



Herbert Wertheim  
College of Engineering  
UNIVERSITY of FLORIDA

# Sunseekers Heliostat

Section 20722, Group 284H

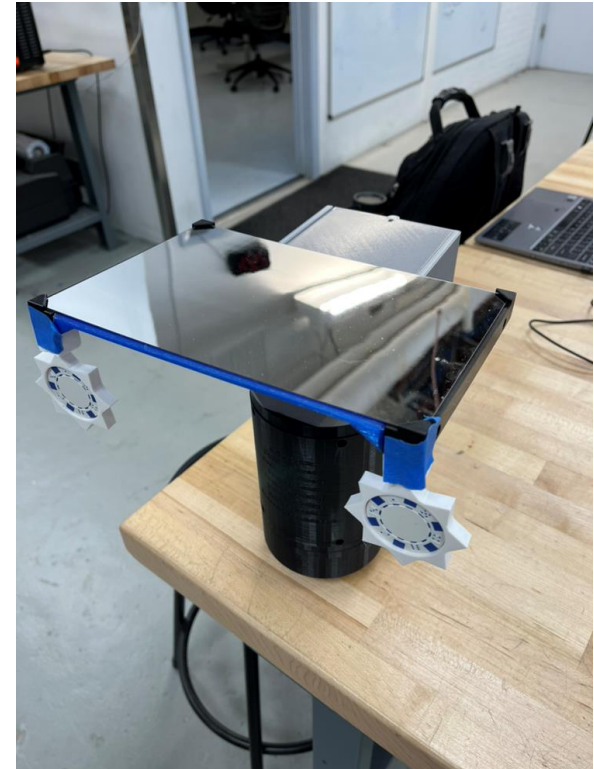
Alexander Lacerna, Elijah Crain, Jacob Jenkins,  
James Soto, Jennifer Brett, Joshua Brett, Olivia  
Dodge



# Hedgehog Concept and Value Proposition

Low maintenance and easily serviceable heliostat

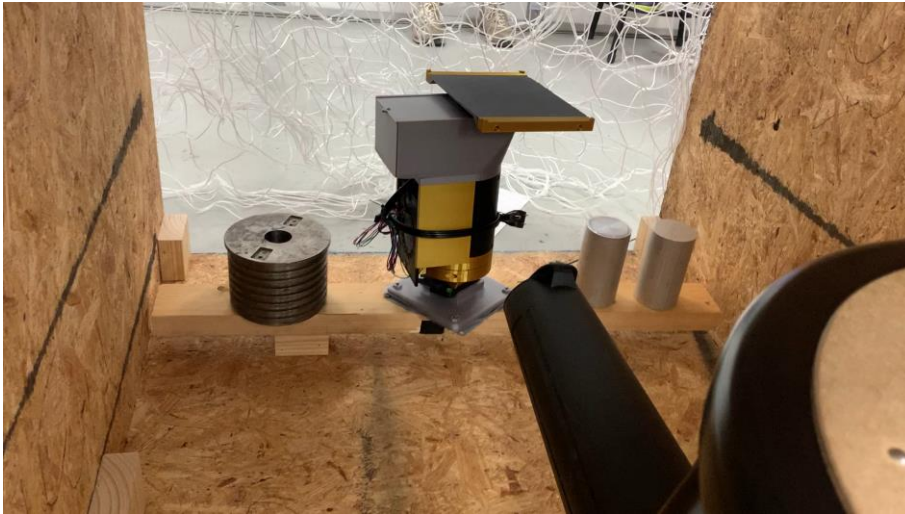
- Motors, wiring, electronics, and most moving parts contained within the body
- Conventional bulkhead plug to exterior power source
- Multiple ports of entry to service internal parts
- 3D-printed structural components



# Key Specifications

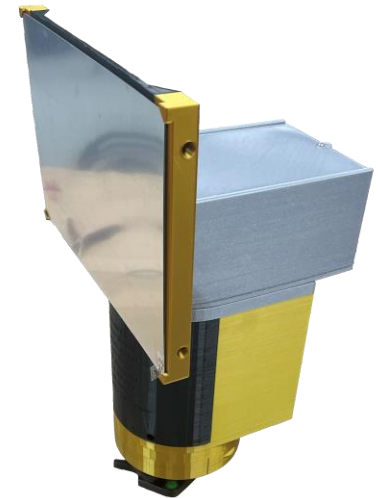
- 360 degrees of azimuthal rotation, 90 degrees of elevation
  - Azimuth resolution:  $0.08^\circ$
  - Elevation resolution:  $0.12^\circ$
- Survived winds of over 120 MPH in testing
- OTS power supply, motor drivers, stepper motors, mirror, sensors, limit switches, microcontroller, and motor drivers
- Compact size: 23.5 cm x 18.0 cm x 35 cm
- High resistance to back-drive

# Wind Survivability Test



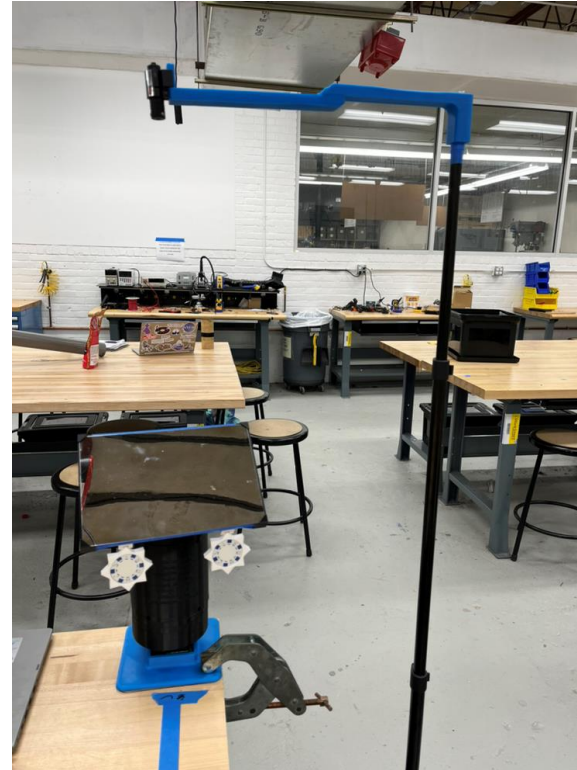
Video courtesy of Dr. Matthew Traum, University of Florida

- Leaf blower (very high tech)
- 120 mph wind
- No damage

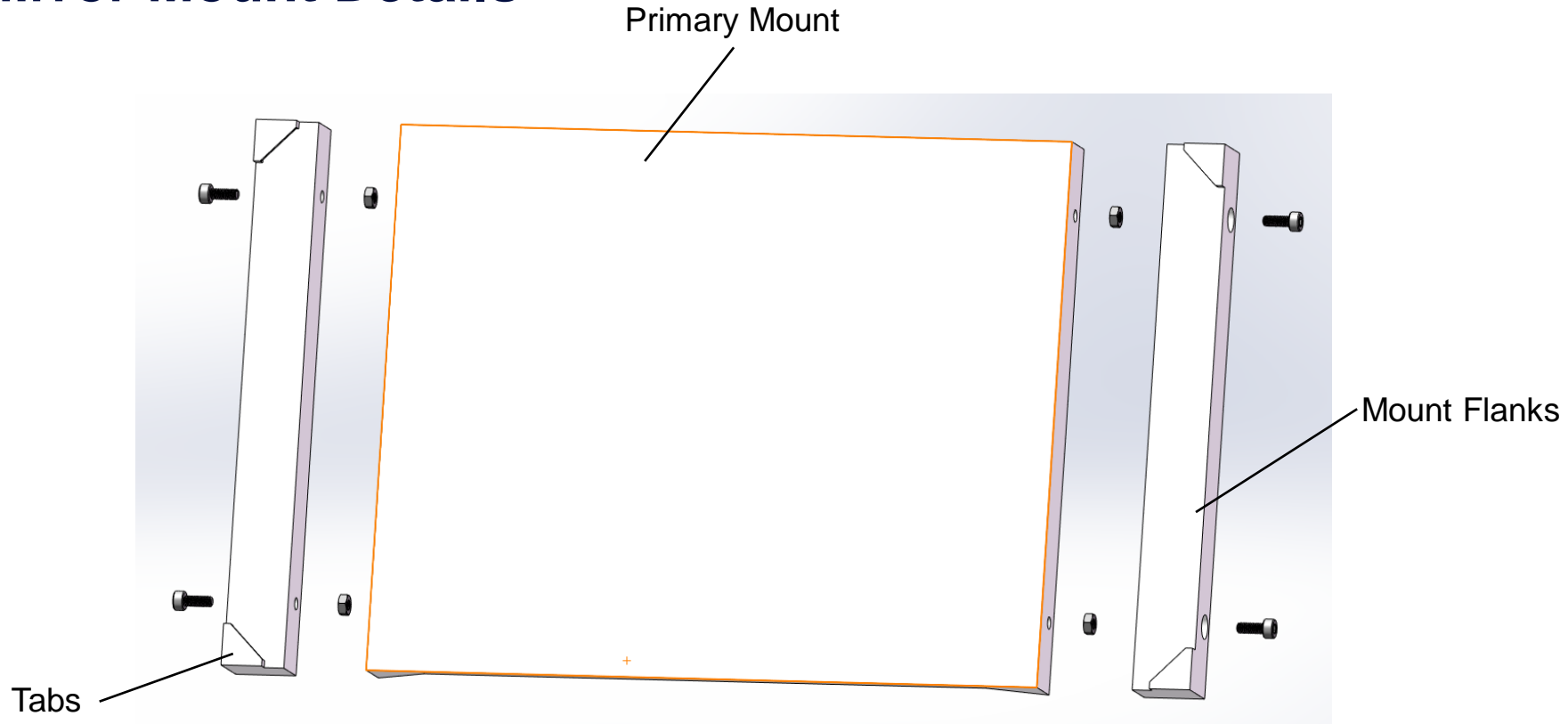


Rain/hail safety mode

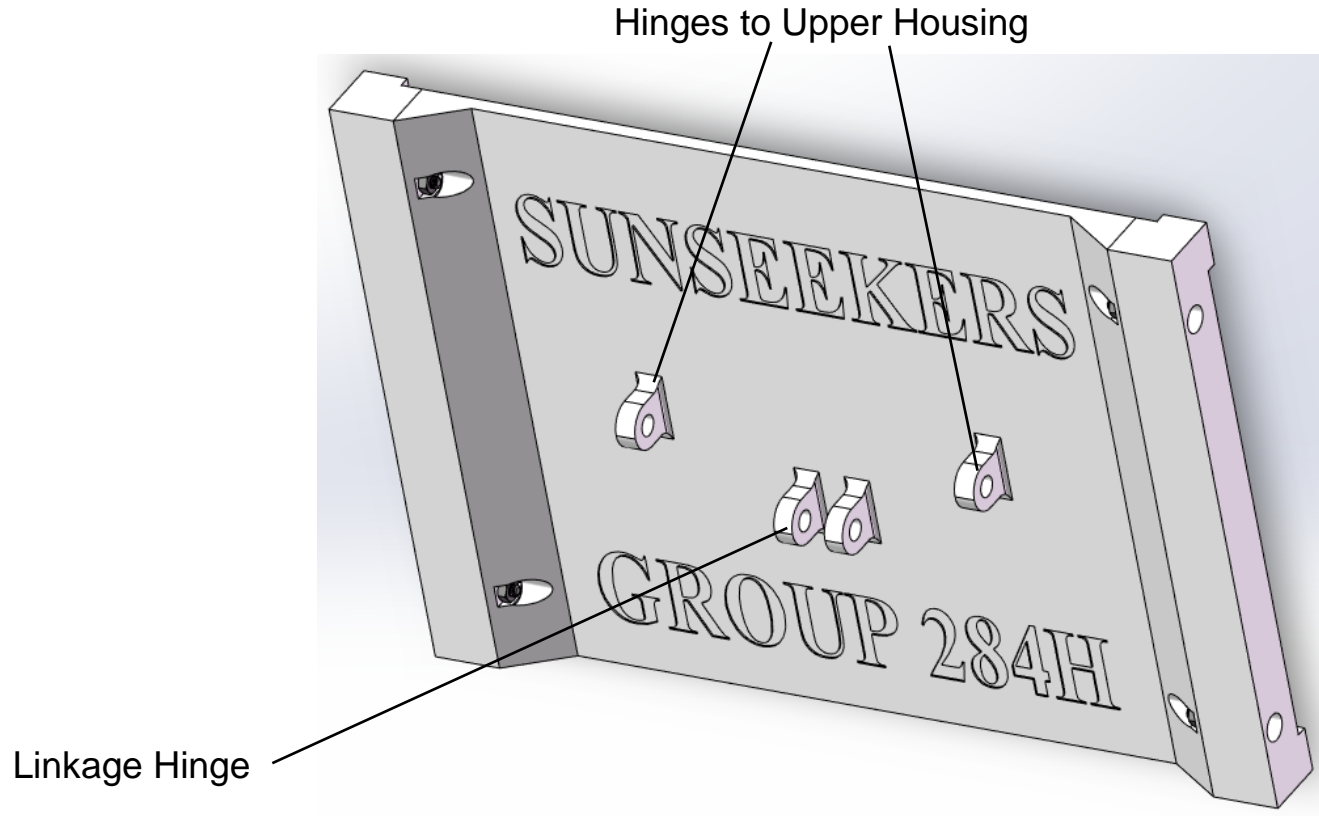
# Laser Reflection Targeting Test



# Mirror Mount Details

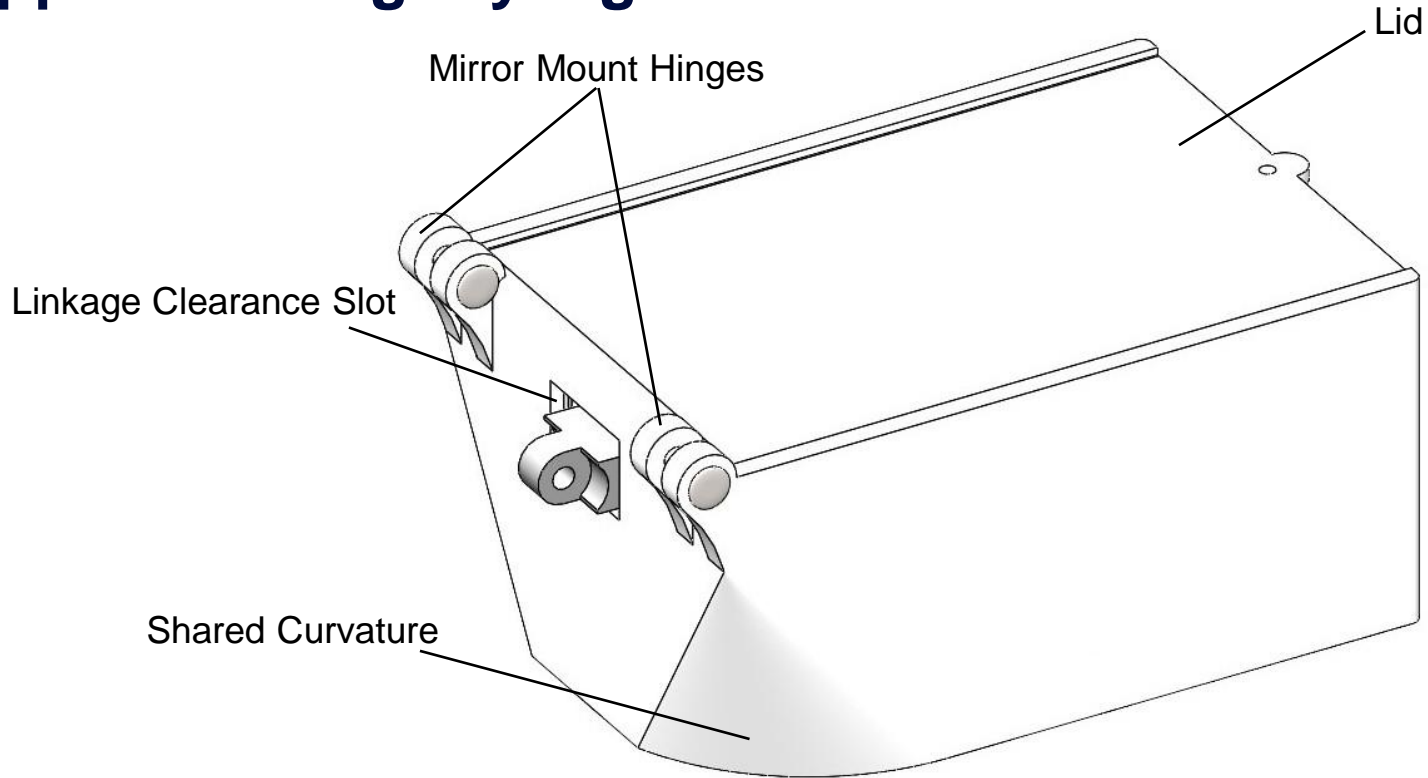


# Mirror Mount Details



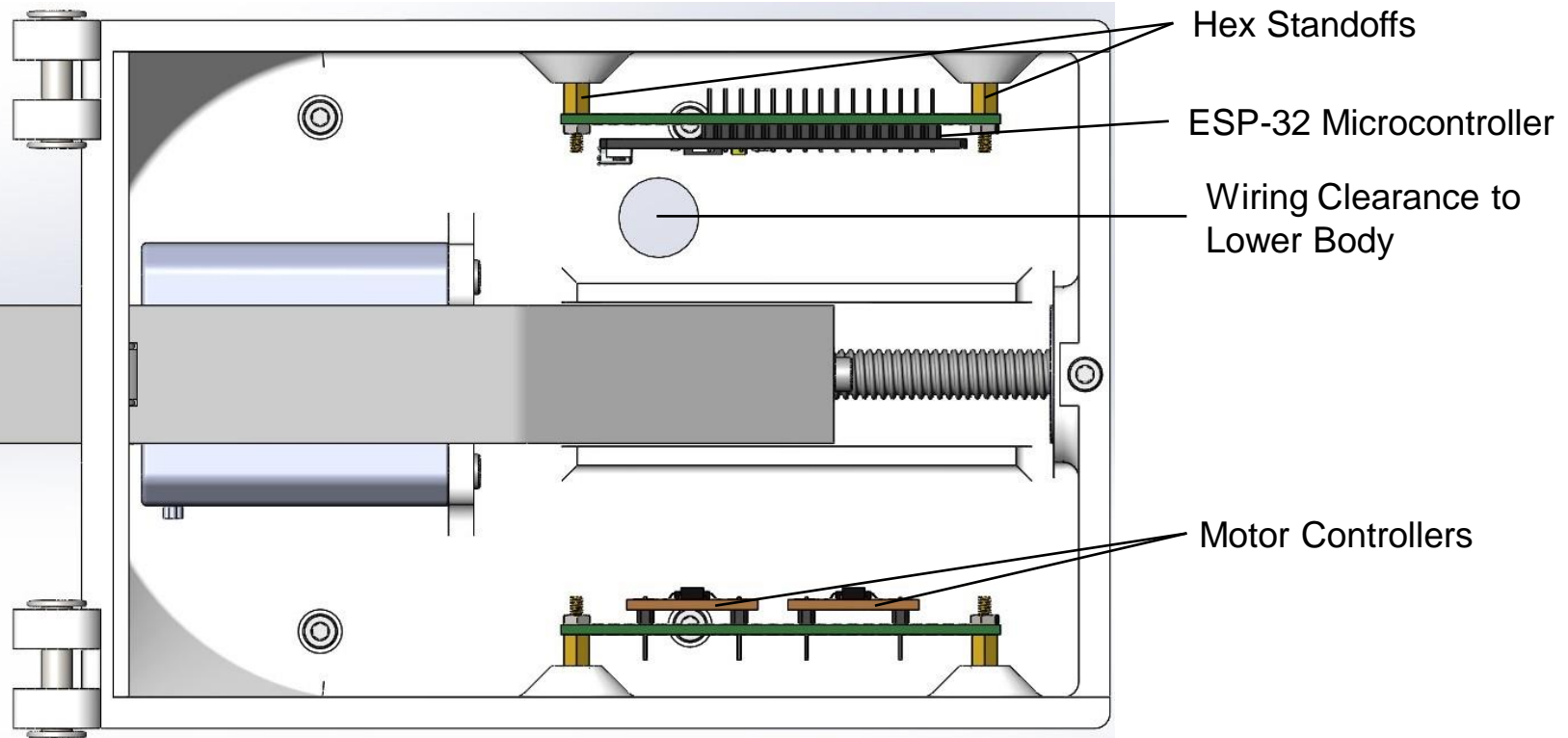


# Upper Housing Styling

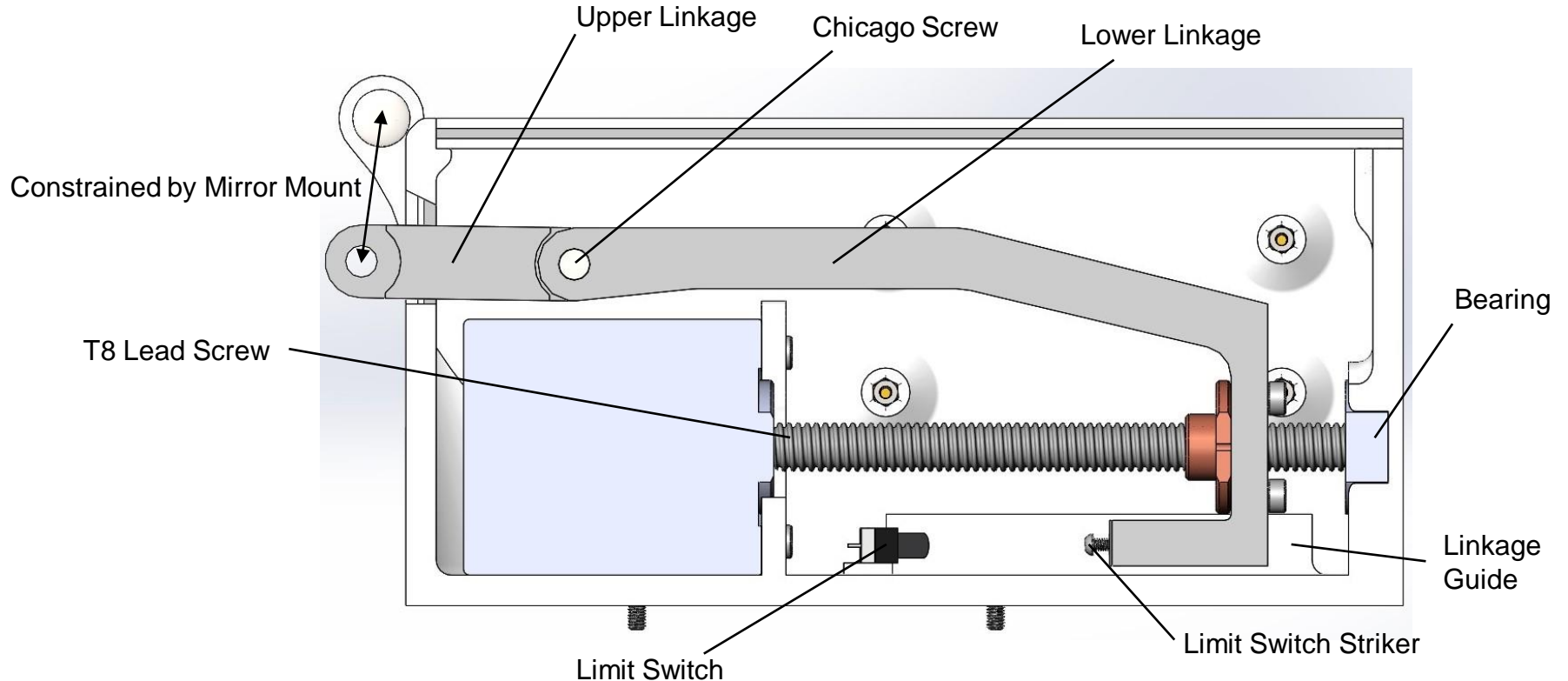




# Upper Housing Electronics and Wiring Provisions

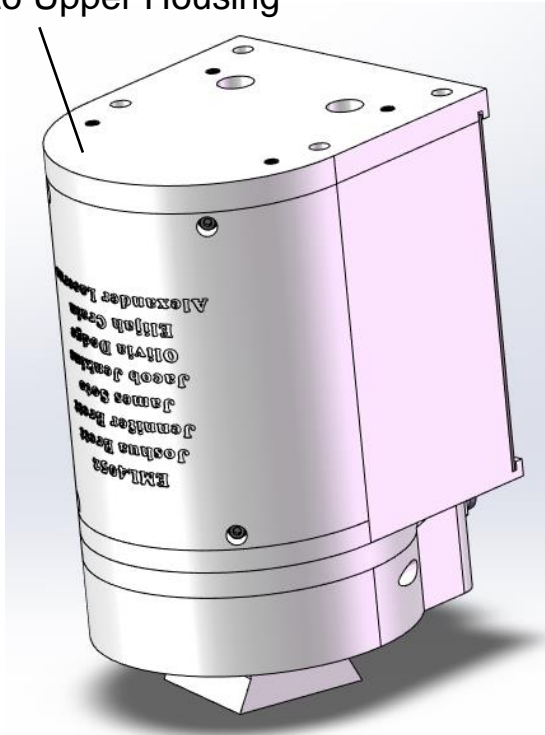


# Lead Screw, Linkage, and Elevation Limit Switch

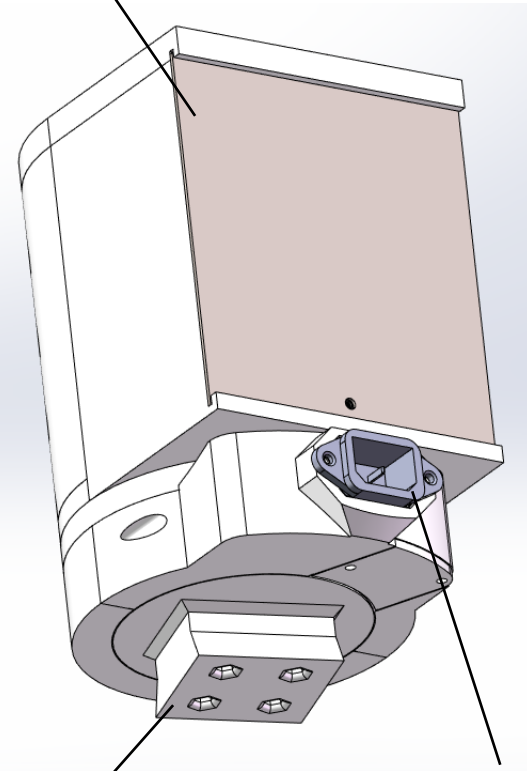


# Lower Housing Styling

Attachment to Upper Housing



Sliding Panel

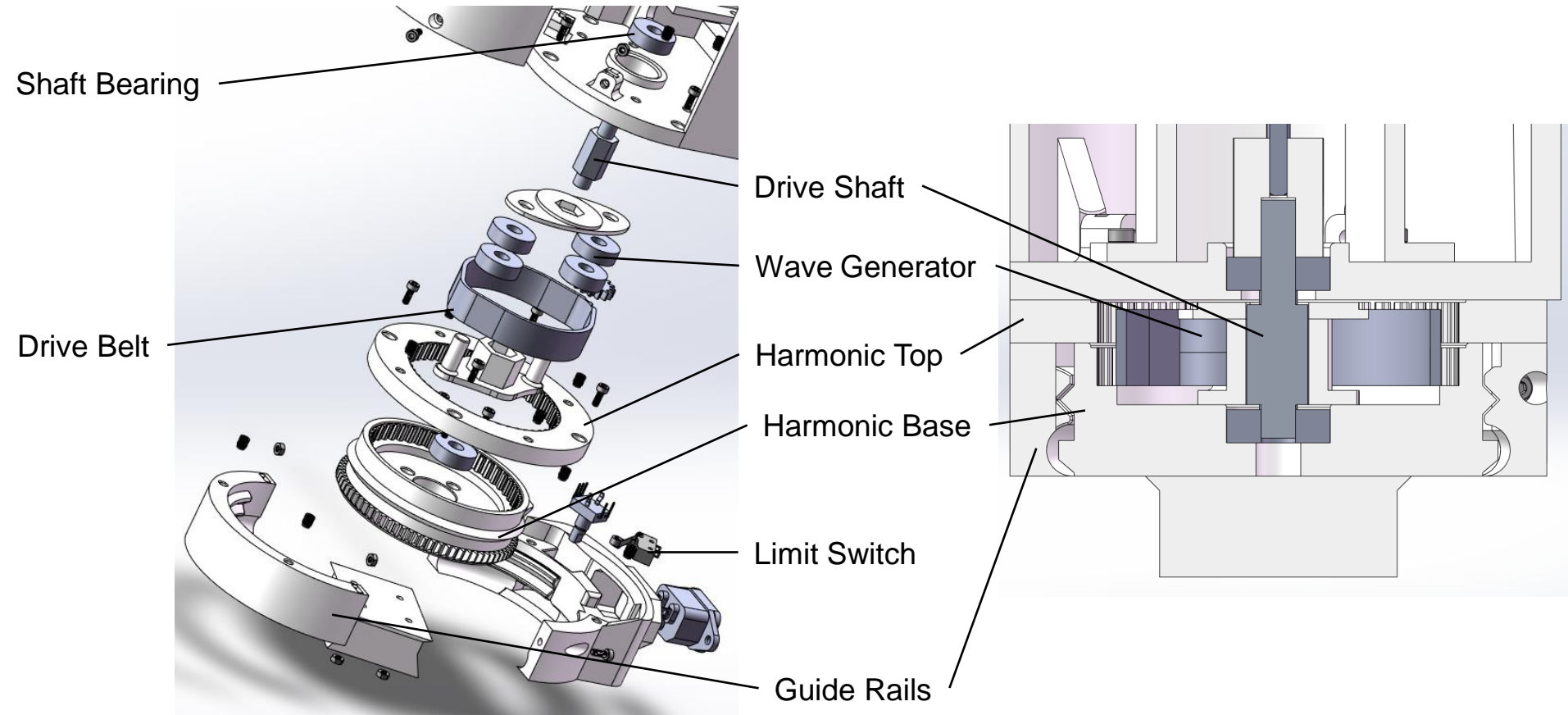


Quick-Release Mount

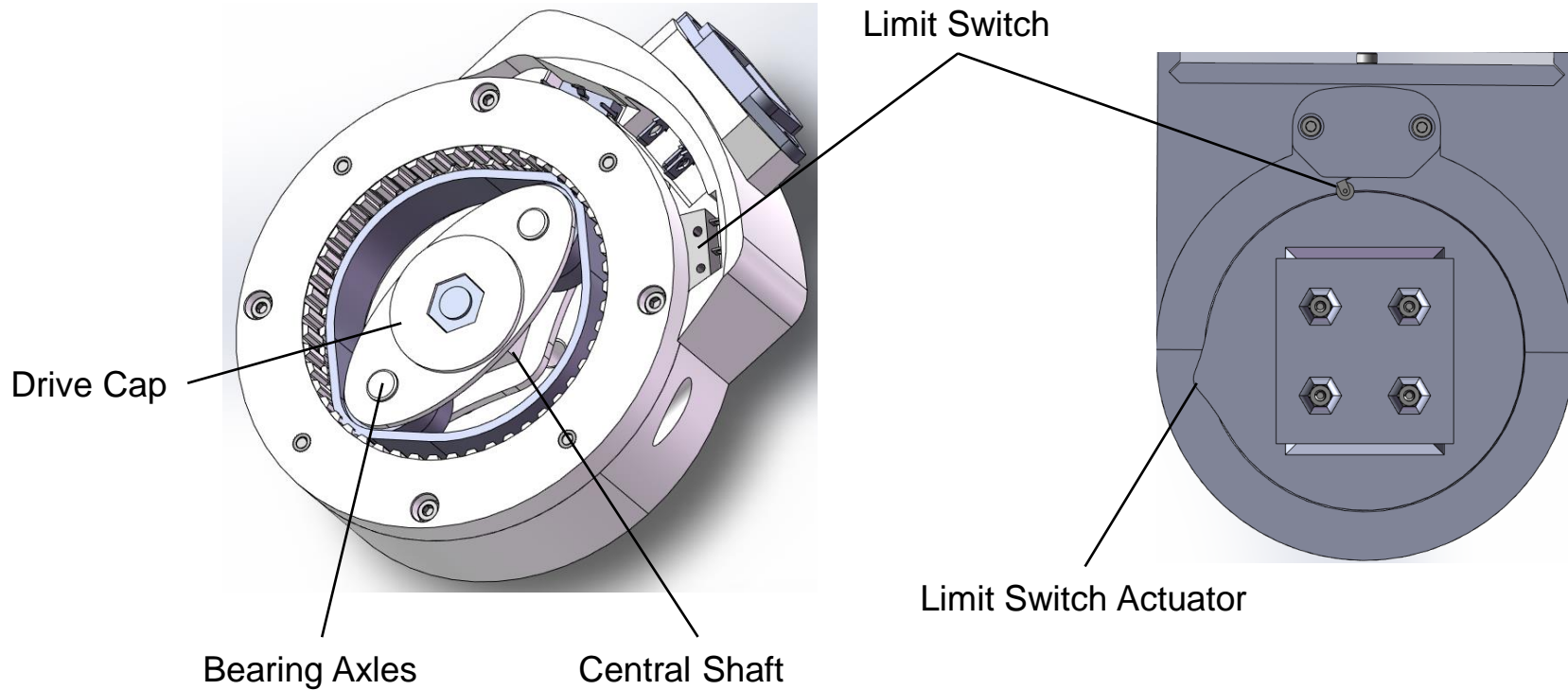
Bulkhead Plug



# Lower Housing Key Features

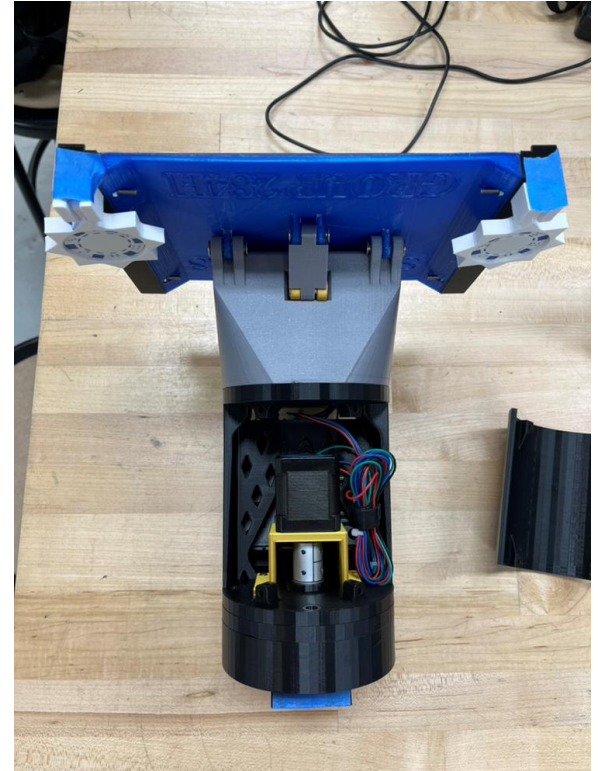
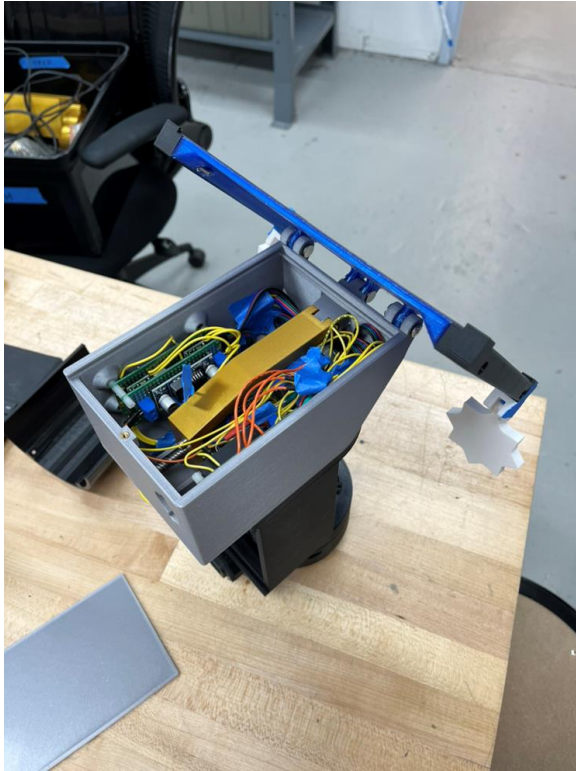


# Azimuthal Rotation Mechanism





# Internal Wiring & Power Connections





# Design Analysis – Mirror Mount

Bending analysis to determine required thickness

- Flat plate model
- Resultant load from 90 MPH wind pressure acting with a lever arm of 115 mm

- $\sigma_{max} = \frac{M * \frac{t}{2}}{I} = 7.5 \text{ MPa for } n = 2$

- $F = qA = \frac{1}{2} \rho v^2 lw = 17.5 \text{ N}$

- $I = \frac{bt^3}{12}$

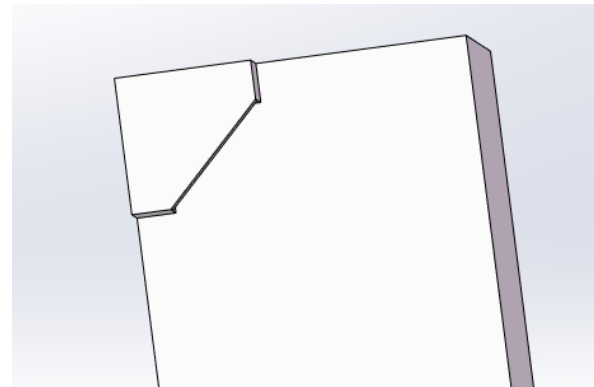
- $t_{min} = 3.236 \text{ mm}$

- $t = 4 \text{ mm used in design}$

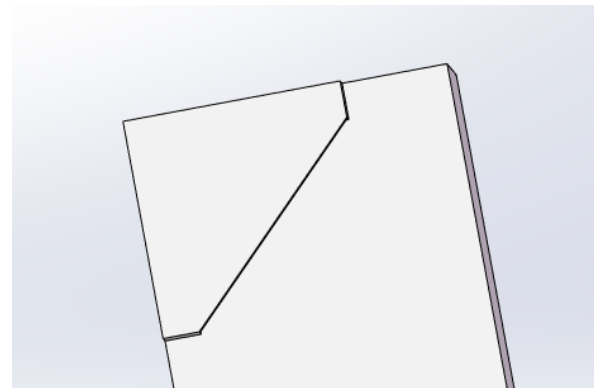
# Design Evolution – Mirror Mount

## Mirror attachment method

- Originally planned to use mirror adhesive
- V1: 5 mm leg tabs
- V2: 10 mm leg tabs



V1 mirror tabs

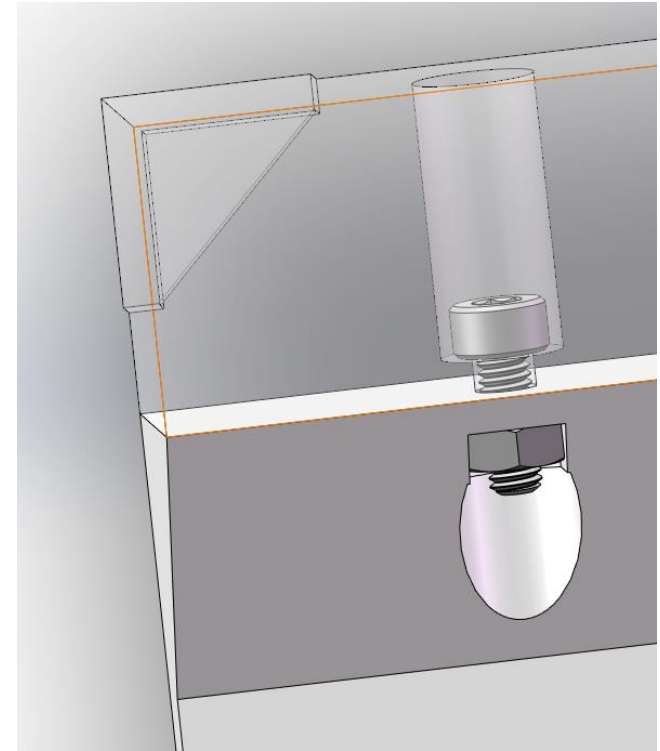


V2 mirror tabs

# Design Evolution – Mirror Mount

## Mount flank attachment method

- V1: Strong adhesive
- V2: M3 fasteners with pocket holes and hex profile
  - Already used in other parts of the assembly

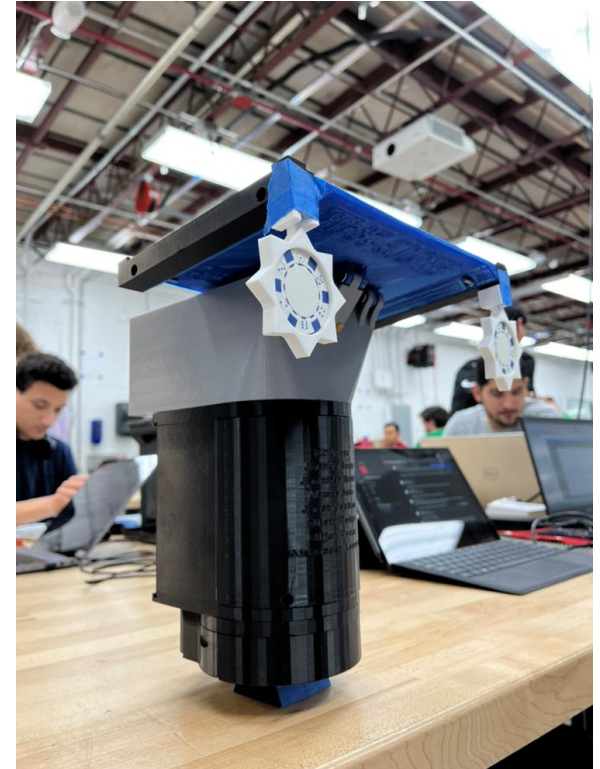


V2 mirror mount flank attachment

# Design Evolution – Mirror Mount

## Counterweights

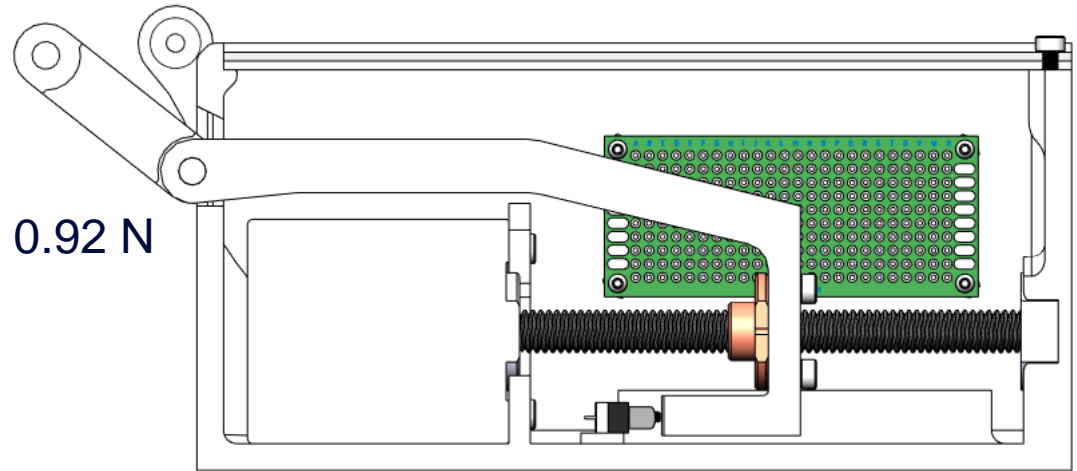
- Slack observed in elevation control
- Counterweights added to maintain consistency
- Final production weights will be heavier



# Design Analysis – Linkage

Bending analysis to determine required thickness

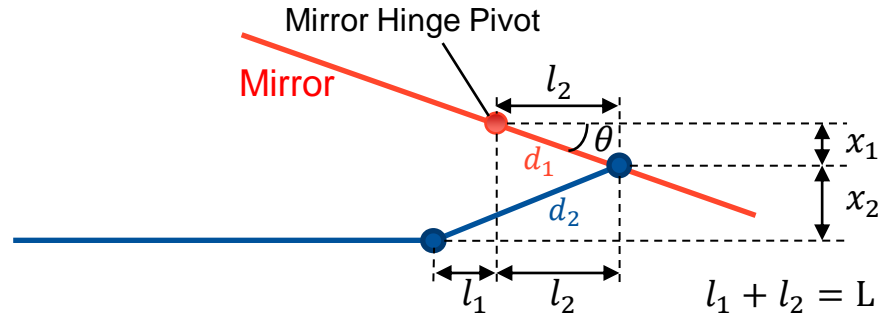
- Modeled as a cantilever beam
- $\delta = \frac{FL^3}{3EI}$
- Static loading force: 0.56 N
- Clearance: 0.565 mm
- Force to cause interference: 0.92 N



# Design Analysis – Linkage Kinematics

## Elevation range of motion

- Find required distance  $l_1$  linkage must move for a desired elevation angle  $\theta$ .
- Convert  $l_1$  to a required step rotation by the stepper motor.



Side View Schematic

# Design Analysis - Housing

## Internal Temperature Analysis (for electronics)

2 motor drivers (1A, 12V) = 24 W

Voltage regulator (4.5 A, 12V) = 54 W

Power out to motor (2 A, 12V) = 24 W

- $\dot{W}_{in} = 78 \text{ W}$

- $\dot{W}_{out} = 24 \text{ W}$

- $\dot{Q}_{out} = q_{rad} + q_{conv} = 54 \text{ W}$

- $q_{rad} = A_s(\epsilon\sigma T_s^4 - \alpha G)$

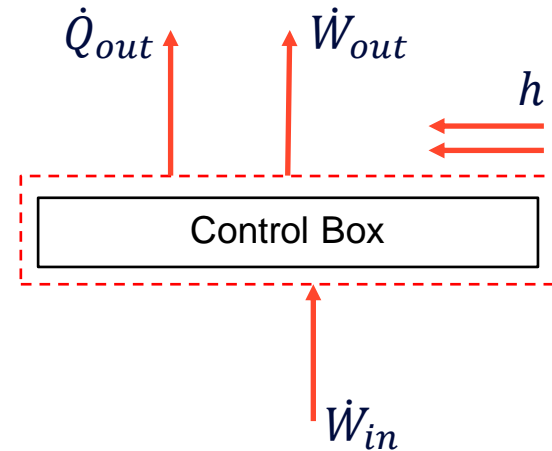
- $q_{conv} = hA_s(T_s - T_\infty)$

- Solve for  $T_s$ :

- $A_s(\epsilon\sigma T_s^4 - \alpha G) + hA_s(T_s - T_\infty) = 54 \text{ W}$

- $0.03775 \text{ m}^2 \left[ \left( (0.39) \left( 5.67 \times 10^{-8} \frac{\text{W}}{\text{m}^2 \cdot \text{K}^4} \right) (T_s^4) - (0.31) \left( 1367 \frac{\text{W}}{\text{m}^2} \right) \right) + \left( 20 \frac{\text{W}}{\text{m}^2 \cdot \text{K}} \right) (T_s - 313.55 \text{ K}) \right]$

- $T_s = 324.48 \text{ K} = 51.33 \text{ }^\circ\text{C}$





# Cost Table Summary

- Prototype and 3,000-unit production run unit cost

Prototype Cost		Mass Production Cost	
3-D printed parts	\$28.75	3-D printed parts	\$24.73
Machined parts	\$13.72	Machined parts	\$11.57
Provided OTS parts	\$98.39	Provided OTS parts	\$77.73
Chosen OTS parts	\$39.14	Chosen OTS parts	\$29.36
Total cost	\$178.27	Total cost	\$143.39
Total cost excluding provided OTS parts	\$81.61	Total cost excluding provided OTS parts	\$65.66

## Summary

This design is focused on ease of construction as well as ease of maintenance. With multiple points of access all functional parts can be accessed and modified readily. Furthermore, this design is protected against its environment with fully shielded motors and electronics, dust and debris is no concern. The orthogonal drive system operates well under the required 0.5 degrees of accuracy to provide optimal power output to the receiving tower.

With readily removable paneling, integrated electronics, and simple thoughtful design, this heliostat is optimal for in field performance and maintenance.

# Conclusion

## Key Features

- 360 degrees of azimuthal rotation, 90 degrees of elevation
  - Azimuth resolution:  $0.08^\circ$
  - Elevation resolution:  $0.12^\circ$
- 120+ MPH wind stability
- Compact size: 23.5 cm x 18.0 cm x 35 cm
- Wi-Fi controllability
- Low compliance
- Simple assembly and maintenance
- Shielded motors and electronics
- Cost is \$28.39 under budget

