

# Measurement and modeling of the mechanical and electrochemical response of amorphous *Si* thin film electrodes during cyclic lithiation

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# Mechanical-Electrochemical response of *Si* thin film anodes

## *Potential impact*

**Silicon high capacity** ( $3579\text{Ah/kg}$ ) can increase the theoretical energy density and specific energy of the cell of 25-30% respect to existing graphite-based lithium-ion cells

## *Open issues*

**Large deformations** (a volumetric strain of about 270%) generate plastic flow and substantial stresses in the material, leading to mechanical failure after a few charge-discharge cycles

First-lithiation **capacity loss** due to solid-electrolyte interface formation and **side reactions**, continuously occurring during cycling, have been detrimental to the commercialization of the system

## *Our contribution*

**To aid the development of failure tolerant architectures**, we develop a continuum model that predicts stress, plastic flow, diffusion and the electrochemical response of *Si* during lithiation

## *Test and Calibration*

**In situ measurements** from **ad hoc experiments** are used to calibrate and verify the predictive capability of the model

# State of art

An extensive literature exists on the electrochemical and mechanical response of *Si* anodes and variety of designs have been explored, including

- thin films
- single particles
- nanowires
- patterned electrodes
- composites

Panasonic Corporation announced commercialization of high-capacity lithium-ion batteries with silicon-alloy anode

Accurate predictions require reliable values for *material parameters*, in particular:

- **mechanical properties** of *Si* as functions of *Li* concentration
- **transport properties** of *Li* through *Si*
- parameters related to the **solution chemistry** of *Li* in *Si* (i.e. the concentration dependent activity coefficient)
- parameters characterizing the **electrochemical** main and side **reactions**

# Mechanical parameters in constitutive laws of lithiated $Si$

## Literature data

Continuum models, following results from experimental measurements [Sethuraman et al., 2010] and first principle calculations [Shenoy & Johary, 2010], typically assume that Young's modulus decrease linearly with  $Li$  concentration [Deshpande et al., 2010] [Bower et al., 2010]

In [Shenoy & Johary, 2010], the authors attribute the elastic softening to the reduced stiffness of  $Li-Si$  bonds in comparison to  $Si-Si$  bonds.

Plastic flow has been observed [Sethuraman & Guduru, 2010] when the stress reaches approximately  $1GPa$

## Our contribution

Through a systematic combination of numerical simulations and experimental measurements of the resulting cycle of stress in  $a-Si$  film electrodes, we determined the parameters characterizing the variation of elastic modulus with concentration, together with the parameters that govern the rate dependent plastic flow in the film.

# Lithium transport and kinetics, modeling and measurements of PITT experiments

## Literature data

**Power density** of *Li*-ion cells is strictly related to the **diffusion coefficient** for *Li* transport through electrode materials. The range of values available in literature, from experiments [Xiao et al., 2012] and atomistic scale calculations [Tritsarlis et al., 2012], span over several orders of magnitude.

Parameters characterizing solution thermodynamics and *Li* insertion reactions can be extracted from the potential vs. composition curve available in literature from experimental measurements [Hatchard et al., 2004] and ab-initio DFT calculations [Chevrier & Dahn, 2009].

## Our contribution

Lithium diffusivity and reaction rate constant were determined by fitting full numerical simulation of PITT tests to the experimental data.

Our approach respect to the classical model [Weppner & Huggins, 1977] accounts rigorously for **departures from the ideal diffusion model**

# Governing Equations

## Finite element model in 1D spatial set

$$\rho_{Si} \frac{dc}{dt} = - \frac{\partial j_X}{\partial X} \quad j = - \frac{D}{RT} \rho_{Si} c \frac{\partial \mu}{\partial x}$$
$$\mu = \mu(c, \sigma)$$

Diffusion equation

Chemical potential eq.

## Boundary conditions in galvanostatic tests

$$j_X(H) = \frac{I_R + I_S}{F} \quad j_X(0) = 0$$

Cell voltage computed through Newton's procedure applied to the Butler-Volmer eq

## Boundary conditions in potentiastatic tests

$$j_X(H) = \frac{I(V - U_0(c, \sigma))}{F} \quad j_X(0) = 0$$

Cell voltage  $V$  assigned

## Mechanical Model of a half-cell with a thin-film *Si* anode

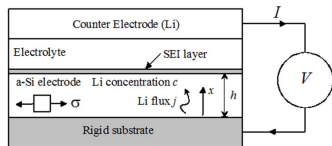
*Li* insertion causes the stress-free *Si* network to increase its volume by a fraction  $dV/dV_0 = 1 + \beta c$  proportional to *Li* molar concentration  $c$ , with a corresponding true strain  $\epsilon_{xx}^c = \epsilon_{yy}^c = \epsilon_{zz}^c = \log(1 + \beta c)/3$ .

Since the substrate prevents the film from expanding in its own plane, the strains are related by the compatibility conditions

$$\frac{1}{3} \log(1 + \beta c) - 2 \log(\lambda^p) + \epsilon_{xx}^e = \log \left( 1 + \frac{\partial u}{\partial X} \right)$$

$$\frac{1}{3} \log(1 + \beta c) + \log(\lambda^p) + \epsilon_{yy}^e = 0$$

$$\frac{1}{3} \log(1 + \beta c) + \log(\lambda^p) + \epsilon_{zz}^e = 0$$



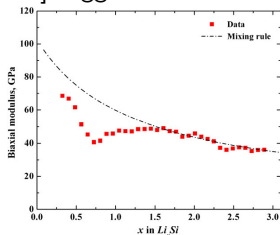
Assuming a plane stress condition, the Cauchy stress  $\sigma(x) = \sigma_{yy} = \sigma_{zz}$  is related to (small) elastic strains by a concentration dependent biaxial modulus

$$\sigma = M(c) \epsilon_{yy}^e$$

Experimental measurements [Sethuraman et al. 2010] suggest that

1. A suitable constitutive law for the biaxial modulus can be a logarithmic function of the kind

$$M(c) = M_0 + M_1 \log \left( 1 + \frac{c}{c_0} \right)$$



2. The plastic deformation can be characterized by a viscoplastic constitutive equation relating the plastic stretch rate to stress

$$\dot{\epsilon}_{yy}^p = \dot{\epsilon}_{zz}^p = \frac{\dot{\lambda}^p}{\lambda^p} = \frac{\dot{\epsilon}_0}{2} \left( \frac{|\sigma|}{\sigma_0} - 1 \right)^m \frac{\sigma}{|\sigma|} \quad \text{if } |\sigma| \geq \sigma_0$$

$$\dot{\epsilon}_{yy}^p = \dot{\epsilon}_{zz}^p = 0 \quad \text{if } |\sigma| < \sigma_0$$

where  $\sigma_0$  is a concentration dependent yield stress;  $\dot{\epsilon}_0$  is a characteristic strain rate, and  $m$  a stress exponent

3. The yield stress constitutive law is assumed to be a linear function of lithium concentration

$$\sigma_0(c) = s_0 + s_1(c - c_0)$$



## Solution thermodynamics and $Li$ transport

Diffusion of  $Li$  through the  $Si$  electrode is driven by a chemical potential

$$\mu = \mu^\theta + RT \ln \left( \frac{c\gamma}{c_{max} - c} \right) - \frac{\sigma^2}{\rho_{Si}} \frac{\partial}{\partial c} \left( \frac{1}{M} \right) - \frac{2\beta\sigma}{3(1 + \beta c)\rho_{Si}}$$

It accounts for higher order interactions in non infinite dilute solutions (through the activity coefficient  $\gamma$ ) and for the mechanical contribution, whose derivation is described by several authors [Larché & Cahn, 1973] [Li, 1978] [Bower et al. 2011].

As proposed in literature [Verbrugge et al. 1996], we assume the excess of free energy expressed as a series expansion in  $c/c_{max}$  and we adopt the following form for the activity coefficient

$$RT \ln \gamma = \sum_{n=2}^N \Omega_n n \left( \frac{c}{c_{max}} \right)^{n-1}$$

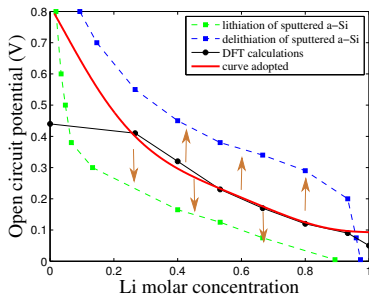
where  $\Omega_n$  are self-interaction coefficient,  $c_{max}$  the maximum number of hosting sites available.

The open circuit potential is expressed by  $U_0(c, \sigma) = -\mu(c, \sigma)/F$

# Solution thermodynamics and $Li$ transport

Series expansion coefficients  $\Omega_n$  are calibrated respect the to potential-v-capacity curves available in literature [Baggetto et al., 2008], [Chevrier & Dahn, 2009].

$$U_0 = U_0^\theta - \frac{RT}{F} \ln \left( \frac{c\gamma}{c_{max} - c} \right) - \sum_{n=2}^N \Omega_n n \left( \frac{c}{c_{max}} \right)^{n-1} + \frac{\sigma^2}{F\rho_{Si}} \frac{\partial}{\partial c} \left( \frac{1}{M} \right) + \frac{2\beta\sigma}{3F(1 + \beta c)\rho_{Si}}$$

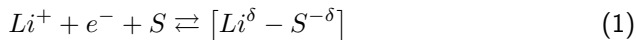


In [Sethuramna et al., 2010] the magnitude of the **stress-potential coupling** in lithiated silicon is estimated to be  $62mV/GPa$  in thin-film geometry

- $\sigma = -1GPa \rightarrow -62mV$
- $\sigma = 1GPa \rightarrow 62mV$

## Electrochemical reactions

At discharging, an electrochemical reaction takes place at the  $Si$ /electrolyte interface, where  $Li$  ions in the electrolyte combine with electrons and are inserted into host sites  $S$  in the  $Si$  network



The Butler-Volmer equation relates the current density  $I_R$  of the Faradaic reaction to the over-potential  $\eta$  at the solid/electrolyte interface as follows

$$I_R = i_0 \left[ \exp\left(\frac{\alpha F \eta}{RT}\right) - \exp\left(\frac{(1 - \alpha) F \eta}{RT}\right) \right] \quad (2)$$

where the exchange current density may be expressed

$$i_0 = F \left[ k_c \rho^+ \left( 1 - \frac{c}{c_{max}} \right) \right]^\alpha \left( k_a \frac{c}{c_{max}} \right)^{(1-\alpha)}$$

$k_c$  and  $k_a$  are the concentration dependent cathodic and anodic rate constants;  $\rho^+$  is the molar density of  $Li^+$  per unit of reference volume in electrolyte.

$$(\rho_{Li^+} k_c)^\alpha k_a^{1-\alpha} = k_0 + k_1 \sin\left(\frac{\pi}{2} \frac{c}{c_{max}}\right)$$

# Modeling of the capacity loss due to SEI layer formation

Side reactions occur at the negative electrode/electrolyte interface whenever the electrode potential falls below the value  $U_{0,SEI}$  necessary to reduce the electrolyte.

Standard SEI models predict that the SEI thickness and total capacity loss vary with time as  $t^{1/2}$  and give a good fit to measurements over a long time period [Pinson & Bazant, 2013] but do not fit our experimental data for a small number of cycles.

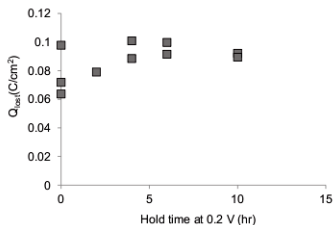


Figure: [Nadimpalli et al., 2012]

We have therefore used a simple phenomenological relation to fit our data

$$I_S = -i_{0,SEI} \left( 1 - \frac{Q_{loss}}{Q_{SEI}} \right) \exp \left( -\frac{2\alpha_{SEI}F}{RT} (V - U_{0,SEI}) \right); \quad Q_{loss} = - \int I_S dt$$

# Discussion of the results

*Experiment description* Half cell made with sputtered amorphous *Si* thin film electrodes and *Li* metal counter-electrode have been subjected to cyclic galvanostatic tests

- lower cut-off voltage of  $0.05V$  vs.  $Li/Li^+$  to prevent crystallization
- upper cut-off voltage of  $0.6V$  vs.  $Li/Li^+$  to prevent film cracking

## *Output of interest*

- Cell Voltage
- Mean stress over the film thickness

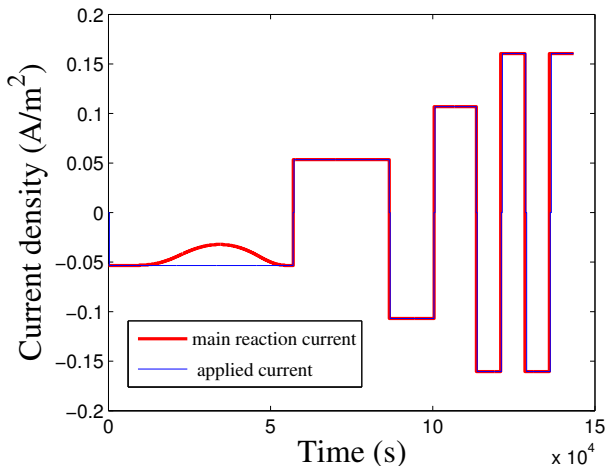
## *Procedure*

- **Cell 151** experimental results adopted for calibrating the model
- **Cell 200** used for verifying the predictive capability of the model

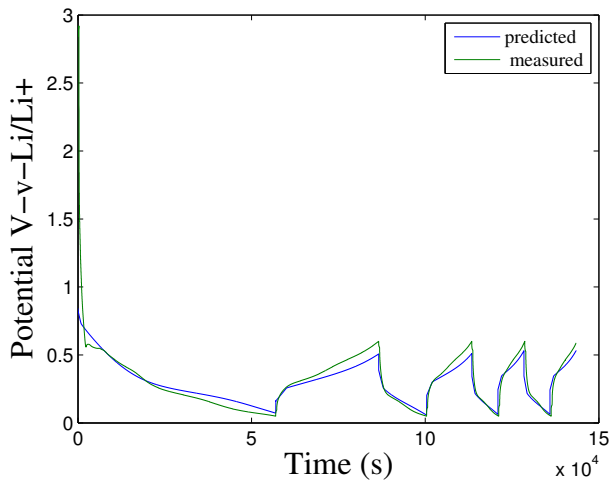
## Numerical results Cell 151

Amorphous *Si* film of  $100\text{nm}$  thickness and  $18.7 \cdot 10^{-4}\text{m}^2$  surface area. Initial residual stress of  $-0.1\text{ GPa}$ .

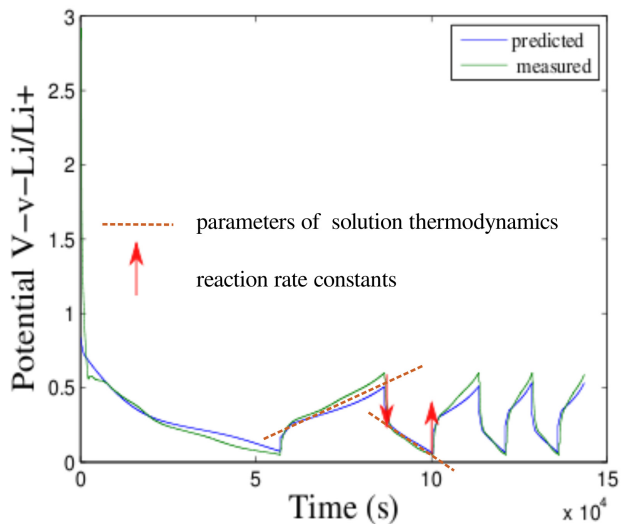
It undergoes cycles of alternate current of 100, 200, 300,  $\mu\text{A}$ .



# Numerical results Cell 151

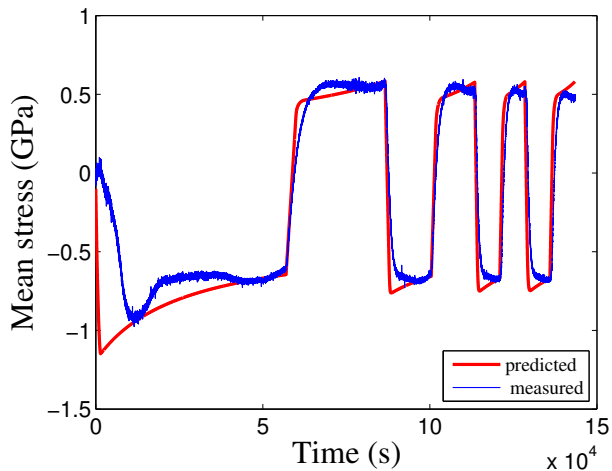


# Numerical results Cell 151



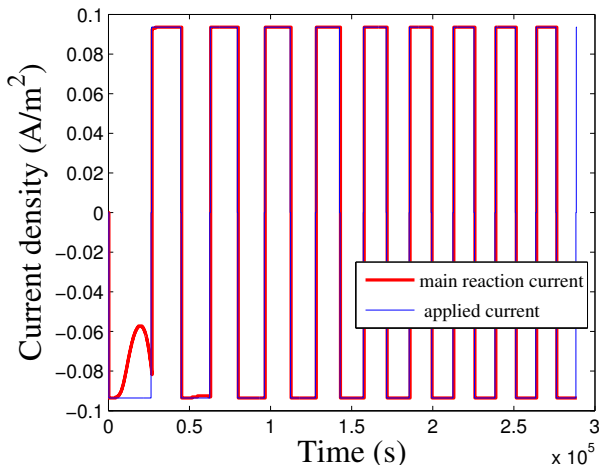


# Numerical results Cell 151

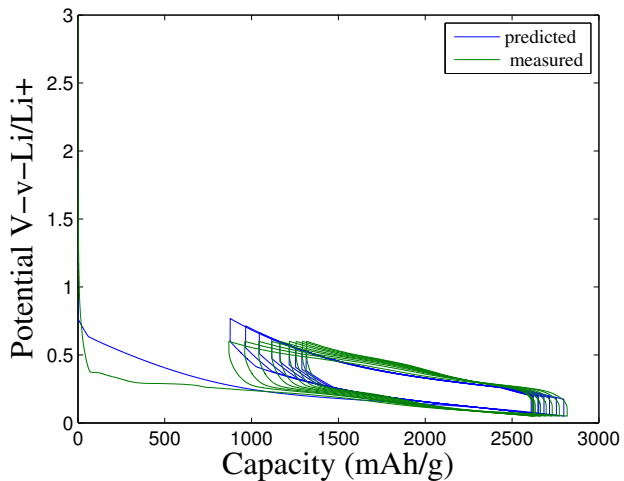


## Numerical results Cell 200

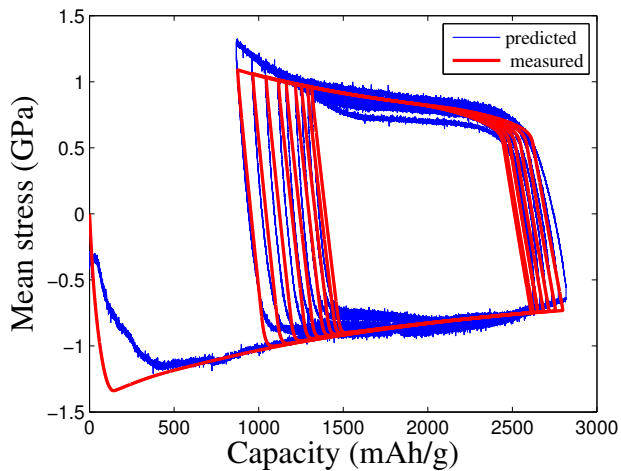
Amorphous *Si* film of  $123\text{nm}$  thickness and  $18.7 \cdot 10^{-4}\text{m}^2$  surface area.  
Initial residual stress of  $-0.36\text{ GPa}$ .  
It undergoes cycles of alternate current of  $175\text{ }\mu\text{A}$ .



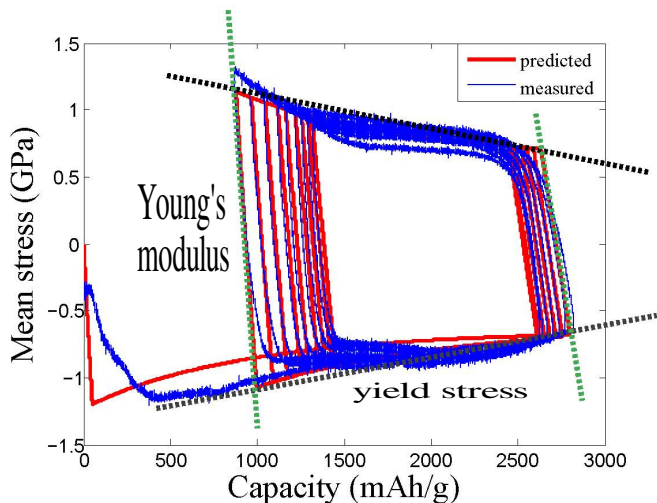
## Numerical results Cell 200



## Numerical results Cell 200



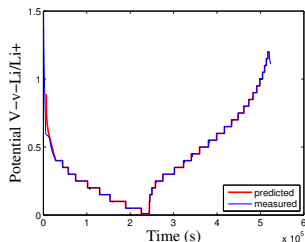
## Numerical results Cell 200



# PITT experiment

## Experiment description

- Half cell made of  $104\text{nm}$   $a\text{-Si}$  thin film electrode against a lithium metal reference and counter electrode
- Lithium insertion was carried out galvanostatically at  $2.5\mu\text{A}/\text{cm}^2$  until the electrode potential reached  $0.4\text{V}$  vs.  $\text{Li}/\text{Li}^+$
- Incremental step changes in potential of  $50\text{mV}$  are applied until  $0.05\text{V}$  vs.  $\text{Li}/\text{Li}^+$ . Each potentiostatic step was carried out until the current decayed to less than  $0.25\mu\text{A}/\text{cm}^2$
- Identical potentiostatic steps in the delithiation direction followed till  $1.2\text{V}$  vs.  $\text{Li}/\text{Li}^+$



*Output of interest* Transient evolution of stress and electric current density

# PITT experiment

Standard PITT measurements rely on the following hypotheses:

- transport in the electrode obeys Fick's law
- $Li$  insertion reaction occurs sufficiently rapidly to ensure that transport in the electrode is the rate limiting process

which are not satisfied by our system.

For small perturbations in concentration  $\delta c$  relative to an initial concentration, the governing equations of diffusion (combined and linearized) yield

$$\frac{\partial \delta c}{\partial t} = \tilde{D} \frac{\partial^2 \delta c}{\partial x^2} \quad \tilde{D} = D \frac{c}{RT} \left[ \left. \frac{\partial \mu}{\partial c} \right|_{\sigma} + \frac{\partial \mu}{\partial \sigma} \left|_c \frac{\partial \sigma}{\partial c} \right. \right]$$

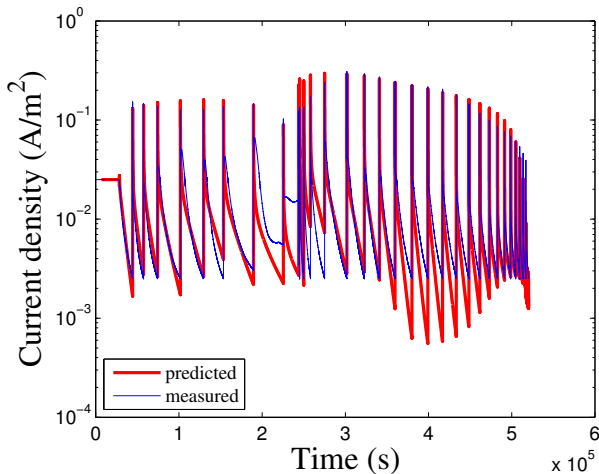
where the apparent diffusion coefficient  $\tilde{D}$ , extracted for PITT measurements, is history dependent.

The effects of stress can be minimized by ensuring that the voltage step  $\delta V$  tends to deform the electrode plastically.

This is the reason to prefer PITT to GITT experiments.

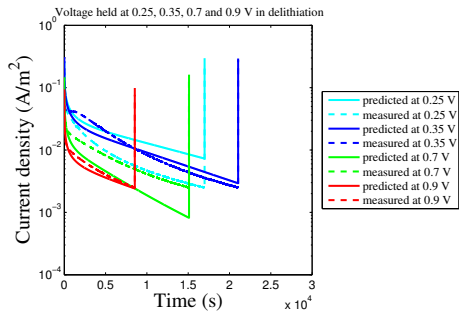
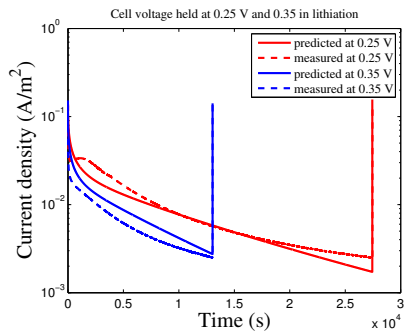
# PITT experiment

Comparison of transient electric current density measured and predicted by assuming in the model  $D = 10^{-19} m^2 s^{-1}$





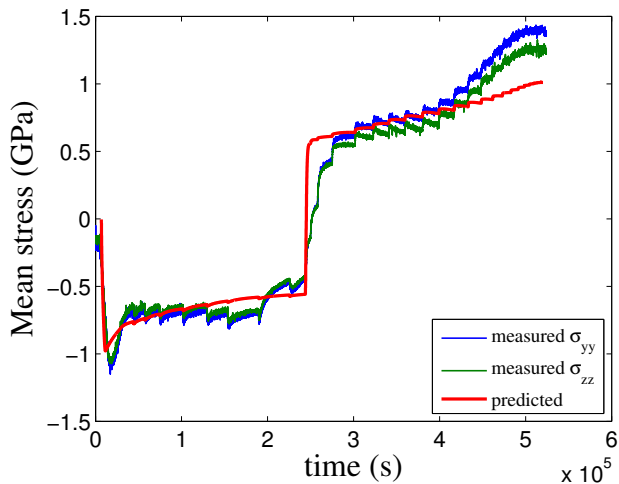
# PITT experiment



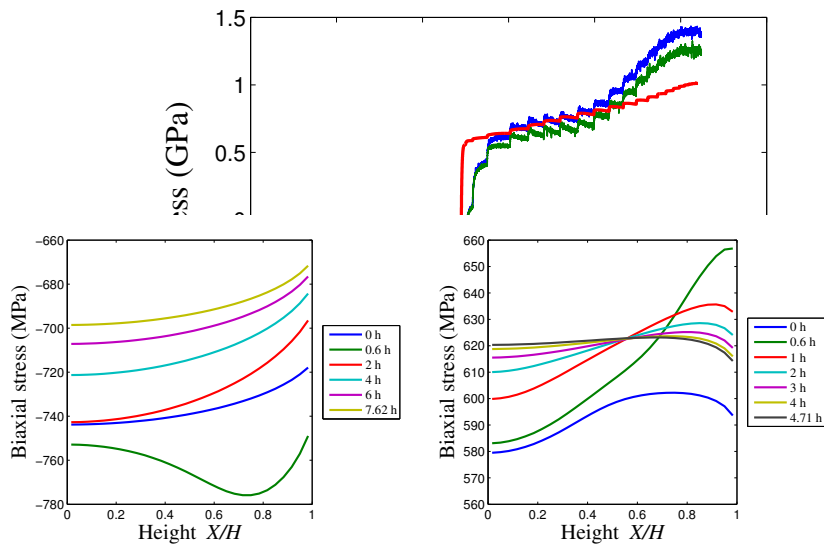
# PITT experiment

video

# PITT experiment



# PITT experiment



## Conclusions and Future work

- 1 Combination of **experiments and modeling** to determine mechanical and electrochemical response of amorphous *Si* films under cyclic *Li* insertion.
- 2 The variation of **elastic biaxial modulus** was fit using a logarithmic variation with *Li* concentration. The Young's modulus was found to vary from  $80 \text{ GPa}$  in the un-lithiated electrode to  $36.8 \text{ GPa}$  at full charge capacity. These values are in good agreement with previously reported data [Shenoy & Johari, 2010].
- 3 The inelastic response is described by a rate-dependent **elastic-viscoplastic** constitutive model, with a linear concentration dependent **flow stress** varying from  $0.60 \pm 0.04 \text{ GPa}$  at zero concentration to  $1.05 \pm 0.04 \text{ GPa}$  at full capacity, and a stress exponent of 50.
- 4 Secondary effects, such as capacity loss in SEI formation and *Li* – *Li* interactions, are taken into account. The activity coefficient of the *Li-Si* solid solution was characterized by a series expansion in  $c/c_{max}$  and it was calibrated to match the potential vs. capacity curves available in literature.

## Conclusions and Future work

- 1 PITT measurements, in combination with numerical simulations, were used to determine the **diffusion coefficient** for *Li* in *a-Si*. Experiments were best fit with a diffusion coefficient  $10^{-15} \text{cm}^2 \text{s}^{-1}$ , which is comparable to, but on the low end of the range  $10^{-16} - 10^{-10} \text{cm}^2 \text{s}^{-1}$  measured in previous experiments [Ding et al., 2009] [Ruffo et al., 2009] [Xiao et al., 2012] [Hüger et al., 2013].
- 2 The experiments were also used to estimate the variation of **exchange-current density** in the *Li* insertion reaction with concentration. It was found to be  $i_0 \sim O(10 \text{ A cm}^{-2})$ , comparable to the one obtained in [Chandrasekaran et al., 2010], while the values reported in literature for *Li-Si* battery systems [Bernardi & Newman, 1987] [Baggetto et al., 2009] vary by several orders of magnitude.
- 3 The 1D formulation, developed for the thin film anode case, is being extended to 3D composite configurations, where the active material is in the form of particles connected by a binder.