

Design of Mat/Raft Foundation

- Mat or raft foundation is a large concrete slab supporting several columns in two or more rows.
- It is used where the supporting soil has low bearing capacity.
- The bearing capacity increased by combining all individual footings in to one mat –since bearing capacity is proportional to width and depth of foundations.
- In addition to increasing the bearing capacity, mat foundations tend to bridge over irregularities of the soil and the average settlement does not approach the extreme values of isolated footings.
- Thus mat foundations are often used for supporting structures that are sensitive to differential settlement.

- **Design of uniform mat**
- Design Assumptions
 - mat is infinitely rigid
 - planner soil pressure distribution under mat
- **Design Procedure**
 - I. Determine the line of action of the resultant of all the loads acting on the mat
 - II. Determine the contact pressure distribution as under
 - If the resultant passes through the center of gravity of the mat, the contact pressure is given by

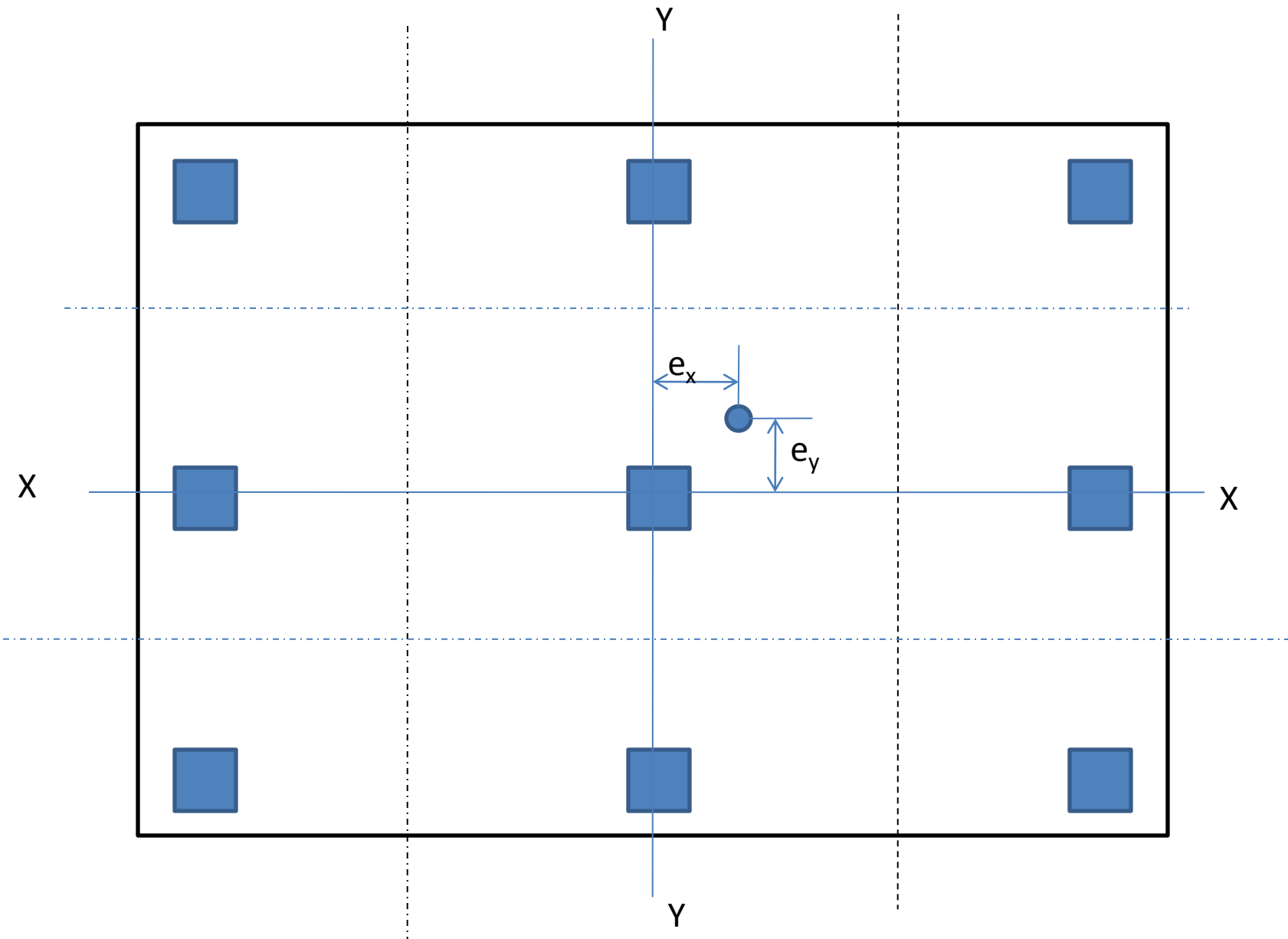
$$\sigma = \frac{Q}{A}$$

- If the resultant has an eccentricity of e_x and e_y in the x and y direction

$$\sigma_{\max/\min} = \frac{Q}{A} \pm \frac{Qe_x}{I_{yy}} x \pm \frac{Qe_y}{I_{xx}} y$$

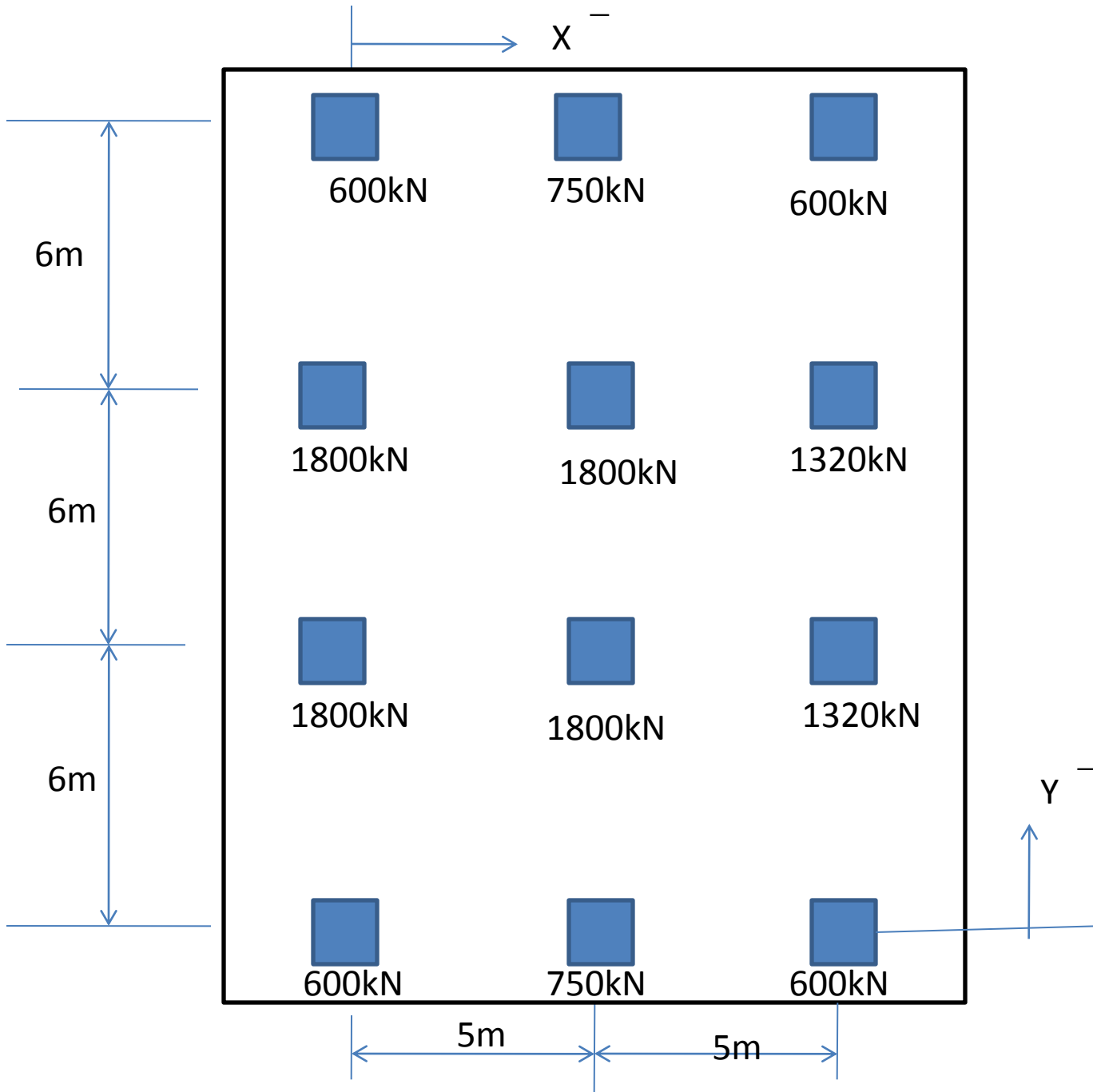
The maximum contact pressure should be less than the allowable soil pressure

- Divide the slab mat into strips in x and y directions. **Each strip is assumed to act as independent beam subjected to the contact pressure and the columns loads.**
- Determine the modified column loads
- Draw the shear force and bending moment diagrams for each strip.
- Select depth of mat for shear requirement
- Select steel reinforcement for moment requirement



• Example

- A mat foundation is to be design by the conventional method (rigid method) for the loadings shown in Fig. below.
 - All columns are 40X40cm
 - Ultimate soil bearing pressure , $q_{ult} = 100\text{kPa}$
 - $f_{yk} = 300\text{MPa} \Rightarrow f_{yd} = 300/1.15 = 260.87 \text{ Mpa}$
 - C25 $\Rightarrow f_{ck} = 20\text{MPa} \Rightarrow f_{ctk} = 1.5 \text{ MPa},$



- **Location of c.g. of loads**

- $\sum P = (600 + 750 + 600) * 2 + (1800 + 1800 + 1320) * 2 = 13740 \text{ kN}$

- $13740 \bar{X} = (750 + 1800 + 1800 + 750) * 5 + (600 + 1320 + 1320 + 600) * 10$

$$\bar{X} = 4.65 \text{ m}$$

$$e_x = 5 - 4.65 = 0.35$$

$$X' = 5 + 0.35 = 5.35 \text{ m}$$

- $B_{\min} = 2 * (5.35 + 0.20 + 0.15) = 11.40 \text{ m}$

- $13740 \bar{Y} = (600 + 750 + 600) * 18 + (1800 + 1800 + 1320) * 12 + (1800 + 1800 + 1320) * 6$

$$\bar{Y} = 9 \text{ m}$$

$$e_y = 6 + 6/2 - 9 = 0$$

- $L_{\min} = 2 * (9 + 0.20 + 0.15) = 18.70 \text{ m}$

- **Dimension of Mat 11.40 X 18.70m**

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- Actual contact pressure

$$\sigma = \Sigma P / (BL) = 13740 / (11.40 * 18.70) = 64.45 \text{ kPa} < \sigma_{ult} = 100 \text{ kPa}$$

- Thickness of the mat

- Punching shear

- Punching shear under 1800kN load

Take $d = 0.70 \text{ m}$ and $\rho = \rho_{min} = 0.50 / f_{yk} = 0.50 / 30$

$$k_1 = (1 + 50\rho) = (1 + 50 * 0.0017) = 1.085$$

$$k_2 = 1.6 - d = 1.6 - 0.70 = 0.90, \text{ Take } K_2 = 1$$

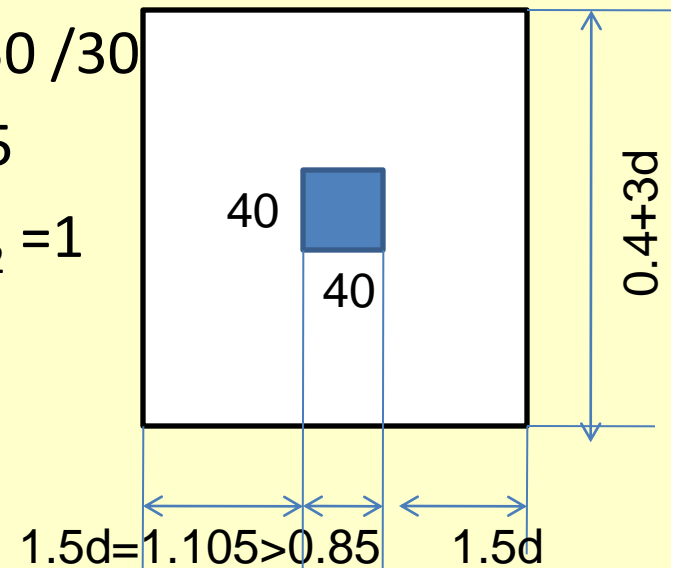
$$P_r = (0.85 + 0.4 + 1.105)2 + (0.4 + 3(0.70))$$

$$= 7.21 \text{ m}$$

- Net shear force developed

$$V_d = 1800 - \sigma * (2.355 * 2.50), \quad \sigma = 64.45 \text{ kPa}$$

$$V_d = 1800 - 64.45 * (2.355 * 2.50) = 1420.55 \text{ kN}$$



- Punching shear resistance

$$V_{up} = 0.25f_{ctd} k_1 k_2 u d \quad (\text{MN})$$

- $V_{up} = 0.25 * 1000 * 1.085 * 1.00 * 7.21 * 0.70$
 $= 1369.00 \text{ kN} < V_d \dots$ **NOT OK! Increase the depth**

Take $d = 0.75 \text{ m}$ and $\rho = \rho_{min} = 0.50 / f_{yk} = 0.50 / 300 = 0.0017$

$$k_1 = (1 + 50\rho) = (1 + 50 * 0.0017) = 1.085$$

$$k_2 = 1.6 - d = 1.6 - 0.75 = 0.85, \text{ Take } K_2 = 1$$

$$P_r = (0.85 + 0.4 + 1.125)2 + (0.4 + 3(0.75))$$

$$= 7.40 \text{ m}$$

- Net shear force developed
- $V_d = 1800 - \sigma * (2.375 * 2.65), \sigma = 64.45 \text{ kPa}$
- $V_d = 1800 - 64.45 * (2.375 * 2.65) = 1394.37 \text{ kN}$

- Punching shear resistance

$$V_{up} = 0.25f_{ctd} k_1 k_2 u d \quad (\text{MN})$$

- $V_{up} = 0.25 * 1000 * 1.085 * 1.00 * 7.40 * 0.75$
 $= 1505.44 \text{ kN} > V_d \dots \text{OK!}$

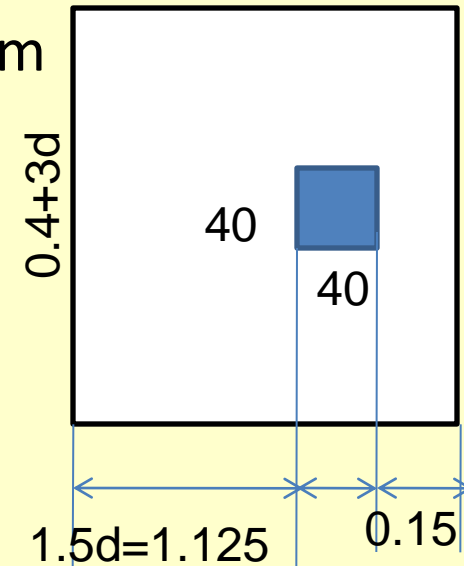
- Check punching shear under 1320kN

$$P_r = (1.125 + 0.15 + 0.4)2 + (0.4 + 3(0.75)) = 6.00 \text{ m}$$

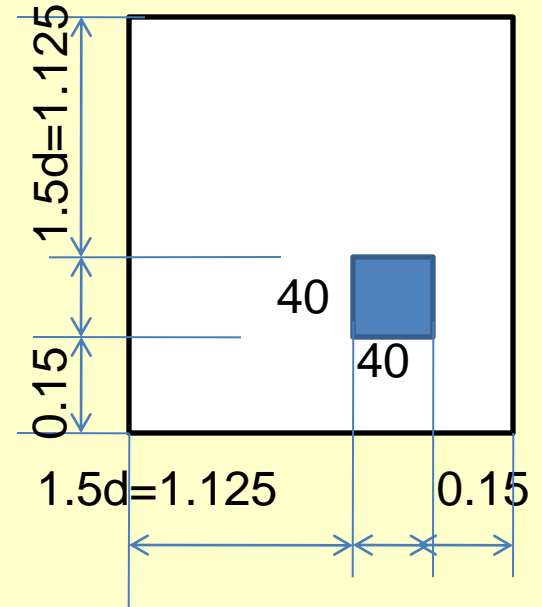
- Net shear force developed
- $V_d = 1320 - 64.45 * (1.675 * 2.65) = 1033.92 \text{ kN}$
- Punching shear resistance

$$V_{up} = 0.25f_{ctd} k_1 k_2 u d \quad (\text{MN})$$

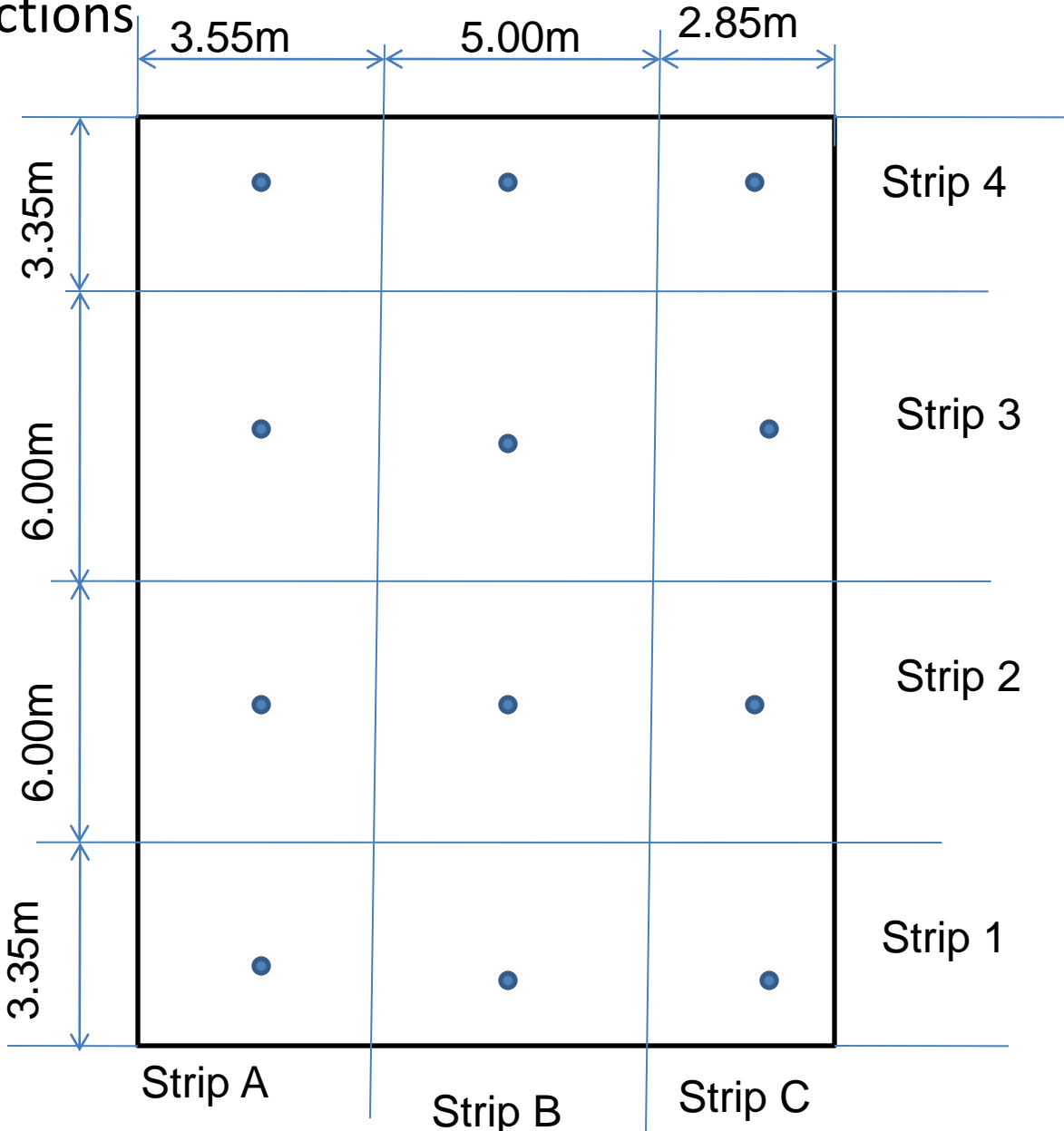
- $V_{up} = 0.25 * 1000 * 1.085 * 1.00 * 6.00 * 0.75$
 $= 1220.63 \text{ kN} > V_d \dots \text{OK!}$



- Check punching shear under 600kN
- $P_r = (1.125+0.15+0.4) + (1.125+0.15+0.4)$
 $= 3.35\text{m}$
- Net shear force developed
- $V_d = 600 - 64.45 * (1.675 * 1.675) = 419.18\text{kN}$
- Punching shear resistance
 $V_{up} = 0.25 f_{ctd} k_1 k_2 u d \quad (\text{MN})$
- $V_{up} = 0.25 * 1000 * 1.085 * 1.00 * 3.35 * 0.75$
 $= 681.52\text{kN} > V_d \dots \text{OK!}$

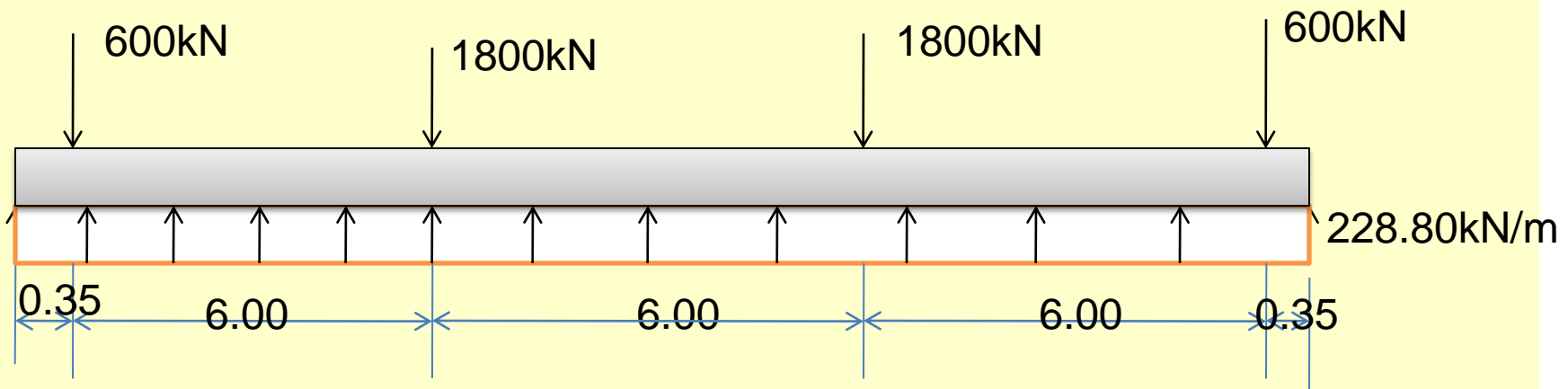


- **Soil reaction analysis:-** Divide the slab mat into strips in x and y directions



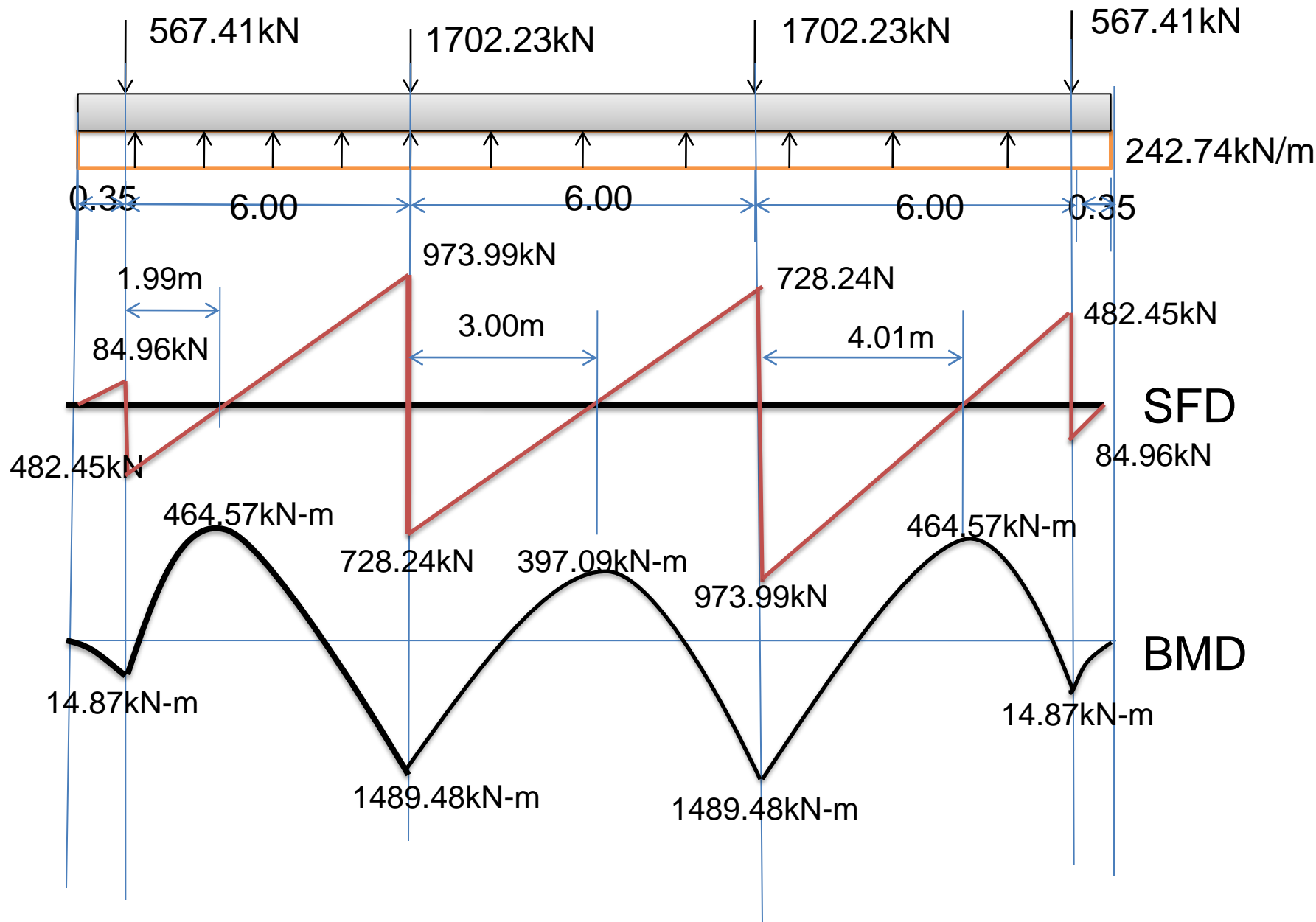
- Strip A, $(64.45) * 3.55 = 228.80\text{kN/m}$
- Strip B, $(64.45) * 5.00 = 322.25\text{kN/m}$
- Strip C, $(64.45) * 2.85 = 183.68\text{kN/m}$
- Strip 1 & Strip 4, $(64.45) * 3.35 = 215.91\text{kN/m}$
- Strip 2 & Strip 3 $(64.45) * 6.00 = 386.70\text{kN/m}$

- Shear force and Bending moment diagrams for each strip
- **Strip A**

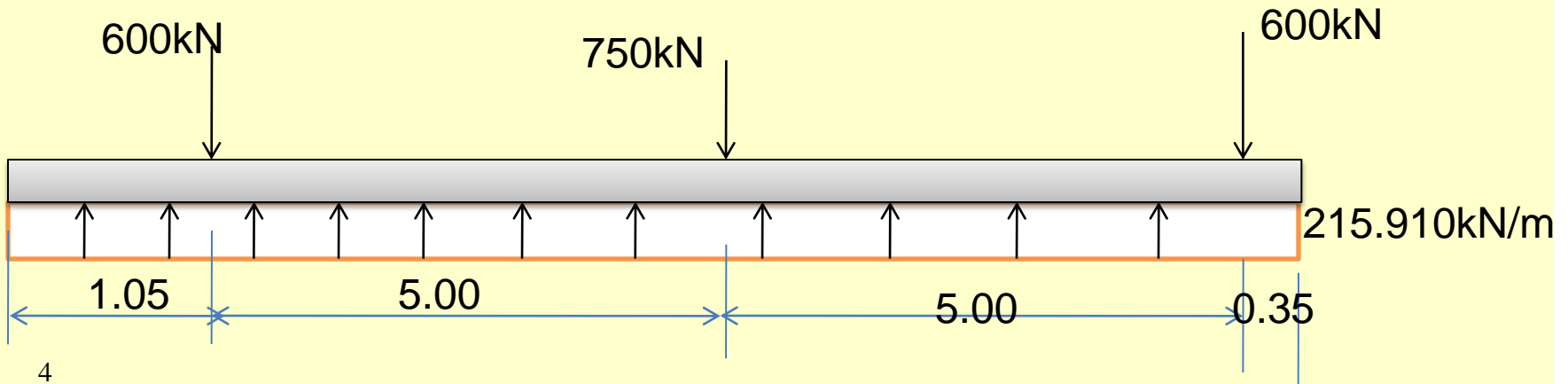


$$\sum_{i=1}^4 P_i = 600 + 1800 + 1800 + 600 = 4800 \text{ kN}$$

- $\Sigma R = 228.80 * 18.70 = 4278.56 \text{ kN}$
- $\Sigma V = \Sigma P - \Sigma R = 4800 - 4278.56 = 521.44 \neq 0$
- Hence take average of ΣP and ΣR
- I.e., $(4800 + 4278.56) / 2 = 4539.28 \text{ kN}$
- $\sigma_{\text{avg}} = (4539.28) / 18.70 = 242.74 \text{ kN/m}$
- $P_{1\text{avg}} = P_{4\text{avg}} = (4539.28 / 4800) * 600 = 567.41 \text{ kN}$
- $P_{2\text{avg}} = P_{3\text{avg}} = (4539.28 / 4800) * 1800 = 1702.23 \text{ kN}$



- Strip 1 & Strip 4, $(64.45) * 3.35 = 215.91 \text{ kN/m}$



$$\sum_{i=1}^4 P_i = 600 + 750 + 600 = 1950 \text{ kN}$$

- $\Sigma R = 215.91 * 11.40 = 2461.37 \text{ kN}$
- $\Sigma V = \Sigma P - \Sigma R = 1950 - 2461.37 = -511.37 \neq 0$
- Hence take average of ΣP and ΣR
- i.e., $(1950 + 2461.37) / 2 = 2205.69 \text{ kN}$
- $\sigma_{\text{avg}} = (2205.69) / 11.40 = 193.48 \text{ kN/m}$
- $P_{1\text{avg}} = P_{3\text{avg}} = (2205.69 / 1950) * 600 = 678.67 \text{ kN}$
- $P_{2\text{avg}} = (2205.69 / 1950) * 750 = 848.34 \text{ kN}$

