

Development of a Mud-Pulse High-Temperature Measurement-While-Drilling (MWD) System

Final Report

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Executive Summary

The overall program objective is to develop a mud-pulse measurement-while-drilling (MWD) tool for oil and gas drilling operations that can be used where downhole temperatures are as high as 195°C (383°F). The work was planned to be completed in two phases: Phase I and an optional Phase II.

The objectives of Phase I were first to identify critical components of existing MWD systems that can or cannot operate at 195°C. For components not able to meet the higher standard, one of several strategies was pursued: 1) locate high-temperature replacement components, 2) develop new designs that eliminate the unavailable components, or 3) use cooling to keep components at acceptable operating temperatures (under 195°C). New designs and components were then tested under high temperatures in the laboratory. The final goal of Phase I was to assemble two high-temperature MWD prototype tools and test each in at least one low-temperature well to verify total system performance.

Phase II was also envisioned as part of this development. Its objective would be to test the two new high-temperature MWD prototype tools in wells being drilled in the United States where the bottom-hole temperatures were 195°C (or the highest temperatures attainable).

The high-temperature MWD tool (**Figure i**) is designed to send directional and formation data to the surface via mud pulses, to aid in the drilling of guided wellbores. The modules that comprise the tool are housed in sealed barrels that protect the electronics from exposure to down-hole fluids and pressures. These pressure barrels are hung inside a non-magnetic collar located above the drilling assembly.

A number of significant accomplishments were achieved during the course of the Phase I project, including:

- Tested two MWD strings for function in an oven at 195°C
- Conducted field test of prototype 195°C MWD tool (at well temperatures up to 140-180°C)

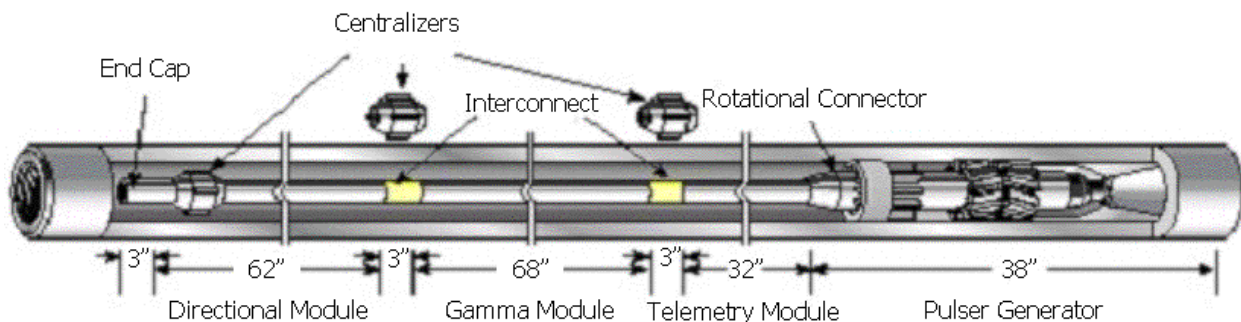


Figure i. High-Temperature MWD Tool

- Tested ELCON hybrid chip with processor, clock, and memory in a custom package for 700 hours at 200°C
- Contracted with APS Technology to conduct study of thermoelectric cooling of downhole electronics
- Conducted successful Peltier cooling test with APS Technology
- Tested and improved the electronics of Sperry Sun's Geiger Muller-based gamma detector for operation at 195°C
- Developed two high-temperature magnetometers (one in-house, one with Tensor)
- Encouraged outside source to develop lithium/magnesium high-temperature batteries (operating temperature of 125 to 215°C)

One of this project's greatest achievements was improvement in Sperry Sun's current tool with changes made as a direct result of work performed under this project. These improvements have resulted in longer life and a more robust MWD tool at the previous temperature rating of 175°C, as well as at higher temperatures.

A field test of two prototype 195°C MWD tools was conducted in Lavaca County, Texas. The purpose of this operation was to provide directional services on a sidetrack of a straight hole. The sidetrack was to intersect the formation up-dip above the water/gas interface. In addition, the gamma tool provided formation data including seam tops and thickness. Results from these field tests indicate progress in the development of a 195°C tool. Although the pulsers failed downhole in both tools, failure of the pulsers was determined to be from mechanical rather than electrical causes.

Analysis of the economics of the 195°C tool highlights the greatest obstacle to future commercialization. Costs to screen individual components, then subassemblies, and finally completed tools for high-temperature operations are very high. Tests to date also show a relatively short life for high-temperature tools – on the order of 300 hours. These factors mean that the daily cost of the tool will be higher (3 to 5 times more) than a conventional tool.

Sperry Sun and the MWD industry have benefited from this program in the following areas:

Pulsar Improvements. Several improvements were implemented in “O” ring selection, oil selection, and other areas.

Magnetometer and Calibration Improvements. Work on the magnetometer included upgrades to Sperry Sun magnetometers. This has led to improvements to the design of Sperry Sun's existing magnetometers, which will be beneficial across all directional work.

Software Improvements, Resetting and Power-Up Problems. Software changes that were required in the downhole code and tool programming code provided another opportunity to improve the robustness of the downhole tool string.

Identification of Circuit Design Weaknesses. While screening components for high temperatures, unexpected problems were observed, including voltage reference drift problems and capacitor failures. Voltage reference drift is another candidate for high-temperature semiconductor technology. The capacitor issue identified a failure in the QC process of production.

The project has helped in clearly demonstrating the limitations of the methods Sperry Sun is currently using to produce high-temperature tools. Based on this work, they are considering the available high-temperature technologies and looking at approaches for introducing these technologies over the longer term.

Conclusions and Recommendations

1. Results of this development effort showed that, while it is possible to build a mud-pulse MWD tool that can operate at 195°C, performance of the current tool is probably not sufficient for commercial success.
2. Industry's current R&D goals and perception of future MWD requirements do not focus on operations in hotter and deeper formations.
3. Due to the extensive testing required and the high percentage of failing components, use of a binning qualification process to build high-temperature (195°C) MWD tools is cost-prohibitive.
4. Increasing the operating temperature of current MWD tools to 195°C and above will require development of a new platform for the electronics used in these tools. This new platform will be based on silicon-on-insulator (SOI) components.
5. There are several hindrances to the development of SOI tools for the MWD industry. Most are economic, rather than technological factors.
6. DOE leadership and partnership with industry can play a significant role in encouraging the development of high-temperature MWD tools to prepare for the future.
7. A critical leadership role for the DOE is to convince the industry that future gas reserves will be produced from high-temperature reservoirs.

Development of a Mud-Pulse High-Temperature Measurement-While-Drilling (MWD) System

Project Objectives

The overall objective of this program is to develop a mud-pulse measurement-while-drilling (MWD) tool for oil and gas drilling operations that can be used where downhole temperatures are as high as 195°C (383°F). The tool is to include a high-temperature (195°C) gamma-ray detector to serve as the formation identification component of the MWD system. Other components in the assembly include triaxial accelerometer and magnetometer suites to provide directional data.

The work was planned to be completed in two phases: Phase I and an optional Phase II. The objectives of Phase I were to:

- Identify critical components of existing MWD systems that can or cannot operate at 195°C
- For those components that cannot meet the new 195°C limit, employ one of the following strategies to achieve required performance: 1) locate high-temperature replacement components, 2) develop new designs that eliminate the unavailable components, or 3) use cooling to keep components at acceptable operating temperatures (under 195°C)
- Test new designs and components under high temperatures in the laboratory
- Assemble two high-temperature MWD prototype tools and test each in at least one low-temperature well to verify total system performance

Phase II was also envisioned as part of this development. Its objective would be to test the two new high-temperature MWD prototype tools in wells being drilled in the United States where the bottom-hole temperatures were 195°C (or the highest temperature attainable in current U.S. deep drilling operations, although at least 185°C). Up to five directional/horizontal wells were planned to be used for the field tests to establish system reliability and the tool's mean-time-between-failure (MTBF) performance.

Project Background

This project was co-proposed by Maurer Technology Inc. (MTI) and Halliburton Energy Services (HES) through its Halliburton Drilling Systems Division. During the course of the project, HES and Dresser Industries merged. The Federal Trade Commission, in their approval of the merger, required Halliburton Drilling Systems to be spun off as a separate company. This new company, called Pathfinder, continued with

the improvement of HES's MWD tools, but had limited funding and could not meet the program's cost-sharing requirements. Halliburton's MWD and LWD services would now be handled by Sperry Sun, a former Dresser Industries company. This significantly impacted the project. Under the original proposal, HES's HDS-1 MWD tool was to be upgraded for operation in temperatures up to 195°C. HES had significant corporate motivation to achieve this objective since their standard tool could only be operated up to 150°C and was below the latest industry standards in reliability. The engineering approach to increase temperature limits was to first test the existing tool using highly-accelerated life testing (HALT) equipment to identify components that would function at higher temperatures and components that would fail at higher temperatures. Once components that fail were identified, improved replacement components were to be located and tested. If these could not be found, new designs were to be developed to replace the missing components. This MWD system development process was well under way when Halliburton and Dresser Industries merged.

The first effect of the merger was a complete work stoppage on the project. Halliburton-Sperry Sun now owned the Solar 175 tool previously developed by Sperry Sun. This tool's upper operating temperature is 175°C. The new company thus had different incentives with respect to continuing the project. It took one year to resolve how the contractual obligations were to be met. In the end, Halliburton-Sperry Sun decided to continue with the project, but would upgrade the existing Solar 175 tool for operations to 195°C.

The new engineering approach was a continuation of Sperry Sun's current "binning" process. In this method, tool components are tested at the desired working conditions. Component lots found to perform satisfactorily are set aside ("binned"). Lots not meeting required performance levels are returned to the manufacturer or discarded. After binning, assemblies and sub-assemblies of components are then tested. This process is very costly, since many components and sub-assemblies must be tested to find enough components that meet acceptable standards. Assembly testing also includes determining failure modes by post-mortem examinations. In cases where component binning or change-out would not achieve required performance, the board design was modified. However, this was considered a last resort, and only minor changes were to be acceptable. The objective was to produce an upgraded Solar 175 tool, not a new 195°C tool.

The effort was also impacted by a complete change in Halliburton personnel assigned to the project. As would be expected, it took time before the new team came "up to speed" on the goals and objectives of the project, and progress could resume. This was further complicated as changeovers in tools and procedures were enacted under the merged companies. In addition, since the Sperry Sun tool was already rated to 175°C (best in the industry at that time) compared to 150°C for HES's HDS-1 tool, the high-temperature MWD market was considered after the merger as a niche market rather than as an opportunity to become the industry leader in high-temperature MWD. These factors led to minimal resources being allocated to the project and slowed its progress. Fortunately, interest in the effort was soon heightened after an important

customer independently approached Sperry Sun and requested MWD tools with higher temperature capabilities.

The merger resulted in some of the work accomplished previously during the project by HES later becoming superfluous to the Halliburton-Sperry Sun effort. That work is still reported here since it was good science and the knowledge gained could help in development with the Solar 195 tool. Other planned activities no longer needed to be pursued since a solution already existed in the merged companies. An example of this was the development of a high-temperature gamma detector based on Geiger Muller tubes. Sperry Sun already had this type of detector available, so that effort was stopped after the merger.

At the end of the effort, Sperry Sun constructed two prototype MWD tools that were successfully tested in the laboratory at 195°C and then field tested in Phase I. Results of these field tests are described in this report.

System Description

The high-temperature measurement-while-drilling (MWD) tool (**Figure 1**) is designed to send directional and formation data to the surface via mud pulses, to aid in the drilling of guided wellbores. The modules that comprise the tool are housed in sealed barrels that protect the electronics from exposure to down-hole fluids and pressures. These pressure barrels are hung inside a non-magnetic collar located above the drilling assembly. Descriptions of the modules and their functions are presented below.

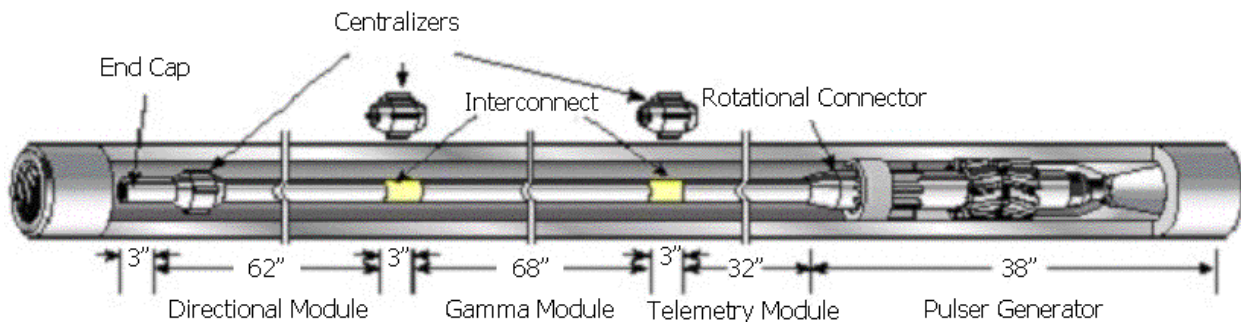


Figure 1. High-Temperature MWD Tool

Telemetry Module (TM). The telemetry module controls the entire tool. It communicates with other modules over the communications line. Data are gathered from the gamma module and directional module, formatted for transmission, and stored in random access memory (RAM) on the TM board. These data can be downloaded at the surface even if they are not relayed via the pulser. The TM also conditions the electric power from the pulser/generator for use by the other modules. The TM uses 512 kB of static RAM divided into 8 kB blocks for continuous memory storage.

Gamma Module (GM). The gamma module measures naturally occurring gamma radiation from formations encountered. It incorporates Geiger Muller tubes because they are rugged and able to survive high temperatures. Conventional gamma sensors based on scintillation technology cannot be used in high-temperature environments because detector performance degrades rapidly at elevated temperatures. Three stacked banks of four Geiger Mueller tubes each make up the sensor section of the GM. None of these tubes are redundant, but are what is required to achieve a statistically accurate count. The Geiger Muller tubes contain a gas that becomes ionized when gamma energy passes through it. This allows high voltage to pass between an anode and cathode, which is recorded as a single pulse. The pulses from all the tubes are added to provide the gamma count. The gamma count is used to determine formation type and transition depths between formations. In horizontal drilling, gamma data are used to steer the drilling assembly within the producing formation.

Pulser/Generator. The pulser module has two functions: to generate electrical power and to restrict the mud flow to create a pressure pulse that can be detected at the surface. It is always connected to the TM and is unique among the modules in this aspect. The pulser contains turbine blades that are driven by the flowing mud to turn a generator and a small hydraulic pump. Power from the generator is sent to the TM for conditioning prior to being sent to the remainder of the tool. The hydraulic pump is used to operate a poppet valve that blocks the flow of mud in the drill string, thereby creating a pressure pulse. The TM controls the pulser operations and encodes data into the pulses that are received and decoded at the surface using a pressure transducer and computer. The pulser is typically found at the top of the MWD stack.

Battery Module (BM). The battery module provides power to the tool when there is no flow of drilling fluid to operate the generator. The MWD tool can operate without a BM, but then could not store data when the rig pumps were off. The BM allows operation during these periods. High-temperature lithium batteries are used in the BM. Halliburton worked with Battery Engineering to develop higher temperature batteries for this project.

Directional Module (DM). The directional module uses magnetometers and accelerometers to measure the compass direction of the bottom-hole assembly and the angle of the hole. These data along with depth are then used to calculate the trajectory of the well. The DM is usually placed near the bottom of the MWD stack so that it will be as close as possible to the drill bit.

Accomplishments

A number of accomplishments were achieved during the course of the project. These are listed below. (More detail is provided in other sections of this report.)

- Tested two MWD strings for function in an oven at 195° C
- Conducted field test of prototype 195° C MWD tool (at well temperatures from 140 to 180° C)
- Tested ELCON hybrid chip with processor, clock, and memory in a custom package for 700 hours at 200° C (see **Figure 3**)
- Contracted with APS Technology to conduct study of thermoelectric cooling of downhole electronics
- Conducted Peltier cooling test with APS Technology
- Tested and improved the electronics of Sperry Sun's Geiger Muller-based gamma detector for operation at 195° C
- Developed two high-temperature magnetometers (one in-house, one with Tensor)
- Encouraged outside source to develop lithium/magnesium high-temperature batteries (operating temperature of 125 to 215° C)

One of this project's greatest achievements was improvement in Sperry Sun's current tool with changes made as a direct result of work performed under this project. Table 1 lists many of the modifications. These have resulted in improved life and a more robust MWD tool at the previous temperature rating of 175° C, as well as at higher temperatures.

Table 1. Solar 175 System Upgrades to Increase Operating Temperature to 195° C

- I. Directional Module (DM)*
 - Increased the life of the DC-DC converter and reduced the amount of 5-volt drift via modifications to the DM power board.
 - Special software was used to create the thermal models at 195° C.
 - Developed magnetometer that operated at 200° C at Cheltenham Engineering Center.

- Worked with Honeywell to develop and test magnetometer package for operation up to 200°C.
- Worked with JAE to provide accelerometer package for operation up to 200°C.
- Changed the download of HC811 code. The appropriate code is stored in all 4 banks of the external EEPROM. This corrects reset problems at temperatures above 175°C.
- Added a brown-out monitor to the power board to insure that HC811 is reset properly.
- Upgraded the CMOS analog switch on the power board.

II. Processor Board

- No hardware was changed in the processor board to reach the 195°C temperatures.
- Changed software to add additional time delay during initialization to allow processor to recover from a Power On Reset when operating above 190°C.
- The only circuit that does not operate reliably at temperatures above 180°C is the Real Time Clock.

III. Power Board

- To solve problems with voltage drift of the precision 5volt reference with time and temperature, it was necessary to decrease the amount of output current the device must source. This increased the life of the reference to approximately 150 hours at 200°C. A reference manufactured by a different vendor was located, that required minor modification to work in Sperry Sun circuit. Five-volt reference used in the power supply circuits prevents drift with temperature and time. Tested three different parts; the ceramic part did not fail after approximately 500 hours at 200°C. Built two 195°C telemetry modules and gamma modules using the new reference chip.
- Increased main power input electrolytic capacitor life to 300 hours at 195°C by lowering the generator supply from 24 volts to 22 volts.

IV. Gamma Module (GM)

- Screened timer chip to operate at higher temperatures. During tests on the first GM's built, we discovered that the high-voltage supply would shut down at temperatures above 183°C. A timer chip used in the high-voltage supply circuit was found to be the cause. We screened different date

codes on these devices to find those that would work above the required 195°C. Also tested two other timers from different vendors that will also work in this circuit. Qualification of these new devices is still in process. The GM's built for this project used the screened timers.

- The 5-volt reference chip was changed to the new type.

V. Battery Module

- Changed 5-volt reference chip to a Maxim brand.
- Changed 5-volt supply from just a reference chip to a reference chip with a buffer and current pump system.
- Change of voltage measurements for Battery and Sub-bus by the PIC A/D. Changed divider networks from high impedance to less than 10 k-Ohms.
- Changed instantaneous current measurement impedance to PIC A/D by decreasing from 50 k-Ohms to 10 k-Ohms.
- Added 10 k-Ohm input impedance lines to PIC on the pulse accumulation measurement. This improves long-term average current draw measurement reliability in the PIC.

VI. Pulser

There were three areas (wear, oil compensation, and sealing) where improvements were made to the pulser for high temperatures.

A. Wear

- Conical rams redesigned with increased contact area for reduced wear
- Conical rams retained with anti-rotation spider to eliminate coil spring wear
- Angle plate bearing races changed to high-grade M50 bearing steel
- Angle plate bearing elements changed to Silicon Nitride balls and precision machined cage
- Tapered roller bearing mounting changed to minimize mechanical shock related spalling
- Oil changed to Mobil SHC 1025 to eliminate viscosity breakdown
- 25-micron filter and auger to circulate oil and trap particles

- Metal screen (70 micron) oil filter with conical rams

B. Oil Compensation

- Piston pressure compensation system replaced boot-style design
- Kemlon caps to reduce oil volume
- Pump outer case

C. Sealing

- Changed to 90-durometer O-rings
- Tee-seals on the bulkhead
- HPHT feed-through connectors for the bulkhead

Project Tasks and Work Completed

Following are listed the Phase I tasks with a discussion of the work conducted under each task. Work on many tasks was accomplished both before and after the Halliburton/Sperry Sun merger. To clarify this distinction, work performed before the merger is referred to as “Halliburton” and work after the merger as “Sperry Sun.”

Task 1. High-Temperature Characterization of HDS-1 MWD/Gamma Tool

Both Halliburton and Sperry Sun used HALT (highly-accelerated life testing) to characterize the HDS-1 and Solar 175 tools. **Figure 2** shows the HALT equipment used by Sperry Sun. HALT allows accelerated life testing of components by subjecting them to vibration and temperature fluctuations. HALT equipment allows desired cycles and rates to be programmed for each test. The product is monitored during the test for function. When components fail, they can be replaced and testing continued, if desired. Good correlation between HALT and field life has been observed.

Halliburton and Sperry Sun were both able to identify components or circuit designs that failed as temperatures were increased to 200°C. For circuit design failures, eliminating components or altering the design addressed the shortcomings. Other failures required that new components be substituted for those that could not meet the temperature requirements.



Figure 2. Sperry Sun HALT Equipment

Task 2. Evaluation of High-Temperature Components

Work under this task highlighted a fundamental difference in the approaches of Halliburton and Sperry Sun. Halliburton's goal was to identify, test, and use components that were either designed to operate at higher temperatures or had been specially modified to operate at higher temperatures. Sperry Sun chose to keep the same components (when possible), but identify batches from the manufacturer that functioned at elevated temperatures. One reason for the difference in this philosophy is that Halliburton's then-current tool was initially only rated to 150°C and they realized that their product was falling behind the industry standard as a whole. Sperry Sun's tool currently achieved a rating of 175°C and was a leader in the industry for temperature capabilities. Sperry Sun believed that they had already identified components with superior temperature performance and that the project's goal to increase temperature capability to 195°C could be accomplished by locating exceptional batches of components that could survive even higher temperatures.



Figure 3. ELCON Hybrid Processor Chip for Test

Halliburton was successful in finding several components that demonstrated improved high-temperature performance. Many of the components were radiation hardened. A major concern at the onset of the project was the performance of the microprocessor and memory chips.

Halliburton located a hybrid chip manufactured by ELCON Technology of Phoenix, Arizona, that was successfully tested at 200°C for over 700 hours. The test was halted at the time of the merger, and was never completed or repeated. Since the chip did not meet Sperry Sun's configuration, it was not considered in their development. **Figure 3** shows the hybrid chip on a test board. It has been isolated so that only the chip will be placed in the test oven and not the circuit used to operate the chip.

Task 2a. Design of Active Cooling System

At part of the contract, Halliburton undertook and paid for the work under this subtask, which involved analytical and experimental work on an active cooling system. Halliburton contracted this work to APS Technology of Cromwell, Connecticut. They developed an analytical model to simulate cooling of an MWD system and a dummy board, using resistance heating to simulate electrical components. **Figure 4** shows

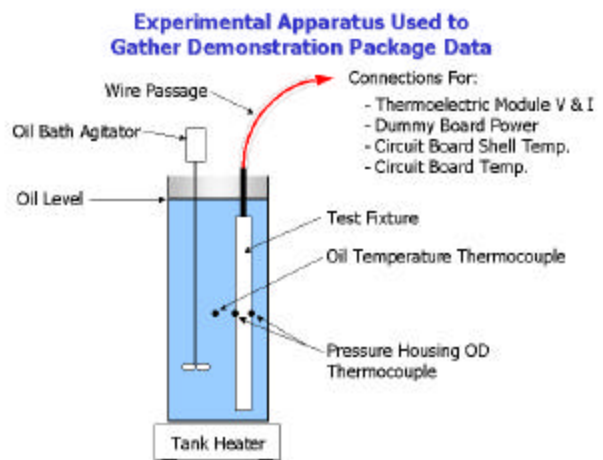


Figure 4. TEC Test Setup

the test set-up employed by APS; **Figure 5** summarizes temperatures during the test.

Thermoelectric coolers (TEC) were used to remove heat from within a pressure barrel containing the dummy MWD board. Temperature and power data were recorded as the assembly was operated in an oil bath. The oil bath represented fluids in a hot well just as the dummy board represented the heat generated by MWD components. The data show that TECs can reduce the temperature inside the pressure barrel and on the circuit boards to acceptable levels. Table 2 summarizes the test data. The temperature of the oil bath was manually controlled and held at 200°C while temperatures were measured at two locations on the housing 180° apart at the inside surface of the pressure housing at the TEC and on the dummy board. Power to the TEC was monitored, as was power to the dummy board. The

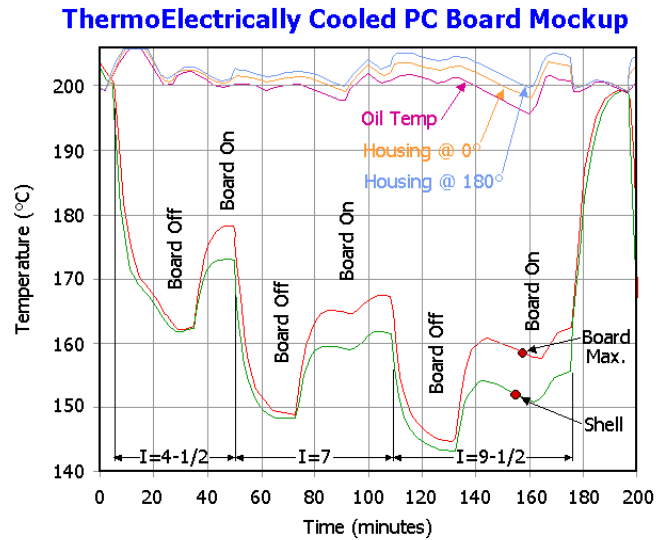


Figure 5. Thermoelectric Cooling Tests

heat that leaks into the pressure barrel is estimated from the analytical model, and the efficiency of the thermoelectric device (ratio of heat pumped to thermoelectric power consumed – COP) calculated. The data show that the thermal model effectively represented the test. Results indicated that the TEC can reduce the board temperature from 40 to 54°C below ambient temperature. Since this is a sufficient reduction to keep the board cool in wells that are 195°C, it was found that a TEC is a possible solution.

Table 2. Thermoelectric Cooling Test Data

Time (min)	Temperatures						Thermoelectric Coolers				Power			COP
	Oil	Housing @TEC	Housing @180°	Shell	Board Max.	Board Avg	ΔT TEC	Amps	Volts	Watts	Board	Leak	Total	
4	202.4	203.1	202.9	162.3	162.5	162.4	40.8	4.5	8.25	37.125	0	21.4	21.4	0.58
48	200.0	201.1	200.6	173.0	178.3	175.7	28.1	4.5	9.52	42.84	15	14.7	29.7	0.69
72	200.5	202.3	201.5	148.3	148.8	148.5	53.9	7	14.26	99.82	0	28.3	28.3	0.28
105	200.5	202.6	201.8	161.9	167.6	164.7	40.7	7	14.06	98.42	15	21.4	36.4	0.37
131	201.3	204.6	203.2	143.2	144.5	143.8	61.4	9.5	18.96	180.12	0	32.2	32.2	0.18
173	200.8	204.9	203.2	155.2	162.0	158.6	49.7	9.5	18.78	178.41	15	26.1	41.1	0.23

The test data also show that a TEC would consume considerable electrical power, thus requiring the use of a turbine generator. Power would then only be available when the pumps were operating, so a Dewar-type pressure housing would be

needed to insulate the MWD electronics and keep them at rated temperatures for acceptable periods of time while the pumps were off. Both the generator and housing increase the cost of this system. In addition, to achieve higher efficiency, the inside of the Dewar would need to be filled with a dielectric fluid. This makes assembly more difficult since the normal potting medium is not a good heat conductor and space would need to be provided for the dielectric when potting the system.

Despite these drawbacks, a cooling system should be considered in the future for high-temperature MWD systems. The market size for these systems will likely remain small and the potential for development of new high-temperature components is not well defined. Both of these factors will dictate whether cooling is a more economical approach.

Task 3. Design of a High-Temperature Gamma-Ray Detector

Many MWD suppliers, including Halliburton, normally use solid-state gamma detectors. Unfortunately, these devices cannot be used at high temperatures because materials used in their construction will break down. The best way to measure gamma radiation at higher temperatures is with Geiger Muller tubes. One advantage to the Halliburton/Sperry Sun merger was that Sperry Sun already had a gamma detector based on Geiger Muller tubes. Halliburton had received designs from two different companies, but neither of these systems was constructed before the merger. CBG group in Austin, Texas, was one of the companies that quoted on the construction of a Geiger Muller-based gamma detector. Halliburton was preparing to release a purchase order at the time of the merger. Instead, Sperry Sun later performed HALT to determine changes needed to upgrade their Geiger Muller unit to 195°C. Testing highlighted problems in the unit's electronics which were modified and repaired successfully.

Task 4. Selection of High-Temperature Components for Use in MWD/Gamma Tool

Both Halliburton and Sperry Sun used HALT to identify components or batches of components that performed adequately at high temperatures. Halliburton sought to develop new components and designs while Sperry Sun identified areas that could not be addressed through the batch process and redesigned the circuits to eliminate these components.

Halliburton had selected many different high-temperature elements before the project was temporarily halted (due to the merger). The processor and memory selected would likely have been the ELCON hybrid chip set. High-temperature passive components such as resistors and capacitors had been purchased. In addition, board, solder, and potting materials for the 195°C tool had all be selected.

Halliburton had made progress on developing high-temperature magnetometers and accelerometers. ATEC agreed to manufacture high-temperature magnetometers at no cost in return for test data from the project. Japan Aviation Electronics in Tokyo completed tests on accelerometers and it appeared that they had solved problems with long-term drift. Halliburton had also located a radiation-hardened hex buffer IC that was test to 250°C (the limit of their oven).

Halliburton ran HALT on the TCM (telemetry communications module), which developed failures at 160 to 165°C due to E-prom read or write errors. This problem had been anticipated and would have been solved by using flash memory in place of the E-prom.

Halliburton, working with Battery Engineering Inc. of Hyde Park, Massachusetts, had developed a lithium-magnesium battery that would operate in the temperature range of 125-214°C. Lithium thionyl chloride batteries are normally used to provide power for MWD tools. Unfortunately, lithium has a melting point of 180°C, and standard lithium batteries are normally limited to operating temperatures of 160°C and below. If magnesium is alloyed with the lithium anode, operating temperature can be increased, although with a reduction in current capacity (Table 3).

Table 3. Temperature Performance of Li-Mg Batteries (DD size)

Anode Type	% Magnesium	Melting Point (°C)	Max Oper Temp (°C)	Current Capacity (A-hr)
Lithium	0	180	160	26
Li-Mg	10	202	180	20
Li-Mg	25	220	200	15

Battery Engineering developed high-temperature batteries based on the lithium/magnesium alloy. A size DD battery with 25% magnesium can be safely used to 200°C (as required for this MWD development). Current capacity, while reduced to 15 A-hr, is sufficient for at least 250 circulating hours downhole. The primary disadvantage of this recipe is that power output below 100°C is poor.

At the time the project was paused due to the merger, discussions were taking place to decide if heaters would be used to maintain the temperature of the lithium/magnesium batteries at minimum operational levels, or if a sacrificial nickel-cadmium battery pack would be used to power the tool at lower temperatures. For the approach incorporating a sacrificial battery, a low-temperature battery pack would shut down and the high-temperature batteries come on-line as the tool's temperature rose above 125°C. The low-temperature batteries would be replaced after each run.

Sperry Sun had difficulty in proving two directional packages (magnetometers and accelerometers) for the test. These were the last individual components proven. One was from Sperry Sun's internal research department in Cheltenham, England and the other from Tensor in Austin, Texas. Work with Tensor began under Halliburton, but no contract was ever placed. Tensor had indicated that they could build the 195°C directional package, but never provided a quote to Halliburton. Only one of three units supplied to Sperry Sun was found to qualify at higher temperatures. This area remains as a key item requiring additional work.

The problem components identified by Halliburton for the directional package (magnetometers and accelerometers) were never tested because they did not fit the

form that Sperry Sun needed. However, the manufacturers felt confident they had succeeded in developing high-temperature components.

Task 5. Design High-Temperature MWD/Gamma Tool

Both Halliburton and Sperry Sun took advantage of the opportunity presented by the project to make changes in the design of their MWD tools. Sperry Sun enhanced many areas of their tool (Table 1 presents a list of major changes that were made and incorporated into their current line of tools). Halliburton was just beginning this task when the merger took place; however, through HALT testing they had identified many changes that would be required to meet the temperature goals.

Task 6. System Fabrication

Halliburton did not have the opportunity to advance as far as system fabrication. Sperry Sun was, in one sense, working on fabrication throughout Tasks 4 and 5 since they used their current system as a base and were only modifying and substituting parts that qualified for higher-temperature service for existing parts. **Figure 6** shows the Sperry Sun tool being loaded into an oven for a high-temperature proof test. **Figure 7** shows the temperature controller during the test. The temperature is 193°C with a set point of 195°C. Both tools were tested and proven in this oven before field testing.



Figure 6. Sperry Sun MWD Tool Being Prepared for Oven Test



Figure 7. Oven Controllers

Task 7. Laboratory Testing

The Sperry Sun tool was under constant laboratory testing during the proofing process. Task 7 was originally conceived for the Halliburton MWD tool since it was basically a new tool (in contrast to Sperry Sun's tool, which had already undergone significant development and testing).

Task 8. Low-Temperature Field Test

A field test was conducted with the two Sperry Sun MWD tools prepared under this project. Originally, this test was to be a shake-out of a new Halliburton tool and therefore was to be conducted at lower temperatures so that problems not related to temperature could be identified. Since the Sperry Sun tool was much closer to a conventional (market-ready) tool, the first test was conducted at elevated temperatures (180°C). While not the tool's limit, this temperature range still represented an ambitious test. (See next section for details on field testing.)

Field Test

A field test of two 195°C MWD tools was conducted in Lavaca County, Texas (**Figure 8**). Sperry Sun's field report is presented in **Appendix A**. The purpose of this operation was to provide directional services on a sidetrack of a straight hole. The sidetrack was to intersect the formation up-dip above the water/gas interface. In addition, the gamma tool provided formation data including seam tops and thickness.

Conventional Solar 175 tools were used in the beginning of the operation. The well temperature at 16,500 ft was 160°C. The prototype 195°C tools were then run instead of the standard Solar 175 tools. The first prototype tool went below the rotary table on August 1, 2001 at 17:30 hours (**Figure 9**). Thirty minutes later, a shallow test was conducted to check for proper operation. At 11:45 hours on August 2, 2001, the tool reached bottom and drilling was begun. (The long trip time is the result of a rig shut-down for BOP repair.) The first recorded temperature was 178°C. The tool stopped pulsing on August 4, 2001 at 23:00 hours, after operating on bottom for 59 hours. Data downloaded at the surface at the end of the test showed that the tool continued to record data until 1:44 hours on August 5, 2001 – an additional 27 hours. The tool was pulled from the well at 2:30 hours on August 6, 2001. Total downhole hours (from the time the tool moves below the rotary table until it is returned to the surface or fails down hole) was 115 hours.



Figure 8. Rig Site



Figure 9. Tool Preparation

The second prototype tool was run into the well at 3:30 hours on August 6, 2001. Gamma logging of a missed interval from the previous run was begun at 18:30 hours the same day. At 22:00 the tool was on bottom drilling. At 5:30 hours on August 7, 2001 the tool stopped pulsing. The highest temperature recorded was 187.2°C. Drilling continued blind and the tool was pulled from the well on August 13, 2001 at 22:00 hours. Total time below the rotary table was 186.5 hours. Total time before data transmission was lost was 26 hours.

Each of the tools was given a post-mortem examination. The first tool was found to have a failed pulser. Drilling fluid had entered the tool past the poppet seals. The poppet bearings also showed unusual wear. Although the barite content of the field mud was high, the amount of wear on the bearing was unexpected. A typical tolerance for this bearing is 0.003 inches. The

bearing in the first tool was found to have a clearance of 0.015 inches. This allowed the poppet to move laterally and damage the seal, ultimately leading to the failure of the pulser. Data from the tool's telemetry module were successfully downloaded after the operation, demonstrating that the electronics had not failed during this run. Battery voltage was very low (which could have been caused by exposure to high temperatures). The special high-temperature batteries do not begin functioning at full voltage until they reach 125°C.

On the second tool, the pulser was also found to have failed. However, a bearing that had been inadvertently left out during assembly caused the premature failure. It was also found that the back-up battery in the telemetry module had vented, which damaged wiring and electronic components. After the battery was removed, attempts to unload memory were unsuccessful due to damage from the battery fluid. Data from this run were determined to be lost. It was not apparent why the battery had vented. Heat could have been a factor, although these batteries should have been capable of operations up to 214°C.

Results from these field tests indicate some progress in the development of a 195°C tool. Failure of the pulsers appears to have been from mechanical rather than electrical causes. The vented battery may indicate that more work is needed in this area, but only further field tests would conclusively highlight the weakness(es). It was particularly unfortunate that the second tool was improperly assembled. Even with a vented battery, data collected from the run would have helped determine how the electronics were performing under elevated temperatures.

Economic Analysis

Analysis of the economics of the 195°C tool highlights the greatest obstacle to future commercialization. Costs to screen individual components, then subassemblies, and finally completed tools for high-temperature operations are very high. Tests to date also show a relatively short life for high-temperature tools – on the order of 300 hours (as compared to approximately 1000 hours for a commercial MWD tool operating at temperatures up to 150°C). These factors mean that the daily cost of the tool will be much higher than a conventional tool. In addition, high-temperature MWD tools are difficult to prepare. For these development efforts, the engineering department made use of highly trained technicians and engineers to prepare these tools. While the normal production staff is well qualified to manufacture tools for conventional applications, it would be difficult for them to prepare, trouble-shoot, and maintain the 195°C tools on a continuing basis.

Table 4 summarizes costs for the extra labor required to produce 195°C tools. These data are then used to calculate a daily cost for the tool. Daily costs are based on an operating life of 300 hours, which was determined from the laboratory testing of the 195°C tools. Table 4 shows additional screening costs to run HALT on components to find those that will function at 195°C.

Table 4. Screening Costs for Higher Temperature Components

Tool Module	Standard Cost	Additional Screening Cost	Total Cost
Pulser	-	-	-
TM	-	-	-
DM	-	-	-
GM	-	-	-
BM	-	-	-
Expendables (flow gear, interconnects)	-	-	-
TOTAL	\$129,062	\$48,000	\$177,062

Table 5 shows the recovered costs after a field run. This is calculated by subtracting the standard (expected) repair costs from the new equipment cost. The cost of a nonmagnetic drill collar to house the tool is approximately \$30,000.

Table 5. Recovered Costs

Tool Module	Standard Cost	Repair Costs	Total Recovered Costs
Pulser	-	-	\$6,927
TM	-	-	\$1,300
DM	-	-	\$2,426
GM	-	-	\$2,426
BM	-	-	\$2,426
Total	\$119,753	\$104,248	\$15,505

The total cost to operate the tool, excluding manpower, will be the cost of a standard tool plus the cost for additional screening minus the recoverable costs or;

$$\text{Operating Cost} = \$129,062 + \$48,000 - \$15,505 = \mathbf{\$161,557}$$

The operating time of 300 hours is equivalent to 12 days; thus, the day rate will be \$13,463. This cost does not include the cost of capital to build the tools or the cost associated with the loss of technical personnel's time when they are needed to keep these tools operating.

Other costs include depreciation (\$282/day) and crew charges (estimated at \$1000/day). The total estimated daily cost for the new tool is \$14,745/day. This cost compares to \$3,000 to \$4,000/day for a Solar 175. Thus, the cost of the 195°C tool is 3 to 5 times more than a conventional tool. It is unlikely that many operators will be willing to pay this price, making the 195°C tool uneconomical to offer commercially.

These estimates are based on an operating life of 300 hours, high costs of screening parts, and a highly technical labor force needed to maintain the prototype

tools. It is difficult to determine whether operational experience could increase operational life and reduce manufacturing and maintenance costs, and thereby reduce the daily rate. Currently, Sperry Sun does not foresee sufficient market size to justify the expense to estimate these parameters. However, it is clear that new gas discoveries will be from increasingly deeper and hotter wells, and that the DOE should aid in the development of tools for these applications. It is also clear that an important area for additional work is to determine what is possible in reducing the costs and extending the life of the 195°C tools.

Benefits to the MWD Industry

Sperry Sun and the MWD industry have benefited from this program in the following areas:

Pulser Improvements. Several improvements were implemented in “O” ring selection, oil selection, and other areas. Many improvements were made to the positive pulser as a result of the 175°C programs, which had taken place before this contract was started with Sperry Sun. Based on project tests, relatively few components of the system needed to be upgraded.

Magnetometer and Calibration Improvements. Work on the magnetometer included upgrades to Sperry Sun (i.e., Tewkesbury) magnetometers in response to higher temperature requirements. This has led to improvements to the design of Sperry Sun’s existing magnetometers as used in the Tewkesbury tool family, which will be beneficial across all directional work. Further work was done with Tensor (then Honeywell) in Austin to obtain high temperature. This work showed clearly some of the limitations in the screening strategy Sperry Sun was following. Tensor has included a redesign of the magnetometers with some high-temperature electronics. It proved very difficult to get magnetometers built that perform consistently. This work in turn revealed deficiencies in the modeling methods used to correct errors introduced by temperature. Required modifications to address these findings are still ongoing within Sperry Sun. They are re-evaluating calibration methods for all of our directional tools used in the USA and internationally.

Software Improvements, Resetting and Power-Up Problems. It was discovered as part of this effort that the processor Sperry Sun was using has anomalous behavior when being reset at high temperatures. This required software changes to be made both in the downhole code and tool programming code. The changes that were required provided another opportunity to improve the robustness of the downhole tool string. This is one of the indicators that translating the processor to a high-temperature semiconductor would be very beneficial in producing a new range of high-temperature tools.

Identification of Circuit Design Weaknesses. As the process of screening MWD components for higher and higher temperatures was conducted, unexpected problems were observed, including voltage reference drift problems

and capacitor failures. Voltage reference drift proved difficult to solve because of its impact on the power supply. (This is another candidate for high-temperature semiconductor technology.) The capacitor issue identified a failure in the QC process of production and led to a re-evaluation of tantalum capacitors and testing under high-stress conditions. This work was undertaken independently (not as part of this contract) with a company, which Sperry Sun subcontracted to investigate this issue. A further conclusion regarding capacitor problems is that only improving the silicon is not enough. To make high-temperature tools, we need to develop designs which eliminate the need for these types of capacitors or work with manufacturers to build very high-temperature (high-capacitance) capacitors. Sperry Sun believes the temperature range of some low (<100,000 pF) capacitor technologies can be extended; however, they are less certain that it will be possible to economically extend high value technologies.

The project has helped in clearly demonstrating the limitations of the methods Sperry Sun is currently using to produce high-temperature tools. Based on this work, they are considering the available high-temperature technologies and looking at approaches for introducing these technologies over the longer term.

Conclusions and Recommendations

- 1. Results of this development effort showed that, while it is possible to build a mud-pulse MWD tool that can operate at 195° C, performance of the current tool is probably not sufficient for commercial success.** The current temperature limit of 175° C is apparently the practical limit for conventional electronics. This conclusion is further supported by Sperry Sun's decision to market two tools, one for service up to 150° C and another (the Solar 175) tool for service from 150 to 175° C. This decision was made based on the additional costs to screen components for the Solar tools, which make it more difficult to compete with lower temperature tools from other manufacturers. Currently, the bulk of commercial MWD work is at temperatures below 150° C.
- 2. Industry's current R&D goals and perception of future MWD requirements do not focus on operations in hotter and deeper formations.** Sperry Sun (for example) is pursuing the larger segment of the market (operations at less than 150° C). Their corporate vision is not in strict agreement with the DOE's vision that future gas needs for the USA will be met with gas produced from deeper, hotter reservoirs. However, businesses almost always trend toward the high-volume sector(s) of business. This apparent difference in vision may indicate that the service industry does not currently recognize what the future needs will be. The DOE can help bridge this gap in perception by presenting data that demonstrate how much gas is located in high-temperature reservoirs. If this information describing future markets is not readily available, the DOE could fund a study to highlight the quantity and location of current and future high-temperature reserves. These data may then serve to encourage the MWD industry to place resources into development of tools for high-temperature operations.

3. **Due to the extensive testing required and the high percentage of failing components, use of a binning qualification process to build high-temperature (195° C) MWD tools is very costly.** Costs to screen individual components, then subassemblies, and finally completed tools for high-temperature operations are very high. Tests also show a relatively short life for high-temperature tools. These factors mean that the daily cost of an MWD tool developed through binning processes will be much higher than a conventional tool.
4. **Increasing the operating temperature of current MWD tools will require development of a new platform for the electronics used in these tools.** This technology already exists in a limited number of components, and has been used to develop some special geothermal tools. Sandia National Laboratory has taken the lead role in this area and is developing or interested in the development of tools based on silicon-on-insulator (SOI) technology to overcome high geothermal temperatures. Oilfield MWD could make use of SOI technology to develop the next generation of tools that could allow raising the current temperature limit (175°C) not marginally (as seems to be the limit with conventional electronics), but to as high as 300°C.
5. **There are several hindrances to the development of silicon-on-insulator (SOI) tools for the MWD industry.** First is the size of the task at hand. Since this represents a new platform, programming would have to be extensively modified. Sperry Sun and MTI estimate that this is at least a 2-man-year effort. This does not include testing and debugging after programming. Completely new circuits would have to be developed to use the SOI chips now available. In addition, some components still need to be improved for high-temperature use including magnetometers and accelerometers needed for determining direction and trajectory of the well. This project has advanced the development of these components, but more work is needed, including examining other non-conventional technologies to measure primary MWD parameters, angle, and direction. Perhaps one of the most challenging obstacles to the development of the next generation of MWD tools is the (understandable) reluctance of service companies to make obsolete their current inventories of tools.
6. **DOE leadership and partnership with industry can play a significant role in encouraging the development of high-temperature MWD tools to prepare for the future.** If the DOE's prediction of future requirements for higher and higher temperatures is correct, then the oil and gas industries could find themselves without proper means to exploit reserves to meet the nation's demand. This could have a significant impact on the US economy. The price of oil and gas is very volatile, and an inability to meet demand can result in rapid price increases. If reserves from hotter reservoirs were soon needed, it could require 2-3 years to develop the tools to efficiently recover them. During this period, prices would continue to rise, increasing the cost of US products and the costs to maintain the current standard of living. The DOE can encourage industry to develop critical components needed to construct new high-

temperature platforms. Providing funding will help reduce the risk and offset the loss for obsolescence of current inventories. Critical components include the magnetometer and accelerometers, as well as the new circuits that implement SOI technology. The final critical area for DOE assistance is in programming required for the new platform. MTI and Sperry Sun believe that the best area to start this work is to develop the primary processor chip using SOI technology. It may be possible to build the current processor using this method, which could reduce reprogramming time. Development of high-temperature directional packages is equally important since these are common to all MWD tools.

Appendix A
Field Test Report

Technical Services

Job Number: HD-MJ-10113

Solar 195

Lavaca Co., Texas

<1 Aug to 14 Aug 2001>

Tech Services Engineers: Harvey Mueller

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Objectives

– Purpose of Job

This well was a sidetrack to the original straight hole. The target zone produced only water. The well was sidetracked to intersect the target payzone updip and above gas/water contact. The open hole sidetrack was done using Solar 175 directional tools. Directional tools were run to maintain directional control of the wellpath and the Natural Gamma Ray logging tool was included to correlate with offset wells, determine formation tops and payzone thickness.

– Goals

The development Solar 195 tools were run in this well to test the operation and survivability of these tools. Anticipated BHT was expected to be 360° F at a depth of 18400 ft. using 18.5# oil base mud. This would test of the operational capabilities of these tools.

– Test Plan

BHT was 321° F at a depth of 16500 toward the end of run 400 using Solar 175 tools. The Solar 195 tools were run on the following and all subsequent runs. The Solar 195 tools are a drop in replacement and will provide surveys and Gamma data.

– NEPA Information

4. Project/Activity Description: The proposed action involves field testing a new drilling services system, specifically a **Solar 195 Directional Gamma MWD tool**, in order to assess the system's performance level. DOE's contractor is responsible for identifying field test opportunities, i.e., a well, and arranging all logistics with the operator (owner) of the well to conduct the drilling system performance test. A wellbore or section of wellbore will be drilled with the motor/bit combination for an appropriately permitted well.

Drill cuttings (sandstone, shale, & limestone fragments) will be generated during operation/testing of the product. These cuttings, however, are not incremental waste. The cuttings will be generated by the well owner's own actions (drilling operations), whether testing of the DOE-sponsored product(s) occurs or not. The well operator/owner is responsible for proper treatment and disposition of the cuttings.

The DOE-sponsored drilling product will be "on location" (at the wellsite) for varying lengths of time. It is anticipated that the drilling system will be on location for about 1 weeks, beginning on or about **24 Jul 2001**.

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

5. Brief Description of Affected Environment: Field performance testing of the drilling system will occur in an appropriately permitted well. Testing of the motor/bits will take place in the **John W. Hancock, Sr A-1 ST**, a **new well**, located **29° 18' N Latitude and 96° 38' W Longitude**. The well is owned/operated by **Louis Dreyfus Natural Gas** and will be located **10 mi SE of Hallettsville, TX**. The surface environment in the immediate vicinity is **gently rolling grassland associated with local farms and ranches**.

The affected environment will be primarily below ground level (subsurface, as a well is being drilled). The drilling, using the **Solar 195 Directional Gamma MWD tool**, will take place in an appropriately permitted well, thus all penetrated strata will be treated in an approved manner, e.g., aquifers isolated, etc.

Summary

Run 500 Timeline

01 Aug 17:30 Below rotary
01 Aug 18:00 Shallow test
02 Aug 11:45 On bottom and start drilling; First recorded temperature- 353° F
04 Aug 23:00 Tool quit pulsing; Drill ahead blind
05 Aug 01:44 Last good data point in Gamma memory; After this point all Bank A, B and C were filled with 7590 or 7650.
05 Aug 01:54 Gap in gamma data 01:54:42 to 01:58:41
05 Aug 10:16 Gap in gamma data from 10:16:13 to 12:49:49
05 Aug 15:13 Gap in gamma data from 15:13:11 to 06 Aug 02:57:02
06 Aug 02:30 End of run

Run 500 Post Run Evaluation

Mk 8 Pulser 8176

Incoming:

Passed resistance test but failed poppet extension and bench test. No signs of mud leaking out of the tool.

Tear down:

The pulser was full of drilling fluids. The origin of the drill fluid intrusion was the seal pack and the o-ring seal on the poppet shaft. The o-rings in the seal pack was nibbled. Where the poppet shaft rides on the seal pack the shaft showed some pitting on it. The o-ring on the poppet shaft was extruded and blown inward into the pulser. All the case seal o-rings looked good. The o-rings on the kemlon feedthru's were still sealing but showed some sign's of extrusion. The intermediate case was checked and it had no cracks.

Over view:

The upper bearing was also very worn. The upper bearing in this pulser measured .4491. The old bearing was worn out so far it couldn't be pressed out. A new bearing in the end plug measured .4341 This leaves a gap of .015. This upper bearing ring ID has an extreme amount of wear. We control the ID to within a

01 Aug 2001 – 14 Aug 2001

.0003" tolerance. It wore .015" oversized diametral in a relatively short amount of time. The wear would have allowed for more and more lateral deflection of the poppet.

A new end plug assembly was picked out at random and was measured.

New housing = .5650

New bearing O.D. = .5675

New bearing I.D. = .4353

New bearing I.D. installed = .4341

Poppet shaft O.D. = .4341

BM 146746

Incoming:

Downloaded memory data successfully using INSITE. Manually enabled sub bus power from the batteries. Sub bus power was ~10 V. and would fail once CIM I/O card power was removed from the SBM. It appears the batteries were depleted, perhaps due to the short in the end plug.

Tear down:

Tested the SBM electronics at 195°C. The board is still working as it is supposed to. It is measuring the battery voltages, currents, and temperature correctly. The battery over-current protection is also still functioning as specified.

The cells do appear to be near dead from room temperature evaluation. In the next 2 weeks I plan on getting the cells heated up and tested again at or above 125°C. Their present poor performance could be due to the cold room temperature.

Overview:

Run 600 Timeline

06 Aug 03:30 Below Rotary

06 Aug 18:30 Begin reaming to log Gamma over section lost when tool failed on previous run

06 Aug 22:00 On bottom; begin drilling

06 Aug 05:30 Tool quit pulsing; Drill ahead blind.

13 Aug 22:00 End of run

Run 600 Post Run Evaluation

Mk 8 Pulser 8178

Incoming:

Passed resistance test but failed poppet extension and bench test. The poppet cap was broken.

Tear down:

The pulser was full of drilling fluids. The origin of the drill fluid intrusion was the seal pack and the o-ring seal on the poppet shaft. The poppet shaft had two grooves in it where it was hitting the end cap. There was no upper bearing in the end cap. This caused premature failure in the bootless top end and the breaking of the poppet cap. All the case seal o-rings looked good. The o-rings on the kemlon feedthru's were still sealing but showed some sign's of extrusion.

The intermediate case was checked and it had no cracks.

Over view:

The upper bearing was not installed and caused the failure of the pulser.

TM 146620

Incoming:

We were unable to communicate with the TM.

Tear down:

Upon pulling the electronics from the case it was found that the backup battery had vented which damaged the wiring to the electronics package. The backup battery was removed and we attempted to communicate with the electronics but were unable to as the vented cell damaged the boards.

Overview:

The backup battery caused the failure on the TM. It has not yet been determined what caused the backup battery to vent.

BM 146747

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

Recommendations

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

Job Report

– End of Well Report

**End of Well Report
for
Louis Dreyfus Natural Gas**

Rig: H & P 89
Well: John W. Hancock Sr. #A-1 ST
Field: Wildcat
Country: U.S.A.
Job No: HD-MJ-10113
Date: 08-Jul-01
API No: 42-285-32871-01

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3. Summary of MWD Runs
4. Bitrun Summary
5. Directional Survey Data
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General Information

Company: Louis Dreyfus Natural Gas
Rig: H & P 89
Well: John W. Hancock Sr. #A-1 ST
Field: Wildcat
Country: U.S.A.
API Number: 42-285-32871-01
Sperry-Sun Job Number: HD-MJ-10113
Job start date: 08-Jul-01
Job end date: 09-Aug-01
North reference: Grid
Declination: 5.138 deg
Dip angle: 58.842 deg
Total magnetic field: 48529.223 nt
Date of magnetic data: 01-Jan-70
Wellhead coordinates N: 29 deg. 18 min 1.640 sec North
Wellhead coordinates E: 96 deg. 38 min 34.350 sec West
Vertical section direction: 122.526 deg
MWD Engineers: K. McCoy T. Bufford
L. Motl

Company Representatives: D. Patton R. Coates

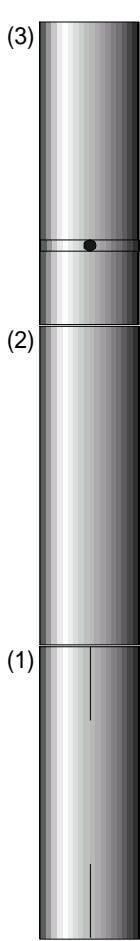
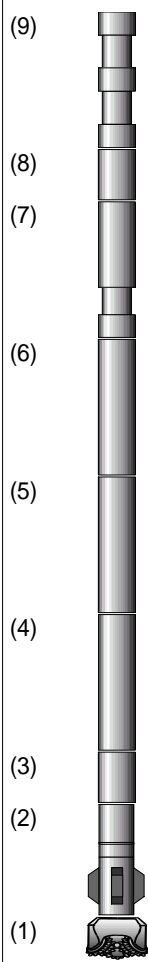
Company Geologist:
Lease Name: John W. Hancock Sr.
Unit Number:
State: Texas
County: Lavaca

Operational Overview

Sperry-Sun Drilling Services was contracted to provide Solar 175 MWD and directional drilling services for sidetracking the John W. Hancock Sr. A-1 well. MWD services began 08-Jul-01. The sidetrack was completed 12-Aug at a measured depth of 17777'. Run 100 was a directional only run to open hole sidetrack the well at 14153' MD. The run started 09-Jul and was completed at 14212' MD 12-Jul after 50 circulating hours. MWD tool RPM's dropped from 3200 to 2200 during the run, but caused no problems during the run. Post-run inspection revealed damaged marine bearings. Run 200 directional / gamma run began 12-Jul and was completed at 15094' MD after 136 circulating hours. MWD tool RPM's caused the intermittent pulsing during the run and ranged from 3200 at run start to 1200 at end of run. Pulser failed post-run poppet extension test. Run 300 began 19-Jul and was completed 20-Jul after MWD quit pulsing after 16.5 circulating hours. Tool sent to R & M for testing. Run 400 began 21-Jul and was completed 31-Jul after 213 circulating hours. MWD setup was changed to compensate for RPM loss during run. Tool RPM's ran from 3900 at start of run to 2200 at end of run. Post run inspection revealed damaged marine bearings. Maximum temperature during run was 332°F. Pulser failed post-run retraction test. Run 500 was the first run for the Solar 195 tool. The run started 01-Aug. at 16719' MD. MWD quit pulsing after 55 circulating hours. Drilled ahead 19 hours without real-time MWD. Tool logged 2 hours after failure before short in end plug turned the subbus off. Maximum temperature prior to failure was 360°F. and maximum temperature recorded in tool was 367 deg. F. Pulser failed post-run retraction test. Run 600 with Solar 195 tool began 06-Aug 17173' MD. Logged 130' of data lost on prior run and started drilling at 2200 06-Aug. MWD quit pulsing at 05:30 07-Aug. Drilled ahead to TD without MWD.^a«

Bitrun Summary

Run Time Data		Drilling Data		Mud Data			
MWD Run :	0100	Start Depth :	14153.00 ft	Mud Type :	Oil Based		
Rig Bit No:	0100	End Depth :	14212.00 ft	Weight / Visc :	18.10 ppg /	90.00	spqt
Hole Size :	6.75 in	Footage :	59.00 ft	Chlorides :	0.00 mg/l		
Run Start :	09-Jul-01 20:00	Avg. Flow Rate :	234.00 gpm	PV / YP :	58.00 cp /	15.00	lhf2
Run End :	12-Jul-01 14:00	Avg. RPM :	40.00 rpm	Solids/Sand :	40 % /	TR	%
BRT Hrs :	66.00	Avg. WOB :	2.00 klb	%Oil / O:W :	53.5 % /	90/10	
Circ. Hrs :	50.00	Avg. ROP :	2.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm
Oper. Hrs :	66.00	Avg. SPP :	3000.00 psig	Max. Temp. :	302.00 degF		

MWD Schematics	BHA Schematics			
 <p>(3) MARK VII SN : 102</p> <p>(2) Telemetry Module SN : 132003 0.00 ft Distance from Bit</p> <p>(1) Directional Module SN : 90554 0.00 ft Distance from Bit</p>		<p>(9) Component</p> <p>(8)</p> <p>(7)</p> <p>(6)</p> <p>(5)</p> <p>(4)</p> <p>(3)</p> <p>(2)</p> <p>(1)</p>	<p>Length (ft)</p> <p>O.D. (in)</p> <p>I.D. (in)</p>	<p>09. 6x HWDP 184.78 4.000 2.560</p> <p>08. Cross Over Sub 2.67 5.188 2.250</p> <p>07. Drilling Jars 30.15 4.750 2.250</p> <p>06. 3x Drill collar 89.41 4.750 2.250</p> <p>05. 1 x Non-Mag Drill Collar 31.19 4.750 2.250</p> <p>04. DWD SlimHole 28.61 4.750 2.810</p> <p>03. Float Sub 2.33 4.750 2.250</p> <p>02. 4-3/4"SperryDrillLobe 4/5-6.3s 25.12 4.750 2.794</p> <p>01. Diamond 0.54 6.750 1.920</p>

Comments	MWD Performance
<p>Time drilled to sidetrack well. POOH to change bit type and BHA. 100% MWD Run. Tool Setup: 35 IMP / 30 IFA Stator / 1.675 DT</p>	<p>Tool OD / Type : 4.75 in / HH</p> <p>MWD Real-time%: 100.00 % / 100.00 %</p> <p>MWD Recorded%: 0.00 % / 0.00 %</p> <p>Min. Inc. : 4.40 deg / 14145.00 ft</p> <p>Max. Inc. : 4.50 deg / 14113.00 ft</p> <p>Final Az. : 120.50 deg</p> <p>Max Op. Press. : 13270.92 psig</p>

Bitrun Summary

Run Time Data		Drilling Data		Mud Data			
MWD Run :	0200	Start Depth :	14212.00 ft	Mud Type :	Oil Based		
Rig Bit No:	0200	End Depth :	15094.00 ft	Weight / Visc :	17.90 ppg /	64.00	spqt
Hole Size :	6.75 in	Footage :	882.00 ft	Chlorides :	0.00 mg/l		
Run Start :	12-Jul-01 14:00	Avg. Flow Rate :	234.00 gpm	PV / YP :	63.00 cp /	16.00	lhf2
Run End :	19-Jul-01 11:00	Avg. RPM :	45.00 rpm	Solids/Sand :	39.44 % /		%
BRT Hrs :	165.00	Avg. WOB :	10.00 klb	%Oil / O:W :	54 % /	90/10	
Circ. Hrs :	136.00	Avg. ROP :	5.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm
Oper. Hrs :	165.00	Avg. SPP :	3200.00 psig	Max. Temp. :	289.00 degF		

MWD Schematics		BHA Schematics			
<p>(4)</p> <p>(3)</p> <p>(2)</p> <p>(1)</p> <p>4. MARK VII SN : 90</p> <p>3. Telemetry Module SN : 86654 0.00 ft Distance from Bit</p> <p>2. Directional Module SN : 90554 0.00 ft Distance from Bit</p> <p>1. Gamma Module SN : 156070 0.00 ft Distance from Bit</p>	<p>(11)</p> <p>(10)</p> <p>(9)</p> <p>(8)</p> <p>(7)</p> <p>(6)</p> <p>(5)</p> <p>(4)</p> <p>(3)</p> <p>(2)</p> <p>(1)</p>	<p>Component</p> <p>Length (ft)</p> <p>O.D. (in)</p> <p>I.D. (in)</p> <p>11. 6x HWDP 184.78 4.000 2.560</p> <p>10. Cross Over Sub 2.67 5.188 2.250</p> <p>09. 3x Drill collar 91.90 4.750 2.250</p> <p>08. 2x Drill collar 60.00 4.750 2.375</p> <p>07. Drilling Jars 30.15 4.750 2.250</p> <p>06. Drill collar 29.41 4.750 2.375</p> <p>05. 1 x Non-Mag Drill Collar 31.19 4.750 2.250</p> <p>04. DGWD SlimHole 28.61 4.750 2.810</p> <p>03. Float Sub 2.33 4.750 2.250</p> <p>02. 4-3/4"SperryDrillLobe 4/5-6.3s 25.10 4.750 2.794</p> <p>01. PDC 1.00 6.750 2.560</p>			

Comments	MWD Performance
<p>Drilled ahead with sliding to build angle. POOH to switch MWD tool failure, change bit and motor. Tool config.30 deg. stator, 35 deg. imp, 1.675 DT orifice.</p>	<p>Tool OD / Type : 4.75 in / HH</p> <p>MWD Real-time%: 100.00 % / 100.00 %</p> <p>MWD Recorded%: 100.00 % / 0.00 %</p> <p>Min. Inc. : 3.20 deg/ 14174.00 ft</p> <p>Max. Inc. : 30.20 deg/ 15004.00 ft</p> <p>Final Az. : 116.10 deg</p> <p>Max Op. Press. : 13868.92 psig</p>

Bitrun Summary

Run Time Data		Drilling Data		Mud Data																																																																																								
MWD Run :	0300	Start Depth :	15094.00 ft	Mud Type :	Oil Based																																																																																							
Rig Bit No:	0300	End Depth :	15195.00 ft	Weight / Visc :	17.90 ppg /	75.00	spqt																																																																																					
Hole Size :	6.75 in	Footage :	101.00 ft	Chlorides :	0.00 mg/l																																																																																							
Run Start :	19-Jul-01 12:00	Avg. Flow Rate :	238.00 gpm	PV / YP :	60.00 cp /	16.00	lhf2																																																																																					
Run End :	20-Jul-01 23:00	Avg. RPM :	45.00 rpm	Solids/Sand :	40.5 % /		%																																																																																					
BRT Hrs :	35.00	Avg. WOB :	5.00 klb	%Oil / O:W :	54 % /	91/9																																																																																						
Circ. Hrs :	18.00	Avg. ROP :	5.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm																																																																																					
Oper. Hrs :	35.00	Avg. SPP :	3200.00 psig	Max. Temp. :	304.00 degF																																																																																							
MWD Schematics		BHA Schematics																																																																																										
<p>(4) MARK VII SN : 102</p> <p>(3) Telemetry Module SN : 132003 0.00 ft Distance from Bit</p> <p>(2) Directional Module SN : 122099 0.00 ft Distance from Bit</p> <p>(1) Gamma Module SN : 78005 0.00 ft Distance from Bit</p>		<table border="1"> <thead> <tr> <th>(11)</th> <th>Component</th> <th>Length (ft)</th> <th>O.D. (in)</th> <th>I.D. (in)</th> </tr> </thead> <tbody> <tr><td>(11)</td><td>6x HWDP</td><td>184.78</td><td>4.000</td><td>2.560</td></tr> <tr><td>(10)</td><td></td><td></td><td></td><td></td></tr> <tr><td>(9)</td><td></td><td></td><td></td><td></td></tr> <tr><td>(8)</td><td></td><td></td><td></td><td></td></tr> <tr><td>(7)</td><td></td><td></td><td></td><td></td></tr> <tr><td>(6)</td><td>11. 6x HWDP</td><td>184.78</td><td>4.000</td><td>2.560</td></tr> <tr><td>(5)</td><td>10. Cross Over Sub</td><td>2.67</td><td>5.188</td><td>2.250</td></tr> <tr><td>(4)</td><td>09. 3x Drill collar</td><td>91.90</td><td>4.750</td><td>2.250</td></tr> <tr><td>(3)</td><td>08. 2x Drill collar</td><td>60.00</td><td>4.750</td><td>2.375</td></tr> <tr><td>(2)</td><td>07. Drilling Jars</td><td>30.15</td><td>4.750</td><td>2.250</td></tr> <tr><td>(1)</td><td>06. Drill collar</td><td>29.41</td><td>4.750</td><td>2.375</td></tr> <tr><td>(11)</td><td>05. 1 x Non-Mag Drill Collar</td><td>31.19</td><td>4.750</td><td>2.250</td></tr> <tr><td>(10)</td><td>04. SOLAR DGWD SlimHole</td><td>28.61</td><td>4.750</td><td>2.810</td></tr> <tr><td>(9)</td><td>03. Float Sub</td><td>2.33</td><td>4.750</td><td>2.250</td></tr> <tr><td>(8)</td><td>02. 4-3/4" SperryDrill 4/5 6.3 stg</td><td>25.01</td><td>4.750</td><td>2.794</td></tr> <tr><td>(7)</td><td>01. PDC</td><td>1.00</td><td>6.750</td><td>2.560</td></tr> </tbody> </table>						(11)	Component	Length (ft)	O.D. (in)	I.D. (in)	(11)	6x HWDP	184.78	4.000	2.560	(10)					(9)					(8)					(7)					(6)	11. 6x HWDP	184.78	4.000	2.560	(5)	10. Cross Over Sub	2.67	5.188	2.250	(4)	09. 3x Drill collar	91.90	4.750	2.250	(3)	08. 2x Drill collar	60.00	4.750	2.375	(2)	07. Drilling Jars	30.15	4.750	2.250	(1)	06. Drill collar	29.41	4.750	2.375	(11)	05. 1 x Non-Mag Drill Collar	31.19	4.750	2.250	(10)	04. SOLAR DGWD SlimHole	28.61	4.750	2.810	(9)	03. Float Sub	2.33	4.750	2.250	(8)	02. 4-3/4" SperryDrill 4/5 6.3 stg	25.01	4.750	2.794	(7)	01. PDC	1.00	6.750	2.560
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Comments				MWD Performance																																																																																								
POOH for MWD. Tool flatlined after 16.5 circ. hrs.. Tool Setup: 35 IMP / 30 IFA / 1.675 DT				Tool OD / Type : 4.75 in / HH MWD Real-time%: 90.00 % / 90.00 % MWD Recorded%: 90.00 % / 0.00 % Min. Inc. : 31.00 deg / 15036.00 ft Max. Inc. : 34.20 deg / 15131.00 ft Final Az. : 118.60 deg Max Op. Press. : 14055.08 psig																																																																																								

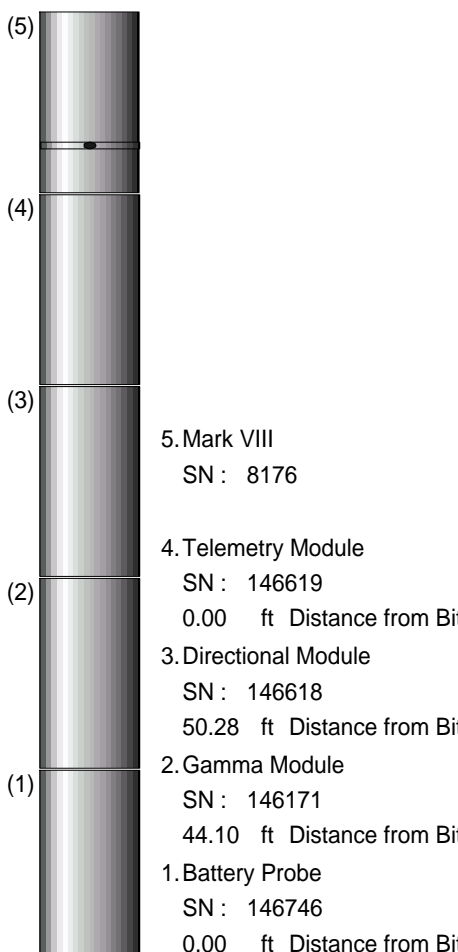
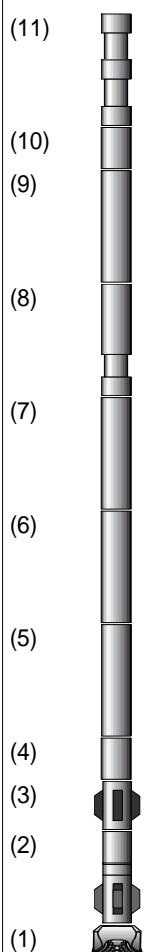
Bitrun Summary

Run Time Data		Drilling Data		Mud Data			
MWD Run :	0400	Start Depth :	15195.00 ft	Mud Type :	Oil Based		
Rig Bit No:	0400	End Depth :	16719.00 ft	Weight / Visc :	18.40 ppg /	90.00	spqt
Hole Size :	6.75 in	Footage :	1524.00 ft	Chlorides :	0.00 mg/l		
Run Start :	21-Jul-01 01:00	Avg. Flow Rate :	215.00 gpm	PV / YP :	74.00 cp /	28.00	lhf2
Run End :	31-Jul-01 13:30	Avg. RPM :	64.00 rpm	Solids/Sand :	41.5 % /		%
BRT Hrs :	252.50	Avg. WOB :	8.00 klb	%Oil / O:W :	53.5 % /	91/9	
Circ. Hrs :	213.00	Avg. ROP :	8.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm
Oper. Hrs :	252.50	Avg. SPP :	3300.00 psig	Max. Temp. :	318.00 degF		

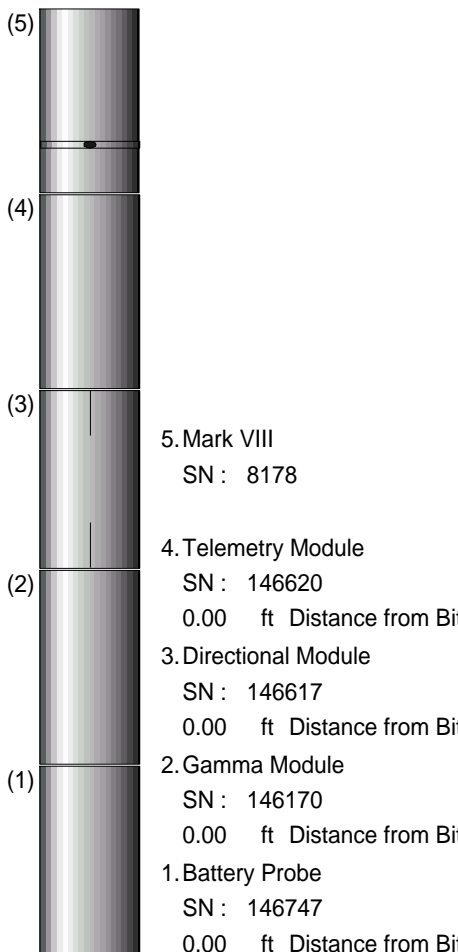
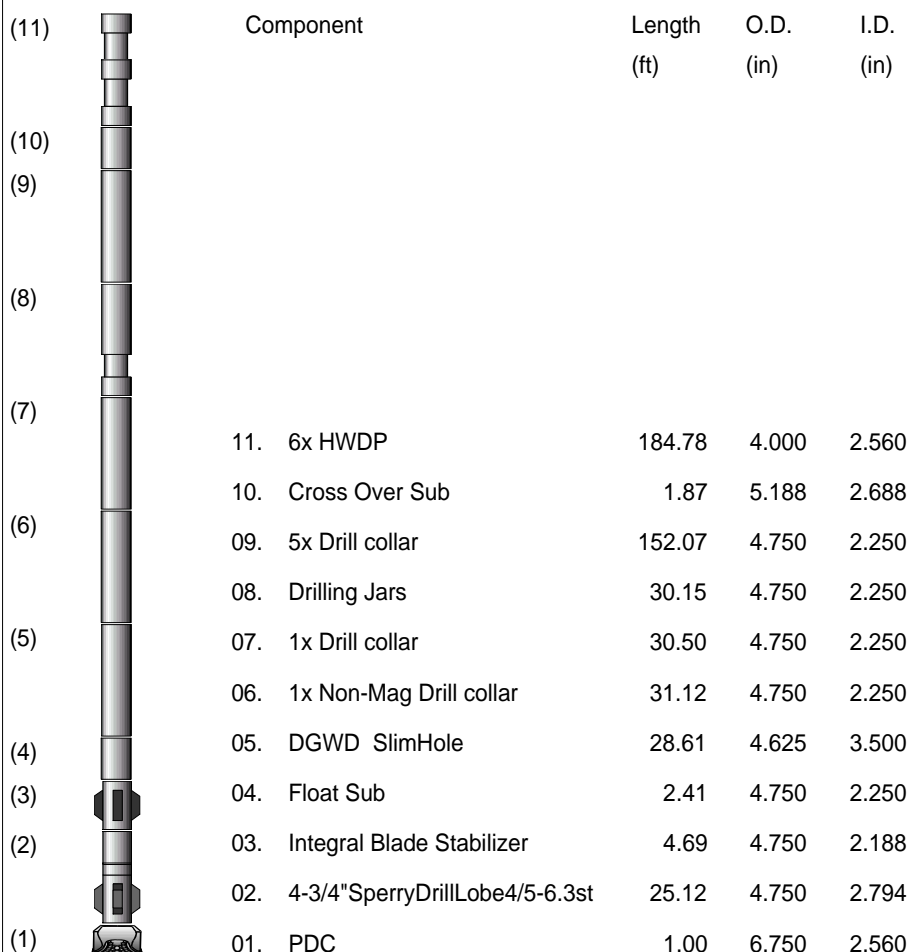
MWD Schematics		BHA Schematics			
<p>(4)</p> <p>(3)</p> <p>(2)</p> <p>(1)</p> <p>4. MARK VII SN : 76</p> <p>3. Telemetry Module SN : 86654 0.00 ft Distance from Bit</p> <p>2. Directional Module SN : 90554 0.00 ft Distance from Bit</p> <p>1. Gamma Module SN : 156070 0.00 ft Distance from Bit</p>	<p>(11)</p> <p>(10)</p> <p>(9)</p> <p>(8)</p> <p>(7)</p> <p>(6)</p> <p>(5)</p> <p>(4)</p> <p>(3)</p> <p>(2)</p> <p>(1)</p>	<p>Component</p> <p>Length (ft)</p> <p>O.D. (in)</p> <p>I.D. (in)</p> <p>11. 6x HWDP 184.78 4.000 2.560</p> <p>10. Cross Over Sub 2.67 5.188 2.250</p> <p>09. 3x Drill collar 91.90 4.750 2.250</p> <p>08. 2x Drill collar 60.00 4.750 2.375</p> <p>07. Drilling Jars 30.15 4.750 2.250</p> <p>06. Drill collar 29.41 4.750 2.375</p> <p>05. 1 x Non-Mag Drill Collar 31.19 4.750 2.250</p> <p>04. SOLAR DGWD SlimHole 28.61 4.750 2.810</p> <p>03. Float Sub 2.33 4.750 2.250</p> <p>02. 4-3/4" SperryDrill 4/5 6.3 stg 24.40 4.750 2.794</p> <p>01. PDC 1.00 6.750 2.560</p>			

Comments	MWD Performance
100 % MWD run. POOH to switch BHA, MWD because of hours, and test BOP's.ª«35 impeller, 41 stator, 1.675 orifice.ª«	<p>Tool OD / Type : 4.75 in / HH</p> <p>MWD Real-time%: 100.00 % / 100.00 %</p> <p>MWD Recorded%: 100.00 % / 0.00 %</p> <p>Min. Inc. : 34.30 deg/ 15131.00 ft</p> <p>Max. Inc. : 48.30 deg/ 16661.00 ft</p> <p>Final Az. : 119.10 deg</p> <p>Max Op. Press. : 15996.74 psig</p>

Bitrun Summary

Run Time Data		Drilling Data		Mud Data																																																															
MWD Run :	0500	Start Depth :	16719.00 ft	Mud Type :	Oil Based																																																														
Rig Bit No:	0500	End Depth :	17173.00 ft	Weight / Visc :	18.50 ppg /	63.00	spqt																																																												
Hole Size :	6.75 in	Footage :	454.00 ft	Chlorides :	0.00 mg/l																																																														
Run Start :	01-Aug-01 17:30	Avg. Flow Rate :	211.00 gpm	PV / YP :	48.00 cp /	7.00	lhf2																																																												
Run End :	06-Aug-01 02:30	Avg. RPM :	55.00 rpm	Solids/Sand :	41.5 % /		%																																																												
BRT Hrs :	105.00	Avg. WOB :	10.00 klb	%Oil / O:W :	53 % /	91/9																																																													
Circ. Hrs :	74.00	Avg. ROP :	12.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm																																																												
Oper. Hrs :	105.00	Avg. SPP :	3200.00 psig	Max. Temp. :	353.00 degF																																																														
MWD Schematics		BHA Schematics																																																																	
 <p>(5) 5. Mark VIII SN : 8176</p> <p>(4) 4. Telemetry Module SN : 146619 0.00 ft Distance from Bit</p> <p>(3) 3. Directional Module SN : 146618 50.28 ft Distance from Bit</p> <p>(2) 2. Gamma Module SN : 146171 44.10 ft Distance from Bit</p> <p>(1) 1. Battery Probe SN : 146746 0.00 ft Distance from Bit</p>		 <table border="1"> <thead> <tr> <th>(11)</th> <th>Component</th> <th>Length (ft)</th> <th>O.D. (in)</th> <th>I.D. (in)</th> </tr> </thead> <tbody> <tr> <td>(11)</td> <td>11. 6x HWDP</td> <td>184.78</td> <td>4.000</td> <td>2.560</td> </tr> <tr> <td>(10)</td> <td>10. Cross Over Sub</td> <td>1.87</td> <td>5.188</td> <td>2.688</td> </tr> <tr> <td>(9)</td> <td>09. 5x Drill collar</td> <td>152.07</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(8)</td> <td>08. Drilling Jars</td> <td>30.15</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(7)</td> <td>07. 1x Drill collar</td> <td>30.50</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(6)</td> <td>06. 1x Non-Mag Drill collar</td> <td>31.12</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(5)</td> <td>05. DGWD SlimHole</td> <td>24.47</td> <td>4.625</td> <td>3.500</td> </tr> <tr> <td>(4)</td> <td>04. Float Sub</td> <td>2.41</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(3)</td> <td>03. Integral Blade Stabilizer</td> <td>5.68</td> <td>4.750</td> <td>1.938</td> </tr> <tr> <td>(2)</td> <td>02. 4-3/4"SperryDrillLobe4/5-6.3st</td> <td>24.40</td> <td>4.750</td> <td>2.794</td> </tr> <tr> <td>(1)</td> <td>01. PDC</td> <td>1.00</td> <td>6.750</td> <td>2.560</td> </tr> </tbody> </table>						(11)	Component	Length (ft)	O.D. (in)	I.D. (in)	(11)	11. 6x HWDP	184.78	4.000	2.560	(10)	10. Cross Over Sub	1.87	5.188	2.688	(9)	09. 5x Drill collar	152.07	4.750	2.250	(8)	08. Drilling Jars	30.15	4.750	2.250	(7)	07. 1x Drill collar	30.50	4.750	2.250	(6)	06. 1x Non-Mag Drill collar	31.12	4.750	2.250	(5)	05. DGWD SlimHole	24.47	4.625	3.500	(4)	04. Float Sub	2.41	4.750	2.250	(3)	03. Integral Blade Stabilizer	5.68	4.750	1.938	(2)	02. 4-3/4"SperryDrillLobe4/5-6.3st	24.40	4.750	2.794	(1)	01. PDC	1.00	6.750	2.560
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Comments				MWD Performance																																																															
MWD Failure. Orifice 1.6375, stator 41, impeller 35				Tool OD / Type : 4.75 in / HH MWD Real-time%: 70.00 % / 70.00 % MWD Recorded%: 70.00 % / 0.00 % Min. Inc. : 48.30 deg / 16662.00 ft Max. Inc. : 49.10 deg / 16757.00 ft Final Az. : 119.80 deg Max Op. Press. : 16434.81 psig																																																															

Bitrun Summary

Run Time Data		Drilling Data		Mud Data																																																															
MWD Run :	0600	Start Depth :	17173.00 ft	Mud Type :	Oil Based																																																														
Rig Bit No:	0600	End Depth :	17777.00 ft	Weight / Visc :	18.60 ppg /	74.00	spqt																																																												
Hole Size :	6.75 in	Footage :	604.00 ft	Chlorides :	0.00 mg/l																																																														
Run Start :	06-Aug-01 03:30	Avg. Flow Rate :	230.00 gpm	PV / YP :	49.00 cp /	9.00	lhf2																																																												
Run End :	13-Aug-01 22:00	Avg. RPM :	55.00 rpm	Solids/Sand :	42 % /		%																																																												
BRT Hrs :	186.50	Avg. WOB :	5.00 klb	%Oil / O:W :	52 % /	90/10																																																													
Circ. Hrs :	106.00	Avg. ROP :	5.00 fph	pH/Fluid Loss:	0.00 pH /	0.00	mptm																																																												
Oper. Hrs :	186.50	Avg. SPP :	3200.00 psig	Max. Temp. :	360.00 degF																																																														
MWD Schematics		BHA Schematics																																																																	
 <p>(5) 5. Mark VIII SN : 8178</p> <p>(4) 4. Telemetry Module SN : 146620 0.00 ft Distance from Bit</p> <p>(3) 3. Directional Module SN : 146617 0.00 ft Distance from Bit</p> <p>(2) 2. Gamma Module SN : 146170 0.00 ft Distance from Bit</p> <p>(1) 1. Battery Probe SN : 146747 0.00 ft Distance from Bit</p>		 <table border="1"> <thead> <tr> <th>(11)</th> <th>Component</th> <th>Length (ft)</th> <th>O.D. (in)</th> <th>I.D. (in)</th> </tr> </thead> <tbody> <tr> <td>(11)</td> <td>11. 6x HWDP</td> <td>184.78</td> <td>4.000</td> <td>2.560</td> </tr> <tr> <td>(10)</td> <td>10. Cross Over Sub</td> <td>1.87</td> <td>5.188</td> <td>2.688</td> </tr> <tr> <td>(9)</td> <td>09. 5x Drill collar</td> <td>152.07</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(8)</td> <td>08. Drilling Jars</td> <td>30.15</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(7)</td> <td>07. 1x Drill collar</td> <td>30.50</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(6)</td> <td>06. 1x Non-Mag Drill collar</td> <td>31.12</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(5)</td> <td>05. DGWD SlimHole</td> <td>28.61</td> <td>4.625</td> <td>3.500</td> </tr> <tr> <td>(4)</td> <td>04. Float Sub</td> <td>2.41</td> <td>4.750</td> <td>2.250</td> </tr> <tr> <td>(3)</td> <td>03. Integral Blade Stabilizer</td> <td>4.69</td> <td>4.750</td> <td>2.188</td> </tr> <tr> <td>(2)</td> <td>02. 4-3/4"SperryDrillLobe4/5-6.3st</td> <td>25.12</td> <td>4.750</td> <td>2.794</td> </tr> <tr> <td>(1)</td> <td>01. PDC</td> <td>1.00</td> <td>6.750</td> <td>2.560</td> </tr> </tbody> </table>						(11)	Component	Length (ft)	O.D. (in)	I.D. (in)	(11)	11. 6x HWDP	184.78	4.000	2.560	(10)	10. Cross Over Sub	1.87	5.188	2.688	(9)	09. 5x Drill collar	152.07	4.750	2.250	(8)	08. Drilling Jars	30.15	4.750	2.250	(7)	07. 1x Drill collar	30.50	4.750	2.250	(6)	06. 1x Non-Mag Drill collar	31.12	4.750	2.250	(5)	05. DGWD SlimHole	28.61	4.625	3.500	(4)	04. Float Sub	2.41	4.750	2.250	(3)	03. Integral Blade Stabilizer	4.69	4.750	2.188	(2)	02. 4-3/4"SperryDrillLobe4/5-6.3st	25.12	4.750	2.794	(1)	01. PDC	1.00	6.750	2.560
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Comments				MWD Performance																																																															
<p>MWD quit pulsing after 13 circulating hours. Drilled to TD without realtime MWD. 41/35, 1.650 DT orifice.</p>				<p>Tool OD / Type : 4.75 in / HH MWD Real-time%: 25.00 % / 25.00 % MWD Recorded%: 25.00 % / 0.00 % Min. Inc. : 48.10 deg / 17141.00 ft Max. Inc. : 48.30 deg / 17012.00 ft Final Az. : 122.60 deg Max Op. Press. : 166842.00psig</p>																																																															

Directional Survey Data

Measured Depth (feet)	Inclination (degrees)	Direction (degrees)	Vertical Depth (feet)	Latitude (feet)	Departure (feet)	Vertical Section (feet)	Dogleg (deg/100f)
14072.00	3.68	105.75	14067.00	109.35 N	23.75 W	-78.82	TIE-IN
14113.00	4.50	115.00	14107.90	108.31 N	21.03 W	-75.97	2.56
14145.00	4.40	120.50	14139.80	107.16 N	18.83 W	-73.49	1.37
14174.00	3.20	154.50	14168.74	105.86 N	17.52 W	-71.70	8.62
14206.00	5.90	195.90	14200.64	103.48 N	17.59 W	-70.47	12.77
14238.00	7.80	186.90	14232.41	99.74 N	18.30 W	-69.06	6.80
14269.00	8.50	177.00	14263.10	95.36 N	18.43 W	-66.82	5.05
14301.00	9.40	169.30	14294.71	90.43 N	17.82 W	-63.65	4.68
14333.00	9.80	159.70	14326.27	85.31 N	16.39 W	-59.69	5.15
14365.00	10.60	147.10	14357.76	80.28 N	13.85 W	-54.84	7.39
14397.00	11.20	143.70	14389.19	75.31 N	10.41 W	-49.27	2.75
14429.00	11.60	142.80	14420.56	70.24 N	6.63 W	-43.35	1.37
14461.00	12.30	137.20	14451.86	65.18 N	2.37 W	-37.04	4.23
14493.00	12.70	131.30	14483.11	60.35 N	2.59 E	-30.26	4.18
14525.00	13.40	124.40	14514.28	55.94 N	8.30 E	-23.08	5.33
14557.00	14.20	121.00	14545.36	51.82 N	14.72 E	-15.45	3.56
14588.00	15.70	117.10	14575.31	47.95 N	21.71 E	-7.47	5.82
14620.00	16.80	117.80	14606.03	43.82 N	29.66 E	1.44	3.49
14652.00	17.50	116.90	14636.61	39.49 N	38.04 E	10.84	2.34
14684.00	18.50	115.60	14667.04	35.12 N	46.91 E	20.67	3.37
14716.00	19.30	115.60	14697.32	30.64 N	56.26 E	30.96	2.50
14749.00	20.20	115.40	14728.37	25.84 N	66.32 E	42.03	2.73
14781.00	21.50	116.00	14758.28	20.90 N	76.58 E	53.34	4.12
14813.00	23.00	116.70	14787.89	15.52 N	87.44 E	65.38	4.76
14845.00	23.80	116.70	14817.26	9.81 N	98.79 E	78.02	2.50
14877.00	24.70	117.30	14846.44	3.84 N	110.50 E	91.11	2.92
14909.00	25.70	117.30	14875.39	2.41 S	122.61 E	104.67	3.13
14941.00	27.20	116.50	14904.04	8.86 S	135.32 E	118.86	4.82
14973.00	28.70	115.90	14932.31	15.48 S	148.78 E	133.76	4.77
15004.00	30.20	116.10	14959.30	22.16 S	162.48 E	148.91	4.85
15036.00	31.00	115.00	14986.85	29.18 S	177.17 E	165.07	3.05
15068.00	31.60	113.90	15014.19	36.06 S	192.31 E	181.53	2.59
15099.00	33.00	115.00	15040.39	42.92 S	207.39 E	197.93	4.90
15131.00	34.30	117.30	15067.03	50.74 S	223.30 E	215.55	5.69
15162.00	35.80	118.00	15092.41	59.00 S	239.06 E	233.29	5.01
15194.00	37.00	118.70	15118.16	68.02 S	255.78 E	252.23	3.97
15226.00	38.10	118.70	15143.53	77.39 S	272.88 E	271.69	3.44
15258.00	38.80	119.30	15168.59	87.03 S	290.28 E	291.55	2.48
15290.00	39.50	120.10	15193.41	97.04 S	307.83 E	311.73	2.70
15321.00	39.60	120.40	15217.31	106.99 S	324.88 E	331.45	0.70

Directional Survey Data

Measured Depth (feet)	Inclination (degrees)	Direction (degrees)	Vertical Depth (feet)	Latitude (feet)	Departure (feet)	Vertical Section (feet)	Dogleg (deg/100f)
15352.00	39.80	119.80	15241.16	116.92 S	342.02 E	351.23	1.39
15384.00	40.70	118.20	15265.59	126.94 S	360.10 E	371.87	4.28
15416.00	41.70	117.60	15289.67	136.80 S	378.73 E	392.88	3.36
15448.00	42.30	117.00	15313.45	146.62 S	397.75 E	414.20	2.26
15479.00	42.70	117.20	15336.30	156.16 S	416.40 E	435.05	1.36
15511.00	43.00	117.10	15359.76	166.09 S	435.76 E	456.72	0.96
15543.00	43.10	117.20	15383.15	176.06 S	455.20 E	478.47	0.38
15575.00	43.70	116.90	15406.40	186.06 S	474.78 E	500.35	1.98
15607.00	43.80	117.10	15429.51	196.10 S	494.50 E	522.38	0.53
15639.00	44.00	117.00	15452.57	206.20 S	514.26 E	544.47	0.66
15671.00	44.20	117.10	15475.55	216.32 S	534.09 E	566.63	0.66
15703.00	44.30	116.90	15498.47	226.46 S	553.99 E	588.86	0.54
15735.00	44.40	117.50	15521.35	236.69 S	573.88 E	611.13	1.35
15766.00	44.70	117.10	15543.45	246.66 S	593.21 E	632.79	1.33
15799.00	44.90	116.80	15566.86	257.20 S	613.94 E	655.93	0.88
15831.00	45.30	116.70	15589.45	267.40 S	634.18 E	678.48	1.27
15863.00	45.40	116.10	15611.94	277.52 S	654.57 E	701.12	1.37
15895.00	45.60	116.30	15634.37	287.60 S	675.05 E	723.80	0.77
15927.00	45.60	115.60	15656.76	297.60 S	695.61 E	746.51	1.56
15959.00	45.90	115.90	15679.09	307.56 S	716.25 E	769.28	1.15
15991.00	46.00	115.70	15701.33	317.57 S	736.96 E	792.12	0.55
16023.00	46.10	115.20	15723.54	327.47 S	757.76 E	814.98	1.17
16054.00	46.50	114.90	15744.96	336.96 S	778.06 E	837.20	1.47
16086.00	46.60	115.50	15766.97	346.85 S	799.08 E	860.24	1.40
16118.00	46.90	114.60	15788.90	356.72 S	820.20 E	883.35	2.25
16150.00	46.90	114.50	15810.76	366.43 S	841.45 E	906.49	0.23
16182.00	47.20	114.80	15832.56	376.20 S	862.74 E	929.69	1.16
16214.00	46.70	116.20	15854.41	386.26 S	883.85 E	952.90	3.56
16246.00	46.70	117.10	15876.35	396.71 S	904.66 E	976.07	2.05
16278.00	46.30	118.60	15898.38	407.55 S	925.18 E	999.20	3.62
16310.00	46.50	118.80	15920.45	418.68 S	945.51 E	1022.32	0.77
16342.00	46.60	119.10	15942.46	429.92 S	965.84 E	1045.51	0.75
16374.00	46.80	118.40	15964.40	441.13 S	986.26 E	1068.74	1.71
16437.00	46.00	119.10	16007.85	463.07 S	1026.25 E	1114.27	1.50
16501.00	46.40	118.70	16052.15	485.39 S	1066.69 E	1160.37	0.77
16533.00	46.60	118.70	16074.17	496.54 S	1087.05 E	1183.53	0.62
16565.00	46.80	118.60	16096.12	507.70 S	1107.49 E	1206.76	0.67
16597.00	47.20	119.20	16117.94	519.02 S	1127.98 E	1230.12	1.86
16629.00	47.70	118.90	16139.58	530.46 S	1148.59 E	1253.65	1.71
16661.00	48.30	119.10	16161.00	541.99 S	1169.39 E	1277.39	1.93

Directional Survey Data

Measured Depth (feet)	Inclination (degrees)	Direction (degrees)	Vertical Depth (feet)	Latitude (feet)	Departure (feet)	Vertical Section (feet)	Dogleg (deg/100f)
16693.00	49.00	118.30	16182.14	553.53 S	1190.46 E	1301.35	2.88
16757.00	49.10	118.80	16224.08	576.63 S	1232.92 E	1349.57	0.61
16821.00	48.80	119.10	16266.11	599.99 S	1275.15 E	1397.75	0.59
16885.00	48.60	119.10	16308.35	623.37 S	1317.16 E	1445.74	0.31
16949.00	48.30	119.80	16350.80	646.92 S	1358.87 E	1493.57	0.94
17012.00	48.30	121.20	16392.71	670.79 S	1399.40 E	1540.57	1.66
17077.00	48.20	121.90	16436.00	696.17 S	1440.72 E	1589.06	0.82
17141.00	48.10	122.60	16478.70	721.61 S	1481.04 E	1636.73	0.83
17777.00	48.10	122.60	16903.44	976.65 S	1879.84 E	2110.11	0.00

Directional Survey Data

CALCULATION BASED ON Minimum Curvature METHOD

SURVEY COORDINATES RELATIVE TO WELL SYSTEM REFERENCE POINT

TVD VALUES GIVEN RELATIVE TO DRILLING MEASUREMENT POINT

VERTICAL SECTION RELATIVE TO WELL HEAD

VERTICAL SECTION IS COMPUTED ALONG A DIRECTION OF 122.53 DEGREES (GRID)

A TOTAL CORRECTION OF 3.98 DEG FROM MAGNETIC NORTH TO GRID NORTH HAS BEEN APPLIED

HORIZONTAL DISPLACEMENT IS RELATIVE TO THE WELL HEAD.

HORIZONTAL DISPLACEMENT(CLOSURE) AT 17777.00 FEET

IS 2118.41 FEET ALONG 117.45 DEGREES (GRID)

TIE-IN SURVEY AT 14072' MD IS PROVIDED BY MULTI-SHOT.

SURVEYS FROM 14113' MD TO 17141' MD IS PROVIDED BY SPERRY-SUN MWD.

SURVEY AT 17141' MD IS PROJECTED TO TD AT 17777' MD.

SPERRY-SUN ENGINEERS, K. MCCOY AND T. BUFFORD.

Service Interrupt Report

MWD run number :	0500	Time/Date of Failure :	04-Aug-01 23:00
Rig Bit Number :	0500	Depth at time of Failure :	17015.00 ft
MWD Run start time/date :	01-Aug-01 17:30	Lost Rig Hours :	18.00
MWD Run end time/date :	06-Aug-01 02:30		

Rig Activity

Drilling ahead.

Description of Failure

Tool quit pulsing.

Action Taken

Cycled pumps, changed flow rates, changed pressure transducer, etc... Drilled ahead 19.5 hrs without MWD.

Operation Impact

POOH for MWD. Lost 130' of data. Delayed data delivery 24 hrs. 20 hrs lost rig time.

Reason for Failure

Pulser failed poppet retraction test. BM shorted sub bus.

Service Interrupt Report

MWD run number :	0600	Time/Date of Failure :	07-Aug-01 05:30
Rig Bit Number :	0600	Depth at time of Failure :	17233.00 ft
MWD Run start time/date :	06-Aug-01 03:30	Lost Rig Hours :	0.00
MWD Run end time/date :	13-Aug-01 22:00		

Rig Activity

Drilling ahead.

Description of Failure

Tool quit pulsing.

Action Taken

Cycled pumps, changed flow rates, changed pressure transducer, etc... Drilled ahead to TD without MWD.

Operation Impact

POOH for MWD. Lost 600' of data, delayed data delivery 96 hrs.

Reason for Failure

Found nut on top of poppet. Surface test revealed a broken poppet, and was unable to communicate with TM. Poppet failed poppet retraction test.

Sperry-Sun, A Halliburton Company



TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

LWD Logs

- Gamma Ray MD log from 16610 to 16760. Last reading from Solar 175 Gamma at 16681. Depths below this point are from Solar 195 Gamma tool.

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

Mud Reports



Drilling Fluids

OIL-BASED MUD REPORT No.94

Date	07/28/2001	Depth/TVD	16343 ft / 15943 ft
Spud Date	04/28/2001	Mud Type	Versadril
Water Depth		Activity	Drilling

Operator : Louis Dreyfus
 Report For : Royce Coats
 Well Name : John Hancock Sr. A-1
 Contractor : Helmerich & Payne #89
 Report For : Rick Hawthorne

Field/Area : NE. Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3887

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in PDC	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	13.375in @2986ft (2986TVD)	934	Pump Size	6 X 11 in	6 X 11 in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	8781 ft	9.625in @10751ft (10751TVD)	599	Pump stk/min	57@95%	
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	219 gal/min	
4 in	7075 ft	7.625in @14072ft (14072TVD)	1533	Bottoms Up	134 min	7636 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	294 min	16758 stk
4.75 in	302 ft		975	Circulating Pressure	3550 psi	

MUD PROPERTIES			
Sample From		PIT@03:00	
Flow Line Temp	°F	168	
Depth/TVD	ft	16343/15943	
Mud Weight	lb/gal	18@160°F	
Funnel Viscosity	s/qt	76	
Rheology Temp	°F	160	
R600/R300		139/79	
R200/R100		-/-	
R6/R3		-/-	
PV	cP	60	
YP	lb/100ft²	19	
10s/10m/30m Gel	lb/100ft²	5/17/24	
API Fluid Loss	cc/30 min	NA	
HTHP FL Temp	cc/30 min	2.8@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	40.5	
Correct Solids	%Vol	39.9	
Oil	%Vol	54	
Uncorr Water	%Vol	5.5	
Oil/Water Ratio		91/9	
Alkal (Pom)		2.8	
Cl Whole Mud	mg/l	13500	
Salt	%Wt	27.75	277500
Lime	lb/bbl	3.64	
E-Stability		1550	
Received Volume	bbl	2907	
Returned Volume	bbl	377	
Present Volume	bbl	2508	
Diff. Volume	bbl	-22	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	175
VERSACOAT	1 GA BK	15
VERSATROL	50 LB BG	2
OIL DRI ABSORBANT	50 LB BG	2
MUD DIESEL	1 GA BK	780
SHRINK WRAP	1 EA	2
TRUCKING SERVICE	1 EA	80
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KNOX)	50 LB BG	12

SOLIDS EQUIP		
	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	24
Derrick Shaker	175/175/175	24
D-Sander	212	0
D-Sifter	8T4	0

REMARKS AND TREATMENT

19 bbls Oil Added
 11 bbls Water Added
 13 bbls Products Added
 43 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2489 bbls Starting Volume
 2508 bbls Present Volume
 -24 bbls Mud Loss /24 hrs
 46 42 bbls Cumulative Mud Loss 8 bbls New Hole Volume

REMARKS

Drilled head rot. and slide to 16343'. Increased mud wt to 18.0 ppg due to high gas. Last survey @16278/15898'- 46.3 deg. BGRN gas - 30 to 110 units. Conn. gas 700 to 1570 units, and down time gas was 800 to 1075 units.

(corrected for side track well)
 Oil Base Mud Cuttings
 00 cu yds Daily Haul Off
 112 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL. ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service		Oil Added	0	Salt Wt%	27.75	np/ns Values
Drilling	24	Water Added	11	Salt Conc./bbl	7.4	0.522/0.522
Tripping		Mud Received	0	Adjusted Solid %	39.95	Bit Loss (psi / %)
Circulating		Dumped	0	Oil/Water Ratio	91/9	407 / 11.5
Chng Swvl Pkng		Shakers	18	Average SG Solids	4.1	Bit HHP (hbp / HSI)
P/U Rot. Head		Evaporation	6	Low Gr %	2.6	52 / 1.5
Slip Drill Line		Formation	0	High Gr Wt, lb/bbl	23.26	Bit Jet Vel (ft/s)
Dir Survey		Left in Hole	0	High Gr %	37.4	159
Testing		Trip Loss	0	High Gr Wt lb/bbl	549.51	Annular Vel DP (ft/min)
Fishing		Other	0			181.57
						Annular Vel DC (ft/min)
						233.37
						Crit Vel DP (ft/min)
						293
						Crit Vel DC (ft/min)
						365
						ECD @ 16343 (lb/gal)
						18.51

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Corky Karher 361 985-7424 Cell Phone 830 708-5715	361 798-7111	361 358-0181	\$ 4,128.66	\$ 802,991.83



M-I Drilling Fluids

P.O. Box 42842

HOUSTON, TEXAS USA

OIL MUD REPORT

REPORT NUMBER: 91

361-886-3400

WELL NUMBER	State TX	County	Well C3887	S/T
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Date 7/24/2001	Depth 15810 ft.
Spud Date 4/26/2001	Present Activity TVD-15575 Drig 8-15/Hr

OPERATOR Louis Dreyfus		CONTRACTOR Helmerich & Payne		RIG NUMBER 89
OPERATOR REPRESENTATIVE Royce Coats		CONTRACTOR REPRESENTATIVE Dale Molar		SECTION-TOWNSHIP-RANGE
WELL NAME AND NUMBER John Hancock Sr. A -1		FIELD OR BLOCK NUMBER NE Speaks	COUNTY, PARISH, OFFSHORE AREA Lavaca	STATE / PROV Texas

BIT DATA		DRILLING ASSEMBLY				MUD VOLUME		CIRCULATION DATA					
No	Size	Drill Pipe OD	ID	Length		Hole	Pits	Pump 1 Make/Model	Garner Denver PZ - 11				
	6.75 in	5	4.276	8248		914	646	Size	6 x 11	% Eff	95	bb/stk	0.0914
Type	SEC. PDC	Drill Pipe OD	ID	Length		Total Circulating Volume		Pump 2 Make/Model	Garner Denver PZ - 11				
		4	3.34	7075		1560		Size	6 x 11	% Eff	95	bb/stk	0.0914
		Drill Collar OD	ID	Length		In Storage	Weight	spm	bb/min	Total gal/min			
		4	2.56	185		395	18 ppg	Total bb/min	5.58	234			
		Drill Collar OD	ID	Length		In Storage	Weight	Circulating Pressure	3,550 psi				
		4.75	2.25	302		500	18 ppg	Ann. Vel. DP	194 ft/min	Ann. Vel. DC	249 ft/min		
DEVIATION		Size	Top @	0 Set @	10751	Mud Type		Bottoms Up Time	123 min	Total Circ. Time	280 min		
Angle	44.2 deg	Size	Top @	10428	Set @ 14072	VERSADRIL		Bottoms Up Stks	7,527	Total Circ. Stks	17,088		
Dir.	117.4	Size	Top @	Set @									
Depth	15660 ft	Size	Top @	Set @									

MUD PROPERTIES			MUD PROPERTY SPECIFICATIONS					
Sample From	PIT		Weight	17.9 ppg	Viscosity	60-70 sec/qt	Filtrate	< 4cc HTHP cc
Time Sample Taken	3:00 am		RECOMMENDED TREATMENT					
Flowline Temperature (deg F)	172	TVD	Oil Added	----- 17 bbls				
Depth (ft)	15810	15575	Water Added	----- 8 bbls				
Mud Weight (ppg)	17.9		Products Added	----- 1 bbls				
Funnel Viscosity @ 163 deg F (sec/qt)	70		Mud Built	----- 26 bbls				
Plastic Viscosity @ 160 deg F (cP)	59		Mud Received	----- 0 bbls				
Yield Point (lbs/100 sq ft)	16		Mud Returned	----- 0 bbls				
Gel Strength (10 sec/10 min) (lbs/100 sq ft)	6 / 16	27 /	Starting Volume	----- 2484 bbls				
API Filtrate (ml/30 min)			Present Volume	----- 2500 bbls				
HTHP Filtrate @ 400 deg F (ml/30 min)	2.4		Mud Loss / 24 hrs	----- 12 bbls				
Cake Thickness (API / HTHP) (32nd in)	/ 3	/	Cumm. Mud Loss	----- 3495 bbls				
Solids Content (% by vol)	40		Oilbase Mud Cuttings					
Oil / Water Content (% by vol)	55 / 6	/	Daily Haul Off	0 cu yds	Cumm. Haul Off	352 cu yds		
Solids Adjusted For Salt (% by vol)	39.3		REMARKS					
Alkalinity Mud (Pom)	1.8		Drig 8' to 15' / hr, Rolled storage tanks 4 hours					
Lime Content (lb/bbl)	2.34							
Salt Content Water Phase (% by Wt)	23.84							
Oil / Water Ratio	90 / 10	/						
Chlorides Whole Mud (mg/L)	11000							
Electrical Stability (volts)	1600							
Salt Content (PPM)	222,949							
New Hole (bbls)	8							
LCM (lb/bbl)								

PRODUCT INVENTORY						
7/24/2001	CLEAN UP	MUD DIESEL	ENGR SERVICE	BUCKLINE (KEND)	VERSATHIN	
DAILY MUD COST						
\$2,707.22						
CUMULATIVE COST						
\$71,207.96						
Starting Inventory	47	3,675		325	5	
Products Received		2,000				
Products Returned						
Used Last 24 Hours	1	383	1	5	5	
Closing Inventory	46	5,292		320		
Cost Last 24 Hours	\$66.80	\$340.87	\$650.00	\$224.00	\$1,266.30	
Used (from IADC)						

BIT RHEOLOGY and HYDRAULICS		SOLIDS ANALYSIS		MUD CONSUMPTION		TIME DISTRIBUTION		FOUR SOLIDS CONTROL EQUIPMENT	
Mud Gradient, psi/ft	0.9306	Low Gravity %	2.8	ADDITIONS bbls	9	RIG OPERATION Hrs		DEVICE / MAKE	SIZE #
Hydrostatic Pressure, psi	14,716	Low Gravity, ppb	25.1	Oil / ABO	12	Drilling	24.00	Derrick Shaker	3 x 14's
ECD, ppg		Bentonite %		Fresh Water		Circulating		Derrick Shaker	3 x 175
Bit weight (WOB), lbs	10	Bentonite, ppb		Brine Water		Tripping		Derrick Shaker	3 x 175
Bit RPM, rpm	70	Drill Solids %		Mud Built	1	Surveys		D-Sander	
		Drill Solids, ppb		Mud Transfer		Logging		D-Sifter	
Back Ground Gas	50-95	Shale CEC, ppb		LOSSES bbls		Run Casing		D-Gasser	
Connection Gas	300-425	D / B Ratio		Mud Lost	6	Testing			
Gas Cut Mud	17.7	High Gravity %	36.8	Mud Dumped		Cementing			
Bottom Hole Temp	310	High Gravity, ppb	540.4	Mud Transfer		Coring / Reaming			
METER READINGS		Avg. SG	4.089	TOTAL bbls					
600	134	300	6	Gain / Loss	16				
300	75	100	3						

ENGINEER	ENGINEER LOCATION	HOME PHONE	MOBILE PHONE	PAGER	WAREHOUSE LOCATION	WHSE PHONE
Joe Barnes	Corpus Christi	361-992-6470	361-442-3734	361-442-3734	Beeville	361-358-0181

The recommendations made herein shall not be construed as authorizing the infringement of any valid patent, and are made without assumption of liability by either the software manufacturer or its author, THE MUD COMPANY or its agents, and are statements of opinion only. Oral or written statements are advisory only and may be rejected by the user.



M-I Drilling Fluids

P.O. Box 42842
HOUSTON, TEXAS USA

OIL MUD REPORT

REPORT NUMBER: 89

361-886-3400

WELL NUMBER	State TX	County	Well C3887	S/T
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Date 7/22/2001	Depth 15440 ft.
Spud Date 4/26/2001	Present Activity (TVD 15310) Drlg

OPERATOR Louis Dreyfus		CONTRACTOR Helmerich & Payne		RIG NUMBER 89
OPERATOR REPRESENTATIVE Royce Coats		CONTRACTOR REPRESENTATIVE Date Molar		SECTION-TOWNSHIP-RANGE
WELL NAME AND NUMBER John Hancock Sr. A -1		FIELD OR BLOCK NUMBER NE Speaks	COUNTY, PARISH, OFFSHORE AREA Lavaca	STATE / PROV Texas

BIT DATA		DRILLING ASSEMBLY				MUD VOLUME		CIRCULATION DATA			
No	Size 8.75 in	Drill Pipe OD 5	ID 4.276	Length 7878	Hole 900	Pits 676	Pump 1 Make/Model	Gerner Denver PZ - 11			
Type	SEC. PDC	Drill Pipe OD 4	ID 3.34	Length 7075	Total Circulating Volume 1576		Size 6 x 11	% Eff 95	bb/stk 0.0914	gal/min 238	
		Drill Collar OD 4	ID 2.56	Length 185			Pump 2 Make/Model	Gerner Denver PZ - 11			
		Drill Collar OD 4.75	ID 2.25	Length 302			Size 6 x 11	% Eff 95	bb/stk 0.0914	gal/min 238	

CASING DATA				MUD TYPE		MUD PROPERTY SPECIFICATIONS			
Size 13.375	Top @ 0	Set @ 2066	In Storage 395	Weight 18	ppg 18	Viscosity 60-70	sec/qt	Filtrate < 4cc	HTHP cc

DEVIATION				MUD TYPE		MUD PROPERTY SPECIFICATIONS			
Size 9.625	Top @ 0	Set @ 10751	In Storage 500	Weight 18	ppg 18	Circulating Pressure 3,550	psi		

MUD PROPERTIES				MUD TYPE		MUD PROPERTY SPECIFICATIONS			
Sample From	PIT	Weight 17.9	ppg 17.9	Viscosity 60-70	sec/qt	Filtrate < 4cc	HTHP cc		
Time Sample Taken	3:00 am			RECOMMENDED TREATMENT					
Flowline Temperature (deg F)	175			Oil Added: 12 bbls					
Depth (ft)	15440			Water Added: 2 bbls					
Mud Weight (ppg)	17.9			Products Added: 3 bbls					
Funnel Viscosity @ 182 deg F (sec/qt)	68			Mud Built: 17 bbls					
Plastic Viscosity @ 160 deg F (cP)	55			Mud Received: 0 bbls					
Yield Point (lbs/100 sq ft)	13			Mud Returned: 0 bbls					
Gel Strength (10 sec/10 min) (lbs/100 sq ft)	5 / 16 / 25			Starting Volume: 2472 bbls					
API Filtrate (ml/30 min)	3			Present Volume: 2476 bbls					
HTHP Filtrate @ 400 deg F (ml/30 min)	3			Mud Loss / 24 hrs: 14 bbls					
Cake Thickness (API / HTHP) (32nd in)	1 / 3			Cumm. Mud Loss: 3466 bbls					
Solids Content (% by vol)	41			Oilbase Mud Cuttings					
Oil / Water Content (% by vol)	53 / 6			Daily Haul Off: 16 cu yds		Cumm. Haul Off: 352 cu yds			
Solids Adjusted For Salt (% by vol)	40.5								
Alkalinity Mud (Ppm)	2.2								
Lime Content (lb/bbl)	2.86								
Salt Content Water Phase (% by Wt)	23.84								
Oil / Water Ratio	90 / 10								
Chlorides Whole Mud (mg/L)	12000								
Electrical Stability (volts)	1500								
Salt Content (PPM)	238385								
New Hole (bbls)	6								
LCM (lb/bbl)									

REMARKS									
Drilling 7 to 10/hr									

PRODUCT INVENTORY										
DATE	MI BULK BAR	MUD DIESEL	ENGR SERVICE	DUKLINE/KENOL						
7/22/2001										
DAILY MUD COST	\$1,796.46									
CUMULATIVE COST	\$66,013.59									
Starting Inventory	1,716	4,676		340						
Products Received										
Products Returned										
Used Last 24 Hours	50	511	1	5						
Closing Inventory	1,666	4,165		335						
Cost Last 24 Hours	\$362.00	\$454.79	\$650.00	\$224.00						
Used (from ADC)										

BIT RHEOLOGY and HYDRAULICS		SOLIDS ANALYSIS		MUD CONSUMPTION		TIME DISTRIBUTION		FOUR SOLIDS CONTROL EQUIPMENT		
Mud Gradient, psf/ft	0.9308	Low Gravity %	4.9	ADDITIONS bbls	12	RIG OPERATION Hrs	24.00	DEVICE / MAKE	SPE #	Wt
Hydrostatic Pressure, psi	14,372	Low Gravity, ppb	44.2	Oil / ABO	2	Drilling		Derrick Shaker	3 x 14's	0
ECD, ppg	18.37	Bentonite %		Fresh Water	2	Circulating		Derrick Shaker	3 x 175	24
Bit weight (WOB), lbs	7	Bentonite, ppb		Mud Built	3	Tripping		Derrick Shaker	3 x 175	24
Bit RPM, rpm	110	Drill Solids %		Mud Transfer		Surveys		D-Sander		0
Back Ground Gas	130-800	Shale CEC, ppb				Logging		D-Sitter		0
Connection Gas	25-55	D / B Ratio		LOSSES bbls	14	Run Casing		D-Gasser		24
Bottom Hole Temp	300	High Gravity %	35.7	Mud Lost		Testing				
Water Meter	42739	High Gravity, ppb	524.3	Mud Dumped		Cementing				
METER READINGS		Avg. SG	4.008	Mud Transfer		Coring / Reaming				
600	123	200	6	TOTAL bbls						
300	68	100	3	Gain / Loss	3					
ENGINEER	ENGINEER LOCATION	HOME PHONE	MOBILE PHONE	PAGER	WAREHOUSE LOCATION	WHSE PHONE				
Ina Ramez	Cornie Christl	361-002-8470	361-442-3734	361-442-3734	Requillo	361-358-0184				



M-I Drilling Fluids

P.O. Box 42842
HOUSTON, TEXAS USA

OIL MUD REPORT

REPORT NUMBER: 88

361-886-3400

WELL NUMBER	State TX	County	Well C3887	S/T
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Date 7/21/2001	Depth 15285 ft.
Spud Date 4/26/2001	Present Activity Drig 15' / hr

OPERATOR Louis Dreyfus		CONTRACTOR Helmerich & Payne		RIG NUMBER 89
OPERATOR REPRESENTATIVE Royce Coats		CONTRACTOR REPRESENTATIVE Dale Molar		SECTION-TOWNSHIP-RANGE
WELL NAME AND NUMBER John Hancock Sr. A -1		FIELD OR BLOCK NUMBER NE Speaks	COUNTY, PARISH, OFFSHORE AREA Lavaca	STATE / PROV Texas

BIT DATA		DRILLING ASSEMBLY			MUD VOLUME		CIRCULATION DATA				
No	Size	Drill Pipe OD	ID	Length	Hole	Pits	Pump 1 Make/Model	Size	% Eff	bb/atk	gal/min
	6.75 in	5	4.276	7723	894	688	Gamer Denver PZ - 11	6 x 11	95	0.0914	
Type	SEC. PDC	Drill Pipe OD	ID	Length	Total Circulating Volume		Pump 2 Make/Model	Size	% Eff	bb/atk	gal/min
		4	3.34	7075	1562		Gamer Denver PZ - 11	6 x 11	95	0.0914	
		Drill Collar OD	ID	Length	In Storage	Weight	Circulating Pressure	Ann.Val. DP	Ann.Val. DC	Bottoms Up Time	Total Circ. Time
		4	2.56	185	396	18 ppg	3,470 psi	194 ft/min	249 ft/min	121 min	280 min
		4.75	2.25	302	500	18 ppg	Bottoms Up Stks	7,407	Total Circ. Stks	17,090	

MUD PROPERTIES			MUD PROPERTY SPECIFICATIONS					
Sample From	PIT		Weight	17.9 ppg	Viscosity	60-70 sec/qt	Filtrate	< 4cc HTHP cc
Time Sample Taken	3:30 am		RECOMMENDED TREATMENT					
Flowline Temperature (deg F)	172		Oil Added:	21 bbls				
Depth (ft)	15285		Water Added:	12 bbls				
Mud Weight (ppg)	17.9		Products Added:	1 bbls				
Funnel Viscosity @ 158 deg F (sec/qt)	70		Mud Built:	34 bbls				
Plastic Viscosity @ 160 deg F (cP)	60		Mud Received:	0 bbls				
Yield Point (lbs/100 sq ft)	15		Mud Returned:	0 bbls				
Gel Strength (10 sec/10 min) (lbs/100 sq ft)	6 / 18		Starting Volume:	2454 bbls				
API Filtrate (ml/30 min)	2.6		Present Volume :-	2472 bbls				
HTHP Filtrate @ 400 deg F (ml/30 min)	/ 3		Mud Loss / 24 hrs:--	12 bbls				
Cake Thickness (API / HTHP) (32nd in)	/ 3		Cumm. Mud Loss:--	3452 bbls				
Solids Content (% by vol)	40.5		Oilbase Mud Cuttings					
Oil / Water Content (% by vol)	54 / 5.5		Daily Haul Off: 0 cu yds	Cumm. Haul Off: 336 cu yds				
Solids Adjusted For Salt (% by vol)	40		REMARKS					
Alkalinity Mud (Pom)	2.5		THH, Drilling, B/up thru seperator 330 max gas w/ 17.8 GCM, Back to shakers had 930 Max Gas w/ 17.7 GC Mud, Rolled Reserve tanks, Drilling at 10 to 20' / hr					
Lime Content (lb/bbl)	3.12							
Salt Content Water Phase (% by Wt)	28.49							
Oil / Water Ratio	91 / 9							
Chlorides Whole Mud (mg/L)	14000							
Electrical Stability (volts)	1530							
Salt Content (PPM)	284,878							
New Hole (bbls)	4							
LCM (lb/bbl)								

PRODUCT INVENTORY							
DATE	VERSATROL	A CHLORIDE (PM)	CLEAN UP	MUD DIESEL	ENGR. SERVICE	DUCKLIN/ENOX	
7/21/2001							
DAILY MUD COST							\$2,679.38
CUMULATIVE COST							\$64,217.13
Starting Inventory	180	80	53	5,576		345	
Products Received							
Products Returned							
Used Last 24 Hours	3	10	3	900	1	5	
Closing Inventory	177	70	50	4,676		340	
Cost Last 24 Hours	\$211.77	\$434.60	\$200.40	\$801.00	\$650.00	\$224.00	
Used (from IADC)							

BIT RHEOLOGY and HYDRAULICS		SOLIDS ANALYSIS		MUD CONSUMPTION		TIME DISTRIBUTION		TOUR SOLIDS CONTROL EQUIPMENT	
Mud Gradient, psi/ft	0.9308	Low Gravity %	3.7	ADDITIONS	bbls	RIG OPERATION	hrs	DEVICE / MAKE	SIZE w/ SCREENS
Hydrostatic Pressure, psi	14,227	Bentonite %	33.5	Oil / ABO	21	Rig Up / Service	0.50	Derrick Shaker	3 x 14s 0
ECD, ppg	18.45	Drill Solids %		Fresh Water	7	Drilling	16.50	Derrick Shaker	3 x 175 24
Bit weight (WOB), lbs	7	Drill Solids, ppb		Brine Water		Circulating		Derrick Shaker	3 x 175 24
Bit RPM, rpm		Shale CEC, ppb		Mud Built	1	Tripping	5.00	Derrick Shaker	3 x 175 24
Back Ground Gas	45	D / B Ratio		Mud Transfer		Surveys		D-Sander	0
Connection Gas	160	High Gravity %	38.2	Mud Lost	12	Logging		D-Sifter	0
Bottom Hole Temp	295-305	High Gravity, ppb	532.7	Mud Dumped		Run Casing		D-Gasser	24
Water Meter	42470	Avg. SG	4.053	Mud Transfer		Testing	2.00		
METER READINGS				TOTAL					
800	135	200	6	Gain / Loss		17			
300	75	100	3						
ENGINEER	ENGINEER LOCATION		HOME PHONE	MOBILE PHONE	PAGER	WAREHOUSE LOCATION		WHISE PHONE	
Joe Barnes	Corpus Christi		361-992-6470	361-442-3734	361-442-3734	Beeville		361-358-0181	

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Drilling Fluids

OIL-BASED MUD REPORT No.84

Date	07/18/2001	Depth/TVD	14950 ft / 14928 ft
Spud Date	04/26/2001	Mud Type	Versadril
Water Depth		Activity	Drilling

Operator : Louis Dreyfus
 Report For : Royce Coats
 Well Name : John Hancock Sr. A-1
 Contractor : Helmerich & Payne #89
 Report For : Rick Hawthorne

Field/Area : NE. Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3887

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Sec. FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	13.375in @2986ft (2986TVD)	881.4	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	7388 ft	9.625in @10751ft (10751TVD)	617.6	Pump stk/min		61@95%
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	234 gal/min	
4 in	7075 ft	7.625in @14072ft (14072TVD)	1499	Bottoms Up	120.4 min	7343 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	269.1 min	16412 stk
4.75 in	302 ft		895	Circulating Pressure	3400 psi	

MUD PROPERTIES			
Sample From		PIT@03:30	
Flow Line Temp	°F	173	
Depth/TVD	ft	14950/14928	
Mud Weight	lb/gal	17.9@162°F	
Funnel Viscosity	s/qt	64	
Rheology Temp	°F	160	
R600/R300		142/79	
R200/R100			
R6/R3		-/3	
PV	cP	63	
YP	lb/100ft²	16	
10s/10m/30m Gel	lb/100ft²	3/22/27	
API Fluid Loss	cc/30 min	NA	
HTHP FL Temp	cc/30 min	2.8@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	40	
Correct Solids	%Vol	39.44	
Oil	%Vol	54	
Uncorr Water	%Vol	6	
Oil/Water Ratio		90/10	
Alkal (Pom)		3.8	
Cl Whole Mud	mg/l	14000	
Salt	%Wt	26.75	267500
Lime	lb/bbl	4.94	
E-Stability		1360	
Received Volume	bbl	2907	
Returned Volume	bbl	377	
Present Volume	bbl	2394	
Diff. Volume	bbl	-136	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amnt
VERSACOAT	1 GA BK	30
VERSATROL	50 LB BG	10
MUD DIESEL	1 GA BK	980
ENGINEERING SERVICE	1 EA	1
175 PMD PYRAMID SCREBI	1 EA	2
VERSAMUL	55 GA DM	1

SOLIDS EQUIP	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	24
Derrick Shaker	175/175/175	24
D-Sander	212	0
D-Sifter	8T4	0

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

23 bbls Oil Added
 15 bbls Water Added
 3 bbls Products Added
 41 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2380 bbls Starting Volume
 2394 bbls Present Volume
 -27 bbls Mud Loss /24 hrs
 -3394 bbls Cumulative Mud Loss 6 bbls New Hole Volume

REMARKS

Drilled to 14950 ft. Last survey at 14909 was 25.7 deg. Bottom hole temperature 286 deg. F. Short tripped with no problems. No increase in Chlorides at bottoms up. BKGRN gas = 15 - 50 units. Trip gas = 50. Last connection gas = 60 units.

Oil Base Mud Cuttings
 00 cu yds Daily Haul Off
 304 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS	MUD RHEOLOGY & HYDRAULICS
Rig Up/Service	0.5	Oil Added	Salt Wt%	np/na Values
Drilling	22.5	Water Added	Salt Conc./lb/bbl	0.846/0.846
Tripping	1	Mud Received	Adjusted Solid %	kp/ka (lb*s^n/100ft²)
Circulating		Dumped	Oil/Water Ratio	Bit Loss (psi / %)
Chng Swvl Pkng		Shakers	Average SG Solids	462 / 13.6
P/U Rot. Head		Evaporation	Low Gr %	Bit HHP (hhp / HSI)
Slip Drill Line		Formation	High Gr %	Bit Jet Vel (ft/s)
Dir Survey		Left in Hole	High Gr Wt lb/bbl	Annular Vel DP (ft/min)
Testing		Trip Loss	Other	Annular Vel DC (ft/min)
Fishing		Other		Crit Vel DP (ft/min)
				Crit Vel DC (ft/min)
				ECD @ 14950 (lb/gal)

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Corky Karober Cell Phone	361 985-7424 830 708-5715	361 798-7111	361 358-0181	\$ 5,378.77 \$ 760,544.33



OIL-BASED MUD REPORT No.78

Date	7/12/2001	Depth/TVD	14202 ft / 14202 ft
Spud Date	4/26/2001	Mud Type	Versadril
Water Depth		Activity	Time Drilling

Operator : Louis Dreyfus
 Report For : Dan Patton
 Well Name : John Hancock Sr. A-1
 Contractor : Helmerich & Payne #89
 Report For : Rick Hawthorne

Field/Area : NE. Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3887

DRILLING ASSEMBLY		CASING		MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Dowco Diamond	Surface		Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	1/32"	13.375in @2986ft (2986TVD)		854.2	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate		Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	6732 ft	9.625in @10751ft (10751TVD)		570.8	Pump stk/min		61@95%
Drill Pipe Size	Length	Intermediate		Total Circulating Vol	Flow Rate	234 gal/min	
4 in	7075 ft	7.625in @14072ft (14072TVD)		1425	Bottoms Up	117.7 min	7177 stk
Drill Collar Size	Length	Production or Liner		In Storage	Total Circ Time	255.8 min	15602 stk
4.75 in	210 ft			895	Circulating Pressure	3200 psi	

MUD PROPERTIES			
Sample From		PIT@03:00	
Flow Line Temp	°F	172	
Depth/TVD	ft	14202/14202	
Mud Weight	lb/gal	17.9+@161°F	
Funnel Viscosity	s/qt	66	
Rheology Temp	°F	160	
R600/R300		108/60	
R200/R100		-/-	
R6/R3		-/3	
PV	cP	48	
YP	lb/100ft²	12	
I0s/10m/30m Gel	lb/100ft²	4/18/24	
API Fluid Loss	cc/30 min	N/A	
HTHP FL Temp	cc/30 min	2.0@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	40.0	
Correct Solids	%Vol	39.4	
Oil	%Vol	54.0	
Uncorr Water	%Vol	6.0	
Oil/Water Ratio		90/10	
Alkal (Pom)		4.6	
Cl Whole Mud	mg/l	15000	
Salt	%Wt	28.12	281200
Lime	lb/bbl	5.98	
E-Stability		1160	
Received Volume	bbl	2907	
Returned Volume	bbl	377	
Present Volume	bbl	2320	
Diff. Volume	bbl	-210	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	50
VERSACOAT	1 GA BK	15
OIL DRI ABSORBANT	50 LB BG	6
CLEAN-UP	5 GA CN	5
MUD DIESEL	1 GA BK	835
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KENOX)	50 LB BG	65
SWA (MAGCO)	55 GA DM	1

SOLIDS EQUIP		
	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	23
Derrick Shaker	175/175/175	23
D-Sander	212	0
D-Sifter	8T4	0

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

20 bbls Oil Added
 15 bbls Water Added
 9 bbls Products Added
 44 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2303 bbls Starting Volume
 2320 bbls Present Volume
 -27 bbls Mud Loss /24 hrs
 -3286 bbls Cumulative Mud Loss 1.5 bbls New Hole Volume

REMARKS

Building angle in 100% shale.

Oil Base Mud Cuttings
 0 cu yds Daily Haul Off
 272 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service	0.5	Oil Added	0	Salt Wt%	28.12	np/na Values
Drilling	22.0	Water Added	15	Salt Conc,lb/bbl	8.22	kp/ka (lb*s/n/100ft²)
Tripping		Mud Received	0	Adjusted Solid %	39.39	Bit Loss (psi / %)
Circulating	0.5	Dumped	0	Oil/Water Ratio	90/10	Bit HHP (hhp / HSI)
Chng Swvl Pkng	1.0	Shakers	18	Average SG Solids	4.1	Bit Jet Vel (ft/s)
P/U Rot. Head		Evaporation	10	Low Gr %	2.3	Annular Vel DP (ft/min)
Slip Drill Line		Formation	0	Low Gr Wt, lb/bbl	20.83	Annular Vel DC (ft/min)
Dir Survey		Left in Hole	0	High Gr %	37.1	Crit Vel DP (ft/min)
Testing		Trip Loss	0	High Gr Wt lb/bbl	545.17	Crit Vel DC (ft/min)
Fishing		Other	0			ECD @ 14202 (lb/gal)
						18.21

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Mark Watson 361 358-4781 Cell Phone 361 362-5940	361 798-7111	361 358-0181	\$ 8,171.87	\$ 727,774.27



Drilling Fluids

OIL-BASED MUD REPORT No.36

Date		Depth/TVD	
Spud Date		Mud Type	
Water Depth		Activity	

Operator : Louis Dreyfus
 Report For : Royce Coats
 Well Name : J. Hancock Sr A-1 ST
 Contractor : Helmerich & Payne #89
 Report For : Dale Moler

Field/Area : NE Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3957

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Security FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	987.9	Pump Size	6 X 11 in	6 X 11 in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	10210 ft	7.625in @14072ft (14072TVD)	650.1	Pump stk/min	25@95%	
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	96 gal/min	
4 in	7075 ft		1638	Bottoms Up	318.1 min	7954 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	716.6 min	17916 stk
4.75 in	307 ft		880	Circulating Pressure	970 psi	

MUD PROPERTIES			
Sample From		PIT@24:00	
Flow Line Temp	°F	153	
Depth/TVD	ft	17777/16904	
Mud Weight	lb/gal	19.0@144°F	
Funnel Viscosity	s/qt	97	
Rheology Temp	°F	160	
R600/R300		148/79	
R200/R100		-/-	
R6/R3		-/3	
PV	cP	69	
YP	lb/100ft²	10	
10s/10m/30m Gel	lb/100ft²	3/13/20	
API Fluid Loss	cc/30 min	NA	
HTHP FL Temp	cc/30 min	2.6@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	43	
Correct Solids	%Vol	42.6	
Oil	%Vol	52	
Uncorr Water	%Vol	5	
Oil/Water Ratio		91/9	
Alkal (Pom)		0.8	
Cl Whole Mud	mg/l	10500	
Salt	%Wt	24.73	247300
Lime	lb/bbl	1.04	
E-Stability		960	
Received Volume	bbl	2747	
Returned Volume	bbl	478	
Present Volume	bbl	2518	
Diff. Volume	bbl	+249	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	500
ASPHASOL SUPREME	50 LB BG	15
VERSACOAT	1 OA BK	10
VERSATROL	50 LB BG	17
OIL DRI ABSORBANT	50 LB BG	12
CLEAN-UP	5 GA CN	10
MUD DIESEL	1 OA BK	1128
SAFE-CARB FINE	50 LB BG	18
SAFE-CARB MEDIUM	50 LB BG	36
SAFE-CARB COARSE	50 LB BG	60
MIX II FINE	25 LB BG	15
MIX II MED	25 LB BG	25
MIX II COARSE	25 LB BG	41
G-SEAL	50 LB BG	34
ENGINEERING SERVICE	1 EA	1

SOLIDS EQUIP		
	Size	Hrs
Derrick Shaker	14/14/14	24
Derrick Shaker	175/175/175	0
Derrick Shaker	175/175/175	0

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

27 bbls Oil Added
 4 bbls Water Added
 50 bbls Products Added
 81 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2473 bbls Starting Volume
 2518 bbls Present Volume
 -36 bbls Mud Loss /24 hrs
 1170 bbls Cumulative Mud Loss 0 bbls New Hole Volume

REMARKS

Circulating well monitoring gas and losses. Gradually increasing and maintaining 18.9/19.0 ppg. B/up #1. 3/4% inc. in retort water, Cl = 177K. #2. 1 % inc. in retort water, Cl = 238K
 Built 120 bbl of lcm (31 PPB) for sweeps and volume. Mud sample is screened before testing due to lcm. LCM concentration in active is 22.2 ppb. ECD with present rheology and 35 stks is 19.3 ppg / 25 stks, see below (19.22).
 Oil Base Mud Cuttings
 16 cu yds Daily Haul Off
 224 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS	MUD RHEOLOGY & HYDRAULICS
Rig Up/Service		Oil Added 0	Salt Wt% 24.73	np/na Values 0.906/0.906
Drilling		Water Added 4	Salt Conc, lb/bbl 5.75	kp/ka (lb-s^n/100ft²) 0.297/0.297
Tripping		Mud Received 0	Adjusted Solid % 42.59	Bit Loss (psi / %) 83 / 8.5
Circulating		Shakers 0	Oil/Water Ratio 91/9	Bit HHP (hhp / HSI) 5 / .1
Shp & Cut		Evaporation 7	Average SG Solids 4.1	Bit Jet Vel (ft/s) 70
Chng Rot. Head		Formation 29	Low Gr % 1.4	Annular Vel DP (ft/min) 79.59
Rig Repair		Left in Hole 0	Low Gr Wt, lb/bbl 13.07	Annular Vel DC (ft/min) 102.3
Wireline Logs		Trip Loss 0	High Gr % 41.2	Crit Vel DP (ft/min) 244
Testing		Other 0	High Gr Wt lb/bbl 604.67	Crit Vel DC (ft/min) 318
Direction Work		Dumped 0		ECD @ 17777 (lb/gal) 19.22

Corky Karocher 361 985-7424
 Cell Phone 830 708-5715 361 798-7111 361 358-0181 \$ 25,550.90 \$ 230,321.08



OIL-BASED MUD REPORT No.31

Date	8/8/2001	Depth/TVD	17415 ft / 16662 ft
Spud Date	7/9/2001	Mud Type	Versadril
Water Depth		Activity	Drilling

Operator : Louis Dreyfus
Report For : Royce Coats
Well Name : J. Hancock Sr A-1 ST
Contractor : Helmerich & Payne #89
Report For : Dale Moler
Field/Area : NE Speaks
Description : A-532
Location : Lavaca County, Texas
Well No. : C3957

DRILLING ASSEMBLY		CASING		MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Security FM2831	Surface	9.625in @10751ft (10751TVD)	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	Intermediate	7.625in @14072ft (14072TVD)	974.2	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate		Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	9848 ft	Production or Liner		575.8	Pump stk/min		60@95%
Drill Pipe Size	Length			Total Circulating Vol	Flow Rate	230 gal/min	
4 in	7075 ft			1550	Bottoms Up	131.5 min	7888 stk
Drill Collar Size	Length			In Storage	Total Circ Time	283 min	16983 stk
4.75 in	307 ft			990	Circulating Pressure	3150 psi	

MUD PROPERTIES			
Sample From		PIT@03:00	
Flow Line Temp	°F	159	
Depth/TVD	ft	17415/16662	
Mud Weight	lb/gal	18.5+@149°F	
Funnel Viscosity	s/qt	70	
Rheology Temp	°F	160	
R600/R300		111/60	
R200/R100		-/-	
R6/R3		-/2	
PV	cP	51	
YP	lb/100ft²	9	
10s/10m/30m Gel	lb/100ft²	3/12/17	
API Fluid Loss	cc/30 min	N/A	
HTHP FL Temp	cc/30 min	2.4@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	42.0	
Correct Solids	%Vol	41.5	
Oil	%Vol	52.0	
Uncorr Water	%Vol	6.0	
Oil/Water Ratio		90/10	
Alkal (Pom)		2.5	
Cl Whole Mud	mg/l	12500	
Salt	%Wt	24.59	245900
Lime	lb/bbl	3.25	
E-Stability		1205	
Received Volume	bbl	2747	
Returned Volume	bbl	478	
Present Volume	bbl	2540	
Diff. Volume	bbl	+271	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	250
CLEAN-UP	5 GA CN	12
MUD DIESEL	1 GA BK	780
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KENOX)	50 LB BG	64

SOLIDS EQUIP	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	24
Derrick Shaker	175/175/175	24

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT
 19 bbls Oil Added
 8 bbls Water Added
 22 bbls Products Added
 49 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2521 bbls Starting Volume
 2540 bbls Present Volume
 -30 bbls Mud Loss /24 hrs
 -784 bbls Cumulative Mud Loss 9 bbls New Hole Volume

REMARKS
 MWD & LWD quit working. Continue drilling. Bottoms up from break @ 17,323'-17,337' had 120 gas units. Circulate connection @ 17,393'; 2,250 gas units and 18.1 #/gal mud cut down flowline then 450 units after mud/gas separator with 6' flare.

 Oil Base Mud Cuttings
 0 cu yds Daily Haul Off
 176 cu yds Cumulative Haul Off

TIME OISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS	MUD RHEOLOGY & HYDRAULICS			
Rig Up/Service	0.5	Oil Added	0	Salt Wt%	24.59	np/na Values	0.888/0.888
Drilling	20.5	Water Added	8	Salt Conc./lb/bbl	6.85	kp/ka (lb-s ² /m/100ft ²)	0.253/0.253
Tripping		Mud Received	0	Adjusted Solid %	41.51	Bit Loss (psi / %)	462 / 14.7
Circulating	3.0	Dumped	0	Oil/Water Ratio	90/10	Bit HHP (hhp / HSI)	62 / 1.7
P/U Trip Nipple		Shakers	14	Average SG Solids	4.1	Bit Jet Vel (ft/s)	167
P/U Rot. Head		Evaporation	8	Low Gr %	2.1	Annular Vel DP (ft/min)	190.69
Running Casing		Formation	0	Low Gr Wt, lb/bbl	18.68	Annular Vel DC (ft/min)	245.1
Wireline Logs		Left in Hole	0	High Gr %	39.5	Crit Vel DP (ft/min)	201
Testing		Trip Loss	0	High Gr Wt lb/bbl	579.76	Crit Vel DC (ft/min)	259
Direction Work		Other	8			ECD @ 17415 (lb/gal)	18.88

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Mark Watson 361 358-4781 Cell Phone 361 362-5940	361 798-7111	361 358-0181	\$ 7,236.16	\$ 143,444.55

**OIL-BASED MUD REPORT No.29**

Date	8/6/2001	Depth/TVD	17170 ft / 16499 ft
Spud Date	7/9/2001	Mud Type	Versadril
Water Depth		Activity	Slug for Trip

Operator : Louis Dreyfus
 Report For : Dan Patton
 Well Name : J. Hancock Sr A-1 ST
 Contractor : Helmerich & Payne #89
 Report For : Dale Moler

Field/Area : NE Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3957

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Security FM2831	Surface	Hole	Pump Make	G.D. FZ-11	G.D. FZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	965	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	9602 ft	7.625in @14072ft (14072TVD)	565	Pump stk/min		58@95%
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	223 gal/min	
4 in	7075 ft		1530	Bottoms Up	134.7 min	7811 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	288.2 min	16713 stk
4.75 in	308 ft		990	Circulating Pressure	3450 psi	

MUD PROPERTIES			
Sample From		PIT@18:30	
Flow Line Temp	°F	161	
Depth/TVD	ft	17170/16499	
Mud Weight	lb/gal	18.5@152°F	
Funnel Viscosity	s/qt	64	
Rheology Temp	°F	160	
R600/R300		110/60	
R200/R100		-/-	
R6/R3		-/2	
PV	cP	50	
YP	lb/100ft ²	10	
10s/10m/30m Gel	lb/100ft ²	3/10/16	
API Fluid Loss	cc/30 min	N/A	
HTHP FL Temp	cc/30 min	2.0@400°F	
Cake API/HTHP	1/32"	-/3	
Unc Ret Solids	%Vol	42.0	
Correct Solids	%Vol	41.5	
Oil	%Vol	52.5	
Uncorr Water	%Vol	5.5	
Oil/Water Ratio		91/9	
Alkal (Pom)		1.6	
Cl Whole Mud	mg/l	12500	
Salt	%Wt	26.24	262400
Lime	lb/bbl	2.08	
E-Stability		1050	
Received Volume	bbl	2747	
Returned Volume	bbl	478	
Present Volume	bbl	2520	
Diff. Volume	bbl	+251	

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	152
VERSACOAT	1 GA BK	5
OIL DRI ABSORBANT	50 LB BG	4
CLEAN-UP	5 GA CN	1
MUD DIESEL	1 GA BK	1130
TRUCKING SERVICE	1 EA	902
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KENOX)	50 LB BG	25

SOLIDS EQUIP	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	14.5
Derrick Shaker	175/175/175	14.5

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

27 bbls Oil Added
 13 bbls Water Added
 12 bbls Products Added
 52 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2488 bbls Starting Volume
 2520 bbls Present Volume
 -20 bbls Mud Loss /24 hrs
 -739 bbls Cumulative Mud Loss 5 bbls New Hole Volume

REMARKS

MWD quit working. Pumped 2 / 5 bbl diesel sweeps but tool wouldn't work. Drill to 17,170 then slug with 70 bbl 21.25 #/gal slug and TOH to change out MWD tool. Maximum connection gas was 800 units with 18.0 #/gal mud cut, maximum down time gas was 700 units with 18.1 #/gal mud cut, and average background gas of 60 units.

Oil Base Mud Cuttings
 16 cu yds Daily Haul Off
 160 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service	0.5	Oil Added	0	Salt Wt%	26.24	np/na Values
Drilling	14.5	Water Added	13	Salt Conc, lb/bbl	6.85	kp/ka (lb-s ⁿ /100ft ²)
Tripping		Mud Received	0	Adjusted Solid %	41.5	Bit Loss (psi / %)
Circulating		Dumped	0	Oil/Water Ratio	91/9	Bit HHP (hhp / HSI)
P/U Trip Nipple		Shakers	13	Average SG Solids	4.1	Bit Jet Vel (ft/s)
P/U Rot. Head		Evaporation	7	Low Gr %	2.4	Annular Vel DP (ft/min)
Pump Repair	0.5	Formation	0	Low Gr Wt, lb/bbl	21.45	Annular Vel DC (ft/min)
Direction Work		Left in Hole	0	High Gr %	39.1	Crit Vel DP (ft/min)
Testing		Trip Loss	0	High Gr Wt lb/bbl	575.17	Crit Vel DC (ft/min)
Wireline Logs		Other	0			ECD @ 17170 (lb/gal)
						18.87

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Mark Watson 361 358-4781 Cell Phone 361 362-5940	361 798-7111	361 358-0181	\$ 5,671.88	\$ 134,818.51



OIL-BASED MUD REPORT No.28

Date	8/5/2001	Depth/TVD	17053 ft / 16420 ft
Spud Date	7/9/2001	Mud Type	Versadrill
Water Depth		Activity	Drilling

Operator : Louis Dreyfus
Report For : Dan Patton
Well Name : J. Hancock Sr A-1 ST
Contractor : Helmerich & Payne #89
Report For : Rick Hawthorne

Field/Area : NE Speaks
Description : A-532
Location : Lavaca County, Texas
Well No. : C3957

DRILLING ASSEMBLY		CASING	MUD VOLUME (bb)	CIRCULATION DATA		
Bit Size	6.75 in Security FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	960.6	Pump Size	6 X 11 in	6 X 11 in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837gal/stk
5 in	9485 ft	7.625in @14072ft (14072TVD)	537.4	Pump stk/min		55@95%
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	211 gal/min	
4 in	7075 ft		1498	Bottoms Up	141.9 min	7803 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	298.2 min	16400 stk
4.75 in	308 ft		990	Circulating Pressure	3100 psi	

MUD PROPERTIES				PRODUCTS USED LAST 24 HRS		
Sample From		PTT@03:00	FL@15:30	Products	Size	Amt
Flow Line Temp	°F	161	165	M-I BAR BULK	100 LB BG	350
Depth/TVD	ft	17053/16420	16930/	CLEAN-UP	5 GA CN	2
Mud Weight	lb/gal	18.5 @152°F	18.4@165°F	MUD DIESEL	1 GA BK	295
Funnel Viscosity	s/qt	63	B/U From	ENGINEERING SERV	1 EA	1
Rheology Temp	°F	160	Break	QUICKLIME (KFN0X)	50 LB BG	15
R600/R300		103/55				
R200/R100		-/-				
R6/R3		-/2				
PV	cP	48				
YP	lb/100ft²	7				
10s/10m/30m Gel	lb/100ft²	3/10/15				
API Fluid Loss	cc/30 min	N/A				
HTHP FL Temp	cc/30 min	1.6@400°F				
Cake API/HTHP	1/32"	-/3				
Unc Ret Solids	%Vol	42.0	41.0			
Correct Solids	%Vol	41.5	40.47			
Oil	%Vol	53.0	54.0	SOLIDS EQUIP	Size	Hr
Uncorr Water	%Vol	5.0	5.0	Derrick Shaker	14/14/14	1
Oil/Water Ratio		91/9	92/8	Derrick Shaker	175/175/175	26
Alkal (Pom)		1.1	0.8	Derrick Shaker	175/175/175	26
Cl Whole Mud	mg/l	12500	13000			
Salt	%Wt	28.12	28.92			
Lime	lb/bbl	1.43	1.04			
E-Stability		1100	710			
Received Volume	bb	2747				
Returned Volume	bb	478				
Present Volume	bb	2488				
Diff. Volume	bb	+219				

MUD PROPERTY SPECIFICATIONS			
Weight	Co. Orders		
Viscosity	50-60		
Filtrate	<4 cc HTHP		

REMARKS AND TREATMENT	REMARKS
7 bbls Oil Added 16 bbls Water Added 25 bbls Products Added 48 bbls Mud Built 239 bbls Mud Received 228 bbls Mud Returned 2505 bbls Starting Volume 2488 bbls Present Volume -76 bbls Mud Loss /24 hrs -719 bbls Cumulative Mud Loss 8 bbls New Hole Volume	Made short trip to liner @ 16,885'. Bottoms up had 300 gas units after mud/gas separator with a 20' flare. Swapped 500 bbls from system with 500 bbls new mud; ROP increased. Bottoms up from drilling break @ 16,925' had 150 gas units after mud/gas separator with no flare. Maximum connection gas was 700 units with 18.2 #/gal mud cut. Maximum down time gas was 575 units with 18.2 #/gal mud cut. Background gas @ 60 units. Last survey @ 16,949' was 48.3 degrees. Oil Base Mud Cuttings 32 cu yds Daily Haul Off 144 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bb)	SOLIDS ANALYSIS	MUD RHEOLOGY & HYDRAULICS
Rig Up/Service	0.5	Oil Added 0	Salt Wt% 28.12	np/na Values 0.905/0.905
Drilling	22.5	Water Added 16	Salt Conc,lb/bbl 6.85	kp/ka (lb*s^n/100ft²) 0.208/0.208
Tripping	2.0	Mud Received 11	Adjusted Solid % 41.49	Bit Loss (psi / %) 389 / 12.5
Circulating	4.0	Dumped 0	Oil/Water Ratio 91/9	Bit HHP (hhp / HSI) 48 / 1.3
P/U Trip Nipple	0.5	Shakers 20	Average SG Solids 4.1	Bit Jet Vel (ft/s) 153
P/U Rot. Head	0.5	Evaporation 16	Low Gr % 1.9	Annular Vel DP (ft/min) 174.93
Dir Survey		Formation 0	Low Gr Wt, lb/bbl 17.37	Annular Vel DC (ft/min) 224.85
Direction Work		Left in Hole 0	High Gr % 39.6	Crit Vel DP (ft/min) 180
Testing		Trip Loss 18	High Gr Wt lb/bbl 581.63	Crit Vel DC (ft/min) 234
Wireline Logs		Other 22		ECD @ 17053 (lb/gal) 18.8

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Mark Watson 361 358-4781	361 798-7111	361 358-0181	\$ 4,520.70	\$ 129,146.63
Cell Phone 361 362-5940				



OIL-BASED MUD REPORT No.27

Date	8/4/2001	Depth/TVD	16870 ft / 16296 ft
Spud Date	7/9/2001	Mud Type	Versadrill
Water Depth		Activity	Drilling

Operator : Louis Dreyfus **Field/Area :** NE Speaks
Report For : Dan Patton **Description :** A-532
Well Name : J. Hancock Sr A-1 ST **Location :** Lavaca County, Texas
Contractor : Helmerich & Payne #89 **Well No. :** C3957
Report For : Rick Hawthorne

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Security FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	953.7	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	9302 ft	7.625in @14072ft (14072TVD)	582.3	Pump stk/min	53@95%	
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	203 gal/min	
4 in	7075 ft		1536	Bottoms Up	146.7 min 7775 stk	
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	317.8 min 16843 stk	
4.75 in	308 ft		969	Circulating Pressure	3400 psi	

MUD PROPERTIES		
Sample From	PIT@03:00	
Flow Line Temp	°F	166
Depth/TVD	ft	16870/16298
Mud Weight	lb/gal	18.5@158°F
Funnel Viscosity	s/qt	108
Rheology Temp	°F	160
R600/R300		168/95
R200/R100		-/-
R6/R3		-/3
PV	cP	73
YP	lb/100ft²	22
10s/10m/30m Gel	lb/100ft²	5/20/29
API Fluid Loss	cc/30 min	N/A
HTHP FL Temp	cc/30 min	1.6@400°F
Cake API/HTHP	1/32"	-/3
Unc Ret Solids	%Vol	42.0
Correct Solids	%Vol	41.46
Oil	%Vol	53.5
Uncorr Water	%Vol	4.5
Oil/Water Ratio		92/8
Alkal (Pom)		2.7
CI Whole Mud	mg/l	13000
Salt	%Wt	31.13 311300
Lime	lb/bbl	3.51
E-Stability		1610
Received Volume	bbl	2508
Returned Volume	bbl	250
Present Volume	bbl	2505
Diff. Volume	bbl	+253

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
VERSACOAT	1 GA BK	10
VERSATROL	50 LB BG	7
CLEAN-UP	5 GA CN	3
MUD DIESEL	1 GA BK	440
SAFE-CARB FINE	50 LB BG	5
MIX II FINE	25 LB BG	5
G-SEAL	50 LB BG	5
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KENOX)	50 LB BG	5

SOLIDS EQUIP		
	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	17.5
Derrick Shaker	175/175/175	17.5

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

10 bbls Oil Added
 8 bbls Water Added
 2 bbls Products Added
 20 bbls Mud Built
 244 bbls Mud Received
 250 bbls Mud Returned
 2508 bbls Starting Volume
 2505 bbls Present Volume
 -17 bbls Mud Loss /24 hrs
 -643 bbls Cumulative Mud Loss 4 bbls New Hole Volume

REMARKS

Full day of drilling. Received 244 bbls new mud and returned 250 bbls mud from storage.

 Oil Base Mud Cuttings
 0 cu yds Daily Haul Off
 112 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service	0.5	Oil Added	0	Salt Wt%	31.13	np/na Values
Drilling	17.0	Water Added	8	Salt Conc,lb/bbl	7.12	kp/ka (lb*s^n/100ft²)
Tripping		Mud Received	-6	Adjusted Solid %	41.46	Bit Loss (psi / %)
Circulating		Dumped	0	Oil/Water Ratio	92/8	Bit HHP (hhp / HSI)
Reaming		Shakers	4	Average SG Solids	4.1	Bit Jet Vel (ft/s)
Chng. Rot. Head	0.5	Evaporation	8	Low Gr %	2.2	Annular Vel DP (ft/min)
Dir Survey		Formation	0	Low Gr Wt, lb/bbl	19.94	Annular Vel DC (ft/min)
Direction Work		Left in Hole	0	High Gr %	39.3	Crit Vel DP (ft/min)
Testing		Trip Loss	0	High Gr Wt lb/bbl	576.97	Crit Vel DC (ft/min)
Wireline Logs		Other	5			ECD @ 16870 (lb/gal)

M-I ENGR / PHONE		RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Mark Watson	361 358-4781				
Cell Phone	361 362-5940	361 798-7111	361 358-0181	\$ 3,412.28	\$ 124,625.70



Drilling Fluids

OIL-BASED MUD REPORT No.24

Date	08/01/2001	Depth/TVD	16719 ft / 16200 ft
Spud Date	07/09/2001	Mud Type	Versadril
Water Depth		Activity	Test BOPs

Operator : Louis Dreyfus
 Report For : Dan Patton
 Well Name : John Hancock Sr. A-1ST
 Contractor : Helmerick & Payne #89
 Report For : Rick Hawthorne

Field/Area : NE. Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3957

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Sec FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	1047.9	Pump Size	6 X 11 in	6 X 11 in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	gal/stk	gal/stk
5 in	ft	7.625in @14072ft (14072TVD)	523.1	Pump stk/min		
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	gal/min	
4 in	7075 ft		523.1	Bottoms Up		
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time		
4.75 in	309 ft		975	Circulating Pressure		

MUD PROPERTIES		
Sample From	PIT@24:00	
Flow Line Temp	°F	NA
Depth/TVD	ft	16719/16200
Mud Weight	lb/gal	18.6@120°F
Funnel Viscosity	s/qt	95
Rheology Temp	°F	162
R600/R300		169/96
R200/R100		-/-
R6/R3		-/3
PV	cP	73
YP	lb/100ft²	23
10s/10m/30m Gel	lb/100ft²	6/19/30
API Fluid Loss	cc/30 min	NA
HTHP FL Temp	cc/30 min	3.0@400°F
Cake API/HTHP	1/32"	-/3
Unc Ret Solids	%Vol	43
Correct Solids	%Vol	42.5
Oil	%Vol	52
Uncorr Water	%Vol	5
Oil/Water Ratio		91/9
Alkal (Pom)		2.5
Cl Whole Mud	mg/l	13000
Salt	%Wt	28.92
Lime	lb/bbl	3.25
E-Stability		1610
Received Volume	bbl	2264
Returned Volume	bbl	0
Present Volume	bbl	2546
Diff. Volume	bbl	+282

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	112
VERSACOAT	1 GA BK	5
VERSATROL	50 LB BG	2
CLEAN-UP	5 GA CN	7
MUD DIESEL	1 GA BK	221
SAFE-CARB FINE	50 LB BG	2
MIX II FINE	25 LB BG	2
G-SEAL	50 LB BG	2
TRUCKING SERVICE	1 EA	887
ENGINEERING SERVICE	1 EA	1
QUICKLIME (KENOX)	50 LB BG	5

SOLIDS EQUIP		
	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	0
Derrick Shaker	175/175/175	0

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

5 bbls Oil Added
 3 bbls Water Added
 9 bbls Products Added
 17 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2561 bbls Starting Volume
 2546 bbls Present Volume
 -32 bbls Mud Loss /24 hrs
 -571 bbls Cumulative Mud Loss * bbls New Hole Volume

REMARKS

Pump slug, POOH for new bit, BHA and test BOPs.

Oil Base Mud Cuttings
 00 cu yds Daily Haul Off
 112 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service		Oil Added	0	Salt Wt%	28.92	np/na Values
Drilling		Water Added	3	Salt Conc, lb/bbl	7.12	kp/ka (lb-s ² /n/100ft ²)
Tripping	7	Mud Received	0	Adjusted Solid %	42.47	Bit Loss (psi / %)
BOP Testing	17	Centrifuge	0	Oil/Water Ratio	91/9	Bit HHP (lhp / HSI)
Condition Hole		Formation	0	Average SG Solids	4.1	Bit Jet Vel (ft/s)
Circ. out Gas		Left in Hole	0	Low Gr %	3.3	Annular Vel DP (ft/min)
Slip and Cut		Other	21	Low Gr Wt, lb/bbl	29.97	Annular Vel DC (ft/min)
Condition Mud		Dumped	0	High Gr %	39.2	Crit Vel DP (ft/min)
Chg Swvl Pkng		Shakers	3	High Gr Wt lb/bbl	575.62	Crit Vel DC (ft/min)
		Evaporation	8			

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Conry Karoher Cell 361 985-7424 830 708-5715	361 798-7111	361 358-0181	\$ 4,493.28	\$ 117,112.64



Drilling Fluids

OIL-BASED MUD REPORT No.23

Table with 4 columns: Date, Spud Date, Water Depth, Depth/TVD, Mud Type, Activity. Values include 07/31/2001, 07/09/2001, 18200 ft, 18719 ft / 18200 ft, Versadri, Drilling.

Operator : Louis Dreyfus
Report For : Dan Patton
Well Name : John HancockSr.A-1ST
Contractor : Helmerick & Payne #89
Report For : Rick Hawthorne

Field/Area : NE. Speaks
Description : A-532
Location : Lavaca County, Texas
Well No. : C3957

Table with 4 main sections: DRILLING ASSEMBLY, CASING, MUD VOLUME (bbl), CIRCULATION DATA. Includes bit size, nozzle sizes, pipe lengths, hole depth, active pits, and circulation rates.

MUD PROPERTIES table with 2 columns: Property Name and Value. Includes Flow Line Temp, Depth/TVD, Mud Weight, Viscosity, Rheology, and various chemical and physical properties.

PRODUCTS USED LAST 24 HRS table with 3 columns: Products, Size, Amt. Lists various mud additives like ASPHASOL SUPREME, VERSACOAT, VERSATROL, etc.

SOLIDS EQUIP table with 3 columns: Equipment Name, Size, Hrs. Lists Derrick Shaker and other equipment used.

REMARKS AND TREATMENT
22 bbls Oil Added
3 bbls Water Added
42 bbls Products Added
67 bbls Mud Built
0 bbls Mud Received
0 bbls Mud Returned
2560 bbls Starting Volume
2561 bbls Present Volume
-67 bbls Mud Loss /24 hrs
-539 bbls Cumulative Mud Loss 5 bbls New Hole Volume

REMARKS
Drilled to 16605' and short tripped. Pulled tight at 16404'. B/up was 1200 units thru flow line and 190 units thru Buster with a 12' flare. No increase in chlorides at b/up. Drilled ahead pumping 5 bbl sweeps every hours. Conn Gas 330-625 u. w/mud cut 18.1 ppg Bknd gas 25-55 u. Last survey at 16661/48.3 deg. Cost includes a Vacuum Truck Credit.
Oil Base Mud Cuttings
16 cu yds Daily Haul Off
112 cu yds Cumulative Haul Off
Note:Mud Acctg Vol, Other losses are trip losses.

Summary table with 4 columns: TIME DISTR Last 24 Hrs, MUD VOL ACCTG (bbl), SOLIDS ANALYSIS, MUD RHEOLOGY & HYDRAULICS. Includes rig up/service, drilling, tripping, reaming, condition hole, etc.

Contact information table with 4 columns: M-I ENGR / PHONE, RIG PHONE, WAREHOUSE PHONE, DAILY COST, CUMULATIVE COST. Includes names like Corky Karcher and phone numbers.

F. Hoar D.U.



Drilling Fluids

OIL-BASED MUD REPORT No.22

Date	07/30/2001	Depth/TVD	16594 ft / 16116 ft
Spud Date	07/09/2001	Mud Type	Versadriil
Water Depth		Activity	Drilling

Operator : Louis Dreyfus
 Report For : Royce Coats
 Well Name : John Hancock Sr. A-1ST
 Contractor : Helmerick & Payne #89
 Report For : Rick Hawthorne

Field/Area : NE. Speaks
 Description : A-532
 Location : Lavaca County, Texas
 Well No. : C3957

DRILLING ASSEMBLY		CASING	MUD VOLUME (bbl)	CIRCULATION DATA		
Bit Size	6.75 in Sec FM2831	Surface	Hole	Pump Make	G.D. PZ-11	G.D. PZ-11
Nozzles	4x12 / 1/32"	9.625in @10751ft (10751TVD)	943.5	Pump Size	6 X 11.in	6 X 11.in
Drill Pipe Size	Length	Intermediate	Active Pits	Pump Cap	3.837 gal/stk	3.837 gal/stk
5 in	9032 ft	7.625in @14072ft (14072TVD)	641.5	Pump stk/min	56@95%	
Drill Pipe Size	Length	Intermediate	Total Circulating Vol	Flow Rate	215 gal/min	
4 in	7075 ft		1585	Bottoms Up	137.4 min	7696 stk
Drill Collar Size	Length	Production or Liner	In Storage	Total Circ Time	309.6 min	17339 stk
4.75 in	302 ft		975	Circulating Pressure	3550 psi	

MUD PROPERTIES		
Sample From		PIT@03:00
Flow Line Temp	°F	170
Depth/TVD	ft	16594/16116
Mud Weight	lb/gal	18.4@162°F
Funnel Viscosity	s/qt	90
Rheology Temp	°F	160
R600/R300		176/102
R200/R100		-/-
R6/R3		-.4
PV	cP	74 <----LCM in
YP	lb/100ft²	28 <---- Mud
10s/10m/30m Gel	lb/100ft²	5/19/29
API Fluid Loss	cc/30 min	NA
HTHP FL Temp	cc/30 min	2.6@400°F
Cake API/HTHP	1/32"	-.3
Unc Ret Solids	%Vol	41.5
Correct Solids	%Vol	40.40
Oil	%Vol	53.5
Uncorr Water	%Vol	5
Oil/Water Ratio		91/9
Alkal (Pom)		3.0
Cl Whole Mud	mg/l	10500
Salt	%Wt	24.73 247300
Lime	lb/bbl	3.9
E-Stability		1700
Received Volume	bbl	2264
Returned Volume	bbl	0
Present Volume	bbl	2560
Diff. Volume	bbl	+296

PRODUCTS USED LAST 24 HRS		
Products	Size	Amt
M-I BAR BULK	100 LB BG	526
VERSACOAT	1 GA BK	30
VERSATROL	50 LB BG	5
CLEAN-UP	5 GA CN	3
MUD DIESEL	1 GA BK	490
VACUUM TRUCK HAULING	1 EA	452
SAFE-CARB FINE	50 LB BG	13
SAFE-CARB MEDIUM	50 LB BG	6
MIX II FINE	25 LB BG	8
MIX II MED	25 LB BG	2
G-SEAL	50 LB BG	7
TRUCKING SERVICE	1 EA	452
ENGINEERING SERVICE	1 EA	1

SOLIDS EQUIP	Size	Hrs
Derrick Shaker	14/14/14	0
Derrick Shaker	175/175/175	24
Derrick Shaker	175/175/175	24

MUD PROPERTY SPECIFICATIONS	
Weight	Co. Orders
Viscosity	50-60
Filtrate	<4 cc HTHP

REMARKS AND TREATMENT

12 bbls Oil Added
 8 bbls Water Added
 39 bbls Products Added
 59 bbls Mud Built
 0 bbls Mud Received
 0 bbls Mud Returned
 2522 bbls Starting Volume
 2560 bbls Present Volume
 -21 bbls Mud Loss /24 hrs
 -472 bbls Cumulative Mud Loss 4.5 bbls New Hole Volume

REMARKS

Drilled ahead slowly increasing mud weight to 18.4+ ppg. Connection gas 360 to 375 units with a 7 to 10 ft. flare. D/T gas, 400 units w/6 flare. BKGRN gas, 35 to 350 units. Maintaining LCM sweeps at 5 bbls on the hour. Last survey: 16533/16074' = 46.6 deg. Last connection gas at 16559', 365 units gas w/no flare.

Oil Base Mud Cuttings
 00 cu yds Daily Haul Off
 96 cu yds Cumulative Haul Off

TIME DISTR	Last 24 Hrs	MUD VOL ACCTG (bbl)	SOLIDS ANALYSIS		MUD RHEOLOGY & HYDRAULICS	
Rig Up/Service	0.5	Oil Added	0	Salt Wt%	24.73	np/na Values
Drilling	18	Water Added	8	Salt Conc./bbl	5.75	kp/ka (lb-s^n/100ft²)
Tripping		Mud Received	0	Adjusted Solid %	41.09	Bit Loss (psi / %)
Reaming		Centrifuge	0	Oil/Water Ratio	91/9	Bit HHP (hhp / HSI)
Condition Hole		Formation	0	Average SG Solids	4.1	Bit Jet Vel (ft/s)
Circulating	5.5	Left in Hole	0	Low Gr %	1.7	Annular Vel DP (ft/min)
Slip and Cut		Other	0	Low Gr Wt, lb/bbl	15.5	Annular Vel DC (ft/min)
Condition Mud		Dumped	0	High Gr %	39.4	Crit Vel DP (ft/min)
Chg Swvl Pkng		Shakers	15	High Gr Wt lb/bbl	578.7	Crit Vel DC (ft/min)
P/U Rot. Head		Evaporation	6			ECD @ 16594 (lb/gal)
						19.1

M-I ENGR / PHONE	RIG PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
Corky Karcher Cell 361 985-7424 830 708-5715	361 798-7111	361 358-0181	\$ 9,714.99	\$ 102,056.43

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

Digital Data

- INSITE adi backup with Data directory on MO disk

TS01-001-HT195: <Solar 195>

01 Aug 2001 – 14 Aug 2001

Miscellaneous