

Berlin Hauptbahnhof

(Berlin Central Station)



Case Study
ARCH 631 - Fall 2017

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- Overview
- Background
- Building Specifics
- Building Components
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Overview

- Location: Berlin, Germany
- Project Duration: 1996 - 2006
- Gross Floor Area: 175,000 m² (1.9 million ft²)
- Site Area: 100,000 m² (1.1 million ft²)
- Client: Deutsche Bahn AG
- Project Cost: \$894 million



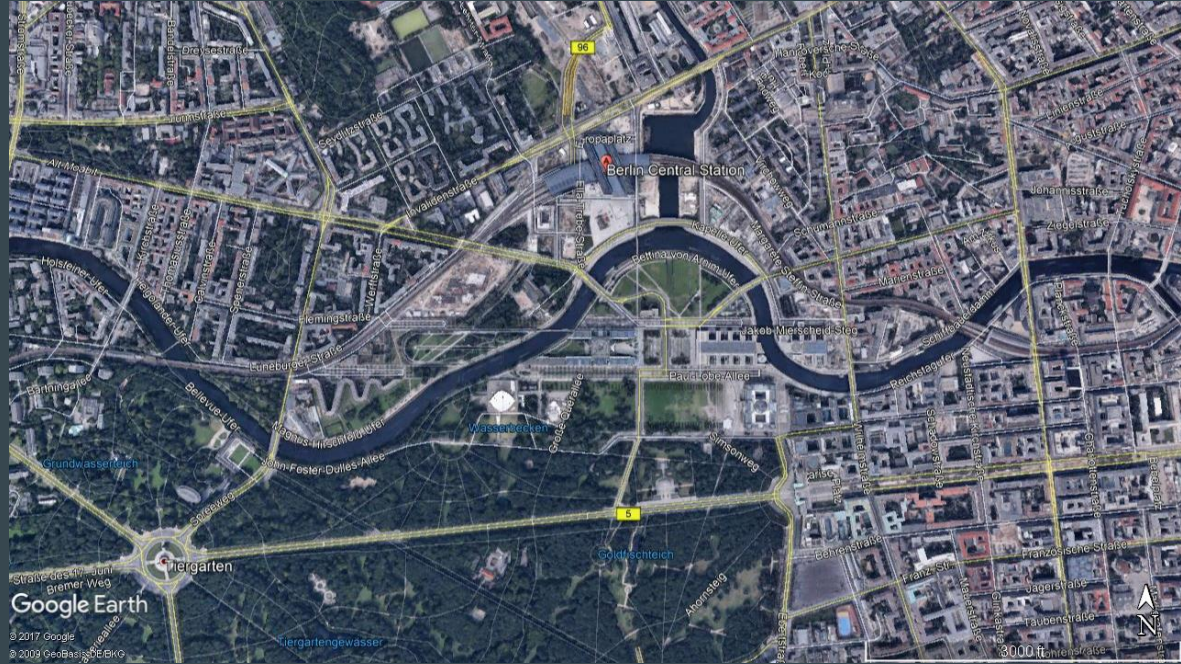
Background

- Architect: GMP Architects
- Design: Meinhard von Gerkan and Jurgen Hillmer
- Structural Engineer: Schlaich, Bergermann, and Partners
- Lighting Design: Peter Andres and Conceptlicht
- Mechanical: Ingenieurgesellschaft Hopfner



Background

- Europe's largest train station
- Located along the Spree River, north of the Tiergarten
- Located on the site of historic Lehrter Bahnhof
- Central node for tracks in all four cardinal directions
- Apart of a design competition in 1993



Building Specifics

- Area Breakdown
 - Shops and Gastronomy - 15,000 m² (162,000 ft²)
 - Office - 50,000 m² (540,000 ft²)
 - Railway Operations - 15,000 m² (162,000 ft²)
 - Circulation - 21,000 m² (230,000 ft²)
 - Platforms - 32,000 m² (350,000 ft²)
 - Parking - 25,000 m² (270,000 ft²)
- North-South tracks located 15m below ground level in tunnel
- East-West tracks located 10m above ground level
- Ground level accesses public, individual, and tourist transportation

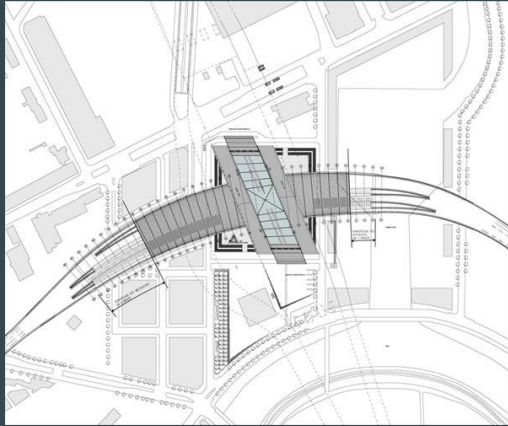


Building Specifics

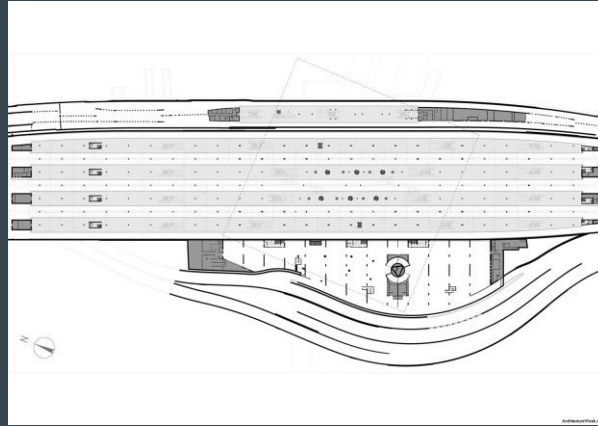
- Cruciform shape created by crossing of north-south and east-west tracks
- East-West tracks covered by long, curved glass hall
- Five story main hall runs north-south with barrel vault roof
- Two twelve story office buildings flank the sides of the main hall
- Two bridges link the office towers above the east-west hall
- Use of glass allows natural light throughout entire building



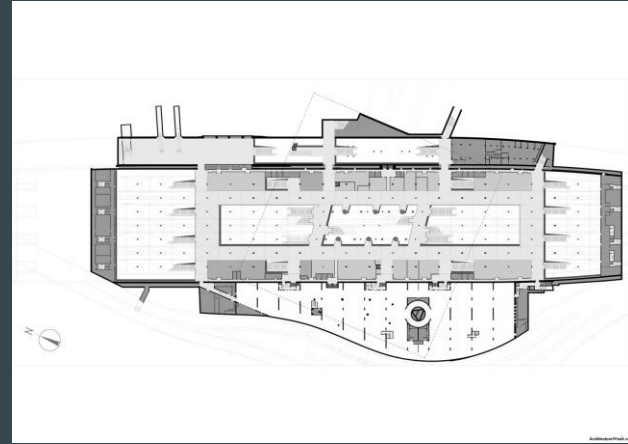
Plans



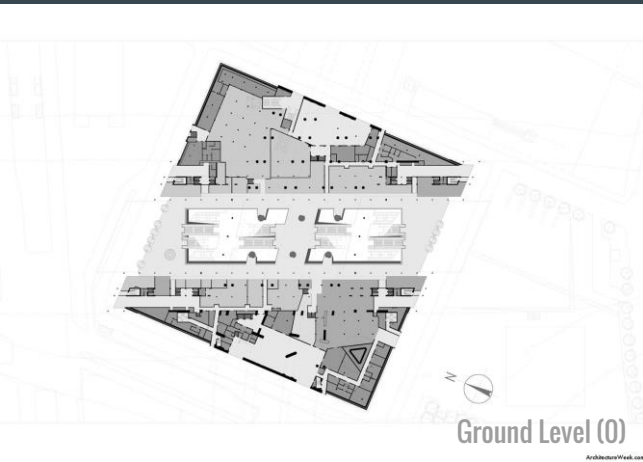
Site Plan



First Level (-2)



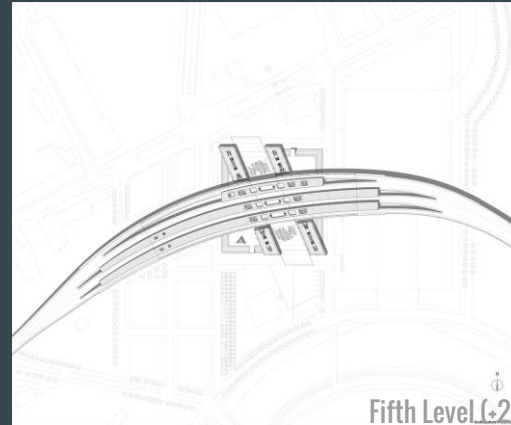
Second Level (-1)



Ground Level (0)

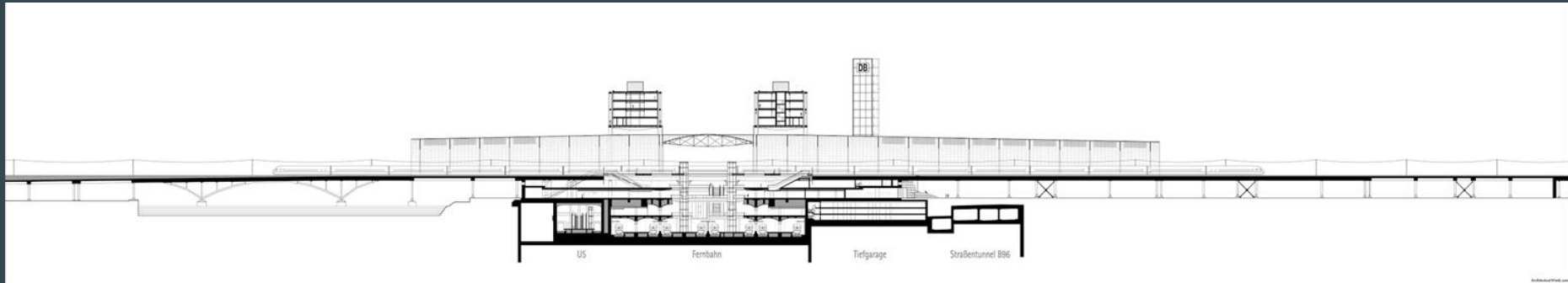
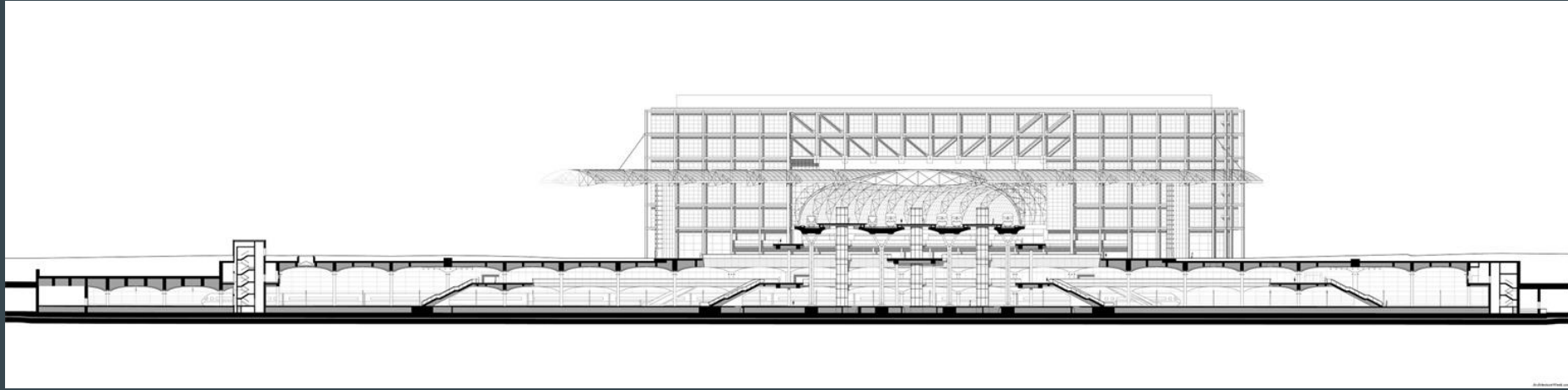


Fourth Level (+1)



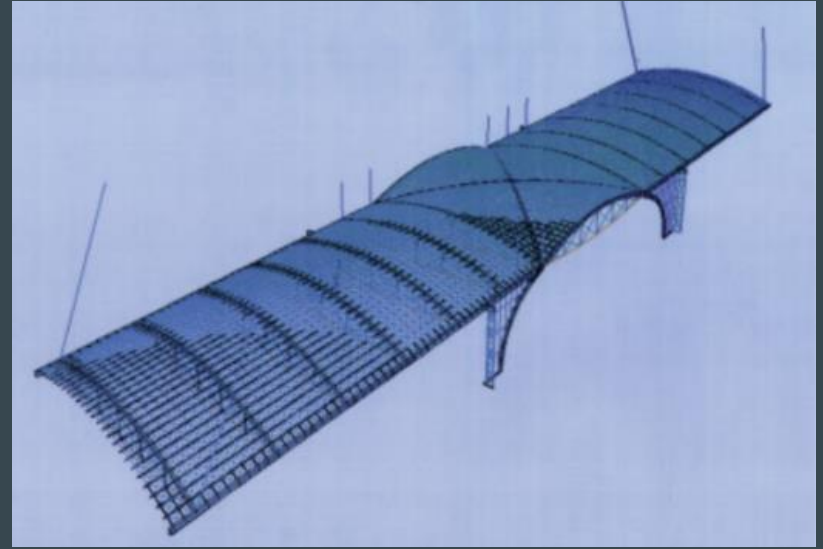
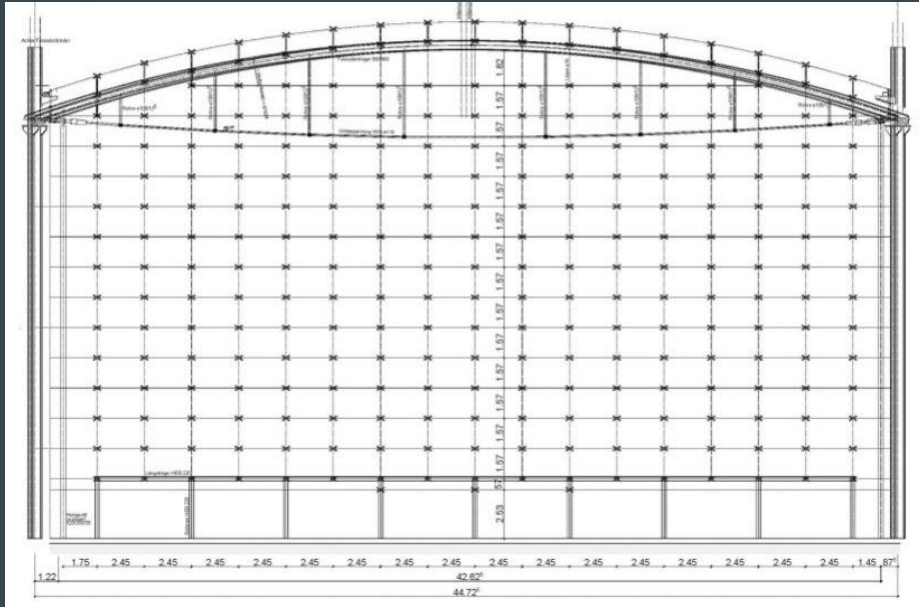
Fifth Level (+2)

Sections



Dimensions

- Structural system of North-South arch roof



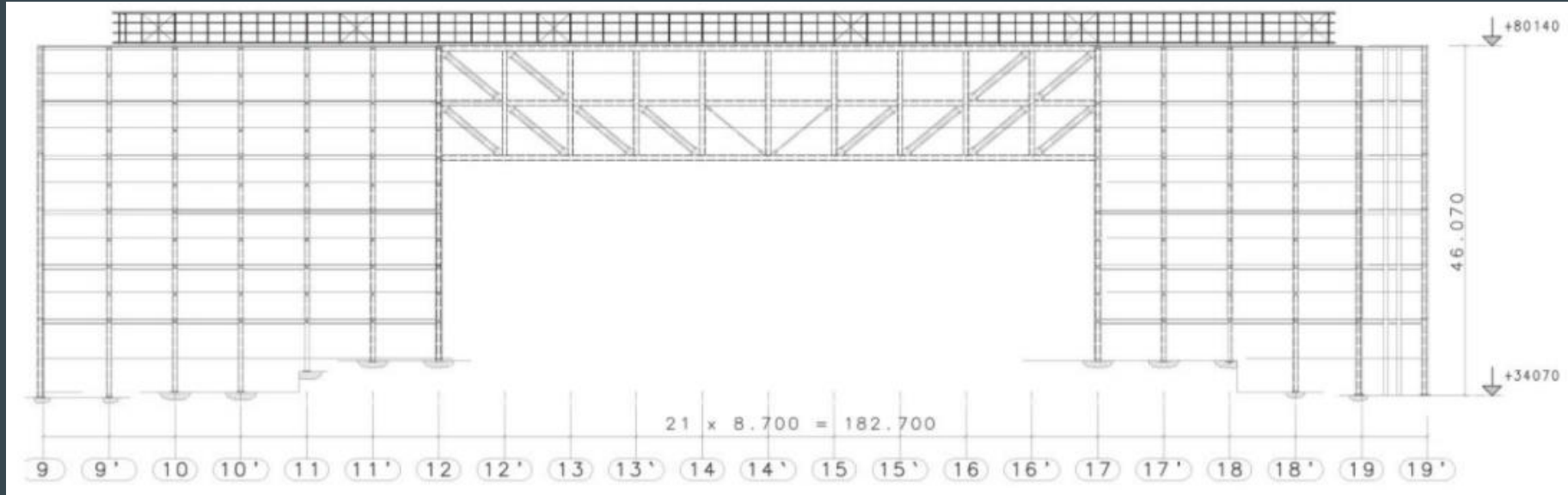
Length: 200m Width: 44.72m

Span of center cross are 65m and 45m

Dimensions of the facade with a width of 44.72m and a height of 25 m

Dimensions

- Structural system of office building (North-South)



Length: 182.70m Height: 46.07m

Each span is 8.70m

Dimensions

- The supporting structure of the roof surface directly covered with glass is provided by a quadrangular network .
- Mesh sizes of about 1.50 m to 1.70 m formed, which is braced diagonally with ropes.

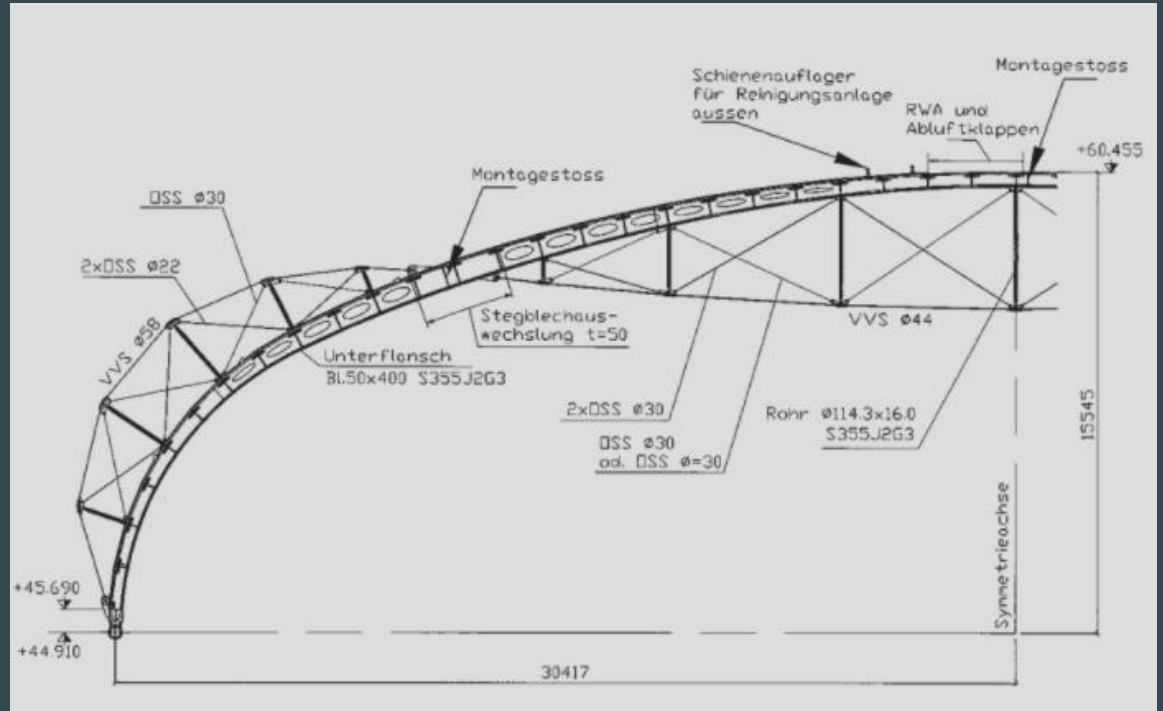


Dimensions

- Structural system of half arch girder

Width: 30.417m

Height: 15.545m



Materials

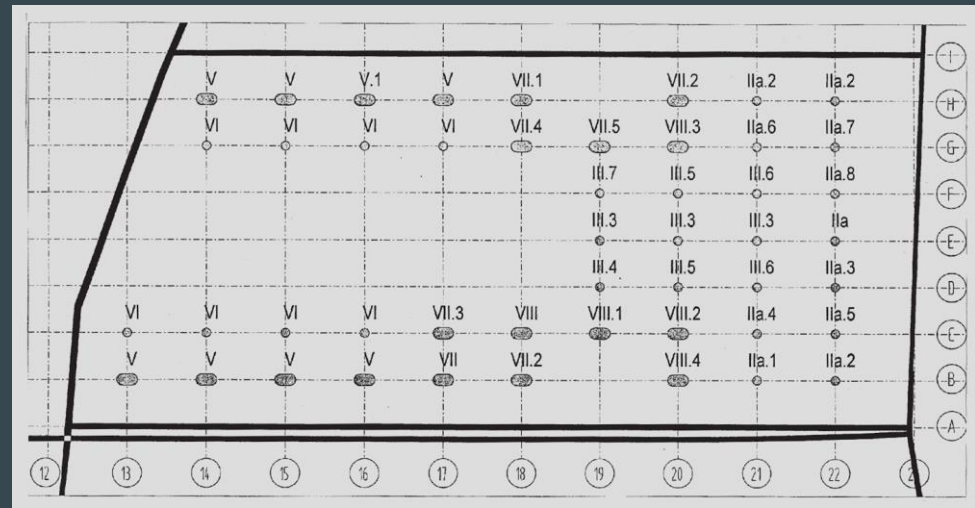
- Concrete
 - 500,000 m³
 - Foundation/Floors/Tracks
- Steel
 - 85,000 tons
 - 85 miles of steel cable
 - 23 steel trusses
- Glass
 - 27,000 glass blocks in ventilation tower
 - 20,000 m²/11,800 panels
- Solar Panels
 - Integrated into glass roof
 - 780 panels on the east-west roof



Structural Components

Composite columns

The main structure is formed by the railway tunnels and the supporting ceiling construction. The composite columns are connected rigidly to the structure base and the ceiling.

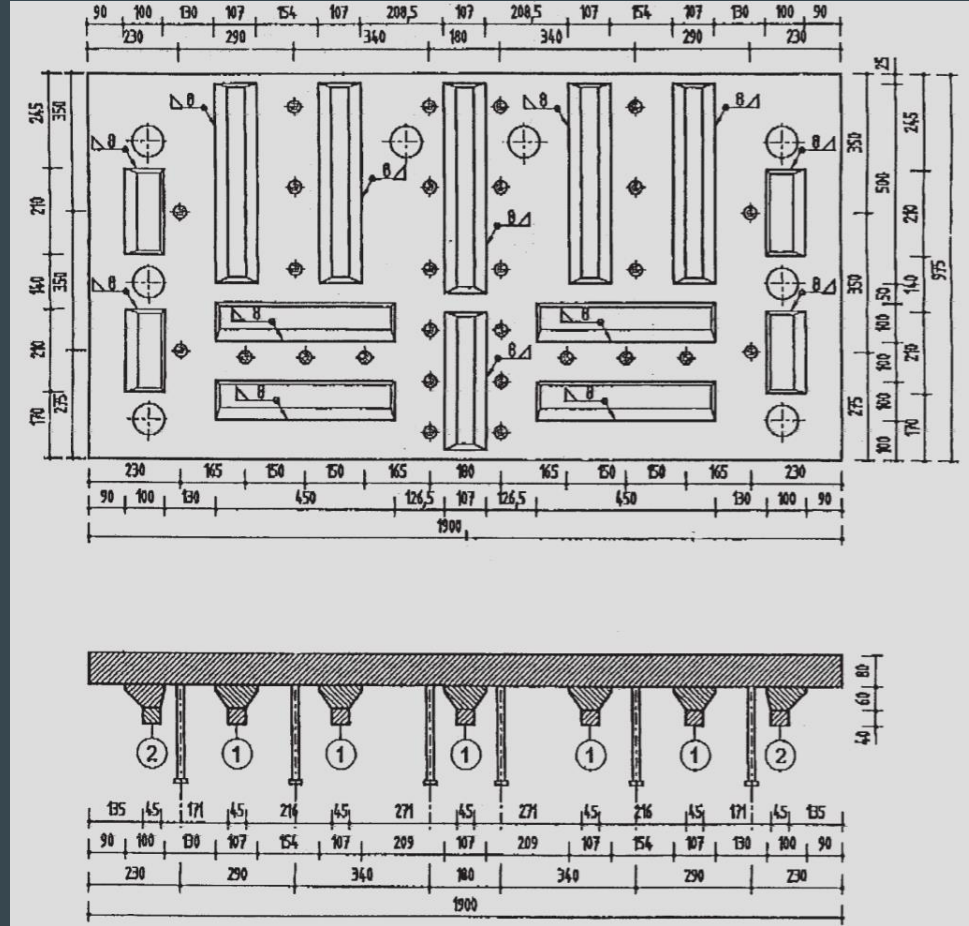


| Typ | V | VI | VII/VIII |
|-------------|---------------------------------|---------------------------------|---|
| Querschnitt | | | |
| Profil | 2 × HD 400 × 634 HISTAR 460 | HD × 1086 HISTAR 460 | 2 × HD 400 × 1086 HISTAR 460 (VII) S 355 K2 G3 (VIII) |
| Rohr | 2 × Bl. 45 × 400 S 355 K2 G3 | 2 × Bl. 45 × 400 S 355 K2 G3 | 2 × Bl. 60 × 500 S 355 K2 G3 |
| Beton | B55 | B55 | B55 |

Structural Components

Base plate

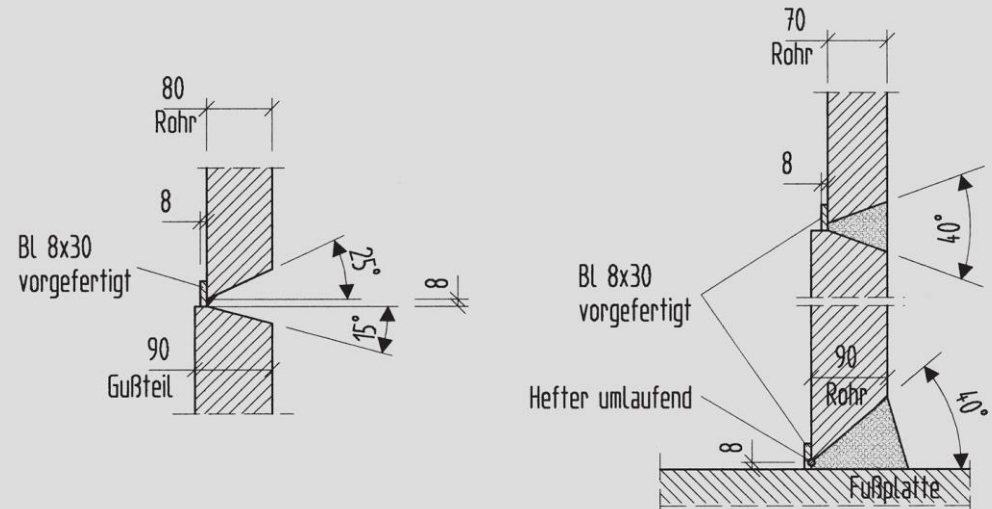
Push strips welded to the base plate.
The studs serve as “connecting reinforcement” that is anchored to the base plate. The concrete failure under tensile stress on the anchor was detected after the approval.



Structural Connections

Welded joint between duct and casting of the tree column and welding of the tree columns with induction grinding

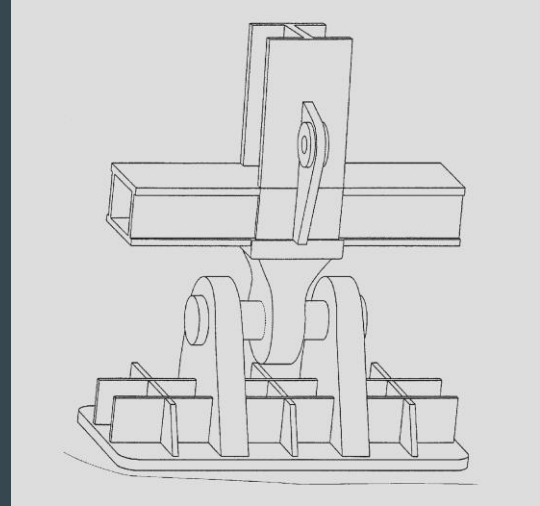
The welds were made with MAG-cored wire, the preheating temperatures were 145-165C, the intermediate layer temperatures 250C, in welding the castings induction loops have been set



Structural Connections

Bottom part of the bearing,
footpoint of the truss

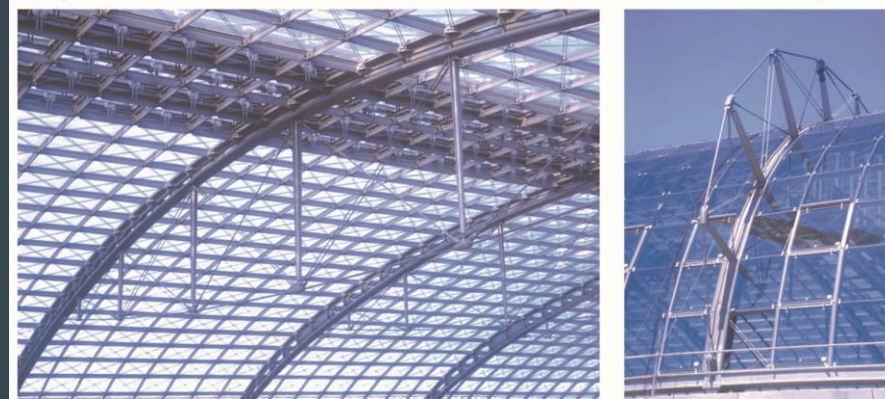
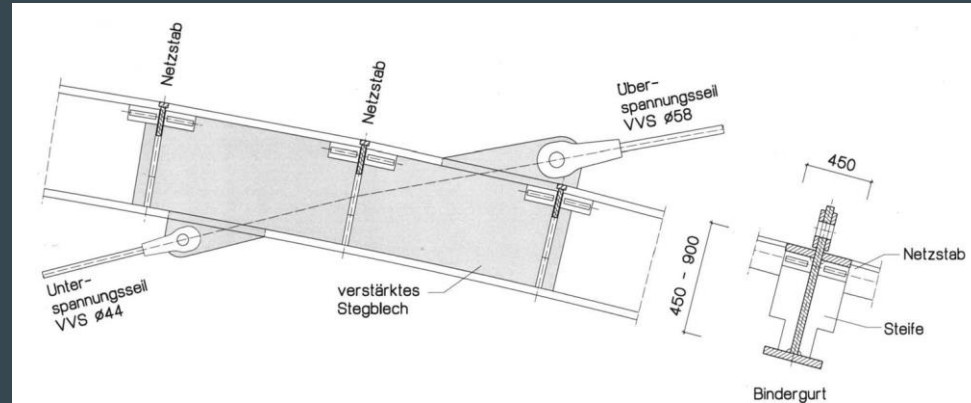
The first step in analysis of a truss
is to determine whether the truss
is a stable configuration of
members.



Structural Connections

Connection of the cables to the girder

Cables are used for long spans and in situation that allow the structure to be shaped with a significant depth. Of particular concern are the reaction forces at the connections of the cables to the supporting structure and especially the horizontal components of reactions.



Gravity Loads

LRFD basic Combinations: $1.2D+1.6L+0.5(L_r \text{ or } S \text{ or } R)$

Dead loads: Load (weight of building materials)

Office Building: concrete floor+steel frame+curtain wall

Station: Dome structure

Live loads: Defined by Occupancy type (Table 1607.7)

Office Building: office building--80 psf

Station: Assembly area--100 psf

Gravity Loads

Snow loads: Defined by snow zone

This project is located in Berlin.

In ZONE 2

SO the snow load is 18lb/sq.ft



Germany: snow

| Snow Zone | Snow load | | |
|-----------|-------------------|-------------------|------------|
| | kN/m ² | kg/m ² | lbs/sq.ft. |
| 1 | ≥0,65 | 66 | 14 |
| 1a | ≥0,81 | 83 | 17 |
| 2 | ≥0,85 | 87 | 18 |
| 2a | ≥1,06 | 108 | 22 |
| 3 | ≥1,10 | 112 | 23 |

Source: DIN1055-5

Lateral Loads

The basic lateral loads of buildings in

Berlin is wind load, From WEST, 100MPH

Wind direction distribution in (%)
Year

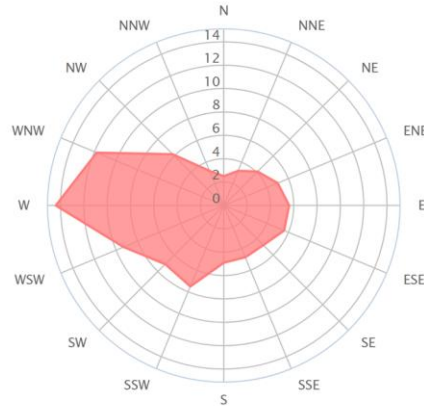


TABLE1604.10

GROUND SNOW LOADS; BASIC WIND SPEEDS; EARTHQUAKE DESIGN FACTORS

| City/Town | Ground Snow Load p_g , psf | Basic Wind Speed V , MPH | Earthquake Design Factors | |
|-------------------------|------------------------------|----------------------------|---------------------------|-------|
| | | | S_s | S_1 |
| Abington | 45 | 110 | 0.26 | 0.064 |
| Acton | 55 | 100 | 0.29 | 0.071 |
| Acushnet | 45 | 110 | 0.23 | 0.058 |
| Adams | 65 | 90 | 0.22 | 0.068 |
| Agawam | 55 | 100 | 0.23 | 0.065 |
| Alford | 65 | 90 | 0.22 | 0.066 |
| Amesbury | 55 | 110 | 0.35 | 0.077 |
| Amherst | 55 | 100 | 0.23 | 0.067 |
| Andover | 55 | 110 | 0.32 | 0.075 |
| Aquinnah (see Gay Head) | | | | |
| Arlington | 45 | 105 | 0.29 | 0.069 |
| Ashburnham | 65 | 100 | 0.27 | 0.072 |
| Ashby | 65 | 100 | 0.28 | 0.072 |
| Ashfield | 65 | 100 | 0.22 | 0.068 |
| Ashland | 55 | 100 | 0.25 | 0.066 |
| Athol | 65 | 100 | 0.25 | 0.070 |
| Attleboro | 55 | 110 | 0.24 | 0.062 |
| Auburn | 55 | 100 | 0.23 | 0.065 |
| Avon | 55 | 100 | 0.26 | 0.064 |
| Ayer | 65 | 100 | 0.28 | 0.071 |
| Barnstable | 35 | 120 | 0.20 | 0.054 |
| Barre | 55 | 100 | 0.24 | 0.068 |
| Becket | 65 | 90 | 0.22 | 0.066 |
| Bedford | 55 | 100 | 0.29 | 0.071 |
| Belchertown | 55 | 100 | 0.23 | 0.066 |
| Bellingham | 55 | 100 | 0.24 | 0.064 |
| Belmont | 45 | 105 | 0.28 | 0.069 |
| Berkley | 55 | 110 | 0.24 | 0.061 |
| Berlin | 55 | 100 | 0.26 | 0.068 |

Analysis (Gravity)

Office Building:

Total of 85000 tons of steel, Curtain wall, Steel deck Concrete floors

1) Dead loads: Steel Frame: 360 lb/sq.ft

25mm thick Curtain Wall: 12 lb/sq.ft

Steel deck concrete floors: 8 lb/sq.ft

2) Live loads: Occupancy type--Office Building, 80 lb/sq.ft

Roof-- Steel deck, 8 lb/sq.ft

3) Snow loads: In zone 2, 18lb/sq.ft

Analysis (Gravity)

Station:

Dome consisting by glass panels.

- 1) Dead loads: Same material as curtain wall--12 lb/sq.ft
- 2) Live loads: Occupancy type--Assembly area, 100 lb/sq.ft
- 3) Snow loads: 18 lb/sq.ft

Analysis (Lateral)

According to the table, wind speed in Berlin is 100 Mph

Calculating the wind pressure: $p = 0.00256 \times V^2$

$p = 25.6 \text{ lb/sq.ft}$

TABLE 1604.10
GROUND SNOW LOADS; BASIC WIND SPEEDS; EARTHQUAKE DESIGN FACTORS

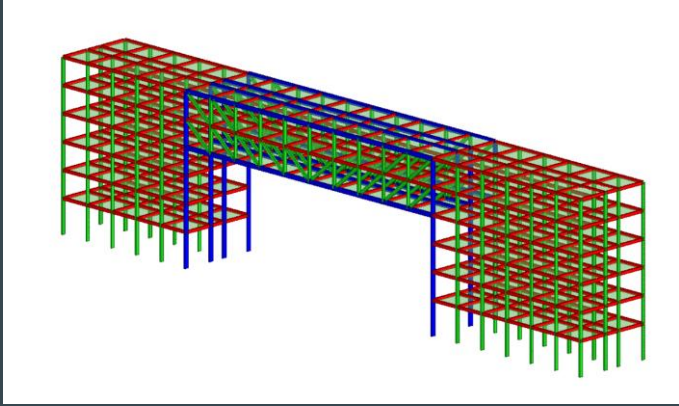
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| Belmont | 45 | 105 | 0.28 | 0.069 |
| Berkley | 55 | 110 | 0.24 | 0.061 |
| Berlin | 55 | 100 | 0.26 | 0.068 |

Foundation

- Sandy soil created complexities
- 1.5 million m³ of soil removed on barges
- Concrete ponds 25m deep were poured for groundwater retention
- Divers constructed diaphragm walls and set concrete base slab in pits before they were drained
- Flat foundation
- Shallow foundation due to water level

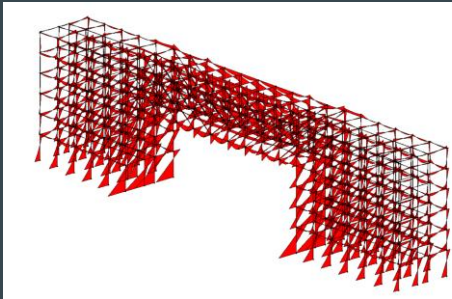
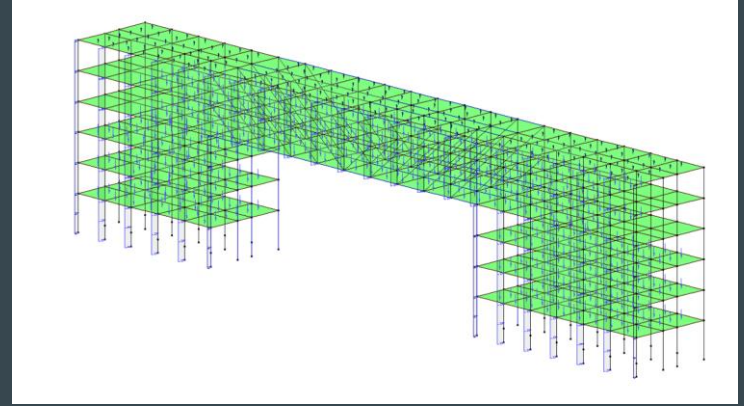


Office Building Analysis

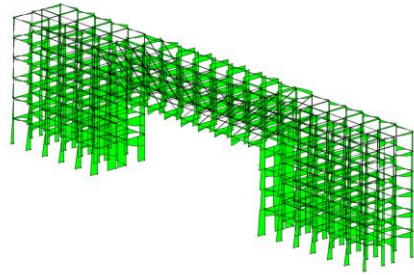


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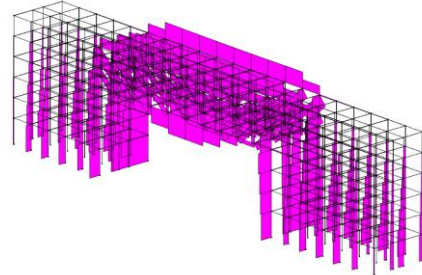
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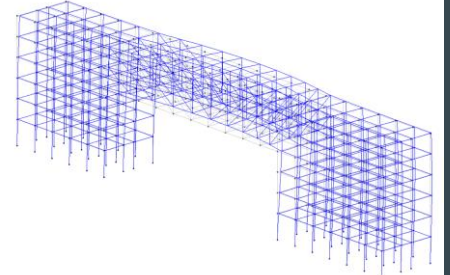
Mz



Vy

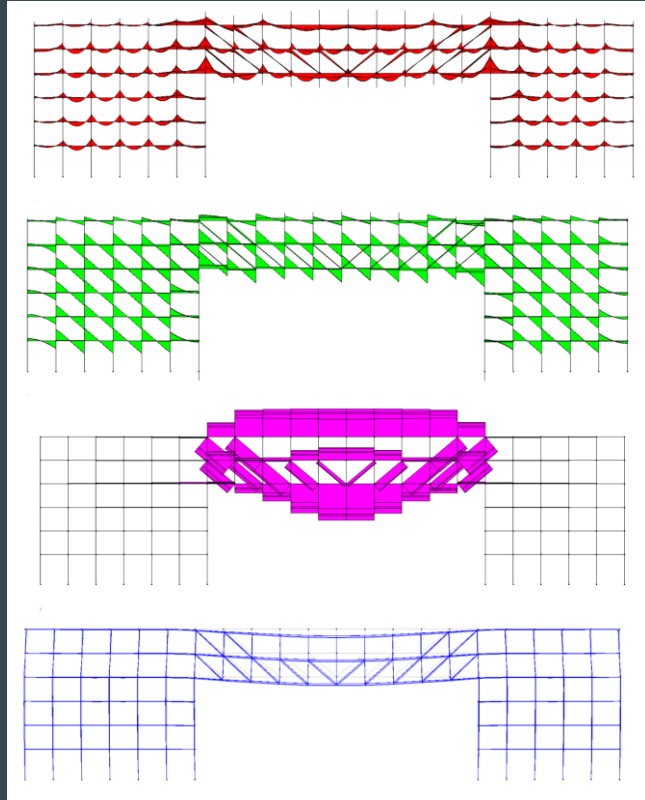


Px



Defl.

Office Building Analysis

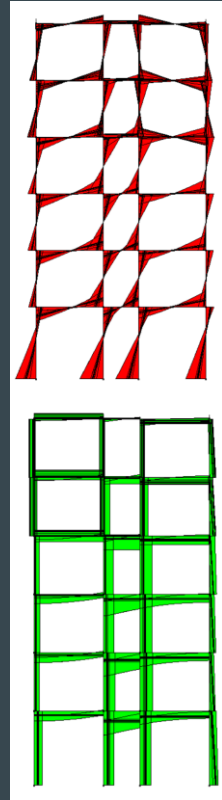


M_z

V_y

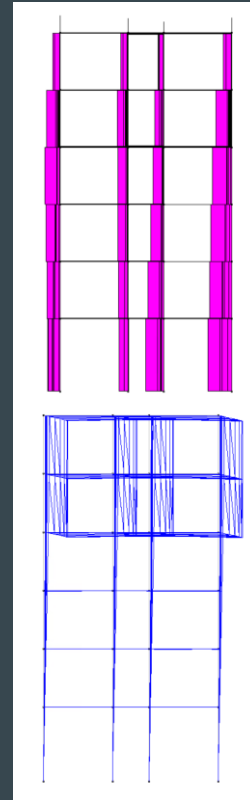
P_x

Defl.



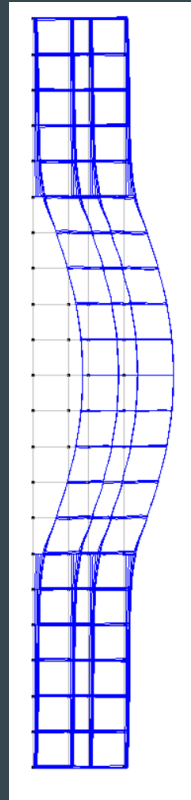
M_z

V_y



P_x

Defl.



Office Building Analysis



Train Tunnel Analysis

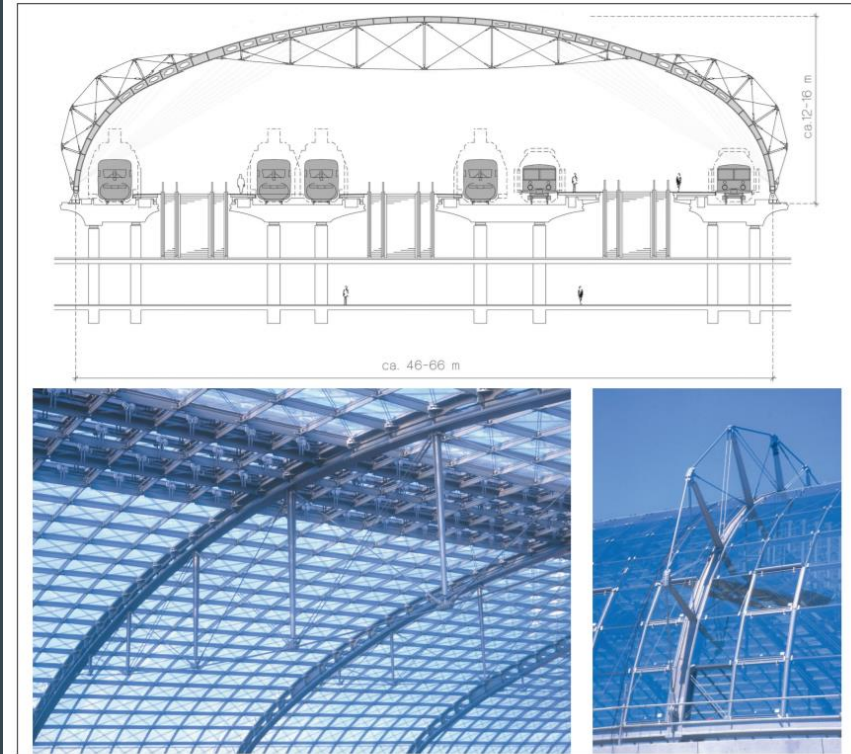


Bild 4. Dachbinder
Fig. 4. Roof girders

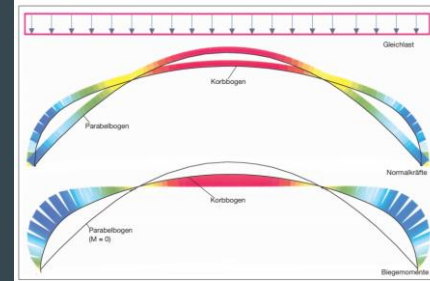


Bild 15. Das korbobogenartige Profil des Daches ist weit weg von der Sättellinienform
Fig. 15. The basket arch profile differs from the thrust line

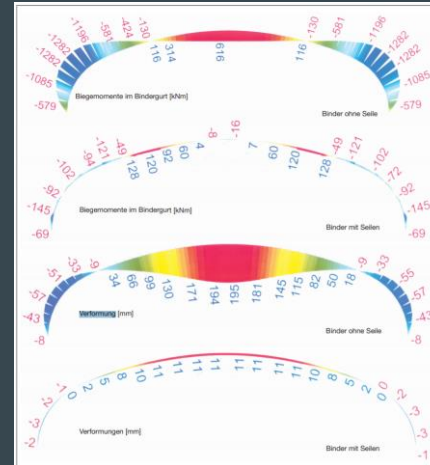


Bild 16. Die Seile sind so geführt, daß unter Gleichlast nur Normalkräfte im Bindergerüst auftreten
Fig. 16. The bracing cables are so arranged that only normal forces result in the chord under uniformly distributed loads

Atrium Analysis

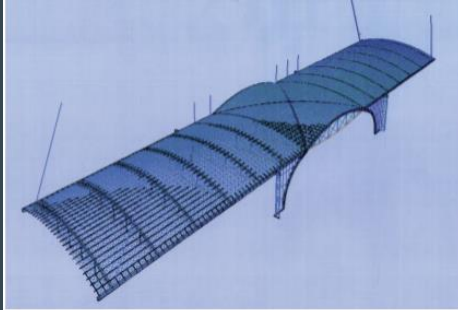


Bild 5. Tragsystem des Nord-Süd-Daches
Fig. 5. Structural system of North-South-roof

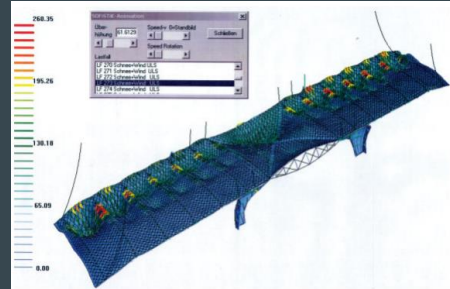


Bild 11. Spannungen und Verformungen im Lastfall 273 (Eigengewicht, Vorspannung, Schneeverwehung und asymmetrischer Wind)
Fig. 11. Stresses and deflections of load case combination 273 (dead loads, pre-stress, snow and asymmetric wind loads)

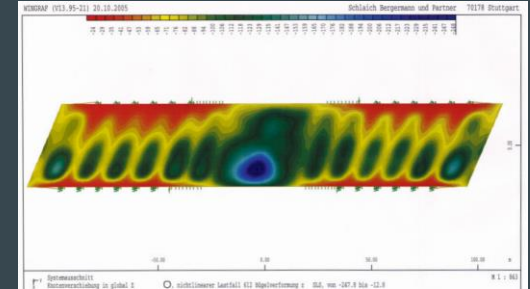


Bild 12. Vertikale Verformungen im Lastfall 612 (Eigengewicht, Vorspannung, Schneeverwehung, asymmetrischer Wind, Verhalverschiebung Biegelbauten, Anhängelasten, Dachbefahrungslage)
Fig. 12. Vertical deflection of load case combination 612 (dead loads, pre-stress, snow, asymmetric wind loads, support movement and live loads)



Bild 8. Ansicht Seilbinder
Fig. 8. View of the cable-span girder



Bild 14. Binderseilklammern
Fig. 14. Clamps of girder cables

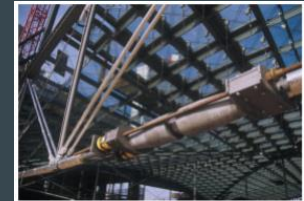
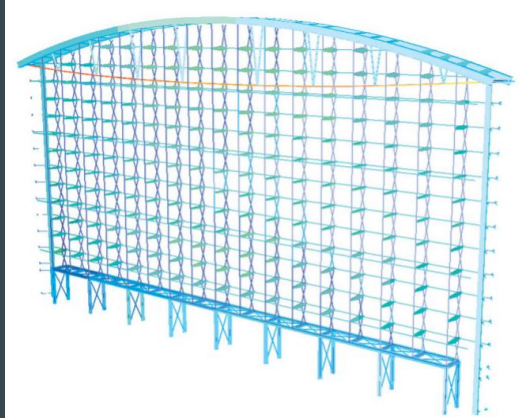


Bild 22. Hydraulische Pressen zur Seilvorspannung
Fig. 22. Hydraulic press to pre-stress the cables

Atrium Curtain Wall Analysis



Lastfall 18 Bezogene Spannung σ_{max}
 [Max.sig.bezucht ca. 100.37 N/mm²]
 Exakte Spannungen nur über ADR!
 Druck
 $\sigma_{\text{max}} = -0.405$

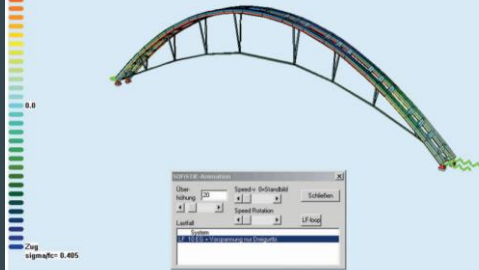
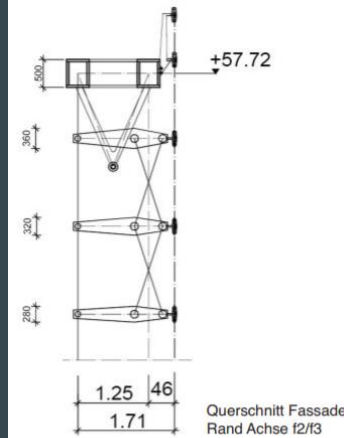


Bild 17 Dreigübrinder mit vorgespanntem Unterspannseil (Überhöhung 20fach)
 Fig. 17. Anched girder with prestressing



Querschnitt Fassade
 Rand Achse I2/I3

Bild 2. Seilbinder
 Fig. 2. Cable girders



Bild 7. Ansicht der unteren Glasschwerter
 Fig. 7. View of the glass fins over the portal frame

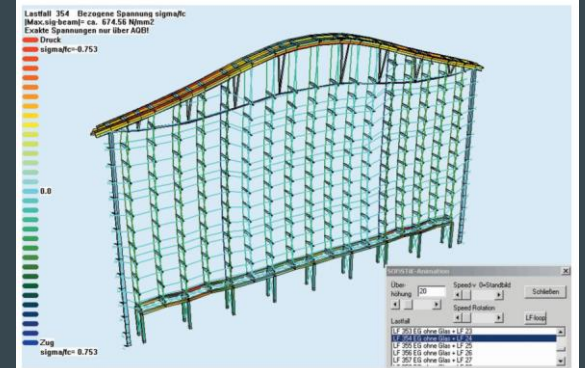


Bild 18. Vorspannung der fünf äußeren Seilbinder
 Fig. 18. Prestressing of the five outer cable girders

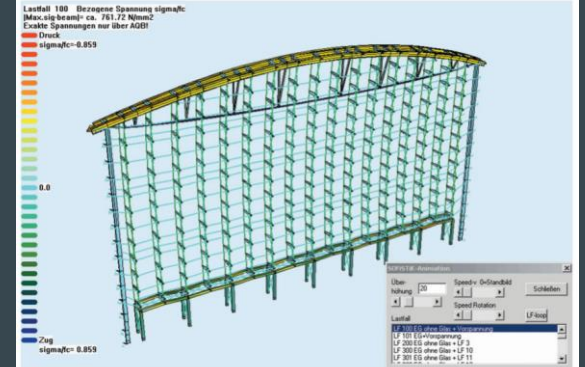


Bild 20. Vollständig vorgespannte Fassade
 Fig. 20. Completely prestressed facade

References

<http://www.spiegel.de/international/spiegel/berlin-s-new-train-station-a-glass-armadillo-for-germany-s-capital-a-417598.html>

<http://www.gmp-architekten.com/projects/berlin-central-station.html>

<https://en.wikiarquitectura.com/building/berlin-central-station/>

http://www.architectureweek.com/2006/1108/design_1-2.html

<http://www.sbp.de/en/project/berlin-main-train-station-1/>

http://constructalia.arcelormittal.com/en/case_study_gallery/germany/histar_steel_columns_in_the_structure_of_berlin_central_station

<http://www.aviewoncities.com/berlin/hauptbahnhof.htm>

<https://www.scribd.com/doc/78414396/Snow-Maps>

<https://www.windfinder.com/windstatistics/berlin-tegel>

<http://www.mass.gov/eopss/docs/dps/7th-mass-basic/16-table1604.pdf>

References

Albrecht, G., Klähne, T., & Stucke, W. (2002). Aspects of the technical examination of the construction project Lehrter Bahnhof Berlin. Steel construction , 71 (12), 890-903.

Kina, J., Klähne, T., Nguyen, KM, & Einhäuser, O. (2002). Constructional examination of the east-west roof of the Lehrter station. Steel construction , 71 (12), 904-912.

Schlaich, J., Schober, H., & Justice, S. (2002). Design and construction of the platform hall of the Lehrter station. Steel construction , 71 (12), 853-868.

Petersen, L., & Naujoks, B. (2006). Composite supports of the ironwork over the Berlin main station. Concrete and reinforced concrete construction , 101 (2), 108-114.

Gugeler, J., Gerber, H., Schneider, J., & Havemann, K. (2006). Lehrter Bahnhof Berlin: The main entrance facades. Steel construction , 75 (6), 415-427.

Gugeler, J., Havemann, K., & Schober, H. (2006). Lehrter Bahnhof Berlin: The north-south roof. Steel construction , 75 (3), 194-202.

Schodek, D. L., & Schodek, D. L. (2001). Structures.