68882 NHT3A-98-3.588-72 Crash Test Protocol Development for Fuel System Integrity Assessment

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Abstract

This report presents the basis, test description, and test results of a research project comprising rear impact crash tests of five passenger cars. The project's purpose was to study a potential upgrade to existing crash test protocols for motor vehicle fuel system integrity assessment. The research augmented previous National Highway Traffic Safety Administration tests by focusing on small U.S. passenger cars. The test configuration was a 80.5 km/h offset rear impact crash test using a moving deformable barrier. These tests were conducted by GM pursuant to an agreement between GM and U.S. Department of Transportation. The tests constituted Project B.5 under the Fire Safety Research section of that agreement.

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1. Background and Introduction

Motor vehicle post-collision fuel-fed fires are rare events, and those that result in a fatality are even less common. Current U.S. federal requirements for passenger motor vehicle fuel system integrity limit the allowable fuel spillage in specified frontal, side and rear impact crash tests. The U.S. Department of Transportation's (USDOT) National Highway Traffic Safety Administration (NHTSA) is evaluating a potential upgrade to these tests. The potential upgrade is a rear impact test different from the one presently incorporated in Federal Motor Vehicle Safety Standard 301, "Fuel System Integrity."

The current FMVSS 301 rear impact crash test is a 48.3 km/h, full overlap, collinear impact using an 1814 kg, flat-faced, rigid moving barrier. The rear impact test under development is a substantially higher energy crash test. It is an 80.5 km/hr, collinear impact engaging 70% of the vehicle's rear width. The impact barrier used in the test under development is an uncrabbed version of the 1368 kg crabbed moving deformable barrier specified for FMVSS 214, "Side Impact Protection," crash testing. Crabbed in this case designates a condition where the barrier wheels are aligned at an acute angle relative to the barrier's longitudinal axis (producing a type of sliding, angled impact motion). Uncrabbed designates the condition in which the barrier wheels are aligned parallel to the barrier's longitudinal axis.

Following an earlier testing phase examining rear impact test configuration differences, the NHTSA evaluated six different U.S. passenger vehicles using the new rear impact test [1]. Of those vehicles, the three larger ones met the fuel spillage limits of FMVSS 301 (the basic spillage rate limit by weight is 28 grams / minute), and the three smaller ones did not. Accordingly, the NHTSA decided that additional testing of small cars was warranted to help determine if the new test would be feasible and achievable as a federally mandated fuel system integrity test.

Consistent with the March 7, 1995 GM / USDOT Settlement Agreement, GM and the NHTSA agreed that the additional rear impact crash tests on small cars would be conducted by GM. Established under the Agreement were a number of Fire Safety Research projects. The project under which the work in this report was conducted was identified as Project B.5 - Development of Crash Test Protocols.

This report summarizes the test configuration basis and presents the test vehicle selection, test conditions, test setup, and test results of the five rear impact research crash tests which constitute Project B.5. A brief discussion and conclusions section also is included. Individual test reports for each test are listed as References [2] - [6]. Each report has been provided to the NHTSA, along with all of the test data, films and photographs [7]. The GM tests were conducted on 1998 Model Year (M.Y.) small U.S. passenger cars during December 1997 and January 1998 at GM's Proving Ground in Milford, Michigan.

2. Test Configuration Basis

The NHTSA selected the test configuration for the Project B.5 tests. The configuration developed from a NHTSA case study of fatal motor vehicle crashes involving fire [8]. A case study approach was used because none of the existing fatal crash databases provided sufficient information to establish the impact configuration or the cause of the fatality (e.g.,

impact trauma vs. burn trauma). Sixteen (16) rear impact field collision cases with 30 fatalities were found out of 45 cases (65 fatalities) in which the fatalities were judged to be due to fire. Impact speed was determined for 8 of the 16 cases.

When NHTSA conducted its six tests [1], it chose a specific, consistent test protocol (impact speed, overlap, barrier, etc.) reflecting the results from its case study and the earlier similar tests it had conducted. The test protocol and conditions used in the GM tests were chosen to match, as close as practicable, the protocol and nominal targeted conditions from the six NHTSA tests. The impact speed was agreed to be 80.5 km/h (50 mph).

3. Test Configuration and Test Conditions

Figure 1 illustrates the test configuration. The stationary target vehicle is struck in its rear by the moving deformable barrier. Nominal impact speed is 80.5 km/h and the impact is collinear. Barrier overlap with 70% of the car's rear is established toward the fuel filler side of the car.

Figure 1 - Test Configuration



The impactor for the GM tests was a modified version of the 1368 kg FMVSS 214 dynamic side impact crabbed moving deformable barrier (Appendix A) [9, 10]. It was adjusted to an uncrabbed configuration for collinear impact. Barrier face construction consisted of the normal FMVSS 214 aluminum honeycomb blocks and aluminum faces. However, barrier face height for the new rear impact test was lowered 51 mm from the FMVSS 214-specified height. This modification was determined by NHTSA to represent rear impacts with pre-impact braking. Specifically, it represented the dip at the front bumper or rise at the rear bumper based on average vehicle pitch due to panic braking.

There were some differences between the moving barrier carriage used in the GM tests and the one used in the NHTSA tests. First, GM used an available carriage similar to the FMVSS 214 carriage but which previously had been adapted to allow barrier face height adjustment. The GM carriage had a taller barrier face mounting plate and taller vertical supports behind the barrier face (see the photos in Appendix A). Second, GM's barrier did not incorporate load cells. The barrier that NHTSA used in its tests incorporated five load cells, which are not part of the FMVSS 214 barrier. Even with these differences, the weight of the GM barrier (1371 kg) was comparable to the barrier used in the NHTSA tests (1337 – 1344 kg).

It is not known what effect resulted from the slightly different barrier carriage GM used compared with the barrier carriage used in the NHTSA tests. Review of the crash test films from the GM tests indicated some interaction of the vehicle deck lid with the taller portions of the GM barrier assembly. The interaction was relatively late in the impact event. For this

reason, it is believed that a relatively small percentage of the impact loading was carried through those portions of the test car that were contacted by the taller portions of the GM barrier assembly.

4. Test Vehicle Selection and Description

Approved funding for this research project was provided for five crash tests. Accordingly, five 1998 M.Y. small U.S. passenger cars were selected based on the following criteria agreed between the NHTSA and GM:

- 1. Projected 1998 M.Y. small car market segment sales leaders with 100,000 or more units sold (including "sister" cars)
- 2. Curb weight under 3000 pounds
- 3. Car or its "sister" car had not been tested previously in the NHTSA tests
- 4. No more than one car in the selected group from a single manufacturer.

These criteria were intended to aid selection of a reasonable assortment of small cars to test.

Complete 1997 M.Y. sales data were not available at the time test vehicle selection was required (July 1997). Therefore, based on criteria numbers 1 and 2, the following group of cars were identified from the 1996 calendar year small car market segment sales reported by Ward's Automotive Reports, January 20, 1997:

- 1. Chevrolet Cavalier (Pontiac Sunfire)
- 2. Ford Escort
- 3. Saturn
- 4. Honda Civic
- 5. Toyota Corolla
- 6. Dodge/Plymouth Neon
- 7. Nissan Sentra
- 8. Volkswagen Jetta (Golf)

The Corolla was not selected, based on criterion number 3, because it was considered a "sister" car to the Geo Prizm, which NHTSA already had tested. Similarly, the Neon was not selected because it, too, already has been tested by the NHTSA. The Saturn was not selected, based on criterion number 4, because the Cavalier (also manufactured by GM) was selected. The Cavalier selection was based on higher combined sales of the Cavalier/Sunfire line compared to the Saturn line, and higher Cavalier sales compared to the Sunfire.

Accordingly, the five selected test cars were the 1998 Chevrolet Cavalier, Ford Escort, Honda Civic, Nissan Sentra and Volkswagen Jetta. For consistency, only the 4-door models of these cars were chosen (some only were available as 4-door models). The 4-door models generally had higher sales volumes than their 2-door versions (if available), based on the 1996 calendar year data.

The test cars were new and similarly equipped. Each car was ordered with factory equipment expected to be on a large percentage of these models. All had 4-cylinder engines, air conditioning and an automatic transmission except the Jetta, which had a manual transmission.

These equipment choices reflected the best-selling factory-installed equipment / option for the identified feature in each car based on data in the 1997 Wards Automotive Yearbook (for 1996 M.Y. cars). Representative pre-test photographs of each car, along with the car's Vehicle Identification Number (VIN), are provided in Appendix B.

For reference, Table 1 provides the locations of significant fuel system components for each car.

	Fuel Tank	Filler Neck	Fuel Line Path to Front
Honda Civic	Between and forward of rear wheels	Left rear quarter	Left center underbody
Ford Escort	Forward of rear wheels	L eft rear quarter	Left center underbody
Volkswagen Jetta	Between rear wheels	Right rear quarter	Right center underbody
Nissan Sentra	Forward of rear wheels	Left rear quarter	Left center underbody
Chevrolet Cavalier	Between and forward of rear wheels	Right rear quarter	Left center underbody

Table 1 - Fuel Tank, Filler Neck and Fuel Line Locations(Cars listed in order tested)

5. Vehicle Preparation

Each test car initially was prepared generally as it would be for an FMVSS 301 rear impact test. This included establishing the test mass and the fuel system fill level.

The target test mass (kg) was established using a procedure similar to that described in the reports of the NHTSA tests, and outlined below:

RCLW UDW VCW ^a DSC	 Rated Cargo and Luggage Weight = VCW - (68 x DSC) Unloaded Delivered Weight Vehicle Capacity Weight Designated Seating Capacity
Target te	st mass = UDW + RCLW + (2 test dummies x 90 kg / dummy ^b)
^a From ca ^b Hybrid I	n's tire load label Il 50th % adult male (highly instrumented, including cables).

Actual test mass (Table 2) was established as close as practical to the target mass.

Pre-test vehicle attitude measurements are shown in Table 3.

Fuel tank usable capacity was determined from the car's manufacturer or the owners manual. The 93% Stoddard solvent fill level, added to the unusable level in the tank, was consistent with that used in the NHTSA tests. It is the center of the range (90-95%) specified in FMVSS 301. Fuel tank fill data for each test car are shown in Table 4. As in FMVSS 301 tests, the engine of the test car was cranked for a few seconds (the ignition was moved to the "START" position) pre-test to distribute Stoddard fluid throughout the fuel system.

	Test No.	As Received Mass Front / Rear Totai (kg)	Target Test Mass Front / Rear Total (kg)*	Actual Test Mass Front / Rear Total (kg)*
Civic	C11817	676 / 404 1080	818 / 488 1306	827 / 527 1354
Escort	C11818	730 / 430 1160	867 / 509 1376	882 / 503 1385
Jetta	C11816	730 / 456 1186	850 / 567 1417	853 / 576 1429
Sentra	C11828	697 / 394 1093	781 / 521 1302	831 / 513 1344
Cavalier	C11829	794 / 418 1212	871 / 581 1452	924 / 544 1468

Table 2 - Vehicle Test Mass

• including two instrumented test dummies (90 kg each)

	Test Attitude			
	LF	RF	LRr	Rn
	(mm) *			
Civic	160	160	170	170
Escort	200	200	210	210
Jetta	175	175	190	190
Sentra	205	205	220	220
Cavalier	220	225	225	225
* measured vertically from rocker to ground				

Table 3 - Pre-test Vehicle Attitude

(L = left, R = right, F = front. Rr = rear)

Table 4 - Fuel Tank Fill Data

	Fuel Tank Usable Capacity (L)	Stoddard Solvent Added to Fuel Tank (L) *
Civic	45.0	41.8
Escort	48.1	44.7
Jetta	55.0	51.2
Sentra	50.0	46.5
Cavalier	57.5	53.5

* 93% of usable capacity (added to unusable capacity)

Additional vehicle preparation highlights are listed below:

- The standard equipment spare tire was in its normal stowed position for all tests.

- Each test car, and the moving barrier, was instrumented with accelerometers at various locations. See Section 7 of this report for additional information.

- Underbody components, especially fuel system components, were painted with contrasting colors for film coverage purposes.

- Camera mounts were attached to the front doors of each car to record test dummy motions. The camera and mount on the rear door of the Civic (the first test) were deleted for the subsequent test vehicles. Visual inspection of the Civic post-test indicated that the right rear door was a load path during the impact event (as was the left rear door). This was evidenced by the crush damage that door exhibited. The camera mount on the door may have limited the crush in this area. However, the influence of the mount could not be quantified. To avoid this potential non-representative effect on the subsequent tests, the rear door camera and mount were not used.

6. Test Preparation and Test Procedure

The tests were conducted as close as practicable to the procedures outlined in the test reports for the NHTSA tests and specified in FMVSS 301. Overlap was determined by lateral measurement at the widest point of the car's body vertically in line with the center of the rear wheels.

An instrumented Hybrid III 50th percentile adult male anthropomorphic test device (ATD, or alternatively referred to as test dummy) was positioned in the driver and right front passenger seating positions. FMVSS 208 ("Occupant Crash Protection") positioning procedures (mid fore-aft seat track position, etc.) were used. Each dummy was restrained by the standard equipment 3-point lap and shoulder belt at its seating position. Test dummy instrumentation is described in the next section of this report.

The test vehicle's brakes were not engaged initially and its transmission was in neutral. To retard the vehicle's post-impact motion, the test vehicle's brakes were activated using an auxiliary source approximately 250-300 msec after impact time-zero. The moving barrier motion was also retarded approximately 250 msec after impact time-zero.

Impact speed was measured with radar equipment.

The crash event was recorded by high-speed motion picture cameras as described in Section 7 of this report.

A total of 92 data channels were recorded for each test as follows:

- 39 on each test car
- 26 on the driver test dummy
- ~ 21 on the passenger test dummy
- 6 on the moving barrier.

Section 7 of this report provides additional instrumentation information.

A post-test static roll-over test was conducted according to FMVSS 301 practices following the Civic, Escort and Sentra impact tests. The roll-over test was not conducted following the Jetta and Cavalier impact tests. This decision for the Jetta and Cavalier was based on the need to drain the fuel tank quickly post-test at the impact site to reduce the clean-up task associated with the amount of Stoddard which spilled from the tank.

7. Instrumentation and Camera Coverage

Each test car was instrumented to make the following measurements:

- Center front radiator tie bar 3-axis accelerations
- Upper engine 3-axis accelerations
- Left and right front seat outboard mounting rail 3-axis accelerations
- Left and right front seat back 3-axis accelerations
- Left and right front rocker 3-axis accelerations
- Left and right rear rocker 3-axis accelerations
- Center rear seatback close-out panel 3-axis accelerations
- Left and right rear frame rail 3-axis accelerations.

The moving barrier was instrumented to make the following measurements:

- center of gravity 3-axis accelerations
- rear cross member 3-axis accelerations.

Each test dummy was instrumented to make the following measurements for injury assessment purposes:

- Head 3-axis accelerations
- Thorax (chest) 3-axis accelerations
- Head/neck interface (upper neck):
 - longitudinal shear force (Fx) lateral shear force (Fy) axial force (Fz)
 - axial loice (FZ)
 - moments about longitudinal, lateral and vertical axes (Mx, My, Mz)
- Neck/torso interface (lower neck) driver dummy only:
 - longitudinal shear force (Fx) lateral shear force (Fy) axial force (Fz) moments about longitudinal, lateral and vertical axes (Mx, My, Mz)

- Chest (sternum) compressive displacement
- Lower lumbar:

longitudinal shear force (Fx) axial force (Fz) moment about lateral axis (My)

- Pelvis 3-axis accelerations
- Femur axial loads, left and right femurs,

Real-time and high-speed motion picture cameras were used to film each test. Cameras were located as illustrated in Figure 2. Post-test conditions and the post-test static roll-over tests were documented by video camera.

Still photographs also were taken to document the pre- and post-test conditions of each test.



Figure 2 - High-speed Motion Picture Camera Locations

- 1.2 Overall side view
- 3, 4 Rear half side view

 - 7 Rear half overhead offboard
 - 8 Driver rearward motion onboard
- 13 Underbody fuel tank area in pit

8. Test Results

Fuel System Integrity

Fuel system integrity test results are summarized in Table 5. Additional details are provided in the paragraphs below. Representative post-test photographs are provided in Appendix C. For reference, the relevant FMVSS 301 Stoddard fluid fuel system spillage limits by weight are: 28 grams / minute and 142 grams / 5 minutes.

<u>Civic</u> - There was no fuel system fluid spillage from the car during or after the impact test or during the two subsequent quasi-static roll-over tests. The car was rolled in both the clockwise and counterclockwise directions about its longitudinal axis.

<u>Escort</u> - A trace amount (0.3 gram) constituting a few drops of Stoddard fluid dripped from the vehicle during the 30 minutes after impact. The source of the spillage could not be confirmed at the impact test site.

During the first 90-degree quadrant of the post-test quasi-static roll-over test (the fuel filler neck side of the car was rolled downward first), an amount of Stoddard fluid noticeably exceeding 142 grams spilled from the fuel filler cap area in the first 5 minutes. Due to this result, the remaining roll-over testing was terminated. Inspection revealed that the fuel filler cap exterior had fractured off, and the top end of the filler neck had deformed. The plastic "plug" or sealing portion of the cap remained in the filler neck. However, a portion of the plug periphery appeared to have deformed and partially fractured during the impact test, allowing the spillage during the roll-over test. This result appeared to have been caused by the local deformation and crash forces in the fuel filler area.

<u>Jetta</u> - During the first 5 minutes after impact, at least 421 grams of Stoddard fluid spilled from the vehicle. The spillage source appeared to be from somewhere on the top of the fuel tank. The fuel tank top was not visible or accessible at the impact site due to the impact deformation of the car.

Due to the amount of fluid spillage at the impact test site, and the need to quickly drain the fuel tank to reduce the site clean-up task, it was decided not to conduct the quasi-static roll-over test. Instead, a post-test inspection and partial disassembly of the test car were conducted to reveal the site of the fluid spillage. Many of the vehicle components in the rear of the vehicle (suspension, wheels, etc.) had to be removed (some cut away) to extricate the plastic fuel tank in order to inspect its top. Additionally, the tank had to be cut away from its integral filler neck to remove the tank from the vehicle.

Inspection revealed a fracture (hairline type crack) in the fuel sender unit plastic sealing plate on the tank top side. The fracture was at the base of the attachment of the sender unit electrical connector to the sealing plate. This fracture site was confirmed by partially refilling the tank, inverting it, and observing the Stoddard fluid leakage through the crack. It appeared that crash forces exerted by contact of the connector/attachment with the floor pan may have caused the fracture.

<u>Sentra</u> - There was no fuel system fluid spillage during the 30 minutes after the impact test. There also was no spillage during the first quasi-static roll-over test which placed the fuel filler side (left side) of the car downward during the first quadrant of the roll.

Similarly, no spillage occurred during the first two quadrants of the second quasi-static roll-over test. However, during the 3rd quadrant of this roll-over (the fuel filler side of the car was downward during this quadrant), a trace amount (a few drops, substantially less than 28 grams) of Stoddard fluid spillage was observed. The spillage came from the vent tubing which had become disconnected from the vapor canister due to the crash forces. The vapor canister was located on the car's left side outboard of the spare tire tub.

<u>Cavalier</u> - During the first 5 minutes after impact, at least 450 grams of Stoddard fluid spilled from the vehicle. The spillage came from a cut in the fuel tank. The deformed right rear underside of the tank had been penetrated by a protruding edge (from crash deformation) of the intruding right side rear suspension trailing arm bracket.

Due to the amount of fluid spillage at the impact test site, and the need to quickly drain the fuel tank to reduce the site clean-up task, the quasi-static rollover tests were not conducted for the Cavalier. A post-test inspection confirmed the tank fuel spillage location and cause.

Impact Test Stoddard Spillage Roll-over Test Stoddard Impact Speed Test Dummy Data Spillage (km/h) Civic 80.7 None All < IARVs* None 80.9 > FMVSS 301 limits RF HIC > IARV Escort Trace** Fractured fuel filler cap seal All others < IARVs 81.2 > FMVSS 301 limits No roll-over conducted All < IARVs Jetta Fractured fuel sender seal plate All < IARVs Sentra 81.0 None Trace** RF HIC > IARV 81.0 Cavalier > FMVSS 301 limits No roll-over conducted RF Nk. Ext. > IARV Cut in fuel tank All others < IARVs

Table 5 - Fuel System and Injury Measurements Performance Results Summary

* IARV = Iniury Assessment Reference Value

** Trace = a few drops (<< 28 grams)

Front Seat Test Dummy Injury Measurements

Table 5 also summarizes the front seat test dummy injury measurement results. Data plots for the head and neck injury measurements are provided in Appendix D -- no other injury criteria limits except for the head and neck were exceeded in any of the Project B.5 tests conducted by GM. Additional details are provided in the following paragraphs.

<u>Civic</u> - None of the Injury Assessment Reference Values (IARVs) described in Appendix E were exceeded for either front seat test dummy.

<u>Escort</u> - The right front passenger test dummy head injury criteria, or HIC (1370), exceeded the IARV (1000). The rear of the dummy's head contacted the intruding right side rear seat back during the time interval of this maximum HIC measurement. No other IARVs were exceeded for the driver and passenger test dummies.

Jetta - None of the IARVs were exceeded for either front seat test dummy.

Sentra - None of the IARVs were exceeded for either front seat test dummy

<u>Cavalier</u> - The right front passenger HIC exceeded the IARV (1000) by an unknown amount. The dummy head longitudinal acceleration data channel exceeded its full scale value (approximately 150 g) during the time interval in which the rear of the dummy's head contacted the intruding rear seat back and rear package shelf. The right front dummy neck extension moment (103 N•m) also exceeded the IARV (57 N•m). No other IARVs were exceeded for either dummy.

Test Vehicle Velocity Change and Residual Crush

Table 6 summarizes two measurements illustrating the crush performance for each test car. The first is the longitudinal velocity change (delta V) the car experienced. The delta V was obtained by integrating the car's longitudinal acceleration measured at the front rocker on the side opposite to the impact overlap side. Corresponding data plots are provided in Appendix F. The second measurement is the residual crush or difference between the pre-test and post-test static longitudinal reference measurements made on the vehicle.

	Car Delta V (km/h)	Car Residual Crush	
	. ,	Driver I Passenger Sides (mm)	
Civic	41.5	1190 / 465	
Escort	40.5	1030 / 495	
Jetta	40.4	490 990	
Sentra	42.8	970 / 465	
Cavalier	40.2	640 / 1250	

Table 6 - Deita V and Crush Results

9. Discussion and Conclusions

This new rear impact test constitutes a substantial initial impact energy increase over the existing FMVSS 301 rear impact test (Figure 3). Initial impact energy (the kinetic energy of the moving barrier) is approximately twice that of the FMVSS 301 test¹. In this new test, the kinetic energy of the moving barrier primarily is dissipated by the crush of the test vehicle and the deformable element barrier. In the existing FMVSS 301 rear impact test, the kinetic energy primarily is dissipated by the crush of the test, the kinetic energy primarily is dissipated by the crush of the test, the kinetic energy primarily is dissipated by the crush of the test, the kinetic energy primarily is dissipated by the crush of the test vehicle.

¹ Initial K.E. = $1/2(m)(v)^2$; m and v are the mass and impact velocity, respectively, of the moving barrier. Accordingly, K.E._{new} / K.E.₃₀₁ = $(m_{new} / m_{301})(v_{new} / v_{301})^2 = (1368 / 1814)(80.5 / 48.3)^2 = 2.1.$



Fuel system integrity performance was mixed among the cars in the GM tests, but two of the cars performed reasonably well in this regard. No measure of performance repeatability was available because only one test of each car was conducted.

The potential for occupant injury induced by crash forces in these tests cannot be established from the results of the Project B.5 tests. However, the tests provided some qualitative insight regarding that potential. For example, the front seat test dummy head or neck injury measurement data in two of the Project B.5 tests were above injury assessment reference levels described in Appendix E. Representativeness (biofidelity) of some of the injury measurements has been debated regarding use of the Hybrid III 50th-percentile adult male test dummy in rear impact tests. However, some researchers [12] have found that this test dummy is suitable for rear impact testing. Also, there was noticeable reduction of the rear seat occupant space in the Project B.5 tests. Qualitatively, this space often is associated with rear occupant injury or survivability potential.

Accordingly, even if all small cars could be developed to meet fuel system performance requirements in a repeatable fashion during this test, taken together, the results and observations from the Project B.5 tests suggest that further study may be appropriate regarding what level of crash-induced injury occupants would experience in this type of crash.

References

- 1. Ragland, Carl L., NHTSA, "Research Tests to Develop Improved FMVSS 301 Rear Impact Test Procedure," paper no. 98-S4-P-16, 16th International Conference on the Enhanced Safety of Vehicles, Windsor, Ontario, Canada, May 31 - June 4, 1998
- 2. GM Test Report No. PG-68269, Test No. C11817, 1998 Honda Civic 4-door
- 3. GM Test Report No. PG-68270, Test No. C11818, 1998 For Escort 4-door
- 4. GM Test Report No. PG-68351, Test No. C11816, 1998 Volkswagen Jetta 4-door
- 5. GM Test Report No. PG-68353, Test No. C11828, 1998 Nissan Sentra 4-door
- 6. GM Test Report No. PG-68354, Test No. C11829, 1998 Chevrolet Cavalier 4-door
- 7. June 26, 1998 letter from David A. Collins (GM) to Philip R. Recht (NHTSA) transmitting test report, test data, video and photographs from the five tests conducted under Project B.5.
- Ragland, Carl L., Hsia, Hsi-Sheng, NHTSA, "A Case Study of 214 Fatal Crashes Involving Fire," paper no. 98-S4-O-08, 16th International Conference on the Enhanced Safety of Vehicles, Windsor, Ontario, Canada, May 31 - June 4, 1998
- 9. Title 49 Code of Federal Regulations, Part 571.214, Side Impact Protection (FMVSS 214)
- 10. Title 49 Code of Federal Regulations, Part 587, Side Impact Moving Deformable Barrier
- 11. AGARD Report AR-330, "Anthropomorphic Dummies for Crash and Escape System Testing," Advisory Group for Aerospace Research and Development, Neuilly-Sur Seine, France, July 1996.
- 12. Prasad, P., et al, "Biofidelity of Anthropomorphic Test Devices for Rear Impact," SAE Technical Paper No. 973342.
- 13. Melvin, J.W., "Lumbar Spine Injury Assessment Values for 50th Percentile Male and 5th Percentile Female Dummies," General Motors Corporation research paper, January, 1988.

Appendix A

Moving Deformable Barrier

FEDERAL SAFETY STANDARDS

MOTOR VEHICLE SAFETY STANDARD No. **214** SIDE IMPACT PROTECTION -PASSENGER CARS, TRUCKS, BUSES & MULTIPURPOSE PASSENGER VEHICLES WITH A **GVWR** OF **10,000** POUNDS OR LESS





Project B.5 Moving Deformable Barrier



FMVSS 214 Moving Deformable Barrier

Appendix B

Representative Pre-test Photographs











Appendix C

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Representative Post-test Photographs











1998 Ford Escort

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Appendix D

Head and Neck Injury Measurement Data Plots



C11817 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 8W9185D 4-DOOR SC ELEC DATA, SAE CLASS 1000

L, FRT HEAD ACCEL. (HIC I LIMITED TO 36MS) 80.7KM/H ATO TYPE: GM50H TEST DATE: 12/18/1997

RESULTANT ACCELEARTION-C'S 3 HS CON ACC. MAXIMUM HIC (11 INO - 790 0 80.5 5: 110 - 123 MS FH0 AFT ×0.0 U 50 COMPONENT ACCELERATIONS. 100 5 RIGHT 0.0 50 100 50 5 DOHN ~0.0 UP SOULUNIU 200 160 180 220 100 120 14D TIME IN MILLISECONDS 1 PROCESSED 12/18/1997 14:15 V2.07

C11817 L.REAR IMP 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 8W91850 4-000A SC ELEC DATA, SAE CLASS 1000

L, FRT HEAD ACCEL. (HIC I LIMITED TO 15MS) 80.7KM/H ATO TYPE: CM50H TEST DATE: 12/18/1997

- 6*5

- 185 -

MAX RECEL = 127 G'S AT 110.9 MS

CI1817 L. REAR I M P 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 80.7KM/H 8W9185D 4-DOOR L. FRT NECK LOADING ON HEAD, UPPER LOAD TEST DATE: 12/18/1997 SC ELEC DATA L.FRT NECK LORDING ON HERD



10 PROCESSED 12/10/1997 14:17 V2.07

C11817 L.REAR IMP 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 80.7KM/H

ATD TYPE: GM50H

TEST DATE: 12/18/1997

8W91850 4-DOOR SC ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HERD, L. FRT INJURY REFERENCE



C11817 L. REA	RIMP 70% OVERLA	DIT V MOB TO STATIONARY VEHICLE	80.7KM/H
50	8891850 4-0008	NECK LOADING ON HEAD	TEST DATE: 12/18/1997
ELEC DATA		L. FRI NECK LOADING ON HEF	D
_ 400 <u>, SRE_CLA</u>	ASS 600 FILTER	MAX CALC'D MOMENT = 15.5 N-M AT 147.7 M5 MI	n = -28,2 n-h rt 129,3 MS
ž Ž			



11 PROCESSED 12/18/1997 14:17 V2.07

C11817 L.REAR M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.7KM/H
SC 8W9185D 4-DOOR	FORWARD NECK SHEAR ON HEAD.	ATD TYPE: GM50H Test Date:12/18/1997
ELEC DATA, SAE CLASS 1000	L. FRT INJURY REFERENCE	



CI1817 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.7 KM/H REARWARD NECK SHEAR ON HEAD,

RTD TYPE: GMSOH TEST DATE: 12/18/1997

8W91850 4-000R SC ELEC DATA, SAE CLASS 1000

L. FRT INJURY REFERENCE

MAX 18V = 10 % OF 188V AT 298 N. 0.1 MS 6.0 5.5 5.0 ч. 4.0 2. 1.1 1. 0. 55 60 40 45 0.0 30 10 20 CUMULATIVE DURATION OF LORDING ABOVE GIVEN FORCE LEVEL, MS 13 PROCESSED 12/18/1997 14:17 V2.07

C11817 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.7KM/H

ELEC DATA, SAE CLASS 1000

SC

8W91850 4-000R

AXIAL COMPRESSION ON HEAD. L. FRT INJURY REFERENCE

ATD TYPE: GM50H TEST DATE: 12/18/1997

MAX TAV = 31 % OF TARY AT 1198 N. 1.7 MS 6.0 5.5 5.0 4.5 4.0 HX IRL COMPRESS NECK FORCE, KN 2.0 1.5 1.0 0. 0.0 10 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS





* PROCESSE0 12/19/1997 07:23 V2.07

C1 1817 L. R	ear imp 70% overlap	LTV MDB TO STATIONARY VEHICLE	80.7KM/H
SC	8W9185D 4-D008	L.FRINECK LOADING LOAD	TEST DATE: 12/18/1997
ELEC DATA		(TORSOON BASE OF NECK)	



CII817 L. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

80.7KM/H ATD TYPE: CM50H TEST DATE: 12/18/1997

8W91850 4-000R SC ELEC DATA, SAE CLASS 1000

R.FRTHERO ACCEL.

(HIC | LIMITED TO 15MS)



16 PROCESSED 12/18/1997 14:17 V2.07

C11817 L. REAR I M P 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 80.7KM/H

ATD TYPE: GMSOH TEST DATE: 12/18/1997

8W91850 4-DOOR SC ELEC DATA, SAE CLASS 1000

20

B.FRTHERD ACCEL. (HICILIMITED TO 36MS)

MAX ACCEL = 77.6 6'5 AT 112.7 MS ACCELERATION-C'S 3 MS CON ACC. = 61 6'S MAXINUM MIC (1) IND = 310 • 42.4 C'S : 98 - 124 MS FND ×0.0 Ο 50 COMPONENT ACCELERATIONS. 100 50 RICHT 0.0 LEFT 50 100 50 DOWN ~0.0 UP 500000000 200 220 2un 180 160 120

80

60

100

TIME IN MILLISECONDS

C11817 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.7KM/H SC 8H9185D 4-DODR R.FRT N E C K LOADING ON HEAD, UPPER LOAD T E S T DATE: 12/18/1997 ELEC DATA R.FRT N E C K LOADING ON HEAD



25 PROCESSED 12/18/1997 14:17 V2.07

C11817 L. REAR	I M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.7KM/H
SC	8W91850 U-DOOR	NECK LOADING on Hero	ATO TYPE: GM50H Test Date:12/18/1997
ELEC DATA		R.FRTNECK LOADINGON	HEAD



CI1817 L. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.7KM/H RTD TYPE: CM50H FORWARD NECK SHEAR ON HEAD. 8W9185D 4-DOOR TEST DATE: 12/18/1997 SC ELEC DATA, SAE CLASS 1000 **R. FRT** INJURY REFERENCE



27 PROCESSED 12/18/1997 14:17 V2.07





ELEC DATA, SAE CLASS 1000

TEST DATE: 12/18/1997

C11817 L. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.7 KM/H AXIAL COMPRESSION ON HEAD, ATD TYPE: CMSON 6W91850 U-DOOR TEST DATE: 12/18/1997 SC ELEC DATA, SAE CLASS 1000 R. FRT INJURY REFERENCE



29 PROCESSED 12/18/1997 14:17 V2.07

C11817 L. REAR I M P 70% OVERLAP L T V MOB TO STATIONARY VEHICLE 80.7KM/H

8W9185D 4-DOOR SC ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HEAD, TEST DOTE 10/10 R. FRT INJURY REFERENCE

TEST DATE: 12/18/1997



C11818 L. REAR I M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC 8N9182D 4-DOOR	L.FAT HERO ACCEL.	ATD TYP Test of
ELEC DATA, SAE CLASS 1000	(HICLLIMITED TO 15MS)	

(HIC | LIMITED TO 15MS)

'PE: **CM50H** RTE:12/18/1997

MAX ACCEL + 60.1 G*S AT 121.0 MS RESULTANT ACCELERATION-C'S M _ B B B <u>3 MS CON ACC. = 54 G'S</u> HAXIMUM HIF 11) IND = 220 • 46.5 C'S : 116 - 131 MS FHD PF1 ×0.0 G COMPONENT ACCELERRY ONS. 100 5 RIGHT 0.0 50 100 50 DOHN 0.0 UP SOMMUM 200 221 2un 120 160 180 100 140 20 80 ü۵ TIME IN MILLISECONDS

1 PROCESSED 12/18/1997 14:21 ¥2.07

CI1818 L.REAR IN	19 70% o	VERLAP	LTV MOB TO STATIONARY VEHICLE	80
SC BI	W9182D	4-D00R	L, FRT HEAD ACCEL.	

.9KM/H ATO TYPE: GM50H TEST DATE: 12/18/1997

ELEC DATA, SAE CLASS 1000

(HIC | LIMITED TO 36MS)

HAX ACCEL + 60.1 6'S AT 121.0 HS ACCELERATION-C'S ACCELERATION-C'S A.C. & B. B 3 MS CON ACC. = 54 6'5 ~~~~ MAXIMUM HIC (1) IND = 250 • 34.6 C'5 : 97 - 133 MS FND ×0.0 COMPONENT ACCELERATIONS. G 50 100 50 RIGHT LEFT _ 0.0 5Ç 100 SC DOHN UP 0.0 س solumm 200 200 220 60 100 120 140 160 180 zô

TIME IN MILLISECONDS





11 PROCESSED 12/18/1997 14:21 V2.07

CI1818 L.REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

80.9KM/H ATD TYPE: GM50H TEST DATE: 12/18/1997

SC 8W9182D 4-DOOR FORWARD NECK SHEAR ON HERO.

MAX 1AV * 32 % OF 1ARV AT 985 N. 0.3 MS 6.0 5. 5.0 ч.! 4.0 SHEAR FORWARD NECK FOACE, KN 2.1 1.5 1.0 ٥. 0.0 20 25 ŝ 55 66 30 un CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL, MS

ELEC DATA, SAE CLASS 1000

L FRT INJURY REFERENCE



CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS

13 PROCESSED 12/18/1997 14:21 V2.07

C11818 L.REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

80.9KM/H ATD TYPE: GMSOH TEST OATE: 12/18/1997

AXIAL COMPRESSION ON HEAD. L. FRT INJURY REFERENCE

MAX 1AV = 34 % OF 1ARV AT 376 N. 30.0 MS 6.0 5.1 5.0 ۹. ۱ 4. RECK FORCE, KN 2. 1.5 1.0 0.5 0.0L 10 15 20 25 30 35 UD. 55 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL, MS

8W91820 4-0008 SC

ELEC DATA, SAE CLASS 1000

80.9KM/H



10 PROCESSED 12/18/1997 14:21 V2.07

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C11818 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

80.9KM/H ATD TYPE: CMSOH TEST DATE: 12/18/1997

8W91820 4-D00R SC ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HEAD, L. FRT INJURY REFERENCE







31 PROCESSED 12/19/1997 07:24 12.07



80.9KM/H ATO TYPE: GM50H TEST DATE: 12/18/1997

SC ELEC DATA (TORSO ON BASE OF NECK)

MIN = -40.5 N-H AT 120.3 MS NAX CAL'D MOMENT = 72.2 N-M AT 149.4 MS SHE CLASS 600 FILTER 300 T - Z 10 MONENT N-00 MONENT N-00 00 000 FLEX EXT . ជ.₁₀₀ MIN LORD = -0.41 KN AT 146.7 MS MAX LOAD = 1.30 KN AT 108.7 H SAE CLASS 1000 FILTER FZ-AXIAL LOAD, KN TENS MIN LOAD = -0.99 KN AT 103.4 MS MAX LOAD = 0.65 KN AT 121.4 MS SAE CLASS 1000 FILTER FX-FORE/AFT LOAD. KN FND 160 180 200 220 200 20 120 100

TIME IN MILLISECONDS

CI1818 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

80.9KM/H

ATD TYPE: GM50H TEST DATE: 12/18/1997

8W9182D 4-000R SC ELEC DATA, SAE CLASS 1000

R.FRTHERO ACCEL. (HICI LIMITED TO 15MS)



16 PROCESSED 12/18/1997 14:21 V2.07

C11818 L.REAR IMP 70% OVERLAP	LTV MDB TO STATIONARY VEHICLE 80.9KM	IZH
SC 8W9182D 4-DDOR	R.FRTHERO ACCEL.	ATD TYPE: CM50H TEST DATE:12/18/1997
ELEC DATA, SAE CLASS 1000	(HICILIMITED T O 36MS)	







25 PPROCESSED 12/18/1997 14:22 V2.07

C11818 L.REA	r imp 70% overlap	LTV MDB TO STATIONARY VEHICLE	80.9KM/H
SC	8W9182D U-ODOR	NECK LOADING ON HERO	AID TYPE: GM50H TEST DATE: 12/18/1997
elec data		R.FRTNECK LOADING ON HER	0



C11818 L.REAR M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC 8W9182D 4-DOOR	FORWARD NECK SHEAR ON HERO.	ATD TYPE: CM50H TEST DATE:12/18/1997
- CL CC DOTA COT CLOCC 1000		

ELEC DATA, SAE CLASS 1000

A. FRT INJURY REFERENCE



27 PROCESSED 12/18/1997 14:22 V2.07

CI1818 L. REAR I M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC 8W9182D U-DOOR	REARWARD NECK SHEAR ON HERO.	ATD TYPE: GM50H TEST DATE:12/18/1997
ELEC DATA, SAE CLASS 1000	R. FRT INJURY REFERENCE	



C11818 L.REAR IMP 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC 8W91820 4-DOOR	AXIAL COMPRESSION ON HEAD.	ATD TYPE: GMSOH Test Date: 12/18/1997
CLEC DOTO COE CLASS 1000		

S ELEC DATA, SAE CLASS 1000

R, FRT INJURY REFERENCE



29 PROCESSED 12/18/1997 14:22 V2.07

CI1818 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 80.9KM/H

5Ç 8W9182D 4-DOOR ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HEAD. **R. FRT INJURY REFERENCE** ATD TYPE: CM50H TEST DATE: 12/18/1997

MAX IAV = 28 % OF LARY AT 937 N. 0.1 MS 6.0 5.5 5.0 4.5 4.0 5.0 1.5 1.0 0. o.ol 15 20 25 30 35 40 45 ιõ

C11816 R. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

81.2KM/H RTD TYPE: GM50H TESTDATE: 01/28/1998

SC

L. FRT HERO ACCEL. (HIC I LIMITED TO 15MS)

8W9183D 4-DOOR ELEC DATA, SAE CLASS 1000



1 PROCESSED 1/28/1998 09:07 V2.07

CI1816 R.REAR IMP 70% OVERLAP LITV HOE TO STATIONARY VEHICLE

L.FRTHERO ACCEL.

-

81.2KM/H ATO TYPE: GM50H TEST 0ATE:01/28/1998

8W9183D 4-DOOR SC ELEC DATA, SAE CLASS 1000

(HICILIMITED TO 36MS)



2 PROCESSED 1/28/1998 09:07 V2.07





C11816 R.REAR I M P70% OVERLAPLTVMDB TOSTATIONARY VEHICLEB1.2 KM/HSC8W9183D 4-DOORL.FRT NECK LOADING ON HEAD, UPPER LOADATD TYPE: GMSOHELEC DATAL.FRT N E C KLOADING ON HEAD

C11816 A.REAR IMP 70% OVERLAP	LTV MOB TO STATIONRAY VEHICLE B1.2	KM/H
SC 8W9183D Y-DOOR	FORWARD NECK SHEAR ON HEAD,	TEST DATE: 01/28/1998
ELEC DATA. SAE CLASS 1000	FRT INJURY REFERENCE	



12 PROCESSED 1/26/1998 09:07 V2.07

C11816 R. BEAR I M P70% OVERLAPLTVMOB TOSTATIONARY VEHICLE81.2 KM/HSC8W9183D 4-DOORREARWARD NECK SHEAR ON HEAD.ATD TYPE: CM50HELEC DATA, SAE CLASS 1000L. FRT INJURY REFERENCE

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C11816 R. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE AXIAL COMPRESSION ON HERO.

81.2KM/H RTD TYPE: GM50H

YES, DATE:01/28/1998

8W9183D U-ODOR SC ELEC DATA, SAE CLASS 1000

L. FRT INJURY REFERENCE



14 PROCESSED 1/28/1998 09:07 V2.07

C11B16 R.REAR IMP 70% OVERLAP LTV MDB TO STATIONARY VEHICLE

AXIAL TENSION ON HERO.

81.2KM/H ATD TYPE: GM50H TEST DATE: 01/28/1998

8W91830 4-000R SC ELEC DATA, SAE CLASS 1000

> 6.0 5.5 5.0 4.5 4.0

AXIAL TENSION NECK FORCE, KN

s., 1. 1.0 0.5 0.0

10



• • •

MAX IAV = 36 % OF IARV AT 393 N, 60.1 MS

IS CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS



C11816 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

81.2KM/H ATD TYPE: GM50H TEST DATE:01/28/1998

8W9183D 4-DOOR SC ELEC DATA, SAE CLASS 1000

(HIC I LIMITED TO 15MS)

R.FRTHERD ACCEL.



CI1816 R.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.2KM/H ATO TYPE: GM50H R. FRT HEAD ACCEL. 8W91830 4-DOOR TEST DATE:01/28/1998 SC ELEC DATA, SAE CLASS 1000 (HIC I LIMITED TO 36MS)



CIIBIS R. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE B1.2KM/H ATO TYPE: GM50H BW91830 4-DOOR R. FRT NECK LOADING ON HEAD, UPPER LOAD TEST DATE:01/28/1998 SC ELEC DATA R. FRT NECK LOADING ON HEAD



25 PROCESSED 1/20/1998 09:07 V2.07

C11816 R. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.2KM/H

AXIAL TENSION ON HEAD,

ATO TYPE, GMSOH TEST DATE: 01/28/1998

8W9183D 4-000R SC

> 6.0 5.5 5.0 ч. 4.0

NECK FORCE KN

2.1 1.3 1.0 Ο. 0.0⊨ ö

ELEC DATA, SAE CLASS 1000

10

R. FRT INJURY REFERENCE

MAX TAV = 22 % OF TARY AT 243 N. 60.1 MS

25 30 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS

CI1816 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.2KM/H NECK LOADING ON HEAD 8W9183D 4-DOOR SC

ATD TYPE: GM50H TEST DATE: 01/28/1998

ELEC DATA

B. FRINECK LOADING ON HEAD



26 PROCESSED 1/28/1998 09:07 V2.07

8W9183D 4-D008 SC ELEC DATA, SAE CLASS 1000

C1 1816 R. REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.2KM/H FORWARD NECK SHEAR ON HEAD, R. FRT INJURY REFERENCE

. . .

ATD TYPE: GMSOH TEST DATE: 01/28/1998



C11816 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.2KM/H REARWARD NECK SHEAR ON HEAD, ATD TYPE: CM50H TEST DATE:01/28/

TEST DATE: 01/28/1998

6W9163D 4-DOOR SC ELEC DATA, SAE CLASS 1000

R.FRTINJURY REFERENCE



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28 PROCESSED 1/28/1998 09:07 V2.07

CI1816 R. REAR I M P 70% OVERLAP LTV MDB TO STATIONARY VEHICLE 81.2KM/H AXIAL COMPRESSION ON HEAD, 8W91830 4-000R **R.FRT**INJURY **REFERENCE**

ATD TYPE: GM50H TEST DATE: 01/28/1998

SC ELEC DATA, SAE CLASS 1000



C11828 L.REAR IMP 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	81.0KM/H
SC 8W9184D 4-DOOR	L. FRT HEAD ACCEL.	HID ITPE: GMSOH TEST DATE:01/28/1998
ELEC DATA, SAE CLASS 1000	(HIC I LIMITED TO 15MS)	



1 PROCESSED 1/29/1998 07:59 V2.07

C11828 L. REAR | M P 70% OVERLAP LTV MOE TO STATIONARY VEHICLE

TO STATIONARY VEHICLE L.FRT H E R O ACCEL. 81.0KM/H

ATD TYPE: GM50H TEST DATE:01/28/1998

SC 8W9184D 4-DOOR ELEC DATA, SAE CLASS 1000

(HIC I LIMITED TO 36MS)

HESULTANT ACCELERATION-C'S M B B MRX ACCEL = 175 G'S AT 107.8 MS 3 MS CON ACC. = 74 G'S MAXIMUM HIC (11 IND = 410 • 99.2 G'S : 107 - 111 MS IAV = 417 OF IMPRV F ND AF T × 0.0 U SC COMPONENT ACCELERATIONS. 100 50 RIGHT 0.0 5 100 50 $\boldsymbol{\mathcal{M}}$ DOWN **⊳**0.0 UP solummin 0 100 200 220 20 60 120 140 160 180 240 80

TIME IN MILLISECONDS

C11828 L.REAR IMP 70% OVERLAPLTV MDB TO STATIONARY VEHICLE81.0 KM/HSC8W9184D 4-DOORL. FRT NECK LOADING ON HEAD. UPPER LOADTEST DATE:01/28/1998ELEC DATAL.FRT NECK LORDING ON HEAD



10 PROCESSED 1/29/1998 07:59 V2.07

C11828 L.REAR	R IMP 70%	OVERLAP	LTV MOE TO STATIONARY VEHICLE	81.0KM/H
SC	8W9184D	4-000R	NECK LOADING ON HEAD	ATD TYPE: GM50H Test Date:01/28/1998
elec data			L.FRTNECK LOADING ON HEF	O



C11828	L.REAR IMP 70%	OVERLAP	LTV MOB TO STATIONARY VEHICLE	B1.0KM/H
SC	8W9184D	4-000A	FORWARD NECK SHEAR ON HERO.	RTO TYPE: CM50H Test Date:01/28/1998

ELEC DATA, SAE CLASS 1000

L. FRT INJURY REFERENCE



12 PROCESSED 1/29/1998 07:59 ¥2.07



ELEC DATA, SAE CLASS 1000

L. FRT INJURY REFERENCE

. . .

MAX IAV = 23 % OF LARV AT 700 N. 0.0 MS 6.0 . • 5. 5.0 4.5 4.0 SHERR REPRIMARD NECK FORCE. KN 2. 1.5 1.0 _ 0.5 0.0 50 15 20 35 40 55 60 25 10 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS



ATO TYPE: CMSOH TEST DATE:01/28/1998

ELEC DATA, SAE CLASS 1000

L.FRT INJURY REFERENCE



14 PROCESSED 1/29/1998 07:59 V2.07

C11828 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H

AXIAL TENSION ON HERD.

ATD TYPE: GMSOH TEST DATE: 01/28/1998

8W9184D 4-000R SC

ELEC DATA, SAE CLASS 1000

L. FRT INJURY REFERENCE

MAX 1AV = 22 % OF 1ABY AT 736 N. 0.0 MS 6.0 **s**. ! 5.0 ų. S 4.0 RXIAL TENSION NECK FORCE, KN 2.4 1.3 1.0 0.1 0.0L 25 35 50 55 15 20 30 40 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS




31 PROCESSED 1/29/1998 08:00 V2.07

C11828 L.REAR IMP 70% OVERLAP		VERLAP	LTV MOB TO STATIONARY VEHICLE	81.0KM/H	
^{SC} Elec Data	8W91840	4-DOOR	L. FRT NECK LOADING LOAD (TORSO ON BASE OF NECK)	TEST DATE:01/28/1998	



30 PROCESSED 172971998 08-00 92 07

C11828 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H

ATD TYPE: GM50H TEST DATE: 01/28/1998

8W91840 4-DOOR SC

R.FRTHERO ACCEL.

ELEC DRTA, SAE CLASS 1000

(HICILIMITED TO 15MS)



16 PROCESSED 1/29/1998 07:59 V2.07

C11828 L.REAR I M P 70% QVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H

8W9184D 4-DOOR SC ELEC DATA, SHE CLASS 1000

R.FRTHERO ACCEL. (HIC | LIMITED TO 36MS)

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ATD TYPE: GM50H TEST DATE: 01/28/1998







26 PROCESSED 1/29/1998 06:00 V2.07

8W9184D 4-DOOR

FORWARD NECK SHEAR ON HEAD, **R. FRT** INJURY REFERENCE

e - *

81.0KM/H ATD TYPE: GMSOH TEST DATE:01/28/1998



C11828 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

SC ELEC DATA, SAE CLASS 1000 CIJ828 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H REARWARD NECK SHEAR ON HEAD,

ATO TYPE, GM50H TEST DATE: 01/28/1998

8W9184D U-DOOR

R. FRT INJURY REFERENCE

SC ELEC DATA, SAE CLASS 1000

MAX IAV = 5 % OF IARV AT 154 N. 1.9 MS 6.0 5.5 5.0 4.5 4.0 NECK FORCE, KN -2.0 1.5 1.0 0.5 0.0L 35 40 45 55 60 10 20 30 15 25 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS

28 PROCESSED 1/29/1998 08:00 V2.07









25 PROCESSED 1/29/1998 08:00 V2.07

C11828 L.REAR IMP 70% OVERLAP LTV MDB TO STATIONARY VEHICLE 81.0KM/H

ATD TYPE: GM50H

8W91840 4-DOOR SC ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HEAD. **R.FRT** INJURY REFERENCE

TEST DATE:01/28/1998



C11829 B. REAR I M P 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 81.0KM/H

ATD TYPE: CMSOH TEST DATE:01/28/1998

1JW99326 4-DOOR SC ELEC DATA, SAE CLASS 1000

L.FRTHERD ACCEL. (HIC I LIMITED TO 15MS)



CI1829 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

81.0KM/H ATO TYPE: GM50H TEST DATE:01/28/1998

1JW99326 4-DOOR SC ELEC DATA, SAE CLASS 1000

L.FRTHEAD ACCEL. (HICILIMITED TO 36MS)



2 PROCESSED 1/28/1998 15:12 V2.07

 C11829 R.REAR I M P 70% OVERLAP
 LTV MDB TO STATIONARY VEHICLE
 B1.0KM/H

 SC
 1JW99326 4-DOOR I - .
 FRT NECK LOAD ING ON HEAD, UPPER LOAD TEST DATE:01/28/1998

 ELEC DATA
 L.FRT NECK LOADING ON HEAD



C11829 R. REAP	IMP 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	81.0KM/H
SC	1JW99326 4-DOOR	NECK LOADING on Head	ATD TYPE: GM50H Test Date:01/26/1998
elec data		L.FRTNECK LOADING ON HER	D



CI1829 B, REAR IMP 70%, OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H FORWARD NECK **SHEAR** ON HERO. I JW99326 4-DOOR SC L. FRT INJURY REFERENCE

ELEC DATA. SAE CLASS 1000

6.0

MAX 1AV # 3 % OF LARY AT 53 N, 20.9 MS

20 30 un 10 Ē 15 CUMULATIVE OURATION OF LOADING ABOVE GIVEN FORCE LEVEL, MS 12 PROCESSED 1/28/1998 15:12 V2.07

C11829 R. REAR I M P 70% OVERLAP LTV MDB TO STATIONARY VEHICLE 81. DKM/H

1JW99326 4-DOOR SC ELEC DATA, SAE CLASS 1000

REARWARD NECK SHEAR ON HEAD. L. FRT INJURY REFERENCE

ATO TYPE: GM50H TEST DATE: 01/28/1998

MAX 1RV = 19 % OF 1ARV AT 515 N, 6.8 MS 6.0 5.9 5.0 4.5 4.0 2.0 1.5 1.0 _ 0.5 0.0<u>0</u> 30 35 50 25 40 10 20 CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL, MS



ATD TYPE: CM50H TEST DATE:01/28/1998

C11829 R. REAR	M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	BI.OKM/H
SC	1JW99326 4-DOOR	AXIAL COMPRESSION ON HEAD.	TEST DATE:01/28/1998
ELEC DATA, SAE	CLASS 1000	L.FRT INJURY REFERENCE	



14 PROCESSED 1/28/1998 15:12 V2.07

C11829 R.REAR IMP 70% OVERLAP

LTV MOE TO STATIONARY VEHICLE

81.0KM/H ATD TYPE: GM50H TEST DATE: 01/28/1998

1JW99326 4-DOOR SC

ELEC DATA, SAE CLASS 1000

L.FRT INJURY REFERENCE

MAX 18V = 21 % OF 188V AT 684 N, 0.0 MS 6.0 5. 5.0 4.5 4.0 AXIAL TENSION NECK FORCE, KN 2.0 1.5 1.0 0.S 0.0 6/ 50 30 35 40 45 10 15 20 25

CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS

AXIAL TENSION ON HEAD,

C11829 R. REAR I M P 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 81.0 KM/H

ATD TYPE: CM50H TEST DATE:01/28/1998

SC 1JW99325 4~DOOR Elec Data

(TORSO ON BASE OF NECK)



31 PROCESSED 1/20/1990 15:13 V2.07





32 PROCESSED 1/28/1998 15:13 V2.07



C11829 R. REAR IMP 70% OVERLAP LTV MOE TO STATIONARY VEHICLE 81.0KM/H REARWARD NECK SHEAR ON HEAD,

ATD TYPE: GM50H TEST DATE: 01/28/1998

1JW99326 4-DOOR 5C ELEC DATA, SAE CLASS 1000

R. FRTINJURY REFERENCE



28 PROCESSED 1/28/1998 15:13 V2.07

C11829 R.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

81.0KM/H

ATD TYPE: GMSOH TEST DATE: 01/28/1998

AXIAL COMPRESSION ON HERD.

1 JN99326 4-DOOR SC

ELEC DATA, SAE CLASS 1000

R. FRT INJURY REFERENCE

. . .

HAX JAY = 16 % OF LARY AT 651 N. 0.0 MS 6.0 5.5 5.0 ч.5 4.0 NECK FORCE, KN 2.0 1.5 1.0 0.5 0.0 55 50 60 35 20 25 30 40 45 15 iñ CUMULATIVE DURATION OF LOADING REDVE GIVEN FORCE LEVEL, MS

C11829 R.REAR M P	70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	81.0KM/H
co	0000 (1. 0000	NECK LOADING ON HEAD	F -

ATD TYPE: GM50H TEST DATE:01/28/1998

SC 1 JW99326 4-DOOR Elec Data

R. FRT NECK LOADING ON HEAD



26 PROCESSED 1/28/1998 15113 V2.07

C11829 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE

FORWARD NECK SHEAR ON HEAD.

81.0KM/H ATO TYPE: GM50H TEST DATE:01/28/1998

SC 1JN99326 4-D00R ELEC DATA, SAE CLASS 1000 **B.FRT**INJURY REFERENCE

2 . . .



C11829 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H 1JW99326 4-000R R. FRT NECK LOADING ON HEAD, UPPER LOAD TEST DATE: 01/28/1998 SC ELEC DATA R. FRT NECK LOADING ON HERO



25 PROCESSED 1/28/1998 15:13 V2.07

C11829 R.REAR IMP 70% OVERLAP LTV MDB TO STATIONARY VEHICLE

81.0KM/H

ATO TYPE: GM50H TEST DATE: 01/28/1998

1 JW99326 4-000R SC ELEC DATA, SAE CLASS 1000

AXIAL TENSION ON HERO. **R. FRT** INJURY REFERENCE

MAX 1AV = 47 % OF IARY AT 1535 N. 0.0 MS 6.0 5.5 5.0 4.5 4.0 NECK FORCE, KN 2.0 1.5 1.0 0. 0.0 50 55 ΫŪ 'n

CUMULATIVE DURATION OF LOADING ABOVE GIVEN FORCE LEVEL. MS

Appendix E

Anthropomorphic Test Device (ATD) Injury Assessment Reference Values (IARVs)

The **JARVs** used for the **mid-sized** adult male Hybrid **III ATD** in the Project **B.5** tests are recreated here from the Advisory Group for Aerospace Research & Development, Report **330**, "Anthropomorphic Dummies for Crash and Escape System Testing" **[11]**, except for the lower neck extension moment **JARV** which came from **SAE** Technical Paper No. **973342 [12]** and the lumbar spine **JARVs** which came from a General Motors Corporation research paper [**I 3**].

3ody Region Injury Assessment Criteria	Injury Assessment Reference Value for the mid sized male Hybrid III
lead HIC; (t ₂ –t ₁) ≤15 msec*	1000
 -lead/Neck Interface Upper neck longitudinal shear force, +Fx and -Fx Upper neck axial force, compression, -Fz Upper neck axial force, tension, +Fz Upper neck longitudinal moment, flexion, +My Upper neck longitudinal moment, extension, -My 	Figure El Figure E2 Figure E3 190 N•m 57 N•m
Neck/Thorax Interface Lower neck longitudinal shear force, +Fx and -Fx Lower neck axial force, compression, -Fz Lower neck axial force, tension, +Fz Lower neck longitudinal moment, extension, -My	Figure El Figure E2 Figure E3 1 54 N-m
Thorax/Chest Resultant spinal acceleration Sternal deflection due to shoulder belt	60 g 50 mm
Femurs Axial compression	Figure E4
Lumbar spine Bending, flexion Bending, extension Axial force, tension Axial force, compression Fore • aft shear force	1125 N∙m 338 N•m Figure E5 Figure E6 Figure E7

• The Head Injury Criterion (HIC) is defined as: $HIC = (Aavg)^{2.5} (t_2 - t_1)$, where Aavg is the average resultant acceleration of the center of mass of the head (expressed in gs) for the time interval $t_2 - t_1$ (expressed in seconds).





Figure E2 - Injury Assessment Criteria for Axial Neck Compression Measured with Hybrid III Mid-sized Adult Male ATD







Figure E4 - Injury Assessment Criteria for Axial Compressive Femur Force Measured with Hybrid III Mid-sized Adult Male ATD









Appendix F

Test Vehicle Acceleration, Velocity and Displacement Data Plots

C11817 L. REAR M P 70% OVE	RLAP LTV MOB	TO STATIONARY	VEHICLE	80
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0.7KM/H

SC	8W9185D 4-DOOR	L. FRT ROCKER	TEST DATE: 12/18/1997
ELEC DATA			

Ε



57 PROCESSED 12/18/1997 14:17 V2.07





60 PROCESSED 12/18/1997 14:17 V2.07

CI1818 L.REAR I M P 70% OVERLAP	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC 8W9182D 4-DOOR Elec Data	L. FRT ROCKER	TEST DATE:12/18/1997



\$7 PROCESSED 12/18/1997 14:22 V2.07

C11818 L.REAR	IMP 70	0% overlap	LTV MOB TO STATIONARY VEHICLE	80.9KM/H
SC	8W9182D	4-000R	R. FRT ROCKER	1

ELEC DATA

TEST DATE: 12/18/1997



C11816 R. REAR I M P 70% OVERLAP	LTV MOE TO STATIONARY VEHICLE	81.2KM/H
SC 8W9183D 4-DOOR Elec Data	L. FRT ROCKER	TEST DATE:01/28/1998



57 PROCESSED 1/28/1998 09:08 V2.07









57 PROCESSED 1/29/1998 08:00 Y2:07

C11828 L.REAR IMP 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H B. FRT ROCKER

8W9184D 4-000R

TEST DATE: 01/28/1998

sc Elec oata



C11829 R. REAR I M P 70% OVERLAP LTV MOB TO STATIONARY VEHICLE 81.0KM/H SC 1JW99326 4-000R L.FRT ROCKER TEST DATE:01/28/1998 ELEC DATA



57 PROCESSED 1/28/1998 15:14 V2.07





60 PAOCESSED 1/28/1998 15:14 V2.07