

Introductions to aberrations

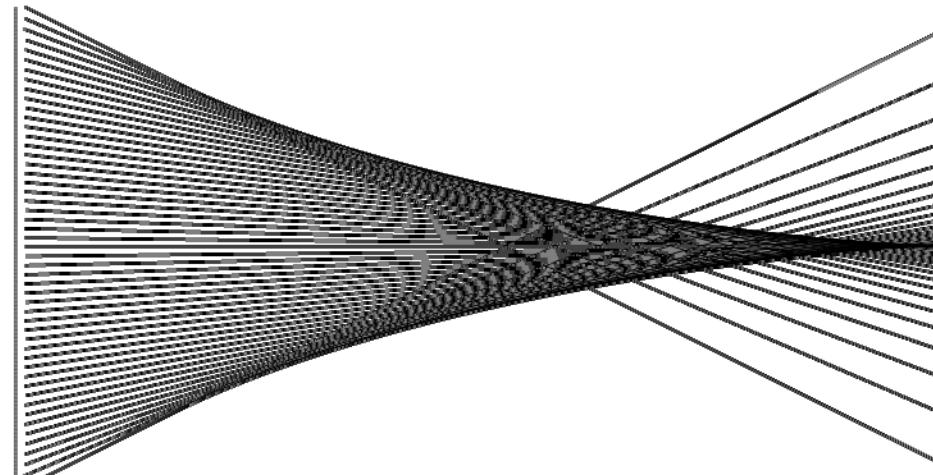
OPTI 517

Lecture 11

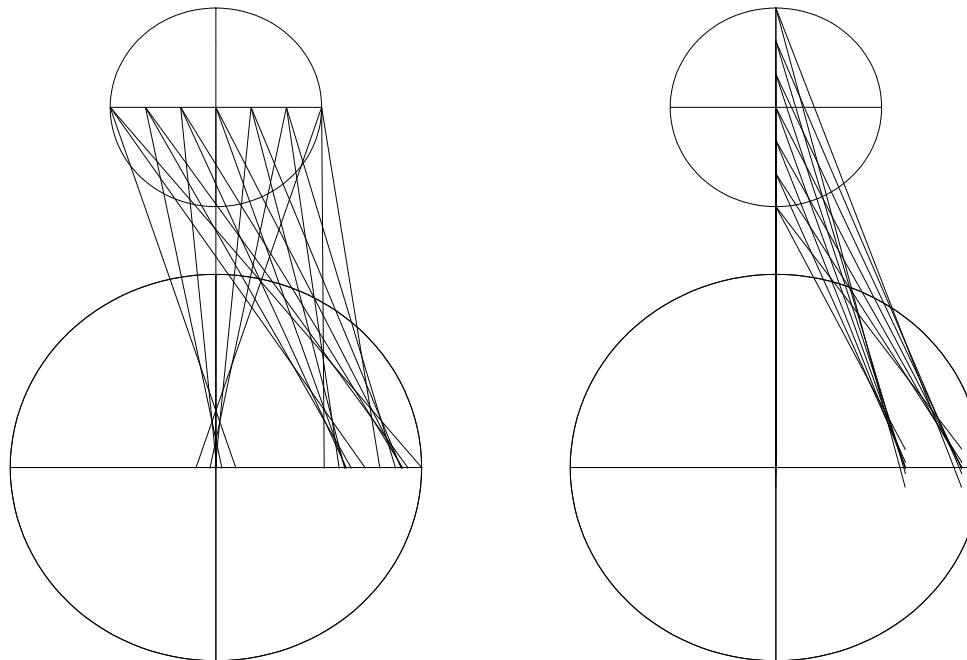
Prof. Jose Sasian
OPTI 518



Spherical aberration



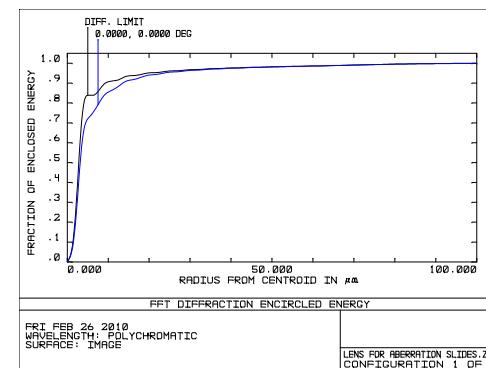
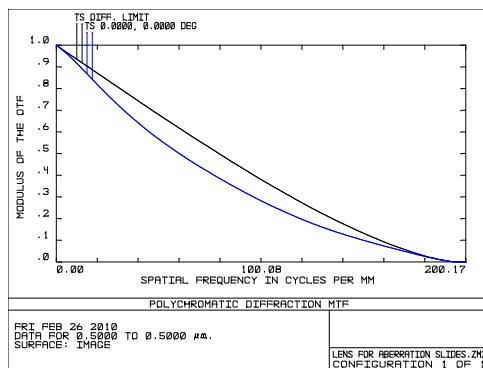
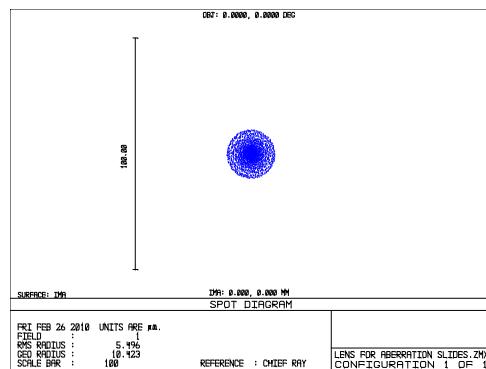
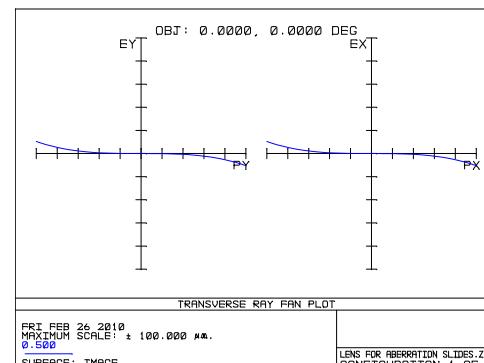
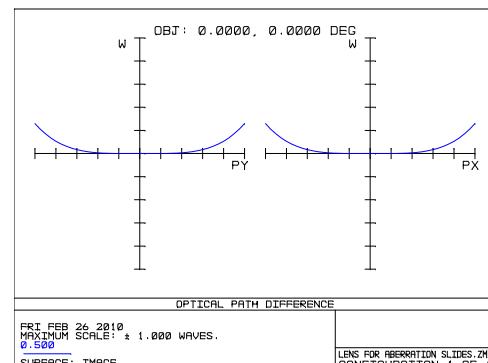
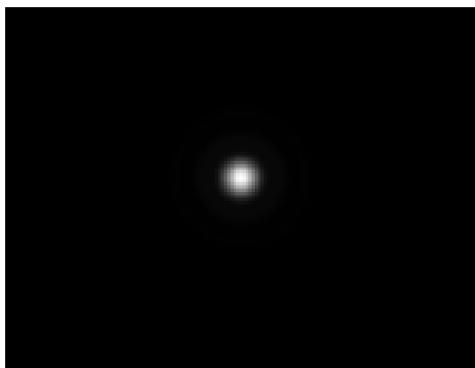
Meridional and sagittal ray fans



Prof. Jose Sasian
OPTI 518

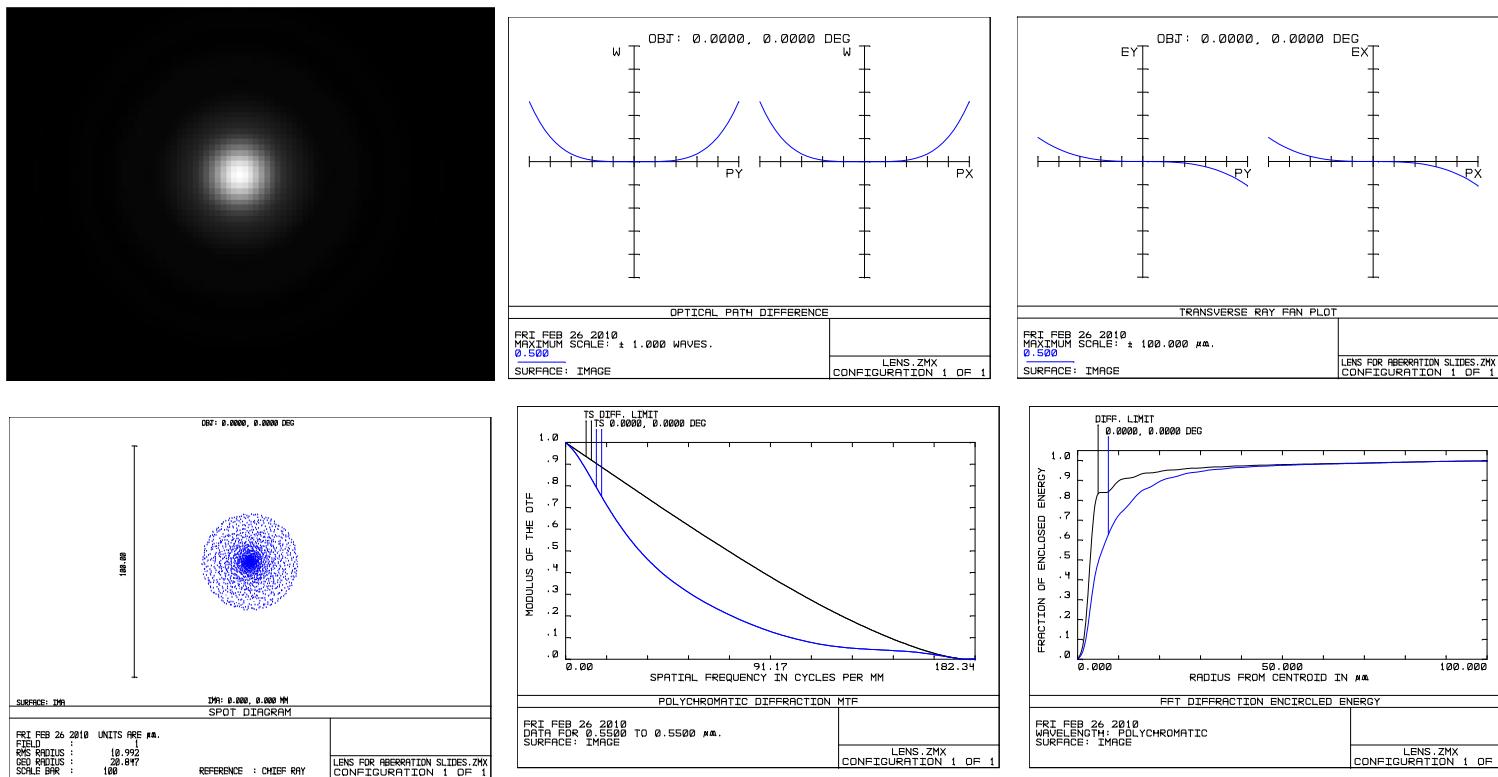
Spherical aberration 0.25 wave

f/10; f=100 mm; wave=0.0005 mm



Spherical aberration 0.5 wave

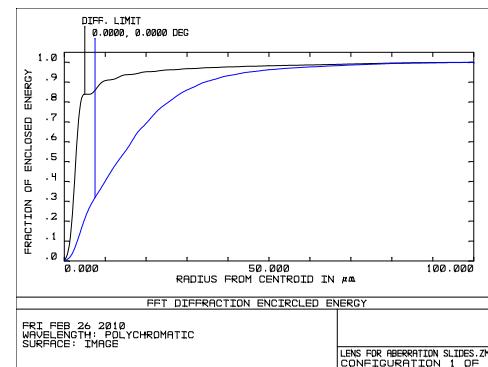
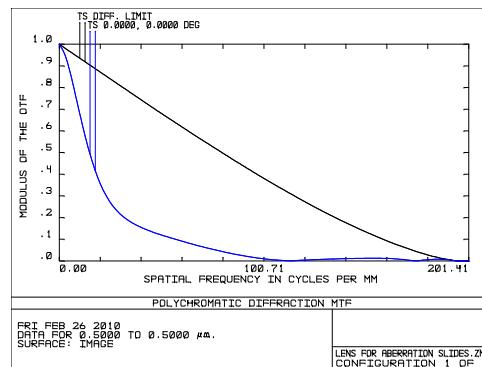
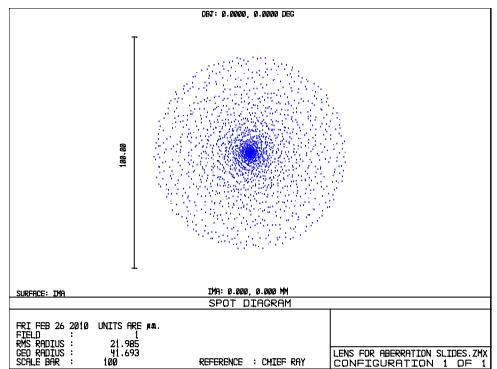
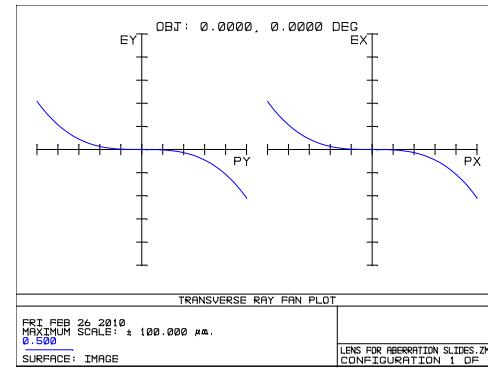
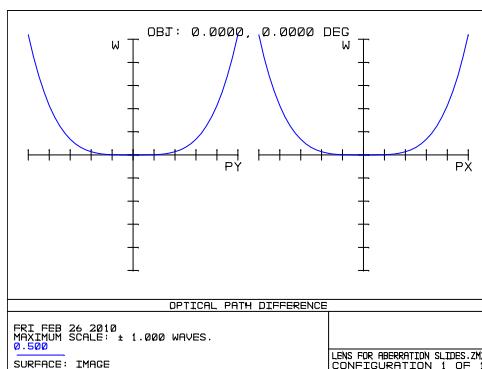
f/10; f=100 mm; wave=0.0005 mm



Prof. Jose Sasian
OPTI 518

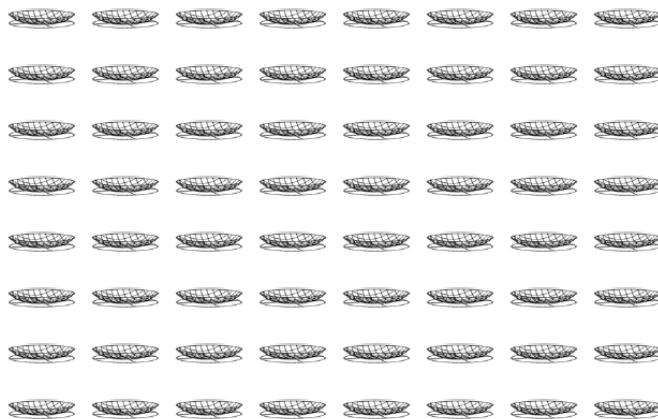
Spherical aberration 1 wave

f/10; f=100 mm; wave=0.0005 mm

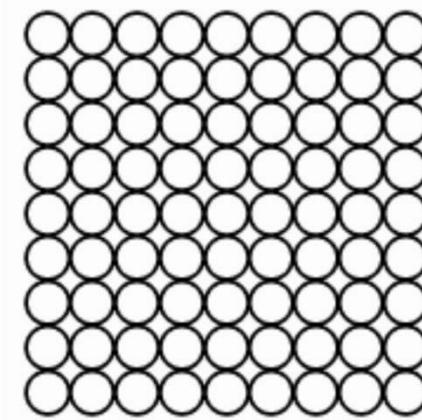


Spherical aberration is uniform over the field of view

$$W_{040} (\vec{\rho} \cdot \vec{\rho})^2$$

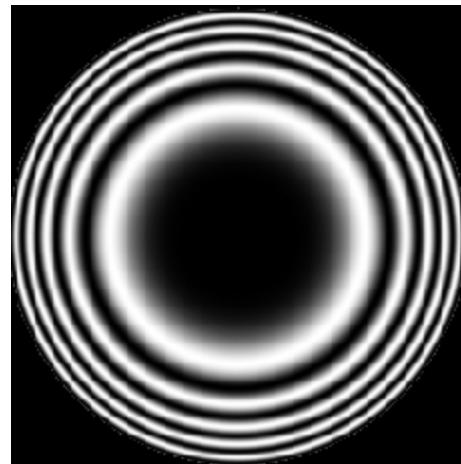


Wavefront



Spots

Interferometric representation



5 waves

Prof. Jose Sasian
OPTI 518

Cases of zero spherical aberration from a spherical surface

$$W_{040}(\vec{\rho} \cdot \vec{\rho})^2 \quad W_{040} = \frac{1}{8} S_I \quad S_I = -\sum A^2 y \Delta \left(\frac{u}{n} \right)$$

$$y = 0$$

$$A = 0$$

$$\Delta(u/n) = u'/n' - u/n = 0$$

y=0 the aperture is zero or the surface is at an image

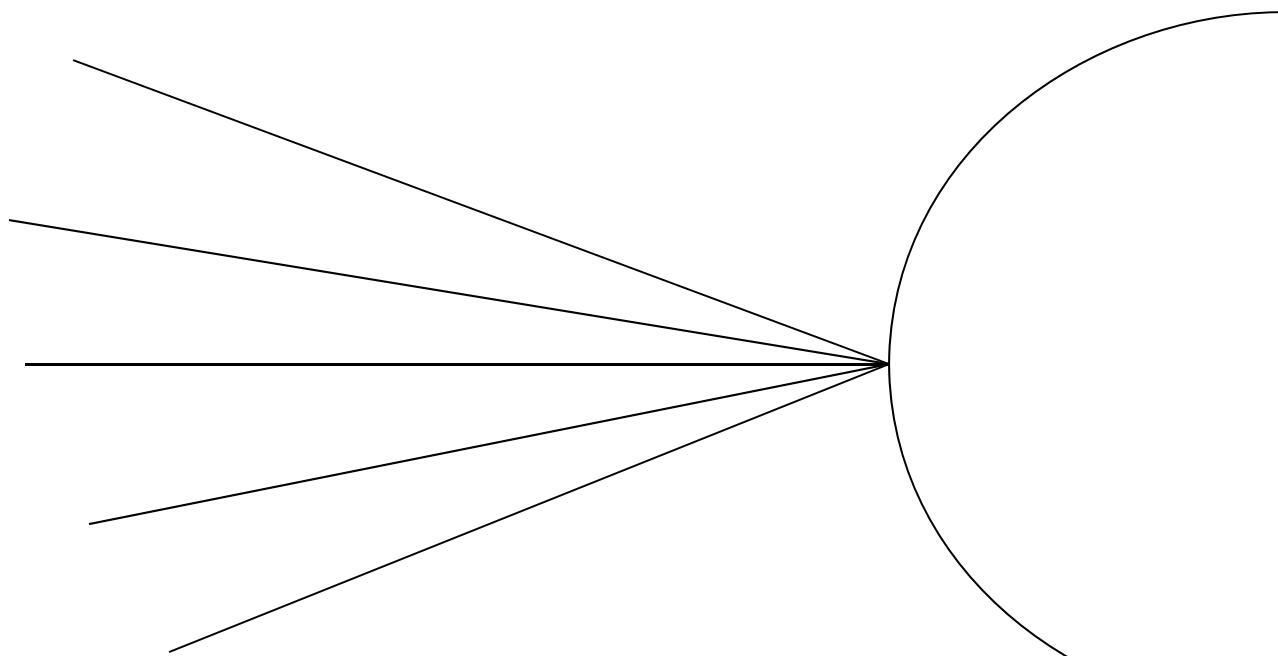
A=0 the surface is concentric with the Gaussian image point on axis

u'/n-u/n=0 the conjugates are at the aplanatic points

Aplanatic means free from error;
freedom from spherical aberration and coma

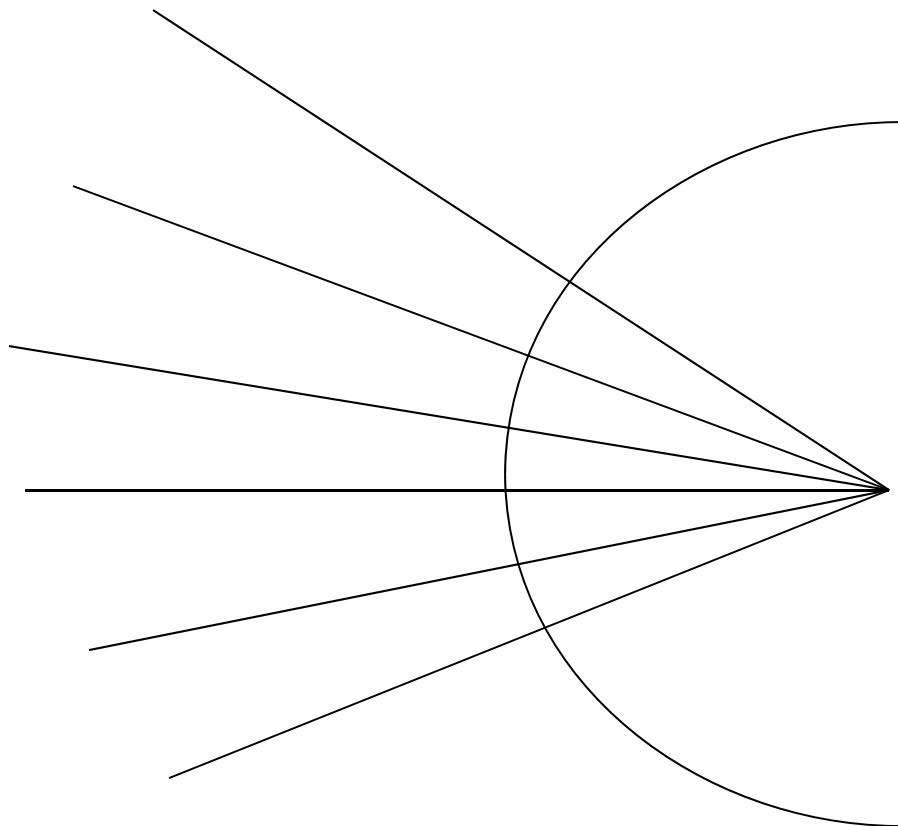
Surface at image

$$y = 0$$



Concentric surface

$$A = 0$$



Prof. Jose Sasian
OPTI 518

Aplanatic points of a spherical surface

$$-\frac{1}{n's'} + \frac{1}{ns} = 0$$

$$\frac{n'}{s'} - \frac{n}{s} = \frac{n' - n}{r}$$

$$S = r \frac{n' + n}{n}$$

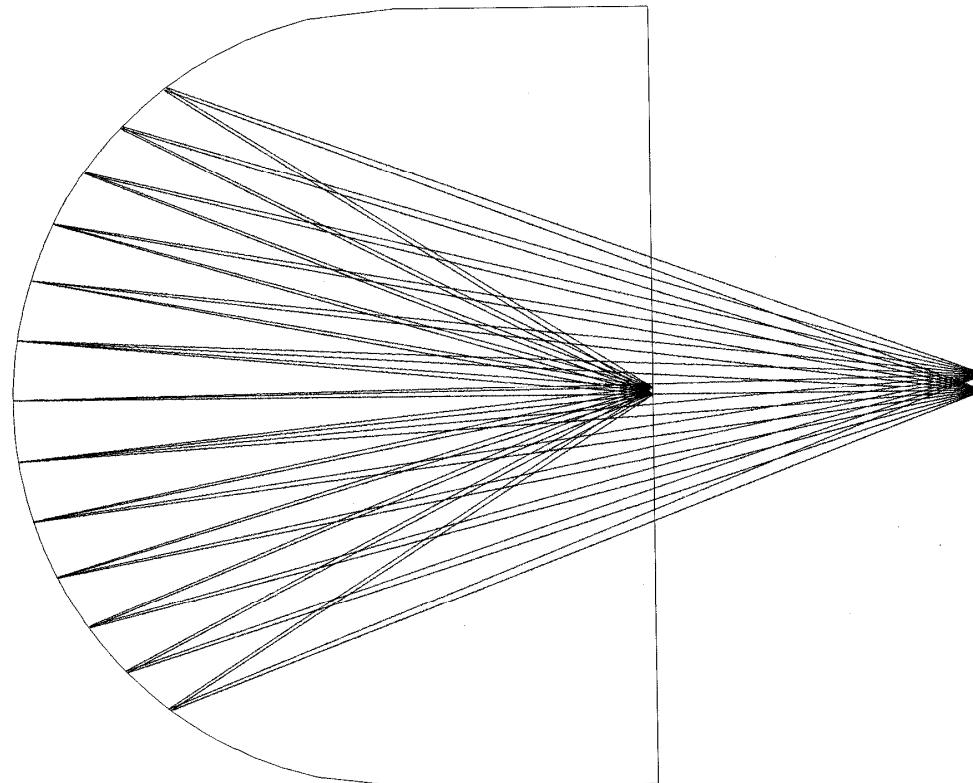
$$S' = r \frac{n' + n}{n'}$$

$$S = 2.5r$$

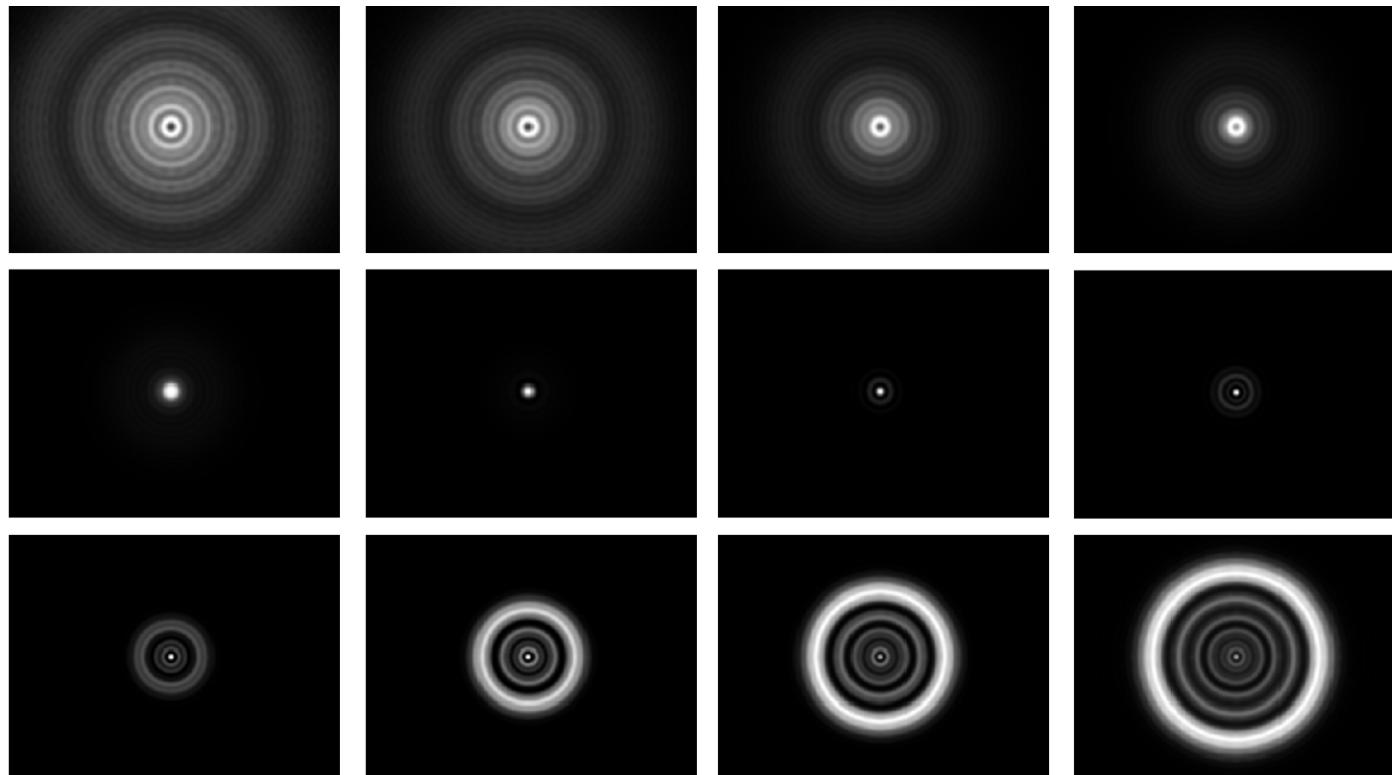
$$S' = (5/3)r$$

$$n = 1.5$$

$$\Delta(u/n) = u'/n - u/n = 0$$



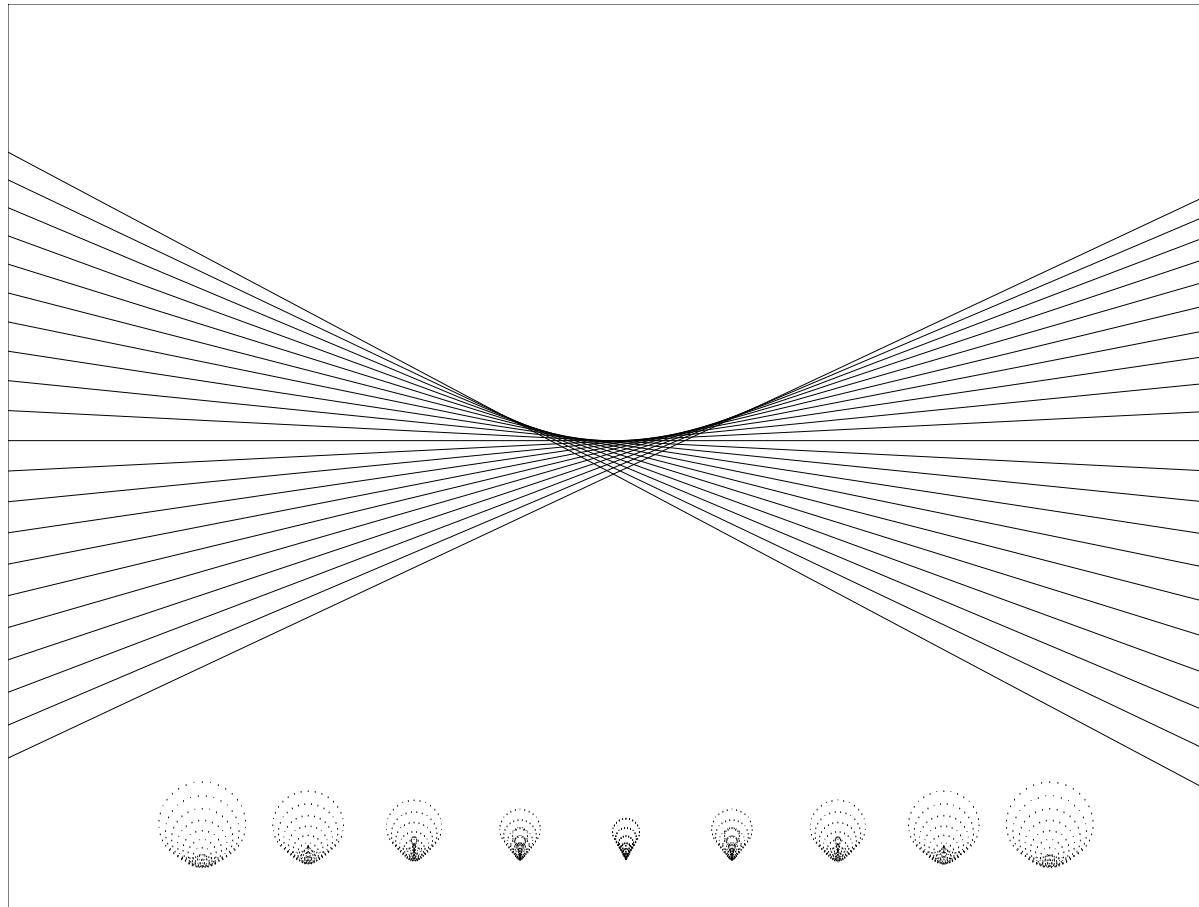
Diffraction images



Two waves of spherical aberration

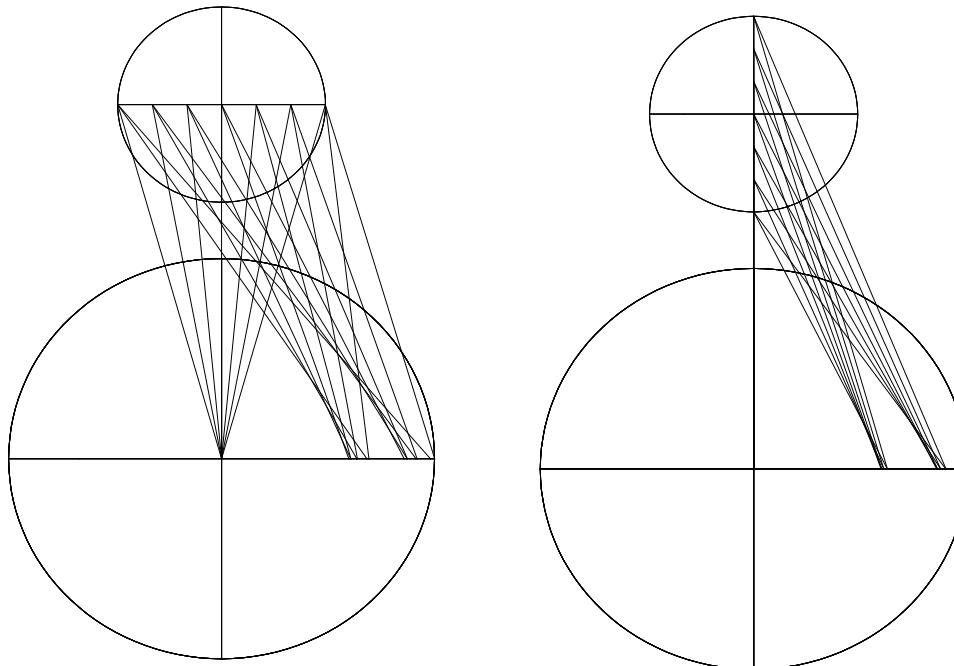
Prof. Jose Sasian
OPTI 518

Coma aberration



Prof. Jose Sasian
OPTI 518

Meridional and sagittal ray fans



Prof. Jose Sasian
OPTI 518

WAVE ABERRATION

$$W = W_{131} H \rho^3 \cos \phi + \Delta W_{20} \rho^2$$

TRANSVERSE RAY ABERRATION

$$\omega' \vec{e} = [W_{131} H \rho^2] \vec{h} + z [\Delta W_{20} \rho + (W_{131} H \rho^2) \cos \phi] \vec{g}$$

FOR $\rho = \text{CONST.}$ (ZONAL DIAGRAM), $a = W_{131} H \rho^2$, $b = \Delta W_{20} \rho$

$$\begin{aligned}\omega' \vec{e} &= a \vec{h} + z(b + a \cos \phi) \vec{g} \\ &= a \vec{h} + n \vec{g}\end{aligned}$$

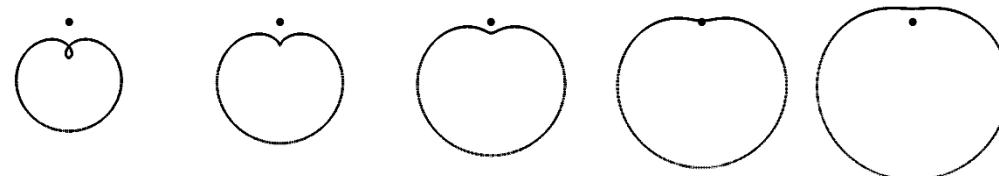
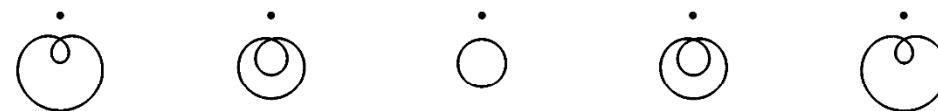
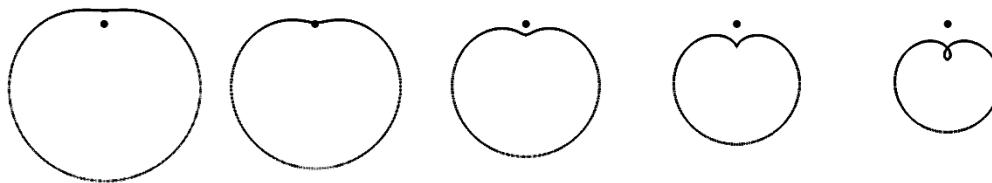
$$n = 2(b + a \cos \phi) \quad \text{LIMAÇON OF PASCAL}$$

FOR $b = 0$ ($\Delta W_{20} = 0$), $n = 2a \cos \phi$ DOUBLE CIRCLE

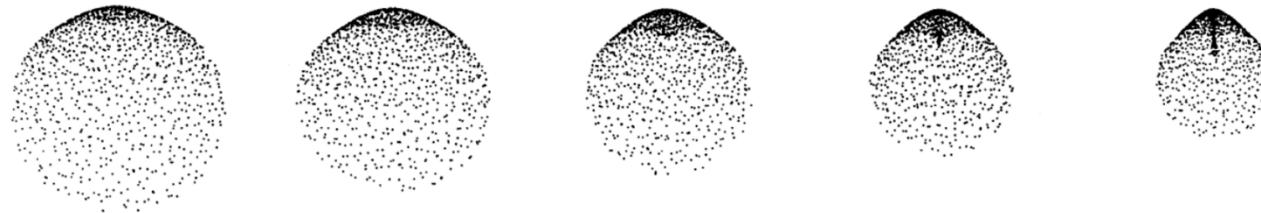
FOR $b = \pm a$ ($\Delta W_{20} = \pm W_{131} H \rho$), $n = 2a(\pm 1 + \cos \phi)$ CARDIOID

Roland Shack's notes

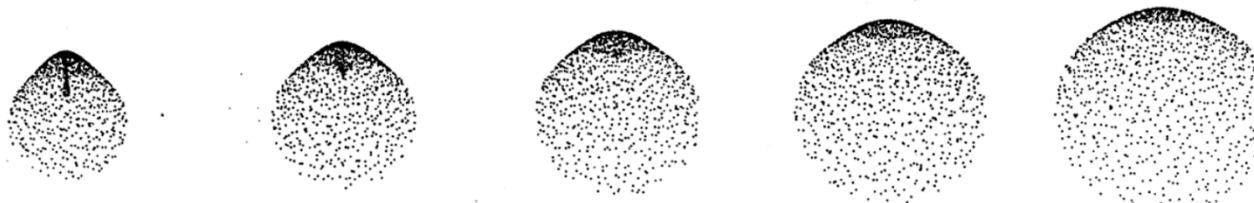
Coma zonal diagrams



Spot diagrams through focus



122

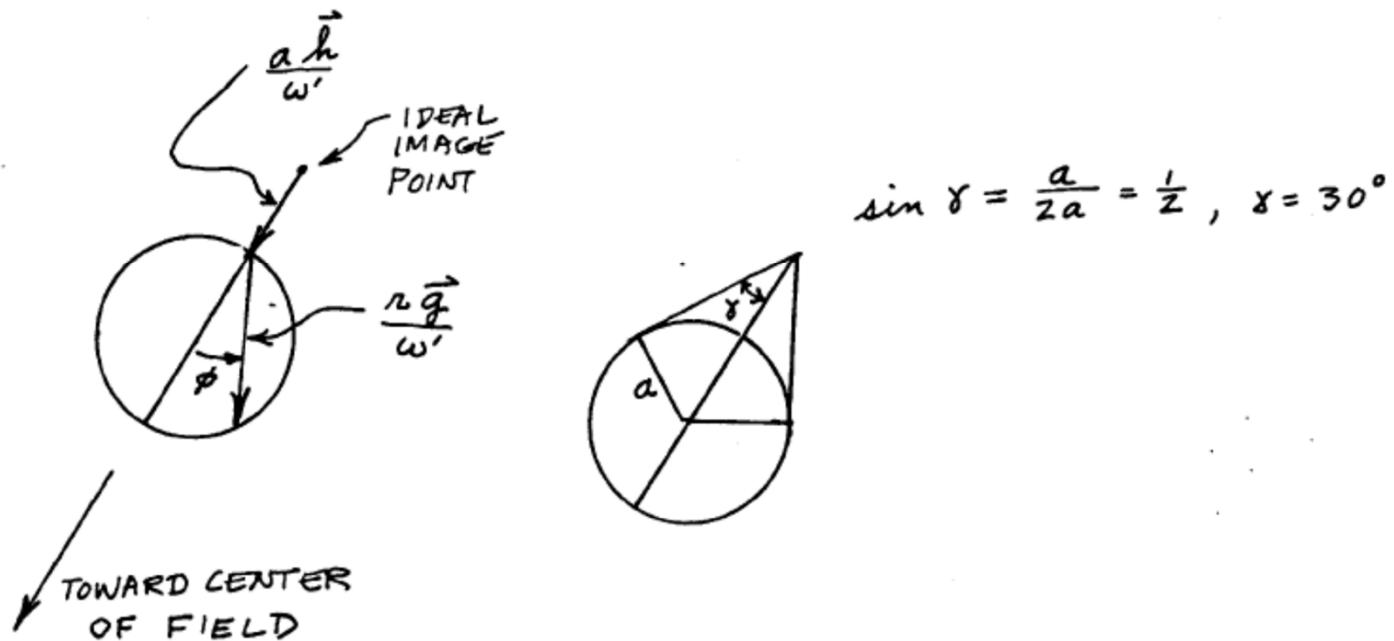


Roland Shack's notes

Prof. Jose Sasian
OPTI 518

Coma zonal diagrams

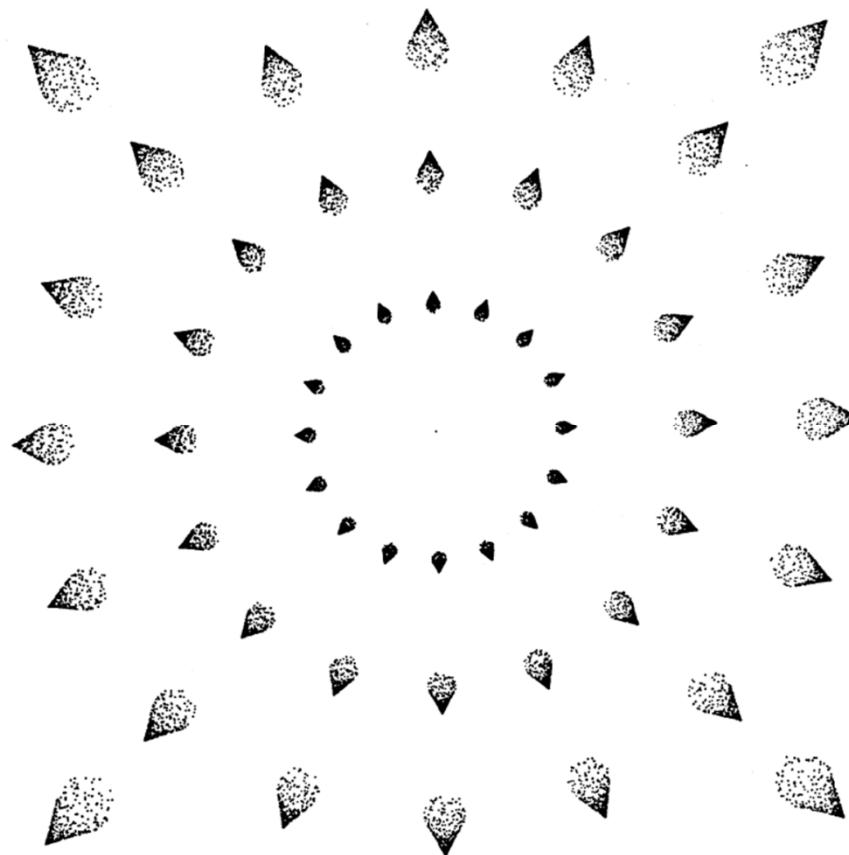
$$\rho = 1, \Delta W_{z0} = 0 \quad (\text{ZONAL DIAGRAM})$$



Roland Shack's notes

Prof. Jose Sasian
OPTI 518

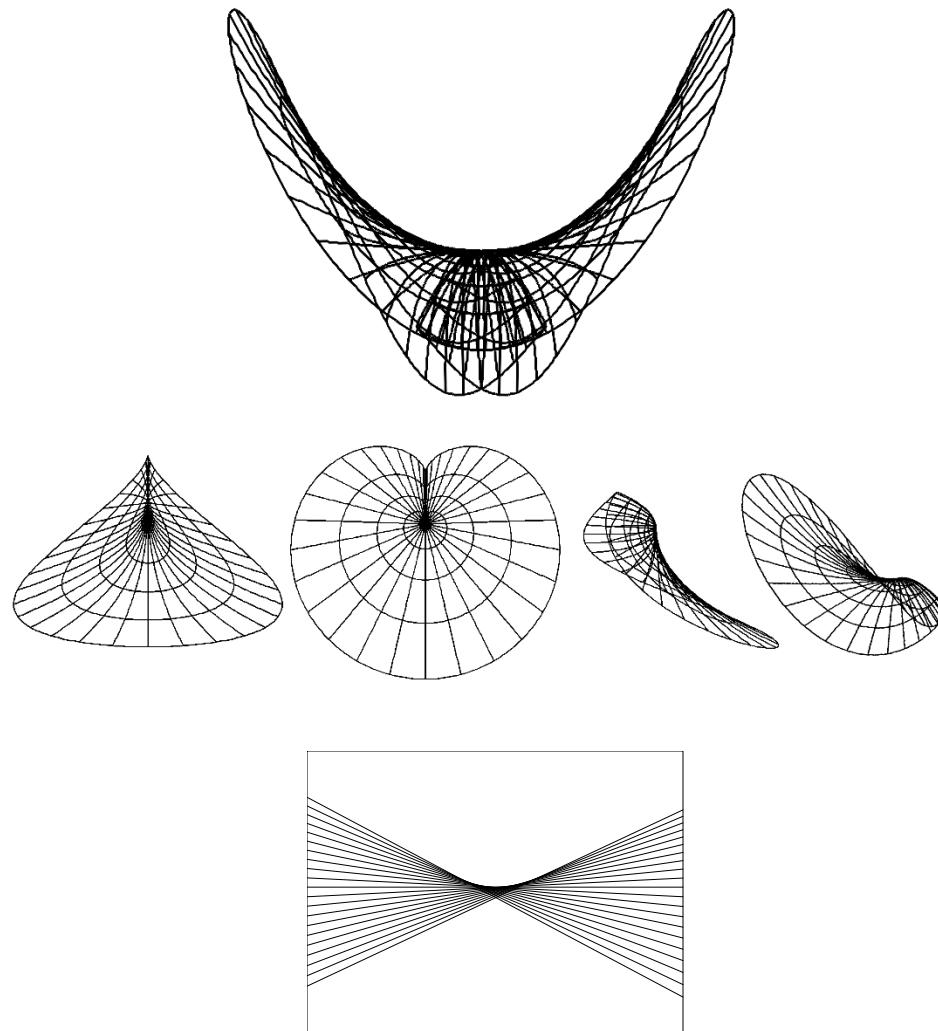
Positive coma over the field of view



Roland Shack's notes

Prof. Jose Sasian
OPTI 518

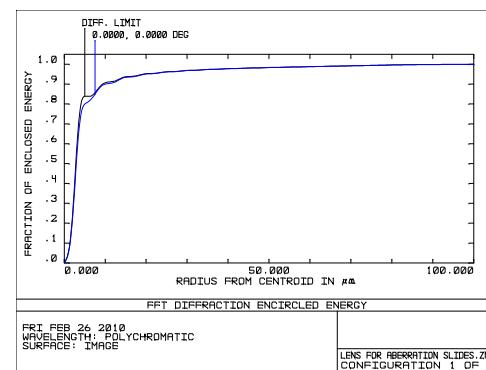
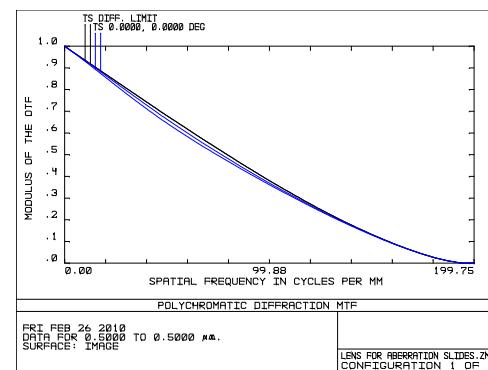
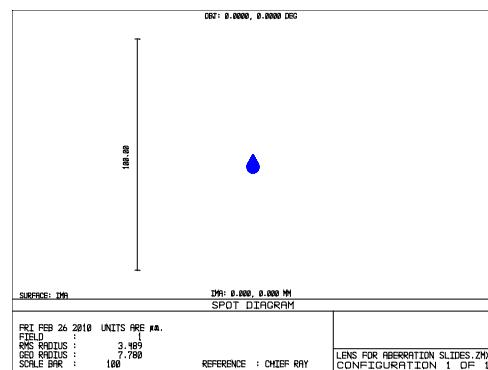
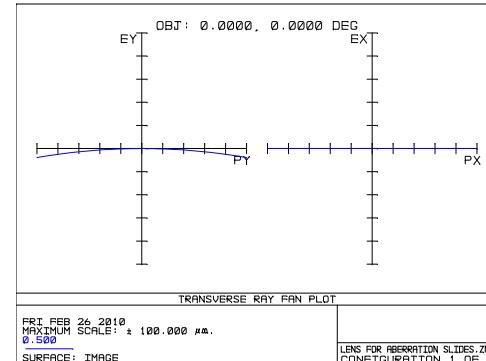
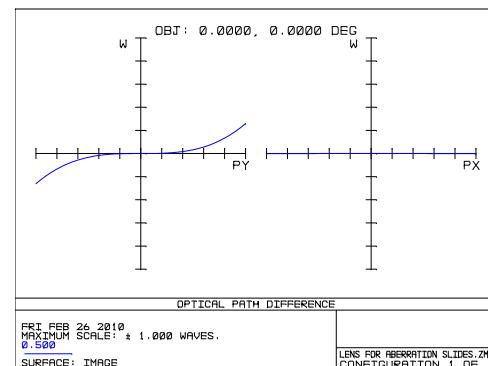
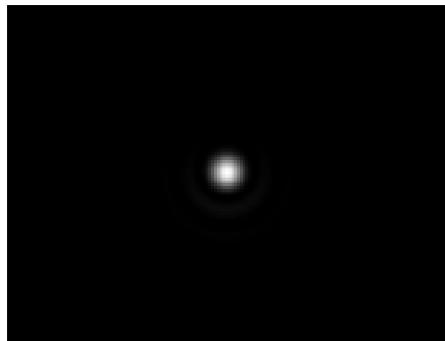
Caustic sheets



Prof. Jose Sasian
OPTI 518

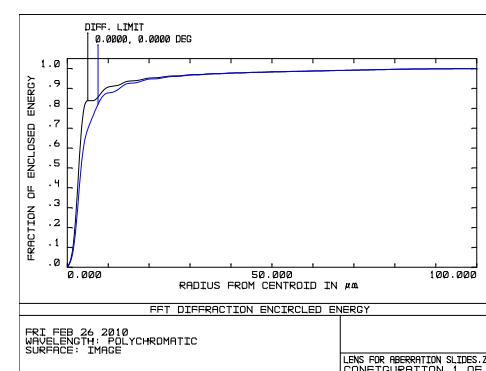
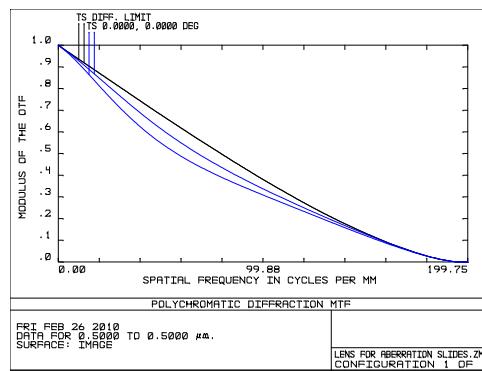
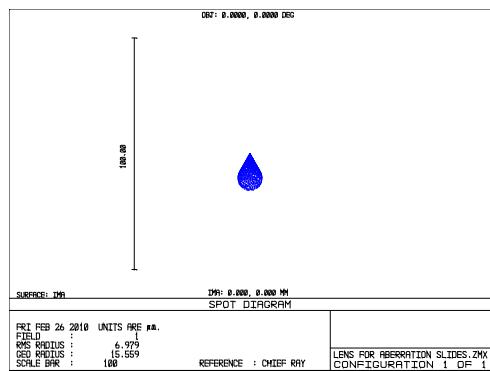
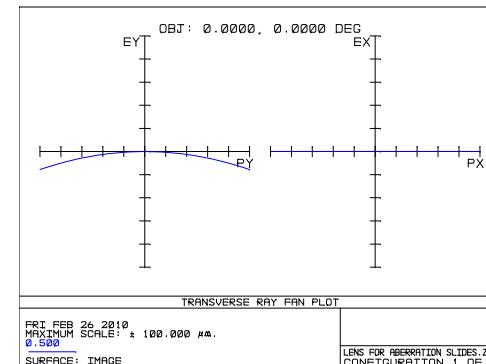
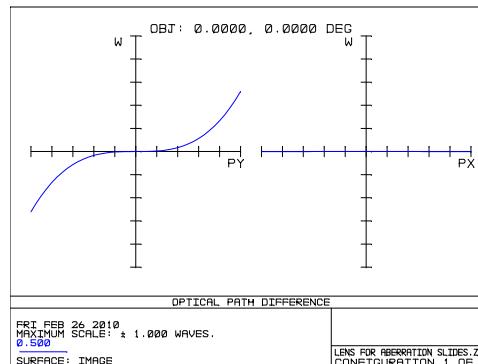
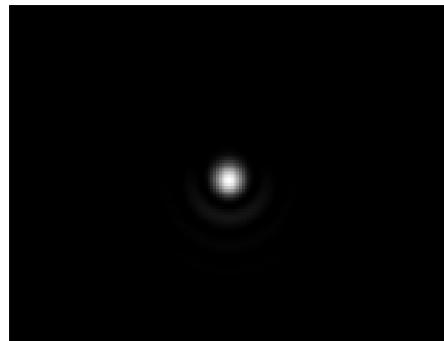
Coma aberration 0.25 wave

f/10; f=100 mm; wave=0.0005 mm



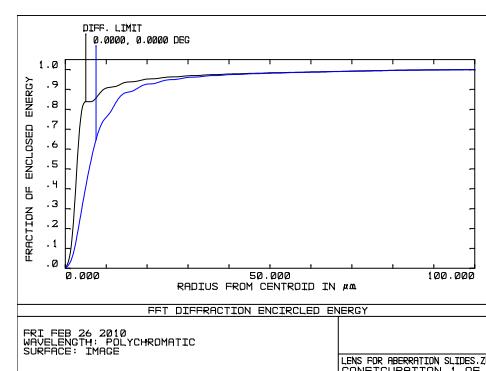
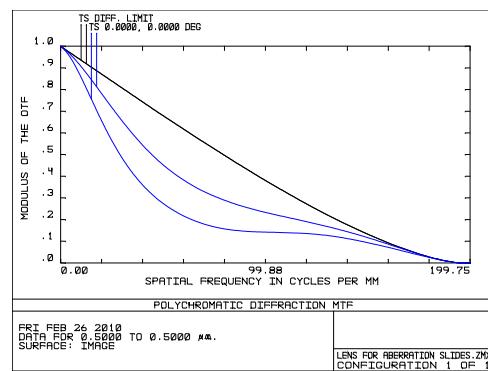
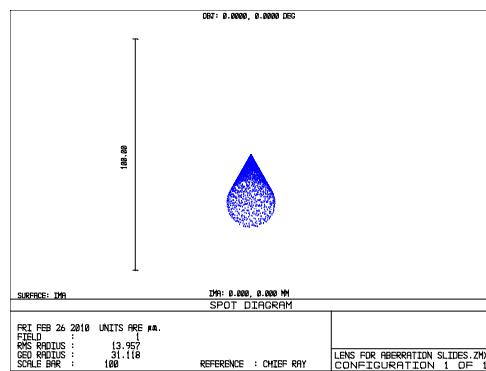
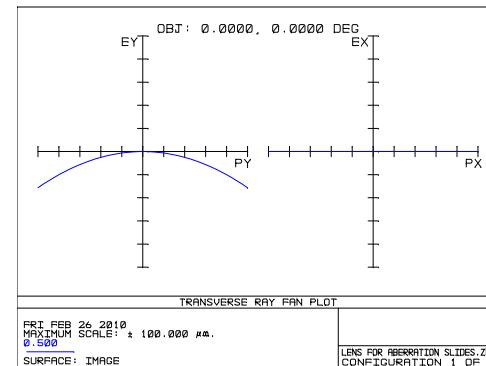
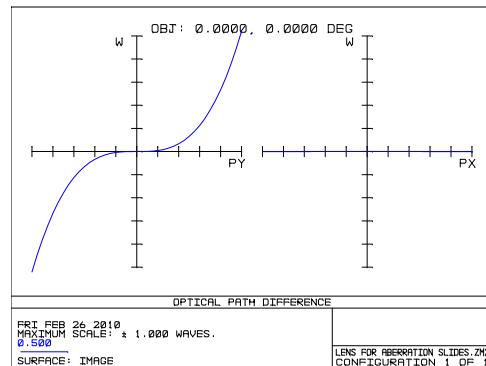
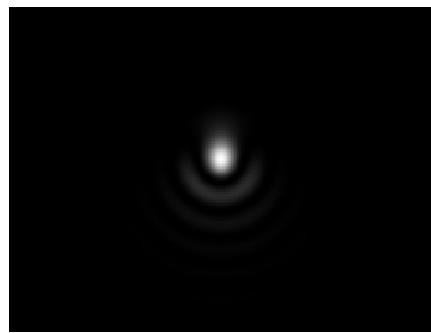
Coma aberration 0.5 wave

f/10; f=100 mm; wave=0.0005 mm



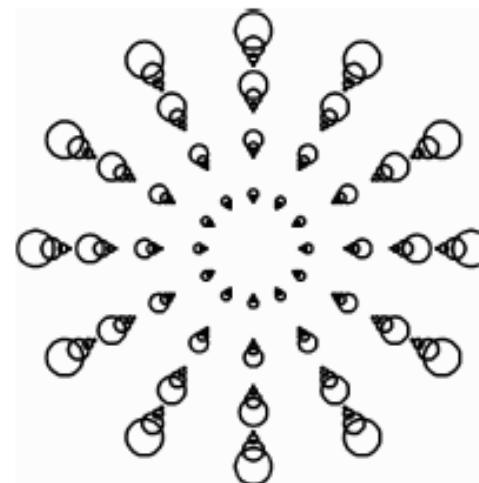
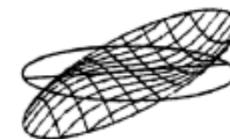
Coma aberration 1.0 wave

f/10; f=100 mm; wave=0.0005 mm

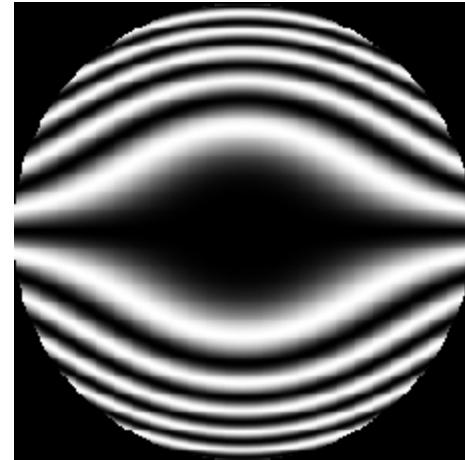


Coma varies linearly over the field of view

$$W_{131}(\vec{H} \cdot \vec{\rho})(\vec{\rho} \cdot \vec{\rho})$$



Interferometric representation



5 waves

Prof. Jose Sasian
OPTI 518

Cases of zero coma aberration from a spherical surface

$$W_{131}(\vec{H} \cdot \vec{\rho})(\vec{\rho} \cdot \vec{\rho})$$

$$W_{131} = \frac{1}{2} S_{II}$$

$$S_{II} = -\sum A\bar{A}y\Delta\left(\frac{u}{n}\right)$$

$$y = 0$$

$$A = 0$$

$$\bar{A} = 0$$

$$\Delta(u/n) = u'/n' - u/n = 0$$

y=0 the aperture is zero or the surface is at an image

A=0 the surface is concentric with the Gaussian image point on axis

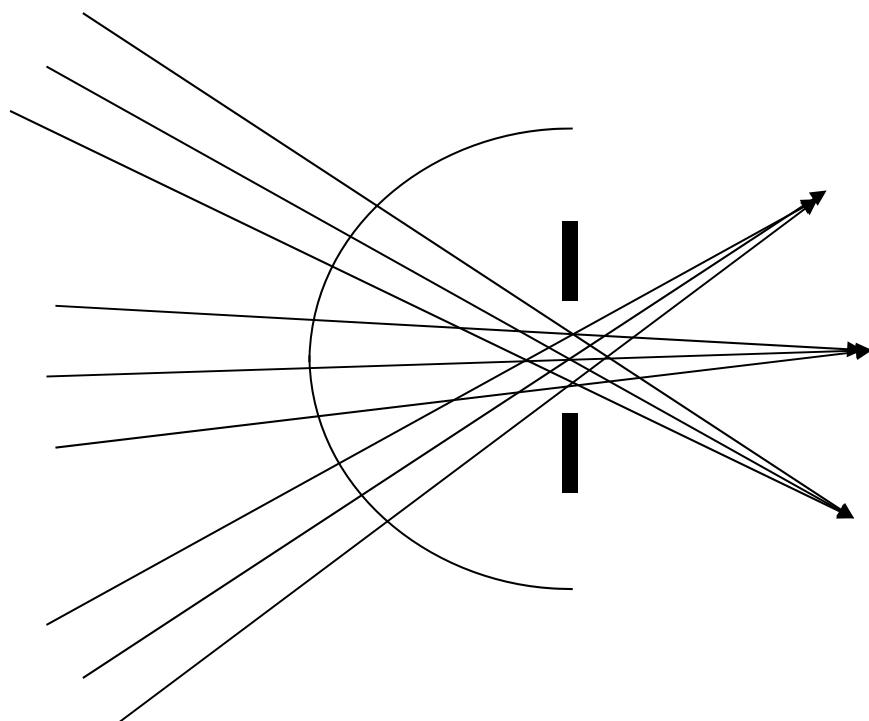
Abar=0 surface is concentric with stop or pupils

u'/n-u/n=0 the conjugates are at the aplanatic points

Aplanatic means free from error;
freedom from spherical aberration and coma

Concentric surface with stop or pupils

$$\bar{A} = 0$$



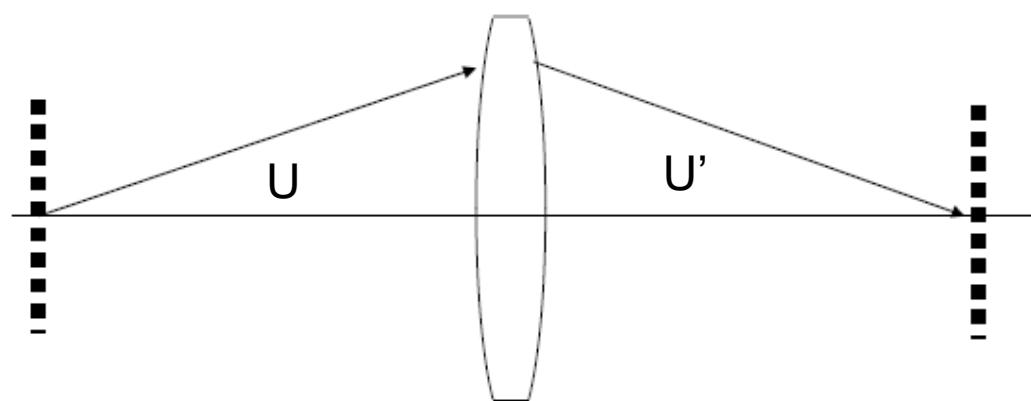
Sine condition

- In the absence of spherical aberration there are no linear phase errors that depend on the field of view if the sine condition is met:

$$\frac{\sin(U)}{\sin(U')} = \frac{u}{u'}$$

The first-order magnification is equal to the real marginal ray magnification

Imaging a grating



$$\sin(U) = \frac{m \cdot \lambda}{d}$$

$$d \cdot \sin(U) = m \cdot \lambda = d' \sin(U')$$



Diffraction images

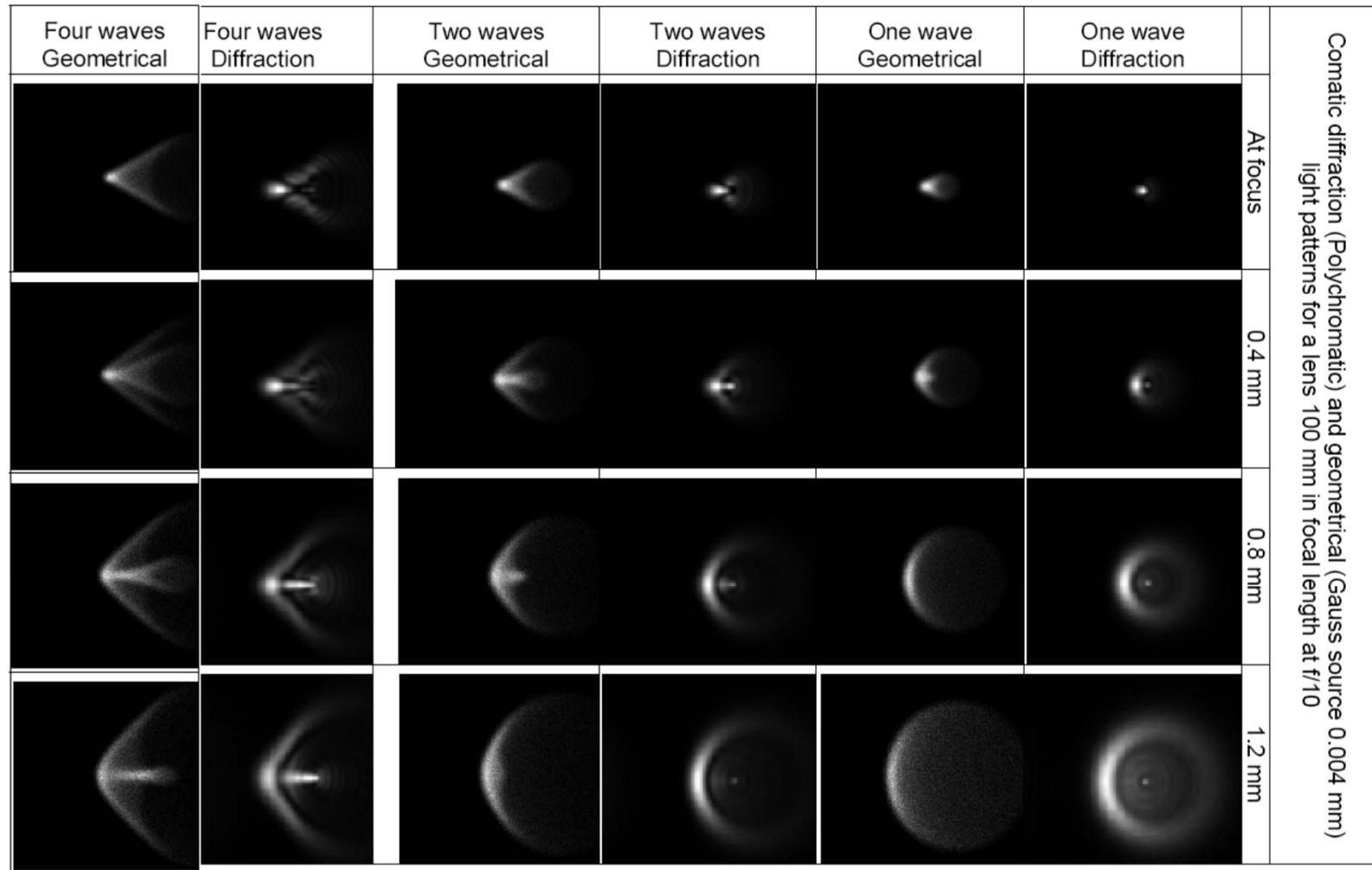


2 waves



4 waves

Geometrical and diffraction

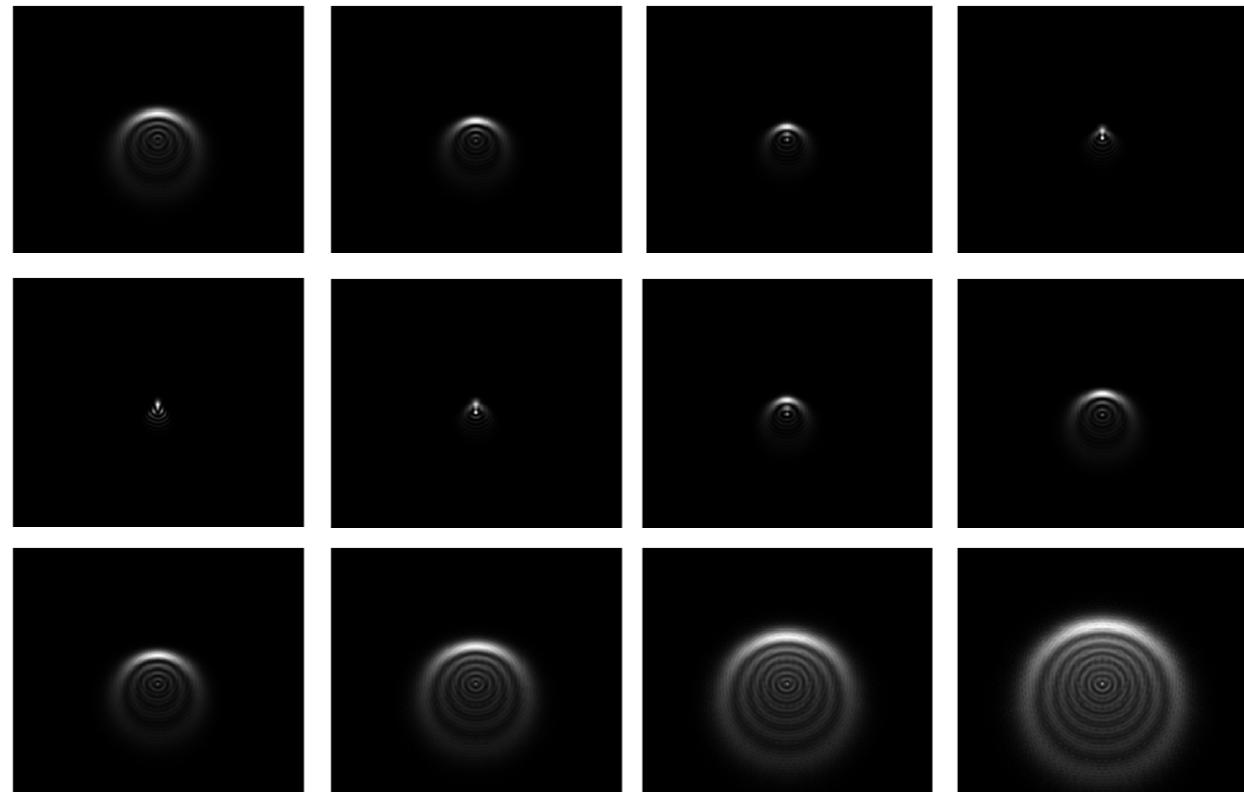


Prof. Jose Sasian
OPTI 518



College of Optical Sciences
THE UNIVERSITY OF ARIZONA®

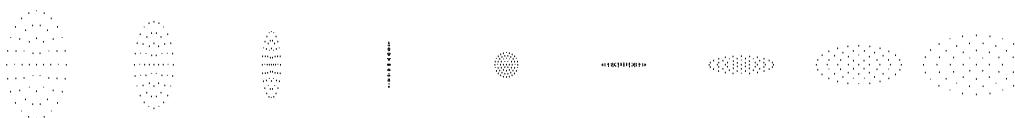
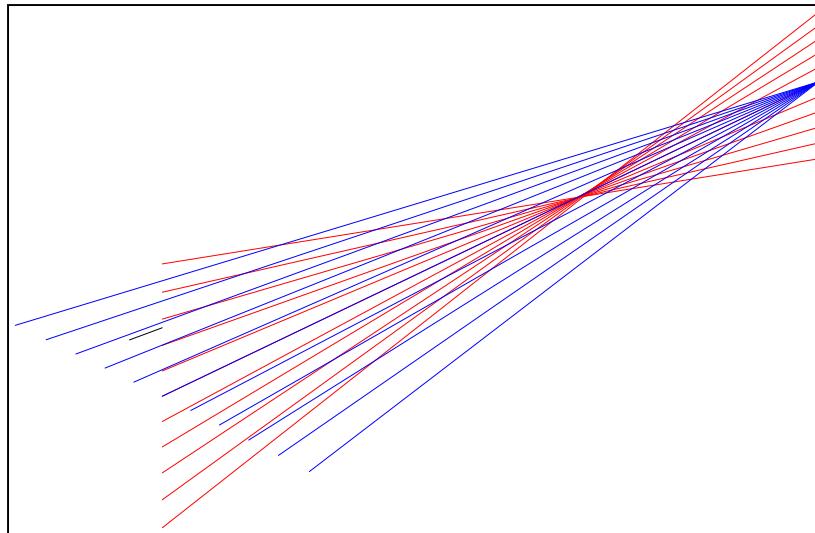
Coma



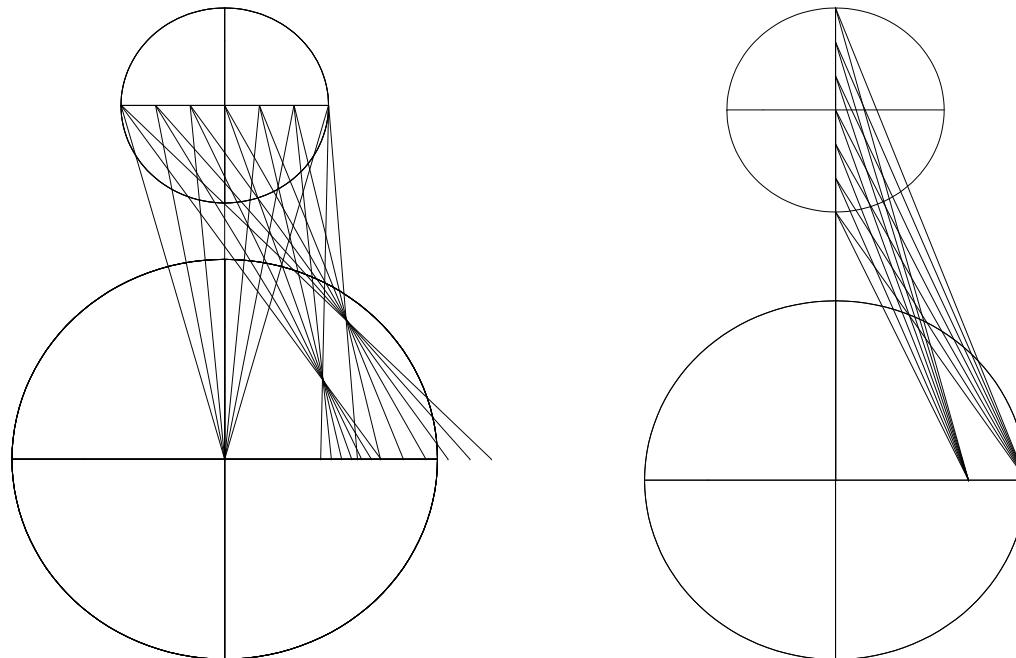
Two waves of coma through focus

Prof. Jose Sasian
OPTI 518

Astigmatism aberration



Meridional and sagittal ray fans



Prof. Jose Sasian
OPTI 518

Astigmatism

WAVE ABERRATION

$$W = W_{zzz} H^2 \rho^2 \cos^2 \phi + W_{z20} H^2 \rho^2 + \Delta W_{20} \rho^2$$

TRANSVERSE RAY ABERRATION

$$\omega' \vec{e} = 2 [(W_{zzz} + W_{z20}) H^2 + \Delta W_{20}] \rho \cos \phi \vec{h} + 2 [W_{z20} H^2 + \Delta W_{20}] \rho \sin \phi \vec{i}$$

$$\omega' \vec{e} = a \cos \phi \vec{h} + b \sin \phi \vec{i} \quad \text{ELLIPSE}$$

SAGITTAL FOCUS ($b=0$)

$$\Delta W_{20} = - W_{z20} H^2$$

$$\omega' \vec{e} = 2 W_{zzz} H^2 \rho \cos \phi \vec{h} \quad \text{MERIDIONAL LINE SEGMENT}$$

Roland Shack's notes

Prof. Jose Sasian
OPTI 518



College of Optical Sciences
THE UNIVERSITY OF ARIZONA®

Astigmatism

TANGENTIAL FOCUS ($\alpha = 0$)

$$\Delta W_{20} = -(W_{220} + W_{222})H^2$$

$$\omega' \vec{e} = -2W_{222} H^2 \rho \sin \phi \vec{i} \quad \text{TRANSVERSE LINE SEGMENT}$$

MEDIAL FOCUS ($b = -a$)

$$\Delta W_{20} = -(W_{220} + \frac{1}{2}W_{222})H^2$$

$$\omega' \vec{e} = W_{222} H^2 \rho [\cos \phi \vec{h} - \sin \phi \vec{i}] \quad \text{CIRCLE (COUNTER-ROTATING)}$$

Roland Shack's notes

Prof. Jose Sasian
OPTI 518



Spots through focus



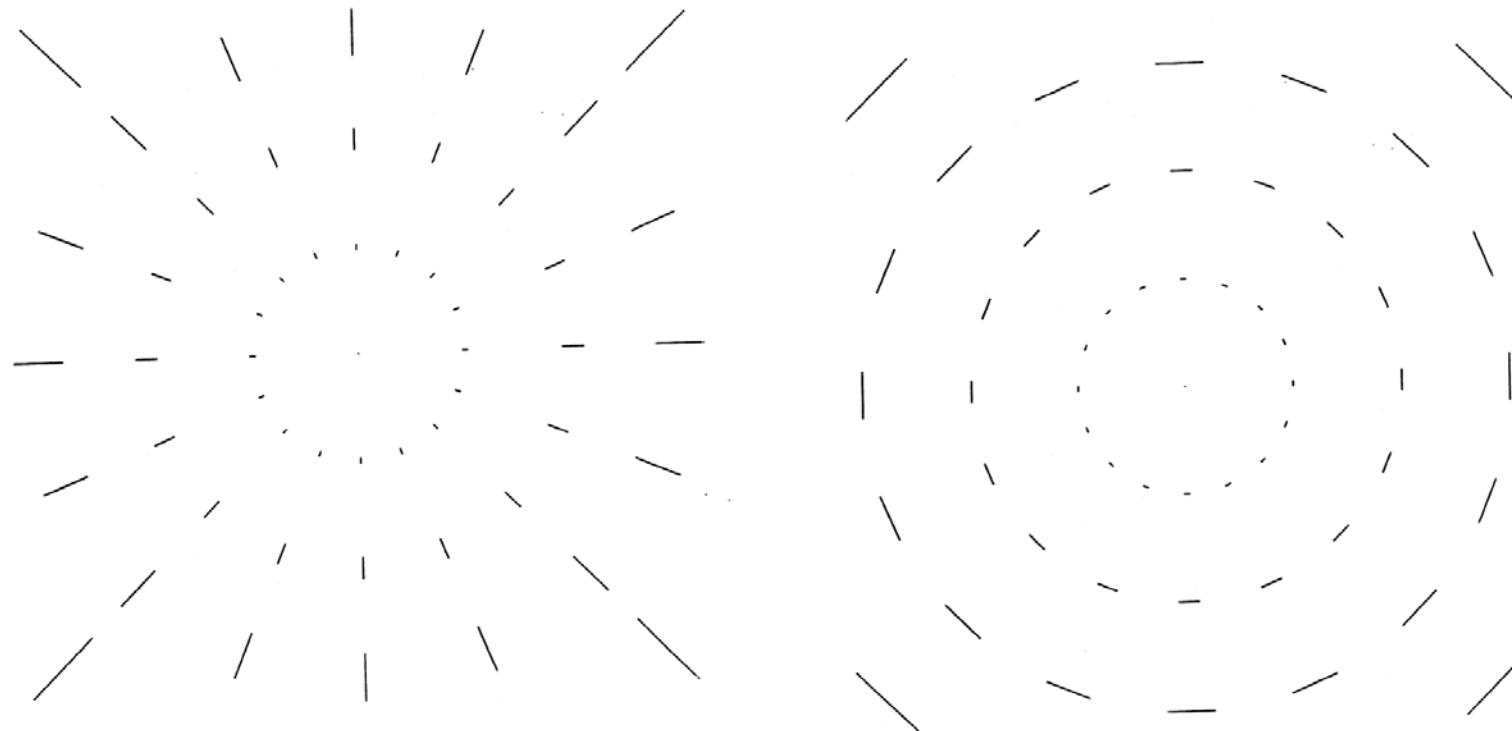
105



Prof. Jose Sasian
OPTI 518

Roland Shack's notes

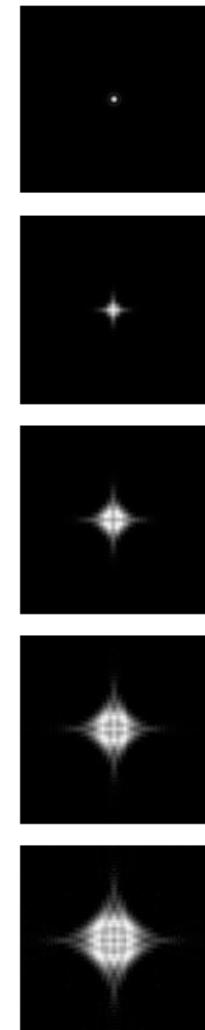
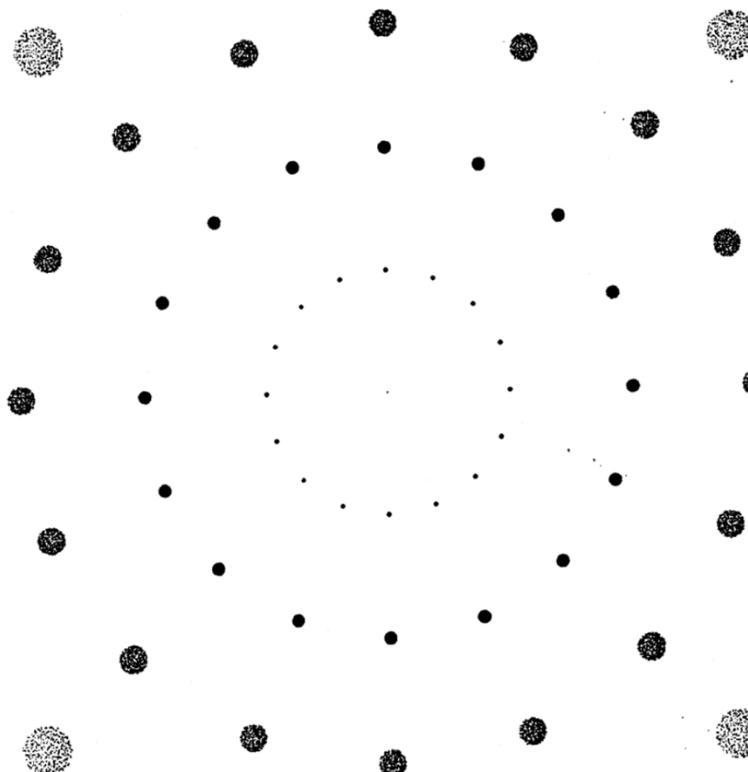
Quadratic (radial) Astigmatism



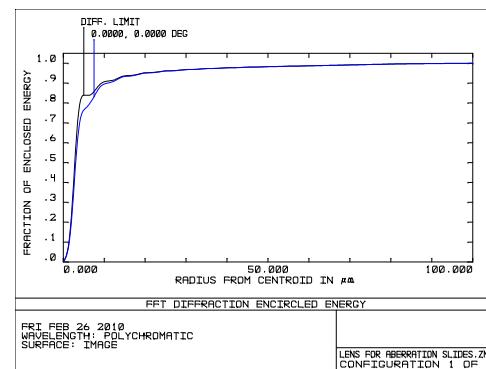
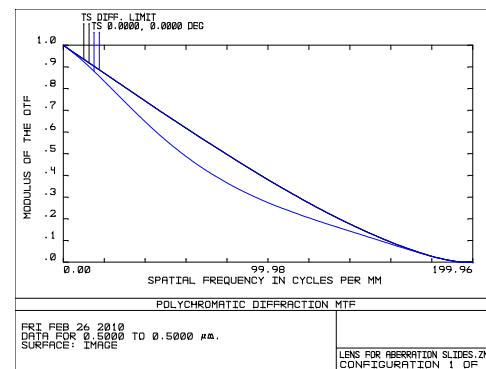
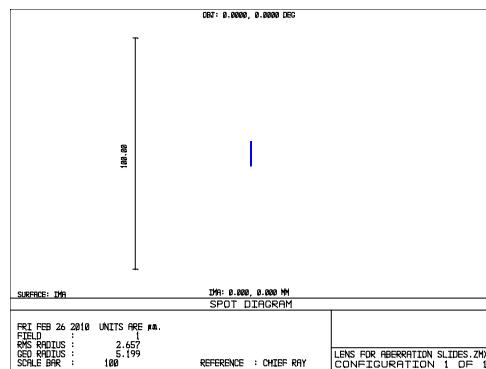
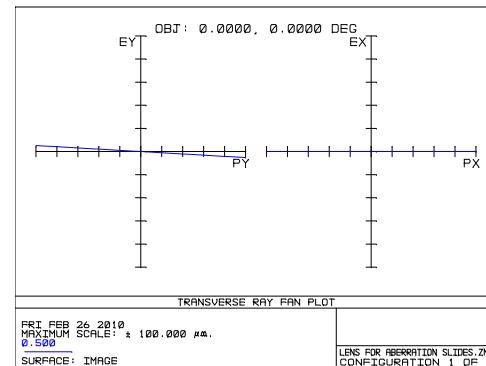
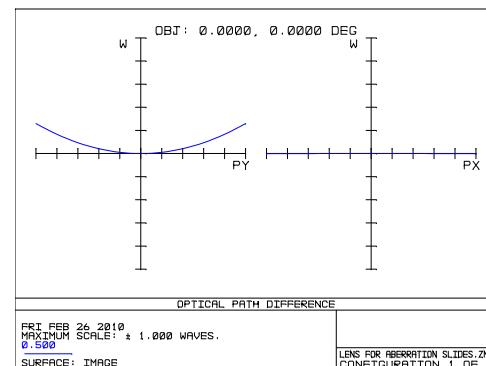
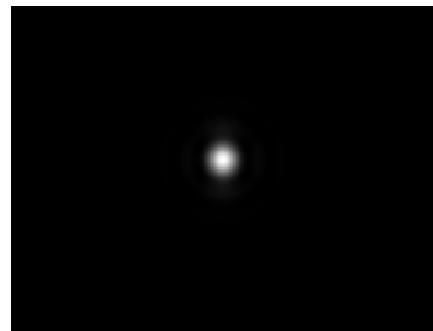
Prof. Jose Sasian
OPTI 518

Theoretical behavior

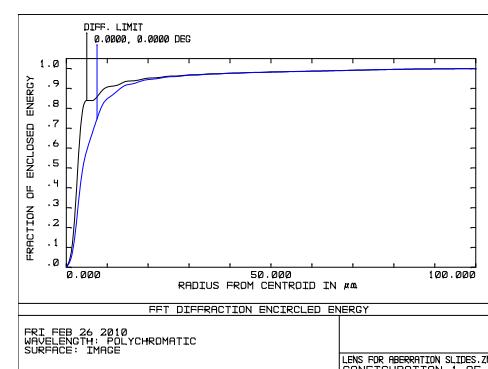
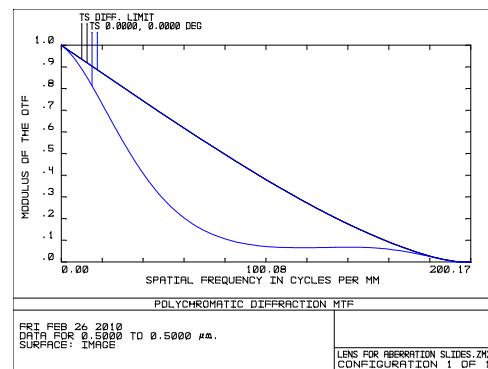
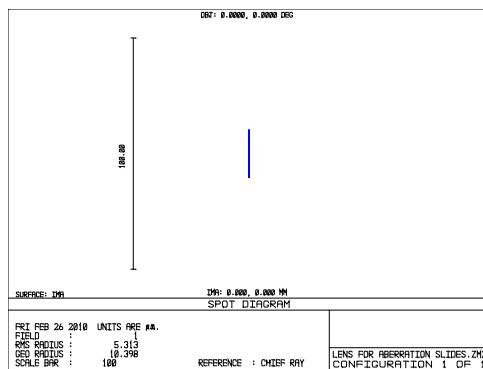
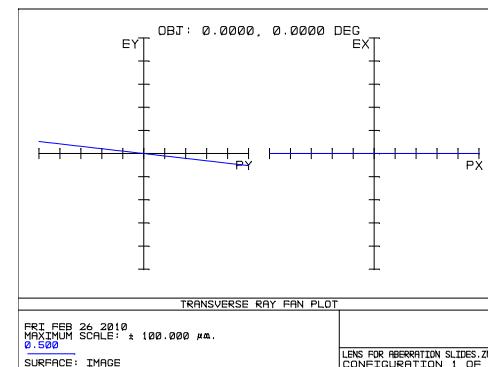
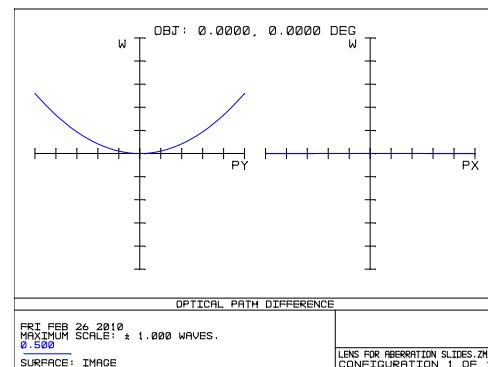
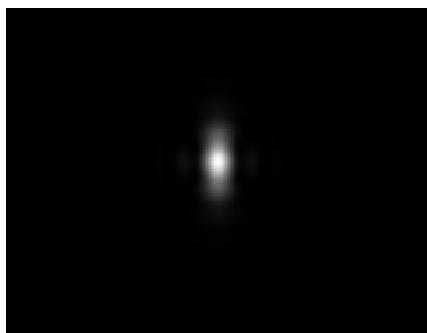
Medial focus



Astigmatism aberration 0.25 wave f/10; f=100 mm; wave=0.0005 mm

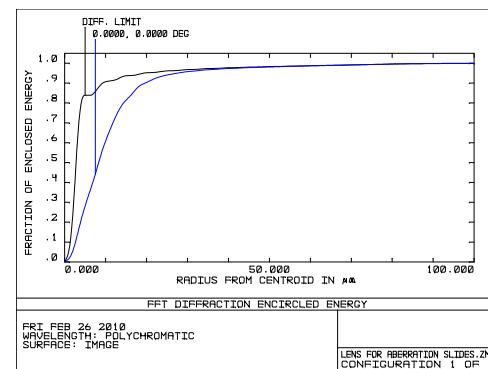
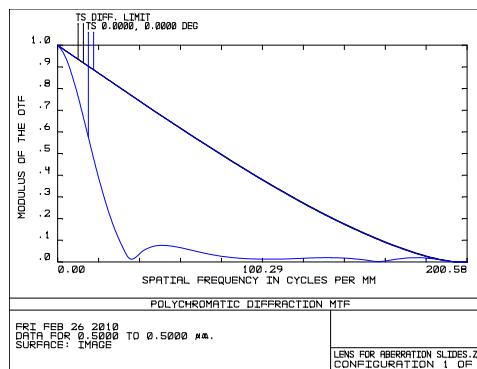
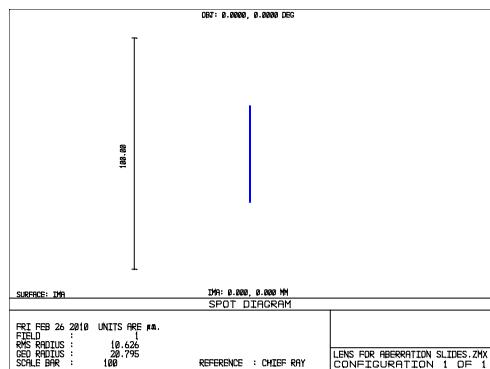
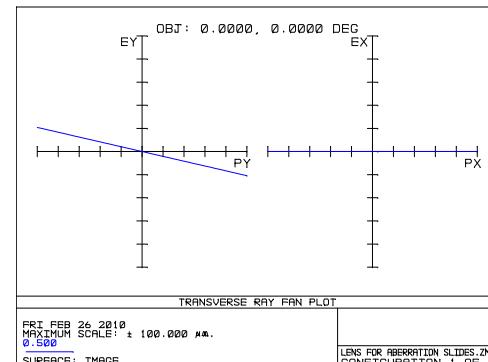
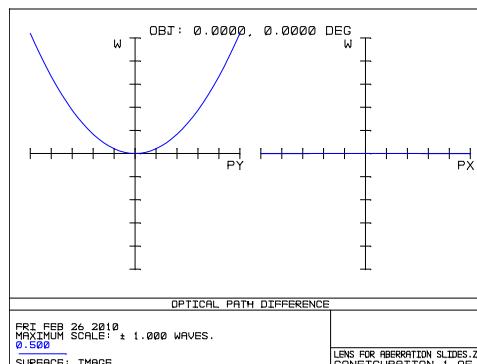
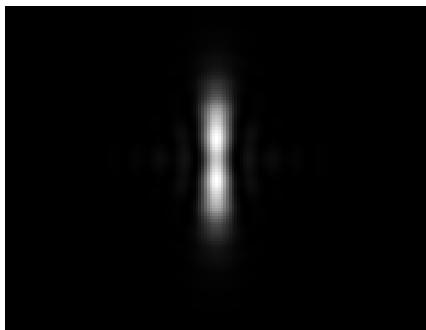


Astigmatism aberration 0.5 wave f/10; f=100 mm; wave=0.0005 mm



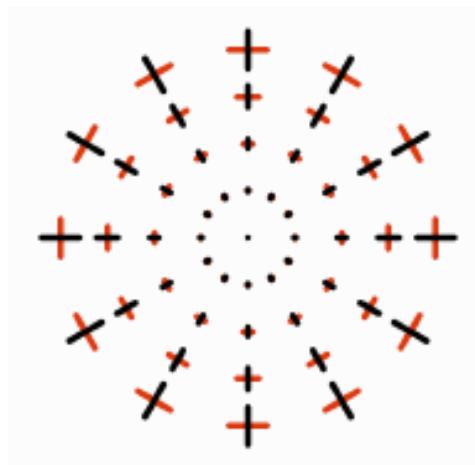
Astigmatism aberration 1.0 wave

f/10; f=100 mm; wave=0.0005 mm

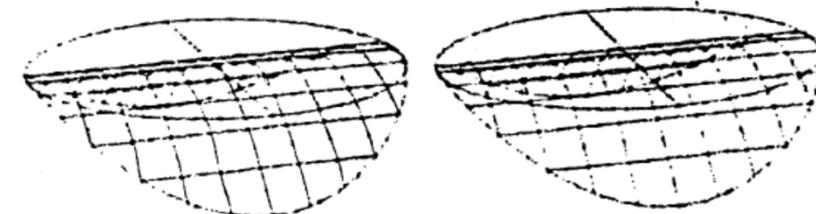
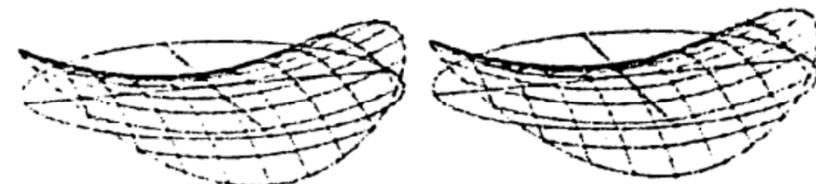
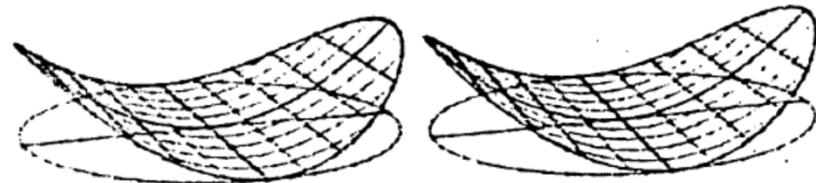


Astigmatism varies as the square of the field of view

$$W_{222} (\vec{H} \cdot \vec{\rho})^2$$



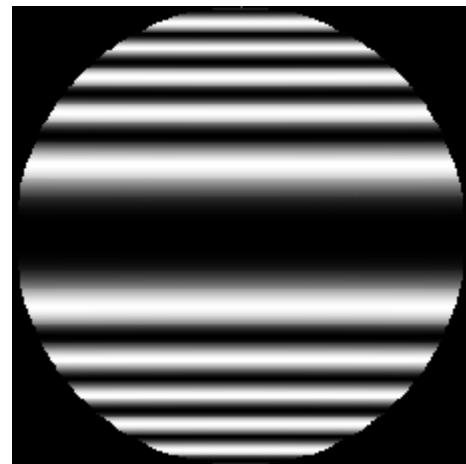
Astigmatism



Prof. Jose Sasian
OPTI 518

Roland Shack's notes

Interferometric representation



5 waves

Prof. Jose Sasian
OPTI 518

Cases of zero astigmatism aberration from a spherical surface

$$W_{222}(\vec{H} \cdot \vec{\rho})^2 \quad W_{222} = \frac{1}{2} S_{III} \quad S_{III} = -\sum \bar{A}^2 y \Delta \left(\frac{u}{n} \right)$$

$$y = 0$$

$$\bar{A} = 0$$

$$\Delta(u/n) = u'/n' - u/n = 0$$

y=0 the aperture is zero or the surface is at an image

Abar=0 surface is concentric with stop or pupils

u'/n-u/n=0 the conjugates are at the aplanatic points

Aplanatic means free from error;

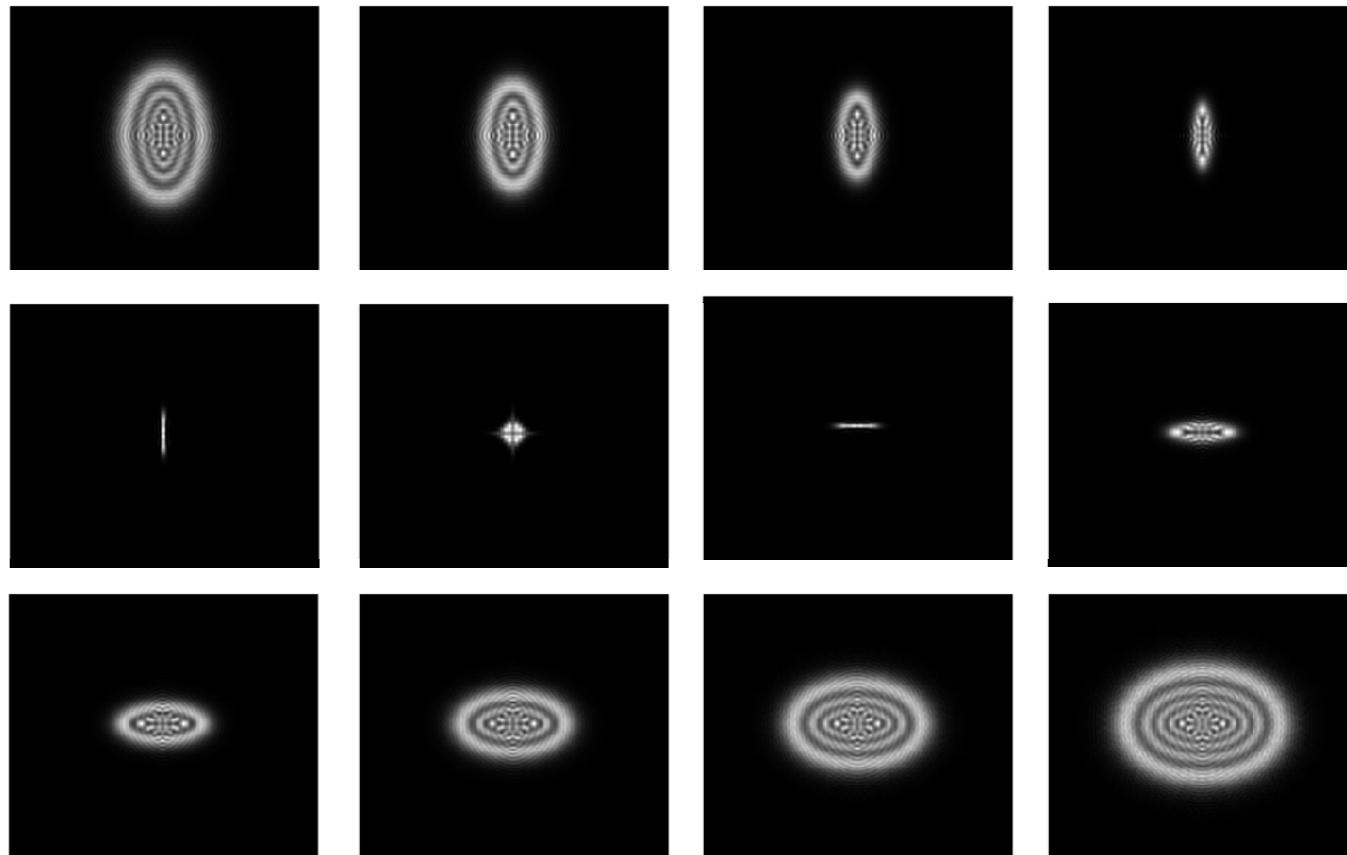
freedom from spherical aberration and coma.

Aplanatic spherical surface is also anastigmatic

Anastigmatic: free from spherical, coma and astigmatism

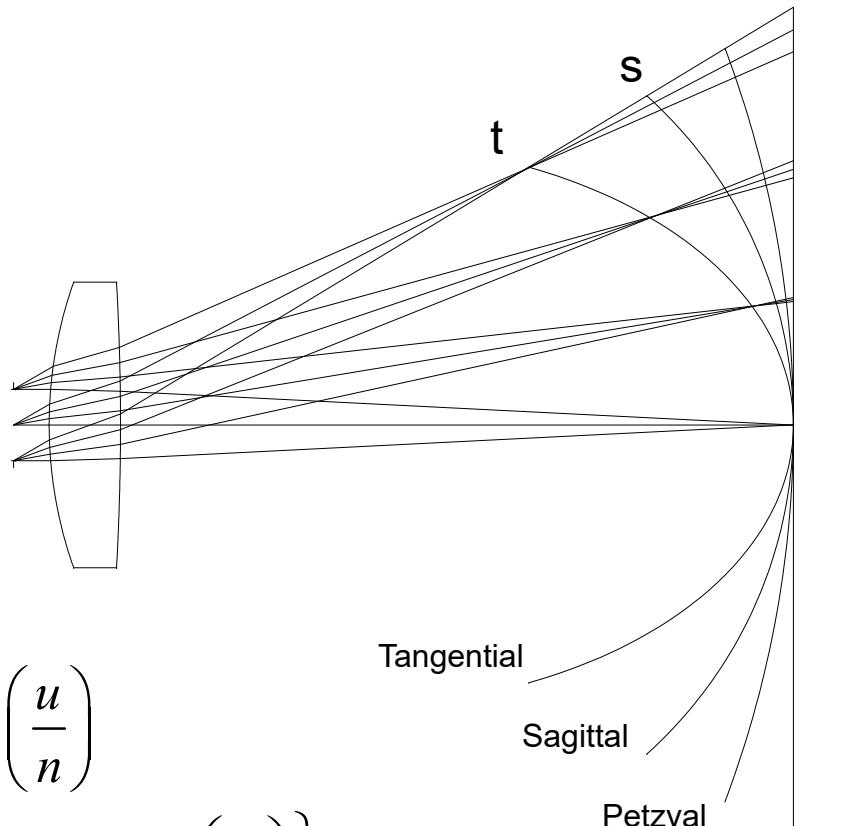


Two waves of astigmatism



Prof. Jose Sasian
OPTI 518

The field curves

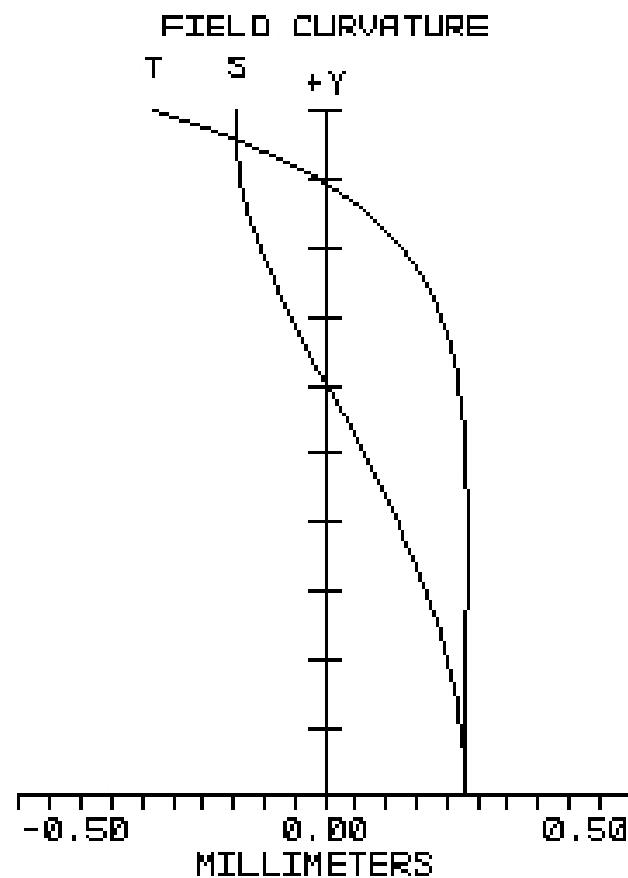


$$W_{222} = -\frac{1}{2} \sum \bar{A}^2 y \Delta \left(\frac{u}{n} \right)$$

$$W_{220} = -\frac{1}{4} \sum \left\{ \mathcal{K}^2 P + \bar{A}^2 y \Delta \left(\frac{u}{n} \right) \right\}$$

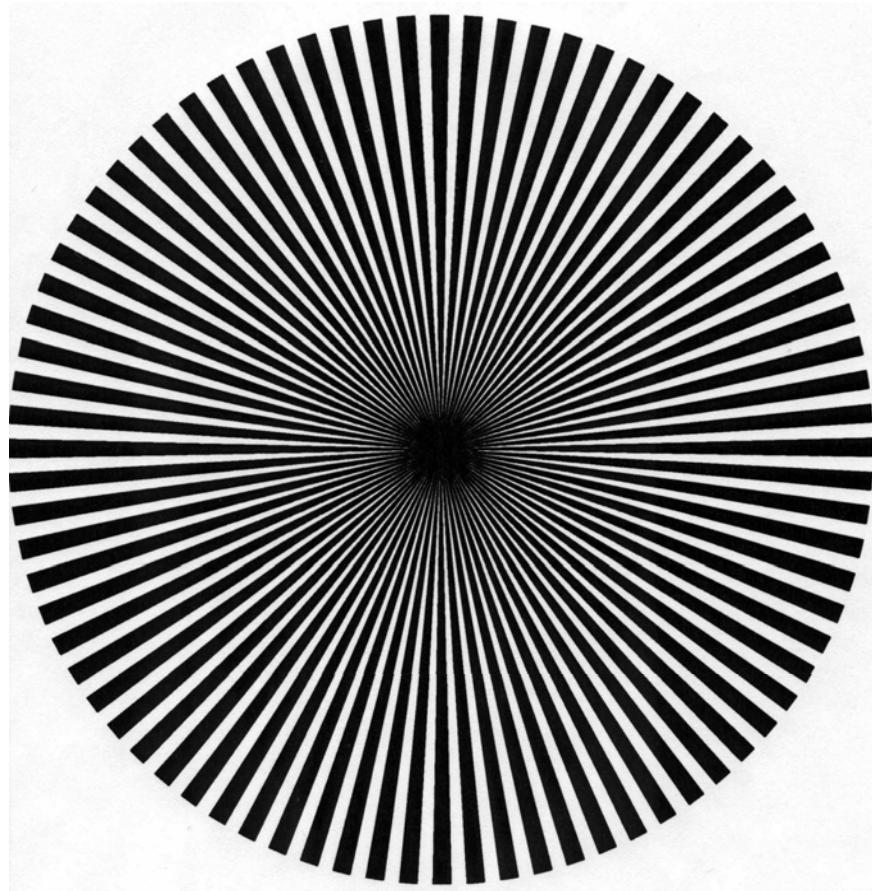
Prof. Jose Sasian
OPTI 518

Field curves by an optical design program



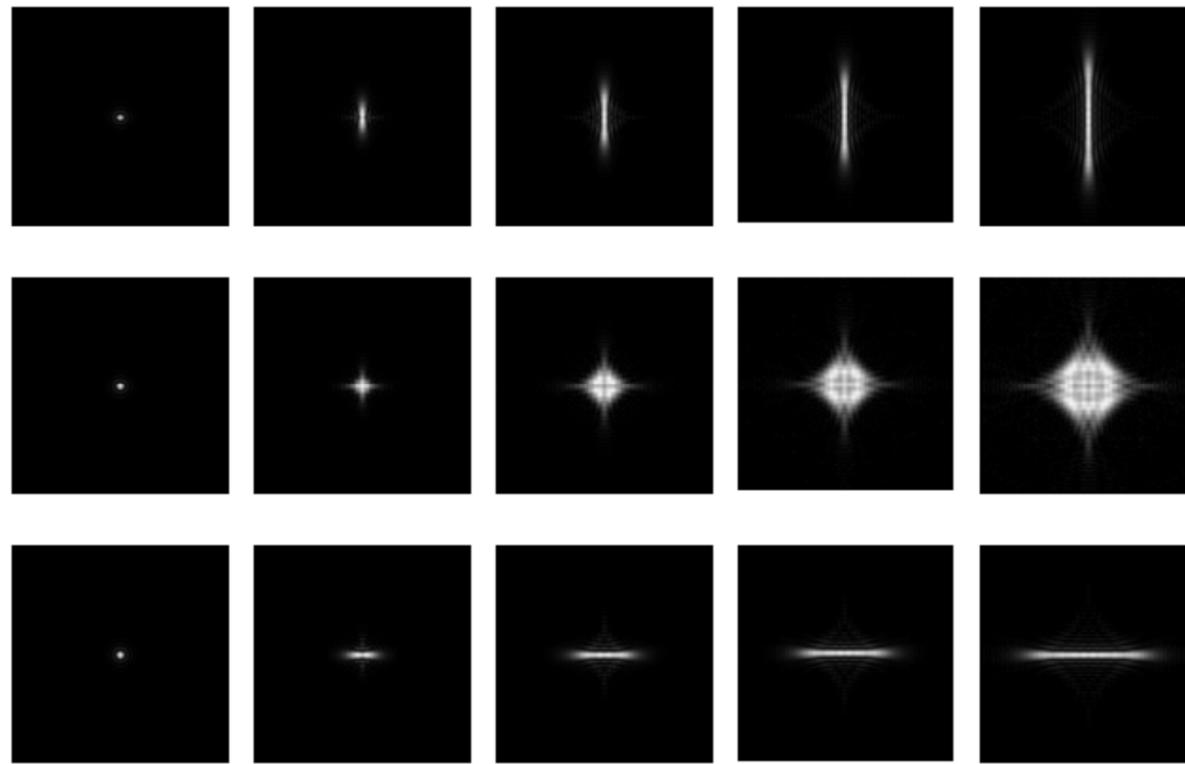
Prof. Jose Sasian
OPTI 518

Eye astigmatism



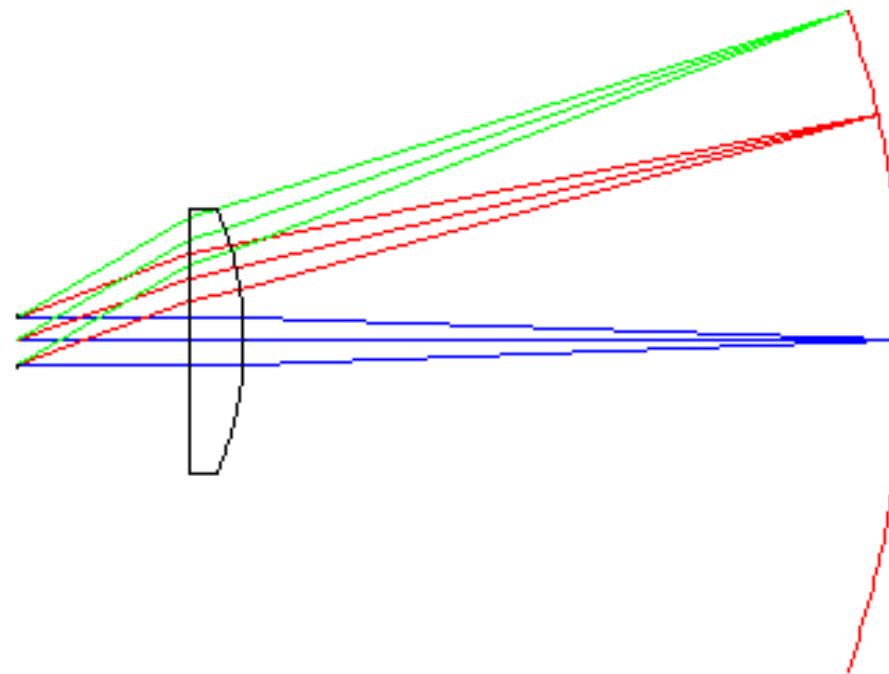
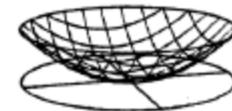
Prof. Jose Sasian
OPTI 518

Diffraction images



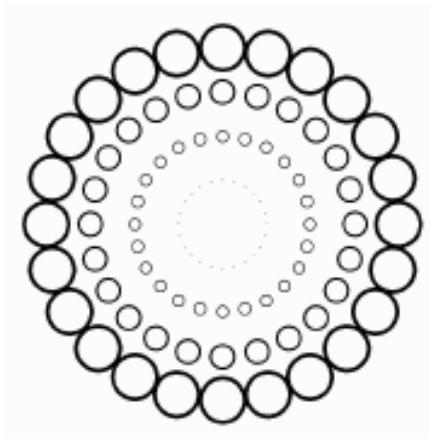
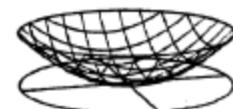
Field curvature

$$W_{220}(\vec{H} \cdot \vec{H})(\vec{\rho} \cdot \vec{\rho})$$

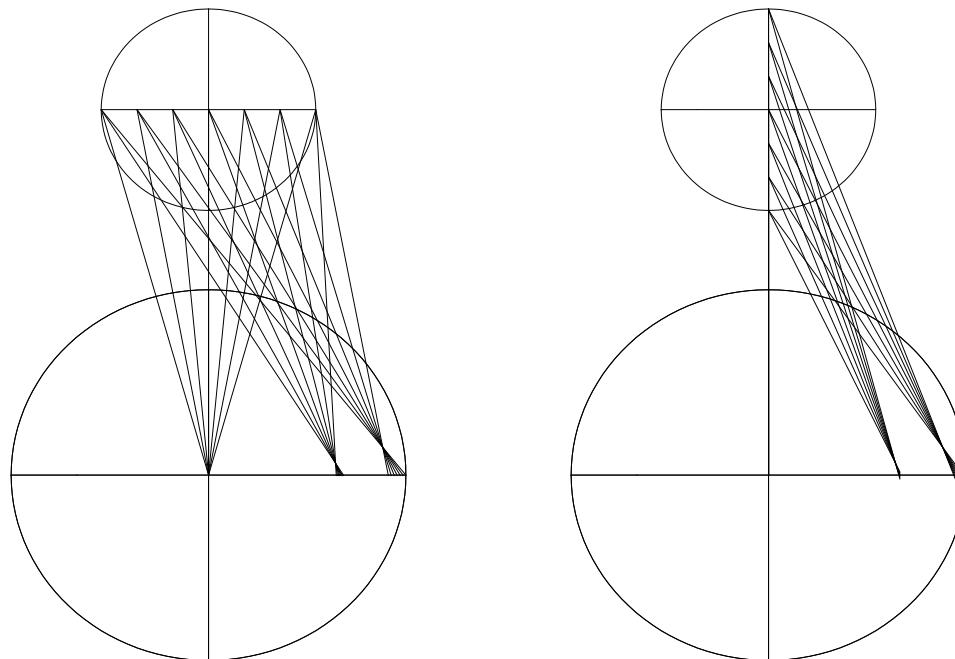


Field curvature varies as the square of the field of view

$$W_{220}(\vec{H} \cdot \vec{H})(\vec{\rho} \cdot \vec{\rho})$$



Meridional and sagittal ray fans



Prof. Jose Sasian
OPTI 518

Field curvature

$$W_{220} = -\frac{1}{4} \sum \left(\mathcal{K}^2 P + \bar{A}^2 \Delta \left\{ \frac{u}{n} \right\} y \right) \quad P = C \cdot \Delta \left(\frac{1}{n} \right)$$

Petzval sum:

$$\frac{1}{n'_k \rho'_k} - \frac{1}{n_1 \rho_1} = - \sum_{i=1}^k \frac{n' - n}{n' n r}$$

For a system of thin lenses
In air:

$$\frac{1}{\rho'_k} = - \sum_{i=1}^k \frac{\phi_i}{n_i}$$

Petzval field curvature interpretation

For a single lens

$$-\frac{1}{\rho_{Petzval}} = \sum_{i=1}^2 \frac{n'-n}{n'nr} = \frac{n'-1}{n'r_1} - \frac{n'-1}{n'r_2} = \frac{n'-1}{n'} \left(\frac{1}{r_1} - \frac{1}{r_2} \right)$$

Multiply by

$$\frac{h^2}{2}$$

or

$$-\frac{h^2}{2\rho_{Petzval}} = \frac{n'-1}{n'} \left(\frac{1}{r_1} - \frac{1}{r_2} \right) \frac{h^2}{2} = \frac{n'-1}{n'} t$$

h is a given height; t is the lens sag or thickness at height h

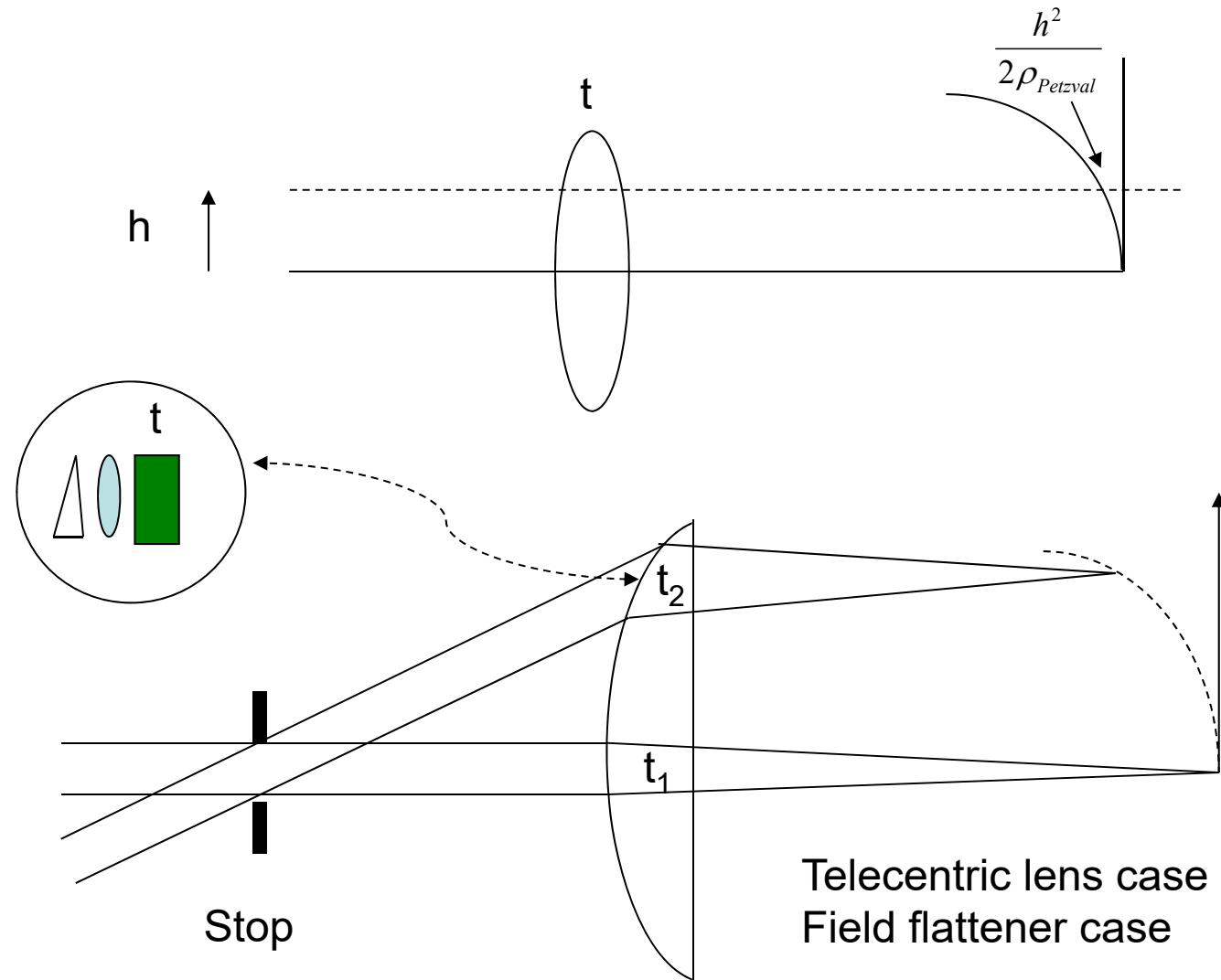
Then $\frac{h^2}{2\rho_{Petzval}}$

Is the sag of the Petzval field curvature and $\frac{n'-1}{n'} t$

is the image displacement by a parallel plate of thickness t .

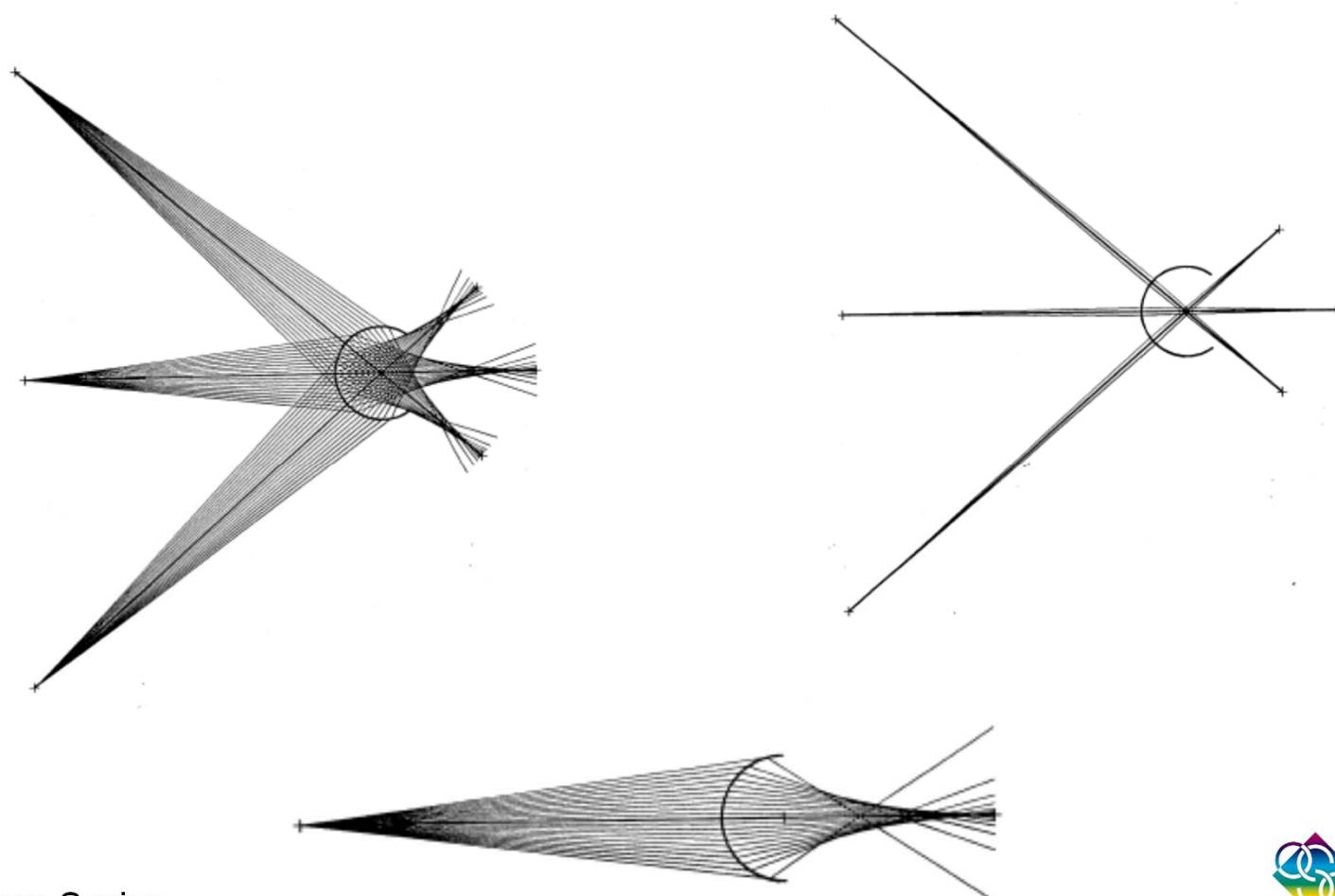
Thus Petzval field curvature can be interpreted as the image shift due to a “parallel plate” of varying thickness t .

Petzval field curvature interpretation



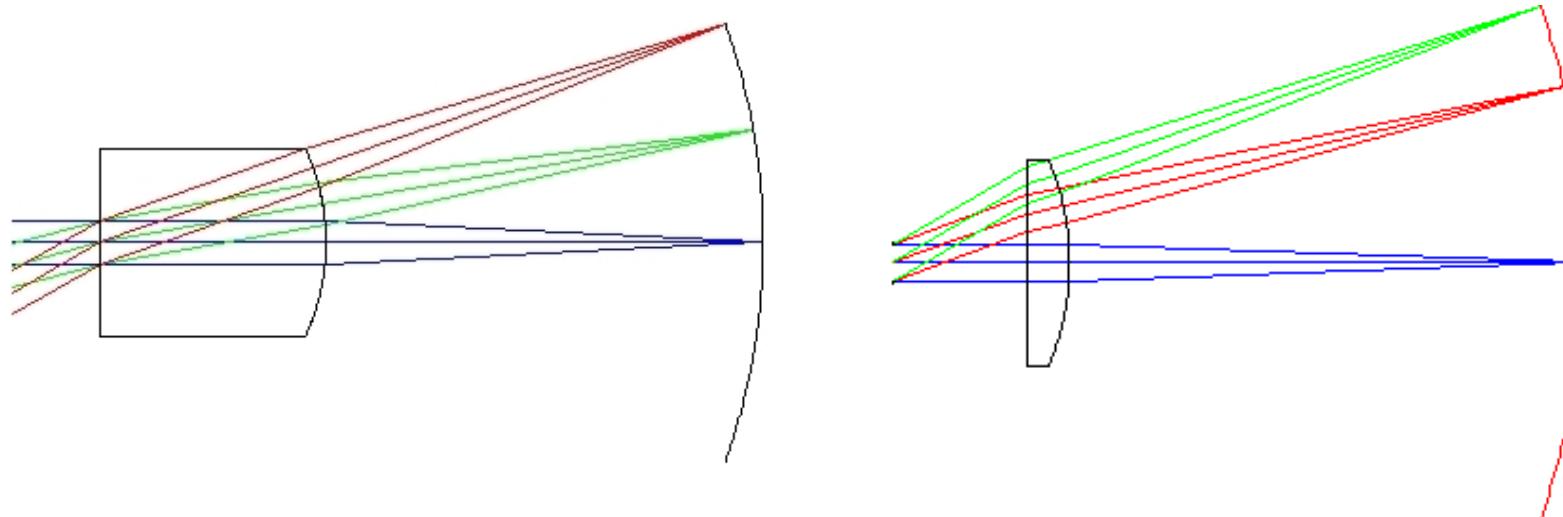
Telecentric lens case
Field flattener case

Petzval field curvature: Stop at center of curvature



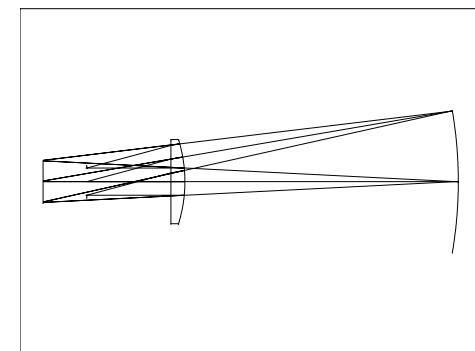
Prof. Jose Sasian
OPTI 518

Petzval radius for a lens

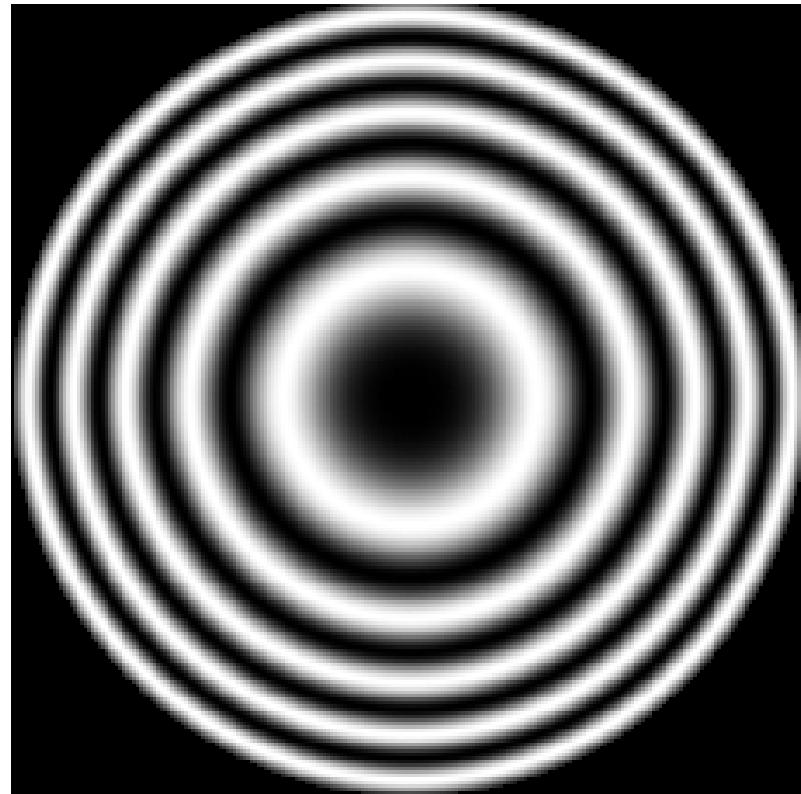


$$\frac{1}{\rho'_k} = - \sum \frac{\phi}{n}$$

R=t=51.852239
F=100 mm
Petzval radius=151.852239=nf
Bk7 glass



Interferometric representation



5 waves

Field curves vertex curvature

$$\Delta z = -2 \frac{W_{020}}{n' u'^2} = -2 n' \frac{\bar{y}_I^2}{\mathcal{K}^2} W_{020}$$

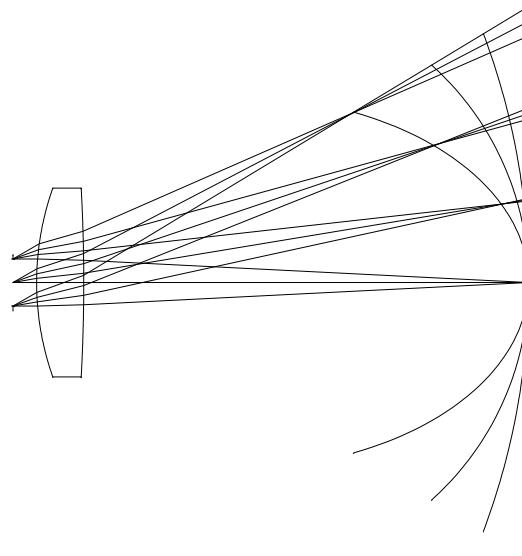
$$\frac{2\Delta z}{\bar{y}_I^2} = -4 n' \frac{1}{\mathcal{K}^2} W_{020}$$

$$C_t = -4 \frac{n'}{\mathcal{K}^2} \left(W_{220P} + \frac{3}{2} W_{222} \right)$$

$$C_m = -4 \frac{n'}{\mathcal{K}^2} (W_{220P} + W_{222})$$

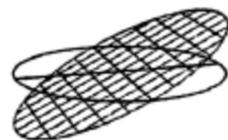
$$C_s = -4 \frac{n'}{\mathcal{K}^2} \left(W_{220P} + \frac{1}{2} W_{222} \right)$$

$$C_P = -4 \frac{n'}{\mathcal{K}^2} W_{220P}$$



Distortion

$$W_{311}(\vec{H} \cdot \vec{H})(\vec{H} \cdot \vec{\rho})$$



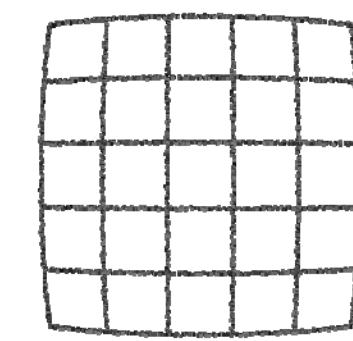
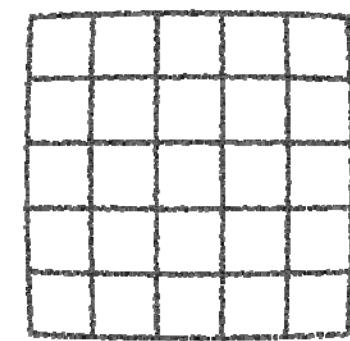
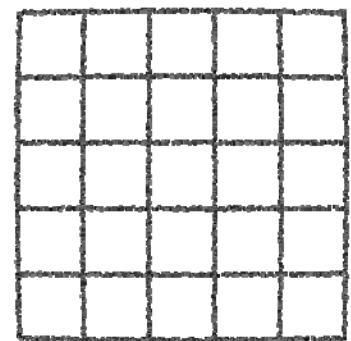
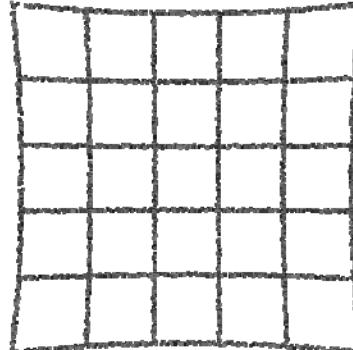
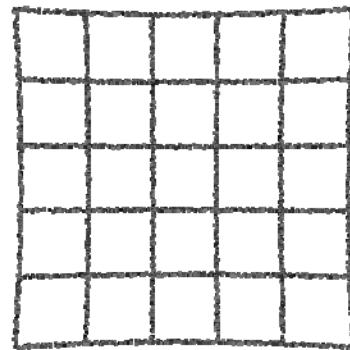
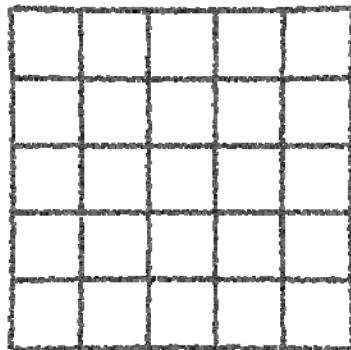
$$W_{311} = \frac{1}{2} S_V$$

$$S_V = -\sum \frac{\bar{A}}{A} \left[\mathcal{K}^2 P + \bar{A}^2 y \Delta \left(\frac{u}{n} \right) \right]$$

$$S_V = -\sum \bar{A} \left[\bar{A}^2 \Delta \left(\frac{1}{n^2} \right) y - (\mathcal{K} + \bar{A}y) \bar{y} P \right]$$

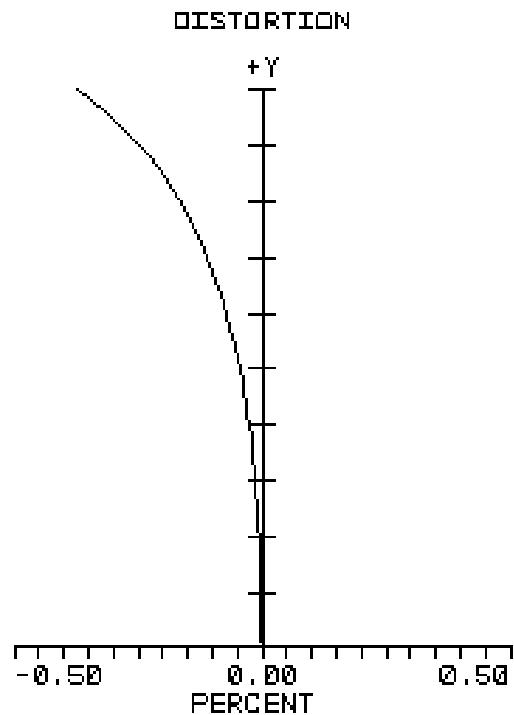


Distortion



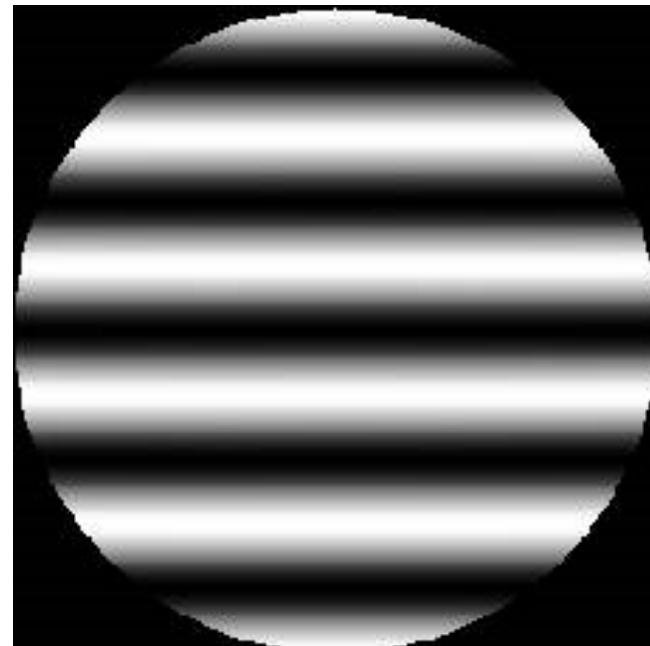
2.5%, 5% and 10%

Distortion



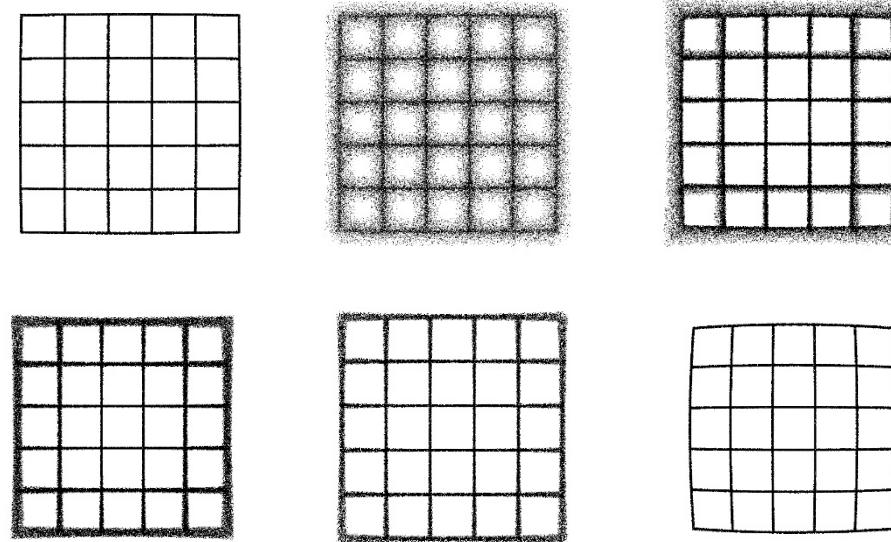
$$Distortion = \frac{Y - \bar{y}}{\bar{y}} \cdot 100$$

Interferometric representation



Prof. Jose Sasian
OPTI 518

Geometrical imaging with aberrations



Spot diagram concept applied to
an extended object

Parity of the aberrations

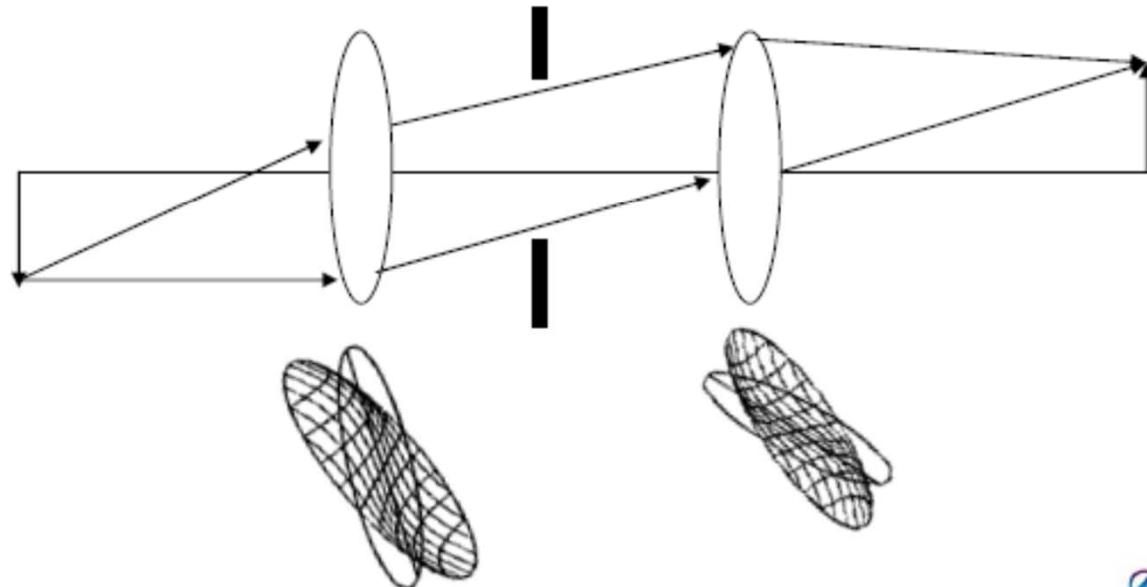
The aberrations can be classified as even and odd aberrations. Spherical aberration, astigmatism, field curvature, and longitudinal color are even aberrations. Coma, distortion, and transverse color are odd aberrations. The parity is found by observation of the algebraic power's parity of the field and aperture vectors in the aberration coefficients.

The odd aberrations have the important property that in a symmetrical system they Cancel (fourth-order), each half contributes the same amount of aberration but with opposite algebraic sign. The symmetry is about the aperture stop. In comparison in a symmetrical system the even aberrations from each half of the system add, rather than cancel

Aberrations and symmetry

$$\begin{aligned}W(H, \rho, \theta) = & W_{200}H^2 + W_{020}\rho^2 + W_{111}H\rho\cos\theta + \\& + W_{040}\rho^4 + W_{131}H\rho^3\cos\theta + W_{222}H^2\rho^2\cos^2\theta + \\& + W_{220}H^2\rho^2 + W_{311}H^3\rho\cos\theta + W_{400}H^4 + \\& + \dots\end{aligned}$$

- Coma is an odd aberration with respect to the stop
- Natural stop position to cancel coma by symmetry



Summary

- Discussion of the primary aberrations
- Use of several types of plots
- Main point is to gain understanding and familiarity
- Must be able to recognize the aberrations under a variety of representations.
- Must be able to appreciate how the ideal image degrades in the presence of aberration