delta_{23}$$

In the case of result state is below saturation curve:

state 3 is oversaturated air \Rightarrow air immediately changes to the saturated air according to the line of constant temperature, Dx is amount of condensed water steam.

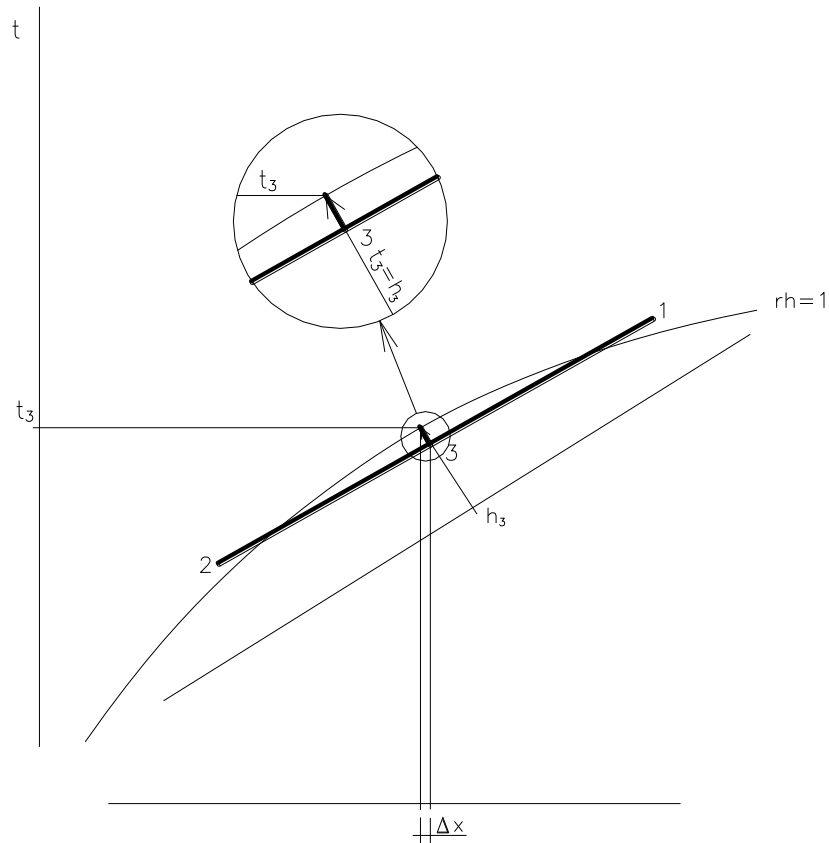


Figure 10 - State is below saturation curve