

Monday, March 24, 2014

CHAPTER 15

Kinematics of Rigid Bodies

Chapter Outline

1. Introduction

2. Translation

3. Rotation About a Fixed Axis

4. General Plane Motion

- ✓ Absolute and Relative Velocity
- ✓ Instantaneous Center of Rotation
- ✓ Absolute and Relative Acceleration
- ✓ Analysis of Plane Motion in Terms of a Parameter

5. Rate of Change wrt a Rotating Frame

6. Coriolis Acceleration

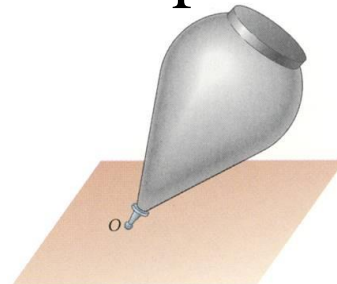
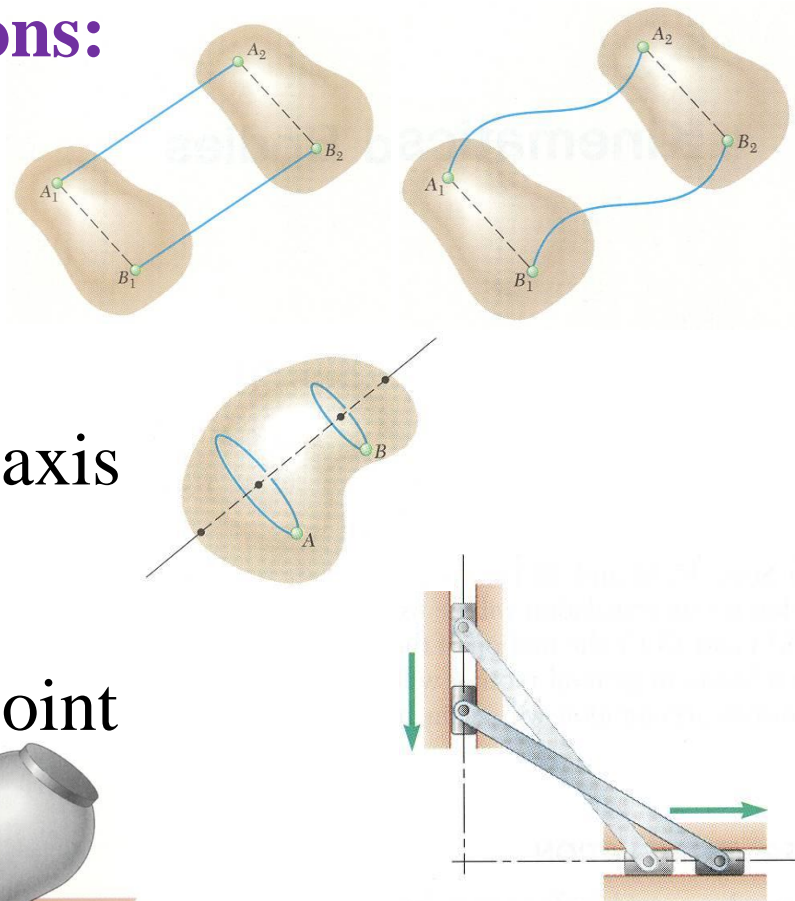
Introduction

Kinematics of rigid bodies (RB): relations between time and the positions, velocities, and accelerations of the particles forming a rigid body.

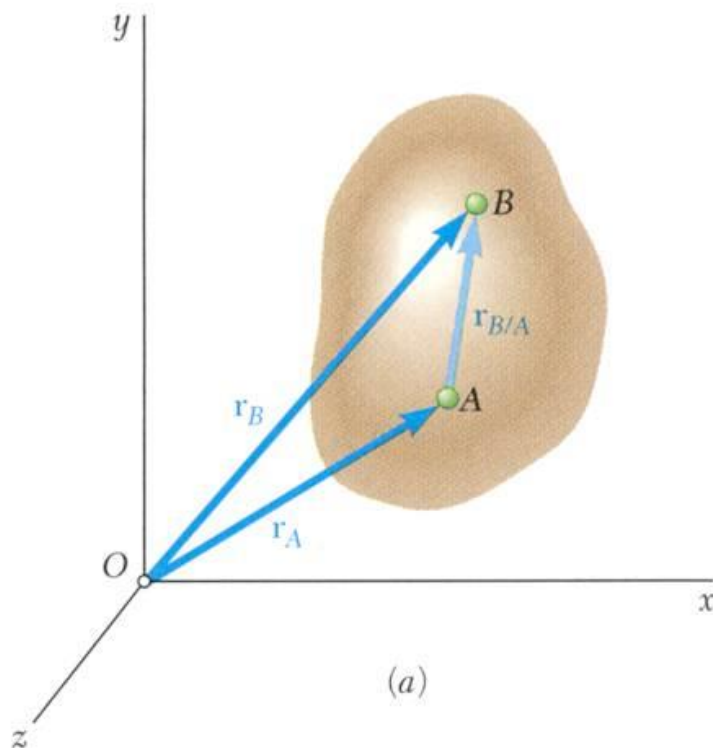
Introduction

Classification of RB motions:

- Translation:
 - rectilinear translation
 - curvilinear translation
- Rotation about a fixed axis
- General plane motion
- Motion about a fixed point
- General motion



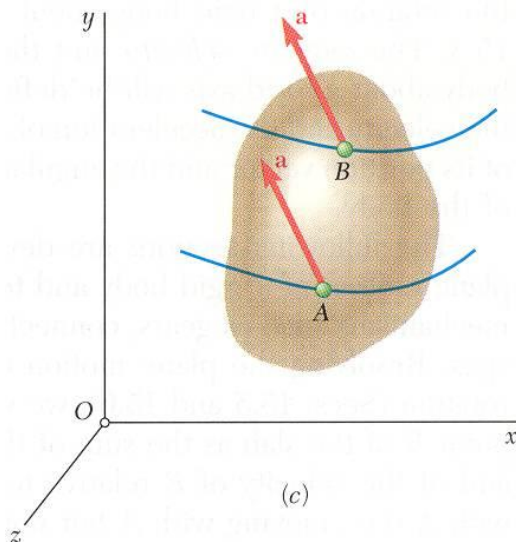
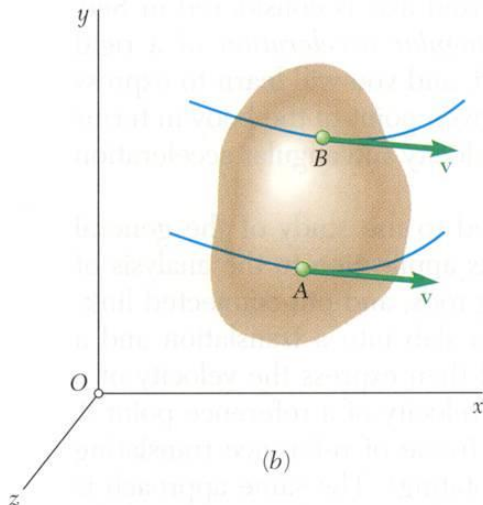
Translation



- **RB in translation:**
 - Direction of any straight line inside body is constant
 - All particles forming RB move in parallel lines.
- For any two particles in the body,

$$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$$

Translation



- Differentiating wrt time,

$$\dot{\vec{r}}_B = \dot{\vec{r}}_A + \dot{\vec{r}}_{B/A} = \dot{\vec{r}}_A$$

$$\vec{v}_B = \vec{v}_A$$

All particles have same velocity.

- Differentiating wrt time again,

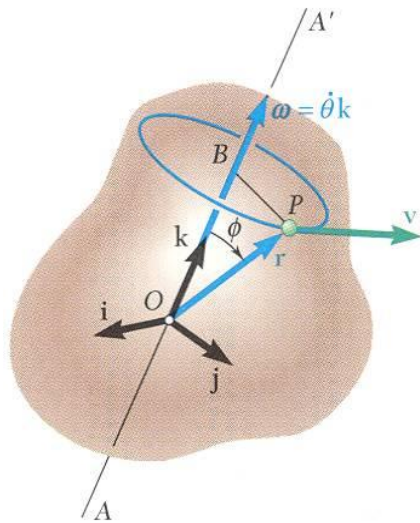
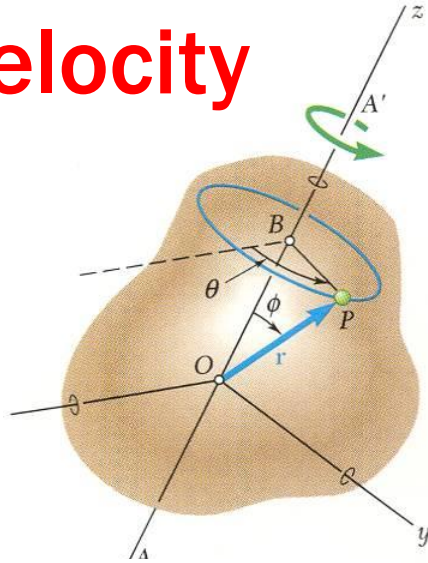
$$\ddot{\vec{r}}_B = \ddot{\vec{r}}_A + \ddot{\vec{r}}_{B/A} = \ddot{\vec{r}}_A$$

$$\vec{a}_B = \vec{a}_A$$

All particles have same acceleration.

Rotation About a Fixed Axis

Velocity



- Velocity vector $\vec{v} = d\vec{r}/dt$ of particle P is tangent to the path with magnitude $v = ds/dt$
 $\Delta s = (BP)\Delta\theta = (r \sin\phi)\Delta\theta$

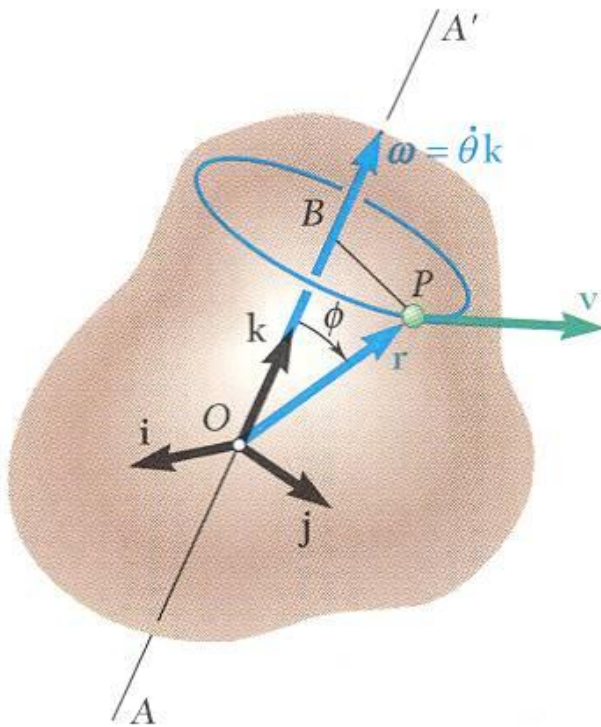
$$v = \frac{ds}{dt} = \lim_{\Delta t \rightarrow 0} (r \sin\phi) \frac{\Delta\theta}{\Delta t} = r\dot{\theta} \sin\phi$$

$$\vec{v} = \frac{d\vec{r}}{dt} = \vec{\omega} \times \vec{r}$$

$$\vec{\omega} = \omega\vec{k} = \dot{\theta}\vec{k} = \text{angular velocity}$$

Rotation About a Fixed Axis

Acceleration ■ Differentiating to get,



$$\vec{a} = \frac{d\vec{v}}{dt} = \frac{d}{dt}(\vec{\omega} \times \vec{r}) = \frac{d\vec{\omega}}{dt} \times \vec{r} + \vec{\omega} \times \frac{d\vec{r}}{dt}$$

$$= \frac{d\vec{\omega}}{dt} \times \vec{r} + \vec{\omega} \times \vec{v}$$

$$\frac{d\vec{\omega}}{dt} = \vec{\alpha} = \text{angular acceleration}$$

$$= \alpha \vec{k} = \dot{\omega} \vec{k} = \ddot{\theta} \vec{k}$$

$$\vec{a} = \vec{\alpha} \times \vec{r} + \vec{\omega} \times \vec{\omega} \times \vec{r}$$

$\vec{\alpha} \times \vec{r}$ = tangential acceleration component

$\vec{\omega} \times \vec{\omega} \times \vec{r}$ = radial acceleration component

Rotation About a Fixed Axis

Representative Slab

- Velocity of any point P of slab,

$$\vec{v} = \vec{\omega} \times \vec{r} = \omega \vec{k} \times \vec{r} \quad v = r\omega$$

- Acceleration of point P of slab,

$$\vec{a} = \vec{\alpha} \times \vec{r} + \vec{\omega} \times \vec{\omega} \times \vec{r} = \alpha \vec{k} \times \vec{r} - \omega^2 \vec{r}$$

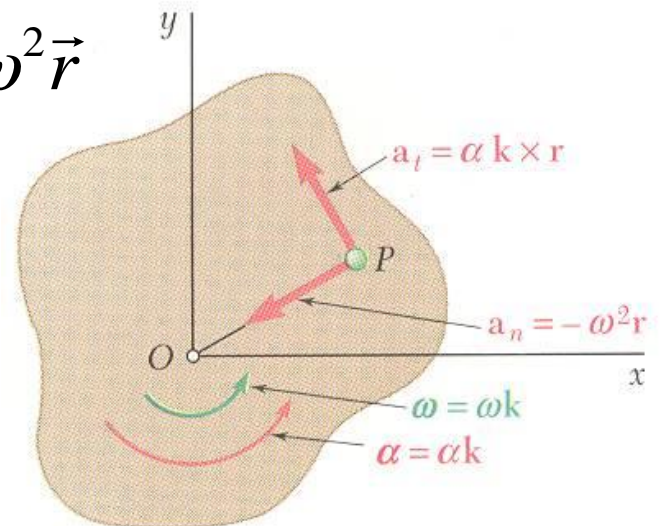
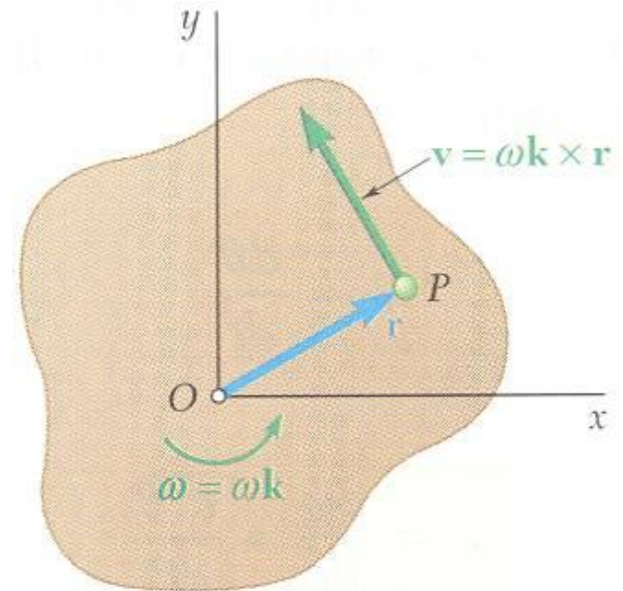
- Tangential & normal components of acceleration ,

$$\vec{a}_t = \alpha \vec{k} \times \vec{r}$$

$$a_t = r\alpha$$

$$\vec{a}_n = -\omega^2 \vec{r}$$

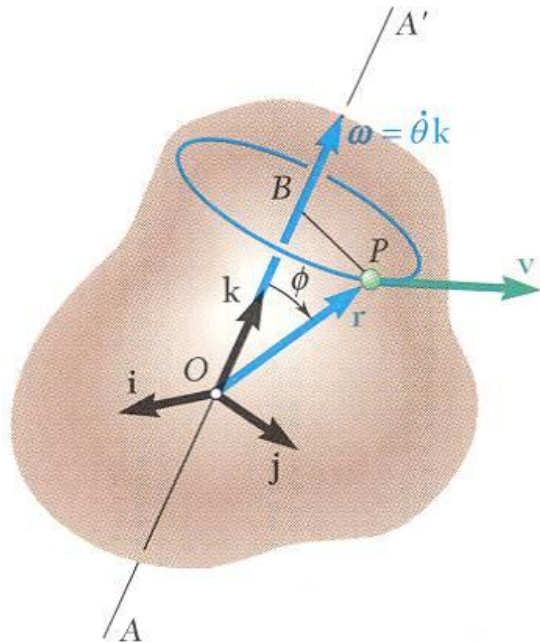
$$a_n = r\omega^2$$



Equations Defining Rotation of a RB About a Fixed Axis

$$\omega = \frac{d\theta}{dt} \quad \text{or} \quad dt = \frac{d\theta}{\omega}$$

$$\alpha = \frac{d\omega}{dt} = \frac{d^2\theta}{dt^2} = \omega \frac{d\omega}{d\theta}$$



- *Uniform Rotation, $\alpha = 0$:*

$$\theta = \theta_0 + \omega t$$

- *Uniformly Accelerated Rotation, $\alpha = \text{constant}$:*

$$\omega = \omega_0 + \alpha t$$

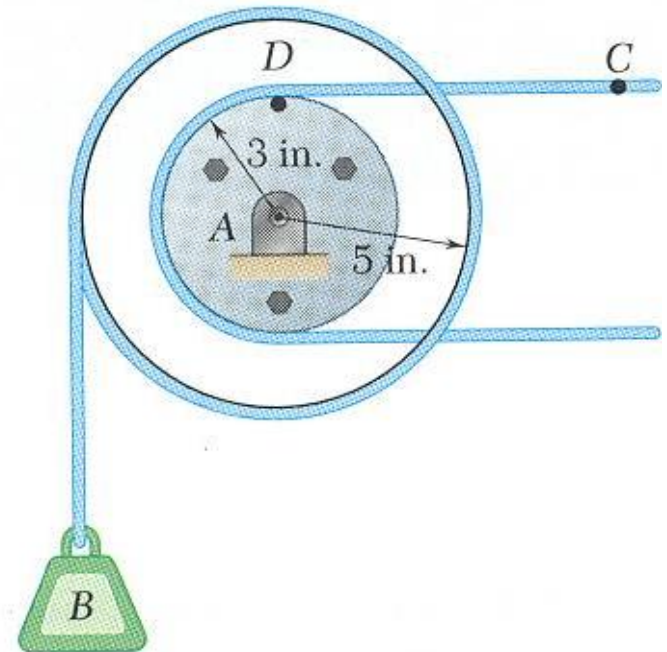
$$\theta = \theta_0 + \omega_0 t + \frac{1}{2} \alpha t^2$$

$$\omega^2 = \omega_0^2 + 2\alpha(\theta - \theta_0)$$

Sample Problem 5.1

Cable C has a constant acceleration of 9 in/s^2 and an initial velocity of 12 in/s , both directed to the right. Determine:

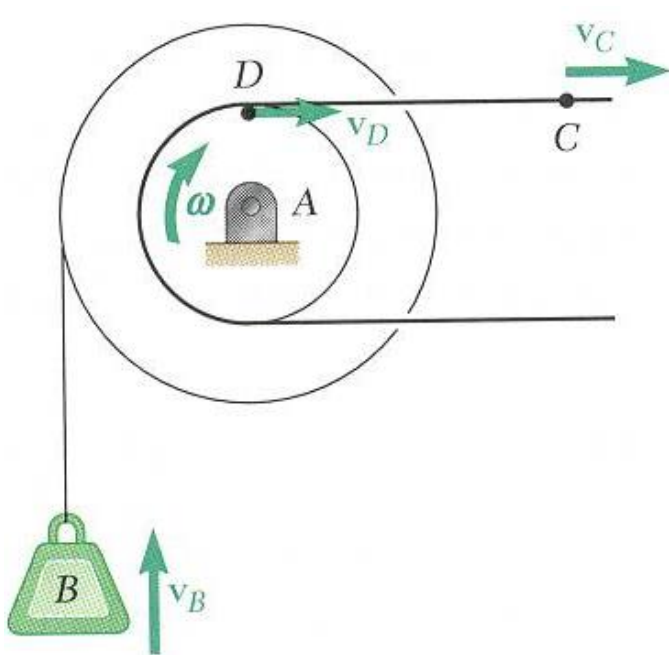
- number of revolutions of pulley in 2 s ,
- velocity & change in position of load B after 2 s
- acceleration of point D on the rim of the inner pulley at $t = 0$.



Sample Problem 5.1

Solution:

- Tangential velocity & acceleration of D are equal to velocity & acceleration of C .



$$(\vec{v}_D)_0 = (\vec{v}_C)_0 = 12 \text{ in./s} \rightarrow$$

$$(v_D)_0 = r\omega_0$$

$$\omega_0 = \frac{(v_D)_0}{r} = \frac{12}{3} = 4 \text{ rad/s}$$

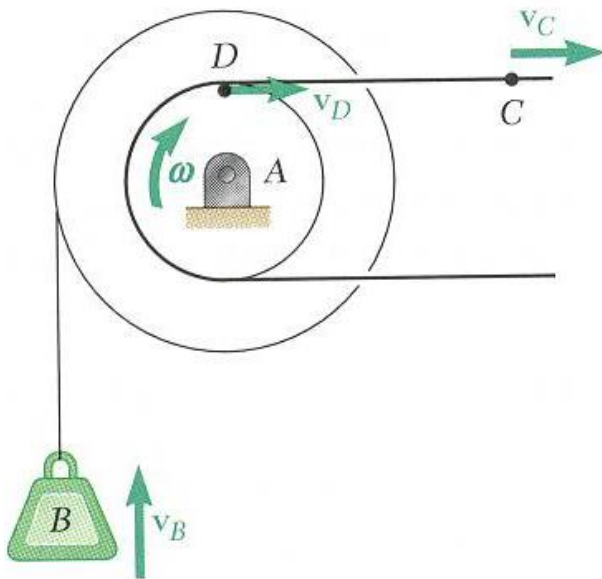
$$(\vec{a}_D)_t = \vec{a}_C = 9 \text{ in./s} \rightarrow$$

$$(a_D)_t = r\alpha$$

$$\alpha = \frac{(a_D)_t}{r} = \frac{9}{3} = 3 \text{ rad/s}^2$$

Sample Problem 5.1

- Uniformly accelerated rotation: determine velocity & angular position of pulley after 2 s.



$$\omega = \omega_0 + \alpha t = 4 \text{ rad/s} + (3 \text{ rad/s}^2)(2 \text{ s}) = 10 \text{ rad/s}$$

$$\theta = \omega_0 t + \frac{1}{2} \alpha t^2$$

$$= (4 \text{ rad/s})(2 \text{ s}) + \frac{1}{2} (3 \text{ rad/s}^2)(2 \text{ s})^2$$

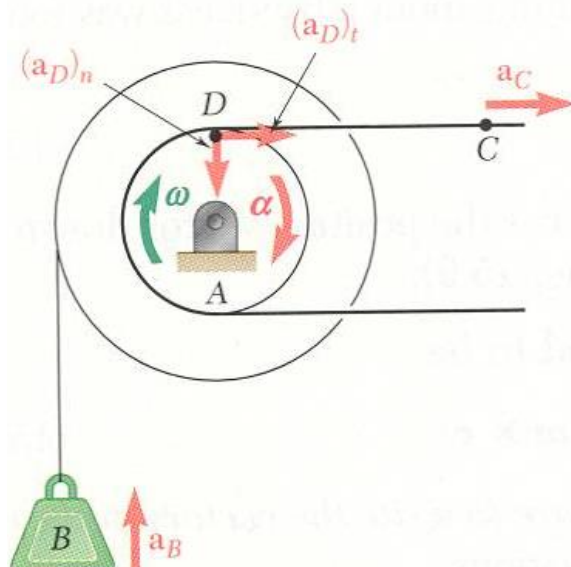
$$= 14 \text{ rad}$$

$$N = (14 \text{ rad}) \left(\frac{1 \text{ rev}}{2\pi \text{ rad}} \right) = \text{number of revs} = 2.23 \text{ rev}$$

$$v_B = r\omega = (5 \text{ in.})(10 \text{ rad/s}) = 50 \text{ in/s (upward)}$$

$$\Delta y_B = r\theta = (5 \text{ in.})(14 \text{ rad}) = 70 \text{ in}$$

Sample Problem 15.1



- Initial tangential & normal acceleration components of D .

$$(\vec{a}_D)_t = \vec{a}_C = 9 \text{ in./s} \rightarrow$$

$$(a_D)_n = r_D \omega_0^2 = (3 \text{ in.})(4 \text{ rad/s})^2 = 48 \text{ in./s}^2 \text{ (downward)}$$

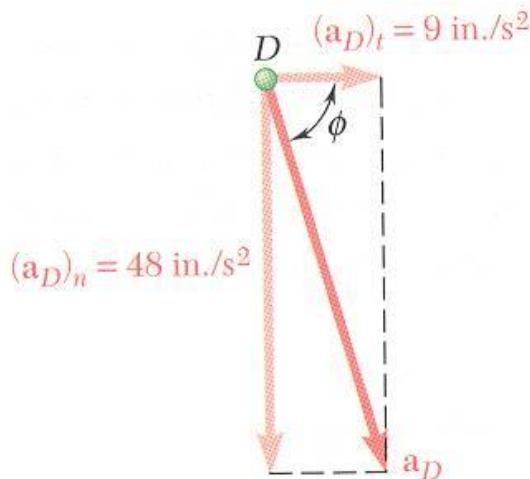
Magnitude & direction of total acceleration,

$$a_D = \sqrt{(a_D)_t^2 + (a_D)_n^2}$$

$$= \sqrt{9^2 + 48^2} = 48.8 \text{ in./s}^2$$

$$\tan \phi = \frac{(a_D)_n}{(a_D)_t} = \frac{48}{9} \quad \phi = 79.4^\circ$$

Dr. Mohammad Suliman Abuhaiba, PE



Home Work Assignment # 15.1

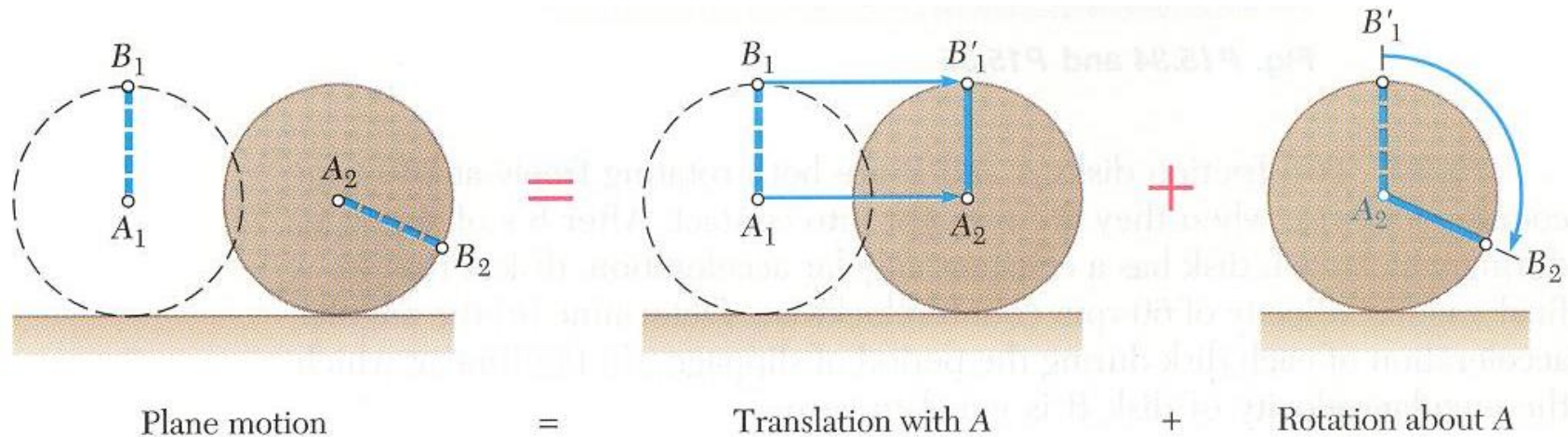
1, 8, 14, 21, 28, 35

Due

Saturday 29/3/2014 (Civil)

Sunday 30/3/2014 (Mechanical)

General Plane Motion (GPM)

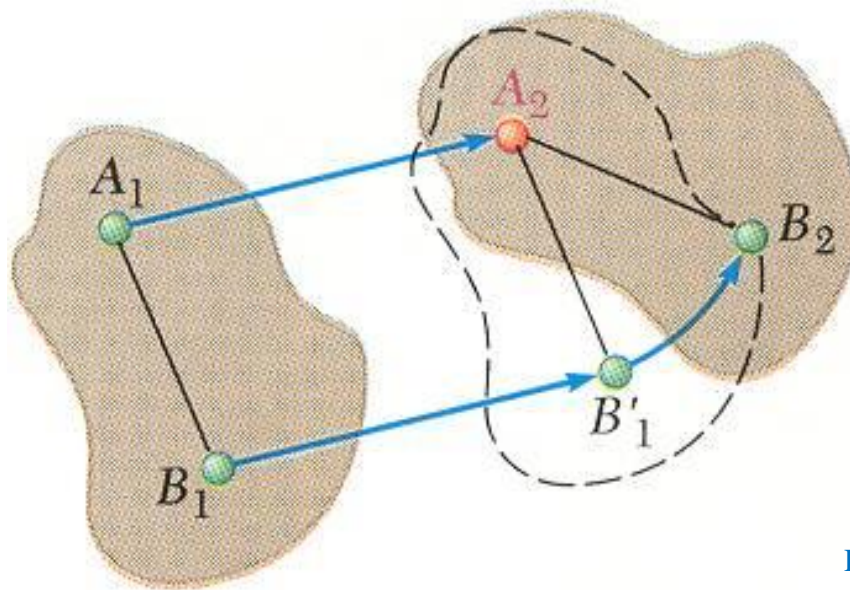


- *GPM* is neither a translation nor a rotation.
- $GPM = \text{translation} + \text{rotation}$

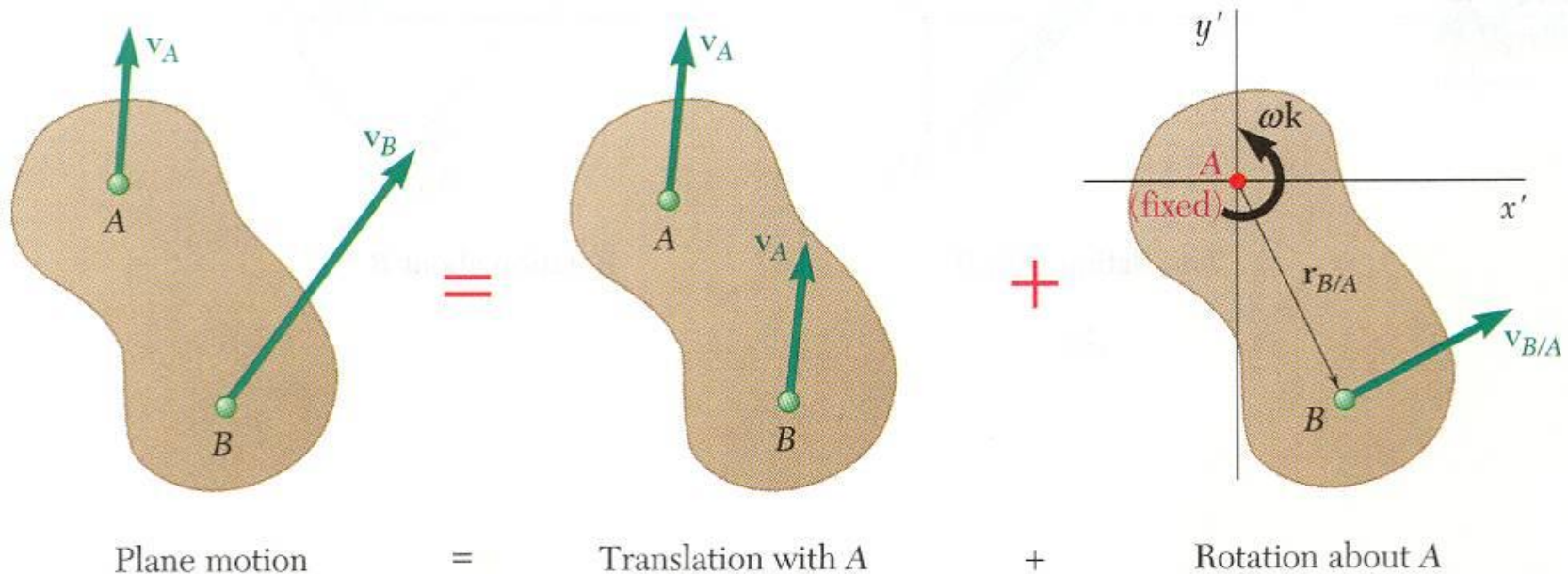
General Plane Motion (GPM)

Displacement of particles A_1 & B_1 to A_2 & B_2 can be divided into two parts:

1. translation to A_2
2. rotation of B_1' about A_2 to B_2



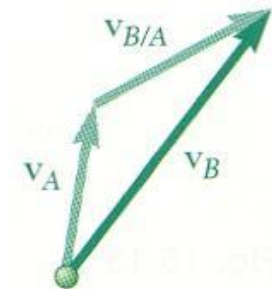
Absolute and Relative Velocity in Plane Motion



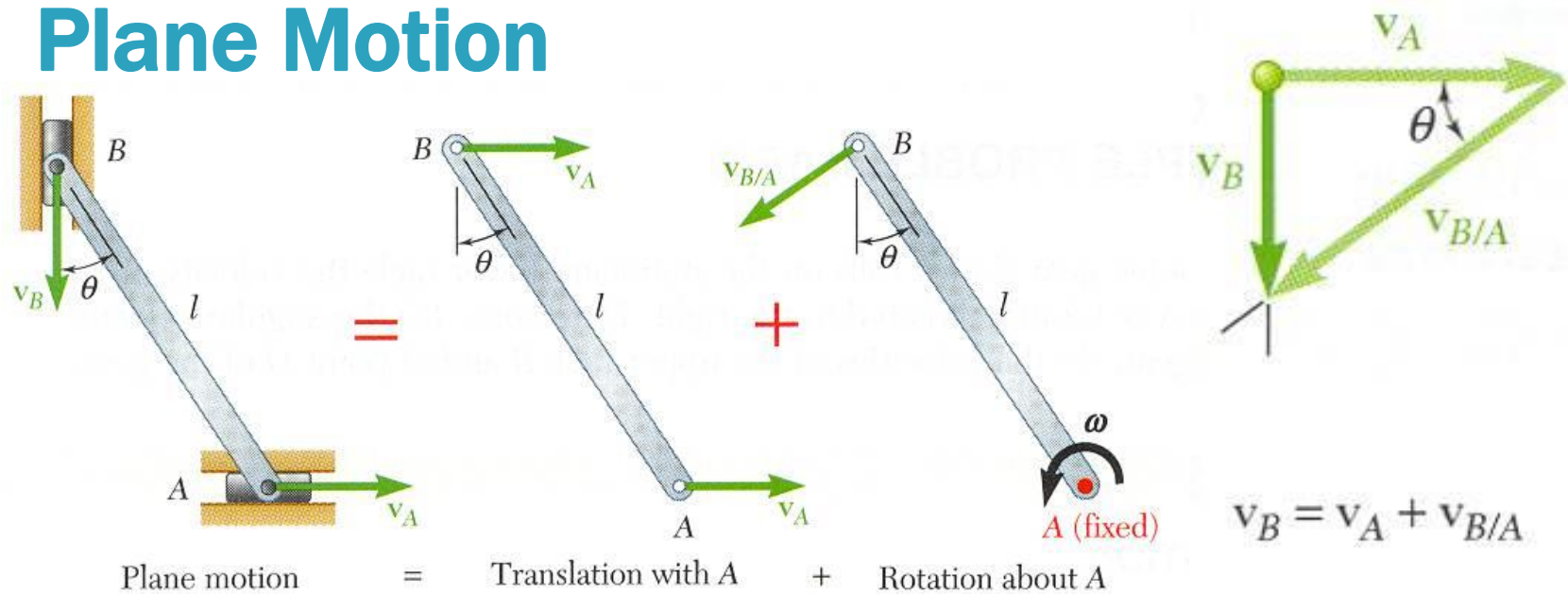
$$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$$

$$\vec{v}_B = \vec{v}_A + \omega \vec{k} \times \vec{r}_{B/A}$$

$$\vec{v}_{B/A} = \omega \vec{k} \times \vec{r}_{B/A}$$

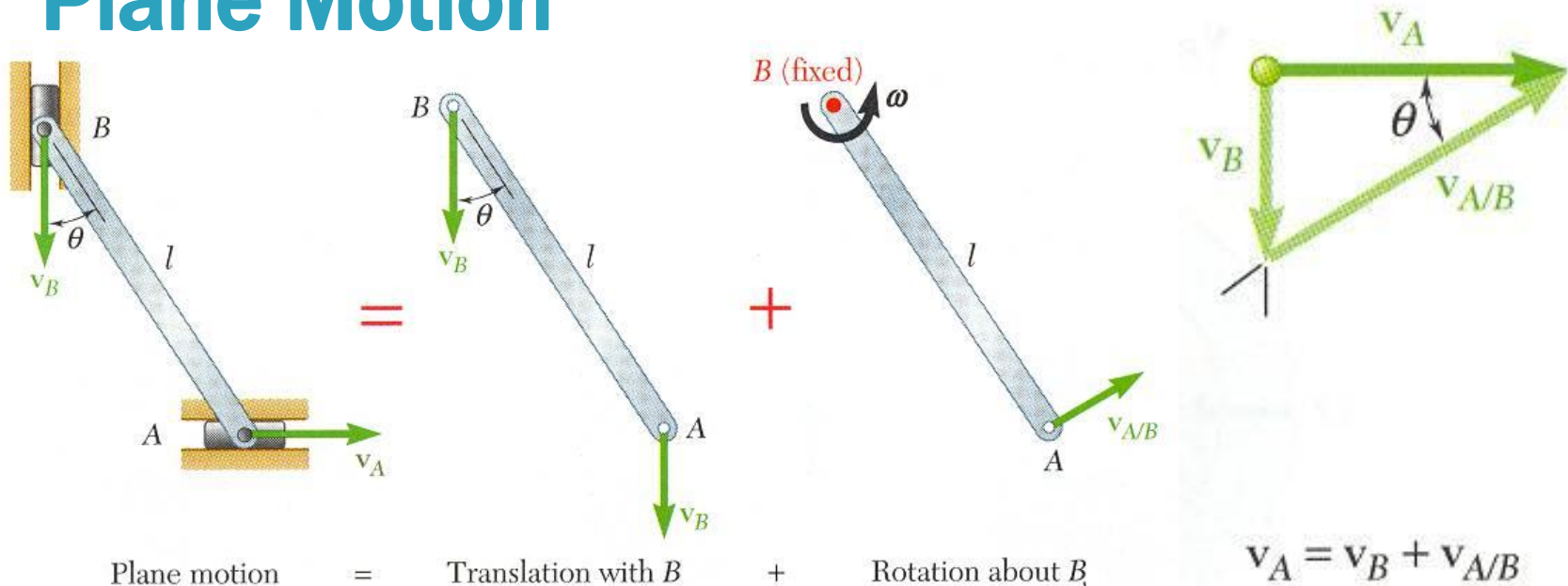


Absolute and Relative Velocity in Plane Motion



Assuming that velocity v_A of end A is known, determine velocity v_B of end B and angular velocity ω in terms of v_A , l , and θ .

Absolute and Relative Velocity in Plane Motion

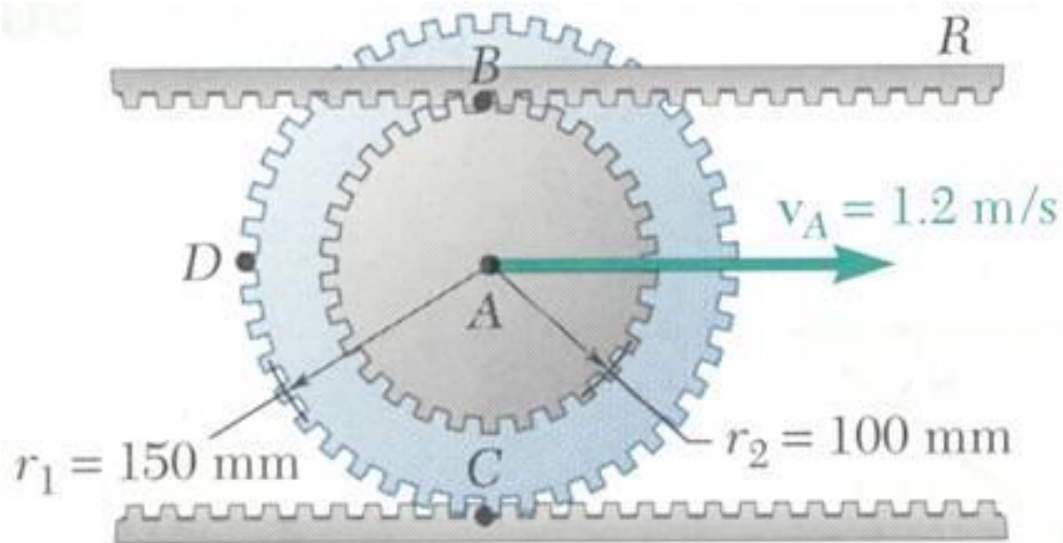


Selecting point B as the reference point and solving for velocity v_A of end A and angular velocity ω leads to an equivalent velocity triangle.

Sample Problem 15.2

The double gear rolls on the stationary lower rack: the velocity of its center is 1.2 m/s . Determine:

- angular velocity of gear
- velocities of upper rack R and point D of gear.



Sample Problem 15.2

Solution:

Displacement of gear center in one revolution = outer circumference

$$\frac{x_A}{2\pi r} = -\frac{\theta}{2\pi} \quad x_A = -r_1\theta$$

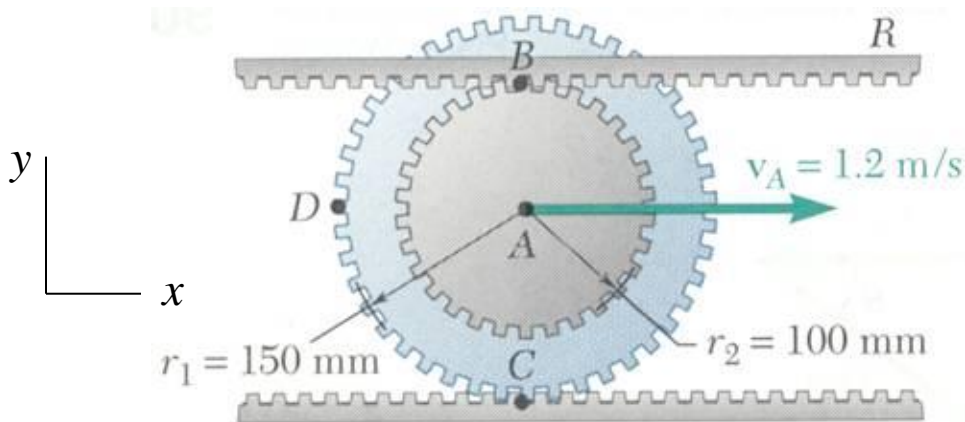
For $x_A > 0$ (to right), $\omega < 0$ (rotates cw),

Differentiate to relate translational & angular velocities.

$$v_A = -r_1\omega$$

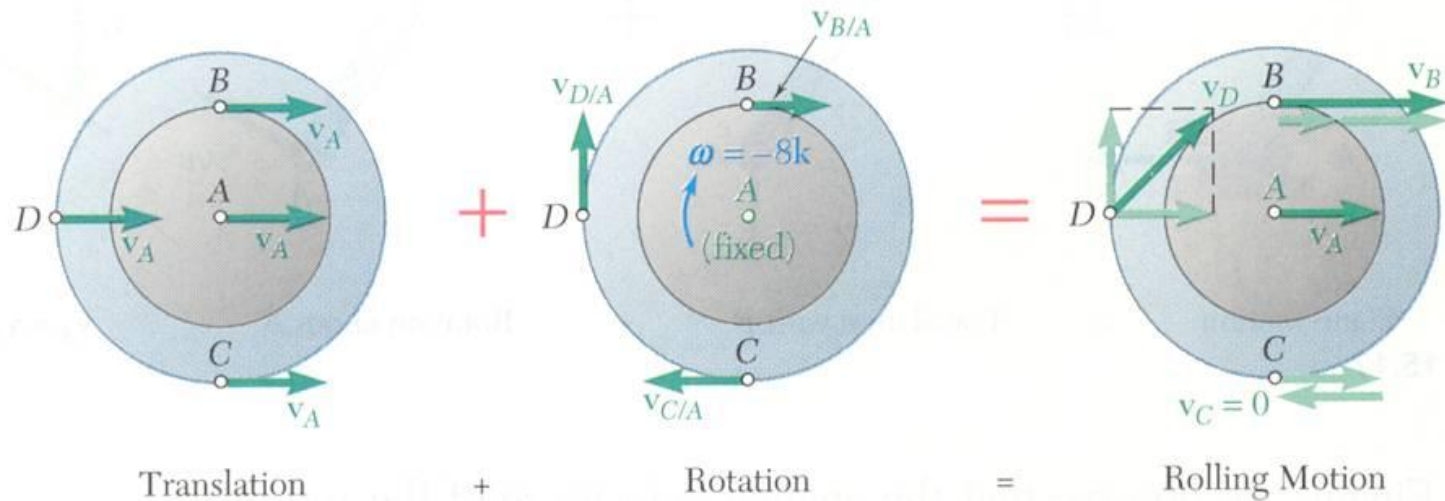
$$\omega = -\frac{v_A}{r_1} = -\frac{1.2 \text{ m/s}}{0.150 \text{ m}}$$

$$\vec{\omega} = \omega \vec{k} = -(8 \text{ rad/s}) \vec{k}$$



Sample Problem 15.2

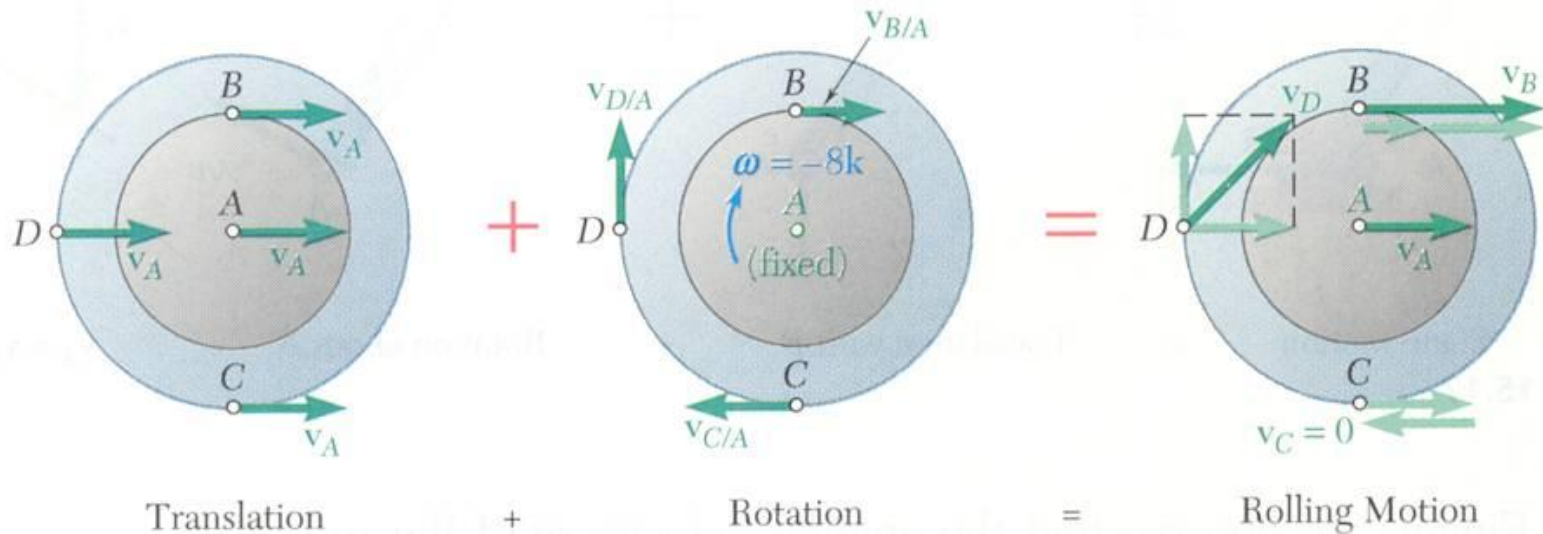
- For any point P on the gear, $\vec{v}_P = \vec{v}_A + \vec{v}_{P/A} = \vec{v}_A + \omega \vec{k} \times \vec{r}_{P/A}$



Velocity of upper rack is equal to velocity of point B :

$$\begin{aligned} \vec{v}_R = \vec{v}_B &= \vec{v}_A + \omega \vec{k} \times \vec{r}_{B/A} = (1.2 \text{ m/s})\vec{i} + (8 \text{ rad/s})\vec{k} \times (0.10 \text{ m})\vec{j} \\ &= (1.2 \text{ m/s})\vec{i} + (0.8 \text{ m/s})\vec{i} \quad \vec{v}_R = (2 \text{ m/s})\vec{i} \end{aligned}$$

Sample Problem 15.2



Velocity of the point D :

$$\vec{v}_D = \vec{v}_A + \omega \vec{k} \times \vec{r}_{D/A} = (1.2 \text{ m/s})\vec{i} + (8 \text{ rad/s})\vec{k} \times (-0.150 \text{ m})\vec{i}$$

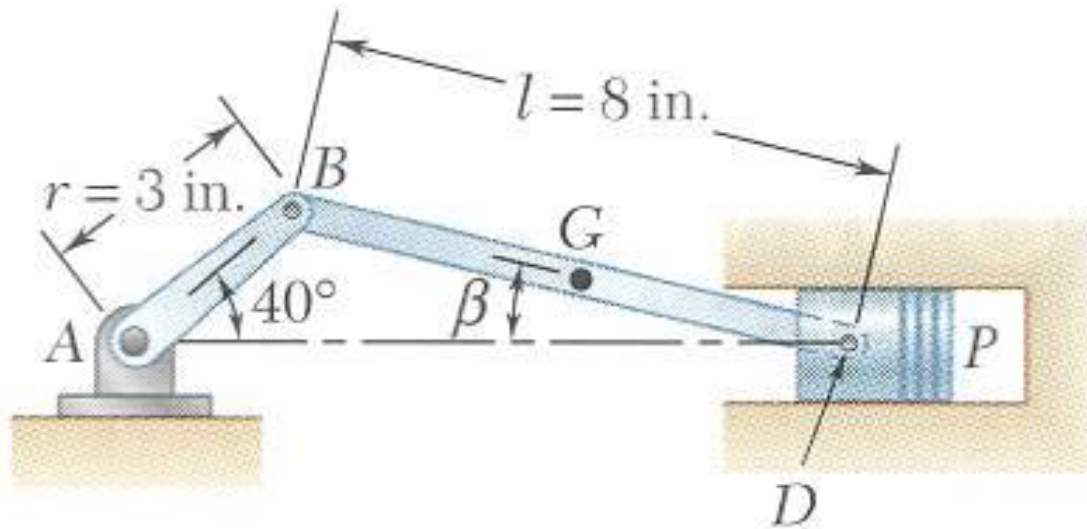
$$\vec{v}_D = (1.2 \text{ m/s})\vec{i} + (1.2 \text{ m/s})\vec{j}$$

$$v_D = 1.697 \text{ m/s}$$

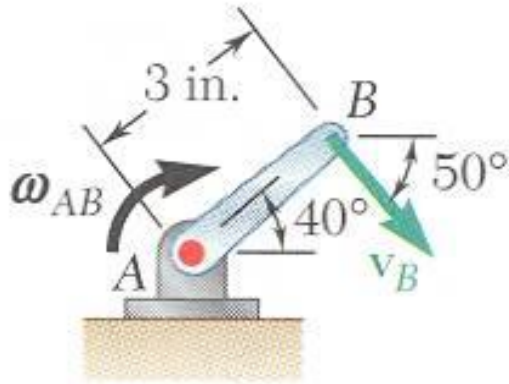
Sample Problem 15.3

The crank AB has a constant cw angular velocity of 2000 rpm. For the crank position indicated, determine:

- angular velocity of connecting rod BD
- velocity of piston P



Sample Problem 15.3



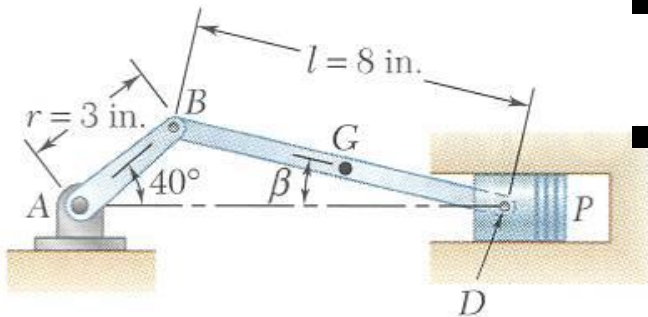
Solution: $\vec{v}_D = \vec{v}_B + \vec{v}_{D/B}$

$$\omega_{AB} = \left(2000 \frac{\text{rev}}{\text{min}} \right) \left(\frac{\text{min}}{60 \text{ s}} \right) \left(\frac{2\pi \text{ rad}}{\text{rev}} \right)$$

$$= 209.4 \text{ rad/s}$$

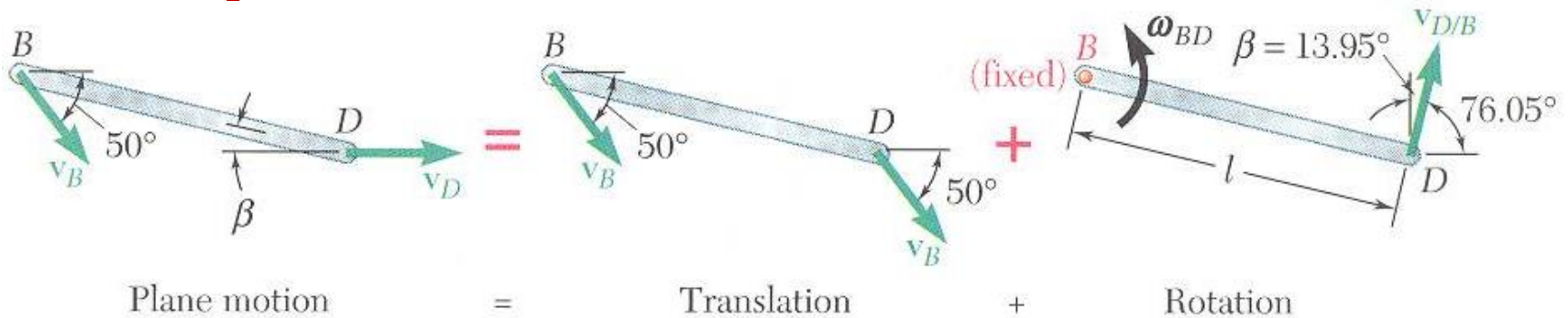
$$v_B = (AB)\omega_{AB} = (3 \text{ in.})(209.4 \text{ rad/s})$$

- Direction of \vec{v}_D is horizontal.
- Direction of relative velocity $\vec{v}_{D/B}$ is perpendicular to BD .



$$\frac{\sin 40^\circ}{8 \text{ in.}} = \frac{\sin \beta}{3 \text{ in.}} \quad \beta = 13.95^\circ$$

Sample Problem 15.3



$$\vec{v}_D = \vec{v}_B + \vec{v}_{D/B}$$

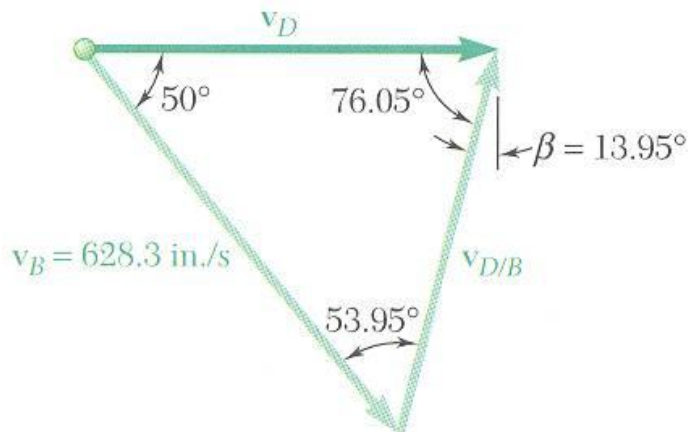
$$\frac{v_D}{\sin 53.95^\circ} = \frac{v_{D/B}}{\sin 50^\circ} = \frac{628.3 \text{ in./s}}{\sin 76.05^\circ}$$

$$v_D = v_P = 523.4 \text{ in./s} = 43.6 \text{ ft/s}$$

$$v_{D/B} = 495.9 \text{ in./s}$$

$$v_{D/B} = l \omega_{BD}$$

$$\omega_{BD} = \frac{v_{D/B}}{l} = \frac{495.9 \text{ in./s}}{8 \text{ in.}} = 62.0 \text{ rad/s}$$



Home Work Assignment # 15.2

38, 46, 53, 59, 66, 72

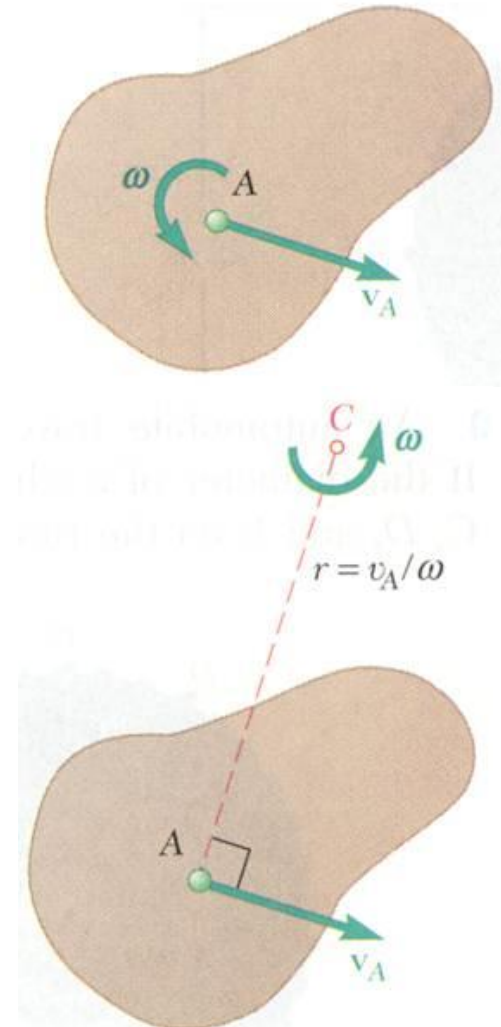
Due

Wednesday 2/4/2014 (Civil)

Tuesday 1/4/2014 (Mechanical)

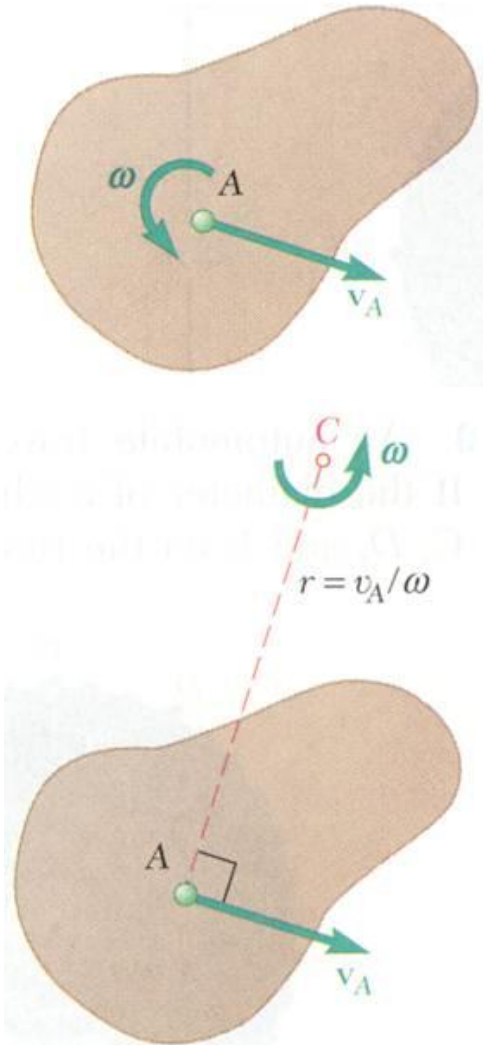
Instantaneous Center of Rotation (ICR) in Plane Motion

- Plane motion of all particles in a slab can be replaced by:
 1. translation of an arbitrary point A
 2. rotation about A with an angular velocity that is independent of choice of A



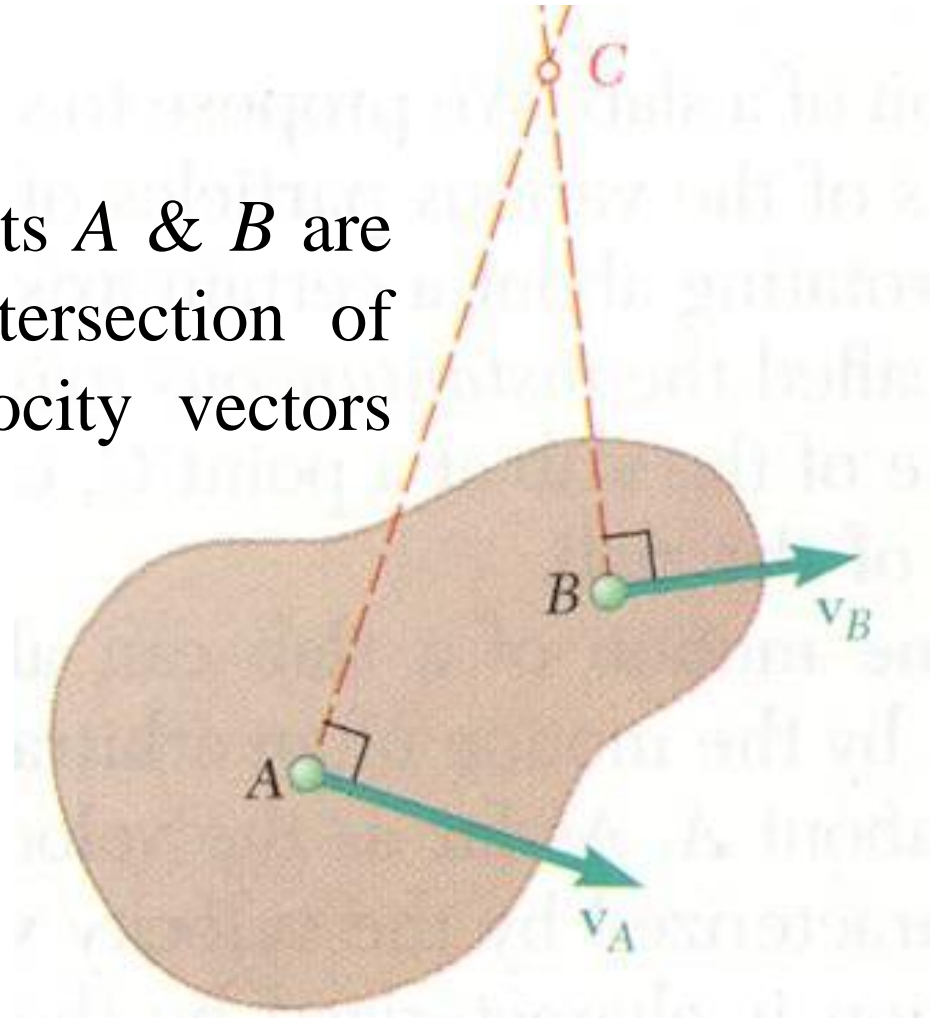
Instantaneous Center of Rotation in Plane Motion

- Same translational & rotational velocities at A are obtained by allowing slab to rotate with same angular velocity about some point C .
- The slab seems to rotate about the *instantaneous center of rotation* C .



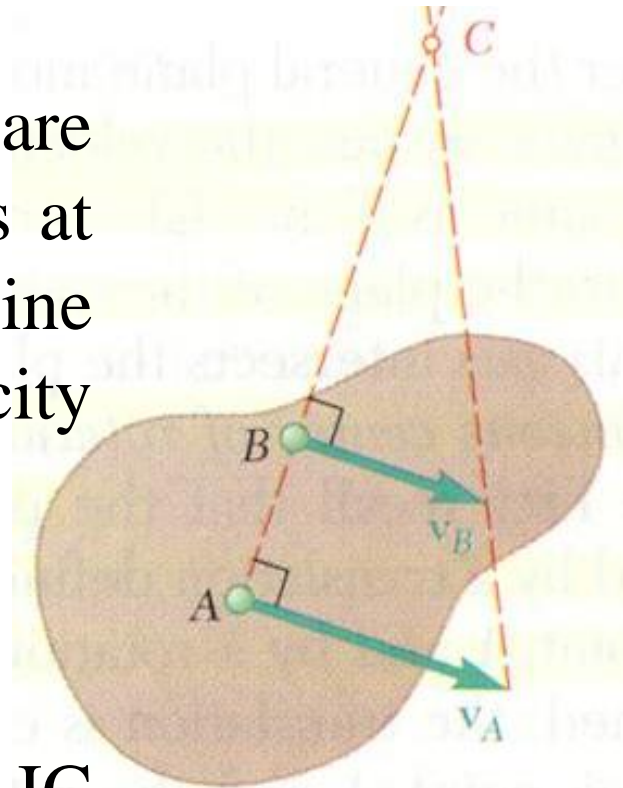
Instantaneous Center of Rotation in Plane Motion

- If velocity at two points A & B are known, IC lies at intersection of perpendiculars to velocity vectors through A & B

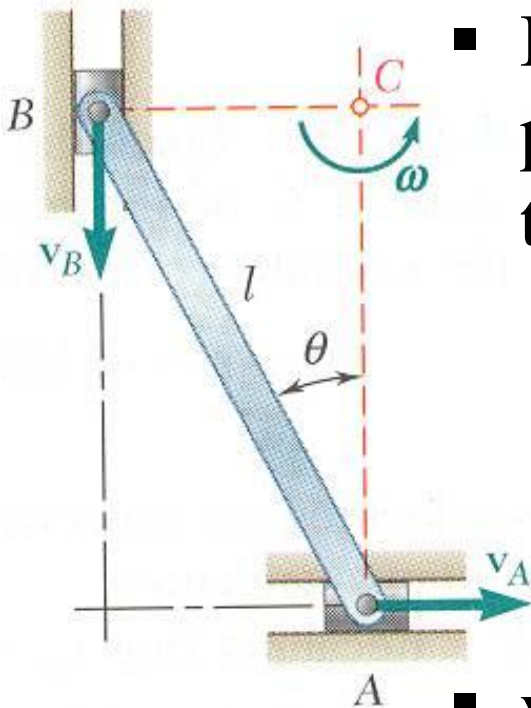


Instantaneous Center of Rotation in Plane Motion

- If velocity vectors at A and B are perpendicular to line AB , IC lies at intersection of line AB with line joining extremities of velocity vectors at A & B .
- If velocity magnitudes are equal, IC is at infinity & angular velocity is zero.



Instantaneous Center of Rotation in Plane Motion



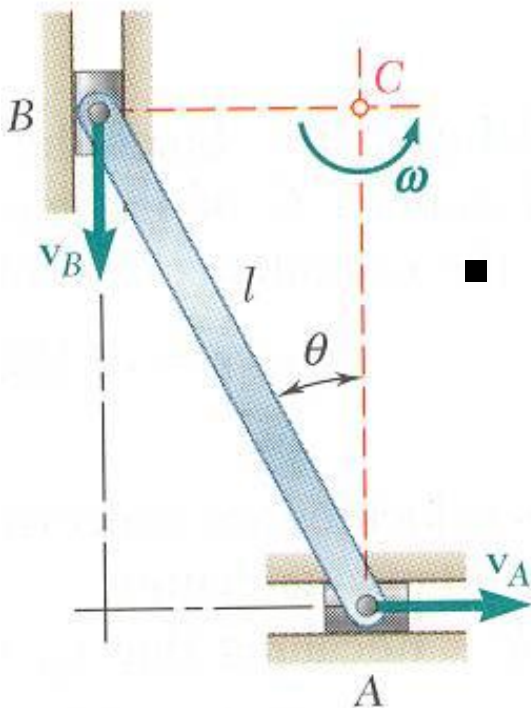
- ICR lies at intersection of perpendiculars to velocity vectors through A and B .

$$\omega = \frac{v_A}{AC} = \frac{v_A}{l \cos \theta}$$

$$v_B = (BC)\omega = (l \sin \theta) \frac{v_A}{l \cos \theta} = v_A \tan \theta$$

- velocities of all particles on rod are as if they were rotated about C .
- particle at ICR has zero velocity.

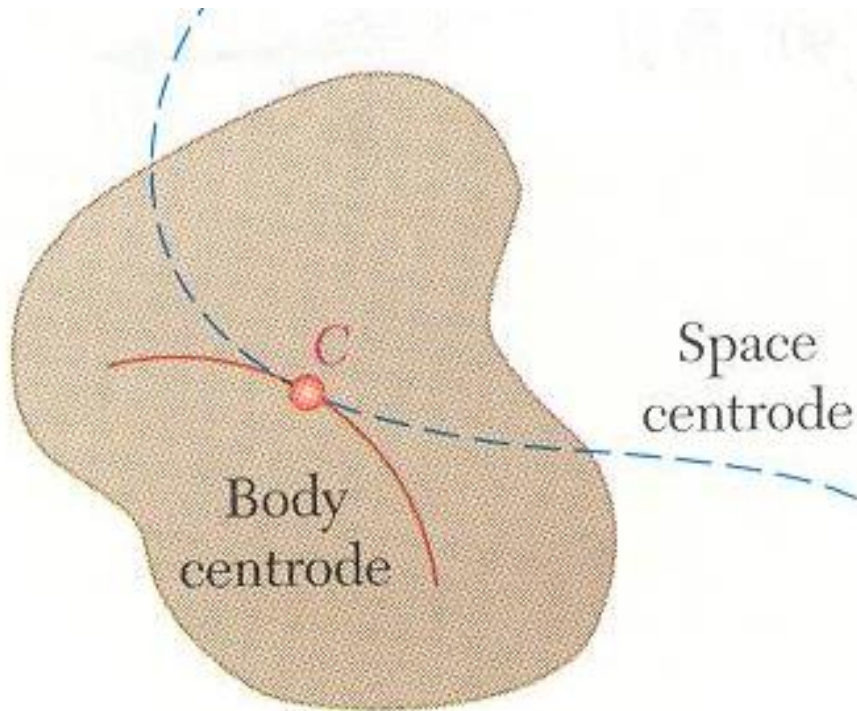
Instantaneous Center of Rotation in Plane Motion



- particle coinciding with ICR changes with time and acceleration of particle at ICR is not zero.
- acceleration of particles in the slab cannot be determined as if the slab were simply rotating about C .

Instantaneous Center of Rotation in Plane Motion

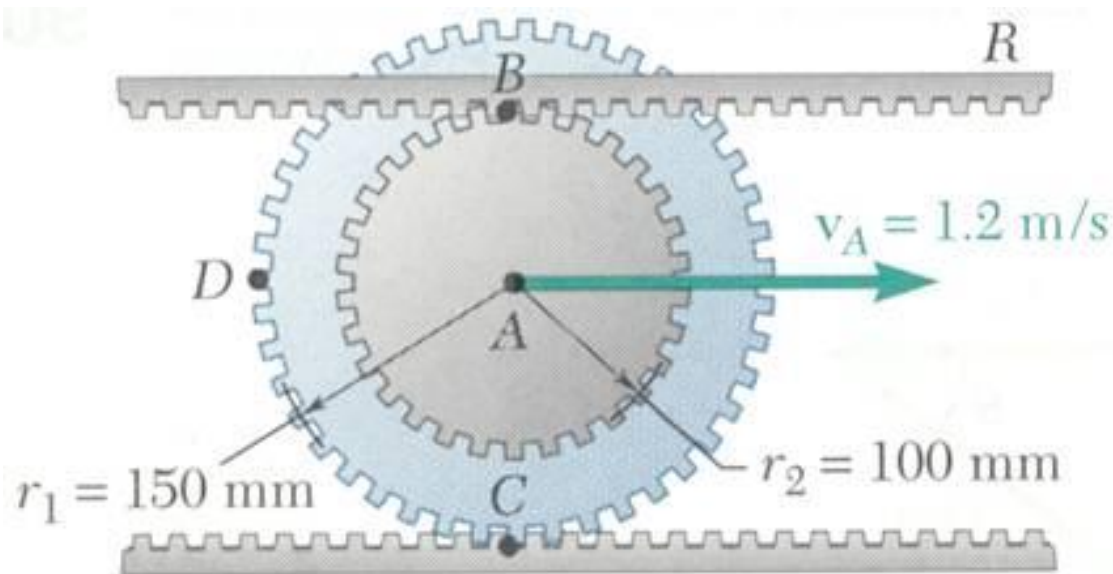
- **Body centrode:** trace of locus of ICR on the body
- **space centrode:** trace of locus of ICR in space



Sample Problem 15.4

The double gear rolls on the stationary lower rack: the velocity of its center is 1.2 m/s . Determine:

- angular velocity of the gear
- velocities of upper rack R and point D of the gear.



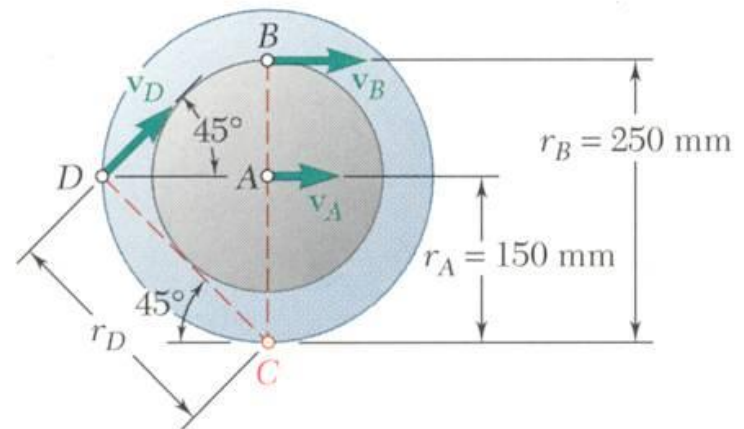
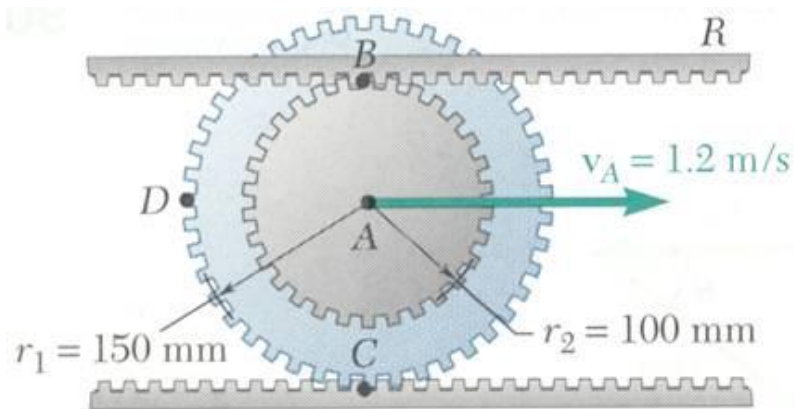
Sample Problem 15.4

Solution:

- point C is in contact with stationary lower rack and, instantaneously, has zero velocity. It must be the location of ICR.
- Determine angular velocity about C based on given velocity at A .

$$v_A = r_A \omega$$

$$\omega = \frac{v_A}{r_A} = \frac{1.2 \text{ m/s}}{0.15 \text{ m}} = 8 \text{ rad/s}$$



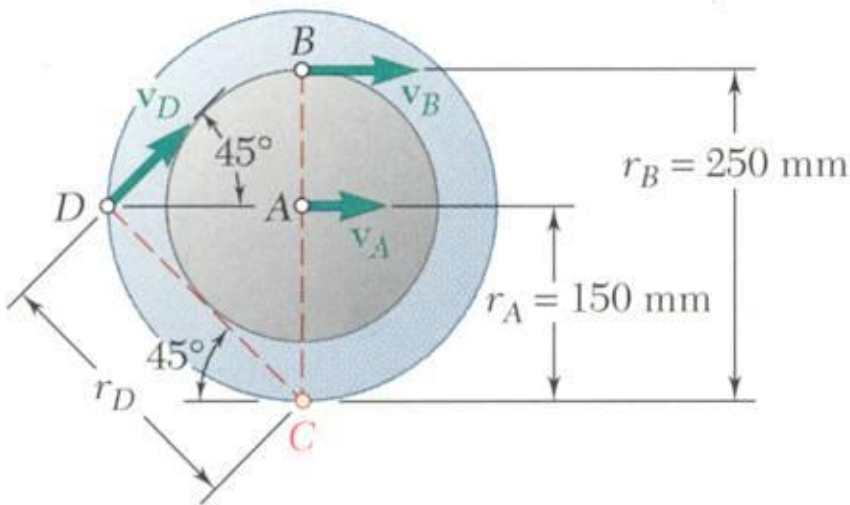
Sample Problem 15.4

- Evaluate velocities at B & D based on their rotation about C .

$$v_R = v_B = r_B \omega = (0.25 \text{ m})(8 \text{ rad/s}) = (2 \text{ m/s})\vec{i}$$

$$r_D = (0.15 \text{ m})\sqrt{2} = 0.2121 \text{ m}$$

$$v_D = r_D \omega = (0.2121 \text{ m})(8 \text{ rad/s})$$



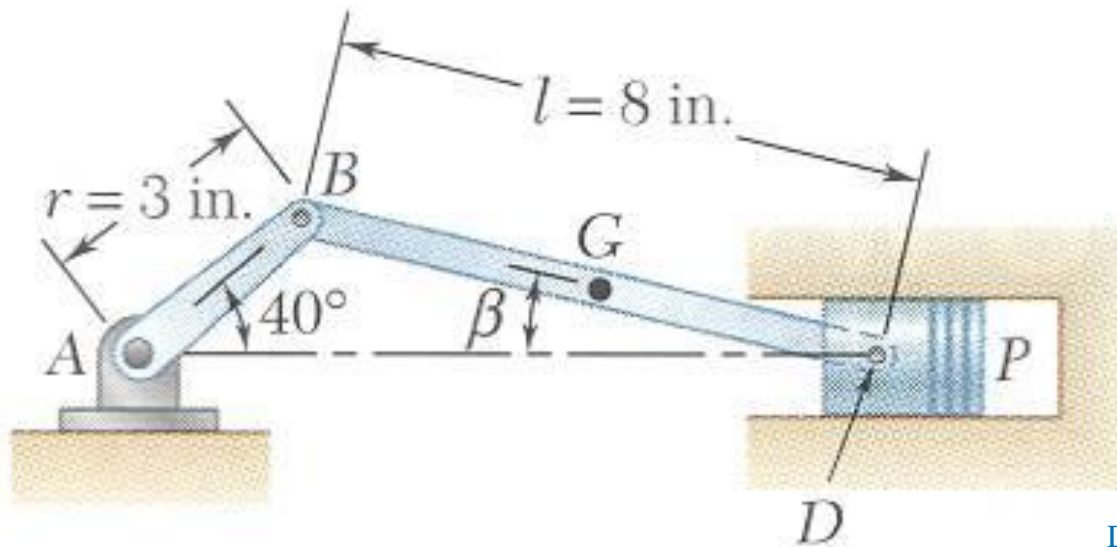
$$v_D = 1.697 \text{ m/s}$$

$$\vec{v}_D = (1.2\vec{i} + 1.2\vec{j})(\text{m/s})$$

Sample Problem 15.5

The crank AB has a constant cw angular velocity of 2000 rpm. For the crank position indicated, determine:

- angular velocity of connecting rod BD
- velocity of piston P



Sample Problem 15.5

- From Sample Problem 15.3,

$$\vec{v}_B = (403.9\vec{i} - 481.3\vec{j}) \text{ (in./s)}, \quad v_B = 628.3 \text{ in./s}, \quad \beta = 13.95^\circ$$

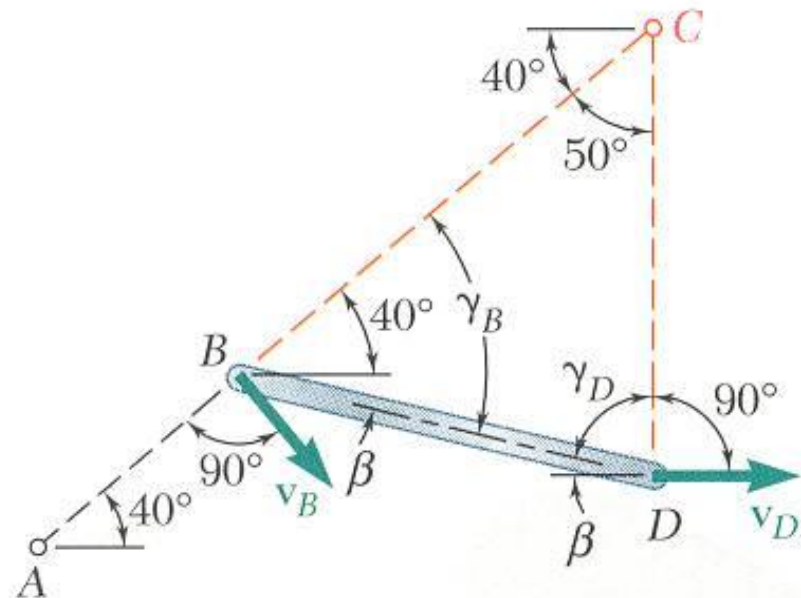
- ICR is at intersection of perpendiculars to velocities through B & D .

$$\gamma_B = 40^\circ + \beta = 53.95^\circ$$

$$\gamma_D = 90^\circ - \beta = 76.05^\circ$$

$$\frac{BC}{\sin 76.05^\circ} = \frac{CD}{\sin 53.95^\circ} = \frac{8 \text{ in.}}{\sin 50^\circ}$$

$$BC = 10.14 \text{ in.} \quad CD = 8.44 \text{ in.}$$



Sample Problem 15.5

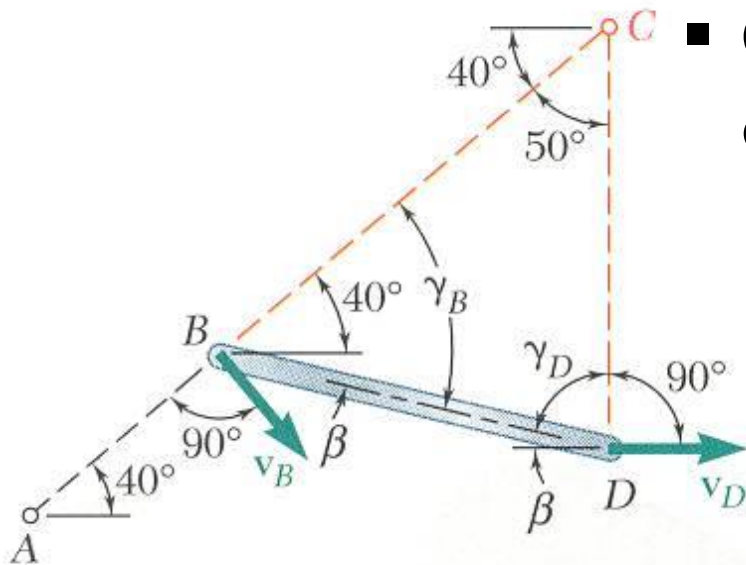
- Determine angular velocity about ICR based on velocity at B

$$v_B = (BC)\omega_{BD}$$

$$\omega_{BD} = \frac{v_B}{BC} = \frac{628.3 \text{ in./s}}{10.14 \text{ in.}} = 62.0 \text{ rad/s}$$

- Calculate velocity at D based on its rotation about ICR

$$v_D = (CD)\omega_{BD} = (8.44 \text{ in.})(62.0 \text{ rad/s}) = 43.6 \text{ ft/s}$$



Home Work Assignment # 15.3

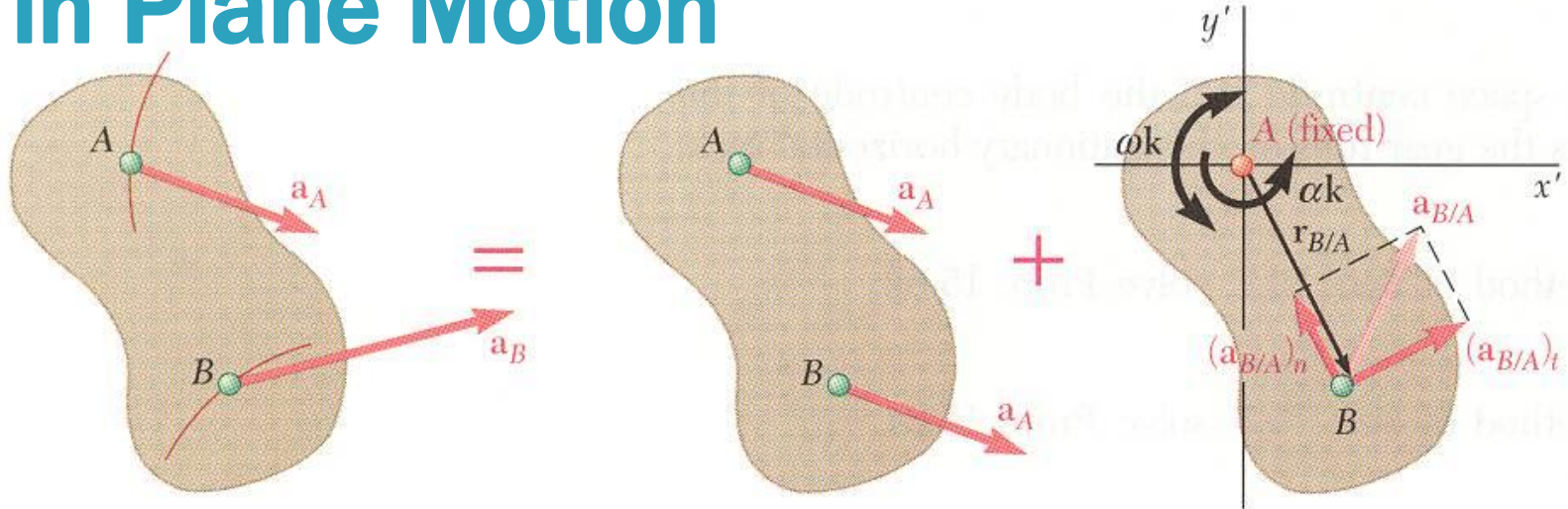
74, 80, 88, 95

Due

Saturday 5/4/2014 (Civil)

Sunday 6/4/2014 (Mechanical)

Absolute and Relative Acceleration in Plane Motion



Plane motion

=

Translation with A

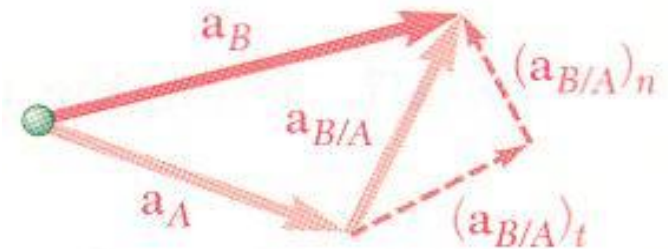
+

Rotation about A

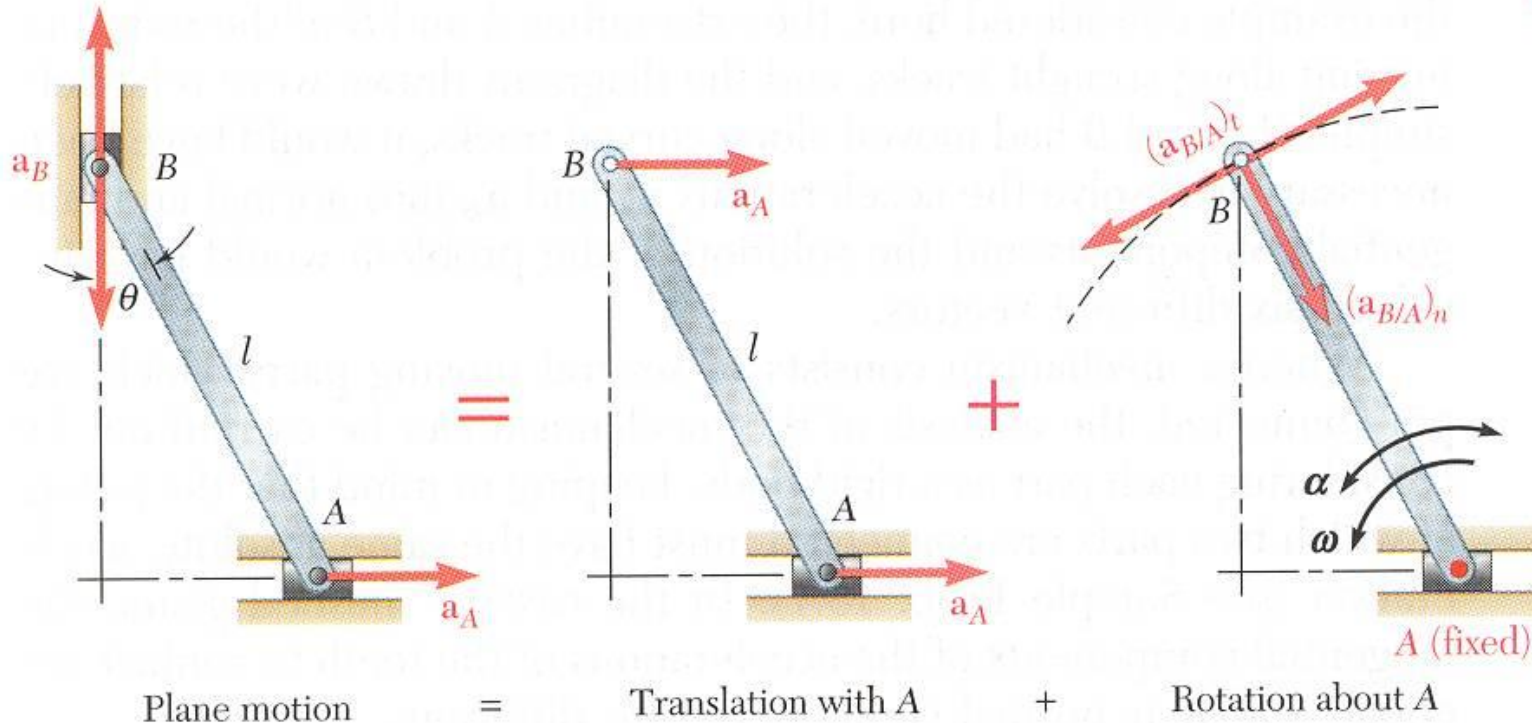
$$\vec{a}_B = \vec{a}_A + \vec{a}_{B/A}$$

$$(\vec{a}_{B/A})_t = \alpha \vec{k} \times \vec{r}_{B/A} \quad (a_{B/A})_t = r\alpha$$

$$(\vec{a}_{B/A})_n = -\omega^2 \vec{r}_{B/A} \quad (a_{B/A})_n = r\omega^2$$



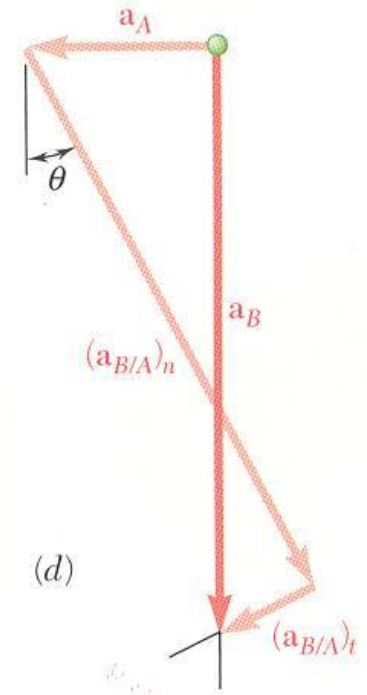
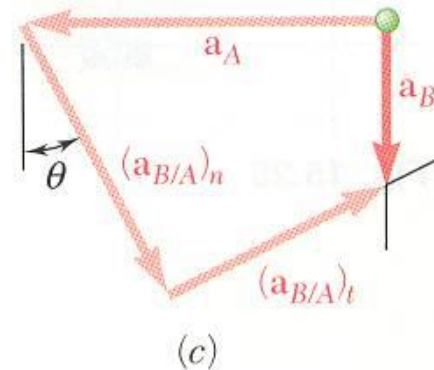
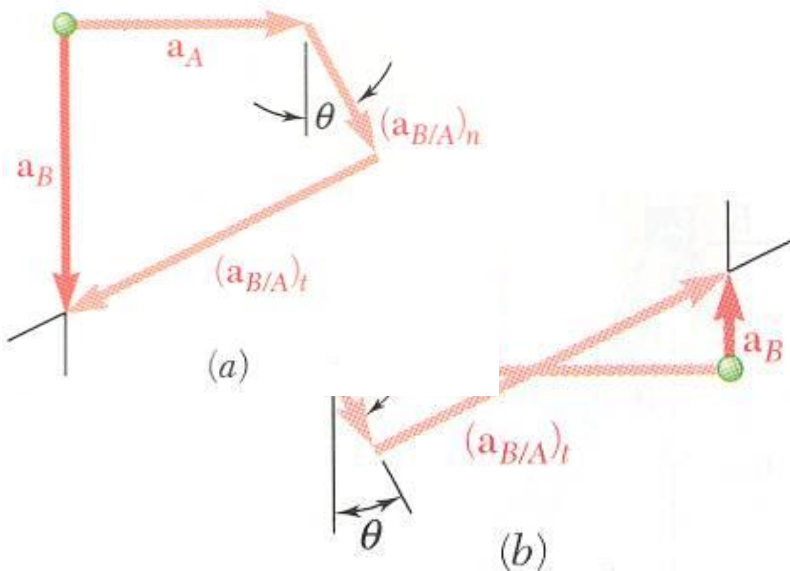
Absolute and Relative Acceleration in Plane Motion



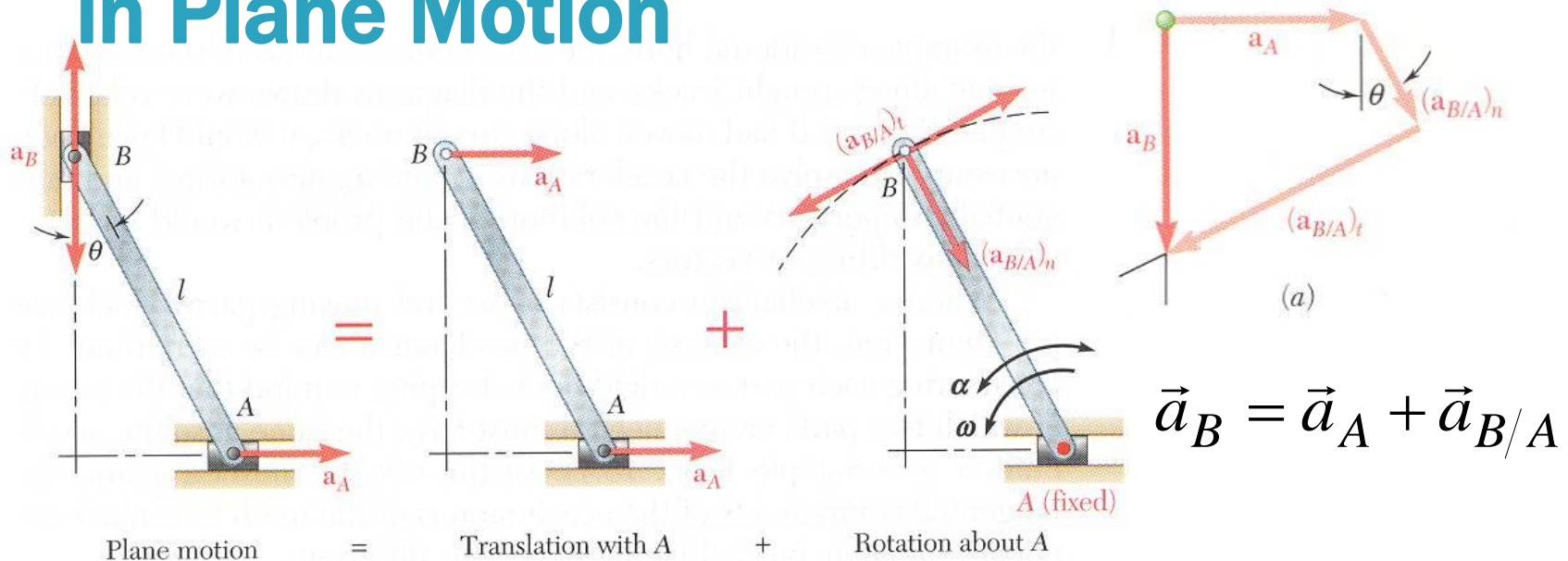
$$\begin{aligned}\vec{a}_B &= \vec{a}_A + \vec{a}_{B/A} \\ &= \vec{a}_A + \left(\vec{a}_{B/A}\right)_n + \left(\vec{a}_{B/A}\right)_t\end{aligned}$$

Absolute and Relative Acceleration in Plane Motion

- Vector result depends on sense of ω and the relative magnitudes of a_A and $(a_{B/A})_n$
- Must also know angular velocity ω .



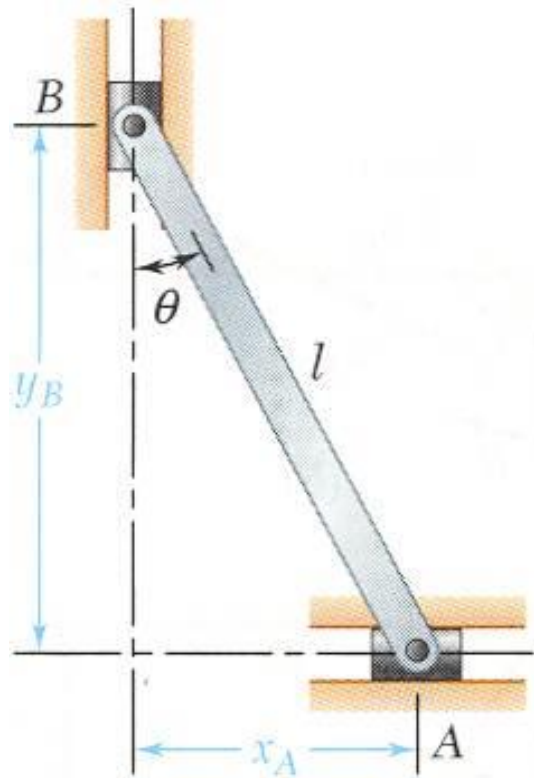
Absolute and Relative Acceleration in Plane Motion



→ +x components: $0 = a_A + l\omega^2 \sin\theta - l\alpha \cos\theta$

+ ↑ y components: $-a_B = -l\omega^2 \cos\theta - l\alpha \sin\theta$

Analysis of Plane Motion in Terms of a Parameter



$$x_A = l \sin \theta \qquad y_B = l \cos \theta$$

$$v_A = \dot{x}_A = l \dot{\theta} \cos \theta = l \omega \cos \theta$$

$$v_B = \dot{y}_B = -l \dot{\theta} \sin \theta = -l \omega \sin \theta$$

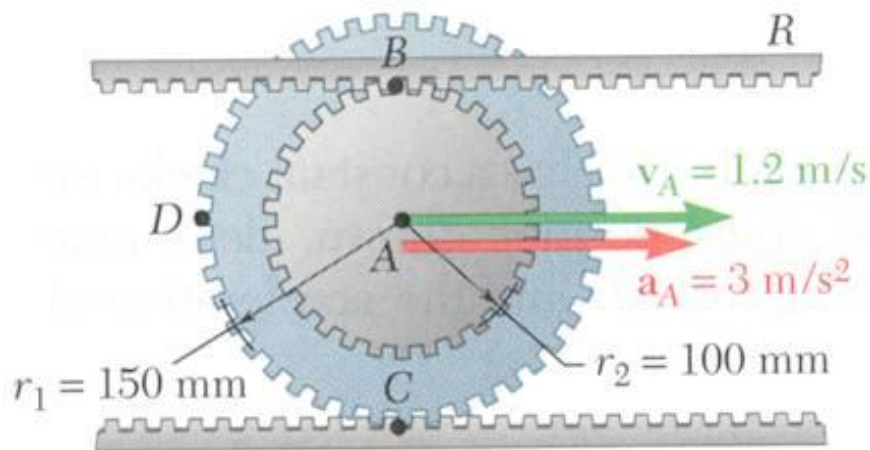
$$\begin{aligned} a_A = \ddot{x}_A &= -l \dot{\theta}^2 \sin \theta + l \ddot{\theta} \cos \theta \\ &= -l \omega^2 \sin \theta + l \alpha \cos \theta \end{aligned}$$

$$\begin{aligned} a_B = \ddot{y}_B &= -l \dot{\theta}^2 \cos \theta - l \ddot{\theta} \sin \theta \\ &= -l \omega^2 \cos \theta - l \alpha \sin \theta \end{aligned}$$

Sample Problem 15.6

The center of the double gear has a velocity and acceleration to the right of 1.2 m/s and 3 m/s^2 , respectively. The lower rack is stationary. Determine:

- angular acceleration of the gear
- acceleration of points B , C , D



Sample Problem 15.6

Solution:

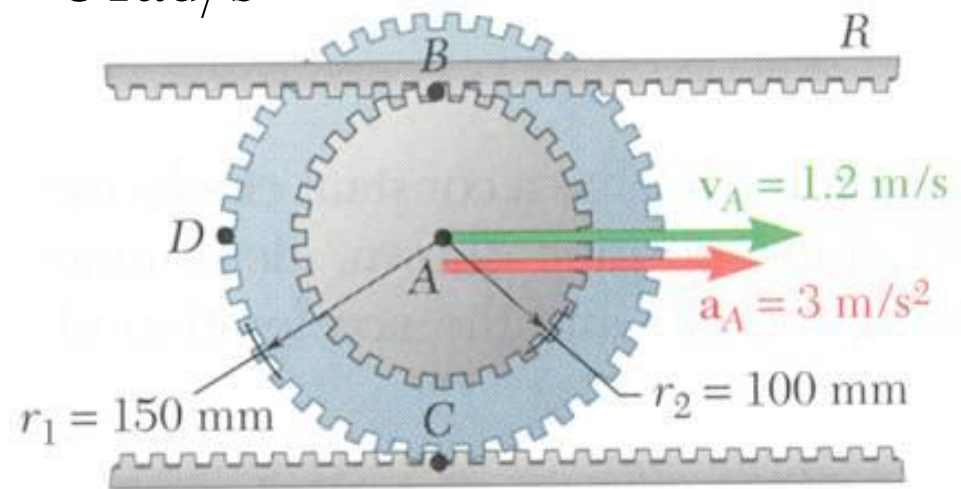
$$x_A = -r_1\theta, \quad v_A = -r_1\dot{\theta} = -r_1\omega$$

$$\omega = -\frac{v_A}{r_1} = -\frac{1.2 \text{ m/s}}{0.150 \text{ m}} = -8 \text{ rad/s}$$

$$a_A = -r_1\ddot{\theta} = -r_1\alpha$$

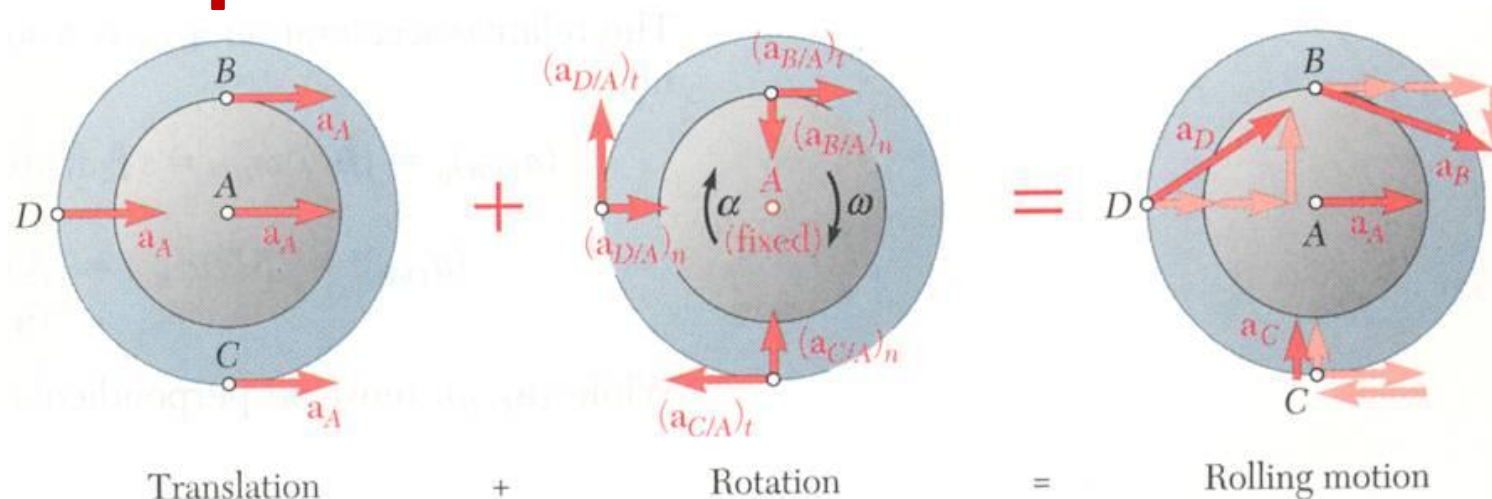
$$\alpha = -\frac{a_A}{r_1} = -\frac{3 \text{ m/s}^2}{0.150 \text{ m}}$$

$$\vec{\alpha} = \alpha \vec{k} = -(20 \text{ rad/s}^2) \vec{k}$$



Dr. Mohammad Suliman Abuhaiba, PE

Sample Problem 15.6



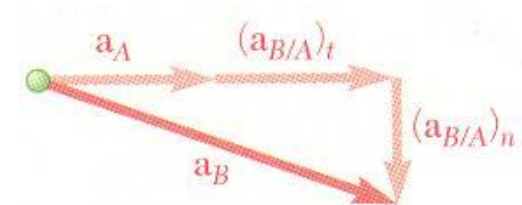
$$\vec{a}_B = \vec{a}_A + \vec{a}_{B/A} = \vec{a}_A + (\vec{a}_{B/A})_t + (\vec{a}_{B/A})_n$$

$$= \vec{a}_A + \alpha \vec{k} \times \vec{r}_{B/A} - \omega^2 \vec{r}_{B/A}$$

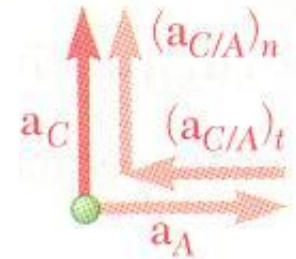
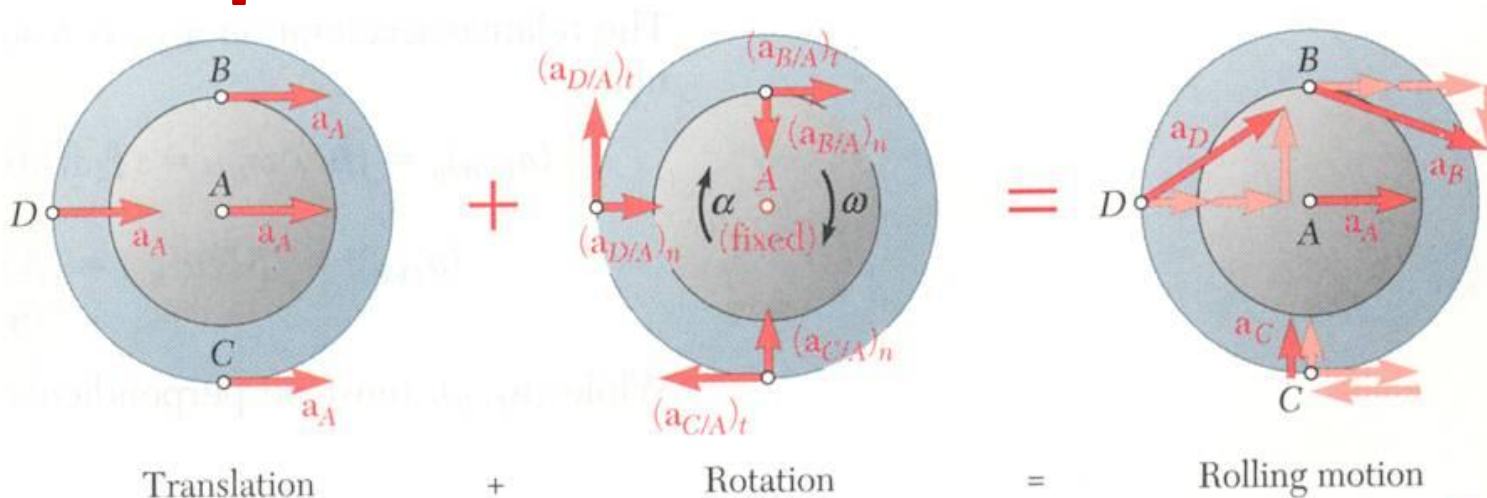
$$= (3 \text{ m/s}^2) \vec{i} - (20 \text{ rad/s}^2) \vec{k} \times (0.100 \text{ m}) \vec{j} - (8 \text{ rad/s})^2 (-0.100 \text{ m}) \vec{j}$$

$$= (3 \text{ m/s}^2) \vec{i} + (2 \text{ m/s}^2) \vec{i} - (6.40 \text{ m/s}^2) \vec{j}$$

$$\vec{a}_B = (5 \text{ m/s}^2) \vec{i} - (6.40 \text{ m/s}^2) \vec{j} \quad a_B = 8.12 \text{ m/s}^2$$

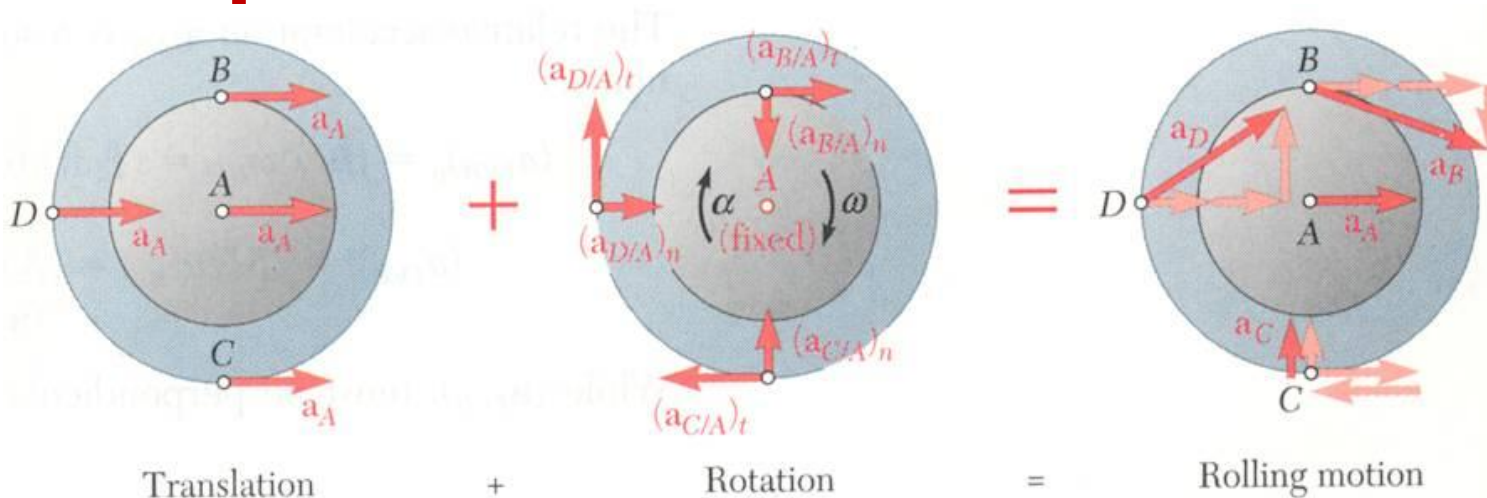


Sample Problem 15.6

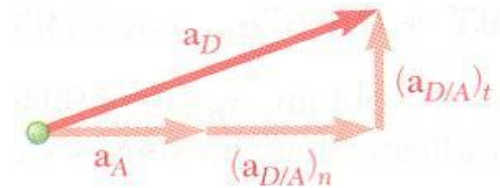


$$\begin{aligned}
 \vec{a}_C &= \vec{a}_A + \vec{a}_{C/A} = \vec{a}_A + \alpha \vec{k} \times \vec{r}_{C/A} - \omega^2 \vec{r}_{C/A} \\
 &= (3 \text{ m/s}^2) \vec{i} - (20 \text{ rad/s}^2) \vec{k} \times (-0.150 \text{ m}) \vec{j} - (8 \text{ rad/s})^2 (-0.150 \text{ m}) \vec{j} \\
 &= (3 \text{ m/s}^2) \vec{i} - (3 \text{ m/s}^2) \vec{i} + (9.60 \text{ m/s}^2) \vec{j} \\
 \vec{a}_c &= (9.60 \text{ m/s}^2) \vec{j}
 \end{aligned}$$

Sample Problem 15.6



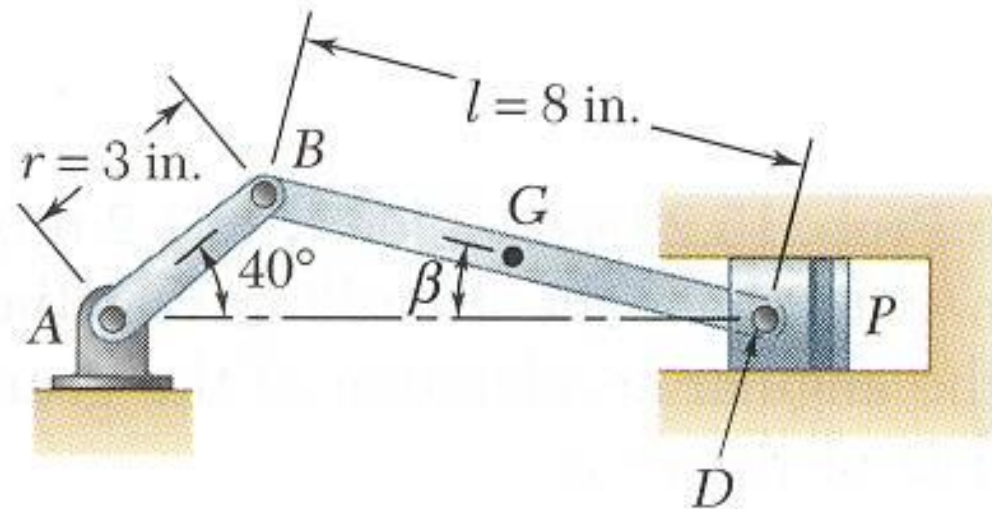
$$\begin{aligned}\vec{a}_D &= \vec{a}_A + \vec{a}_{D/A} = \vec{a}_A + \alpha \vec{k} \times \vec{r}_{D/A} - \omega^2 \vec{r}_{D/A} \\ &= (3 \text{ m/s}^2) \vec{i} - (20 \text{ rad/s}^2) \vec{k} \times (-0.150 \text{ m}) \vec{i} - (8 \text{ rad/s})^2 (-0.150 \text{ m}) \vec{i} \\ &= (3 \text{ m/s}^2) \vec{i} + (3 \text{ m/s}^2) \vec{j} + (9.60 \text{ m/s}^2) \vec{i}\end{aligned}$$



$$\vec{a}_D = (12.6 \text{ m/s}^2) \vec{i} + (3 \text{ m/s}^2) \vec{j} \quad a_D = 12.95 \text{ m/s}^2$$

Sample Problem 15.7

Crank AB of the engine system has a constant cw angular velocity of 2000 rpm. For the crank position shown, determine angular acceleration of the connecting rod BD and the acceleration of point D .

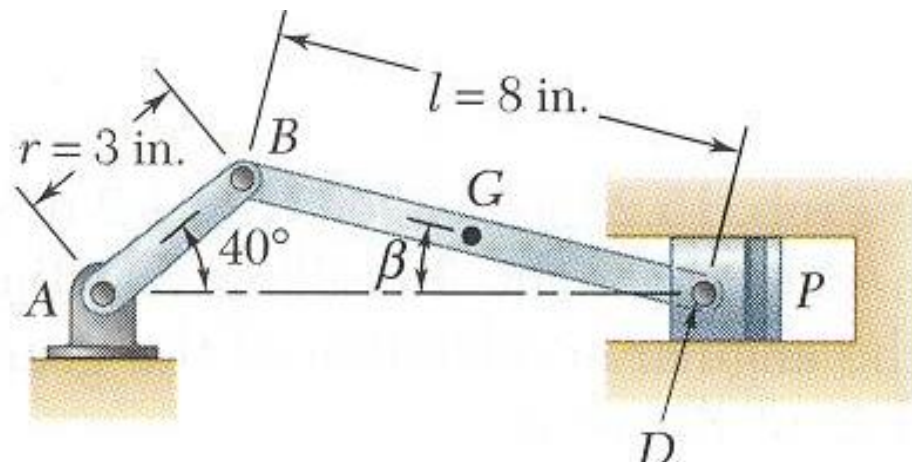


Sample Problem 15.7

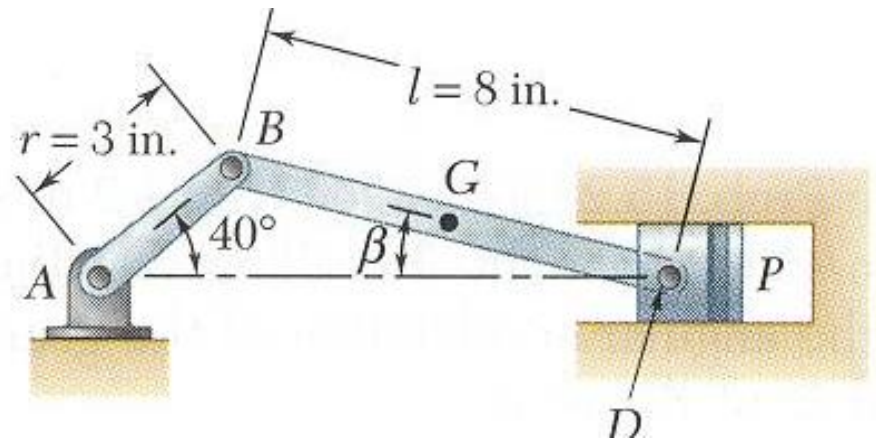
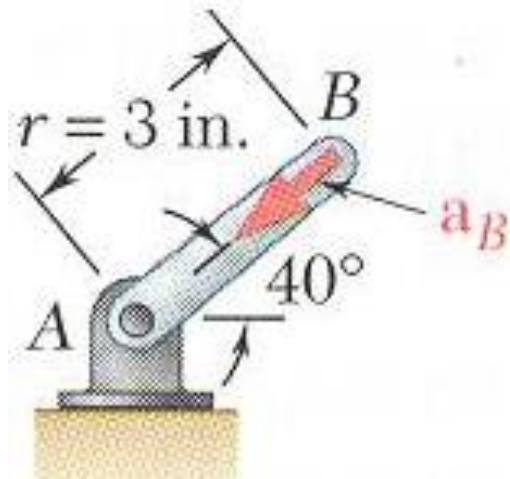
Solution:

- Angular acceleration of connecting rod BD and acceleration of point D will be determined from

$$\vec{a}_D = \vec{a}_B + \vec{a}_{D/B} = \vec{a}_B + (\vec{a}_{D/B})_t + (\vec{a}_{D/B})_n$$



Sample Problem 15.7



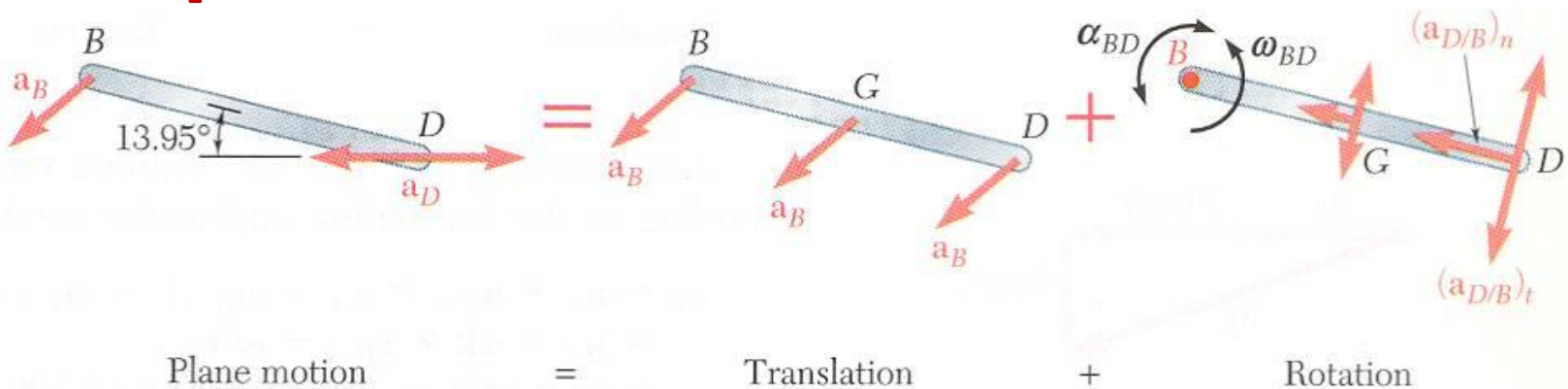
$$\omega_{AB} = 2000 \text{ rpm} = 209.4 \text{ rad/s} = \text{constant}$$

$$\alpha_{AB} = 0$$

$$a_B = r\omega_{AB}^2 = \left(\frac{3}{12} \text{ ft}\right)(209.4 \text{ rad/s})^2 = 10,962 \text{ ft/s}^2$$

$$\vec{a}_B = (10,962 \text{ ft/s}^2)(-\cos 40^\circ \vec{i} - \sin 40^\circ \vec{j})$$

Sample Problem 15.7



$$\vec{a}_D = \mp a_D \vec{i}$$

Sample Problem 15.3: $\omega_{BD} = 62.0 \text{ rad/s}$, $\beta = 13.95^\circ$.

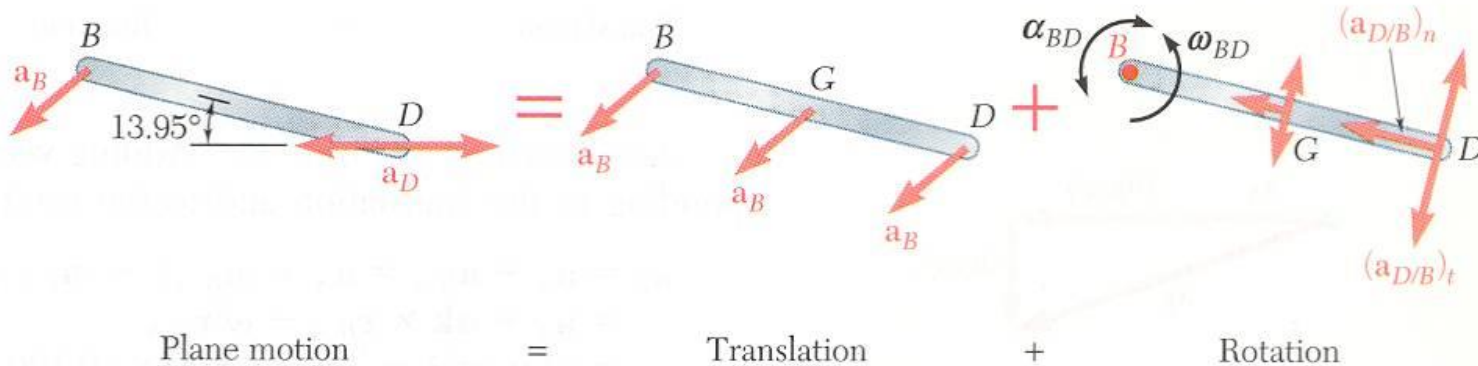
$$(a_{D/B})_n = (BD)\omega_{BD}^2 = \left(\frac{8}{12} \text{ ft}\right)(62.0 \text{ rad/s})^2 = 2563 \text{ ft/s}^2$$

$$(\vec{a}_{D/B})_n = (2563 \text{ ft/s}^2)(-\cos 13.95^\circ \vec{i} + \sin 13.95^\circ \vec{j})$$

$$(a_{D/B})_t = (BD)\alpha_{BD} = \left(\frac{8}{12} \text{ ft}\right)\alpha_{BD} = 0.667\alpha_{BD}$$

$$(\vec{a}_{D/B})_t = (0.667\alpha_{BD})(\pm \sin 76.05^\circ \vec{i} \pm \cos 76.05^\circ \vec{j})$$

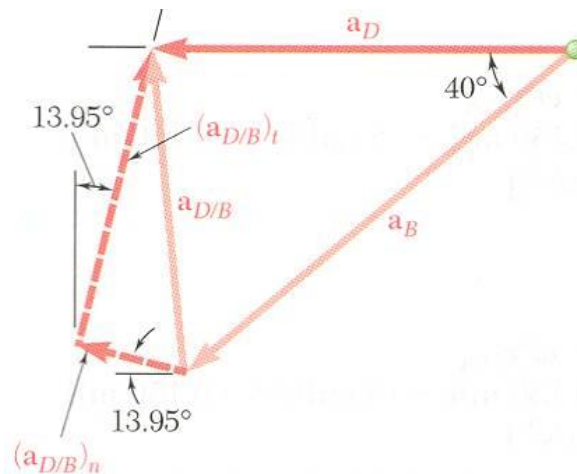
Sample Problem 15.7



$$\vec{a}_D = \vec{a}_B + \vec{a}_{D/B} = \vec{a}_B + (\vec{a}_{D/B})_t + (\vec{a}_{D/B})_n$$

x components: $-a_D = -10,962 \cos 40^\circ - 2563 \cos 13.95^\circ + 0.667 \alpha_{BD} \sin 13.95^\circ$

y components: $0 = -10,962 \sin 40^\circ + 2563 \sin 13.95^\circ + 0.667 \alpha_{BD} \cos 13.95^\circ$

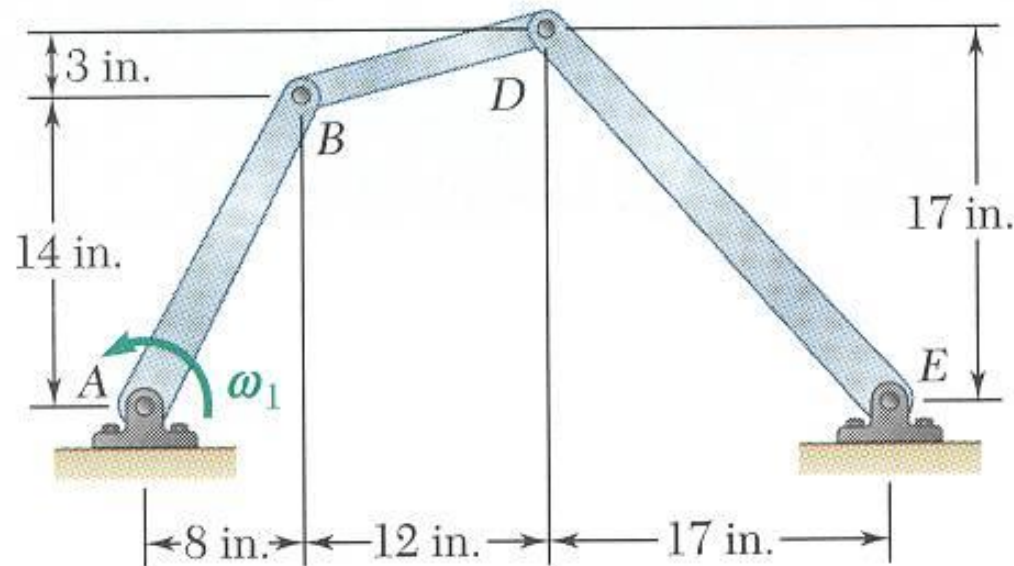


$$\vec{\alpha}_{BD} = (9940 \text{ rad/s}^2) \vec{k}$$

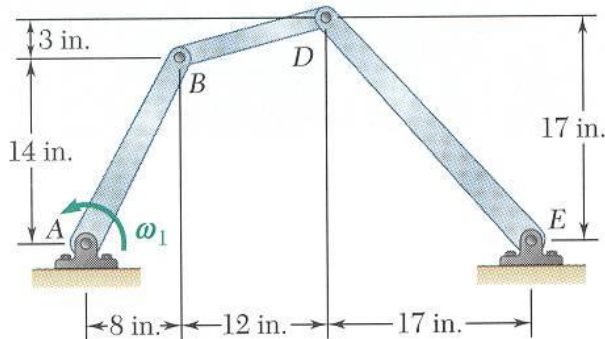
$$\vec{a}_D = -(9290 \text{ ft/s}^2) \vec{i}$$

Sample Problem 15.8

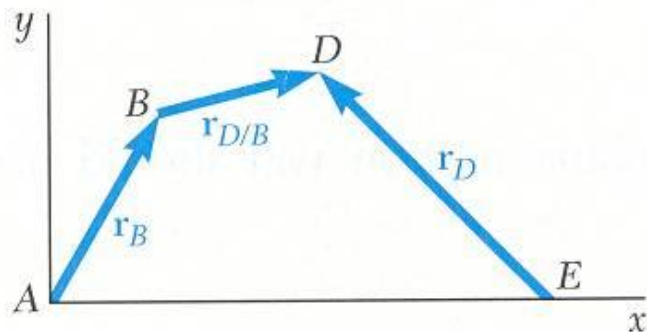
In the position shown, crank AB has a constant angular velocity $\omega_1 = 20$ rad/s ccw. Determine angular velocities and angular accelerations of connecting rod BD and crank DE .



Sample Problem 15.8



Solution:



$$\begin{aligned} \mathbf{r}_B &= 8\mathbf{i} + 14\mathbf{j} \\ \mathbf{r}_D &= -17\mathbf{i} + 17\mathbf{j} \\ \mathbf{r}_{D/B} &= 12\mathbf{i} + 3\mathbf{j} \end{aligned}$$

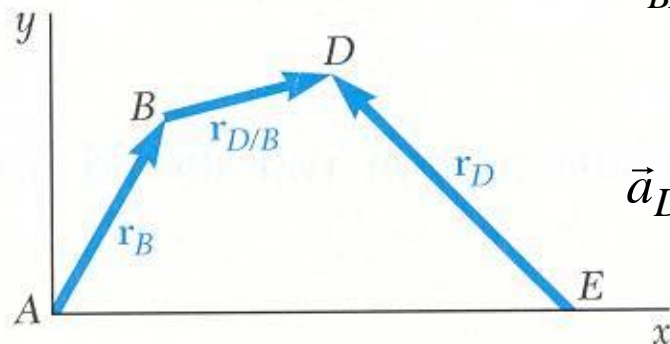
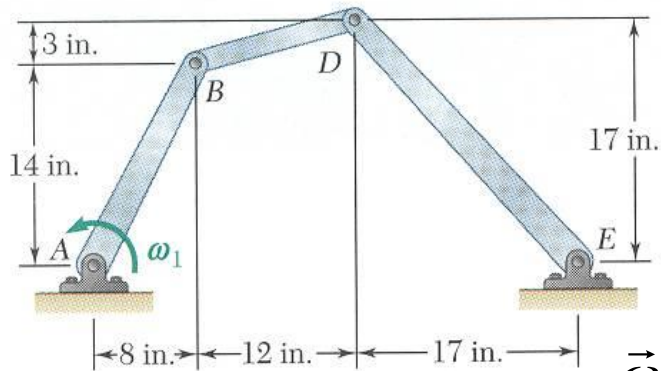
$$\vec{v}_D = \vec{v}_B + \vec{v}_{D/B}$$

$$\begin{aligned} \vec{v}_D &= \vec{\omega}_{DE} \times \vec{r}_D = \omega_{DE} \vec{k} \times (-17\vec{i} + 17\vec{j}) \\ &= -17\omega_{DE}\vec{i} - 17\omega_{DE}\vec{j} \end{aligned}$$

$$\begin{aligned} \vec{v}_B &= \vec{\omega}_{AB} \times \vec{r}_B = 20\vec{k} \times (8\vec{i} + 14\vec{j}) \\ &= -280\vec{i} + 160\vec{j} \end{aligned}$$

$$\begin{aligned} \vec{v}_{D/B} &= \vec{\omega}_{BD} \times \vec{r}_{D/B} = \omega_{BD} \vec{k} \times (12\vec{i} + 3\vec{j}) \\ &= -3\omega_{BD}\vec{i} + 12\omega_{BD}\vec{j} \end{aligned}$$

Sample Problem 15.8



$$\begin{aligned} \mathbf{r}_B &= 8\mathbf{i} + 14\mathbf{j} \\ \mathbf{r}_D &= -17\mathbf{i} + 17\mathbf{j} \\ \mathbf{r}_{D/B} &= 12\mathbf{i} + 3\mathbf{j} \end{aligned}$$

x components:

$$-17\omega_{DE} = -280 - 3\omega_{BD}$$

y components:

$$-17\omega_{DE} = +160 + 12\omega_{BD}$$

$$\vec{\omega}_{BD} = -(29.33 \text{ rad/s})\vec{k}, \quad \vec{\omega}_{DE} = (11.29 \text{ rad/s})\vec{k}$$

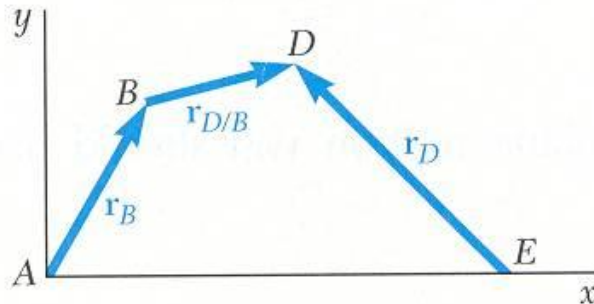
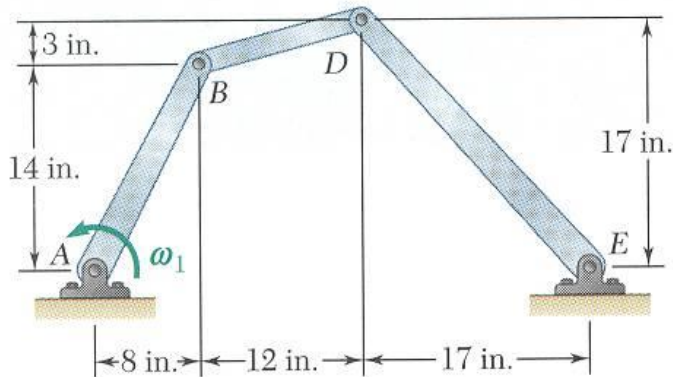
$$\vec{a}_D = \vec{a}_B + \vec{a}_{D/B}$$

$$\vec{a}_D = \vec{\alpha}_{DE} \times \vec{r}_D - \omega_{DE}^2 \vec{r}_D$$

$$= \alpha_{DE} \vec{k} \times (-17\vec{i} + 17\vec{j}) - (11.29)^2 (-17\vec{i} + 17\vec{j})$$

$$= -17\alpha_{DE}\vec{i} - 17\alpha_{DE}\vec{j} + 2170\vec{i} - 2170\vec{j}$$

Sample Problem 15.8



$$\begin{aligned} \mathbf{r}_B &= 8\mathbf{i} + 14\mathbf{j} \\ \mathbf{r}_D &= -17\mathbf{i} + 17\mathbf{j} \\ \mathbf{r}_{D/B} &= 12\mathbf{i} + 3\mathbf{j} \end{aligned}$$

$$\begin{aligned} \vec{a}_B &= \vec{\alpha}_{AB} \times \vec{r}_B - \omega_{AB}^2 \vec{r}_B = 0 - (20)^2 (8\vec{i} + 14\vec{j}) \\ &= -3200\vec{i} + 5600\vec{j} \end{aligned}$$

$$\begin{aligned} \vec{a}_{D/B} &= \vec{\alpha}_{BD} \times \vec{r}_{B/D} - \omega_{BD}^2 \vec{r}_{B/D} \\ &= \alpha_{B/D} \vec{k} \times (12\vec{i} + 3\vec{j}) - (29.33)^2 (12\vec{i} + 3\vec{j}) \\ &= -3\alpha_{B/D} \vec{i} + 12\alpha_{B/D} \vec{j} - 10,320\vec{i} - 2580\vec{j} \end{aligned}$$

y components:

$$-17\alpha_{DE} - 12\alpha_{BD} = -6010$$

x components:

$$-17\alpha_{DE} + 3\alpha_{BD} = -15,690$$

$$\vec{\alpha}_{BD} = -(645 \text{ rad/s}^2) \vec{k} \quad \vec{\alpha}_{DE} = (809 \text{ rad/s}^2) \vec{k}$$

Home Work Assignment # 15.4

105, 112, 119, 126, 133, 141

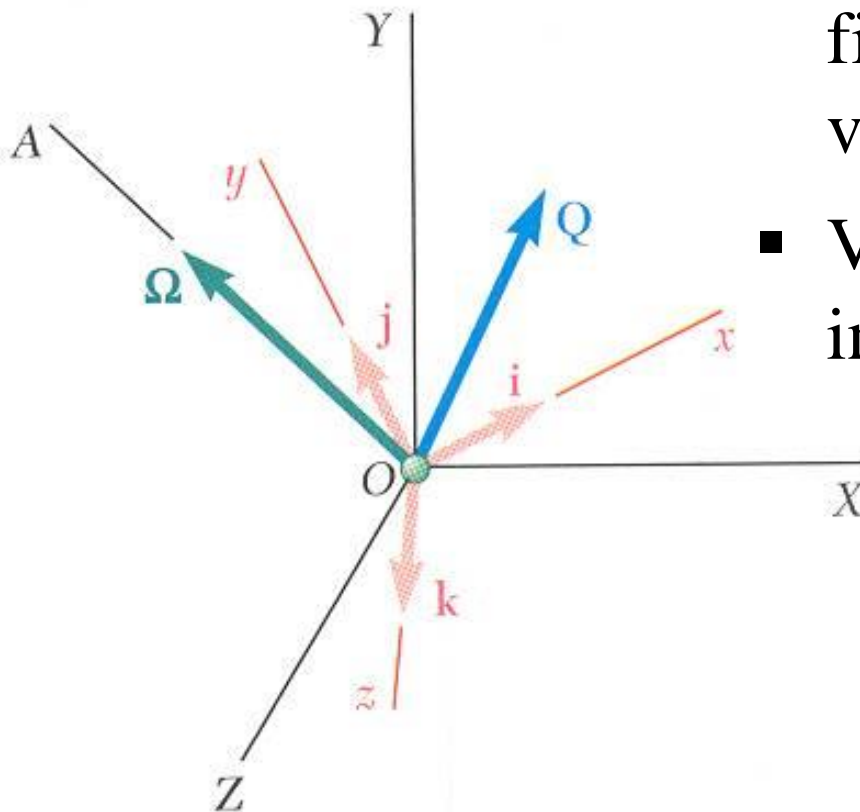
Due

Wednesday 9/4/2014 (Civil)

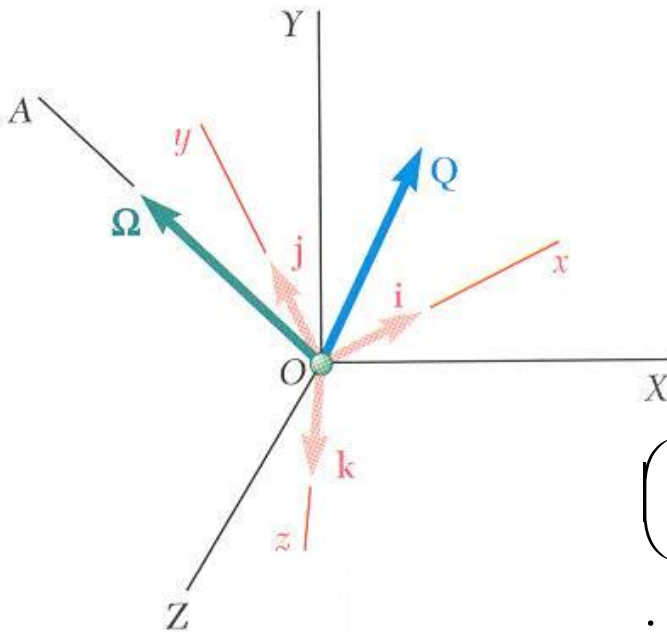
Tuesday 8/4/2014 (Mechanical)

Rate of Change wrt a Rotating Frame

- Frame $OXYZ$ is fixed.
- Frame $Oxyz$ rotates about fixed axis OA with angular velocity $\vec{\Omega}$
- Vector function $\vec{Q}(t)$ varies in direction and magnitude.



Rate of Change wrt a Rotating Frame



- Wrt the rotating $Oxyz$ frame,

$$\vec{Q} = Q_x \vec{i} + Q_y \vec{j} + Q_z \vec{k}$$

$$\left(\dot{\vec{Q}} \right)_{Oxyz} = \dot{Q}_x \vec{i} + \dot{Q}_y \vec{j} + \dot{Q}_z \vec{k}$$

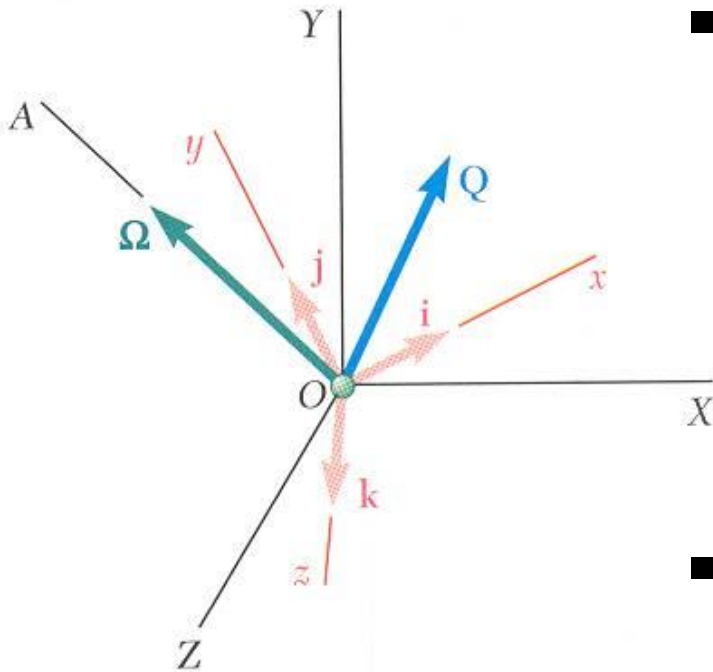
- Wrt the fixed $OXYZ$ frame,

$$\left(\dot{\vec{Q}} \right)_{OXYZ} = \dot{Q}_x \vec{i} + \dot{Q}_y \vec{j} + \dot{Q}_z \vec{k} + Q_x \dot{\vec{i}} + Q_y \dot{\vec{j}} + Q_z \dot{\vec{k}}$$

$$\dot{Q}_x \vec{i} + \dot{Q}_y \vec{j} + \dot{Q}_z \vec{k} = \left(\dot{\vec{Q}} \right)_{Oxyz}$$

= rate of change wrt rotating frame

Rate of Change wrt a Rotating Frame



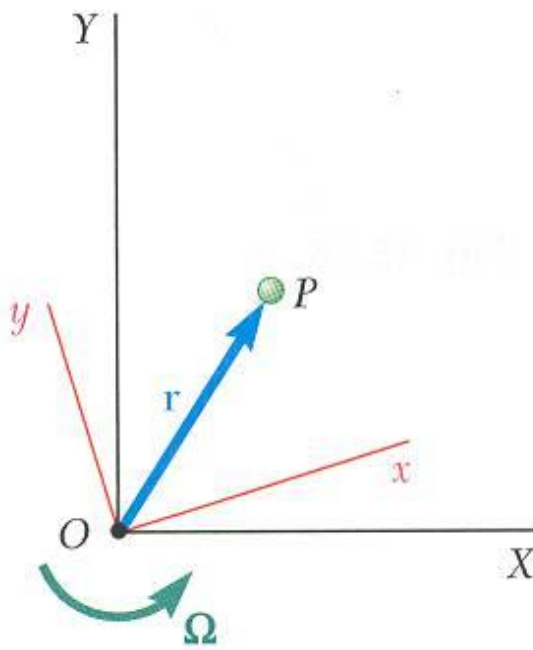
- If \vec{Q} were fixed within $Oxyz$ then $(\dot{\vec{Q}})_{OXYZ}$ is equivalent to velocity of a point in a rigid body attached to $Oxyz$ and

$$Q_x \dot{\vec{i}} + Q_y \dot{\vec{j}} + Q_z \dot{\vec{k}} = \vec{\Omega} \times \vec{Q}$$

- wrt to the fixed $OXYZ$ frame,

$$(\dot{\vec{Q}})_{OXYZ} = (\dot{\vec{Q}})_{Oxyz} + \vec{\Omega} \times \vec{Q}$$

Coriolis Acceleration



- Frame OXY is fixed
- frame Oxy rotates with angular velocity $\vec{\Omega}$.
- Position vector \vec{r}_P for particle P is the same in both frames
- Rate of change depends on choice of frame
- Absolute velocity of particle P is

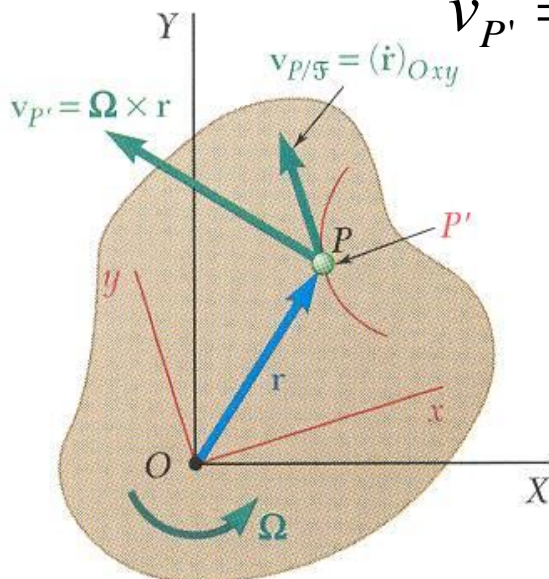
$$\vec{v}_P = \left(\dot{\vec{r}}\right)_{OXY} = \vec{\Omega} \times \vec{r} + \left(\dot{\vec{r}}\right)_{Oxy}$$

Coriolis Acceleration

- A rigid slab attached to rotating frame Oxy (\mathcal{F}).
- P' = point on slab which corresponds instantaneously to position of particle P

$\vec{v}_{P/\mathcal{F}} = \left(\dot{\vec{r}}\right)_{Oxy}$ = velocity of P along its path on the slab

$\vec{v}_{P'}$ = absolute velocity of point P' on the slab



- Absolute velocity for particle P may be written as

$$\vec{v}_P = \vec{v}_{P'} + \vec{v}_{P/\mathcal{F}}$$

$$\vec{v}_P = \vec{\Omega} \times \vec{r} + \left(\dot{\vec{r}}\right)_{Oxy}$$

$$= \vec{v}_{P'} + \vec{v}_{P/\mathcal{F}}$$

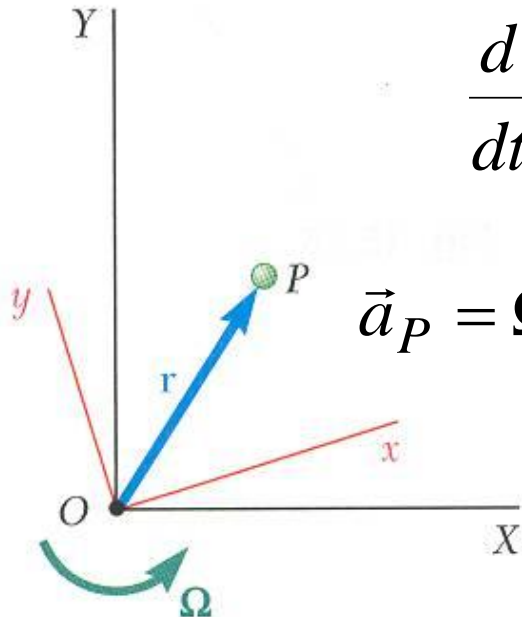
Coriolis Acceleration

- Absolute acceleration for particle P is

$$\vec{a}_P = \dot{\vec{\Omega}} \times \vec{r} + \vec{\Omega} \times (\dot{\vec{r}})_{OXY} + \frac{d}{dt} [(\dot{\vec{r}})_{Oxy}]$$

$$(\dot{\vec{r}})_{OXY} = \vec{\Omega} \times \vec{r} + (\dot{\vec{r}})_{Oxy}$$

$$\frac{d}{dt} [(\dot{\vec{r}})_{Oxy}] = (\ddot{\vec{r}})_{Oxy} + \vec{\Omega} \times (\dot{\vec{r}})_{Oxy}$$



$$\vec{a}_P = \dot{\vec{\Omega}} \times \vec{r} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}) + 2\vec{\Omega} \times (\dot{\vec{r}})_{Oxy} + (\ddot{\vec{r}})_{Oxy}$$

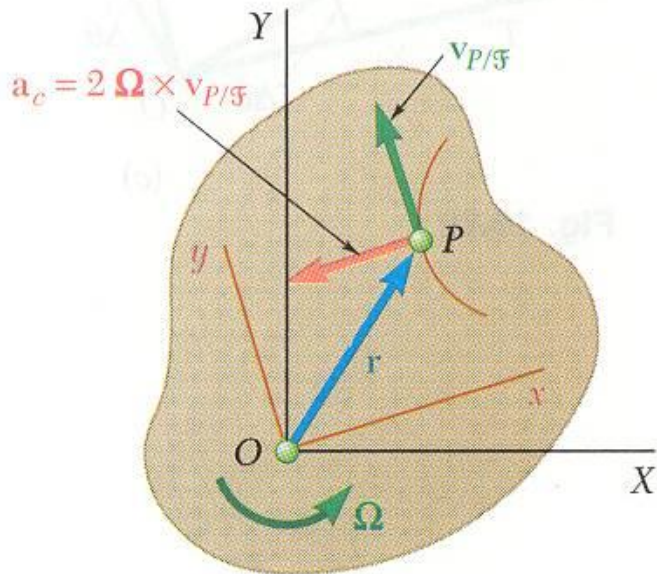
Coriolis Acceleration

- Utilizing the conceptual point P' on the slab,

$$\vec{a}_{P'} = \dot{\vec{\Omega}} \times \vec{r} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r})$$

$$\vec{a}_{P/\mathcal{F}} = \left(\ddot{\vec{r}} \right)_{Oxy}$$

- Absolute acceleration for the particle P becomes



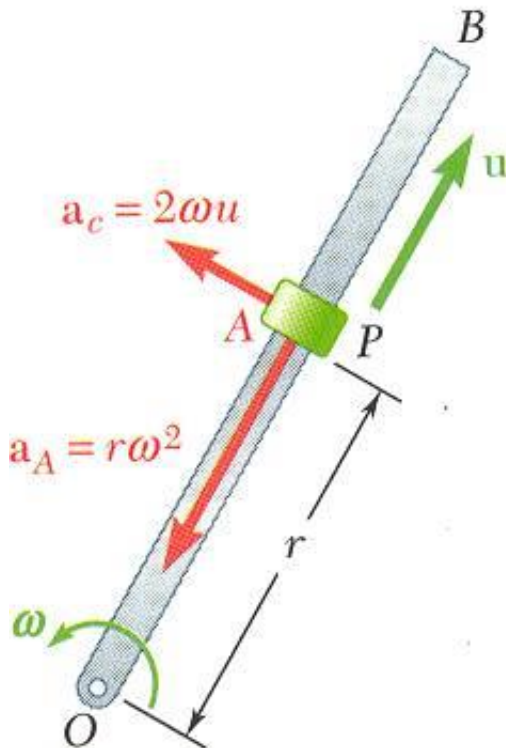
$$\vec{a}_P = \vec{a}_{P'} + \vec{a}_{P/F} + 2\vec{\Omega} \times \left(\dot{\vec{r}} \right)_{Oxy}$$

$$= \vec{a}_{P'} + \vec{a}_{P/F} + \vec{a}_c$$

$$\vec{a}_c = 2\vec{\Omega} \times \left(\dot{\vec{r}} \right)_{Oxy} = 2\vec{\Omega} \times \vec{v}_{P/F} =$$

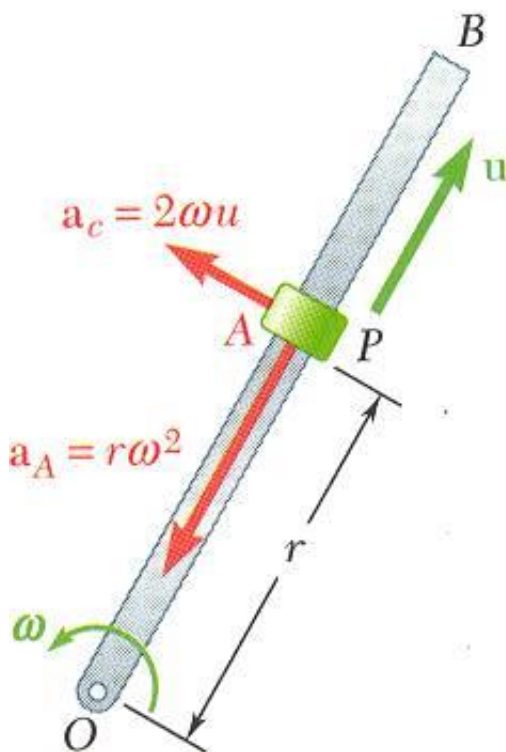
$$= \text{Coriolis acceleration}$$

Coriolis Acceleration



- Collar P is sliding at constant relative velocity u along rod OB.
- The rod is rotating at a constant angular velocity ω .
- Point A on the rod corresponds to instantaneous position of P.

Coriolis Acceleration



- Absolute acceleration of collar is

$$\vec{a}_P = \vec{a}_A + \vec{a}_{P/\mathcal{F}} + \vec{a}_c$$

$$\vec{a}_A = \dot{\vec{\Omega}} \times \vec{r} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}) \quad a_A = r\omega^2$$

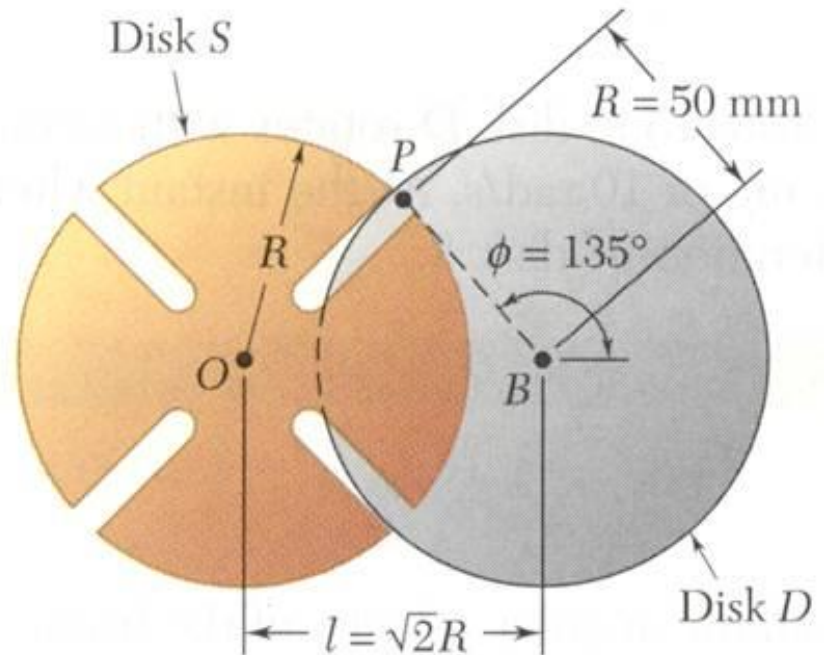
$$\vec{a}_{P/\mathcal{F}} = (\ddot{\vec{r}})_{Oxy} = 0$$

$$\vec{a}_c = 2\vec{\Omega} \times \vec{v}_{P/\mathcal{F}} \quad a_c = 2\omega u$$

Sample Problem 15.9

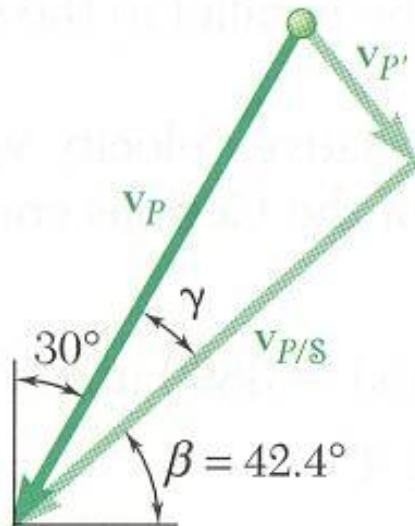
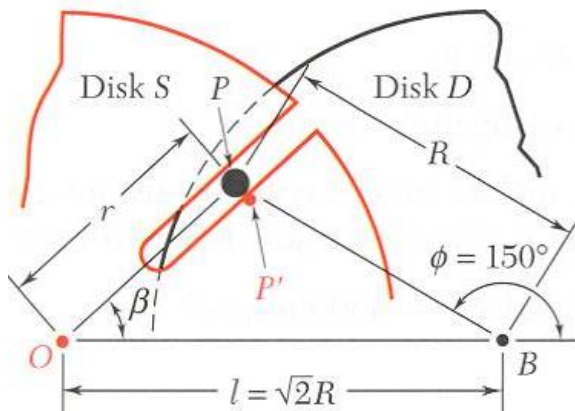
Disk D of the Geneva mechanism rotates with constant ccw angular velocity $\omega_D = 10 \text{ rad/s}$. At the instant when $\phi = 150^\circ$, determine:

- angular velocity of disk S
- velocity of pin P relative to disk S



Sample Problem 15.9

Solution:



- Absolute velocity of point P :

$$\vec{v}_P = \vec{v}_{P'} + \vec{v}_{P/S}$$

- Magnitude & direction of absolute velocity of pin P :

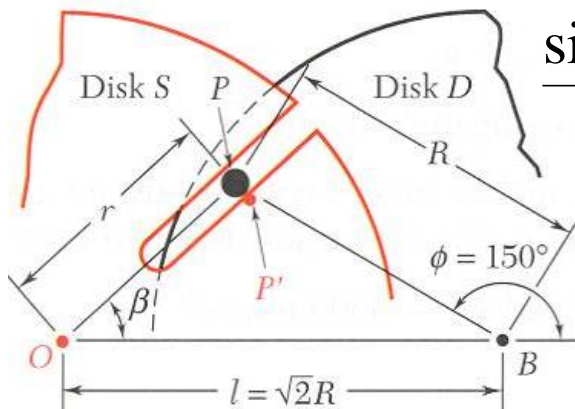
$$v_P = R\omega_D = (50 \text{ mm})(10 \text{ rad/s}) = 500 \text{ mm/s}$$

- Direction of velocity of P wrt S is parallel to slot. From the law of cosines,

$$r^2 = R^2 + l^2 - 2Rl \cos 30^\circ = 0.551R^2$$

$$r = 37.1 \text{ mm}$$

Sample Problem 15.9



$$\frac{\sin \beta}{R} = \frac{\sin 30^\circ}{r} \quad \sin \beta = \frac{\sin 30^\circ}{0.742} \quad \beta = 42.4^\circ$$

$$\gamma = 90^\circ - 42.4^\circ - 30^\circ = 17.6^\circ$$

$$v_{P'} = v_P \sin \gamma = (500 \text{ mm/s}) \sin 17.6^\circ = 151.2 \text{ mm/s}$$

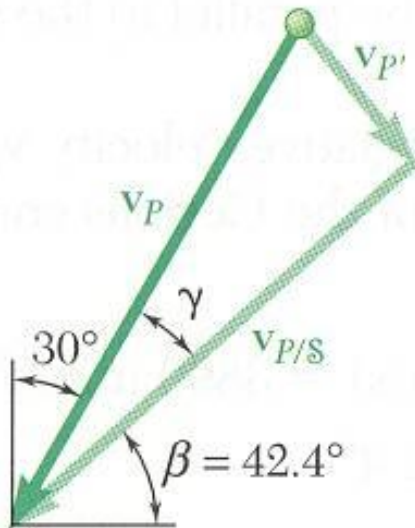
$$= r \omega_s \quad \omega_s = \frac{151.2 \text{ mm/s}}{37.1 \text{ mm}}$$

$$\vec{\omega}_s = (-4.08 \text{ rad/s}) \vec{k}$$

$$v_{P/S} = v_P \cos \gamma = (500 \text{ m/s}) \cos 17.6^\circ$$

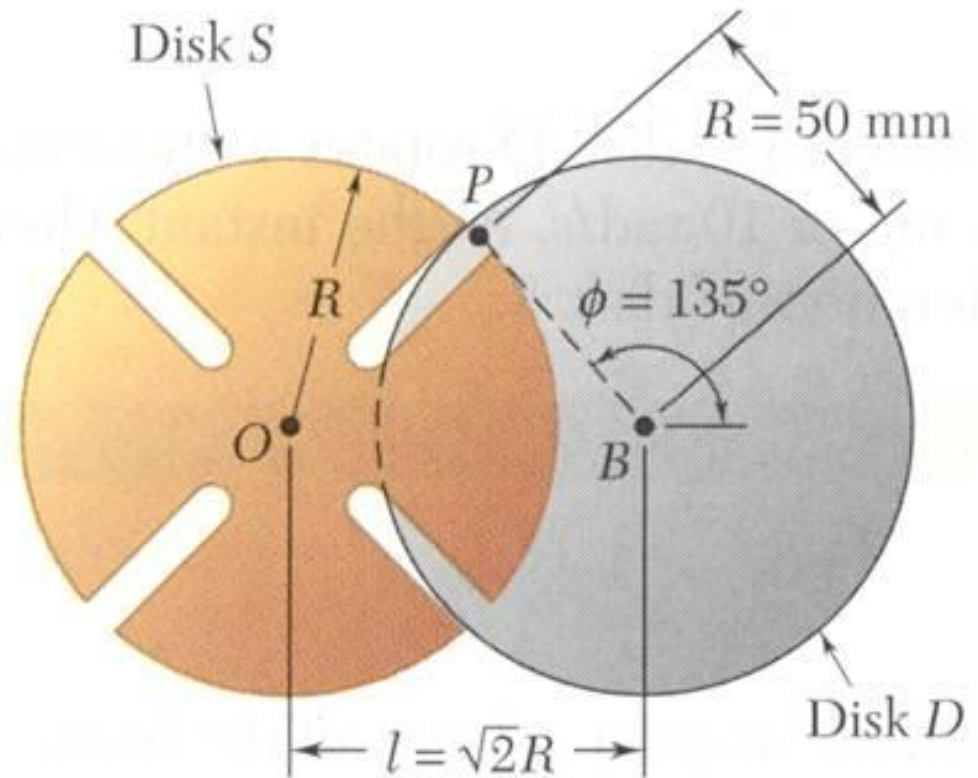
$$\vec{v}_{P/S} = (477 \text{ m/s}) (-\cos 42.4^\circ \vec{i} - \sin 42.4^\circ \vec{j})$$

$$v_P = 500 \text{ mm/s}$$

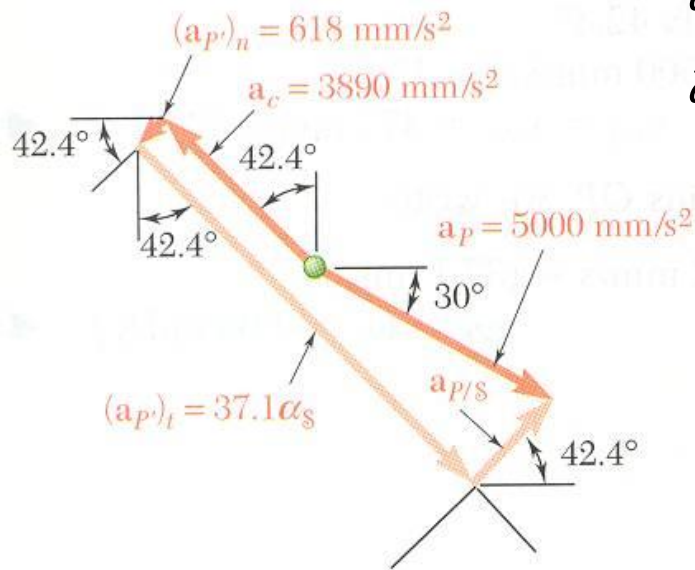
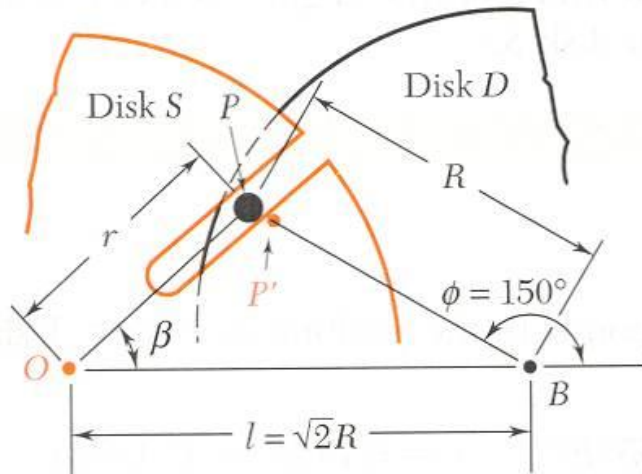


Sample Problem 15.10

In the Geneva mechanism, disk D rotates with a constant ccw angular velocity of 10 rad/s . At the instant when $\phi = 150^\circ$, determine angular acceleration of disk S .



Sample Problem 15.10



Solution: $\vec{a}_P = \vec{a}_{P'} + \vec{a}_{P/S} + \vec{a}_c$

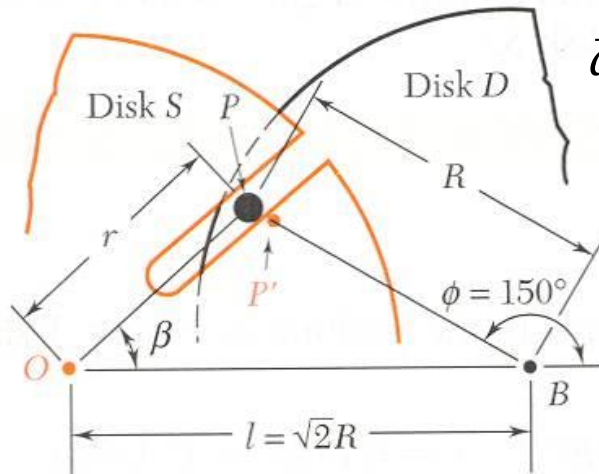
$$\beta = 42.4^\circ \quad \vec{\omega}_S = (-4.08 \text{ rad/s})\vec{k}$$

$$\vec{v}_{P/S} = (477 \text{ mm/s})(-\cos 42.4^\circ \vec{i} - \sin 42.4^\circ \vec{j})$$

$$a_P = R\omega_D^2 = (500 \text{ mm})(10 \text{ rad/s})^2 = 5000 \text{ mm/s}^2$$

$$\vec{a}_P = (5000 \text{ mm/s}^2)(\cos 30^\circ \vec{i} - \sin 30^\circ \vec{j})$$

Sample Problem 15.10

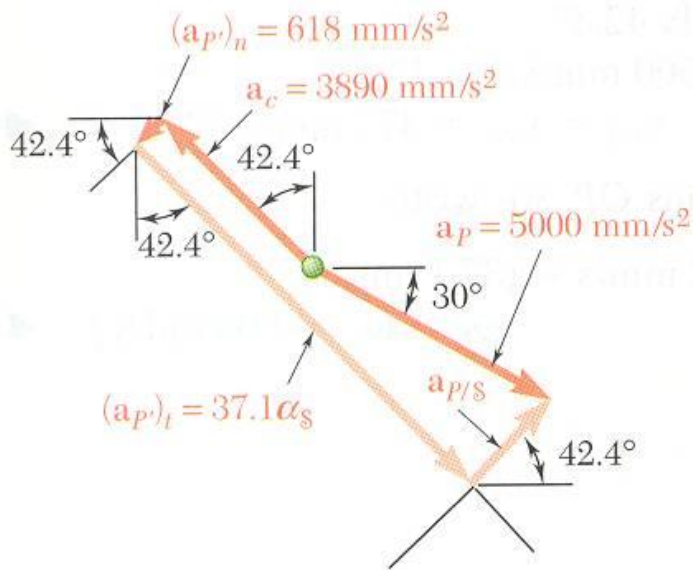


$$\vec{a}_{P'} = (\vec{a}_{P'})_n + (\vec{a}_{P'})_t$$

$$(\vec{a}_{P'})_n = (r\omega_S^2)(-\cos 42.4^\circ \vec{i} - \sin 42.4^\circ \vec{j})$$

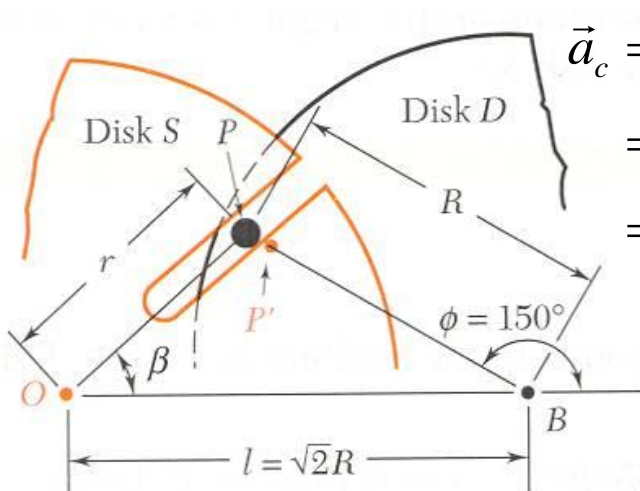
$$(\vec{a}_{P'})_t = (r\alpha_S)(-\sin 42.4^\circ \vec{i} + \cos 42.4^\circ \vec{j})$$

$$(\vec{a}_{P'})_t = (\alpha_S)(37.1 \text{ mm})(-\sin 42.4^\circ \vec{i} + \cos 42.4^\circ \vec{j})$$



- Direction of Coriolis acceleration is obtained by rotating direction of relative velocity $\vec{v}_{P/S}$ by 90° in the sense of ω_S .

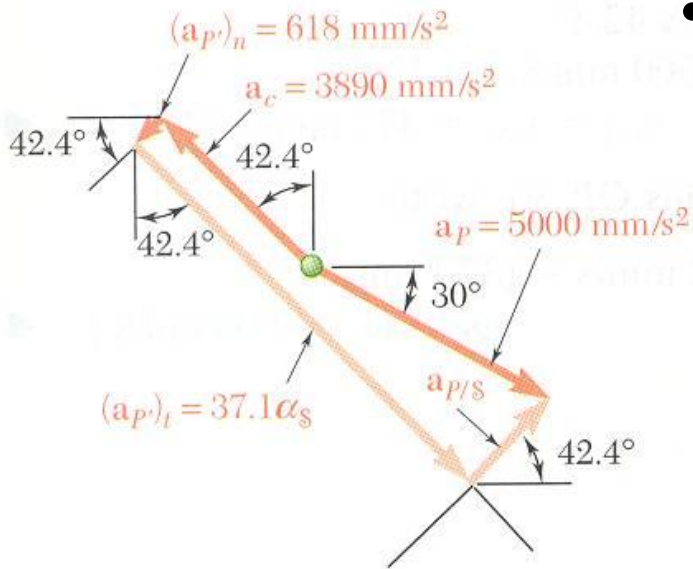
Sample Problem 15.10



$$\begin{aligned}\vec{a}_c &= (2\omega_S v_{P/S}) \left(-\sin 42.4^\circ \vec{i} + \cos 42.4^\circ \vec{j} \right) \\ &= 2(4.08 \text{ rad/s})(477 \text{ mm/s}) \left(-\sin 42.4^\circ \vec{i} + \cos 42.4^\circ \vec{j} \right) \\ &= (3890 \text{ mm/s}^2) \left(-\sin 42.4^\circ \vec{i} + \cos 42.4^\circ \vec{j} \right)\end{aligned}$$

- Relative acceleration $\vec{a}_{P/S}$ must be parallel to the slot.

- Equating components perpendicular to slot,



$$37.1\alpha_S + 3890 - 5000 \cos 17.7^\circ = 0$$

$$\alpha_S = -233 \text{ rad/s}$$

$$\vec{\alpha}_S = (-233 \text{ rad/s}) \vec{k}$$

Home Work Assignment # 15.5

150, 158, 166, 172, 179

Due

Saturday 12/4/2014 (Civil)

Sunday 13/4/2014 (Mechanical)