

# **CHAPTER 3**

## **Noise in Amplitude Modulation Systems**

# NOISE

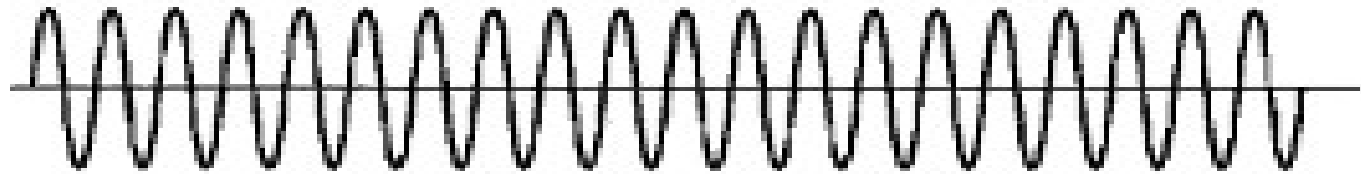
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## Review:

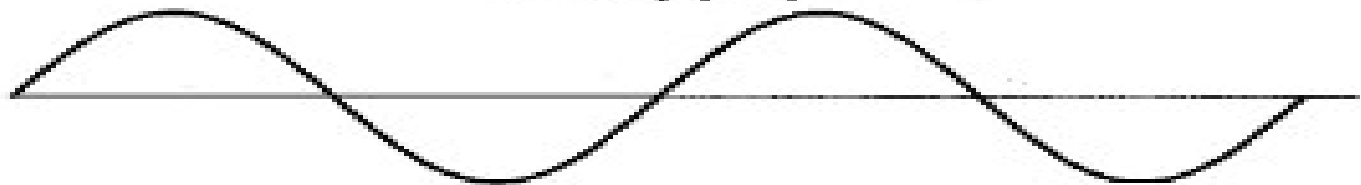
- **Types of Noise**
  - **External**  
(Atmospheric(sky), Solar(Cosmic), Hotspot)
  - **Internal(Shot, Thermal)**
- **Parameters of Noise**
  - Signal to Noise ratio
  - Noise Figure or Noise Factor
  - Effective Noise temperature
  - Noise Bandwidth
- **Narrow Band noise and its Components**

# Representation of AM Modulated signal

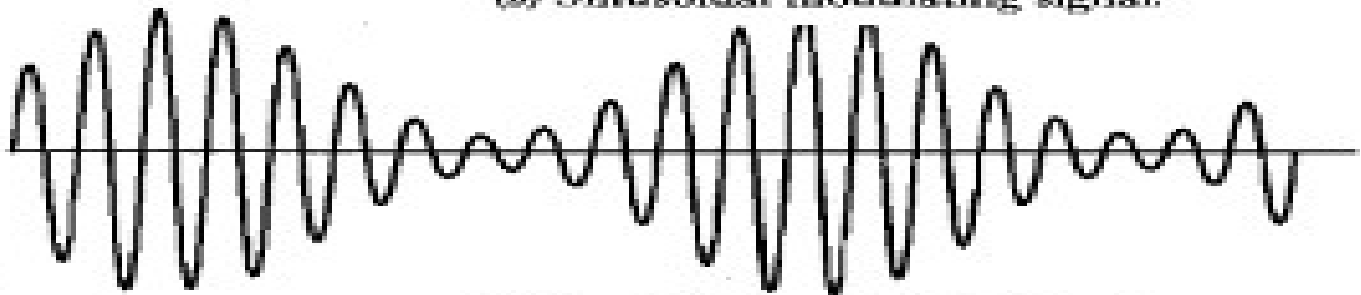
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(a) Carrier wave.

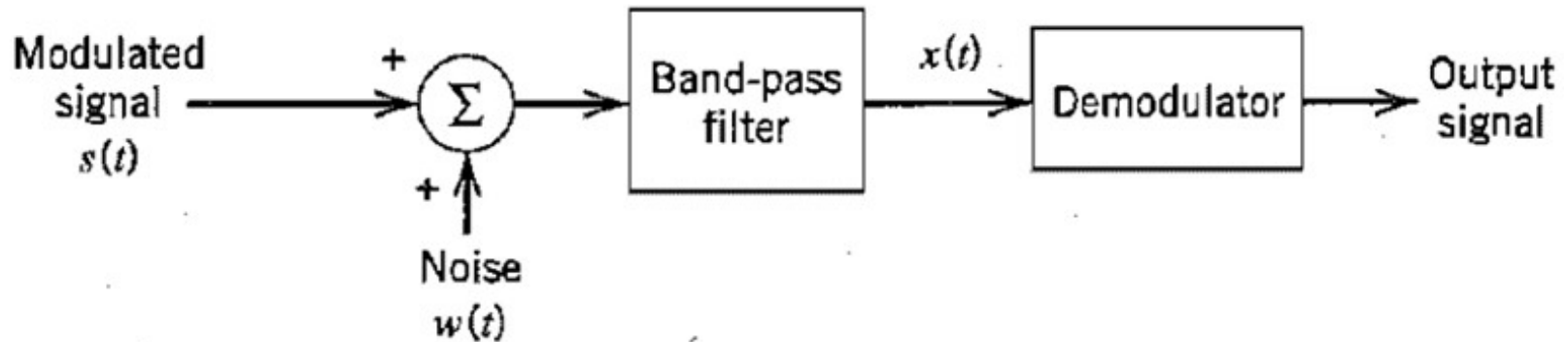


(b) Sinusoidal modulating signal.



(c) Amplitude-modulated signal.

# Noisy Receiver Model



- where the receiver noise is included in  $N_0$  given by:

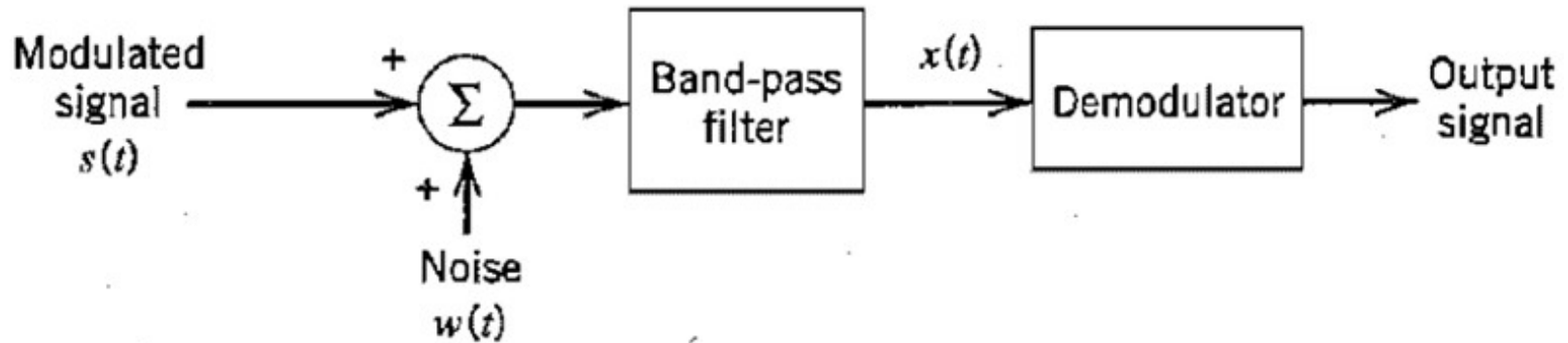
$$N_0 = kT_e$$

the bandwidth and center frequency of ideal band-pass channel filter are identical to the transmission bandwidth  $B_T$  and the center frequency of modulated waveform, respectively.

- The filtered noisy received signal  $x(t)$  available for demodulation is defined by:

$$x(t) = s(t) + n(t)$$

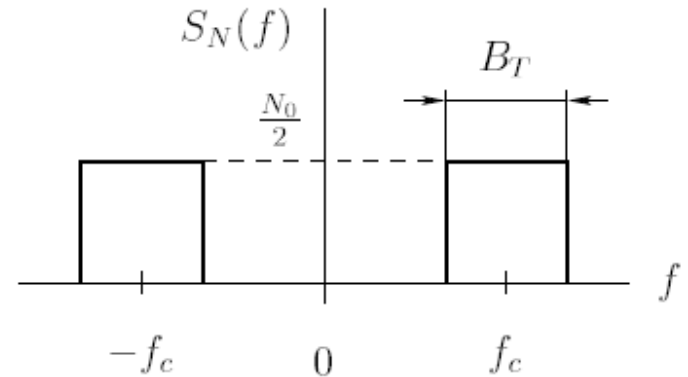
- Note: Noise  $n(t)$  is the band-pass filtered version of  $w(t)$



# Power spectral density (PSD) of band-pass filtered noise

$$S_N(f) = |H(f)|^2 S_W(f) = |H(f)|^2 \frac{N_0}{2}$$

where  $H(f)$  is the frequency response of channel filter and  $S_W(f)$  denotes the psd of white noise



- The *average noise power may be calculated from the power spectral density.*
- The average power  $N$  of filtered Gaussian white noise is:

$$N = \sigma^2 = 2 \frac{N_0}{2} B_T = N_0 B_T$$

# Signal to Noise Ratio (SNR)

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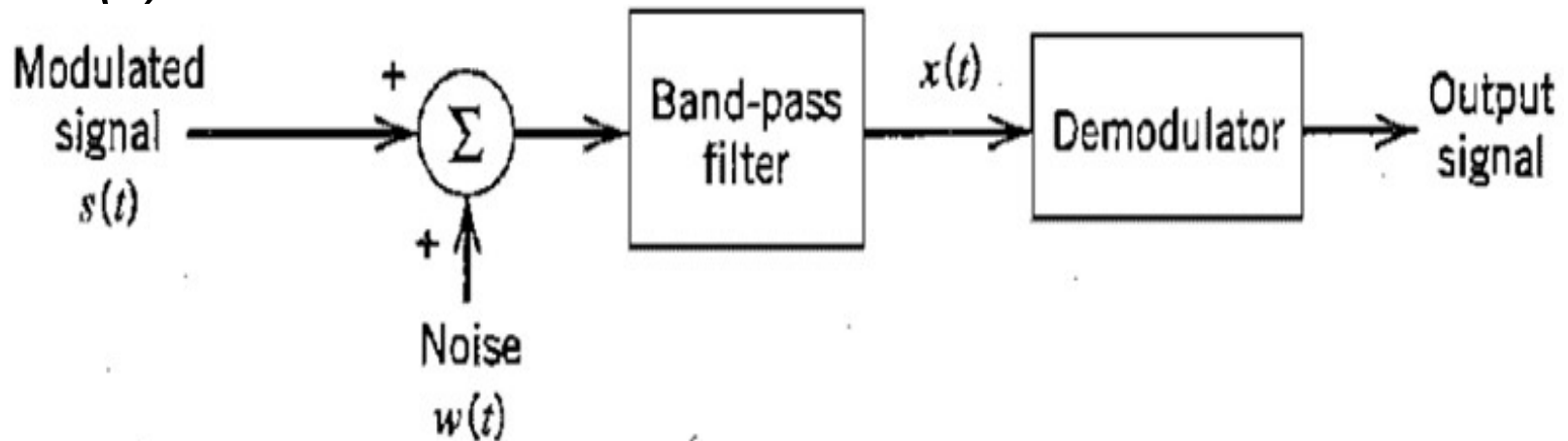
- A measure of the degree to which a signal is contaminated with *additive noise* is the ***signal-to-noise ratio (SNR)***

$$\text{SNR} = \frac{\text{average power of a signal } s(t)}{\text{average power of noise } n(t)} = \frac{S}{N}$$

# Figure of Merit Of CW Modulation Schemes

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- Signal-to-noise ratio (SNR) is a measure of the degree to which a signal is contaminated by noise.
- Assume that the only source of degradation in message signal quality is the additive noise  $w(t)$ .





- **The signal-to-noise ratio at the demodulator input:**

$$(SNR)_I = \frac{\text{average power of the modulated signal } s(t)}{\text{average power of noise } n(t)}$$

- **The**

$$(SNR)_O = \frac{\text{average power of the demodulated message signal } \hat{m}(t)}{\text{average power of noise } n(t)}$$

- *Under the condition that signal and noise appear additively at demodulator output. This condition is:*
  - *Always valid for coherent demodulators*
  - *But is valid for non-coherent demodulators only if the input signal to-noise ratio  $(SNR)_I$  is high enough*
- **Output signal-to-noise ratio  $(SNR)_O$  depends on:**
  - *Modulation scheme*
  - *Type of demodulator*

## Conditions of comparison

- To get a fair comparison of CW modulation schemes and receiver configurations, it must be made on an *equal basis*.
  - *Modulated signal  $s(t)$  transmitted by each modulation scheme has the same average power*
  - *Channel and receiver noise  $w(t)$  has the same average power measured in the message bandwidth  $W$*
- According to the equal basis, the **channel signal-to-noise ratio** is defined as:

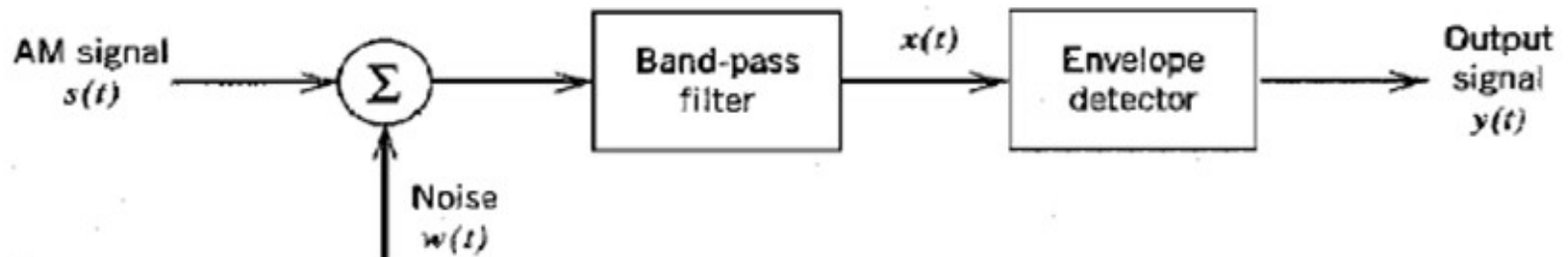
$$\begin{aligned}(\text{SNR})_C &= \frac{\text{average power of the modulated signal } s(t)}{\text{average power of noise in the message bandwidth}} \\ &= \frac{\text{average power of the modulated signal } s(t)}{N_0 W}\end{aligned}$$

- Noise performance of a given CW modulation scheme and a given type of demodulator is characterized by the ***figure of merit***.
- By definition, the figure of merit is:

$$\text{Figure of merit} = \frac{(\text{SNR})_O}{(\text{SNR})_C}$$

- The higher the value of the figure of merit, the better the noise performance

# Noise in AM DSB-FC Receivers



- *AM signal*

$$s(t) = A_C [1 + k_a m(t)] \cos(2\pi f_c t)$$

- Average signal power =  $A_C^2 (1 + k_a^2 P) / 2$

- Average noise power =  $WN_0 \leftarrow (2W \times \frac{N_0}{2})$

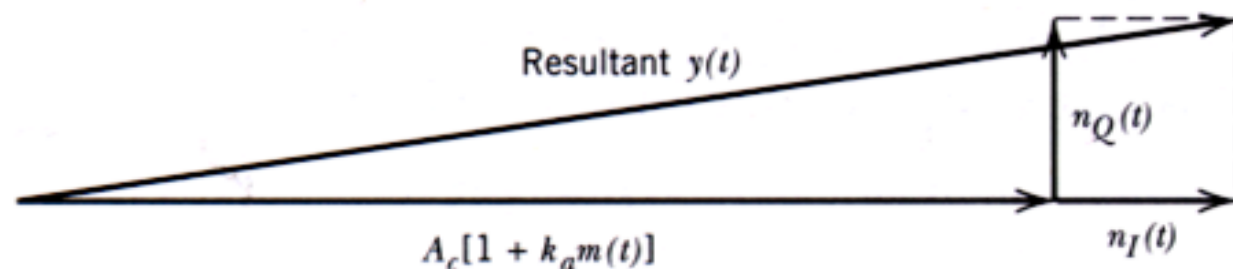
$$(\text{SNR})_{C,AM} = \frac{A_C^2 (1 + k_a^2 P)}{2WN_0}$$

- *Filtered signal*

$$x(t) = s(t) + n(t)$$

$$= [A_C + A_C k_a m(t) + n_I(t)] \cos(2\pi f_c t) - n_Q(t) \sin(2\pi f_c t)$$

$y(t) = \text{envelop of } x(t)$



$$= \left\{ \left[ A_c + A_c k_a m(t) + n_I(t) \right]^2 + n_Q^2(t) \right\}^{\frac{1}{2}}$$

Assume  $A_c [1 + k_a m(t)] \gg n_I(t), n_Q(t)$

$$y(t) \cong A_c + A_c k_a m(t) + n_I(t)$$

$$- (\text{SNR})_{o,AM} = \frac{A_c^2 k_a^2 P}{2W N_0}$$

$\left\{ \begin{array}{l} \text{Avg carrier power} > \text{Avg noise power} \\ k_a \leq 1 \end{array} \right.$

Figure of merit  $\frac{(\text{SNR})_o}{(\text{SNR})_c} \Big|_{AM} \cong \frac{k_a^2 P}{1 + k_a^2 P} < 1$

# Threshold effect

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- The ***threshold is a value of carrier-to-noise ratio below which*** the noise performance of a demodulator deteriorates much more rapidly than proportionately to the carrier-to-noise ratio.
- **Every noncoherent detector** exhibits a threshold effect, below the threshold the restored message signal becomes practically useless.

# Threshold effect

## Physical explanation:

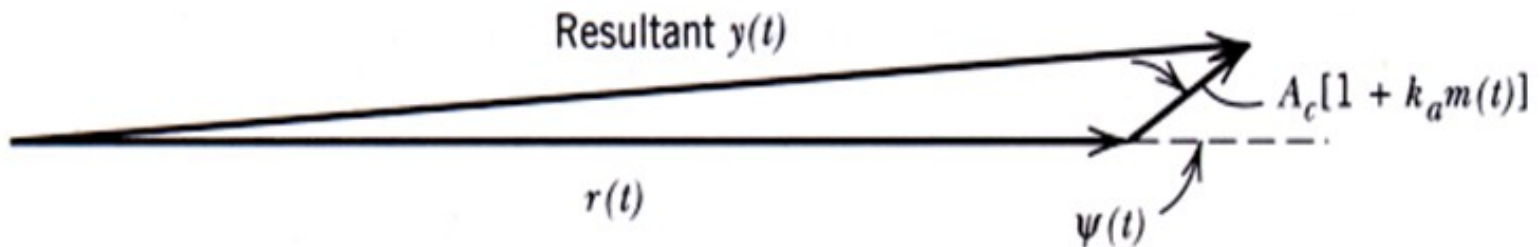
- **If the carrier-to-noise ratio is high enough** then the signal dominates and the noise causes only a small unwanted AM and PM.
- However, **if the carrier-to-noise ratio is small** then the noise dominates which results in a complete loss of information.
- As a result, **the demodulator output does not contain the message signal at all.**

$$n(t) = r(t)\cos[2\pi f_c(t) + \psi(t)]$$

where  $r(t)$  is envelope,  $\psi(t)$  is phase

$$x(t) = s(t) + n(t)$$

$$= A_c[1 + k_a m(t)]\cos(2\pi f_c t) + r(t)\cos(2\pi f_c t + \psi(t))$$



$$y(t) \cong r(t) + A_c[1 + k_a m(t)]\cos[\psi(t)]$$

$$\cong r(t) + A_c \cos[\psi(t)] + A_c k_a m(t)\cos[\psi(t)]$$

where  $\psi(t)$  is uniformly distributed over  $[0, 2\pi]$

⇒ complete loss of information

**Threshold Effect** : loss of message in an envelope detector that operates at a *low CNR*.



- Figure of merit for DSB modulation:

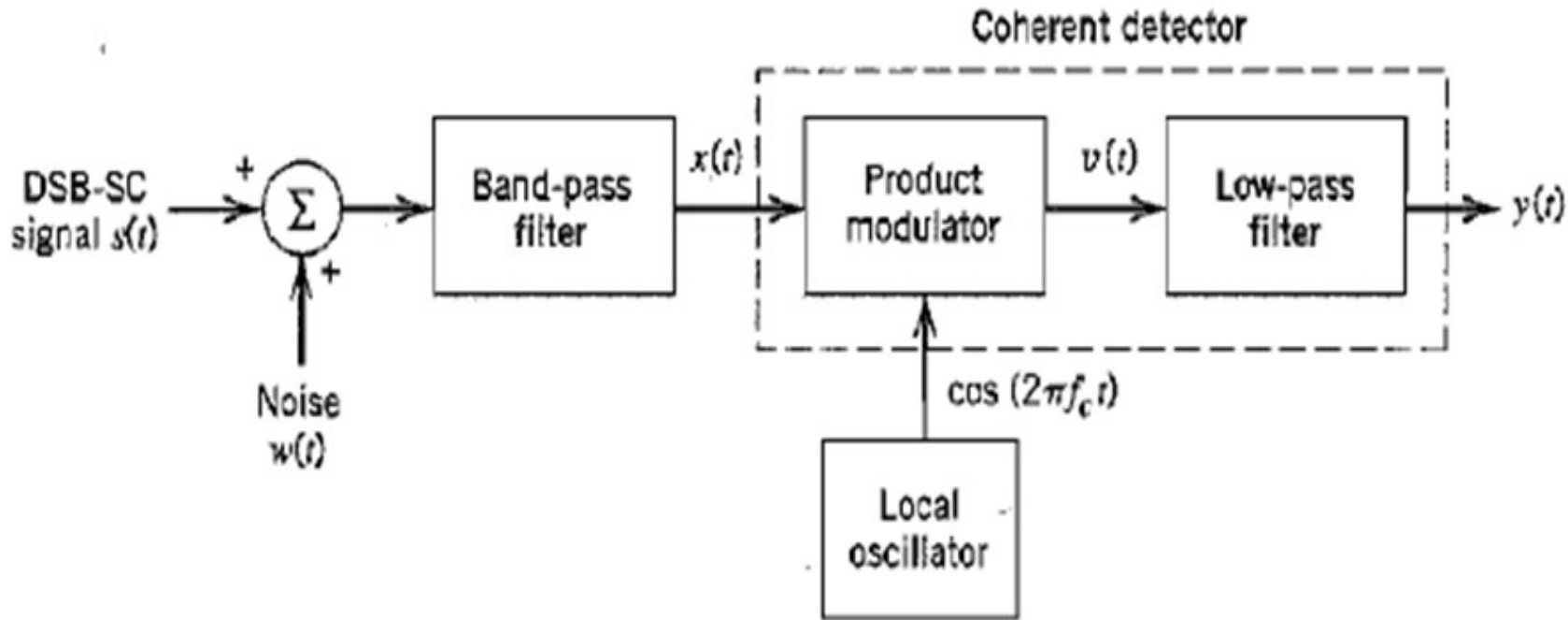
$$\text{Figure of merit} = \frac{(\text{SNR})_O}{(\text{SNR})_C} = \frac{k_a^2 P}{1 + k_a^2 P}$$

where ***P*** denotes the average power of message signal  $m(t)$  and ***k<sub>a</sub>*** is the ***amplitude sensitivity*** of AM modulator.

- The best figure of merit is achieved if the modulation factor is  **$\mu = k_a A_m = 1$**

- DSB SSB detection  
 $\text{Figure of merit} = \frac{\mu^2}{2 + \mu^2} = \frac{1}{3}$  must transmit three times as much average power as a suppressed-carrier system

# Noise in AM DSB-SC Receivers



-  $s(t) = CA_C \cos(2\pi f_c t)m(t)$

where  $C$  : scaling factor

Power spectral density of  $m(t)$  :  $S_M(f)$

$W$  : message bandwidth

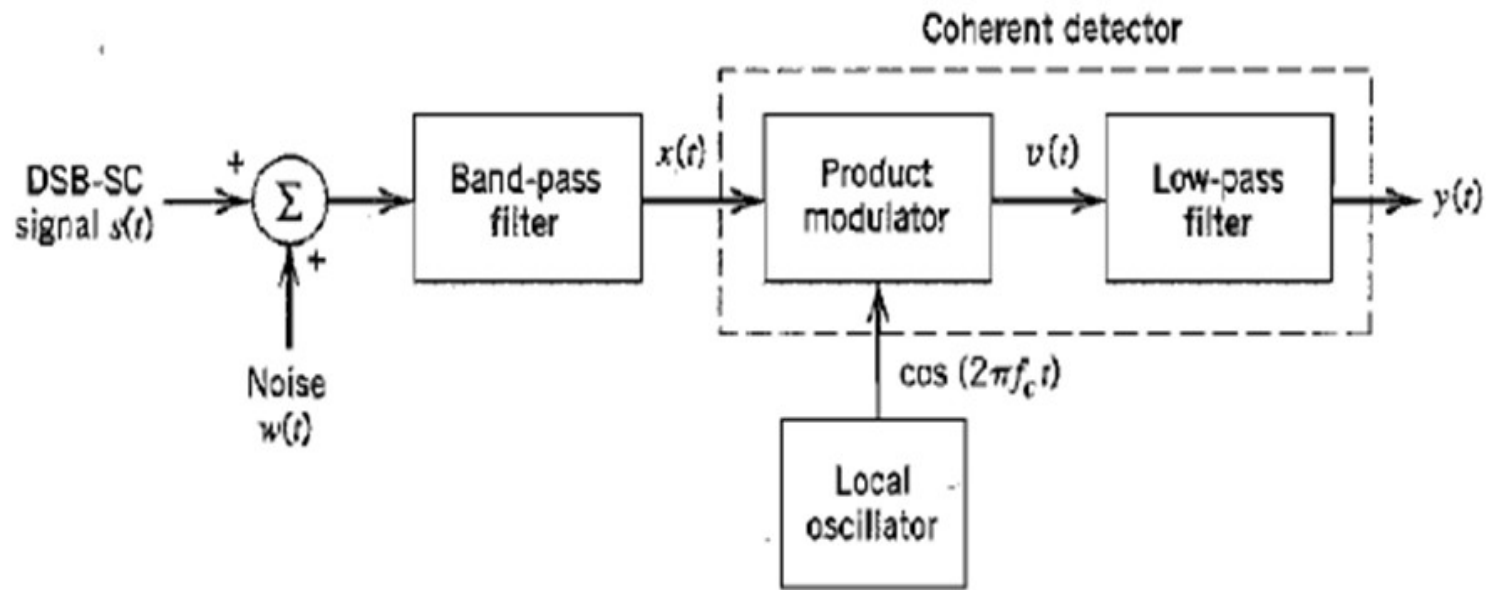
- Average signal power

$$P = \int_{-W}^W S_M(f) df$$

- Average power of  $s(t) = \frac{C^2 A_C^2 P}{2}$

- Average noise power =  $2W \times \frac{N_0}{2} = WN_0$   
(baseband)

-  $(\text{SNR})_{C, \text{DSB}} = \frac{C^2 A_C^2 P}{2WN_0}$



## Finding (SNR)<sub>o</sub>

$$\begin{aligned}
 - \quad x(t) &= s(t) + n(t) \\
 &= CA_c \cos(2\pi f_c t) m(t) + n_1(t) \cos(2\pi f_c t) - n_2(t) \sin(2\pi f_c t) \\
 - \quad v(t) &= x(t) \cos(2\pi f_c t) \\
 &= \frac{1}{2} CA_c m(t) + \frac{1}{2} n_1(t) + \frac{1}{2} [CA_c m(t) + n_1(t)] \cos(4\pi f_c t) - \frac{1}{2} A_c n_2(t) \sin(4\pi f_c t)
 \end{aligned}$$

$$\therefore y(t) = \frac{1}{2} CA_c m(t) + \frac{1}{2} n_1(t)$$

- Average signal power =  $\frac{C^2 A_C^2 P}{4}$

- Average noise power =  $\frac{1}{4}(2W)N_0 = \frac{1}{2}WN_0$  (passband)

$\therefore$  Power( $n_1(t)$ ) = Power of band pass filtered noise  $n(t) = 2WN_0$

-  $\therefore (SNR)_O = \frac{C^2 A_C^2 P / 4}{WN_0 / 2} = \frac{C^2 A_C^2 P}{2WN_0}$

$\therefore$  Figure of merit

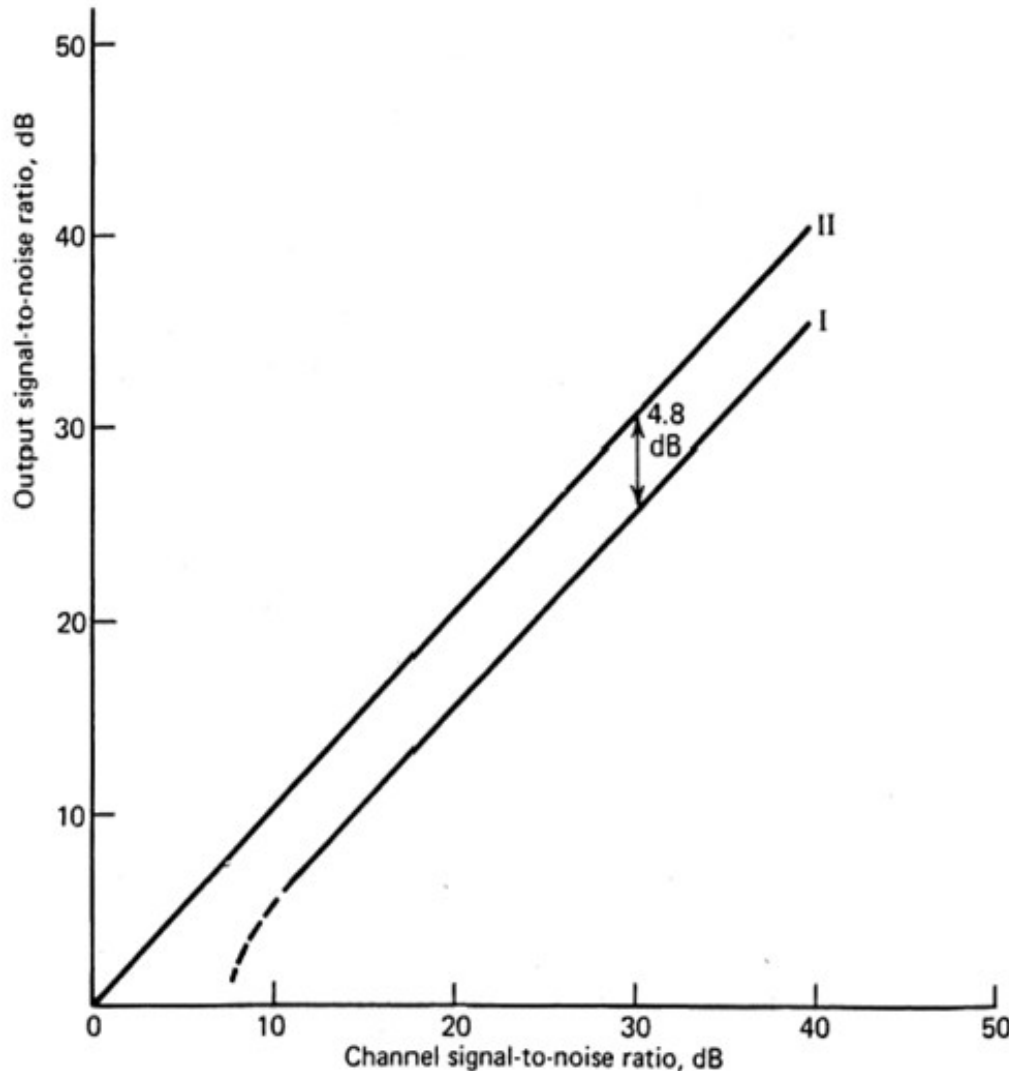
$$\frac{(SNR)_O}{(SNR)_C} \Big|_{DSB-SC} = 1$$

# Noise performance of AM receivers

		Type of demodulator			
		Coherent		Noncoherent	
		Figure of merit	Threshold effect	Figure of merit	Threshold effect
Type of CW modulation	DSB	$\frac{k_a^2 P}{1+k_a^2 P} \leq \frac{1}{3}$	no	$\frac{k_a^2 P}{1+k_a^2 P} \leq \frac{1}{3}$	yes
	DSB-SC	1	no	×	×
	SSB	1	no	×	×

**Note:** For high value of  $(\text{SNR})_c$ , *the noise performance of coherent and noncoherent DSB are identical. But noncoherent DSB has a threshold effect. Coherent AM detectors have no threshold effect!*

# Comparison of noise performance of AM modulation schemes



## Remarks

- **Curve I:** DSB modulation and envelope detector with modulation factor  $\mu = 1$
- **Curve II:** DSB-SC and SSB with coherent demodulator
- **Note the threshold effect that appears at about 10 dB**