

Cutting Processes I

Reading assignment:

- 20.1 – 20.3, 20.5

Cutting processes I

Cutting processes

- Process planning, Cost, Quality, Rate and Flexibility

Modeling: Orthogonal cutting

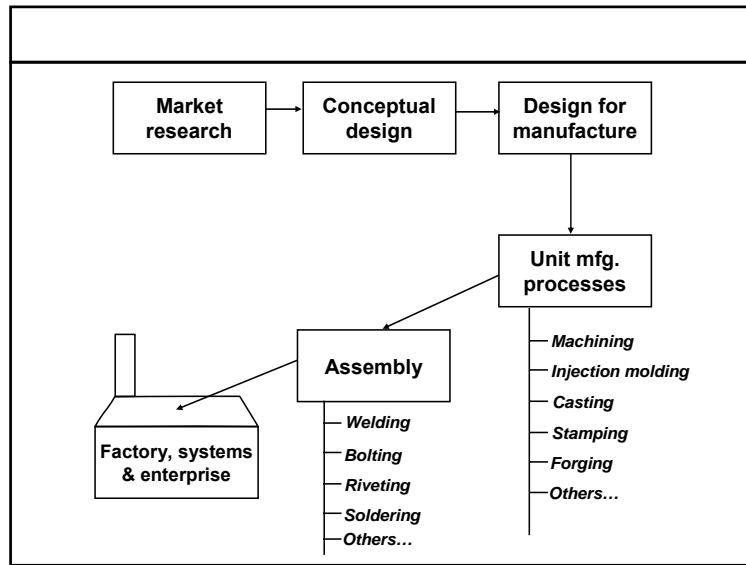
- Video, geometry, forces and power

Demonstration

Cutting equipment/tools

Design for Manufacturing: Cutting

Process variation



Material removal processes

Mechanical removal processes

- Milling Turning Shaping
- Grinding Broaching

Others

- Thermal Electrochemical Chemical

In general:

<u>Cost</u>	<u>Flexibility</u>	<u>Quality</u>	<u>Rate</u>
Expensive	Complex shapes	Depends	Slow

Understanding what is going on

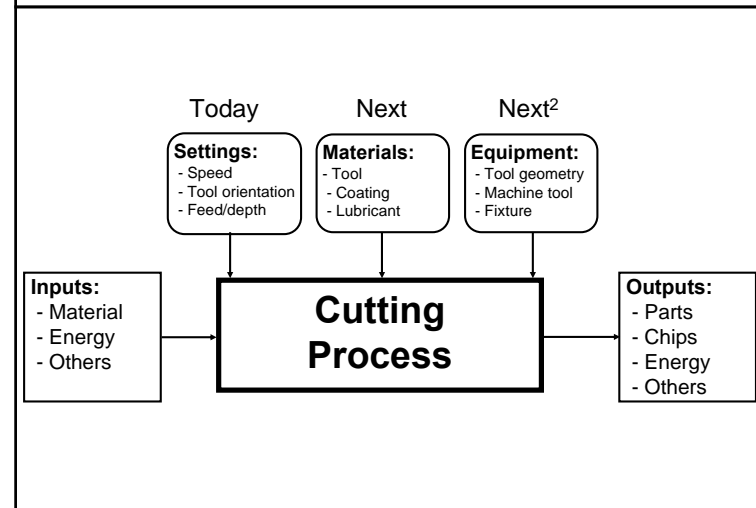
Key issues

- How does cutting work?
- Linking the Cost, Flexibility, Quality and Rate to process parameters

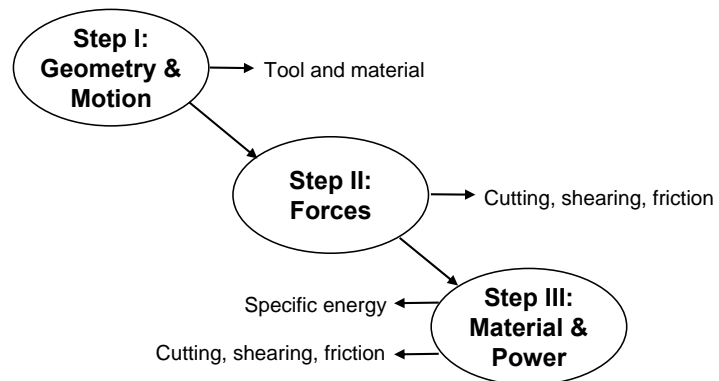
Available methods to design process parameters:

- Analytic
- Numerical
- Experimental

Process planning & cutting process

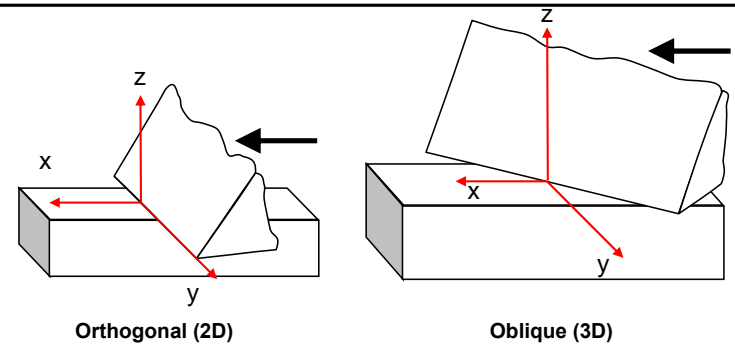


Steps we will take to get there



Geometry & Motion → Forces → Material & Energy/Power

Basic cutting geometries

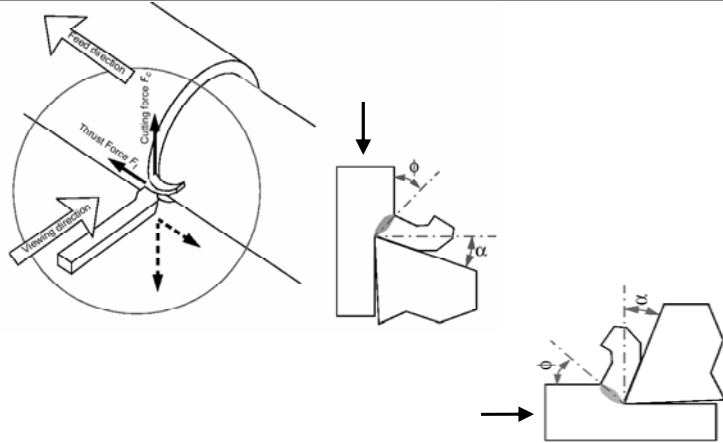


Orthogonal → Provides insight for understanding

Oblique → Complex, diminishing returns

Geometry & Motion → Forces → Material & Energy/Power

Orthogonal cutting in a lathe

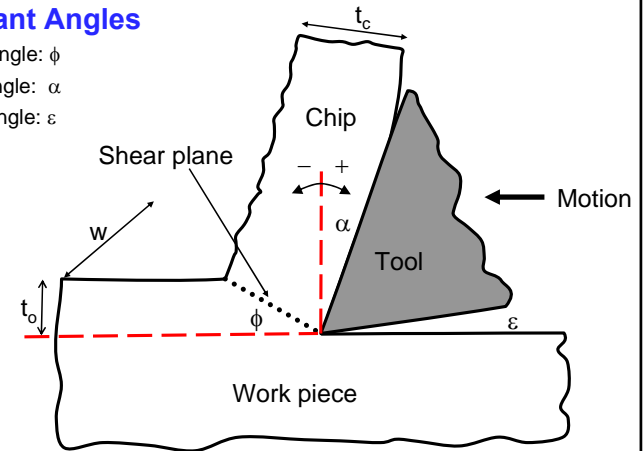


Geometry & Motion → Forces → Material & Energy/Power

Orthogonal cutting zone geometry

Important Angles

- Shear angle: ϕ
- Rake angle: α
- Relief angle: ϵ



Geometry & Motion → Forces → Material & Energy/Power

CUTTING VIDEO

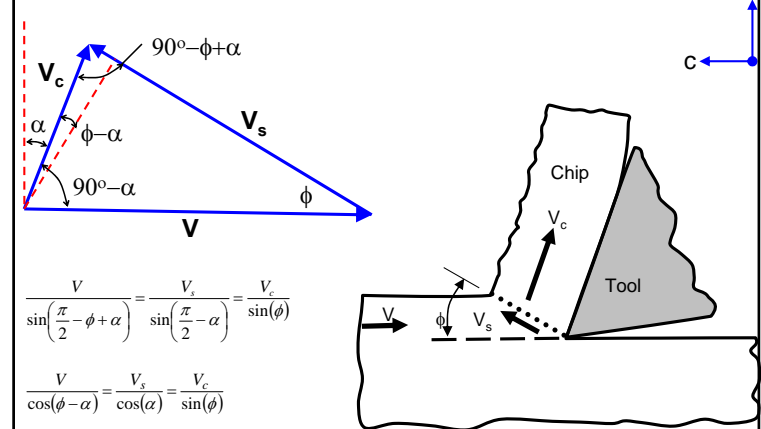
Key issue:

- Motion and material flow
- Types of chips
- How chip type relates to material

Geometry & Motion → Forces → Material & Energy/Power

Velocity diagram of cutting zone

Need velocities to obtain power estimates



Geometry & Motion → Forces → Material & Energy/Power

Cutting ratio, r

From mass conservation:

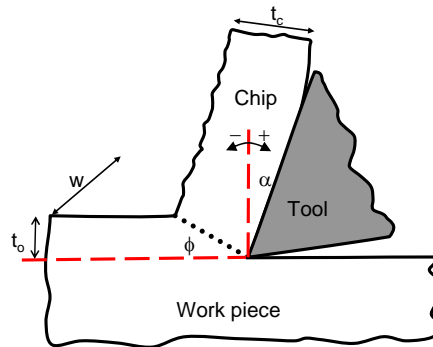
$$\rho \cdot t_o \cdot w \cdot V = \rho \cdot t_c \cdot w \cdot V_c$$

From velocity diagram:

$$\frac{V}{\cos(\phi - \alpha)} = \frac{V_c}{\sin(\phi)}$$

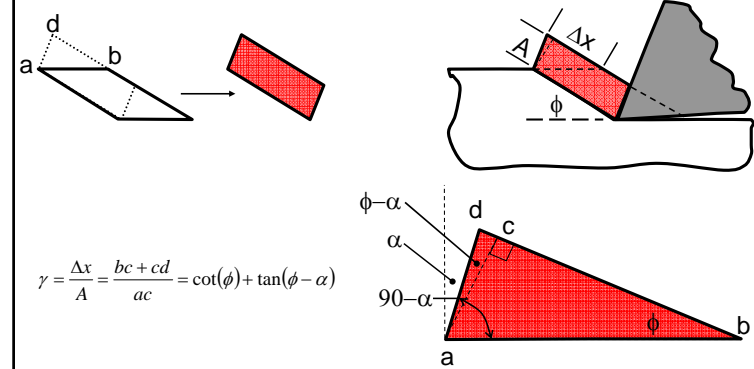
Cutting ratio:

$$\frac{V_c}{V} = \frac{t_o}{t_c} = r = \frac{\sin(\phi)}{\cos(\phi - \alpha)}$$



Geometry & Motion → Forces → Material & Energy/Power

Analysis of shear strain



What does this mean:

$$\phi \downarrow = \gamma \uparrow$$

Geometry & Motion → Forces → Material & Energy/Power

Cutting forces and power

Why do we need to know the cutting force/power?

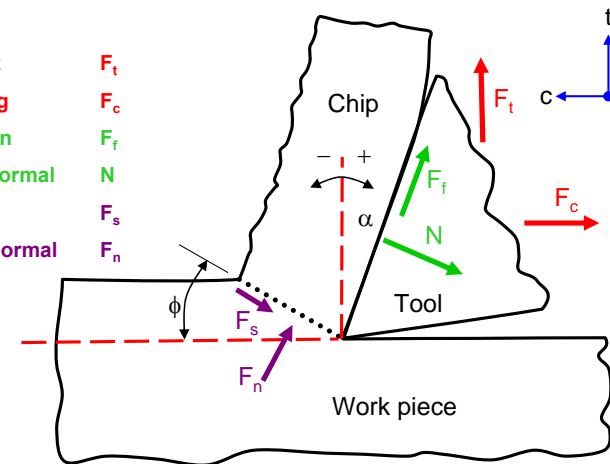
- Designing parts / machine tools (power and stiffness)
- Part, machine and tool deflection
- Trade offs in process planning, CFQR...
- Equipment suitability
- Others....

Geometry & Motion → Forces → Material & Energy/Power

Cutting forces

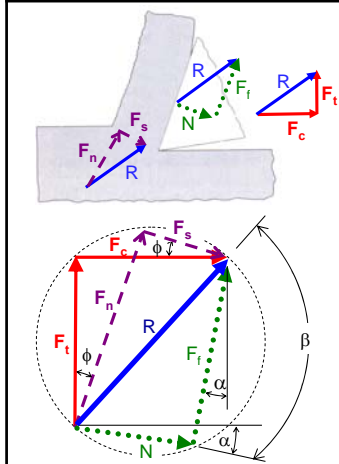
Forces:

- Thrust F_t
- Cutting F_c
- Friction F_f
- Tool normal N
- Shear F_s
- Chip normal F_n



Geometry & Motion → Forces → Material & Energy/Power

Merchant's diagram: Force relationships



Shear plane forces:

$$F_s = F_c \cdot \cos(\phi) - F_t \cdot \sin(\phi)$$

$$F_n = F_c \cdot \sin(\phi) + F_t \cdot \cos(\phi)$$

Tool-chip forces:

$$F_f = F_c \cdot \sin(\alpha) + F_t \cdot \cos(\alpha)$$

$$N = F_c \cdot \cos(\alpha) - F_t \cdot \sin(\alpha)$$

$$\mu = \frac{F_f}{N} = \tan(\beta)$$

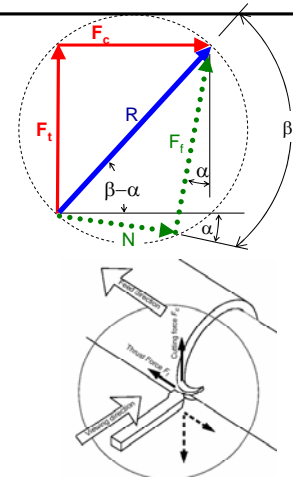
Typically: $0.5 < \mu < 2$

Geometry & Motion → Forces → Material & Energy/Power

Cutting and thrust forces

$$F_t = F_c \tan(\beta - \alpha)$$

- $\beta < \alpha$ tool is pulled into part
- $\beta > \alpha$ tool is pushed away
- $\beta = \alpha$ no thrust force



Use high α for thin cuts?

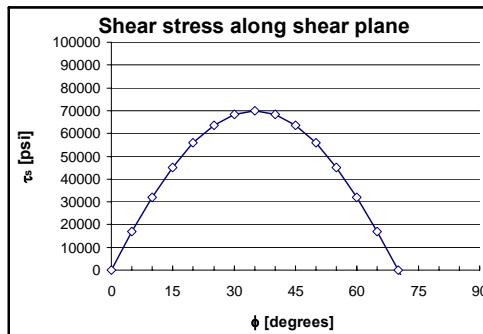
Geometry & Motion → Forces → Material & Energy/Power

ϕ and τ_s

Magnitude of shear stress varies with angle of shear plane

$$\tau_s = \frac{F_s}{A_s} = \frac{F_c \cdot \cos(\phi) - F_t \cdot \sin(\phi)}{\left[\frac{t_o}{\sin(\phi)} \right] \cdot w}$$

ϕ_{max}	35	degrees
	0.61	radians
F_c	225	lbf
α	20	degrees
	0.35	radians
β	40	degrees
	0.70	radians
t_o	0.015	inches
w	0.075	inches
τ_s	70021	psi



Geometry & Motion → Forces → Material & Energy/Power

Merchant's relationship

Merchant's assumption:

- Shear angle adjusts to maximize τ_s

$$\tau_s = \frac{F_s}{A_s} = \frac{F_c \cdot \cos(\phi) - F_t \cdot \sin(\phi)}{\left[\frac{t_o}{\sin(\phi)} \right] \cdot w}$$

$$\frac{F_t}{F_c} = \tan(\beta - \alpha)$$

$$\frac{d\tau_s}{d\phi} = \frac{F_c}{t_o \cdot w} \left[\cos^2(\phi) - \sin^2(\phi) - \frac{F_t}{F_c} \cdot 2 \cdot \sin(\phi) \cdot \cos(\phi) \right] = \frac{F_c}{t_o \cdot w} \left[\cos(2\phi) - \frac{F_t}{F_c} \cdot \sin(2\phi) \right]$$

$$\frac{d\tau_s}{d\phi} = 0 \rightarrow \left[\frac{\cos(2\phi)}{\sin(2\phi)} - \frac{F_t}{F_c} \right] = 0 = \frac{\cos(2\phi)}{\sin(2\phi)} - \frac{\sin(\beta - \alpha)}{\cos(\beta - \alpha)}$$

$$\cos(2\phi) \cdot \cos(\beta - \alpha) - \sin(2\phi) \cdot \sin(\beta - \alpha) = 0 = \cos(2\phi + \beta - \alpha)$$

$$2\phi + \beta - \alpha = \frac{\pi}{2} \rightarrow \phi = \frac{\pi}{4} - \frac{\beta}{2} + \frac{\alpha}{2} \rightarrow \text{Merchant's relationship [radians]}$$

Geometry & Motion → Forces → Material & Energy/Power

The use of Merchant's relationship

$$\phi = \frac{\pi}{4} - \frac{\beta}{2} + \frac{\alpha}{2} \quad \leftarrow \text{Merchant's relationship [radians]}$$

As rake angle ↓ or as friction angle ↑

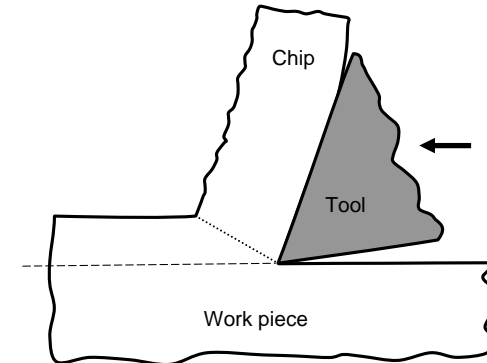
- Shear angle ↓
- Chip thickness ↑
- Energy dissipation via shear ↑
- Heat generation ↑
- Temperature ↑

Geometry & Motion → Forces → Material & Energy/Power

Power/energy requirements

What happens to energy you put in?

- Shear
- Friction
- Others?



Geometry & Motion → Forces → Material & Energy/Power

Specific energy (table from Kalpakjian)

$$u_s = \frac{\text{Energy}}{\text{Volume}} \Big|_{\text{certain conditions}}$$

Approximate Energy Requirements in Cutting Operations

Assumed for 80 % motor efficiency

	J / mm ³
Aluminum alloys	0.40 – 1.10
Copper alloys	1.40 – 3.30
Cast irons	1.60 – 5.50
Steels	2.70 – 9.30
Stainless steels	3.00 – 5.20

Geometry & Motion → Forces → Material & Energy/Power

Power and specific energy

Specific energies to consider:

Shear	+	Friction	+	Others	=	Total
$u_s = \frac{F_s \cdot V_s}{w \cdot t_o \cdot V}$		$u_f = \frac{F_f \cdot V_c}{w \cdot t_o \cdot V}$		Others		$u_t = \frac{F_c \cdot V}{w \cdot t_o \cdot V}$
$u_s = \frac{\tau_s}{\sin(\phi)} \cdot \frac{V_s}{V}$						
$u_s = \tau_s \cdot \gamma$						
~75%		~20%		~5%		100%

Geometry & Motion → Forces → Material & Energy/Power

Cutting Processes II

Reading assignment:

- 20.6 – 20.8
- 21.1 – 21.6, 21.13

Cutting processes II

Cutting processes

- Process planning, Cost, Quality, Rate and Flexibility

Modeling: Orthogonal Cutting

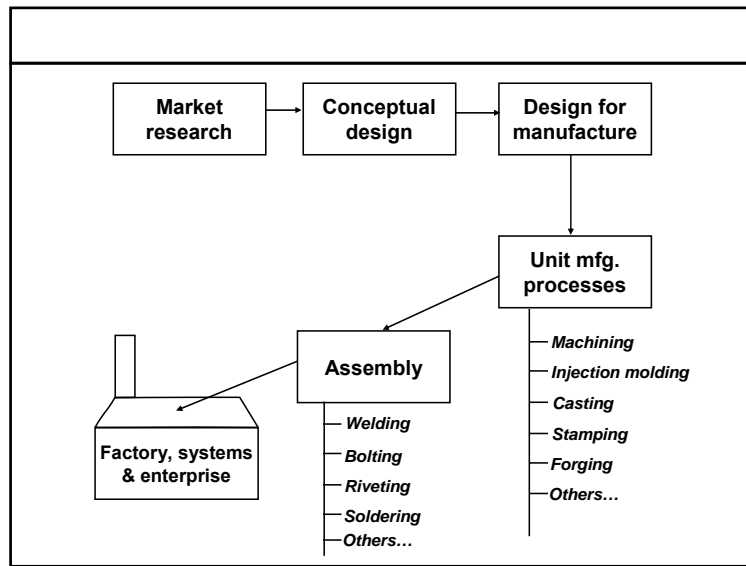
- Video, geometry, forces and power

Demonstration

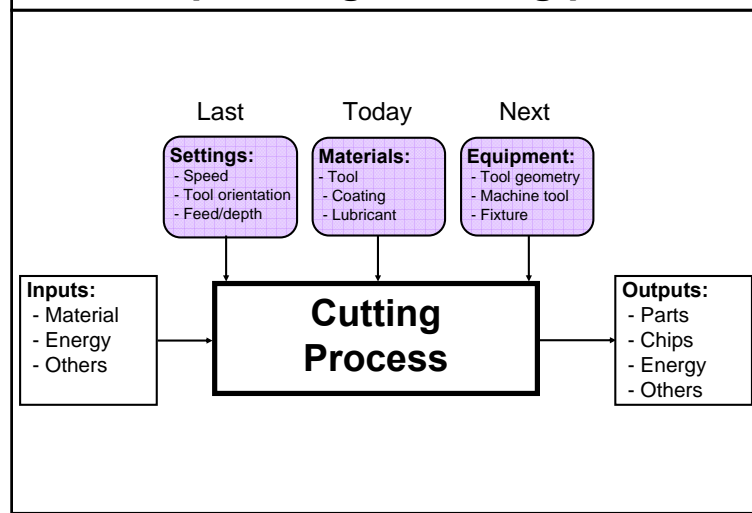
Equipment and tools

Design for Manufacturing

Process variation



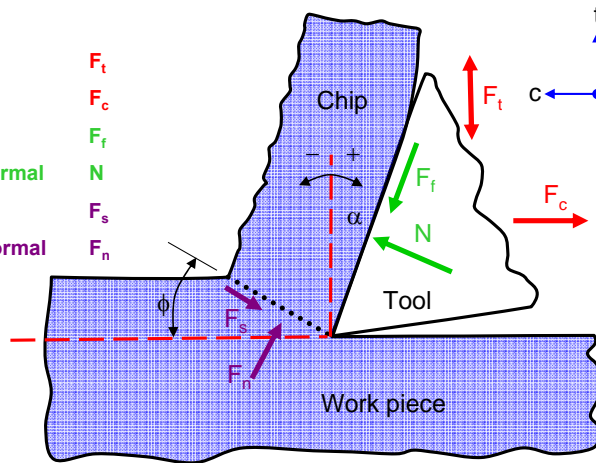
Process planning & cutting process



Review: Cutting forces

Forces:

- Thrust F_t
- Cutting F_c
- Friction F_f
- Tool normal N
- Shear F_s
- Chip normal F_n



Merchant's minimum energy assumption

Assumption: ϕ adjusts to value that minimizes cutting energy

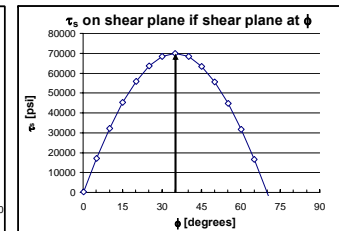
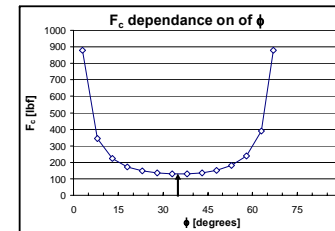
○ If Energy need to cut is minimized, F_c is minimized for a given V

$$\frac{\partial}{\partial t} (E_{cut}) = P_{cut} = F_c \cdot V$$

Minimize Minimized Minimized Constant

○ F_c is minimum when shear plane is plane of maximum shear stress

○ Example: $F_c = \text{minimum}$ and $\tau_s = \text{maximum}$ for $\phi = 35^\circ$ (for same α and β)



Merchant's relationship

Merchant's relationship:

- $\phi = \frac{\pi}{4} - \frac{\beta}{2} + \frac{\alpha}{2}$
- It is an idealization, not always accurate, BUT the trend is consistent

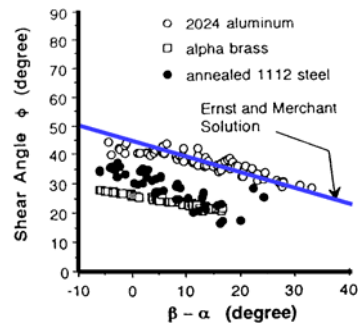


Chart adapted from: Metal Cutting Theory and Practice, Stephenson and Agapiou

Review: Power and specific energy

Specific energies to consider:

Shear energy + Friction energy + Others = Total energy

$$u_s = \frac{F_s \cdot V_s}{w \cdot t_o \cdot V}$$

$$u_f = \frac{F_f \cdot V_c}{w \cdot t_o \cdot V}$$

Others

$$u_t = \frac{F_c \cdot V}{w \cdot t_o \cdot V}$$

$$u_s = \frac{\tau_s}{\sin(\phi)} \cdot \frac{V_s}{V}$$

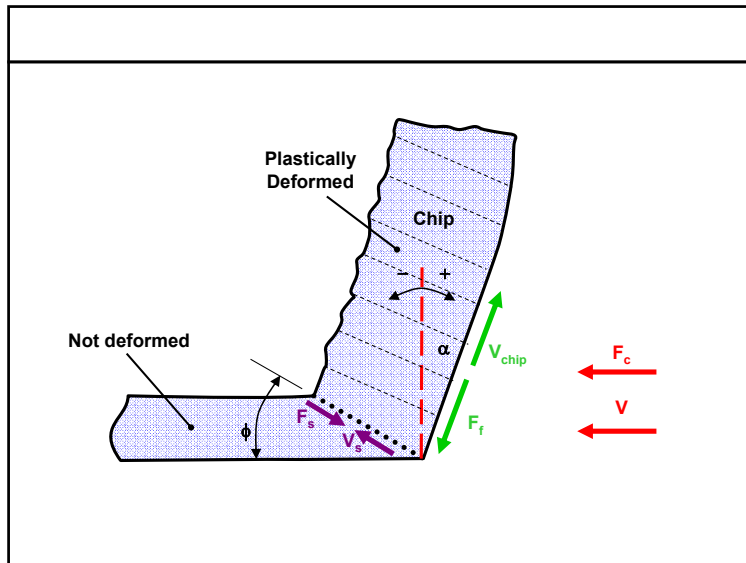
$$u_s = \tau_s \cdot \gamma$$

~75%

~20%

~5%

100%



Caution on modeling and reality

Our assumptions:

- Slow, orthogonal cutting
- Material properties invariant
- Constant temperature
- Simple sliding friction
- No strain hardening

Use our analysis for:

- Trends & building intuition
- Basis for detailed study

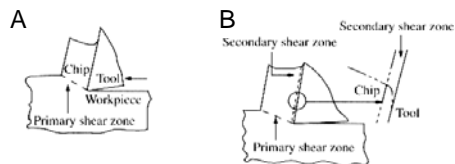
Chip types (source: Kalpakjian)

A) Continuous chip with narrow primary shear zone

- Ductile materials @ high speed
- Bad for automation (use chip breakers)

B) Secondary shear zone at chip-tool interface

- Secondary shear zone -> increased energy dissipation



Source: Kalpakjian

Chip types (source: Kalpakjian)

D) Continuous chip with build up edge (BUE)

- High plastic working and bad for automation

E) Serrated chip:

- Low thermal conductivity materials

F) Discontinuous chip (good chips)

- Low ductility materials and/or negative rake angles



Source: Kalpakjian

CUTTING DEMONSTRATION

Example

Given:

- t_o
- w
- ω
- P_{lathe}

Find:

- Velocity at which lathe stalls
- Cutting force

TOOL MATERIALS AND TOOL WEAR

Cutting tool requirements

Maintain:

- Hardness at operating temperature
- Toughness
- Low wear rate

Should be easy to repair/sharpen

Tool-part combination should be chemically inert

- Diamond and steel....

Cutting tool characteristics

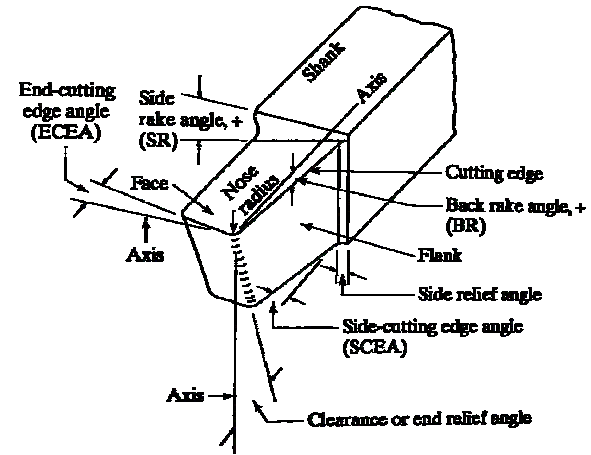
Why do we worry about tool wear?

- Tool can cease to cut Dimensional accuracy
- Surface finish Cutting force/power
- Cost Flexibility Rate Quality

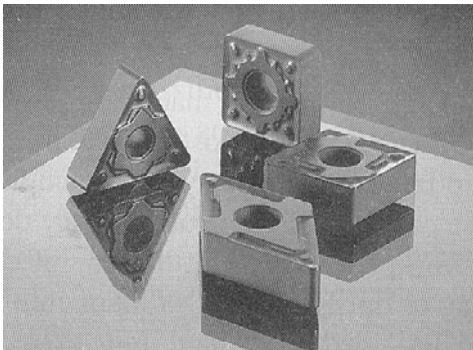
Is a function of many parameters

- Coolant Geometry Lubricant Process parameters

Cutting tools: Geometry



Cutting tools: Geometry

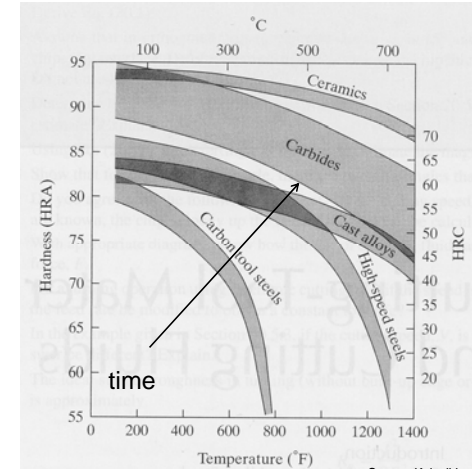


Source: Kalpakjian

Tooling hardness and temperature

Things to note:

- Performance ↑
- Rate of change ↓

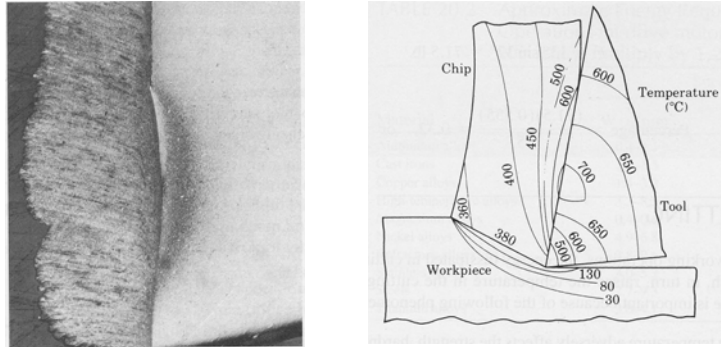


Source: Kalpakjian

Temperature and wear

Diffusion is thought to dominate crater wear

This is a function of temperature



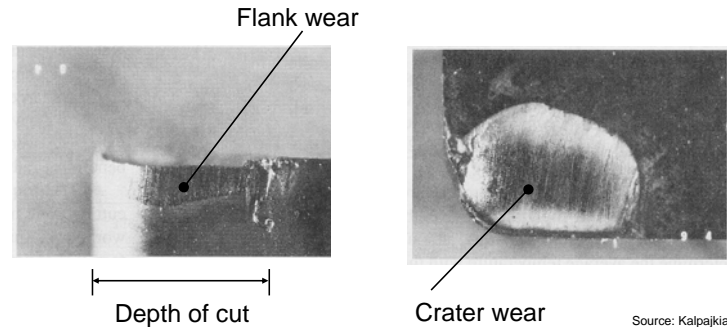
Source: Kalpakjian

Tool wear up close

Crater wear affected by same parameters as flank wear

In addition:

- Material affinity and temperature

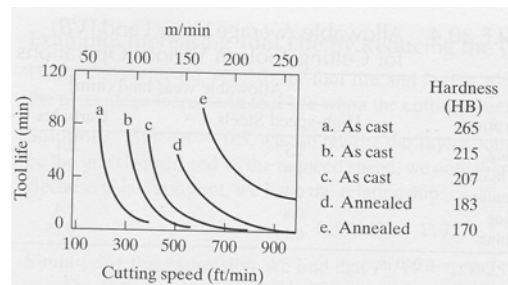


Source: Kalpakjian

Taylor's wear relationship (flank wear)

Relationship between tool life and cutting speed

- Use to set optimum cutting speed for CFRQ
- Represents a given wear condition
- Define wear condition for failure



Source: Kalpakjian

Defining tool failure

Wear "snowballs" to set limit

Force/power increase to set limit

Surface finish becomes unacceptable

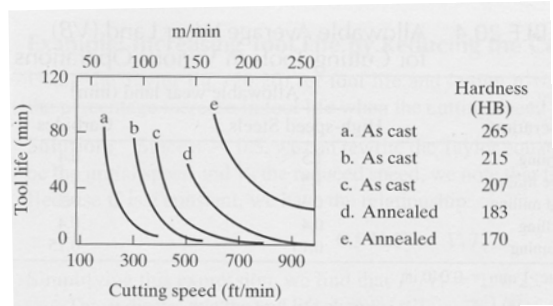
Wear land size for given process

Taylor's wear relationship (flank wear)

C = constant & n = exponent (from experimental data)

$$v \cdot t^n = C$$

v = cutting velocity (fpm) t = time to failure (min)



Source: Kalpakjian

Taylor's tool life curves (Experimental)

Coefficient n varies from:

Steels

Ceramics

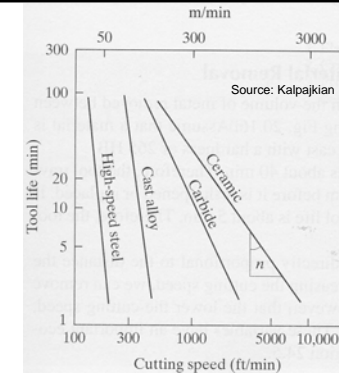
0.1

0.7

$$v \cdot t^n = C$$

v = cutting velocity (fpm)

t = time to failure (min)



As n ↑, wear is less sensitive to cutting speed

Preventing tool failure with coatings

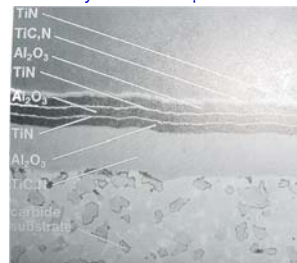
Tools may be coated for many reasons:

- Chemically inert
- Temperature resistance
- Surface energy/specific energy
- Low friction

Common coatings

- Titanium nitride (TiN)
- Cubic boron nitride (CBN)
- Multi-phase coatings

Multi-phase coating
Layers ½ – 10 μm thick



CUTTING PROCESS DFM

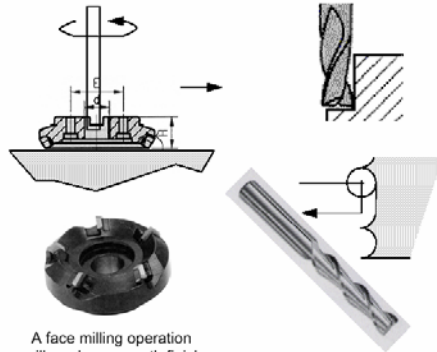
DFM for cutting: Surface roughness

Surface roughness:

- Definition

Depends on :

- Mass removed
- Size of tool
- Cutter
- Speed



A face milling operation will render a smooth finish

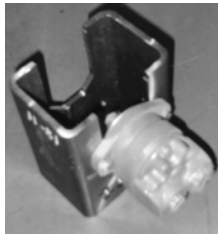
Side milling with an end-mill will give you some surface roughness.

Finish by process (source = machinery handbook)

Process	ROUGHNESS AVERAGE, R_a —MICROMETERS μm (MICROINCHES $\mu in.$)												
	50 (2000)	25 (1000)	12.5 (500)	6.3 (250)	3.2 (125)	1.6 (63)	0.80 (32)	0.40 (16)	0.20 (8)	0.10 (4)	0.05 (2)	0.025 (1)	0.012 (0.5)
Flame Cutting													
Snagging													
Sawing													
Planing, Shaping													
Drilling													
Chemical Milling													
Elect. Discharge Mach.													
Milling													
Broaching													
Reaming													
Electron Beam													
Laser													
Electro-Chemical													
Boring, Turning													
Barrel Finishing													
Electrolytic Grinding													
Roller Burnishing													
Grinding													
Honing													
Polishing													
Lapping													

DFM for cutting: Part geometry

Thin sections and tubes (vibration)



Overhanging parts

Inclined planes and drilling....



DFM for cutting: Ala features

Use common dimensions / parts / shapes / sizes

- Proper tolerance
- Use common/important datums
- Standard features (i.e. don't use octagon shaped holes)

DFM for cutting: Ala tooling

Avoid deep pockets and holes

Design should include real shape tool makes

- Tapped holes
- Pocket corners

DFM for cutting: Ala equipment

Beware of fixturing needs

- Minimize number of fixture cycles
- Design an interface for part-fixture

Machine and tool access to create features