

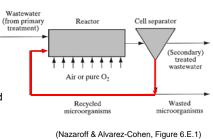
Secondary Treatment: Activated Sludge (Nazaroff & Alvarez-Cohen, Section 6.E.1)

An activated-sludge reactor is a system in which pre-treated sewage (*i.e.* having passed through primary treatment) is aerated to promote the growth of bacteria (cells) that gradually consume the organics in the sewage.

The result is the development of cells acclimated to the particular mix of substances present in the sewage and a significant consumption of the organic material. The effluent is a mixture of water with suspended cells and drastically reduced BOD content.

This mixture is then passed through a clarifier (settling tank) where the solids (mostly cells, called sludge at this stage) are separated from the water. The system is commonly operated in continuous mode (as opposed to batch mode).

The system is properly speaking an *activated-sludge* system when a portion of the sludge (cells) collected from the bottom of the clarifier is returned to the aerator. Not only are these cells already acclimated to the sewage, but by the time they are collected from the clarifier, they are also starved and really "hungry" for another meal!



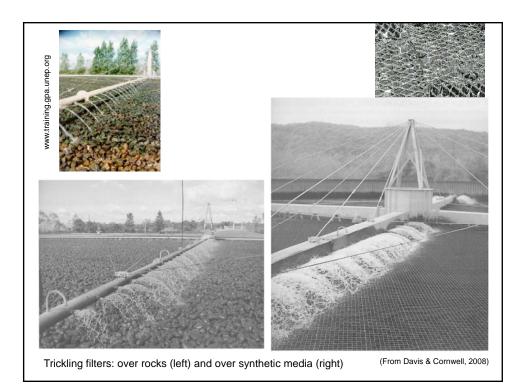
Alternative 1: Trickling Filter

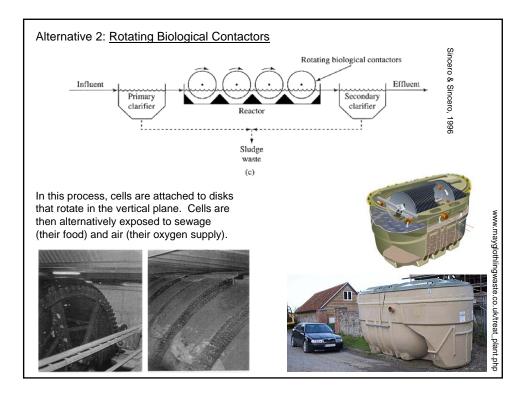
A trickling filter consists of a substrate (rocks or other material) on which cells can grow and over which the pre-treated sewage is sprayed. The spraying action creates contact between BOD in sewage, oxygen in the air and cells on the substrate. Cells grow and degrade the sewage. Excess cells (slime) need to be periodically removed from the substrate.

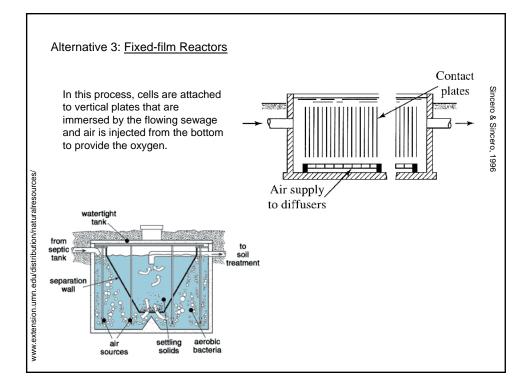


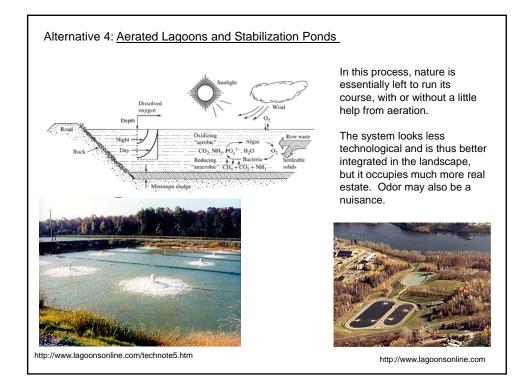


A trickling filter in action at the wastewater treatment plant in Portland, Indiana.



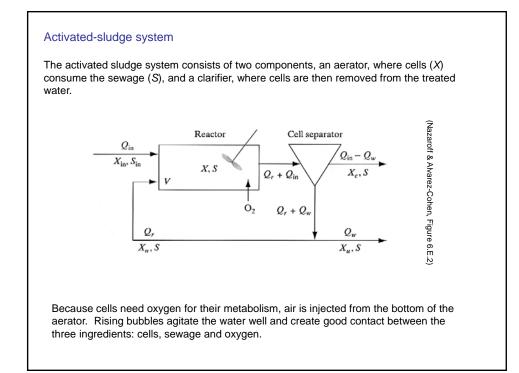




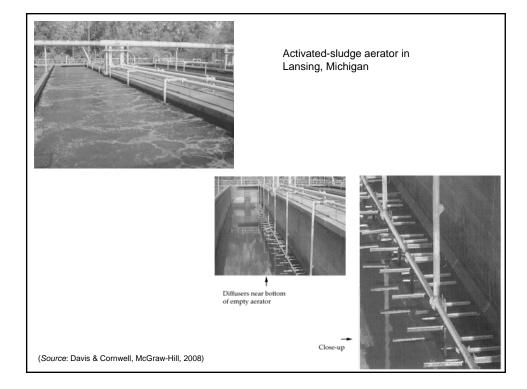


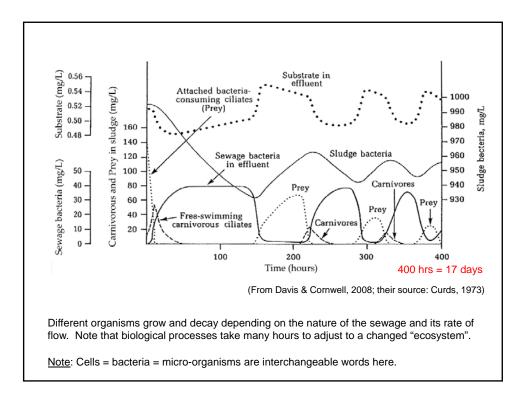


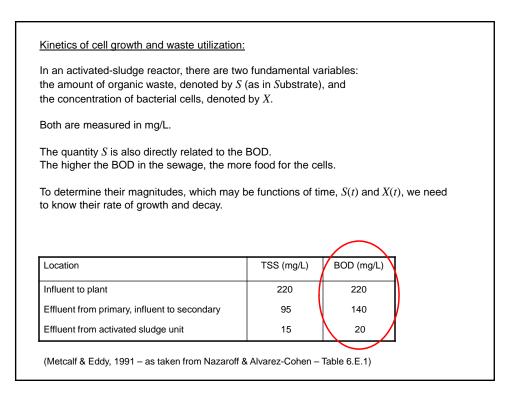
	Technology	Applications	Advantages	Disadvantages
Comparative summary of biological wastewater treatment technologies	Activated sludge	Low concentration organics Some inorganics	Removal of dissolved constituents Low maintenance Destruction process Relatively safe Low capital costs Relatively easy to operate	Volatile emissions Waste sludge disposal High energy costs Susceptible to shock and toxins Susceptible to seasonal changes
	Trickling filters, Fixed-film reactors	Low concentration organics Some inorganics	Removal of dissolved constituents Low maintenance Destruction process Relatively safe Reduced sludge generation	Volatile emissions Susceptible to shocks and toxins Susceptible to seasonal changes Relatively high capital costs Relatively high operating costs
	Aerated lagoons, Stabilization ponds	Low concentration organics Some inorganics	Removal of dissolved constituents Low maintenance Destruction process Relatively safe Low capital costs Low energy costs Easy to operate Infrequent waste sludge	Volatile emissions Susceptible to shocks and toxins Susceptible to seasonal changes High land requirement No operational control
	Anaerobic degradation (septic systems)	Low concentration organics Chlorinated organics Inorganics	Removal of dissolved constituents Destruction process Treatment of chlorinated wastes Methane generation (= fuel) Reduced sludge generation	Susceptible to shocks and toxins Susceptible to seasonal changes Relatively high capital costs Relatively high operating costs











Let us define:

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r_{S} = rate of substrate consumption = decay rate of waste
[in mg of substrate/(L.day)]
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 r_X = rate of cell formation = growth rate – decay rate [in mg of cells/(L.day)] = $r_g - r_d$

Empirical observation #1: The rate of cell growth r_g is proportional to the substrate consumption rate r_S , because the substrate is consumed by the cells to make more cells.

The coefficient of proportionality is defined as the yield and denoted by Y (no units).

Thus,

$$r_{\rho} = Y r_{S}$$

Typically, the value of Y is 0.6 or less because cells emit carbon dioxide and therefore put on as weight only a fraction of their food consumption.

Empirical observation #2:

The cell growth rate r_g is proportional to the cell concentration X, when all other variables are held unchanged, because the more cells there are, the more new cells can be manufactured.

Thus,

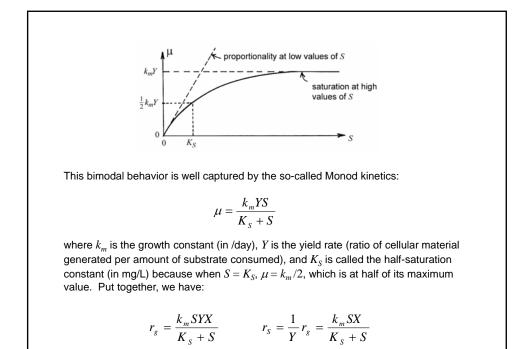
$$r_g = \mu X$$

where the coefficient μ depends on other variables, such as the amount of substrate present, *S*.

Empirical observation #3: (Mihelcic & Zimmerman, pages 171-174; Mines & Lackey, pages 67-69)

The coefficient μ of proportionality depends on the substrate concentration as follows: - At low *S* values, μ increases in proportion to increasing *S*, because the more food is available, the faster the cells multiply;

- At high S values, μ reaches a constant maximum value, because there is then a superabundance of food and cells cannot consume all of it right away.



Empirical observation #4:

The death rate r_d of cells is proportional to the cell concentration X, because cells die in proportion to their number.

Thus,

$$r_d = k_d X$$

Recycling

To promote growth of the cells already adapted to the nature of the sewage, some fraction of the sludge collected at the bottom of the clarifier is recycled into the aerator.

Let us denote by Q_r the volumetric flow rate of sludge added to the inflowing rate of sewage Q_{in} , and by X_u the cell concentration inside the sludge collected at the bottom of the clarifier.

It goes without saying that X_u is expected to be significantly larger than the concentration X of cells in the aerator.

Table 6.E.2	Parameter Values for Conventional Activated
Sludge Syste	ms Using a Completely Mixed Flow Reactor

Parameter	Typical range	Typical value
Microbial par	rameters	
$k_m (\text{mg BOD}_5 \text{ per mg VSS}^* \text{per day})$	2-10	5
$K_s (\text{mg BOD}_5 \text{ per L})$	25-100	60
Y (mg VSS*per mg BOD ₅)	0.4-0.8	0.6
$k_d (d^{-1})$	0.025-0.075	0.06
Operational pa	arameters	
Mean cell residence time, Θ_c (d)	5-15	
F/M (mg BOD ₅ per mg VSS [*] per day)	0.2-0.6	
Loading (kg BOD ₅ m ^{-3} d ^{-1})	0.8-1.9	
Total suspended solids (kg m ⁻³)	2.5-6.5	
Hydraulic detention time, Θ (h)	3–5	
Recycle ratio, $R = Q_r / Q_{in}$	0.25 - 1	
BOD removal efficiency (%)	85–95	
Source: Metcalf & Eddy, 1991.		
/olatile Suspended Solids = biomass conce	entration ^{(Nazaroff & A}	lvarez-Cohen, pag