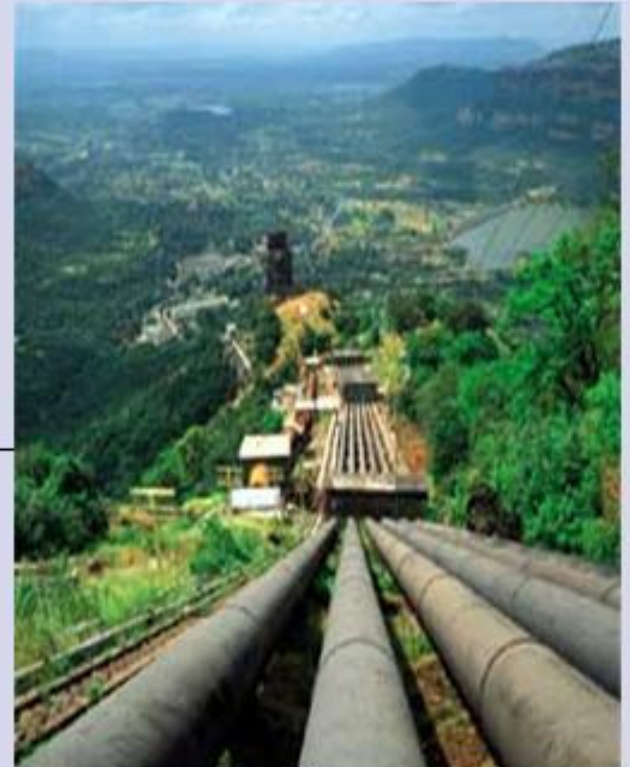


DESIGN OF PENSTOCKS

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Introduction

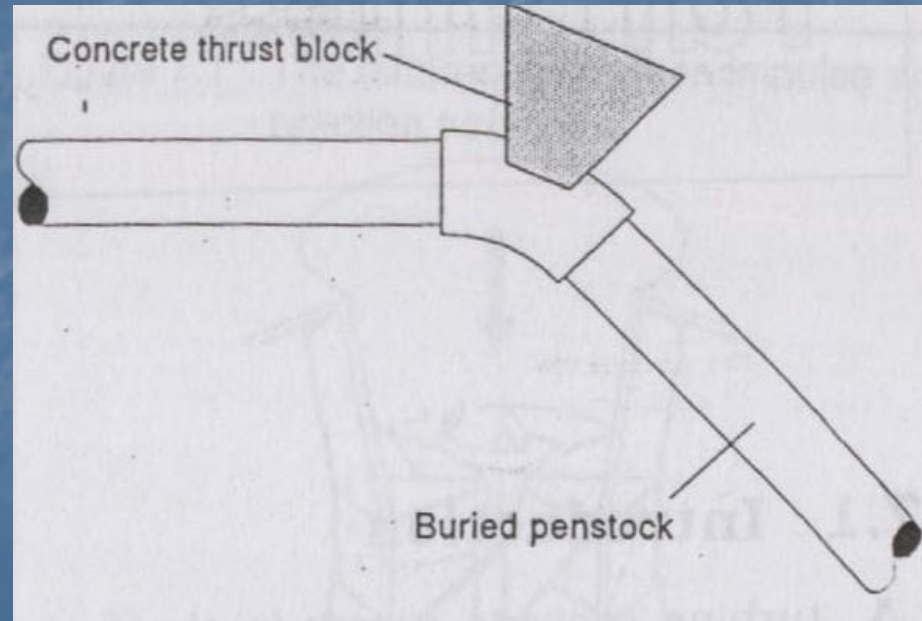
- From the forbay tank down to the turbine water is conveyed through the penstock.

Major components

- Forbay
- Penstock valve
- Vent pipe
- Support pier

Components.....

- Anchors
- Drain valve
- Air bleed value
- Bends
- Thrust block



Major components (joint types)

- flanged

- Socket

- Sleeve type

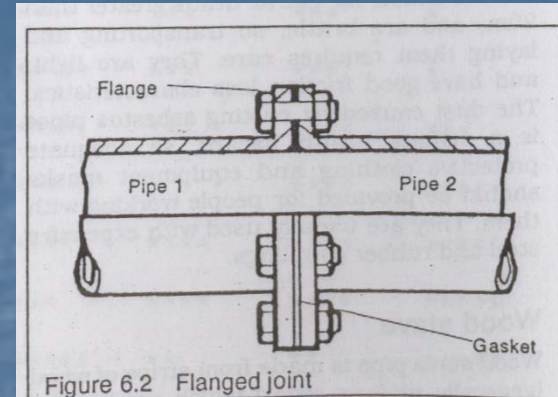


Figure 6.2 Flanged joint

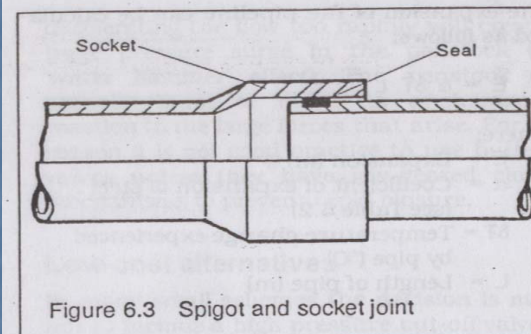


Figure 6.3 Spigot and socket joint

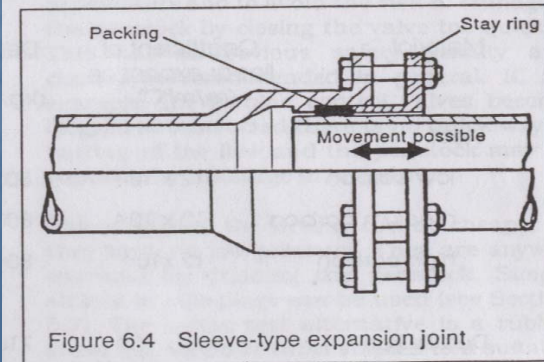
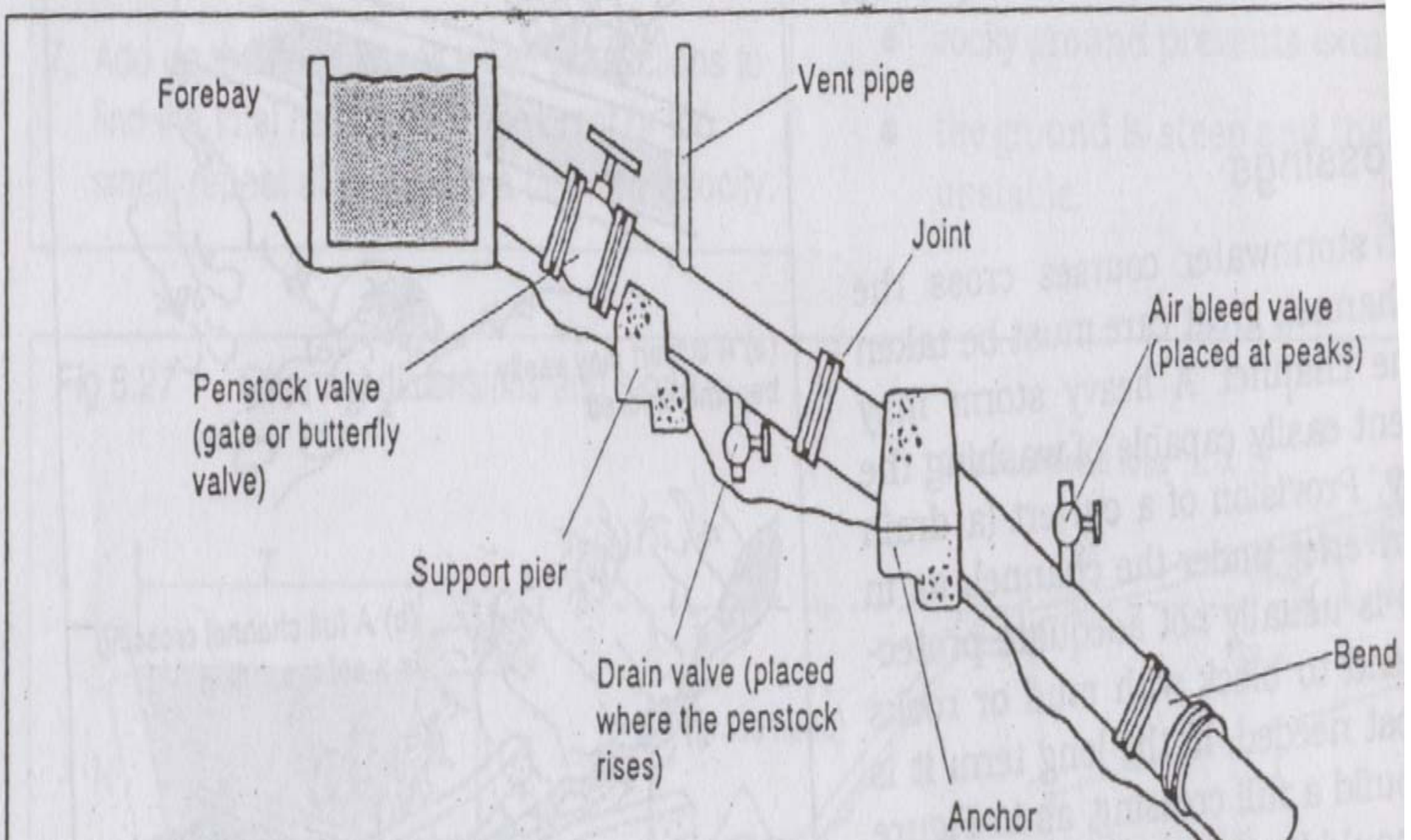


Figure 6.4 Sleeve-type expansion joint

Components of penstock



Material used for construction...

- Mild steel
- uPVC (unplastized polyvinyl chloride)
- HDPE (high density polyethylene)
- Ductile iron
- Prestressed concrete
- GRP (glass reinforced plastic)

Important factors to be considered when selecting material

- **Design Pressure**
- **Surface Roughness**
- **Weight of material**
- **Ease of transportation**
- **Method of jointing**
- **Cost of material etc**

Constraints in deciding diameter

- Price
- Head loss

Compromise: Minimum cost (smallest diameter)

or

Minimum head loss ? (acceptable head loss)

Major contributions to head loss, h_f

* Friction (due to surface roughness)

$$h_f = \frac{1}{2} \cdot V^2 \cdot L \cdot f / g \cdot D \quad \leftarrow$$

Darcy's equation

V – flow velocity

L – penstock length

D – diameter

f -- friction constant

from moody chart

Major contributions to head loss, h_f

- Turbulence (caused by due to bends ,inlet, valves ,reductions etc)

$$h_f = \sum K_i \cdot V_i^2 / 2.g$$

K_i = turbulence loss coefficient

Calculation of head loss & diameter

- **CASE STUDY:-** A steel penstock ,500 m long has a design flow of $0.42 \text{ m}^3/\text{s}$ and a gross head of 220 m. Calculate and diameter and wall thickness. head loss $< 2\%$ of gross head.

- Select diameter as , $D = 300 \text{ mm}$

- Flow velocity $V = \frac{4.Q}{\pi .D^2}$
 $= 5.9 \text{ m/s}$

Renolds no $= V.D \times 10^6$
 $= 1.8 \times 10^6$

- Surface roughness of mild steel is, $f = 0.3$

So , $K/D = 0.3/300 = 1 \times 10^{-3}$

from Moody chart $f = 0.005$, 

From Darcy's eqⁿ ,

$$h_f = \frac{1}{2} \times 5.9^2 \times 500 \times 0.0046 / 9.81 \times 0.25$$
$$= 15.0 \text{ m}$$

in our case gross head = 220 m

$$H_f = (15 / 220) \times 100 = 6.8 \%$$

Calculation of diameter is an iterative process , 

increase D by 10 mm ,

$$\text{now } V = 5.5 \text{ m/s}$$

$$K/D = 0.3/310 = 9.6 \times 10^{-4}$$

$$\text{Re} = V \times D = 5.5 \times .310 = 1.7 \times 10^6$$

corresponding $f = 0.005$

$$h_f = 12.7 \text{ m}$$

$$h_f = 5.77 \%$$

Results of 15 iterations

| iterations | Diameter (mm) | hf / (m) | V /(m/s) | %hf |
|------------|----------------|------------|------------|-------------|
| 1 | 300 | 15 | 5.9 | 6.82 |
| 2 | 310 | 12.7 | 5.5 | 5.77 |
| 3 | 315 | 11.8 | 5.3 | 5.36 |
| 4 | 320 | 10.8 | 5.22 | 4.91 |
| 5 | 325 | 10 | 5 | 4.55 |
| 6 | 330 | 9.3 | 4.9 | 4.23 |
| 7 | 335 | 8.2 | 4.7 | 3.73 |
| 8 | 340 | 7.7 | 4.6 | 3.50 |
| 9 | 350 | 6.6 | 4.3 | 3.00 |
| 10 | 355 | 6.2 | 4.2 | 2.82 |
| 11 | 360 | 5.7 | 4.1 | 2.59 |
| 12 | 365 | 5.4 | 4 | 2.45 |
| 13 | 370 | 5 | 3.9 | 2.27 |
| 14 | 375 | 4.7 | 3.8 | 2.14 |
| 15 | 380 | 4.3 | 3.7 | 1.95 |

Calculation of wall thickness

- Wall should be thick enough to withstand the maximum water pressure
- **Maximum pressure = static + surge**
- Surge pressure :- worst possible case
(instantaneous closure of valve)

Surge pressure , h_{surge}

- $h_{\text{surge}} = C \cdot V / g$

- V – flow velocity
- C – velocity of pressure wave

- $C = 1 / [\rho (1/k + D/E.t)]^{1/2}$

- D – diameter
- t – Wall thickness
- E - Young's modulus of elasticity
- K – Bulk modulus of water
- ρ – density of water

- **Thickness ,**

$$t_{\min} = \rho \cdot g \cdot h_{\max} \cdot D / (2 \cdot \sigma_T / S)$$





- σ_T – ultimate tensile strength
- S - safety factor typically 3

Procedure: this is an iterative process

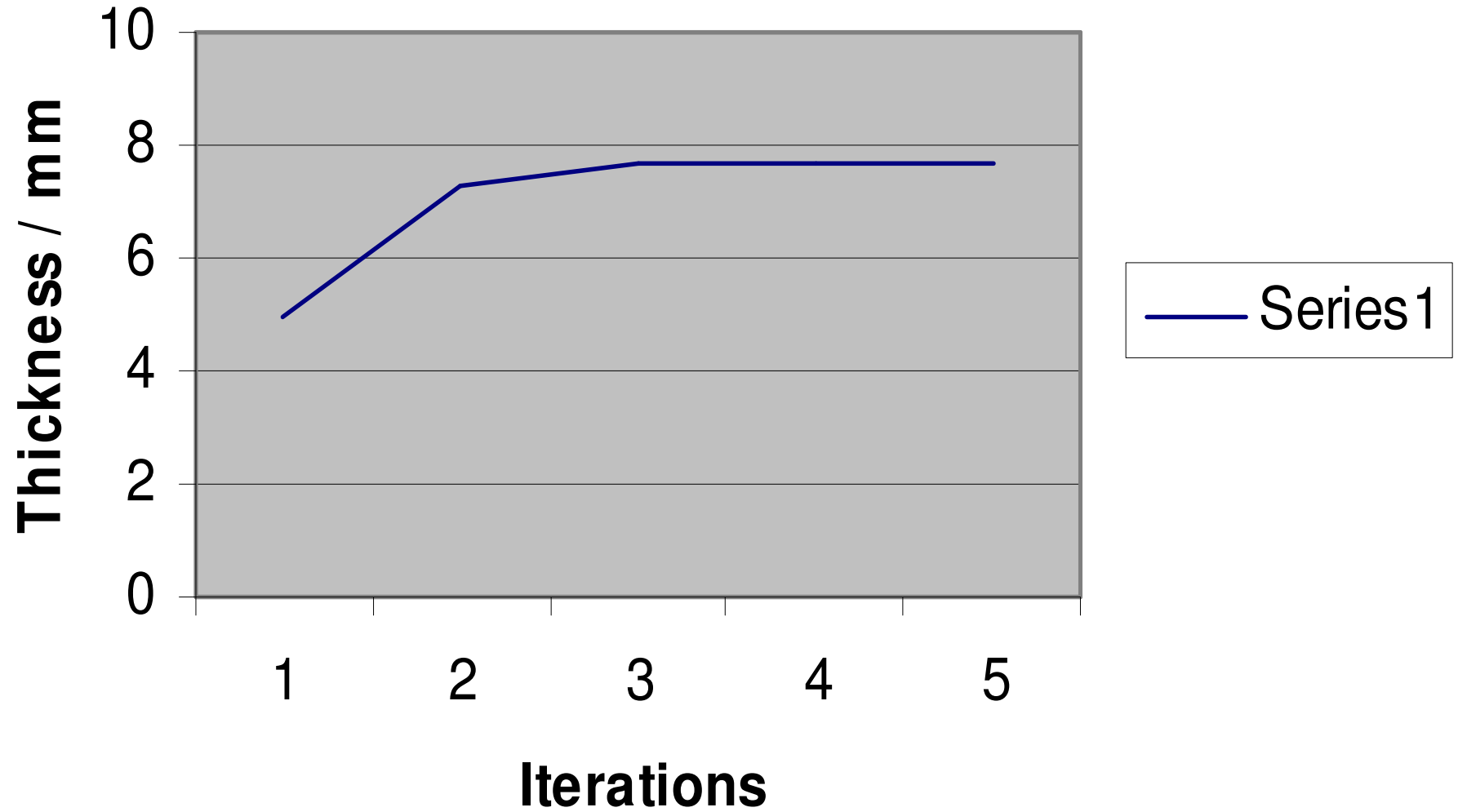
- 1 Estimate t
- 2 Calculate C, h_{\max}, t_{\min}
- 3 Compare t with t_{\min}
- 4 If $t < t_{\min}$ increase t
- 5 if $t > t_{\min}$ reduce t close to t_{\min}
- 6 Repeat 2 and 3

Calculation of penstock wall Thickness

Let us select t as 5 mm , $D = 380$ mm

- Iteration 1 
- Iteration 2 
- Iteration 3 
- Iteration 4 

Penstock Wall thickness



References :

- Micro hydro power –Adam Harvey
 ,Andrew Brown , Rod Edward , VAris
 Bokalders

Thank You !

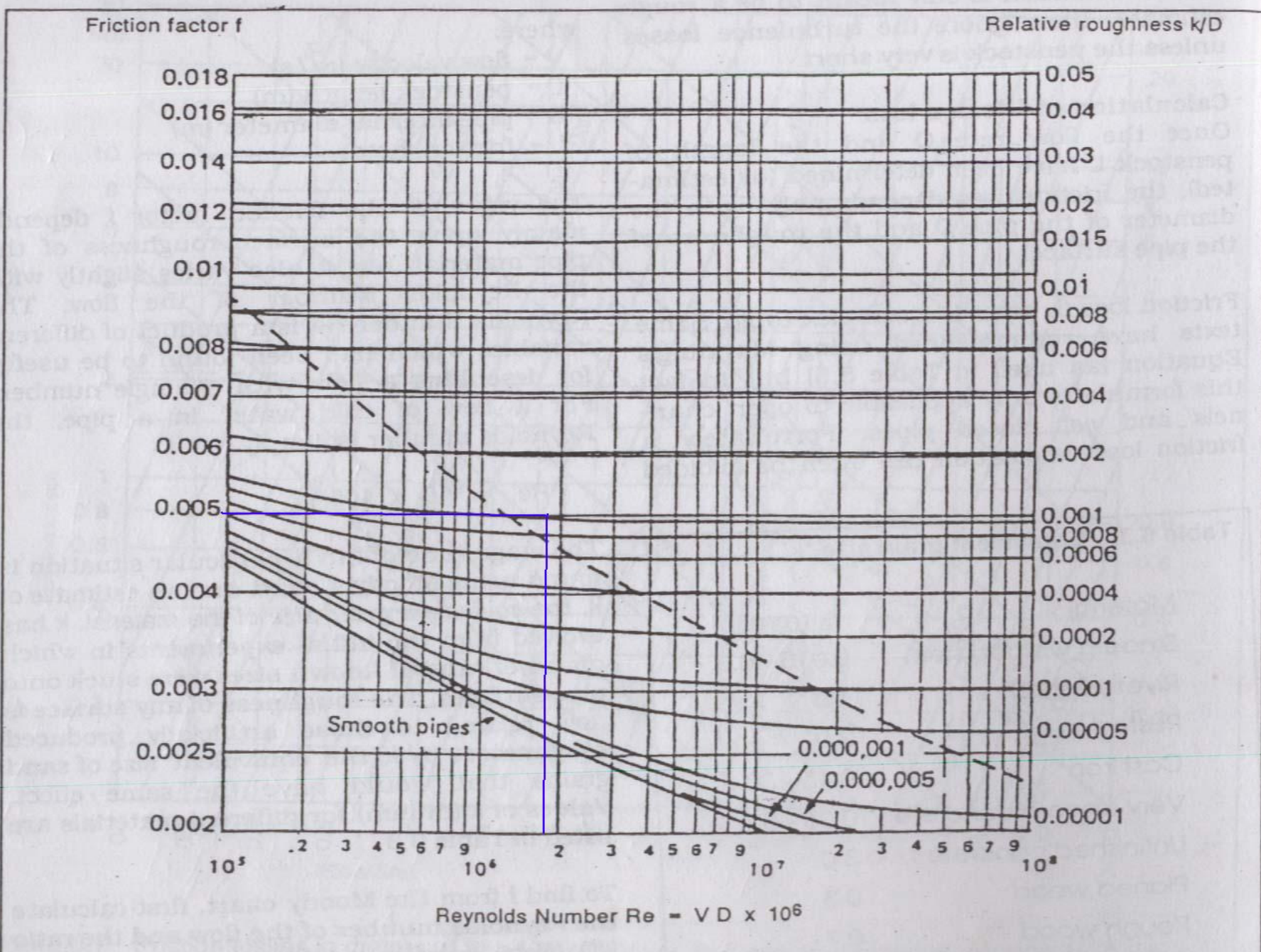
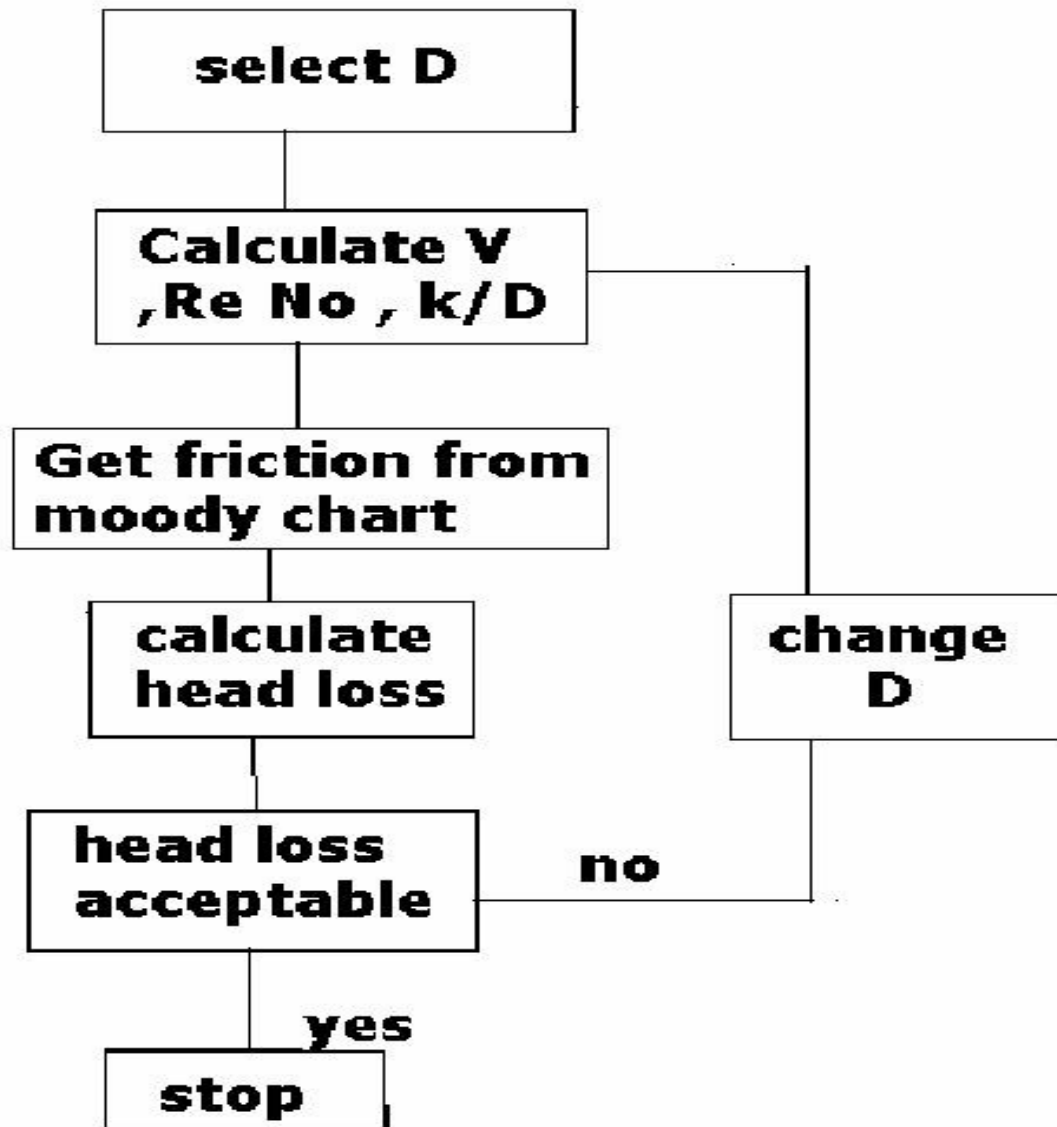


Figure 6.8 Moody's chart for finding the friction factor f of pipes



Results of iterations



1

| | | | |
|-----------------------|-----|---------|-----|
| Wall Thickness | t = | 5.00 | mm |
| Diameter | D = | 380 | mm |
| Velocity | V = | 3.70 | m/s |
| Surge wave velocity | C = | 1088.93 | m/s |
| h surge | = | 410.71 | m |
| P max =hstatic+hserge | | 626.41 | m |
| t min | | 7.30 | mm |



2

| | | | |
|-----------------------|-----|---------|-----|
| Wall Thickness | t = | 7.30 | mm |
| Diameter | D = | 380 | mm |
| Velocity | V = | 3.70 | m/s |
| Surge wave velocity | C = | 1172.29 | m/s |
| h surge | = | 442.15 | m |
| P max =hstatic+hserge | | 657.85 | m |
| t min | | 7.66 | mm |



3

| | | | |
|-----------------------|-----|---------|-----|
| Wall Thickness | t = | 7.66 | mm |
| Diameter | D = | 380 | mm |
| Velocity | V = | 3.70 | m/s |
| Surge wave velocity | C = | 1181.93 | m/s |
| h surge | = | 445.78 | m |
| P max =hstatic+hserge | | 661.48 | m |
| t min | | 7.71 | mm |



4

| | | | |
|-----------------------|-----|---------|-----|
| Wall Thickness | t = | 7.71 | mm |
| Diameter | D = | 380 | mm |
| Velocity | V = | 3.70 | m/s |
| Surge wave velocity | C = | 1183.21 | m/s |
| h surge | = | 446.27 | m |
| P max =hstatic+hserge | | 661.97 | m |
| t min | | 7.71 | mm |