

## Chapter 2 Axially Loaded Members

Structural components subjected only to **tension** or **compression**: solid bars with straight longitudinal axes, cables and coil springs – can be seen in truss members, connecting rods, spokes in bicycle wheels, columns in buildings, and struts in aircraft engine mounts

### 2.2 Changes in Lengths of Axially Loaded Members

#### ⊙ Springs

1. If the material of the spring is linear elastic,

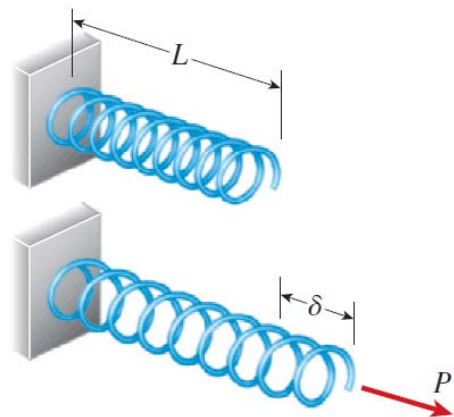
$$P = k\delta$$

where  $k$  is the **stiffness** of the spring, or spring constant, defined as the force required to produce a unit elongation.

2. The inverse relationship is

$$\delta = \frac{1}{k}P = fP$$

where  $f$  is the **flexibility** of the spring, or compliance, defined as the elongation produced by a unit force.



#### ⊙ Prismatic Bars

1. If the load acts through the centroid of the end cross section (proof at pp. 31-32), at a point away from the ends (Saint-Venant's principle), the normal stress is uniformly distributed and thus

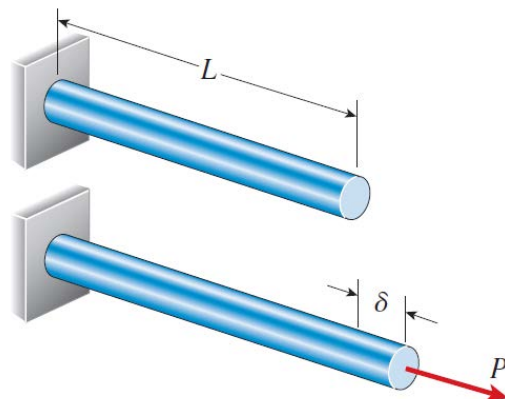
$$\sigma = \frac{P}{A}$$

2. If the bar is homogeneous, the axial strain is

$$\varepsilon = \frac{\delta}{L}$$

3. Using Hooke's law  $\sigma = E\varepsilon$ , the elongation is derived as

$$\delta = \frac{PL}{EA} \quad \text{where } EA: \text{axial rigidity}$$



4. The relationship above works for both tension and compression with a proper sign convention (plus sign for  $P$  and  $\delta$  in tension and negative in compression)
5. Stiffness and flexibility of a prismatic bar:

$$k = \frac{EA}{L}$$

$$f = \frac{L}{EA}$$



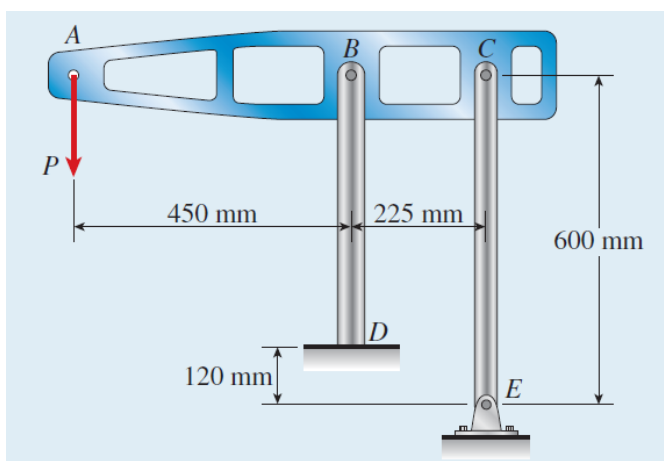
⊙ Cables

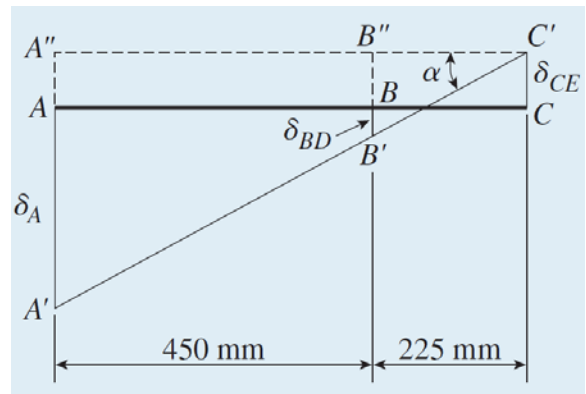
1. Important structural elements used when lifting/pulling/sustaining heavy objects (elevators, suspension bridges, cable-stayed bridges)
2. Cannot resist c\_\_\_\_\_, thus not used against b\_\_\_\_\_
3. Elongation of a cable is greater than that of a solid bar with the same material because the wires in the cable “tighten up” (instead of deforming in axial direction) → the “effective” modulus of elasticity is less than that of the material



⊙ **Example 2-2:** Cross-sectional areas of the bars BD and CE are 1,020 mm<sup>2</sup> and 520 mm<sup>2</sup>, respectively. The bars are made of steel having a modulus of elasticity  $E = 205$  GPa. Assume the beam ABC is rigid.

- a) Maximum allowable load  $P$  if the displacement of point  $A$  is limited to 1.0 mm
- b) If  $P = 25$  kN, what is the required cross-sectional area of bar CE so that the displacement at point  $A$  is equal to 1.0 mm?



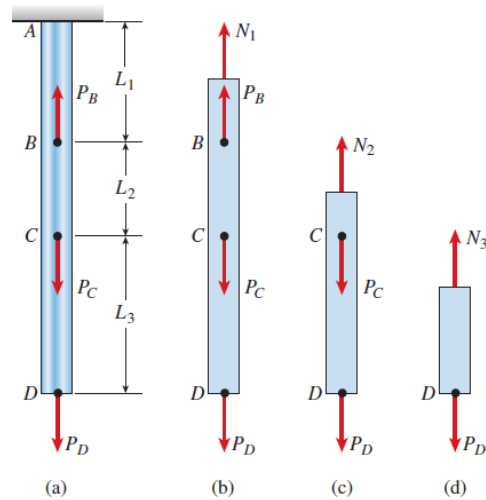


## 2.3 Changes in Lengths under Non-uniform Conditions

### ⊙ Bars with Intermediate Axial Loads

#### 1. Procedure for a prismatic bar

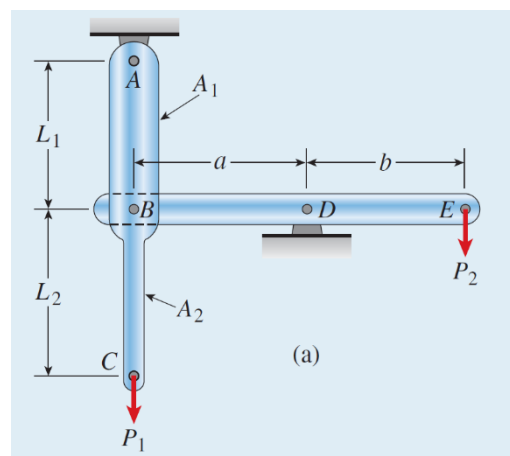
- A. Identify the segments based on the intermediate axial loads
- B. Determine the internal axial forces from equilibrium
- C. Determine the change in each segment using  $\delta_i = N_i L_i / EA$
- D. Add the changes to find the total elongation, i.e.  $\delta = \sum_{i=1}^n \delta_i$



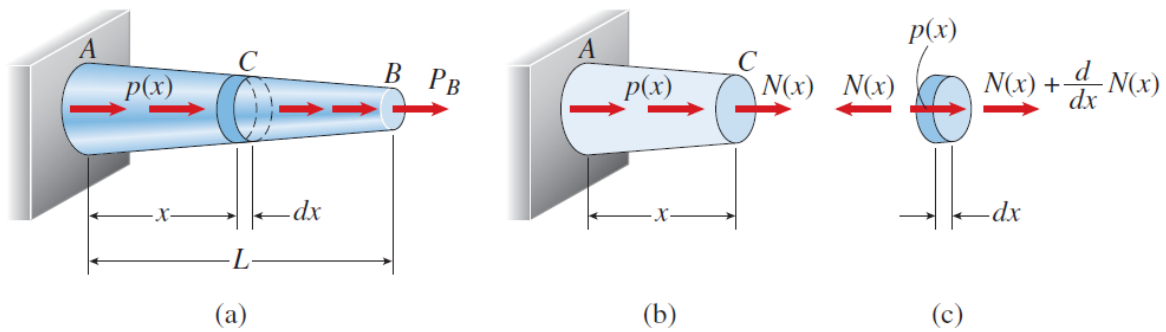
2. If the bar consists of multiple prismatic bars with different materials and/or cross-sectional areas,  $\delta = \sum_{i=1}^n N_i L_i / E_i A_i$

- ⊙ **Example 2-3:**  $L_1 = 20.0$  in.,  $L_2 = 34.8$  in.,  
 $A_1 = 0.25$  in.<sup>2</sup>,  $A_2 = 0.15$  in.<sup>2</sup>,  $E = 29.0 \times 10^6$  psi,  
 $a = 28$  in., and  $b = 25$  in.

Calculate the vertical displacement  $\delta_C$  at C when the load  $P_1 = 2,100$  lb and  $P_2 = 5,600$  lb (Self-weight neglected)

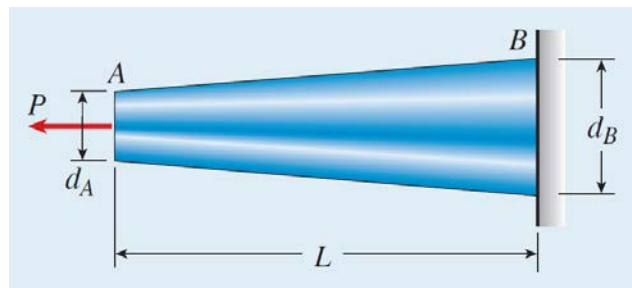


⊙ Bars with Continuously Varying Loads or Dimensions



1. Suppose the axial load  $P(x)$ , Young's modulus  $E(x)$  or cross-sectional area  $A(x)$  vary over the length
2. Consider the cylinder with the infinitesimal length  $dx \rightarrow$  Figure (c)
3. The elongation of the cylinder is  $d\delta = \text{_____}$
4. The total elongation is  $\delta = \int_0^L d\delta = \int_0^L \text{_____} dx$
5. Limitations: works when the material is linear elastic and the stress is uniformly distributed – the latter may not hold if the angle of the tapered bar is large

⊙ **Example 2-4:** Determine the elongation of a tapered bar AB of solid circular cross section



## 2.4 Statically Indeterminate Structures

### ⊙ Statically Indeterminate Structures

1. Statically determinate:  $r$  \_\_\_\_\_ and  $i$  \_\_\_\_\_  
 $f$  \_\_\_\_\_ can be determined solely from free-body diagrams and equations of  $e$  \_\_\_\_\_

**Statically indeterminate:** otherwise

2. Example: axially loaded bar with fixed boundary conditions at both ends ( $\rightarrow$ )

$$R_A - P + R_B = 0 \quad (1)$$

3. How to solve?

Introduce **equation of c** \_\_\_\_\_, i.e.

$$\delta_{AB} = \quad (2)$$

4. Equations (1) and (2) are defined in terms of different terms (force and displacement)  $\rightarrow$  Use

$f$  \_\_\_\_\_ -  $d$  \_\_\_\_\_ relationship  $\delta_{AC} = \frac{R_A a}{EA}$  and

$$\delta_{CB} = -\frac{R_B b}{EA}$$

5. Now, Eq. (2) becomes  $\delta_{AB} = \delta_{AC} + \delta_{CB} = \frac{R_A a}{EA} - \frac{R_B b}{EA} = 0 \quad (3)$

6. Solving Eq. (1) and (3) together, one can get  $R_A = \frac{Pb}{L}$  and  $R_B = \frac{Pa}{L}$

7. With these reactions, one can obtain the internal forces and the elongations. For example, the vertical displacement of point C is  $\delta_C = \delta_{AC} = \frac{R_A a}{EA} = \frac{Pab}{LEA}$

8. Stresses can be found too. For example, the normal stress in the segment AC is

$$\sigma_{AC} = \frac{R_A}{A} = \frac{Pb}{AL}$$

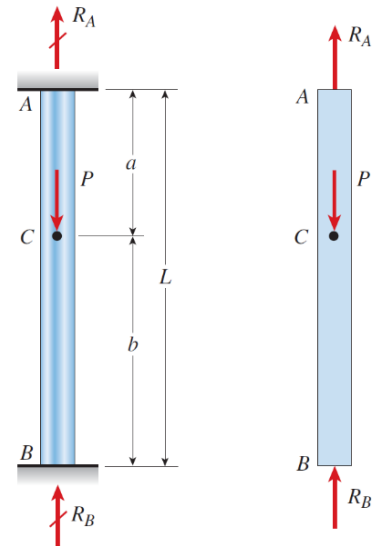
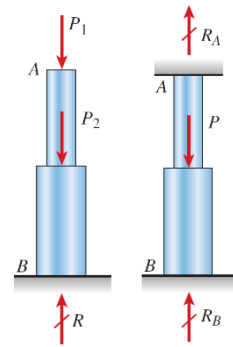
### ⊙ Terminologies

1. **(a) Equilibrium equations:** static or kinetic equations

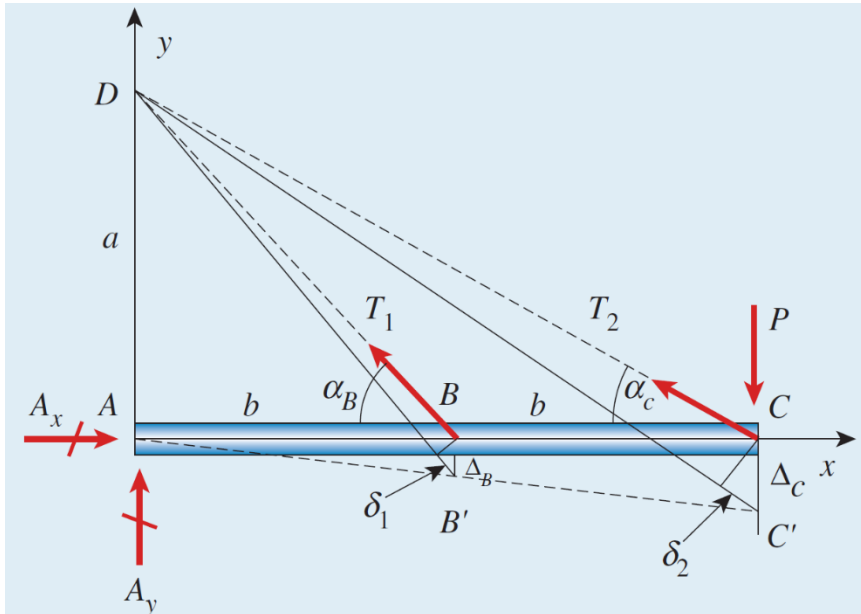
**(b) Compatibility equations:** geometric equations, kinematic equations, equations of consistent deformations

**(c) Force-displacement relations:** constitutive relations

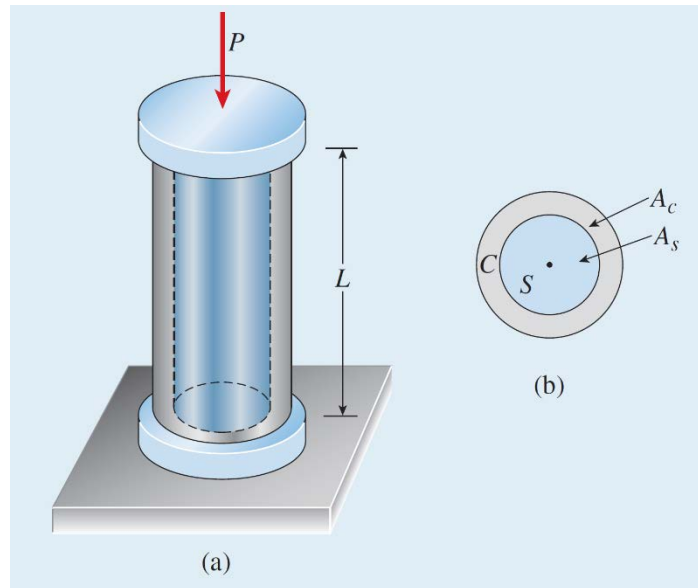
2. **Stiffness method** (displacement method) vs **flexibility method** (force method)



- ⊙ **Example 2-5:** A vertical load  $P$  applied on a horizontal *rigid* bar  $ABC$  is supported by wires  $BD$  and  $CD$  with diameters  $d_1$  and  $d_2$ , modulus of elasticity  $E_1$  and  $E_2$ , and lengths  $L_1$  and  $L_2$  respectively. Obtain formulas for the allowable load  $P$  when the allowable stresses in the wires  $BD$  and  $CD$  are  $\sigma_1$  and  $\sigma_2$ , respectively.



- ⊙ **Example 2-6:** A solid circular steel cylinder  $S$  (with Young's modulus  $E_s$  and cross-sectional area  $A_s$ ) is encased in a hollow circular copper tube  $C$  (with  $E_c$  and  $A_c$ ). When the cylinder and tube are compressed between the *rigid* plates of a testing machine by compressive forces  $P$ , determine the compressive forces  $P_s$  and  $P_c$ , the corresponding stresses, and the shortening of the assembly,  $\delta$ .





## 2.5 Thermal Effects, Misfits, and Prestrains

Other sources of deformations than external loads: thermal effects, misfits (imperfections), prestrains, settlements, inertial loads, etc.

⊙ Thermal Effects (expands when heated; contracted when cooled)

1. For most structural materials, thermal strain  $\varepsilon_T$  is proportional to the temperature change  $\Delta T$

$$\varepsilon_T = \alpha(\Delta T)$$

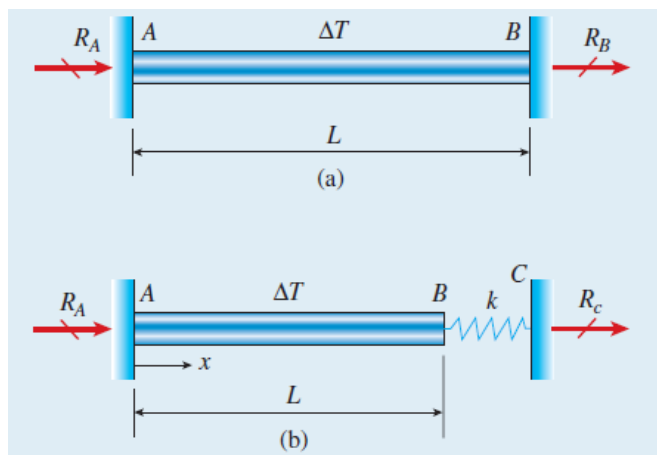
2.  $\alpha$ : **coefficient of thermal expansion** ( $1/K = 1/^\circ\text{C}$ ) or ( $1/^\circ\text{F}$ )

3. Stress that would cause the thermal strain caused by  $\Delta T$ :  $\sigma = E\alpha(\Delta T)$

e.g. the temperature change  $\Delta T = 100^\circ\text{F}$  causes the same strain produced by 29,000 psi (typical allowable stress of stainless steel)

4. Temperature-displacement relation:  $\delta_T = \varepsilon_T L = \alpha(\Delta T)L$

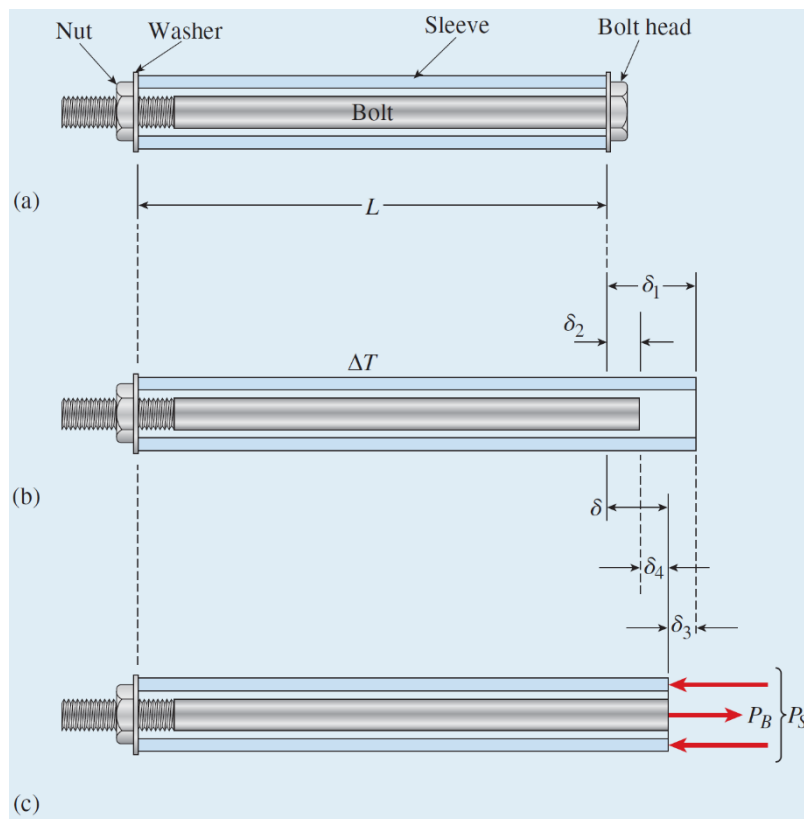
⊙ **Example 2-7:** A prismatic bar  $AB$  of length  $L$ , made of linearly elastic material with modulus  $E$  and thermal expansion coefficient  $\alpha$  is held between immovable supports.



- (a) When the temperature is raised by  $\Delta T$ , derive a formula for the thermal stress  $\sigma_T$

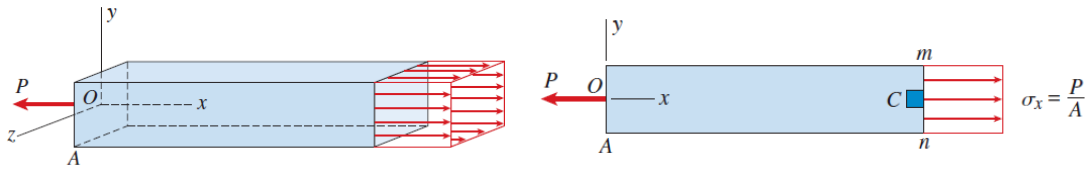
- (b) Modify the formula in (a) if the rigid support  $B$  is replaced by an elastic support having a spring constant  $k$ . Only the bar is subjected to the temperature change  $\Delta T$ .

- ⊙ **Example 2-8:** A sleeve in the form of a circular tube of length  $L$  is placed around a bolt and fitted between washers at each end. Assume  $\alpha_S > \alpha_B$ . (a) If the temperature is raised by  $\Delta T$ , what are the stresses in the sleeve and bolt, respectively? (b) What is the increase  $\delta$  in the length  $L$  of the sleeve and bolt?



## 2.6 Stresses on Inclined Sections

### ⊙ Stresses on Section Perpendicular to Axis

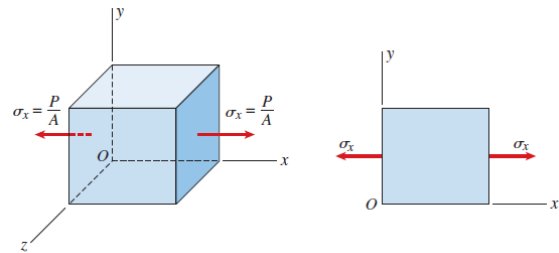


1. Normal stress  $\sigma = P/A$  (prismatic, homogeneous and axial force at the centroid, away from the stress concentration at ends)

2. Normal stress only, i.e no

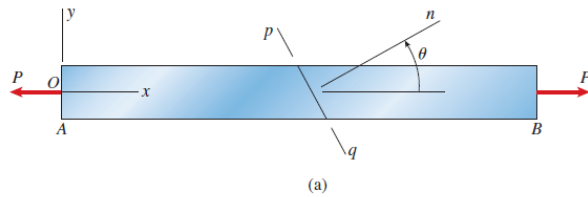
s \_\_\_\_\_

3. "Stress element"( $\rightarrow$ ): an infinitesimal block with its right-hand face lying in cross section ("C" in the figure above)



### ⊙ Stresses on Inclined Sections

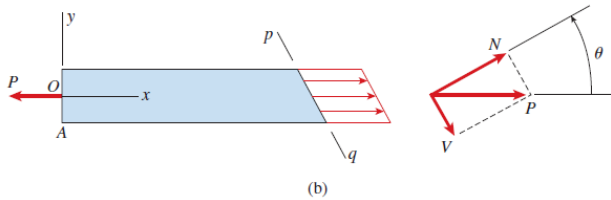
1. Orientation of the inclined section: determined by  $\theta$  ~ angle between x-axis and the normal vector  $n$



2. Two force components for the inclined section pq:

$$N = P \cdot \cos \theta$$

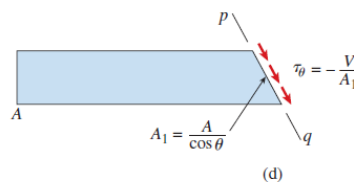
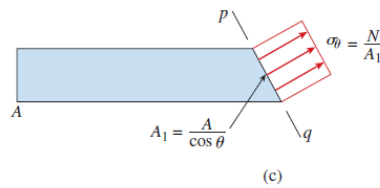
$$V = P \cdot \sin \theta$$



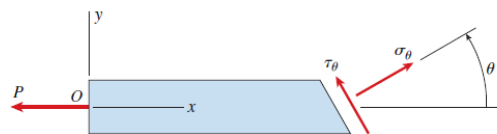
3. Then the normal and shear stresses on the inclined section are:

$$\sigma = \frac{N}{A_1}, \quad \tau = \frac{V}{A_1}$$

where  $A_1 = \frac{A}{\cos \theta}$



4. Sign conventions: normal stress positive in tension, and shear stress positive when it produces counterclockwise rotation



5. Thus, the normal and shear stresses on inclined section with the orientation  $\theta$  are

$$\sigma_\theta = \frac{P}{A} \cos^2 \theta = \sigma_x \cos^2 \theta = \frac{\sigma_x}{2} (1 + \cos 2\theta)$$

$$\tau_\theta = -\frac{P}{A} \sin \theta \cos \theta = -\sigma_x \sin \theta \cos \theta = -\frac{\sigma_x}{2} (\sin 2\theta)$$

⊙ Maximum Normal and Shear Stresses

1. Plots of  $\sigma_\theta$  and  $\tau_\theta$  ( $\rightarrow$ )

2. Maximum normal stress:

$$\sigma_{max} = \sigma_x \text{ at } \theta = 0^\circ$$

Corresponding shear stress = 0

3. Maximum shear stress:

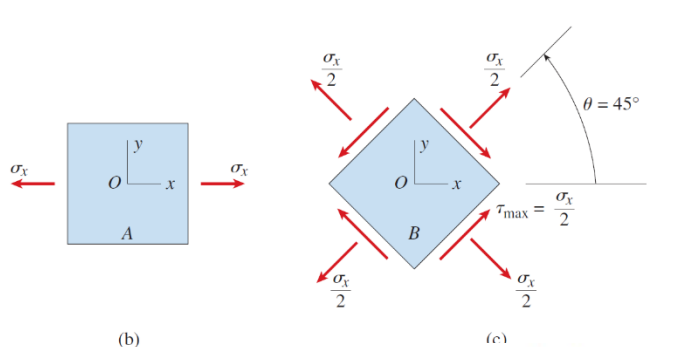
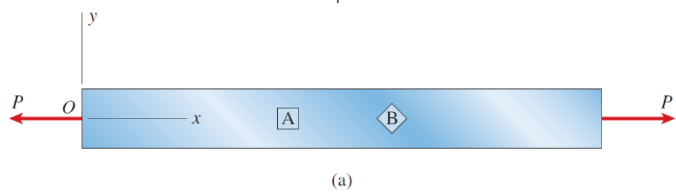
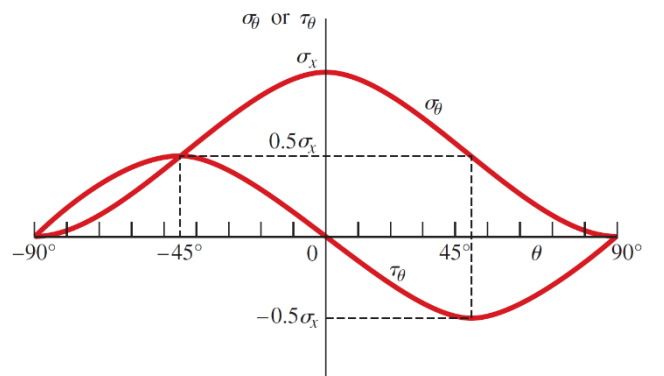
$$\tau_{max} = \frac{\sigma_x}{2} \text{ at } \theta = \pm 45^\circ$$

Corresponding normal stress =  $\frac{\sigma_x}{2}$

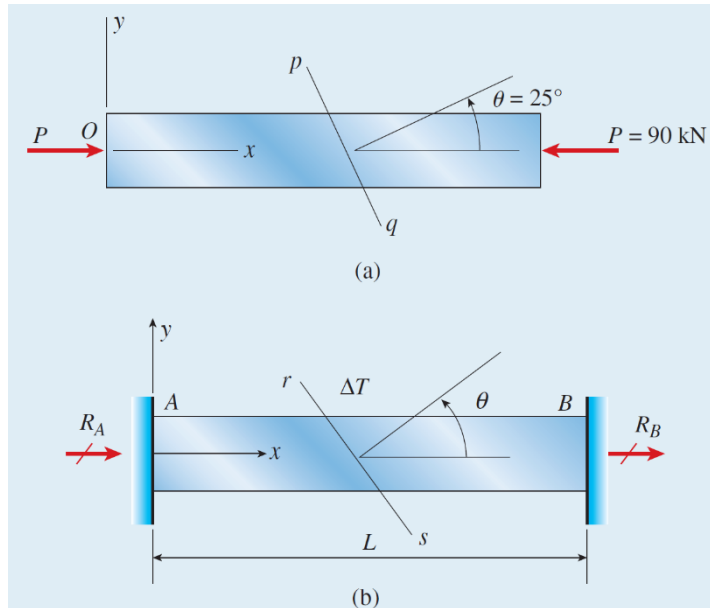
4. The most important orientations for uniaxial stress condition is  $\theta = 45^\circ$  and  $\theta = 135^\circ$

5. Even though  $\sigma_{max} = 2\tau_{max}$ , a bar can fail in shear if the material is more vulnerable to the shear failure.

Examples: shear failure of wood block in compression ( $\rightarrow$ ), and "slip bands" of flat bar of low carbon steel ( $\rightarrow\rightarrow$ )



- ⊙ **Example 2-10:** A prismatic bar with  $L = 0.5$  m and  $A = 1,200$  mm<sup>2</sup> is compressed by an axial load  $P = 90$  kN. (a) Complete state of stress acting on section  $pq$  (angle  $\theta = 25^\circ$ ); (b) Bar fixed between supports  $A$  and  $B$  under temperature change  $\Delta T = 33^\circ\text{C}$ . The compressive shear stress on section  $rs$  is 65 MPa. Find the shear stress  $\tau_\theta$  on plane  $rs$ , and angle  $\theta$  ( $E = 110$  GPa,  $\alpha = 20 \times 10^{-6}/^\circ\text{C}$ )



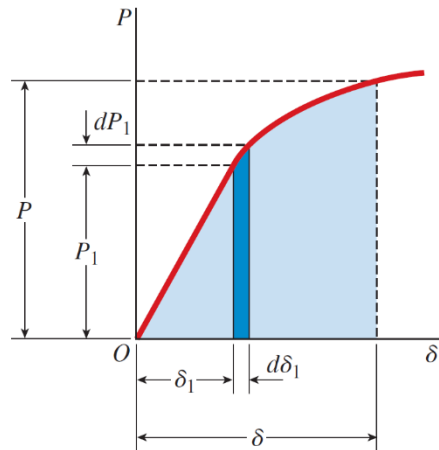
## 2.7 Strain Energy

### ⊙ Strain Energy

1. Suppose a tensile force  $P$  caused a prismatic bar to elongate by  $\delta$ . The work done by the force  $P$  is

$$W = \int_0^{\delta} P_1 d\delta$$

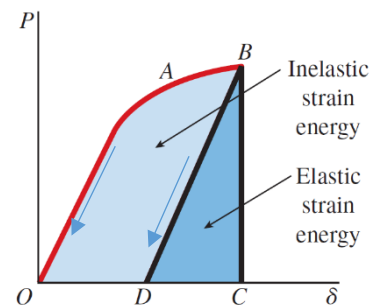
where  $P_1$  is the load at  $\delta = \delta_1$  in the load-displacement diagram ( $\rightarrow$ )



2. The strain caused by the work  $W$  increases the energy level (or the potential to do work) of the bar.
3. **Strain energy:** the energy absorbed by the bar during the loading process
4. From the principle of conservation of energy, the strain energy is

$$U = W = \int_0^{\delta} P_1 d\delta$$

5. Unit of strain energy: J = N · m, ft-lb, ft-kips, in.-lb, in.-k.
6. **Elastic strain energy:** energy recovered in the form of work during unloading

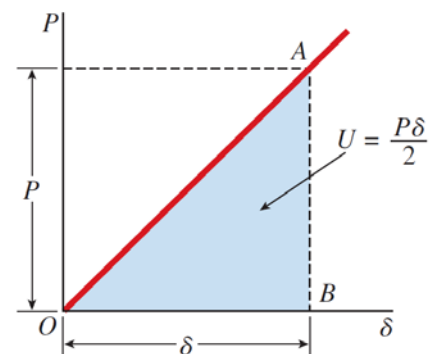


**Inelastic strain energy:** energy not recovered

### ⊙ Linearly Elastic Behavior

1. Strain energy:  $U = \text{---}$
2. Strain energy in terms of load or elongation (using force-displacement relation):

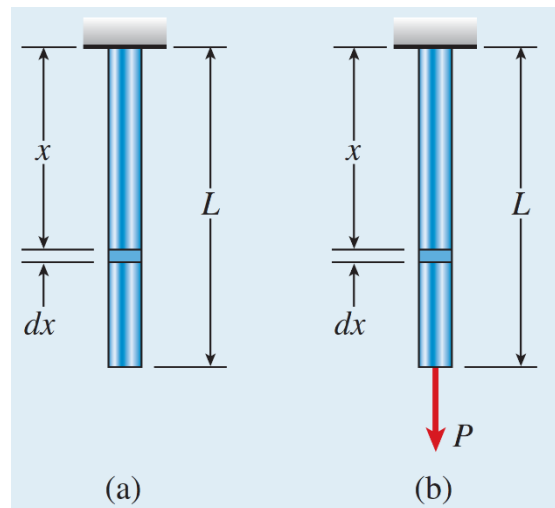
$$U = \text{---} \quad \text{or}$$



### ⊙ Nonuniform Bars

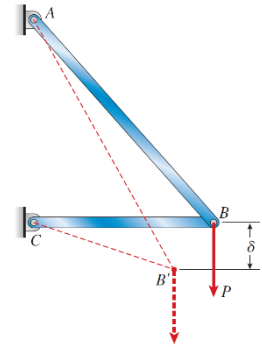
1. Prismatic bar segments:  $U = \sum_{i=1}^n U_i = \sum_{i=1}^n \frac{N_i^2 L_i}{2E_i A_i}$
2. Continuously varying bar:  $U = \int_0^L \frac{[N(x)]^2 dx}{2EA(x)}$

- ⊙ **Example 2-13:** Determine the strain energy of a prismatic bar under the loads: (a) the weight of the bar itself; and (b) the weight of the bar plus a load  $P$  at the lower end.



⊙ Displacements Caused by a Single Load

The displacement of a linearly elastic structure supporting only one load can be determined from its strain energy. From the system shown below,  $U = P\delta/2$ . Therefore, the displacement is  $\delta = 2U/P$ .



- ⊙ **Example 2-14:** Determine the vertical displacement  $\delta_B$  of joint B of the truss under the vertical load  $P$ . Both members of the truss have the same axial rigidity  $EA$ .

