# Naval Diving and Salvage Training Center FORMULA BOOK 

IAW U.S. Navy Diving Manual



PREPARED BY
NAVAL DIVING AND SALVAGE TRAINING CENTER PANAMA CITY, FLORIDA

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## Changes

| DATE REVISED | REASON | INITIALS |
| :---: | :---: | :---: |
| 13 Jul 10 | CFR dated 20 Jun 10 | AMT |
| 21 Mar 11 | Updated Time Fuse Burn |  |
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## Surface Supplied Floodable Volumes

| FARCC | I/L 136 cu ft | O/L 65 cu ft | TOTAL <br> 201 cu ft |
| :---: | :---: | :---: | :---: |
| SNDL chamber | I/L 123 cu ft | O/L 69 cuft | 192 cu ft |
| RCF 5000 | I/L 162 cu ft | O/L 61 cuft | 223 cu ft |
| RCF6500 | I/L 440 cu ft | O/L 144 cu ft | 584 cu ft |
| TRCS | I/L 45 cu ft | O/L 45.5 cu ft | 90.5 cu ft |
| Army aluminum chamber | I/L 192 cu ft | O/L 37 cuft | 229 cu ft |
| Steel chamber | I/L 285 cu ft | O/L 140 cu ft | 425 cu ft |
| Steel chamber (T-ARS 50) | I/L 134 cu ft | O/L 68 cuft | 202 cu ft |
| Scuba tank alum. 100 | .470 cu ft |  |  |
| Scuba tank alum. 80 | .399 cu ft |  |  |
| Scuba tank alum. 63 | .319 cu ft |  |  |
| Scuba tank alum. 50 | .. 281 cu ft |  |  |
| Scuba tank steel 120 | .526 cu ft |  |  |
| Scuba tank steel 100 | .445 cu ft |  |  |
| Scuba tank steel 72 | .420 cu ft |  |  |
| O2 bottle (K) 1800 | 1.64 cu ft |  |  |
| O2 bottle (J) 3500 | 1.568 cu ft |  |  |
| O2 cylinder (E) (2015 psi) | . 163 cu ft |  |  |
| O2 cylinder (D) (2015 psi) | . 099 cu ft |  |  |
| FADS III - ASRA Flask | 3.15 cu ft |  |  |
| MK3 (LWDS) - Flask | .935 cu ft |  |  |
| SDASS - DASS Flask | 3.15 cu ft |  |  |
| SDASS - VTA Tank | 8 cu ft |  |  |
| Mini VTA | 4 cu ft |  |  |
| OSF Complex Volumes |  |  |  |
| - Wet chamber | 7100 cu ft |  |  |
| - 'A' and 'E' chambers | $440 \mathrm{cu} \mathrm{ft} \mathrm{(each)}$ |  |  |
| - 'B' and ' D ' chambers | 620 cu ft (each) |  |  |
| - 'C' chamber | 540 cu ft |  |  |
| - Trunk | 330 cu ft |  |  |
| - Service Lock (5 locks) | $3.7 \mathrm{cu} \mathrm{ft} \mathrm{(each)}$ |  |  |
| OSF Complex Total |  |  | 3300 cu ft |
| OSF Gas Flask ( 2400 psi ) <br> (8 @ 2400 psi) | 78.7 cu ft ea |  |  |

## Conversion Formulas

| Depth (fsw) to ATA : $\frac{(\text { Depth }+33)}{33}=$ ATA 33 | (Carry two decimal places) |
| :---: | :---: |
| ATA to Depth (fsw) : (ATA -1) X $33=$ Depth | (Round up to the next whole number) |
| PSIG to ATA : $\quad \frac{(\text { PSIG }+14.7)}{14.7}=$ ATA | (Carry two decimal places) |
| ATA to PSIG: $\quad(\mathrm{ATA}-1) \mathrm{X} 14.7=$ PSIG | (Round up to the next whole number) |
| Depth (fsw) to PSIG: Depth x . $445=$ PSIG | (Round up to the next whole number) |
| $\text { PSIG to Depth (fsw): } \frac{\text { PSIG }}{.445}=\text { Depth }$ | (Round up to the next whole number) |
| PP of gas ATA $\mathrm{x} \%$ gas $=\mathrm{PP}$ in ATA | (Carry two decimal places) |
| $\mathrm{SEV}=\frac{\mathrm{PP} @ \operatorname{depth}(\text { in ATA }) \times 100 \%}{1 \text { ATA }}$ | (Carry two decimal places) |
| $\mathrm{CO}_{2} \mathrm{SEV}=\frac{1.5}{\mathrm{ATA}} \quad\left(\mathrm{x} 100=\mathrm{CO}_{2} \%\right)$ | (Carry two decimal places) |
| PSIG to PSIA: $\quad$ PSIG + $14.7=$ PSIA | (Round up to next whole number) |
| Percentage to decimal: move decimal 2 place | or divide by 100 |
| Decimal to percent: move decimal 2 places | ght or multiply by 100 |
| Decimal to minutes or seconds: decimal x 60 | $=$ minutes of seconds |
| Minutes or seconds to decimal: $\frac{\text { minutes or s }}{60}$ | conds = decimal |
| PP in ATA to PP in mmHg: ATA X 760 |  |
| PP in mmHg to PP in ATA: mmHg divided by | y 760 |
| Percent to ppm: Move decimal 4 places right | or multiply by 10,000 |
| PPM to percent: Move decimal 4 places left or | divide by 10,000 |
| AIR/O2 Trading Ratio <br> at that stop Total Air | $\frac{\text { Stop time }}{\text { Stop time }}=\text { Air/O2 Trading Ratio }$ |
| AIR/O2 Period Conversion $\quad$ O2 Time | Remaining x 1.1 $=$ Chamber O2 Periods <br> (Round up to next whole minute)  |
| $\begin{array}{ll} \hline \text { SCF to ACF: } & \frac{\text { scf }}{\text { ata }}=\mathrm{acf} \\ \hline \end{array}$ | (Carry two decimal places) |
| ACF to SCF: $\quad$ ata $\times$ acf $=\mathrm{scf}$ | (Carry two decimal places) |
| Fahrenheit to Celsius: $\quad \frac{5(\mathrm{~F}-32)}{9}=\mathrm{C}$ | (Carry one decimal places) |
| Celsius to Fahrenheit: $\quad\left(\frac{9}{5} \mathrm{X} \mathrm{C}\right)+32=\mathrm{F} \quad$ (Carry one decimal place) |  |
| Fahrenheit to Absolute: $\quad \mathrm{F}+460=\mathrm{D}$ | grees Rankine |
| Celsius to Absolute: $\quad \mathrm{C}+273=\mathrm{D}$ | grees Kelvin |

## Divers Breathing Requirements (ACFM)

| System | Descent / <br> Bottom | Ascent/Decompression <br> Stops | Heavy Work / Free <br> Flow Vent |
| :--- | :---: | :---: | :---: |
| MK-21 | 1.4 ACFM | .75 | 6 ACFM / 8 ACFM |
| KM 37 | 1.4 ACFM | .75 | 6 ACFM / 8 ACFM |
| MK-20 | 1.4 ACFM |  |  |
| SCUBA | 1.4 ACFM |  | .3 ACFM |

## Surface Supplied Diving Formulas

## Minimum Manifold Requirements (MMP):

A) MK-20 / MK-21 / KM-37

1) 60 FSW or shallower
(D x .445) $+90=$ MMP (round up to next whole number)
2) 61 FSW to 130 fsw
$(\mathrm{D} \mathrm{x} \mathrm{.445)}+135=$ MMP (round up to next whole number)
3) 130 fsw or deeper
(D x .445) $+165=$ MMP (round up to next whole number

## Surface Supplied Diving Formulas (Continued)

## Compressors:

A) Rating: Capacity in SCFM and delivery of pressure in PSIG
B) Output: PSIG after charging - PSIG before charging $=$

$$
\frac{\text { PSIG charged }}{14.7}=\mathrm{ATM}
$$

ATM x N x FV $=$ SCF (round down to next whole number)

| N | $=$ number of flasks |
| :--- | :--- |
| FV | $=$ floodable volume of flasks $(\mathrm{cu} \mathrm{ft})$ |

$\frac{\text { SCF charged }}{\mathrm{T}} \quad=$ SCF output
$\mathrm{T}=$ Actual time to charge in minutes
C) Compressor percent efficiency:

Compressor SCFM output
Compressor SCFM rating
x $100=$ Percent efficiency
(Round down to next whole number)
D) Flow requirements:

ATA $\times$ ACFM x $\mathrm{N}=$ SCFM required (round up to next whole number)
ACFM - average consumption rate
N - number of divers including standby
E) Compressor depth limit: Note: add output of all compressors used to get total SCFM
(Use the shallower output of steps 1 and 2)

1) SCFM output:

Total SCFM x 33
ACFM x N
$-33=$ Depth Limit

Total SCFM - Output of compressor (s)
ACFM - Average consumption rate
N - Number of divers including standby
2) Pressure rating:

60 fsw or shallower
$\frac{\text { PSIG }-90}{.445}=\begin{aligned} & \text { Depth } \\ & \text { Limit }\end{aligned} \quad$ (round down to next whole number)

# Surface Supplied Diving Formulas (Continued) 

61 fsw to 130 fsw
$\frac{\text { PSIG }-135}{.445}=$ Limit $\quad$ (round down to next whole number)

130 fsw or deeper
$\frac{\text { PSIG }-165}{.445} \quad=$ Depth $\quad$ Limit $\quad$ (round down to next whole number)

$$
P S I G=\text { rated delivery pressure of compressor }
$$

F) Time to charge:

SCF deficit SCFM compressor output $=$ Time to charge (minutes) (Round up to next whole number)

## Duration of SCUBA Air Supply

There are three steps in calculating how long a diver's air supply will last:

1. Calculate the diver's consumption rate:

$$
\mathrm{C}=\frac{\mathrm{D}+33}{33} \times \mathrm{RMV}
$$

Where: $\quad \mathrm{C}=$ Diver's consumption rate, standard cubic feet per minute ( scfm ) D = Depth, fsw
RMV = Diver's Respiratory Minute Volume, actual cubic feet per minute (acfm)

## Duration of SCUBA Air Supply (Continued)

2. Calculate the available air capacity provided by the cylinders. The air capacity must be expressed as the capacity that will actually be available to the diver, rather than as a total capacity of the cylinder. The formula for calculating the available air capacity is:

$$
\begin{aligned}
& \qquad \begin{aligned}
& \mathrm{V}_{\mathrm{a}}=\underline{\mathrm{P}_{\mathrm{C}}}-\frac{\mathrm{P}_{\mathrm{m}}}{14.7} \times \mathrm{FV} \times \mathrm{N} \\
& \text { Where: } \mathrm{P}_{\mathrm{c}}= \text { Measured cylinder pressure, psig } \\
& \mathrm{P}_{\mathrm{m}}=\text { Minimum pressure of cylinder, } \mathrm{psig} \\
& \mathrm{FV}=\text { Floodable Volume (scf) } \\
& \mathrm{N}=\text { Number of cylinders } \\
& \mathrm{V}_{\mathrm{a}}=\text { Capacity available }
\end{aligned}
\end{aligned}
$$

3. Calculate the duration of the available capacity (in minutes) by using this formula:

$$
\text { Duration }=\frac{\underline{\mathrm{V}}_{\underline{a}}}{\mathrm{C}}
$$

Where:
$\mathrm{V}_{\mathrm{a}}=$ Capacity available, scf
C $=$ Consumption rate, scfm

## Air / Oxygen / Mixed Gas in Storage

ATA $\times \mathrm{FV} \times \mathrm{N}=$ total SCF in storage (round down to the next whole number)

## ATA - PSIG in flasks

FV - Floodable volume in flasks in cu ft
N - Number of flasks

## Air / Oxygen / Mixed Gas Available for Use

$$
\left.\left.\begin{array}{rl}
\left(\mathrm{P}_{\mathrm{f}}-\left(\mathrm{P}_{\mathrm{mf}}+\mathrm{MMP}\right)\right. \\
14.7
\end{array}\right) \quad \times \mathrm{FV} \times \mathrm{N}=\mathrm{SCF} \text { available for use (round down to next whole number) }\right) \text { (plig) } \quad \begin{aligned}
\mathrm{P}_{\mathrm{f}}- & \text { Flask pressure (psig } \\
\mathrm{P}_{\mathrm{mf}}- & \text { Minimum flask pressure ( } 200 \mathrm{psig} \text { air, } 100 \mathrm{psig} \mathrm{O}_{2} \\
\mathrm{FV}- & \text { Floodable volume in flasks in cu ft } \\
\mathrm{N}- & \text { Number of flasks }
\end{aligned}
$$

Note: If calculating air available for use for chamber operations where NO surface supplied diving is involved, DO NOT USE MMP. Use $\mathrm{P}_{\mathrm{mf}}$ or regulator setting, whichever is higher.

Note: If calculating O2 available for use for chamber operations, DO NOT USE MMP. Use $\mathrm{P}_{\mathrm{mf}}$ +O 2 regulator setting.

## EGS Pressure Calculation

Minimum EGS pressure calculation example
(1) Planning calculations for minimum EGS pressure prior to any dive. Must be figured to divers first stop.
(2) Example:
(a) The Dive Supervisor needs to estimate how long it will take the divers to return to the stage and leave bottom for a 185 fsw stage depth. The divers are going to pick up an object about 15 feet from the stage; the estimated time to return will be 3 minutes.
(i) Estimated time of return to stage on a $185 / 10$ Sur "D" O2 $(185+33) \times 1.4 \times 3 \mathrm{~min}=27.72 \mathrm{scf}$ 33
(ii) Average Depth for ascent to first stop $\frac{(185+20)}{2}=102.5^{\prime}$ 2
$(102.5+33) \times .75 \times 6$ min Time To First Stop $=18.45$ SCF 33

## EGS Pressure Calculation (Continued)

(iii) Formula used to figure the minimum amount of air in PSI needed to start this dive.
27.72 SCF Return to Stage +18.45 SCF Ascent to First Stop
46.17 Total Air to First Stop
$(\underline{\text { Total Air Required })} \times 14.7=($ Depth First stop x $.445+$ Reg setting $)$ FV of EGS
$(46.17) \times 14.7+(20$ ’ x $.445+135)=\mathbf{1 8 4 4 . 9}$ Minimum PSI . 399
. 399 Floodable volume for 80 cuft bottle

## Equivalent Air Depth Calculations

$\mathrm{EAD}=\frac{(1<\mathrm{O} 2 \%)(\mathrm{D}+33)}{.79}-33$ or | ppN 2 |
| :--- |
| $\mathrm{ATA} \mid \mathrm{N} 2 \%$ |

$\mathrm{EAD}=$ equivalent depth on air (fsw)
D
$\mathrm{O} 2 \%=$ diving depth mixture (fsw)

## Surfaced Supplied Air / Mixed Gas Requirements

Calculations are based on 1.4 ACFM for descent and bottom phase, . 75 ACFM for ascent and decompression phase, and .3 ACFM for BIBS. Include standby in the number of divers for all phases of the dive.
A) Descent and Bottom phase:

Bottom depth in ATA's x ACFM x N x $\mathrm{T}=\mathrm{SCF}$ required (carry two decimal places)

ACFM - Average consumption rate
N - Number of divers including standby
T- Time in minutes
B) Ascent to first Air, HeO 2 , and O 2 stop: (ATA's calculated for average depth)
$\frac{\text { Depth left }+ \text { depth reached }}{2}=$ average depth
ATA x ACFM x $\mathrm{N} \times \mathrm{T}=\mathrm{SCF}$ required (carry two decimal places)
C) Decompression stops:

1) Shift and Vent time $\mathrm{O}_{2} / \mathrm{HeO} 2(50 / 50)$ :
(stop depth in ATA x ACFM x $\mathrm{N} \times \mathrm{T}$ )
(carry two decimal places)
Note: - The time used for planning purposes is 3 minutes as stated in the USN Dive Manual.

- For in water O2 and HeO 2 dives use 8 ACFM for each diver venting

2) All Air / $\mathrm{O}_{2} / \mathrm{HEO}_{2}$ stops:

Stop depth in ATA $\times$ ACFM $\times \mathrm{N} \times \mathrm{T}=\mathrm{SCF}$ required (carry two decimal places)

## Surfaced Supplied Air / Mixed Gas Requirements (Continued)

D) Total requirement for dive:

Descent and bottom phase Ascent + Decompression stops
Total SCF required (round up to next whole number)

Note: 1. Add chamber requirement if applicable
2. Secondary system must be capable of recovering divers
3. Add $\mathrm{O}_{2}$ requirement if applicable
a. Amount of air used/required in PSIG:
$($ SCF x 14.7 $)+220=$ PSIG $($ Round up to next whole number $)$ N x FV

SCF $=$ SCF required
N = Number of Flasks
FV = Floodable Volume
PSIG $=$ Pressure required in flasks

## Chamber / Air O2 Requirements

A) Chamber air requirement:

1. Air required for compression:

DEPTH $\times$ FV $=$ SCF required (Carry 2 decimal places)
33
$\mathrm{FV}=$ floodable volume of chamber locks (cu. ft.)
2. Ventilation requirements:

ATA x total ventilation requirement $\mathrm{x}=\mathrm{SCF}$ required (carry 2 decimal places)

On $\mathbf{O}_{2:} \quad 12.5 \mathrm{acfm}$ - each person on $\mathrm{O}_{2}$ at rest, none required for tenders(s)
On AIR: 2 acfm - each person at rest, 4 acfm - each person not at rest (tenders are considered not at rest)

## Chamber / Air O2 Requirements (Continued)

3. Air required for vents on ascent: (ATA figured for average depth)

$$
\frac{\text { Depth left }+ \text { depth reached }}{2}=\text { Average depth }
$$

Average depth in ATA x vent requirement $\mathrm{x} \mathrm{T}=\mathrm{SCF}$ required (carry two decimal places) ( $\mathrm{T}=$ time)

## To Determine Total Ventilation requirement:

On $\mathbf{O}_{2}$ : 12.5 ACFM for each person on $\mathrm{O}_{2}$ at rest, none required for tender(s) 25 ACFM for each person who is not at rest

On AIR: 2 ACFM for each person at rest and 4 ACFM for each person not at rest (tenders are considered not at rest)
*These ventilation rates apply only to the number of people breathing $\mathrm{O}_{2}$ and are used only when no BIBS dump system is installed.
4. Total air vent requirements:
compression
vents on bottom
vents at stops

+ vents on ascent
Total SCF required (round up to next whole number)

5. Reduction in ventilation:
$\underline{\text { SCF available } \mathbf{x} \text { total vent requirement in ACFM }=\text { New vent rate (in acfm)* }}$
SCF required
*(round to the next whole number)

## Chamber / Air O2 Requirements (Continued)

B) Chamber $\mathrm{O}^{2}$ consumption:

1. Descent, bottom and stops:

Bottom or stop depth in ATA x ACFM x $\mathrm{N} \times \mathrm{T}=\mathrm{SCF}$ required (carry two decimal places)
2. Ascent:

Average depth in ATA x ACFM x N x T $=\mathrm{SCF}$ required (carry two decimal places)
3. Total $\mathrm{O}_{2}$ consumption:

Descent, bottom and stops

+ Ascent
Total SCF consumed (round up to next whole number)


## "T" Formulas

A "T" formula is an organizational device for expressing some mathematical concepts.
For example if:

$$
\begin{aligned}
& 2 \text { times } 3=6 \text { then } \\
& 6 \text { divided by } 2=3 \text { then } \\
& 6 \text { divided by } 3=2
\end{aligned}
$$

This can be expressed in a "T" formula.


Of course, we should not use a "T" formula for $2 \times 3=6$, but it is useful to organize more complicated relationships.

NOTE: Do not round numbers when performing conversions (i.e. psig to ata) within the " T " formula, wait until reaching the final answer and round the answer IAW rounding instructions on page 4.

## "T" Formula for Standard Cubic Feet of Gas

| scf |  |
| :---: | :---: |
| ata | $\mathrm{fv}(\mathrm{cuft})$ |

Problem: How many cubic feet of gas are there in a flask that has a floodable volume of 78.7 cu ft , and a pressure of 2400 psi ?

12,927.67959 scf

| $\frac{2400+14.7}{14.7}$ | 78.7 cu ft |
| :---: | :---: |
| $=164.2653061$ ata |  |

ans: $\mathbf{1 2 9 2 7 . 6 7}$ scf (carry 2 decimal places)

## "T" Formula For Cubic Feet of Gas (Continued)

Problem: If $12,900.00$ standard cubic feet of gas is in a 78.7 cu ft floodable volume flask, what is the resultant gauge pressure?

| $12,900.00 \mathrm{scf}$ |  |
| :---: | :---: |
| 163.91359 ata | 78.7 cu ft |
| $\frac{-1}{162.91359} \mathrm{~atm}$ |  |
| $\frac{\mathrm{x} \mathrm{14.7}}{\mathbf{2 3 9 4 . 8 2 9 8 5 9}} \mathbf{~ p s i g}$ |  |

ans: 2395 psig (rounded up)
Problem: One 78.7 cubic foot floodable volume flask is on the line at 2400 psig. During a diving operation the flask pressure dropped to 2234 psig. What was the amount of gas used?

| 2400 psig |
| :---: |
| -2234 psig |
| $=166 \mathrm{psig}$ |

888.7210879 scf

| $166 \mathrm{psig} / 14.7$ <br> $=11.292517 \mathrm{~atm}$ | 78.7 cu ft |
| :---: | :---: |

aans: $\mathbf{8 8 8 . 7 2}$ scf (carry 2 decimal places

## "T" Formula for Equalization

| scf |  | + | scf |  |  | scf |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ata | fv1 |  | ata | fv2 |  | ata | fv1 + fv2 |

Problem: One 78.7 cubic foot floodable volume flask, charged to 1000 psi, is equalized with one 78.7 cubic foot floodable volume flask charged to 2400 psi . What is the new flask pressure?

| 5,432.4414 scf |  | 12, 927.679 scf |  | 18, 360.12 scf |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \frac{1,000 \mathrm{psi}+}{\frac{14.7}{14.7}} \\ & =69.02721 \mathrm{ata} \end{aligned}$ | 78.7 cu ft | $\begin{aligned} & \frac{2,400 \mathrm{psi}+}{} \\ &+\quad \frac{14.7}{14.7} \\ &= 164.26530 \\ & \text { ata } \end{aligned}$ | $\begin{gathered} 78.7 \mathrm{cu} \\ \mathrm{ft} \end{gathered}$ | $\begin{aligned} & 116.64625 \text { ata } \\ & \frac{-1}{115.64625} \mathrm{~atm} \\ & \frac{\times 14.7}{=\mathbf{1 , 6 9 9 . 9 9 9 8}} \begin{array}{c} \text { psig } \end{array} \end{aligned}$ | $\begin{gathered} \frac{78.7 \mathrm{cu} \mathrm{ft}}{\mathrm{x} 2} \\ \frac{157.4 \mathrm{cu}}{\mathrm{ft}} \end{gathered}$ |

ans: $\mathbf{1 , 7 0 0} \mathbf{p s i g}$ (rounded up)

## "T" Formula for Final Pressure



$=\quad$| ata $\mid$ fcf |
| :--- |
| fv1 |

Problem: One bank of eight 78.7 cu ft flasks charged @ 2000 psig is on line. The complex ( 3300 cu ft ) is at 180 fsw . You press down to 279 fsw . What is the final pressure in the bank?

ans: $1,769 \mathbf{p s i g}$ (rounded up)

## "T" Formula for Partial Pressure, Maximum $\mathrm{O}_{2}$ and Cutoff Depth

| PARTIAL PRESSURE IN ATA'S |  |
| :---: | :---: |
| ATA | \% OF GAS |

Problem: What is the cutoff depth for a $25 \% \mathrm{O}_{2}$ mix maintaining a maximum partial pressure of $\mathrm{O}_{2}$ at 1.6 ata?

| $1.6 \mathrm{ppO}_{2}$ ata |  |
| :--- | ---: |
| $\mathbf{6 . 4}$ ata | $25 \%$ |
| $\frac{-1}{5.4 \mathrm{~atm}}$ | $=.25$ |
| $\frac{\mathrm{x} 33}{\mathbf{1 7 8 . 2} \mathbf{~ f s w}}$ |  |
|  |  |

ans: $\mathbf{1 7 8}$ fsw

## "T" Formula for Partial Pressure, Maximum $\mathrm{O}_{2}$ and Cutoff Depth (Continued)

Problem: At 180 fsw , what percent gas is needed to maintain a partial pressure of 1.6 ata?

| $1.6 \mathrm{ppO}_{2}$ ata |  |
| :---: | :---: |
| $\frac{180 \text { fsw }+33}{33}$ | .2478873 |
| $=6.45454$ ata | $=24.78873 \%$ |

ans: $\mathbf{2 4 . 7 9 \%} \mathbf{O}_{\mathbf{2}}$ (rounded up)
Problem: At 180 fsw , and using $15 \% \mathrm{O}_{2}$, what is the partial pressure in ata?


Problem: The $\mathrm{ppO}_{2}$ is .97 ata, and the $\%$ of gas is $15 \%$, what is the depth?

| $.97 \mathrm{ppO}_{2}$ ata |  |
| :--- | :--- |
| 6.4666666 ata | $15 \%$ |
| $\frac{-1}{5.4666666 ~ a t m ~}$ | $=.15$ |
| $\frac{\mathrm{x} 33}{\mathbf{1 8 0 . 3 9 9 9 9} \mathbf{~ f s w}}$ |  |

ans: 180.4 (rounded up)
Problem: The $\mathrm{ppO}_{2}$ is .97 ata and the depth is 180 fsw. What is the percent of gas?
$.97 \mathrm{ppO}_{2}$ ata

| $180 \mathrm{fsw}+33$ <br> 33 | .1502816 |
| :--- | :--- |
| $=6.4545454 \mathrm{ata}$ |  |
|  |  |

ans: $\mathbf{1 5 . 0 3 \%}$ (rounded up)

## General Gas Law Formula

$$
\underline{\mathrm{P}}_{1} \frac{\times \mathrm{V}_{1}}{\mathrm{~T}_{1}} \quad \underline{\mathrm{P}}_{2} \frac{\times \mathrm{V}_{2}}{\mathrm{~T}_{2}}
$$

The General Gas Law can be used to predict the behavior of a given quantity of gas when any of the factors change. *If some factors do not change in the equation $\left(V_{1}=V_{2}\right)$, they can be removed from the equation.

Express all temperatures in absolute (degrees Rankine) by adding 460 to existing temperatures ( ${ }^{\circ} \mathrm{F}+460={ }^{\circ} \mathrm{R}$ ).

Express all pressures or depths in absolute by adding 14.7 psi or 33 fsw.
$\mathrm{P}_{1}$ - Initial Pressure (absolute) To solve for any of the individual factors:
$\mathrm{V}_{1}$ - Initial Volume
$\begin{array}{lrll}\mathrm{T}_{1}-\text { Initial Temperature (absolute) } \\ \mathrm{P}_{2}-\text { Final Pressure (absolute) }\end{array} \quad \mathrm{P}_{1}=\underline{\mathrm{P}}_{2} \underline{\mathrm{~V}_{2}} \underline{\mathrm{~T}}_{2} \mathrm{~T}_{1} \quad \mathrm{P}_{2}=\underline{\mathrm{P}}_{1} \underline{\mathrm{~V}_{1}} \underline{\mathrm{~T}_{2}} \underline{\mathrm{~T}}_{2} \mathrm{~V}_{1}=\underline{\mathrm{P}}_{2} \underline{\mathrm{~V}}_{2} \mathrm{~T}_{1}$
$\mathrm{V}_{2}$ - Final Volume
$\mathrm{T}_{2}$ - Final Temperature (absolute)

$$
\mathrm{V}_{2}=\underline{\mathrm{P}}_{1} \underline{\mathrm{~V}_{1}} \underline{\mathrm{P}}_{2} \underline{\mathrm{~T}_{2}} \quad \mathrm{~T}_{1}=\underline{\mathrm{T}_{2}} \underline{\mathrm{P}_{1}} \underline{\mathrm{P}}_{2} \underline{\mathrm{~V}}_{1} \frac{\mathrm{~T}_{2}}{\mathrm{~V}_{2}}=\underline{\mathrm{P}_{2}} \underline{\mathrm{~V}_{2}} \underline{\mathrm{~T}_{1}} \underline{\mathrm{~T}}_{1}
$$

Problem: The complex is pressed to 220 fsw, it cools from $92^{\circ} \mathrm{F}$ to $76^{\circ} \mathrm{F}$, and no gas is added or lost, what is the final depth?

$$
\begin{aligned}
& \mathrm{P}_{2}=\mathrm{P}_{1} \frac{\mathrm{~V}_{1}-\mathrm{T}_{2}}{\mathrm{~T}_{1} \mathrm{~V}_{2}} \quad \begin{array}{c}
* \text { The volume of the complex is not going to change } \\
\text { (Complex } \mathbf{f v}=\mathbf{3 3 0 0} \text { cu ft), so remove } \mathrm{V}_{1} \text { and } \mathrm{V}_{2} \text { from the } \\
\text { equation. }
\end{array} \\
& \mathrm{P}_{1}=\frac{220 \mathrm{fsw}+33}{33}=\quad 7.666666 \text { ata } \\
& \mathrm{T}_{2}=76^{\circ} \mathrm{F}+460=\quad 536^{\circ} \mathrm{R} \\
& \mathrm{~T}_{1}=92^{\circ} \mathrm{F}+460=\quad 552^{\circ} \mathrm{R} \\
& \mathrm{P}_{2}=\frac{7.66666 \times 536}{552} \\
& \mathrm{P}_{2}=\frac{4109.333332}{552}=7.4444442 \mathrm{ata} \\
& \mathrm{P}_{2}=7.4444442-1=6.4444442 \mathrm{~atm} \\
& \mathrm{P}_{2}=6.4444442 \times 33=212.66665 \mathrm{fsw}
\end{aligned}
$$

ans: 212 fsw

## Metabolic Makeup Formula

$\left(\mathrm{ppO}_{2}\right.$ desired $-\mathrm{ppO}_{2}$ present $) \times 33 \times \frac{\% \text { of gas being added }}{100}=\mathrm{ft}$ of $\mathrm{O}_{\mathbf{2}}$
The metabolic makeup formula is used to calculate how much oxygen addition is needed to maintain the proper partial pressure limits.

Problem: The $\mathrm{ppO}_{2}$ is .40 ata and we wish to increase it to .45 ata, how many additional feet must we press down with $100 \%$ oxygen?
$(.45-.40)=\quad .05$
$.05 \times 1 \times 33=1.65 \mathrm{ft}$ of $\mathrm{O}_{2}$
ans: $\mathbf{1 . 6 5} \mathrm{ft}$ of $\mathrm{O}_{\mathbf{2}}$
To bring the $\mathrm{ppO}_{2}$ up to .45 ata, depth in the complex must be increased 1.65 ft using pure oxygen.

## DEMOLITIONS



## Steel Cutting

A) Structural Steel (I or H BEAMS)

$$
\begin{array}{rl}
P=3 / 8 A & \mathrm{P}=\text { Pounds of Explosive Required } \\
\mathrm{A} & =\text { Area (in square inches) }
\end{array}
$$

B) Steel Bars, Cables and Chain

$$
\mathrm{P}=\mathrm{A}
$$

C) Ribbon Charge

Thickness of charge $=1 / 2$ the thickness of the target
Width of charge $=3$ times the thickness of the charge
Length of charge $=$ length of desired cut

## Steel Cutting (Continued)

D) Cross Fracture Charge (Saddle Charge)

Target Diameter Less Than 3":
Thickness of charge $=1$ " thick (thickness of M112 block)
Long axis of charge = circumference of the target
Base of charge $\quad=1 / 2$ of the long axis

Target Diameter of 3" or Greater:

| Thickness of charge | $=1 "$ thick |
| :--- | :--- |
| Long axis of charge | $=$ circumference of the target +6.25 |
| Base of charge | $=1 / 2$ of the long axis |

## NOTE: Circumference = Diameter $\times 3.14$

E) Stress Wave Method (Diamond Charge)

Target Diameter Less Than 3":
Thickness of charge $=1 "$ thick (thickness of M112 block)
Long axis of charge = circumference of the target
Base of charge $\quad=1 / 2$ of the long axis
Target Diameter 3" or Greater:
Thickness of charge $\quad=1$ " thick
Long axis of charge $\quad=$ circumference of the target +6.25
Base of charge $\quad=1 / 2$ of the long axis

# Timber and Pile Cutting 

External Charge

$$
P=\frac{D^{2}}{40}
$$

P = Pounds of Explosives Required
$\mathrm{D}=$ Diameter of Timber in Inches

Internal Charge

$$
P=\frac{D^{2}}{250}
$$

$$
\mathrm{P}=\text { Pounds of Explosives Required }
$$

$$
\mathrm{D}=\text { Diameter of Timber in Inches }
$$

## Calculation of Time Fuse Burn

1. Burn 6' of time fuse then convert burn time (BT) into seconds. ( $\mathrm{BT}=4$ minutes $(: 4 \mathrm{x}:: 60=240 \mathrm{sec}$ ).
2. Divide seconds by feet $(6)=$ burn rate $(B R)$ seconds per foot. $(B R=40 \mathrm{sec})$.
3. Establish safe separation time (SST) in seconds.
$($ SST is 8 minutes 26 seconds $=506 \mathrm{sec})$.
4. Divide SST (506) by BR (40). This equals 12.65 .
5. Number that is left of decimal is feet of time fuse needed. (12).
6. Multiply remaining (.65) by 12. (7.80).
7. The number left of the decimal is inches of time fuse needed. (7). (In addition to the 12 feet, step 5).
8. Take the number to the right of the decimal (.80) and multiply it by 8 . This number to the left of the decimal is the $1 / 8$ 's of an inch of time fuse to add to the inches from step (7). ( $.80 \times 8=6.4$ ) The ". 4 " is discarded. So $6 / 8$ 's or $3 / 4$ 's of an inch is added to the number of inches in step 8 .
9. This results in a total time fuse length of $\mathbf{1 2}$ feet and 7 - $\mathbf{3} / 4$ inches.

# Breaching Concrete and Masonry 

## External Charge

$$
P=R^{3} K C
$$

$\mathrm{P}=$ Pounds of Explosives Required
$\mathrm{R}=$ Breaching Radius (thickness of the target)
$\mathrm{K}=$ Material Factor
$\mathrm{C}=$ Charge Placement and Tamping Factor

Internal Charge
$\mathrm{P}=$ Pounds of Explosives Required
$\mathrm{R}=$ Breaching Radius (if charge is placed at center

$$
P=R^{3} K C
$$

of target the radius is equal to only half the target thickness)
K = Material Factor $\mathrm{C}=$ Charge Placement and Tamping Factor

NOTE: Add $10 \%$ to a calculated charge of less than 50 lbs for a single target.
NOTE: To calculate these formulas for breaching concrete and masonry, refer to values for K and C factors.

1. Calculate for amount of TNT needed.
2. Add the $10 \%$ if amount for a single target is less than 50 lbs .
3. Multiply the number of targets.
4. Divide the relative effectiveness of explosive being used.

NOTE: To calculate the number of charges required to breach a wall use the following formula:
$\mathrm{N}=\mathrm{L} / 2 \mathrm{R}$ (round up to the next whole number)
$\mathrm{N}=$ Number of charges required
$\mathrm{L}=$ Length of the wall
$\mathrm{R}=$ Breaching Radius (remember that if using internal charges the radius will only be $1 / 2$ the wall thickness)

## Breaching Concrete and Masonry (Continued)

Value of C for the R3KC formula for an Internal Breaching Charge:


Value of C for the R3KC formula for an External Wall Breach Charge:


UNDERWATER C - 1
DEPTH AT WHICH CHARGE IS PLACED IS EQUAL TO OR MORE THAN THE WALL THICKNESS


## Breaching Concrete and Masonry (Continued)

Values for Relative Effectiveness Factor (REF) (Characteristics of U.S. Military Explosives)

| Explosive | Typical Uses | Average <br> Rate of Detonation (Feet Per Second) | Relative Effectiveness as an External Charge (TNT = 1.00) | Intensity of Toxic Fumes | Water Resistance |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Amatol | Bursting Charge | 16,000 fps | 1.17 | Dangerous | Poor |
| Ammonium Nitrate | Cratering Charge and Composition Explosives | 8,900 fps | 0.42 | Dangerous | None |
| Black Powder | Time Blasting Fuse | 1300 fps | 0.55 | Dangerous | None |
| CH-6 | Demolition Charge Booster Charge | 28,000 fps | 1.50 | Dangerous | Excellent |
| Composition A-3 | Booster Charge and Bursting Charge | 26,500 fps | 1.35 | Dangerous | Good |
| Composition A-5 | Booster Charge | 29, 300 fps | 1.40 | Dangerous | Excellent |
| Composition B | Bursting Charge | 25, 600 fps | 1.35 | Dangerous | Excellent |
| Composition C-3 | Demolition Charge | $25,000 \mathrm{fps}$ | 1.26 | Dangerous | Good |
| Composition C-4 | Demolition Charge | 26, 400 fps | 1.34 | Slight | Excellent |
| DXN-1 | Primary Charge | 21, 600 fps | 1.50 | Dangerous | Good |
| H-6 | Demolition Charge | 24, 300 fps | 1.35 | Dangerous | Excellent |
| HBX-1 | Demolition Charge | $24,600 \mathrm{fps}$ | 1.33 | Dangerous | Excellent |
|  | Demolition Charge | 24, 700 fps | 1.11 | Dangerous | Excellent |
|  | Demolition Charge | 30, 000 fps | 1.50 | Dangerous | Excellent |
| Military Dynamite | Demolition Charge | $20,000 \mathrm{fps}$ | 0.92 | Dangerous | Fair |
| Octol-70/25 | Demolition Charge | 27, 500 fps | 1.16 | Dangerous | Excellent |
| Octol-70/30 | Demolition Charge | 26, 400 fps | 1.15 | Dangerous | Excellent |
| PBX | See NAVSEA SW010-AG-ORD-010 |  |  |  |  |
| Pentolite 50/50 | Booster Charge and Bursting Charge | 24, 400 fps | 1.26 | Dangerous | Excellent |
| PETN | Detonation Cord, Blasting Cap and Demolition Charge | 27, 200 fps | 1.66 | Slight | Excellent |
| RDX | Blasting Caps, Composition Explosives | 27, 400 fps | 1.60 | Dangerous | Excellent |
| Tetryl | Booster Charge and Composition Explosives | 23, 300 fps | 1.25 | Dangerous | Excellent |
| Tetrytol 75/25 | Demolition Charge | 23, 000 fps | 1.20 | Dangerous | Excellent |
| TNT | Demolition Charge and Composition Explosives | 22,600 fps | 1.00 | Dangerous | Excellent |
| Sheet Explosive M118 | Cutting Charge | 24, 000 fps | 1.14 | Dangerous | Excellent |
| Shaped Charges | Cutting Charge | 25, 600 fps | 1.17 | Dangerous | Excellent |

## Breaching Concrete and Masonry (Continued)

Values of K for the $\mathrm{R}^{3} \mathrm{KC}$ Formula

| Material | R | K |
| :--- | :---: | :---: |
| Ordinary Earth <br> good | All values | 0.05 |
| Poor masonry, shale and hardpan, <br> timber and earth construction | All values | 0.225 |
| Good masonry, ordinary concrete |  |  |
| and rock | Less than 3 ft | 0.35 |
|  | 3 to 5 ft | 0.275 |
|  | 5 to 7 ft | 0.25 |
| Dense concrete and first class | More than 7 ft | 0.225 |
| masonry | Less than 3 ft | 0.45 |
|  | 3 to 5 ft | 0.375 |
| Reinforced concrete (concrete | 5 to 7 ft | 0.325 |
| only, | Lers than 7 ft | 0.275 |
| Will not cut reinforcing steel) | 3 to 5 ft | 0.70 |
|  | 5 to 7 ft | 0.55 |

## Rigging Formulas

| C | $=$ Circumference |
| :--- | :--- |
| BS | $=$ Breaking Strength |
| SWL or SWC | $=$ Safe Working Load/Capacity |
| SF | $=$ Safety Factor |
| D | $=$ Diameter |

Breaking strength of manila line: $C^{2}$ x $900=B S$
Breaking strength of nylon line: $C^{2} \times 2400=B S$
Safe working load for line: $\frac{\mathrm{BS}}{\mathrm{SF}}=\mathrm{SWL}$
SWL of a shackle: $3 \times \mathrm{D}^{2} \times 1$ ton $=\mathrm{SWL}$ (tons)
SWL of a hook: $2 / 3 \times D^{2} \times 1$ ton $=$ SWL
Safe working load for wire rope: $D^{2} \times 8=S W L$ (tons)
CLIPS: \# of wire rope clips needed
$3 \times \mathrm{D}+1=$ \# of clips
Spacing between wire rope clips
$6 \times \mathrm{D}=$ spacing (inches)
SEIZINGS: \# of seizings for wire rope
$3 \times D=\#$ of seizings (minimum of 3 )
Spacing of seizings for wire rope
$2 \times \mathrm{D}=$ spacing (inches)
Width of seizings for wire rope 1 to $1.5 \times \mathrm{D}=$ width (inches)

## HAND TOOLS

$\cdot T(W)=T(E) \quad X \quad L / L+E$
$-E=$ Effective length of adapter
$-L=$ Length of the wrench
$-\mathbf{T}(\mathrm{W})=$ Torque set or read on wrench
$-T(E)=$ Applied Torque (required torque)


Table 9-7. No-Decompression Limits and Repetitive Group Designators for No-Decompression Air Dives.

| Depth (faw) | No-Stop Limit | Repetitive Group Designation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | D | E | F | G | H | 1 | J | K | L | M | N | 0 | Z |
| 10 | Unlimited | 57 | 101 | 158 | 245 | 426 | * |  |  |  |  |  |  |  |  |  |  |
| 15 | Unlimited | 36 | 60 | 88 | 121 | 163 | 217 | 297 | 449 | * |  |  |  |  |  |  |  |
| 20 | Unlimited | 26 | 43 | 61 | 82 | 106 | 133 | 165 | 205 | 256 | 330 | 461 | * |  |  |  |  |
| 25 | 595 | 20 | 33 | 47 | 62 | 78 | 97 | 117 | 140 | 166 | 198 | 236 | 285 | 354 | 469 | 595 |  |
| 30 | 371 | 17 | 27 | 38 | 50 | 62 | 76 | 91 | 107 | 125 | 145 | 167 | 193 | 223 | 260 | 307 | 371 |
| 35 | 232 | 14 | 23 | 32 | 42 | 52 | 63 | 74 | 87 | 100 | 115 | 131 | 148 | 168 | 190 | 215 | 232 |
| 40 | 163 | 12 | 20 | 27 | 36 | 44 | 53 | 63 | 73 | 84 | 95 | 108 | 121 | 135 | 151 | 163 |  |
| 45 | 125 | 11 | 17 | 24 | 31 | 39 | 46 | 55 | 63 | 72 | 82 | 92 | 102 | 114 | 125 |  |  |
| 50 | 92 | 9 | 15 | 21 | 28 | 34 | 41 | 48 | 56 | 63 | 71 | 80 | 89 | 92 |  |  |  |
| 55 | 74 | 8 | 14 | 19 | 25 | 31 | 37 | 43 | 50 | 56 | 63 | 71 | 74 |  |  |  |  |
| 60 | 60 | 7 | 12 | 17 | 22 | 28 | 33 | 39 | 45 | 51 | 57 | 60 |  |  |  |  |  |
| 70 | 48 | 6 | 10 | 14 | 19 | 23 | 28 | 32 | 37 | 42 | 47 | 48 |  |  |  |  |  |
| 80 | 39 | 5 | 9 | 12 | 16 | 20 | 24 | 28 | 32 | 36 | 39 |  |  |  |  |  |  |
| 90 | 30 | 4 | 7 | 11 | 14 | 17 | 21 | 24 | 28 | 30 |  |  |  |  |  |  |  |
| 100 | 25 | 4 | 6 | 9 | 12 | 15 | 18 | 21 | 25 |  |  |  |  |  |  |  |  |
| 110 | 20 | 3 | 6 | 8 | 11 | 14 | 16 | 19 | 20 |  |  |  |  |  |  |  |  |
| 120 | 15 | 3 | 5 | 7 | 10 | 12 | 15 |  |  |  |  |  |  |  |  |  |  |
| 130 | 10 | 2 | 4 | 6 | 9 | 10 |  |  |  |  |  |  |  |  |  |  |  |
| 140 | 10 | 2 | 4 | 6 | 8 | 10 |  |  |  |  |  |  |  |  |  |  |  |
| 150 | 5 | 2 | 3 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 160 | 5 |  | 3 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 170 | 5 |  |  | 4 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 180 | 5 |  |  | 4 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 190 | 5 |  |  | 3 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |

* Highest repetfive group that can be achieved at this depth regardless of cottom time.

Table 9-8. Residual Nitrogen Time Table for Repetitive Air Dives.

${ }^{\text {" }}$ Residual Nitrogen Time cannot be determined using this table (see paragraph $9-9.1$ subparagraph 8 for instructions).
$\dagger$ Read vertically downward to the 30 fsw repetitive dive depth. Use the corresponding residual nitrogen times to compute the equivalent single dive time. Decompress using the 30 fsw air decompression table.

Table 2A-1. No-Decompression Limits and Repetitive Group Designators for Shallow Water Air NoDecompression Dives.

| Depth <br> (fsw) | $\begin{gathered} \text { No-Stop } \\ \text { Limit(min) } \end{gathered}$ | Repetitive Group Designation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | D | E | F | G | H | 1 | J | K | L | M | N | 0 | z |
| 30 | 371 | 17 | 27 | 38 | 50 | 62 | 76 | 91 | 107 | 125 | 145 | 167 | 193 | 223 | 260 | 307 | 371 |
| 31 | 334 | 16 | 26 | 37 | 48 | 60 | 73 | 87 | 102 | 119 | 138 | 158 | 182 | 209 | 242 | 282 | 334 |
| 32 | 304 | 15 | 25 | 35 | 46 | 58 | 70 | 83 | 98 | 114 | 131 | 150 | 172 | 197 | 226 | 261 | 304 |
| 33 | 281 | 15 | 24 | 34 | 45 | 56 | 67 | 80 | 94 | 109 | 125 | 143 | 163 | 186 | 212 | 243 | 281 |
| 34 | 256 | 14 | 23 | 33 | 43 | 54 | 65 | 77 | 90 | 104 | 120 | 137 | 155 | 176 | 200 | 228 | 256 |
| 35 | 232 | 14 | 23 | 32 | 42 | 52 | 63 | 74 | 87 | 100 | 115 | 131 | 148 | 168 | 190 | 215 | 232 |
| 36 | 212 | 14 | 22 | 31 | 40 | 50 | 61 | 72 | 84 | 97 | 110 | 125 | 142 | 160 | 180 | 204 | 212 |
| 37 | 197 | 13 | 21 | 30 | 39 | 49 | 59 | 69 | 81 | 93 | 106 | 120 | 136 | 153 | 172 | 193 | 197 |
| 38 | 184 | 13 | 21 | 29 | 38 | 47 | 57 | 67 | 78 | 90 | 102 | 116 | 131 | 147 | 164 | 184 |  |
| 39 | 173 | 12 | 20 | 28 | 37 | 46 | 55 | 65 | 76 | 87 | 99 | 112 | 126 | 141 | 157 | 173 |  |
| 40 | 163 | 12 | 20 | 27 | 36 | 44 | 53 | 63 | 73 | 84 | 95 | 108 | 121 | 135 | 151 | 163 |  |
| 41 | 155 | 12 | 19 | 27 | 35 | 43 | 52 | 61 | 71 | 81 | 92 | 104 | 117 | 130 | 145 | 155 |  |
| 42 | 147 | 11 | 19 | 26 | 34 | 42 | 50 | 59 | 69 | 79 | 89 | 101 | 113 | 126 | 140 | 147 |  |
| 43 | 140 | 11 | 18 | 25 | 33 | 41 | 49 | 58 | 67 | 76 | 87 | 98 | 109 | 122 | 135 | 140 |  |
| 44 | 134 | 11 | 18 | 25 | 32 | 40 | 48 | 56 | 65 | 74 | 84 | 95 | 106 | 118 | 130 | 134 |  |
| 45 | 125 | 11 | 17 | 24 | 31 | 39 | 46 | 55 | 63 | 72 | 82 | 92 | 102 | 114 | 125 |  |  |
| 46 | 116 | 10 | 17 | 23 | 30 | 38 | 45 | 53 | 61 | 70 | 79 | 89 | 99 | 110 | 116 |  |  |
| 47 | 109 | 10 | 16 | 23 | 30 | 37 | 44 | 52 | 60 | 68 | 77 | 87 | 97 | 107 | 109 |  |  |
| 48 | 102 | 10 | 16 | 22 | 29 | 36 | 43 | 51 | 58 | 67 | 75 | 84 | 94 | 102 |  |  |  |
| 49 | 97 | 10 | 16 | 22 | 28 | 35 | 42 | 49 | 57 | 65 | 73 | 82 | 91 | 97 |  |  |  |
| 50 | 92 | 9 | 15 | 21 | 28 | 34 | 41 | 48 | 56 | 63 | 71 | 80 | 89 | 92 |  |  |  |

Table 2A-2. Residual Nitrogen Time Table for Repetitive Shallow Water Air Dives.


Residual Nitrogen Times (Minutes)

Table 9-9. Air Decompression Table. (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )


Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)



| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | able 9-9. Air Decompression Table (Continued). DESCENT RATE 75 FPM-ASCENT RATE 30 FPM) |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 | DECO <br> Stop ti: <br> exc <br> 80 | $\begin{aligned} & \text { MPRES } \\ & \text { hes (mi } \\ & \text { ot first } \\ & 70 \end{aligned}$ | $\begin{aligned} & \text { SION } \\ & \text { 1) indu } \\ & \text { ir and } \\ & 60 \end{aligned}$ | $\begin{aligned} & \text { TOPS } \\ & \text { de tray } \\ & \text { irst O } \\ & 50 \end{aligned}$ | $\begin{aligned} & \text { (FSW) } \\ & \text { el time } \\ & \text { stop } \\ & 40 \end{aligned}$ | 30 | 20 |  |  |  |
| 50 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 92 | 1:40 | AIR |  |  |  |  |  |  |  |  | 0 | 1:40 | 0 | M |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 1:40 |  |  |
| 95 | 1:00 | AIR |  |  |  |  |  |  |  |  | 2 | 3:40 | 0.5 | M |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 2:40 |  |  |
| 100 | 1:00 | AIR |  |  |  |  |  |  |  |  | 4 | 5:40 | 0.5 | N |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 3:40 |  |  |
| 110 | 1:00 | AIR |  |  |  |  |  |  |  |  |  | 9:40 | 0.5 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 4 | 5:40 |  |  |
| In-Water Airl $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Recommended |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 120 | 1:00 | AIR |  |  |  |  |  |  |  |  | 21 | 22:40 | 0.5 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 7 | 8:40 |  |  |
| 130 | 1:00 | AIR |  |  |  |  |  |  |  |  | 34 | 35:40 | 0.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 12 | 13:40 |  |  |
| 140 | 1:00 | AIR |  |  |  |  |  |  |  |  | 45 | 46:40 | 1 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 16 | 17:40 |  |  |
| 150 | 1:00 | AlR |  |  |  |  |  |  |  |  | 56 | 57:40 | 1 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 19 | 20:40 |  |  |
| 160 | 1:00 | AIR |  |  |  |  |  |  |  |  | 78 | 79:40 | 1 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 23 | 24:40 |  |  |
| Exoeptional Exposure: In-Water Air Decompression ----- In-Water Airl $\mathrm{O}_{2}$ Decompression or SurDO ${ }_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 170 | 1:00 | AIR |  |  |  |  |  |  |  |  | 96 | 97:40 | 1 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 26 | 27:40 |  |  |
| 180 | 1:00 | AIR |  |  |  |  |  |  |  |  | 111 | 112:40 | 1.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 30 | 31:40 |  |  |
| 180 | 1:00 | AIR |  |  |  |  |  |  |  |  | 125 | 126:40 | 1.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 35 | 36:40 |  |  |
| 200 | 1:00 | AIR |  |  |  |  |  |  |  |  | 136 | 137:40 | 1.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 39 | 45:40 |  |  |
| 210 | 1:00 | AIR |  |  |  |  |  |  |  |  | 147 | 148:40 | 2 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 43 | 49:40 |  |  |
| 220 | 1:00 | AIR |  |  |  |  |  |  |  |  | 168 | 167:40 | 2 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 47 | 53:40 |  |  |
| 230 | 1:00 | AIR |  |  |  |  |  |  |  |  | 183 | 184:40 | 2 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 50 | 56:40 |  |  |
| 240 | 1:00 | AIR |  |  |  |  |  |  |  |  | 198 | 199:40 | 2 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 53 | 59:40 |  |  |
| 270 | 1:00 | AIR |  |  |  |  |  |  |  |  | 236 | 237:40 | 2.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 62 | 68:40 |  |  |
| 300 | 1:00 | AIR |  |  |  |  |  |  |  |  | 285 | 286:40 | 3 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 74 | 85:40 |  |  |
| Exceptional Exposure: In-Water $\mathrm{Air}^{2} \mathrm{O} 2$ Decompression $-\ldots-\ldots-\ldots$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 330 | 1:00 | AIR |  |  |  |  |  |  |  |  | 345 | 346:40 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 83 | 94:40 |  |  |
| 360 | 1:00 | AIR |  |  |  |  |  |  |  |  | 393 | 394:40 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 92 | 103:40 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$--- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 420 | 1:00 | AIR |  |  |  |  |  |  |  |  | 484 | 485:40 | 4.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 113 | 129:40 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ <br> Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |  |
| 55 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 74 | 1.50 | AIR |  |  |  |  |  |  |  |  | 0 | 1:50 | 0 | L |
|  |  | $\mathrm{AlR}^{\text {O }} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 1:50 |  |  |
| 75 | 1:10 | AIR |  |  |  |  |  |  |  |  | 1 | 2.50 | 0.5 | L |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 1 | $2 \cdot 50$ |  |  |
| 80 | 1:10 | AIR |  |  |  |  |  |  |  |  | 4 | 5.50 | 0.5 | M |
|  |  | $\mathrm{AlR}^{\text {( }} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 3:50 |  |  |
| 90 | 1:10 | AIR |  |  |  |  |  |  |  |  | 10 | 11:50 | 0.5 | N |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 5 | 6.50 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 1:10 | AIR |  |  |  |  |  |  |  |  | 17 | 18:50 | 0.5 | 0 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 8 | 9.50 |  |  |
| 110 | 1:10 | AIR |  |  |  |  |  |  |  |  | 34 | 35.50 | 0.5 | 0 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 12 | 13:50 |  |  |
| 120 | 1:10 | AIR |  |  |  |  |  |  |  |  | 48 | 48.50 | 1 | z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 17 | 18:50 |  |  |
| 130 | 1:10 | AIR |  |  |  |  |  |  |  |  | 59 | 60:50 | 1 | $z$ |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 22 | 23:50 |  |  |
| 140 | 1:10 | AIR |  |  |  |  |  |  |  |  | 84 | $85: 50$ | 1 | $z$ |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 26 | 27:50 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water Air/O2 Decompression or SurDO, Required ------ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 150 | 1:10 | AIR |  |  |  |  |  |  |  |  | 105 | 108:50 | 1.5 | Z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 30 | 31:50 |  |  |
| 180 | 1:10 | AIR |  |  |  |  |  |  |  |  | 123 | 124:50 | 1.5 | $z$ |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 34 | 35.50 |  |  |
| 170 | 1:10 | AlR |  |  |  |  |  |  |  |  | 138 | 139:50 | 1.5 | z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 40 | 46:50 |  |  |
| 180 | 1:10 | AIR |  |  |  |  |  |  |  |  | 151 | 152-50 | 2 | z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 45 | 51:50 |  |  |
| 190 | 1:10 | AIR |  |  |  |  |  |  |  |  | 169 | 170:50 | 2 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 50 | 56:50 |  |  |
| 200 | 1:10 | AIR |  |  |  |  |  |  |  |  | 190 | 191:50 | 2 |  |
|  |  | $\mathrm{AlR/O}_{2}$ |  |  |  |  |  |  |  |  | 54 | 60:50 |  |  |
| 210 | 1:10 | AIR |  |  |  |  |  |  |  |  | 208 | 209:50 | 2.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 58 | 64:50 |  |  |
| 220 | 1:10 | AIR |  |  |  |  |  |  |  |  | 224 | 225:50 | 2.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 62 | 68:50 |  |  |
| 230 | 1:10 | AIR |  |  |  |  |  |  |  |  | 239 | 240:50 | 2.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 66 | 77:50 |  |  |
| 240 | 1:10 | AIR |  |  |  |  |  |  |  |  | 254 | 255.50 | 3 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 69 | 80:50 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 270 | 1:10 | AIR |  |  |  |  |  |  |  |  | 313 | 314:50 | 3.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 83 | 94:50 |  |  |
| 300 | 1:10 | AIR |  |  |  |  |  |  |  |  | 380 | 381:50 | 3.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 94 | 105.50 |  |  |
| 330 | 1:10 | AIR |  |  |  |  |  |  |  |  | 432 | 433-50 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 106 | 122.50 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 380 | 1:10 | AIR |  |  |  |  |  |  |  |  | 474 | 475:50 | 4.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 118 | 134:50 |  |  |
| 9-68 |  |  |  |  |  |  |  |  |  |  | Nav | Diving | anual - | olume 2 |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| $\begin{aligned} & \text { Bottom Time } \\ & (\mathrm{min}) \end{aligned}$ | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 10090 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |  |
| 60 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | 2:00 | AIR |  |  |  |  |  |  |  | 0 | 2:00 | 0 | K |
|  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 2:00 |  |  |
| 65 | 1:20 | AIR |  |  |  |  |  |  |  | 2 | 4:00 | 0.5 | L |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 1 | 3:00 |  |  |
| 70 | 1:20 | AIR |  |  |  |  |  |  |  | 7 | 9:00 | 0.5 | L |
| ${\mathrm{AlR} / \mathrm{O}_{2}}^{1}$ |  |  |  |  |  |  |  |  |  | 4 | 6:00 |  |  |
| 80 | 1:20 | AIR |  |  |  |  |  |  |  | 14 | 16:00 | 0.5 | N |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 7 9:00 |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 90 | 1:20 | AIR |  |  |  |  |  |  |  | 23 | 25:00 | 0.5 | 0 |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 10 | 12:00 |  |  |
| 100 | 1:20 | AIR |  |  |  |  |  |  |  | 42 | 44:00 | 1 | z |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 15 | 17:00 |  |  |
| 110 | 1:20 | AIR |  |  |  |  |  |  |  | 57 | 59:00 | 1 | z |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 21 | 23:00 |  |  |
| 120 | 1:20 | AIR |  |  |  |  |  |  |  | 75 | 77:00 | 1 | z |
| AIR/ $/ \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | $26 \quad 28: 00$ |  |  |  |
| Exceptional Exposure: In-Water Air Decompression ---- In-Water Airl $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 130 | 1:20 | AIR |  |  |  |  |  |  |  | 102 | 104:00 | 1.5 | Z |
| $140{\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  |  | 31 | 33:00 |  |  |
| 140 | 1:20 | AIR |  |  |  |  |  |  |  | 124 | 126:00 | 1.5 | z |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 35 | 37:00 |  |  |
| 150 | 1:20 | AIR |  |  |  |  |  |  |  | 143 | 145:00 | 2 | z |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 41 | 48:00 |  |  |
| 160 | 1:20 | AIR |  |  |  |  |  |  |  | 158 | 160:00 | 2 | z |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 48 | 55:00 |  |  |
| AIR $/ \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 178 | 180:00 | 2 |  |
|  |  |  |  |  |  |  |  |  |  | 53 | 60:00 |  |  |
| 180 | 1:20 | AIR |  |  |  |  |  |  |  | 201 | 203:00 | 2.5 |  |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 59 | 66:00 |  |  |
| 180 | 1:20 | AIR |  |  |  |  |  |  |  | 222 | 224:00 | 2.5 |  |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 64 | 71:00 |  |  |
| 200 | 1:20 | AIR |  |  |  |  |  |  |  | 240 | 242:00 | 2.5 |  |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 68 | 80:00 |  |  |
| 210 1:20 AIR $\begin{array}{cc}\text { AIR } / \mathrm{O}_{2}\end{array}$ |  |  |  |  |  |  |  |  |  | 256 | 258:00 | 3 |  |
|  |  |  |  |  |  |  |  |  |  | 73 | 85:00 |  |  |
| $220 \quad 1: 20 \begin{array}{cc}\text { AIR } \\ \text { AIR/O2 }\end{array}$ |  |  |  |  |  |  |  |  |  | 278 | 280:00 | 3 |  |
|  |  |  |  |  |  |  |  |  |  | 77 | 89:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 230 | 1:20 | AIR |  |  |  |  |  |  |  | 300 | 302:00 | 3.5 |  |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 82 | 94:00 |  |  |
| 240 1:20 AIR $\begin{gathered}\text { AIR } / \mathrm{O}_{2}\end{gathered}$ |  |  |  |  |  |  |  |  |  | 321 | 323:00 | 3.5 |  |
|  |  |  |  |  |  |  |  |  |  | 88 | 100:00 |  |  |
| $270 \begin{array}{ccc}1: 20 & \begin{array}{c}\text { AlR } \\ \text { AlR/O }\end{array}\end{array}$ |  |  |  |  |  |  |  |  |  | 398 | 400:00 | 4 |  |
|  |  |  |  |  |  |  |  |  |  | 102 | 119:00 |  |  |
| Excestional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 300 | 1:20 | AIR |  |  |  |  |  |  |  | 456 | 458:00 | 4.5 |  |
|  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 115 | 132:00 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total <br> Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |  |
| 70 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 48 | $2 \cdot 20$ | AIR |  |  |  |  |  |  |  |  | 0 | 220 | 0 | K |
|  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  |  | 0 | 220 |  |  |
| 50 | $1: 40$ | AIR |  |  |  |  |  |  |  |  | 2 | 4:20 | 0.5 | K |
|  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  |  | 1 | $3: 20$ |  |  |
| 55 | $1: 40$ | AIR |  |  |  |  |  |  |  |  | 9 | 11:20 | 0.5 | L |
|  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  |  | 5 | 7:20 |  |  |
| 60 | $1: 40$ | AIR |  |  |  |  |  |  |  |  | 14 | 10:20 | 0.5 | M |
|  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  |  | 8 | 10:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | 1:40 | AIR |  |  |  |  |  |  |  |  | 24 | 26:20 | 0.5 | N |
|  | $\mathrm{AlR}^{\text {( }} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  | 13 | 15:20 |  |  |
| 80 | $1: 40$ | AIR |  |  |  |  |  |  |  |  | 44 | 46:20 | 1 | 0 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 17 | 19:20 |  |  |
| 90 | 1:40 | AIR |  |  |  |  |  |  |  |  | 64 | 68:20 | 1 | $z$ |
|  |  | $\mathrm{AlRJO}_{2}$ |  |  |  |  |  |  |  |  | 24 | 28:20 |  |  |
| 100 | 1:40 | AIR |  |  |  |  |  |  |  |  | 88 | 90:20 | 1.5 | z |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  |  | 31 | 33:20 |  |  |
| Exceptional Exposure: In-Water Air Decompression ---- In-Water Air/ $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 110 | 1:40 | AIR |  |  |  |  |  |  |  |  | 120 | 122-20 | 1.5 | Z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 38 | 45:20 |  |  |
| 120 | 1:40 | AIR |  |  |  |  |  |  |  |  | 145 | 147:20 | 2 | $z$ |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 44 | 51:20 |  |  |
| 130 | 1:40 | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR} / \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  |  | 167 | 109:20 | 2 | z |
|  |  |  |  |  |  |  |  |  |  |  | 51 | 58:20 |  |  |
| 140 | 1:40 | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR} / \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  |  | 189 | 191:20 | 2.5 |  |
|  |  |  |  |  |  |  |  |  |  |  | 59 | 68:20 |  |  |
| 150 | 1.40 | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR}_{2} \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  |  | 219 | 221:20 | 2.5 |  |
|  |  |  |  |  |  |  |  |  |  |  | 66 | 78:20 |  |  |
| 160 | $1: 20$ | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR} / \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  | 1 | 244 | 247:00 | 3 |  |
|  |  |  |  |  |  |  |  |  |  | 1 | 72 | 85:00 |  |  |
| Exceptional Exposure: In-Water AirlO ${ }_{2}$ Decompression $-\ldots-$ SurDO $_{2}$ Required $-\ldots-\ldots$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 170 | $1: 20$ | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR}_{2} \end{gathered}$ |  |  |  |  |  |  |  | 2 | 265 | 269:00 | 3 |  |
|  |  |  |  |  |  |  |  |  |  | 1 | 78 | 91:00 |  |  |
| 180 | $1: 20$ | AIR |  |  |  |  |  |  |  | 4 | 289 | 295:00 | 3.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 2 | 83 | 97:00 |  |  |
| 180 | $1: 20$ | AIR |  |  |  |  |  |  |  | 5 | 316 | 323:00 | 3.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  | 3 | 88 | 103:00 |  |  |
| 200 | 1:20 | AIR |  |  |  |  |  |  |  | 9 | 345 | 356:00 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 5 | 93 | 115:00 |  |  |
| 210 | $1: 20$ | AIR |  |  |  |  |  |  |  | 13 | 378 | 383:00 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 7 | 98 | 122:00 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 240 | 1:20 | AIR |  |  |  |  |  |  |  | 25 | 454 | 481:00 | 5 |  |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 13 | 110 | 140:00 |  |  |
| 9-70 |  |  |  |  |  |  |  |  |  |  | Nav | Diving | anual - | olume 2 |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)


Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 | 80 | 70 | 60 | 50 |  | 30 | 20 |  |  |  |
| 90 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 3.00 | AIR |  |  |  |  |  |  |  |  | 0 | $3: 00$ | 0 | I |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  |  |  | 0 | 3.00 |  |  |
| 35 | $2 \cdot 20$ | AIR |  |  |  |  |  |  |  |  | 4 | 7:00 | 0.5 | J |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 2 | 5.00 |  |  |
| 40 | $2 \cdot 20$ | AIR |  |  |  |  |  |  |  |  | 14 | 17:00 | 0.5 | L |
|  |  | $\mathrm{AlR}^{\mathrm{AlO}}$ |  |  |  |  |  |  |  |  | 7 | 10:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 220 | AIR |  |  |  |  |  |  |  |  | 23 | 28:00 | 0.5 | M |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 12 | 15:00 |  |  |
| 50 | 220 | AIR |  |  |  |  |  |  |  |  | 31 | 34:00 | 1 | N |
|  |  | $\mathrm{AlR}^{\mathrm{A}} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 17 | 20:00 |  |  |
| 55 | 220 | AIR |  |  |  |  |  |  |  |  | 39 | 42:00 | 1 | 0 |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 21 | 24:00 |  |  |
| 60 | $2 \cdot 20$ | AIR |  |  |  |  |  |  |  |  | 56 | 59:00 | 1 | 0 |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 24 | 27:00 |  |  |
| 70 | 2.20 | AlR |  |  |  |  |  |  |  |  | 83 | 88:00 | 1.5 | $z$ |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 32 | 35:00 |  |  |
| Exceptional Exposure: In-Water Air Decompression ———— In-Water Air/ $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 200 | AIR |  |  |  |  |  |  |  | 5 | 125 | 132:40 | 2 | Z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 3 | 40 | 50:40 |  |  |
| 90 | 2.00 | AIR |  |  |  |  |  |  |  | 13 | 158 | 173:40 | 2 | z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 7 | 46 | 60:40 |  |  |
| 100 | 2.00 | AlR |  |  |  |  |  |  |  | 18 | 185 | 200:40 | 2.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 10 | 53 | 70:40 |  |  |
| 110 | 2.00 | AIR |  |  |  |  |  |  |  | 25 | 224 | 251:40 | 3 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 13 | 61 | 88:40 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 120 | 1:40 | AIR |  |  |  |  |  |  | 1 | 29 | 256 | 288:20 | 3.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  | 1 | 15 | 70 | 88:40 |  |  |
| 130 | $1: 40$ | AIR |  |  |  |  |  |  | 5 | 28 | 291 | 320:20 | 3.5 |  |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  | 5 | 15 | 78 | 110:40 |  |  |
| 140 | 1:40 | AIR |  |  |  |  |  |  | 8 | 28 | 330 | 368:20 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  | 8 | 15 | 86 |  |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 150 | 1:40 | AIR |  |  |  |  |  |  | 11 | 34 | 378 | 425:20 | 4.5 |  |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  | 11 | 17 | 94 | 139:40 |  |  |
| 180 | $1: 40$ | AIR |  |  |  |  |  |  | 13 | 40 | 418 | 473:20 | 4.5 |  |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ |  |  |  |  |  |  | 13 | 21 | 100 | 151:40 |  |  |
| 170 | 1:40 | AIR |  |  |  |  |  |  | 15 | 45 | 451 | 513:20 | 5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  | 15 | 23 | 106 | 188:40 |  |  |
| 180 | $1: 40$ | AIR |  |  |  |  |  |  | 16 | 51 | 479 | 548:20 | 5.5 |  |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  | 16 | 26 | 112 | 176:40 |  |  |
| 240 | 1.40 | AIR |  |  |  |  |  |  | 42 | 68 | 502 | 704:20 | 7.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  | 42 | 34 | 159 | 267:00 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) indude travel fime, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 | 80 | 70 | 60 |  |  | 30 | 20 |  |  |  |
| 100 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 3:20 | AIR |  |  |  |  |  |  |  |  | 0 | 3:20 | 0 | H |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 3:20 |  |  |
| 30 | 2:40 | AIR |  |  |  |  |  |  |  |  | 3 | 6:20 | 0.5 | J |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 5:20 |  |  |
| 35 | 2:40 | AIR |  |  |  |  |  |  |  |  | 15 | 18:20 | 0.5 | L |
|  |  | AIR/O2 |  |  |  |  |  |  |  |  | 8 | 11:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 2:40 | AIR |  |  |  |  |  |  |  |  | 26 | 29:20 | 1 | M |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 14 | 17:20 |  |  |
| 45 | 2:40 | AlR |  |  |  |  |  |  |  |  | 36 | 39:20 | 1 | N |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 19 | 22:20 |  |  |
| 50 | 2:40 | AIR |  |  |  |  |  |  |  |  | 47 | 50:20 | 1 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 24 | 27:20 |  |  |
| 55 | 2:40 | AIR |  |  |  |  |  |  |  |  | 65 | 68:20 | 1.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 28 | 31:20 |  |  |
| 60 | 2:40 | AIR |  |  |  |  |  |  |  |  | 81 | 84:20 | 1.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 33 | 35:20 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water Air) $\mathrm{O}_{2}$ Deoompression or SurDO 2 Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | 2:20 | AIR |  |  |  |  |  |  |  | 11 | 124 | 138:00 | 2 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 6 | 39 | 53:00 |  |  |
| 80 | 2:20 | AIR |  |  |  |  |  |  |  | 21 | 180 | 184:00 | 25 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 11 | 45 | 64:00 |  |  |
| 80 | 2:00 | AIR |  |  |  |  |  |  | 2 | 28 | 196 | 228:40 | 2.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 2 | 15 | 52 | 82:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 2:00 | AIR |  |  |  |  |  |  | 9 | 28 | 241 | 280:40 | 3 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 9 | 14 | 66 | 102:00 |  |  |
| 110 | 2:00 | AIR |  |  |  |  |  |  | 14 | 28 | 278 | 322:40 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 14 | 15 | 75 | 117:00 |  |  |
| 120 | 2:00 | AIR |  |  |  |  |  |  | 18 | 28 | 324 | 373:40 | 4 |  |
|  |  | AIR/O2 |  |  |  |  |  |  | 18 | 15 | 84 | 136:00 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 150 | 1:40 | AIR |  |  |  |  |  | 3 | 28 | 46 | 481 | 538:20 | 5 |  |
|  |  | AIR/O2 |  |  |  |  |  | 3 | 28 | 24 | 108 | 183:40 |  |  |

Table 9-9. Air Decompression Table (Continued).
(DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except frst air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total <br> Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet <br> Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 | 80 | 70 | 60 | 50 |  | 30 | 20 |  |  |  |
| 110 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 3:40 | AIR |  |  |  |  |  |  |  |  | 0 | $3: 40$ | 0 | H |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 0 | $3: 40$ |  |  |
| 25 | 3.00 | AIR |  |  |  |  |  |  |  |  |  | 6.40 | 0.5 | 1 |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 2 | 5.40 |  |  |
| 30 | 3.00 | AIR |  |  |  |  |  |  |  |  | 14 | 17:40 | 0.5 | K |
|  |  | AlR/O ${ }_{2}$ |  |  |  |  |  |  |  |  | 7 | 10:40 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 3.00 | AIR |  |  |  |  |  |  |  |  | 27 | $30: 40$ | 1 | M |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 14 | $17: 40$ |  |  |
| 40 | 3.00 | AIR |  |  |  |  |  |  |  |  | 39 | 42.40 | 1 | N |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 20 | 23:40 |  |  |
| 45 | 3.00 | AIR |  |  |  |  |  |  |  |  | 50 | 53.40 | 1 | 0 |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  |  |  | 26 | 29.40 |  |  |
| 50 | 3.00 | AIR |  |  |  |  |  |  |  |  | 71 | 74.40 | 1.5 | $z$ |
|  |  | $\mathrm{AlR}^{(2)}$ |  |  |  |  |  |  |  |  | 31 | 34.40 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water Air/O $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ------ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | 2:40 | AIR |  |  |  |  |  |  |  | 5 | 85 | 93:20 | 1.5 | Z |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  | 3 | 33 | 44:20 |  |  |
| 60 | 2-40 | AIR |  |  |  |  |  |  |  | 13 | 111 | 127:20 | 2 | z |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  | 7 | 36 | 51:20 |  |  |
| 70 | 2-40 | AIR |  |  |  |  |  |  |  | 28 | 155 | 184:20 | 2.5 | z |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 13 | 43 | 64:20 |  |  |
| 80 | $2 \cdot 20$ | AIR |  |  |  |  |  |  | 9 | 28 | 200 | 240:00 | 2.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  | 9 | 15 | 53 | 90:20 |  |  |
| Exceptional Exposure: In-Water AirlO2 Decompression --- SurDO $_{2}$ Required - |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 2:20 | AIR |  |  |  |  |  |  | 17 | 29 | 248 | 297:00 | 3.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  | 17 | 15 | 67 | 112.20 |  |  |
| 100 | $2 \cdot 20$ | AIR |  |  |  |  |  |  | 25 | 28 | 295 | 351:00 | 3.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  | 25 | 15 | 78 | 131:20 |  |  |
| 110 | 2.00 | AIR |  |  |  |  |  | 5 | 26 | 28 | 353 | 414:40 | 4 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 5 | 26 | 15 | 90 | 154:00 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 120 | 2.00 | AIR |  |  |  |  |  | 10 | 26 | 35 | 413 | $488 \cdot 40$ | 4.5 |  |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  | 10 | 26 | 18 | 101 | 173:00 |  |  |
| 180 | $1: 40$ | AIR |  |  |  |  | 3 | 23 | 47 | 68 | 583 | 738:20 | 7.5 |  |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  | 3 | 23 | 47 | 34 | 159 | 298:00 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 | 80 | 70 |  | 50 |  | 30 | 20 |  |  |  |
| 120 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 4:00 | AIR |  |  |  |  |  |  |  |  | 0 | 4:00 | 0 | F |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 0 | 4:00 |  |  |
| 20 | $3: 20$ | AIR |  |  |  |  |  |  |  |  | 2 | 6:00 | 0.5 | H |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 5:00 |  |  |
| 25 | 3:20 | AIR |  |  |  |  |  |  |  |  | 8 | 12:00 | 0.5 | J |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 4 | 8:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 3:20 | AIR |  |  |  |  |  |  |  |  | 24 | 28:00 | 0.5 | L |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 13 | 17:00 |  |  |
| 35 | $3: 20$ | AIR |  |  |  |  |  |  |  |  | 38 | 42:00 | 1 | N |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 20 | 24:00 |  |  |
| 40 | 3:20 | AIR |  |  |  |  |  |  |  |  | 51 | 55:00 | 1 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 27 | 31:00 |  |  |
| 45 | 3:20 | AIR |  |  |  |  |  |  |  |  | 72 | 76:00 | 1.5 | $z$ |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 33 | 37:00 |  |  |
| Excestional Exposure: In-Water Air Decompression --_-- In-Water Air $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | 3:00 | AIR |  |  |  |  |  |  |  | 9 | 86 | 98:40 | 1.5 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 5 | 33 | 46:40 |  |  |
| 55 | 3:00 | AIR |  |  |  |  |  |  |  | 18 | 116 | 138:40 | 2 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 10 | 35 | 53:40 |  |  |
| 60 | $3: 00$ | AIR |  |  |  |  |  |  |  | 27 | 142 | 172:40 | 2 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 14 | 39 | 61:40 |  |  |
| 70 | 2:40 | AIR |  |  |  |  |  |  | 12 | 28 | 189 | 233:20 | 2.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 12 | 15 | 50 | 85:40 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 2:40 | AIR |  |  |  |  |  |  | 24 | 28 | 246 | 301:20 | 3 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 24 | 14 | 67 | 118:40 |  |  |
| 80 | 2:20 | AIR |  |  |  |  |  | 7 | 28 | 28 | 303 | 367:00 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 7 | 28 | 15 | 79 | 140:20 |  |  |
| 100 | 2:20 | AIR |  |  |  |  |  | 14 | 26 | 28 | 372 | 443:00 | 4 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 14 | 28 | 15 | 94 | 167:20 |  |  |
| Exceptional Exposure: SurDO |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 110 | 2:20 | AIR |  |  |  |  |  | 21 | 25 | 38 | 433 | 520:00 | 5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 21 | 25 | 20 | 104 | 188:20 |  |  |
| 120 | 2:00 | AIR |  |  |  |  | 3 | 23 | 25 | 47 | 480 | 580:40 | 5.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 3 | 23 | 25 | 24 | 113 | 211:00 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times ( min ) include travel time, except frst air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 |  |  |  |  |  | 30 | 20 |  |  |  |
| 130 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | $4 \cdot 20$ | AIR |  |  |  |  |  |  |  |  | 0 | 4:20 | 0 | E |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 0 | 4:20 |  |  |
| 15 | $3: 40$ | AIR |  |  |  |  |  |  |  |  | 1 | 5:20 | 0.5 | G |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 1 | 5:20 |  |  |
| 20 | $3: 40$ | AIR |  |  |  |  |  |  |  |  | 4 | $8 \cdot 20$ | 0.5 | 1 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 6:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 3:40 | AIR |  |  |  |  |  |  |  |  | 17 | 21:20 | 0.5 | K |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 9 | 13:20 |  |  |
| 30 | 3:40 | AIR |  |  |  |  |  |  |  |  | 34 | 38:20 | 1 | M |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  |  |  | 18 | 22.20 |  |  |
| 35 | $3: 40$ | AIR |  |  |  |  |  |  |  |  | 49 | 53.20 | 1 | N |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 26 | $30: 20$ |  |  |
| 40 | $3: 20$ | AIR |  |  |  |  |  |  |  | 3 | 67 | 74:00 | 1.5 | $z$ |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  | 2 | 31 | 37:00 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water Air/O $\mathrm{O}_{2}$ Decompression or $\mathrm{SurDO}_{2}$ Required ------ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 3:20 | AIR |  |  |  |  |  |  |  | 12 | 84 | 100:00 | 1.5 | Z |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  | 6 | 33 | 48:00 |  |  |
| 50 | 320 | AIR |  |  |  |  |  |  |  | 22 | 116 | 142:00 | 2 | $z$ |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  |  |  |  | 11 | 35 | 55:00 |  |  |
| 55 | 3.00 | AIR |  |  |  |  |  |  | 4 | 28 | 145 | 180:40 | 2 | z |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ |  |  |  |  |  |  | 4 | 15 | 39 | 67:00 |  |  |
| 60 | 3.00 | AIR |  |  |  |  |  |  | 12 | 28 | 170 | 213:40 | 2.5 | z |
|  |  | $\mathrm{AlR}_{2}$ |  |  |  |  |  |  | 12 | 15 | 45 | 81:00 |  |  |
| Exceptional Exposure: In-Water AirlO2 Decompression --- SurDO $_{2}$ Required - |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | 2:40 | AIR |  |  |  |  |  | 1 | 26 | 28 | 235 | 283:20 | 3 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 1 | 26 | 14 | 63 | 117:40 |  |  |
| 80 | $2 \cdot 40$ | AIR |  |  |  |  |  | 12 | 26 | 28 | 297 | 368:20 | 3.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 12 | 26 | 15 | 78 | 144:40 |  |  |
| 90 | 2:40 | AIR |  |  |  |  |  | 21 | 26 | 28 | 374 | 452.20 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  | 21 | 26 | 15 | 94 | 174.40 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 2:20 | AIR |  |  |  |  | 6 | 23 | 26 | 38 | 444 | 540:00 | 5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  | 6 | 23 | 26 | 20 | 106 | 204:20 |  |  |
| 120 | $2 \cdot 20$ | AIR |  |  |  |  | 17 | 23 | 28 | 57 | 533 | 661:00 | 6 |  |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  |  | 17 | 23 | 28 | 29 | 130 | 255:20 |  |  |
| 180 | 200 | AIR |  |  |  | 13 | 21 | 45 | 57 | 94 | 658 | $890: 40$ | 9 |  |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ |  |  |  | 13 | 21 | 45 | 57 | 46 | 198 | 417:20 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times ( min ) include travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 90 | 80 | 70 | 60 |  |  | 30 | 20 |  |  |  |
| 140 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 4:40 | AIR |  |  |  |  |  |  |  |  | 0 | 4:40 | 0 | E |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 4:40 |  |  |
| 15 | 4:00 | AIR |  |  |  |  |  |  |  |  | 2 | 6:40 | 0.5 | H |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 5:40 |  |  |
| 20 | 4:00 | AIR |  |  |  |  |  |  |  |  | 7 | 11:40 | 0.5 | J |
|  |  | AlR/O2 |  |  |  |  |  |  |  |  | 4 | 8:40 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 4:00 | AIR |  |  |  |  |  |  |  |  | 26 | 30:40 | 1 | L |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 14 | 18:40 |  |  |
| 30 | 4:00 | AIR |  |  |  |  |  |  |  |  | 44 | 48:40 | 1 | N |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 23 | 27:40 |  |  |
| 35 | $3: 40$ | AIR |  |  |  |  |  |  |  | 4 | 59 | 67:20 | 1.5 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 2 | 30 | 36:20 |  |  |
| Exceptional Exposure: In-Water Air Decompression --_- In-Water Airi $\mathrm{O}_{2}$ Decompression or SurDO $\mathrm{S}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 3:40 | AIR |  |  |  |  |  |  |  | 11 | 80 | 95:20 | 1.5 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 6 | 33 | 48:20 |  |  |
| 45 | 3:20 | AIR |  |  |  |  |  |  | 3 | 21 | 113 | 141:00 | 2 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 3 | 11 | 34 | 57:20 |  |  |
| 50 | 3:20 | AIR |  |  |  |  |  |  | 7 | 28 | 145 | 184:00 | 2 | $z$ |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 7 | 14 | 40 | 70:20 |  |  |
| 55 | 3:20 | AIR |  |  |  |  |  |  | 16 | 28 | 171 | 219:00 | 2.5 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 16 | 15 | 45 | 85:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | 3:00 | AIR |  |  |  |  |  | 2 | 23 | 28 | 209 | 265:40 | 3 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 2 | 23 | 15 | 55 | 109:00 |  |  |
| 70 | 3:00 | AIR |  |  |  |  |  | 14 | 25 | 28 | 276 | 346:40 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 14 | 25 | 15 | 74 | 142:00 |  |  |
| 80 | 2:40 | AIR |  |  |  |  | 2 | 24 | 25 | 29 | 382 | 445:20 | 4 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 2 | 24 | 25 | 15 | 91 | 175:40 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ - |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 90 | 2:40 | AIR |  |  |  |  | 12 | 23 | 26 | 38 | 443 | 545:20 | 5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 12 | 23 | 26 | 19 | 107 | 210:40 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 |  | 70 | 60 | 50 |  | 30 | 20 |  |  |  |
| 150 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 5.00 | AIR |  |  |  |  |  |  |  |  | 0 | 5:00 | 0 | C |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 0 | 5:00 |  |  |
| 10 | $4: 20$ | AIR |  |  |  |  |  |  |  |  | 1 | 6:00 | 0.5 | F |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 1 | 6:00 |  |  |
| 15 | $4: 20$ | AIR |  |  |  |  |  |  |  |  | 3 | 8.00 | 0.5 | H |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 7:00 |  |  |
| 20 | 4:20 | AIR |  |  |  |  |  |  |  |  | 14 | 18:00 | 0.5 | K |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  |  | 8 | 13:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 4.20 | AIR |  |  |  |  |  |  |  |  | 35 | 40:00 | 1 | M |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  |  | 19 | 24:00 |  |  |
| 30 | 4:00 | AIR |  |  |  |  |  |  |  | 3 | 51 | 58.40 | 1.5 | 0 |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  | 2 | 26 | 32.40 |  |  |
| 35 | 4:00 | AIR |  |  |  |  |  |  |  | 11 | 72 | 87:40 | 1.5 | z |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  |  | 6 | 31 | 46.40 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water Air/ $\mathrm{O}_{2}$ Decompression or SurDO 2 Required ------ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 3:40 | AIR |  |  |  |  |  |  | 4 | 18 | 102 | 128:20 | 2 | Z |
|  |  | $\mathrm{AlRNO}_{2}$ |  |  |  |  |  |  | 4 | 9 | 34 | 56.40 |  |  |
| 45 | $3: 40$ | AIR |  |  |  |  |  |  | 10 | 25 | 140 | 179:20 | 2 | z |
|  |  | $\mathrm{AlRJ}_{2}$ |  |  |  |  |  |  | 10 | 13 | 39 | 71:40 |  |  |
| 50 | 3.20 | AIR |  |  |  |  |  | 3 | 15 | 28 | 170 | 220:00 | 2.5 | z |
|  |  | AlR/O2 |  |  |  |  |  | 3 | 15 | 15 | 45 | 87:20 |  |  |
| Exceptional Exposure: In-Water Airl $_{2}$ Decompression - $-\ldots \mathrm{SurDO}_{2}$ Required - |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | 3.20 | AIR |  |  |  |  |  | 6 | 22 | 28 | 211 | 271:00 | 3 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 6 | 22 | 15 | 56 | 113:20 |  |  |
| 60 | 3.20 | AIR |  |  |  |  |  | 11 | 26 | 28 | 248 | 317:00 | 3 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 11 | 26 | 15 | 66 | $132 \cdot 20$ |  |  |
| 70 | 3.00 | AIR |  |  |  |  | 3 | 24 | 25 | 28 | 330 | 413:40 | 4 |  |
|  |  | $\mathrm{AlR}_{2}$ |  |  |  |  | 3 | 24 | 25 | 15 | 84 | 170:00 |  |  |
| Exceptional Exposure: SurDO2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 3:00 | AIR |  |  |  |  | 15 | 23 | 26 | 35 | 430 | 532.40 | 4.5 |  |
|  |  | AIR/O2 |  |  |  |  | 15 | 23 | 26 | 18 | 104 | 205:00 |  |  |
| 90 | 2:40 | AIR |  |  |  | 3 | 22 | 23 | 26 | 47 | 488 | 620:20 | 5.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  | 3 | 22 | 23 | 26 | 24 | 118 | 238.40 |  |  |
| 120 | $2 \cdot 20$ | AIR |  |  | 3 | 20 | 22 | 23 | 50 | 75 | 608 | 804:00 | 8 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  | 3 | 20 | 22 | 23 | 50 | 37 | 168 | 355.40 |  |  |
| 180 | 2.00 | AIR |  | 2 | 18 | 20 | 42 | 48 | 79 | 121 | 694 | 1027:40 | 10.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  | 2 | 19 | 20 | 42 | 48 | 79 | 58 | 222 | 537:20 |  |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

|  | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) |  |  | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |  |
| 160 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 5:20 | AIR |  |  |  |  |  |  |  |  | 0 | 5:20 | 0 | C |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  |  | 0 | 5:20 |  |  |
| $\begin{array}{llcc}10 & \text { 4:40 } & \\ & \\ & \\ & \text { AlR } / \mathrm{O}_{2}\end{array}$ |  |  |  |  |  |  |  |  |  |  | 1 | 6:20 | 0.5 | F |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 6:20 |  |  |
| 15 | 4:40 | AIR |  |  |  |  |  |  |  |  | 5 | 10:20 | 0.5 | I |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  |  |  | 3 | 8:00 |  |  |
| In-Water $\mathrm{Air} \mathrm{O}_{2}$ Decompression or Sur) $\mathrm{O}_{2}$ Recommended $\ldots \ldots \ldots$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 4:40 | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR} / \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  |  | 22 | 27:20 | 0.5 | L |
|  |  |  |  |  |  |  |  |  |  |  | 12 | 17:20 |  |  |
| 25 | 4:20 | AIR |  |  |  |  |  |  |  | 3 | 41 | 49:00 | 1 | N |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 2 | 21 | 28:00 |  |  |
| 30 | 4:00 | AIR |  |  |  |  |  |  | 1 | 8 | 60 | 73:40 | 1.5 | 0 |
| $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 5 | 28 | 39:00 |  |  |



| n | S |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 70 | 3:20 | AIR |  | 15 | 23 | 28 | 29 | 399 | 498:00 | 4.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  | 15 | 23 | 28 | 15 | 99 | 197:20 |  |
| 80 | 3:00 | AIR | 6 | 21 | 24 | 25 | 44 | 482 | 805:40 | 5.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ | 6 | 21 | 24 | 25 | 23 | 114 | 237:00 |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

| Bottom Time | Time to First Stop |  | DECOMPRESSION STOPS (FSW) <br> Stop times ( min ) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total <br> Ascent <br> Time <br> (M:S) | Chamber $\mathrm{O}_{2}$ <br> Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | (M:S) | Gas Mix |  |  |  |  |  |  |  | 30 | 20 |  |  |  |
| 170 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 5:40 | AIR |  |  |  |  |  |  |  |  | 0 | 5.40 | 0 | D |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 5.40 |  |  |
| 10 | $5: 00$ | AIR |  |  |  |  |  |  |  |  | 2 | 7:40 | 0.5 | G |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 6.40 |  |  |
| 15 | 5.00 | AIR |  |  |  |  |  |  |  |  | 7 | 12.40 | 0.5 | J |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 4 | 9.40 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 4:40 | AIR |  |  |  |  |  |  |  | 1 | 29 | $35: 20$ | 1 | L |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 1 | 15 | 21:20 |  |  |
| 25 | 420 | AIR |  |  |  |  |  |  | 1 | 6 | 48 | 58:00 | 1 | N |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  | 1 | 4 | 23 | 33:20 |  |  |
| Exceptional Exposure: In-Water Air Decompression ---- In-Water Air/ $\mathrm{O}_{2}$ Decompression or SurDO ${ }_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | $4: 20$ | AIR |  |  |  |  |  |  | 5 | 11 | 72 | 83:00 | 1.5 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 5 | 6 | 29 | 45:20 |  |  |
| 35 | 400 | AIR |  |  |  |  |  | 2 | 9 | 17 | 113 | 145.40 | 2 | $z$ |
|  |  | $\mathrm{AlRJO}_{2}$ |  |  |  |  |  | 2 | 9 | 9 | 35 | 65:00 |  |  |
| 40 | 4:00 | AIR |  |  |  |  |  | 6 | 13 | 23 | 155 | 201:40 | 2.5 | $z$ |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  | 6 | 13 | 12 | 43 | 84:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 4:00 | AIR |  |  |  |  |  | 12 | 16 | 28 | 194 | 254:40 | 2.5 |  |
|  |  | $\mathrm{AlRJ}_{2}$ |  |  |  |  |  | 12 | 18 | 15 | 51 | 109:00 |  |  |
| 50 | $3: 40$ | AIR |  |  |  |  | 5 | 12 | 23 | 28 | 243 | 315:20 | 3 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  | 5 | 12 | 23 | 15 | 65 | 134:40 |  |  |
| 55 | 3.40 | AIR |  |  |  |  | 9 | 16 | 25 | 28 | 287 | 369:20 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 9 | 16 | 25 | 15 | 76 | 155.40 |  |  |
| 60 | 320 | AIR |  |  |  | 2 | 11 | 21 | 28 | 28 | 344 | 438:00 | 4 |  |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  | 2 | 11 | 21 | 26 | 15 | 87 | 181:20 |  |  |
| Exceptional Exposure: SurDO2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | $3 \cdot 20$ | AIR |  |  |  | 7 | 18 | 24 | 25 | 39 | 454 | 572.00 | 5 |  |
|  |  | $\mathrm{AlR}^{(1)}$ |  |  |  | 7 | 18 | 24 | 25 | 20 | 109 | 228:20 |  |  |
| 80 | 320 | AIR |  |  |  | 17 | 22 | 23 | 26 | 53 | 525 | 670:00 | 6 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 17 | 22 | 23 | 28 | 27 | 128 | 267:20 |  |  |
| 90 | 3.00 | AIR |  |  | 7 | 20 | 22 | 23 | 37 | 68 | 574 | 752.40 | 7 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  | 7 | 20 | 22 | 23 | 37 | 33 | 148 | 318:20 |  |  |
| 120 | $2 \cdot 40$ | AIR |  | 9 | 19 | 20 | 22 | 42 | 60 | 94 | 659 | 928:20 | 9 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  | 9 | 18 | 20 | 22 | 42 | 60 | 46 | 198 | 454:00 |  |  |
| 180 | 220 | AIR | 10 | 18 | 18 | 40 | 43 | 70 | 97 | 156 | 703 | 1159:00 | 11.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ | 10 | 18 | 19 | 40 | 43 | 70 | 97 | 75 | 228 | 648:00 |  |  |

Table 9-9. Air Decompression Table (Continued) (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Chamber $\mathrm{O}_{2}$ <br> Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 |  |  | 60 |  | 40 | 30 | 20 |  |  |  |
| 180 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 6:00 | AIR |  |  |  |  |  |  |  |  | 0 | 6:00 | 0 | D |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 0 | 6:00 |  |  |
| 10 | 5:20 | AIR |  |  |  |  |  |  |  |  | 3 | 9:00 | 0.5 | G |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 8:00 |  |  |
| 15 | 5:20 | AIR |  |  |  |  |  |  |  |  | 11 | 17:00 | 0.5 | J |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 6 | 12:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 5:00 | AIR |  |  |  |  |  |  |  | 4 | 34 | 43:40 | 1 | M |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 2 | 18 | 25:40 |  |  |
| 25 | 4:40 | AIR |  |  |  |  |  |  | 4 | 7 | 54 | 70:20 | 1.5 | 0 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 4 | 4 | 26 | 39:40 |  |  |
| Exceptional Exposure: In-Water Air Decompression --- In-Water Air/O2, Decompression or $\mathrm{SurDO}_{2}$ Required ----- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 4:20 | AIR |  |  |  |  |  | 2 | 7 | 14 | 83 | 111:00 | 1.5 | Z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 2 | 7 | 7 | 31 | 57:20 |  |  |
| 35 | 4:20 | AIR |  |  |  |  |  | 5 | 13 | 19 | 138 | 180:00 | 2 | $z$ |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 5 | 13 | 10 | 40 | 78:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 4:00 | AIR |  |  |  |  | 2 | 11 | 12 | 28 | 175 | 232:40 | 2.5 | z |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 2 | 11 | 12 | 14 | 47 | 96:00 |  |  |
| 45 | 4:00 | AIR |  |  |  |  | 7 | 11 | 20 | 28 | 231 | 301:40 | 3 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  | 7 | 11 | 20 | 15 | 61 | 129:00 |  |  |
| 50 | $3: 40$ | AIR |  |  |  | 1 | 11 | 13 | 25 | 28 | 276 | 358:20 | 3.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 1 | 11 | 13 | 25 | 15 | 74 | 153:40 |  |  |
| 55 | 3:40 | AIR |  |  |  | 5 | 11 | 19 | 26 | 28 | 336 | 429:20 | 4 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 5 | 11 | 19 | 28 | 14 | 87 | 181:40 |  |  |
| Exceptional Exposure: $\mathrm{SurDO}_{2}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | 3:40 | AIR |  |  |  | 8 | 13 | 24 | 25 | 31 | 405 | 510:20 | 4.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 8 | 13 | 24 | 25 | 16 | 100 | 205:40 |  |  |
| 70 | $3: 20$ | AIR |  |  | 3 | 13 | 21 | 24 | 25 | 48 | 498 | 636:00 | 5.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  | 3 | 13 | 21 | 24 | 25 | 25 | 118 | 253:20 |  |  |

Table 9-9. Air Decompression Table (Continued).
(DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

|  | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) include travel time, except frst air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | $\begin{aligned} & \text { Chamber } \\ & \mathrm{O}_{2} \\ & \text { Periods } \end{aligned}$ | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) |  |  |  |  |  |  |  |  |  | 30 | 20 |  |  |  |
| 190 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 6.20 | AIR |  |  |  |  |  |  |  |  | 0 | 6.20 | 0 | D |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  |  |  |  | 0 | 6.20 |  |  |
| 10 | $5: 40$ | AIR |  |  |  |  |  |  |  |  | 4 | 10:20 | 0.5 | H |
|  |  | $\mathrm{AlR}_{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 2 | 8:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 5.40 | AIR |  |  |  |  |  |  |  |  | 17 | 23:20 | 0.5 | K |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 9 | 15:20 |  |  |
| 20 | 5:00 | AIR |  |  |  |  |  |  | 1 | 7 | 37 | 50:40 | 1 | N |
|  |  | $\mathrm{AlR}^{\text {O }}$ |  |  |  |  |  |  | 1 | 4 | 19 | 30:00 |  |  |
| 25 | 4.40 | AIR |  |  |  |  |  | 2 | 6 | 9 | 67 | $89: 20$ | 1.5 | $z$ |
|  |  | $\mathrm{AlR}_{2} \mathrm{O}_{2}$ |  |  |  |  |  | 2 | 6 | 5 | 28 | 40:40 |  |  |
| Exceptional Exposure: In-Water Air Decompression ----- In-Water AiriO $\mathrm{O}_{2}$ Decompression or SurDO ${ }_{2}$ Required ------ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 4:40 | AIR |  |  |  |  |  | 6 | 8 | 14 | 111 | 144:20 | 2 | z |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  |  |  | 6 | 8 | 8 | 35 | 67:40 |  |  |
| 35 | $4: 20$ | AIR |  |  |  |  | 3 | 8 | 13 | 22 | 160 | 211:00 | 2.5 | z |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ |  |  |  |  | 3 | 8 | 13 | 12 | 44 | 90:20 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | $4 \cdot 20$ | AlR |  |  |  |  | 7 | 12 | 14 | 29 | 210 | 277:00 | 3 |  |
|  |  | $\mathrm{AlR}^{2} \mathrm{O}_{2}$ |  |  |  |  | 7 | 12 | 14 | 15 | 56 | 119.20 |  |  |
| 45 | 4:00 | AIR |  |  |  | 2 | 11 | 12 | 23 | 28 | 262 | 342.40 | 3.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  |  | 2 | 11 | 12 | 23 | 15 | 70 | 148:00 |  |  |
| 50 | 4:00 | AIR |  |  |  | 7 | 11 | 16 | 26 | 28 | 321 | 413:40 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}$ |  |  |  | 7 | 11 | 16 | 28 | 15 | 83 | 178:00 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | $3: 40$ | AIR |  |  | 2 | 10 | 10 | 24 | 25 | 30 | 398 | 501:20 | 4.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  | 2 | 10 | 10 | 24 | 25 | 16 | 98 | 204:40 |  |  |
| 60 | $3: 40$ | AIR |  |  | 5 | 10 | 16 | 24 | 25 | 40 | 454 | 578:20 | 5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  |  | 5 | 10 | 16 | 24 | 25 | 21 | 108 | 233:40 |  |  |
| 90 | 3.20 | AIR |  | 11 | 19 | 20 | 21 | 28 | 51 | 83 | 628 | 863:00 | 8.5 |  |
|  |  | $\mathrm{AlRO}_{2}$ |  | 11 | 19 | 20 | 21 | 28 | 51 | 42 | 177 | 408:40 |  |  |
| 120 | 3.00 | AIR | 15 | 17 | 19 | 20 | 37 | 46 | 79 | 113 | 681 | 1040:40 | 10.5 |  |
|  |  | $\mathrm{AlR}^{(1)} \mathrm{O}_{2}$ | 15 | 17 | 18 | 20 | 37 | 46 | 79 | 55 | 219 | 550:20 |  |  |


| $\begin{aligned} & \text { Bottom Time } \\ & (\mathrm{min}) \end{aligned}$ | Time to First Stop (M:S) | Gas Mix | DECOMPRESSION STOPS (FSW) Stop times (min) indude travel time, except first air and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  | 20 | Total <br> Ascent Time (M:S) | $\begin{aligned} & \text { Chamber } \\ & \mathrm{O}_{2} \\ & \text { Periods } \end{aligned}$ | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 |  |  | 60 | 50 | 40 | 30 |  |  |  |  |
| 200 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 6:00 | AIR |  |  |  |  |  |  |  |  | 1 | 7:40 | 0.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 7:40 |  |  |
| 10 | 6:00 | AIR |  |  |  |  |  |  |  |  | 2 | 8:40 | 0.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  |  | 1 | 7:40 |  |  |
| 15 | 5.40 | AIR |  |  |  |  |  |  |  | 2 | 22 | 30:20 | 0.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  | 1 | 11 | 18:20 |  |  |
| 20 | 5:20 | AIR |  |  |  |  |  |  | 5 | 6 | 43 | 60:00 | 1 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  | 5 | 4 | 21 | 36:20 |  |  |
| 25 | 5:00 | AIR |  |  |  |  |  | 5 | 6 | 11 | 78 | 105:40 | 1.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  | 5 | 6 | 6 | 29 | 52:00 |  |  |
| 30 | 4:40 | AIR |  |  |  |  | 4 | 5 | 11 | 18 | 136 | 179:20 | 2 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  | 4 | 5 | 11 | 9 | 40 | 79.40 |  |  |
| 35 | 4:20 | AIR |  |  |  | 1 | 6 | 10 | 13 | 26 | 179 | 240:00 | 2.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  | 1 | 6 | 10 | 13 | 13 | 49 | 102:20 |  |  |
| 40 | 4:20 | AIR |  |  |  | 3 | 10 | 12 | 18 | 28 | 243 | 319:00 | 3 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 3 | 10 | 12 | 18 | 15 | 65 | 138:20 |  |  |
| 45 | 4:20 | AIR |  |  |  | 8 | 11 | 12 | 28 | 28 | 300 | 300:00 | 3.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  | 8 | 11 | 12 | 28 | 15 | 79 | 168:20 |  |  |
| 50 | 4:00 | AIR |  |  | 3 | 10 | 11 | 20 | 28 | 28 | 377 | 479:40 | 4.5 |  |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  | 3 | 10 | 11 | 20 | 28 | 15 | 95 | 200:00 |  |  |

## 210 FSW

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 6:20 | AIR |  |  |  |  |  |  | 1 | 8:00 | 0.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 1 | 8:00 |  |
| 10 | 6:20 | AIR |  |  |  |  |  |  | 5 | 12:00 | 0.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  | 3 | 10:00 |  |
| 15 | 6:00 | AIR |  |  |  |  |  | 5 | 26 | 37:40 | 1 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  | 3 | 13 | 22:40 |  |
| 20 | 5:20 | AIR |  |  |  | 2 | 6 | 7 | 50 | 71:00 | 1.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 2 | 6 | 4 | 24 | 42:20 |  |
| 25 | 5:00 | AIR |  |  | 2 | 6 | 7 | 13 | 94 | 127:40 | 1.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  | 2 | 6 | 7 | 7 | 32 | 65:00 |  |
| 30 | 4:40 | AIR |  | 2 | 5 | 6 | 13 | 21 | 156 | 208:20 | 2 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  | 2 | 5 | 6 | 13 | 11 | 43 | 90:40 |  |
| 35 | 4:40 | AIR |  | 5 | 6 | 12 | 14 | 28 | 214 | 284:20 | 3 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  | 5 | 6 | 12 | 14 | 14 | 58 | 124:40 |  |
| 40 | $4: 20$ | AIR | 2 | 6 | 11 | 12 | 22 | 28 | 271 | 357:00 | 3.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ | 2 | 6 | 11 | 12 | 22 | 15 | 74 | 157:20 |  |
| 45 | $4: 20$ | AIR | 4 | 10 | 11 | 16 | 25 | 29 | 347 | 447:00 | 4 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ | 4 | 10 | 11 | 16 | 25 | 15 | 89 | 190:20 |  |
| 50 | $4: 20$ | AIR | 9 | 10 | 11 | 23 | 28 | 35 | 426 | 545:00 | 4.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ | 9 | 10 | 11 | 23 | 28 | 18 | 104 | 221:20 |  |

Table 9-9. Air Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM )

|  | Time to First Stop |  | DECOMPRESSION STOPS (FSW) <br> Stop times (min) include travel time, except first air and frst $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  | Total <br> Ascent Time <br> (M:S) | Chamber $\mathrm{O}_{2}$ Periods | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | (M:S) | Gas Mix | 100 | 90 |  | 70 | 60 | 50 | 40 | 30 | 20 |  |  |  |
| 220 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 6:40 | AlR |  |  |  |  |  |  |  |  | 2 | $9: 20$ | 0.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  |  |  |  | 1 | $8: 20$ |  |  |
| 10 | 8:40 | AIR |  |  |  |  |  |  |  |  | 8 | 15:20 | 0.5 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}$ |  |  |  |  |  |  |  |  | 4 | 11:20 |  |  |
| 15 | 6:00 | AIR |  |  |  |  |  |  | 1 | 7 | 30 | 44.40 | 1 |  |
|  |  | $\mathrm{AlR}^{\text {O }}$ 2 |  |  |  |  |  |  | 1 | 4 | 15 | 27:00 |  |  |
| 20 | $5: 40$ | AIR |  |  |  |  |  | 5 | 6 | 7 | 63 | 87:20 | 1.5 |  |
|  |  | $\mathrm{AlR}^{\text {/ }} \mathrm{O}_{2}$ |  |  |  |  |  | 5 | 6 | 4 | 27 | 48:40 |  |  |
| 25 | $5: 20$ | AIR |  |  |  |  | 5 | 6 | 8 | 14 | 118 | 158:00 | 2 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  | 5 | 6 | 8 | 7 | 38 | 75:20 |  |  |
| 30 | 5:00 | AIR |  |  |  | 5 | 5 | 8 | 13 | 24 | 174 | 234:40 | 2.5 |  |
|  |  | $\mathrm{AlR}^{\text {/ }} \mathrm{O}_{2}$ |  |  |  | 5 | 5 | 8 | 13 | 13 | 47 | 102.00 |  |  |
| 35 | 4.40 | AIR |  |  | 3 | 5 | 9 | 11 | 18 | 28 | 244 | 323:20 | 3 |  |
|  |  | $\mathrm{AlR}^{2}$ |  |  | 3 | 5 | 9 | 11 | 18 | 15 | 66 | 142:40 |  |  |
| 40 | 4.20 | AIR |  | 1 | 4 | 9 | 11 | 11 | 26 | 28 | 312 | 407-00 | 4 |  |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  | 1 | 4 | 9 | 11 | 11 | 26 | 15 | 82 | 179:20 |  |  |

250 FSW

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 7:40 | $\begin{gathered} \mathrm{AlR} \\ \mathrm{AlR} / \mathrm{O}_{2} \end{gathered}$ |  |  |  |  |  |  |  | 3 |  | 11:20 | 0.5 |
|  |  |  |  |  |  |  |  |  |  |  | 2 | 10:20 |  |
| 10 | 7.20 | AIR |  |  |  |  |  |  |  | 2 | 15 | 25:00 | 0.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  |  |  |  |  | 1 | 8 | 17:00 |  |
| 15 | 6.40 | AIR |  |  |  |  |  | 3 | 7 | 7 | 41 | 65:20 | 1 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  |  |  |  |  | 3 | 7 | 4 | 21 | 42-40 |  |
| 20 | 6800 | AIR |  |  |  | 2 | 6 | 5 | 7 | 12 | 106 | 144:40 | 2 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  |  | 2 | 6 | 5 | 7 | 6 | 35 | 73:00 |  |
| 25 | 5.40 | AIR |  |  | 4 | 5 | 5 | 7 | 13 | 24 | 175 | 239.20 | 2.5 |
|  |  | $\mathrm{AlR} / \mathrm{O}_{2}$ |  |  | 4 | 5 | 5 | 7 | 13 | 13 | 47 | 105:40 |  |
| 30 | 5.20 | AIR |  | 4 | 4 | 5 | 9 | 11 | 20 | 28 | 257 | 344:00 | 3.5 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ |  | 4 | 4 | 5 | 9 | 11 | 20 | 14 | 70 | 153:20 |  |
| 35 | 5.00 | AIR | 2 | 5 | 4 | 10 | 11 | 14 | 25 | 29 | 347 | 452.40 | 4 |
|  |  | ${\mathrm{AlR} / \mathrm{O}_{2}}^{2}$ | 2 | 5 | 4 | 10 | 11 | 14 | 25 | 15 | 89 | 198:00 |  |

300 FSW


Table 9-4. Sea Level Equivalent Depth (fsw).

| Actual Depth (fsw) | Altitude (feet) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 |
| 10 | 10 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| 15 | 15 | 20 | 20 | 20 | 20 | 20 | 20 | 25 | 25 | 25 |
| 20 | 20 | 25 | 25 | 25 | 25 | 25 | 30 | 30 | 30 | 30 |
| 25 | 25 | 30 | 30 | 30 | 35 | 35 | 35 | 35 | 35 | 40 |
| 30 | 30 | 35 | 35 | 35 | 40 | 40 | 40 | 45 | 45 | 45 |
| 35 | 35 | 40 | 40 | 45 | 45 | 45 | 50 | 50 | 50 | 60 |
| 40 | 40 | 45 | 45 | 50 | 50 | 50 | 55 | 55 | 60 | 60 |
| 45 | 45 | 50 | 55 | 55 | 55 | 60 | 60 | 70 | 70 | 70 |
| 50 | 50 | 55 | 60 | 60 | 70 | 70 | 70 | 70 | 70 | 80 |
| 55 | 55 | 60 | 70 | 70 | 70 | 70 | 80 | 80 | 80 | 80 |
| 60 | 60 | 70 | 70 | 70 | 80 | 80 | 80 | 90 | 90 | 90 |
| 65 | 65 | 70 | 80 | 80 | 80 | 90 | 90 | 90 | 100 | 100 |
| 70 | 70 | 80 | 80 | 90 | 90 | 90 | 100 | 100 | 100 | 110 |
| 75 | 75 | 90 | 90 | 90 | 100 | 100 | 100 | 110 | 110 | 110 |
| 80 | 80 | 90 | 90 | 100 | 100 | 100 | 110 | 110 | 120 | 120 |
| 85 | 85 | 100 | 100 | 100 | 110 | 110 | 120 | 120 | 120 | 130 |
| 90 | 90 | 100 | 110 | 110 | 110 | 120 | 120 | 130 | 130 | 140 |
| 95 | 95 | 110 | 110 | 110 | 120 | 120 | 130 | 130 | 140 | 140 |
| 100 | 100 | 110 | 120 | 120 | 130 | 130 | 130 | 140 | 140 | 150 |
| 105 | 105 | 120 | 120 | 130 | 130 | 140 | 140 | 150 | 150 | 160 |
| 110 | 110 | 120 | 130 | 130 | 140 | 140 | 150 | 150 | 180 | 180 |
| 115 | 115 | 130 | 130 | 140 | 140 | 150 | 150 | 160 | 170 | 170 |
| 120 | 120 | 130 | 140 | 140 | 150 | 150 | 160 | 170 | 170 | 180 |
| 125 | 125 | 140 | 140 | 150 | 180 | 180 | 170 | 170 | 180 | 190 |
| 130 | 130 | 140 | 150 | 160 | 180 | 170 | 170 | 180 | 180 | 190 |
| 135 | 135 | 150 | 160 | 160 | 170 | 170 | 180 | 180 | 190 | 200 |
| 140 | 140 | 180 | 160 | 170 | 170 | 180 | 180 | 190 | 200 | 210 |
| 145 | 145 | 160 | 170 | 170 | 180 | 190 | 180 | 200 | 210 |  |
| 150 | 180 | 170 | 170 | 180 | 190 | 190 | 200 | 210 |  |  |
| 155 | 170 | 170 | 180 | 180 | 180 | 200 | 210 |  |  |  |
| 160 | 170 | 180 | 180 | 190 | 200 | 200 |  |  |  |  |
| 165 | 180 | 180 | 190 | 200 | 200 |  |  |  |  |  |
| 170 | 180 | 180 | 190 | 200 |  |  |  |  |  |  |
| 175 | 180 | 190 | 200 |  |  |  |  |  |  |  |
| 180 | 180 | 200 | 210 |  |  |  |  |  |  |  |
| 185 | 200 | 200 |  |  |  |  |  |  |  |  |
| 190 | 200 |  |  |  |  |  |  |  |  |  |
| Table Water Stops |  |  |  |  | alent | Depths |  |  |  |  |
| 10 | 10 | 9 | 9 | 9 | 8 | 8 | 8 | 7 | 7 | 7 |
| 20 | 19 | 18 | 18 | 17 | 17 | 16 | 15 | 15 | 14 | 14 |
| 30 | 29 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 | 21 |
| 40 | 39 | 37 | 36 | 35 | 33 | 32 | 31 | 30 | 29 | 28 |
| 50 | 48 | 47 | 45 | 43 | 42 | 40 | 39 | 37 | 36 | 34 |
| 60 | 58 | 56 | 54 | 52 | 50 | 48 | 46 | 45 | 43 | 41 |

Note:

Table 9-6. Required Surface Interval Before Ascent to Altitude After Diving.


NOTE 1 When using Table 9-6, use the highest repetitive group designator obtained in the previous 24 -hour period.
NOTE 2 Table 9-6 may only be used when the maximum altitude achieved is 10,000 feet or less. For ascents above 10,000 feet, consult NAVSEA 00 C for guidance.
NOTE 3 The cabin pressure in commercial aircraft is maintained at a constant value regardless of the actual altitude of the flight. Though cabin pressure varies somewhat with aircraft type, the nominal value is 8,000 feet. For commercial flights, use a final altitude of 8,000 feet to compute the required surface interval before flying.
NOTE 4 No surface interval is required before taking a commercial flight if the dive site is at 8,000 feet or higher. In this case, flying results in an increase in atmospheric pressure rather than a decrease.
NOTE 5 For ascent to altitude following a non-saturation helium-oxygen dive, wait 12 hours if the dive was a no-decompression dive. Wait 24 hours if the dive was a decompression dive.

Table 9.5. Repeitive Groups Associated with Intial Ascent to Aftitude.

| Alitude (feet) | Repetitive Group |
| :---: | :---: |
| 1000 | A |
| 2000 | A |
| 3000 | B |
| 4000 | C |
| 5000 | D |
| 6000 | E |
| 7000 | F |
| 8000 | G |
| 9000 | H |
| 10000 | I |

# MK 16 TABLES 



Table 18-9. No Decompression Limits and Repetitive Group Designators for MK $16 \mathrm{MOD} 1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Dives.

| Depth (fsw) | No-Stop Limit | Repetitive Group Designator |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | D | E | F | G | H | 1 | J | K | L | M | N | 0 | z |
| 10 | Unlimited | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 15 | Unlimited | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | Unlimited | 153 | 420 | * |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | Unlimited | 51 | 87 | 133 | 196 | 295 | 557 | * |  |  |  |  |  |  |  |  |  |
| 30 | Unlimited | 31 | 50 | 72 | 98 | 128 | 164 | 210 | 273 | 372 | 629 | * |  |  |  |  |  |
| 35 | Unlimited | 22 | 35 | 50 | 66 | 84 | 103 | 126 | 151 | 181 | 217 | 263 | 326 | 425 | 680 | * |  |
| 40 | Unlimited | 89 | 168 | 318 | * |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | Unlimited | 27 | 44 | 63 | 84 | 108 | 136 | 169 | 210 | 265 | 344 | 496 | * |  |  |  |  |
| 60 | 297 | 16 | 25 | 36 | 46 | 58 | 70 | 83 | 97 | 113 | 130 | 149 | 170 | 194 | 222 | 255 | 297 |
| 70 | 130 | 11 | 18 | 25 | 32 | 39 | 47 | 55 | 64 | 73 | 83 | 93 | 103 | 115 | 127 | 130 |  |
| 80 | 70 | 9 | 14 | 19 | 24 | 30 | 36 | 42 | 48 | 54 | 61 | 68 | 70 |  |  |  |  |
| 90 | 50 | 7 | 11 | 15 | 20 | 24 | 29 | 33 | 38 | 43 | 48 | 50 |  |  |  |  |  |
| 100 | 39 | 6 | 9 | 13 | 16 | 20 | 24 | 28 | 32 | 36 | 39 |  |  |  |  |  |  |
| 110 | 32 | 5 | 8 | 11 | 14 | 17 | 20 | 24 | 27 | 30 | 32 |  |  |  |  |  |  |
| 120 | 27 | 4 | 7 | 9 | 12 | 15 | 18 | 20 | 23 | 26 | 27 |  |  |  |  |  |  |
| 130 | 23 | 3 | 6 | 8 | 11 | 13 | 16 | 18 | 21 | 23 |  |  |  |  |  |  |  |
| 140 | 21 | 3 | 5 | 7 | 9 | 12 | 14 | 16 | 18 | 21 |  |  |  |  |  |  |  |
| 150 | 17 | 3 | 5 | 6 | 8 | 10 | 12 | 15 | 17 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 160 | 15 | 3 | 4 | 6 | 8 | 9 | 11 | 13 | 15 |  |  |  |  |  |  |  |  |
| 170 | 13 | 4 | 5 | 7 | 9 | 10 | 12 | 13 |  |  |  |  |  |  |  |  |  |
| 180 | 12 |  | 3 | 5 | 6 | 8 | 9 | 11 | 12 |  |  |  |  |  |  |  |  |
| 190 | 10 |  |  | 4 | 6 | 7 | 9 | 10 |  |  |  |  |  |  |  |  |  |

- Diver does not acquire a repettive group designator during dives to these depths.
* Highest repetitive group that can be achieved at this depth regardless of bottom time.

Table 18-10. Residual Nitrogen Timetable for MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Dives.


- Repetitive dives to these depths are equivalent to remaining on the surface. Add the bottom time of the dive to the preceding surface interval. Use the Surface Interval Credit Table (SICT) to determine the repetitive group at the end of the dive.
" Residual Nitrogen Time cannot be determined using this table (see paragraph $9-9.1$ for instructions).


## REPETITIVE DIVE WORKSHEET FOR <br> MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ DIVES

Part 1. Previous Dive
minutes
feet
repetitive group designator from Table 18-9
if the dive was a no-decompression dive, or
Table 18-11 if the dive was a decompression dive.

## Part 2. Surface Interval:

Enter the top section of Table 18-10 at the row for the repetitive group designator from Part 1 and move horizontally to the column in which the actual or planned surface interval time lies. Read the final repetitive group designator from the bottom of this column.
$\qquad$ hours $\qquad$ minutes on the surface
$\qquad$ final repetitive group from Table 18-10

## Part 3. Equivalent Single Dive Time for the Repetitive Dive:

Enter the bottom section of Table 18-10 at the row for the maximum depth of the planned repetitive dive. Move horizontally to the column of the final repetitive group designator from Part 2 to find the Residual Nitrogen Time (RNT). Add this RNT to the planned bottom time for the repetitive dive to obtain the equivalent single dive time.
$\qquad$ minutes: RNT
$+$ minutes: planned bottom time
$\qquad$ minutes: equivalent single dive time

## Part 4. Decompression Schedule for the Repetitive Dive:

Locate the row for the depth of the planned repetitive dive in Table 18-9. Move horizontally to the column with bottom time equal to or just greater than the equivalent single dive time and read the surfacing repetitive group for the repetitive dive from the top of the column. If the equivalent single dive time exceeds the no-decompression limit, locate the row for the depth and equivalent single dive time in Table 18-11. Read the required decompression stops and surfacing repetitive group from the columns to the right along this row.
$\qquad$ minutes: equivalent single dive time from Part 3
$\qquad$ feet: depth of the repetitive dive.
$\qquad$ Schedule (depth/bottom time) from Table 18-9 or Table 18-11.
Ensure RNT Exception Rule does not apply.
Figure 18-5. Repetitive Dive Worksheet for MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$.

Table 18-11. MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables.
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw) Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 60 FSW |  |  |  |  |  |  |  |  |  |  |
| 297 | 2:00 |  |  |  |  |  |  | 0 | 2:00 | $z$ |
| 300 | 120 |  |  |  |  |  |  | 1 | 3:00 | $z$ |
| 310 | 120 |  |  |  |  |  |  | 2 | 4:00 | $z$ |
| 320 | 1:20 |  |  |  |  |  |  | 3 | 5:00 | $z$ |
| 330 | 1:20 |  |  |  |  |  |  | 4 | 6:00 | $z$ |
|  |  |  |  |  |  |  |  |  |  |  |
| 340 | 1:20 |  |  |  |  |  |  | 5 | 7:00 |  |
| 350 | 120 |  |  |  |  |  |  | 6 | 8:00 |  |
| 360 | 1:20 |  |  |  |  |  |  | 7 | 9:00 |  |
| 370 | 1:20 |  |  |  |  |  |  | 8 | 10:00 |  |
| 380 | 1:20 |  |  |  |  |  |  | 9 | 11:00 |  |
| 390 | 1:20 |  |  |  |  |  |  | 10 | 12-00 |  |


| 70 FSW |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 130 | 2-20 | 0 | 220 | 0 |
| 140 | 1:40 | 3 | 5:20 | 0 |
| 150 | 1:40 | 6 | 8:20 | 0 |
| 160 | 1:40 | 8 | 10:20 | z |
| 170 | 1:40 | 10 | 12-20 | z |
| 180 | 1:40 | 12 | 14:20 | $z$ |
| 190 | 1:40 | 14 | 16:20 | $z$ |
| 200 | 1:40 | 16 | 18:20 | $z$ |
| 210 | 1:40 | 19 | 21:20 | $z$ |
| 220 | 1:40 | 22 | 24:20 | $z$ |
| 230 | 1:40 | 24 | 26:20 | $z$ |
|  |  |  |  |  |
| 240 | 1:40 | 26 | 28:20 |  |
| 250 | 1:40 | 29 | 31:20 |  |
| 260 | 1:40 | 31 | 33-20 |  |
| 270 | 1:40 | 33 | 35:20 |  |
| 280 | 1:40 | 35 | 37:20 |  |
| 290 | 1:40 | 37 | 39:20 |  |
| 300 | 1:40 | 38 | 40:20 |  |
| 310 | $1: 40$ | 40 | 42:20 |  |
| 320 | 1:40 | 42 | 44:20 |  |
| 340 | 1:40 | 47 | 49:20 |  |
| 350 | 1:40 | 49 | 51:20 |  |

Table 18-11. MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw)Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 80 FSW |  |  |  |  |  |  |  |  |  |  |
| 70 | 2:40 |  |  |  |  |  |  | 0 | 2:40 | L |
| 75 | 2:00 |  |  |  |  |  |  | 2 | 4:40 | L |
| 80 | 2:00 |  |  |  |  |  |  | 4 | 6:40 | M |
| 85 | 2:00 |  |  |  |  |  |  | 5 | 7:40 | M |
| 90 | 2:00 |  |  |  |  |  |  | 6 | 8:40 | N |
| 95 | 2:00 |  |  |  |  |  |  | 7 | 9:40 | N |
| 100 | 2:00 |  |  |  |  |  |  | 9 | 11:40 | N |
| 110 | 2:00 |  |  |  |  |  |  | 12 | 14:40 | 0 |
| 120 | 2:00 |  |  |  |  |  |  | 16 | 18:40 | 0 |
| 130 | 2:00 |  |  |  |  |  |  | 20 | 22:40 | $z$ |
| 140 | 2:00 |  |  |  |  |  |  | 24 | 26:40 | $z$ |
| 150 | 2:00 |  |  |  |  |  |  | 27 | 29:40 | z |
| 160 | 2:00 |  |  |  |  |  |  | 30 | $32 \cdot 40$ | z |
| 170 | 2:00 |  |  |  |  |  |  | 34 | 36:40 | z |
|  |  |  |  |  |  |  |  |  |  |  |
| 180 | 2:00 |  |  |  |  |  |  | 39 | 41:40 |  |
| 180 | 2:00 |  |  |  |  |  |  | 43 | 45:40 |  |
| 200 | 2:00 |  |  |  |  |  |  | 47 | 49:40 |  |
| 210 | 2:00 |  |  |  |  |  |  | 50 | 52:40 |  |
| 220 | 2:00 |  |  |  |  |  |  | 54 | 56:40 |  |
| 230 | 2:00 |  |  |  |  |  |  | 57 | 59:40 |  |
| 240 | 2:00 |  |  |  |  |  |  | 60 | 62:40 |  |
| 250 | 2:00 |  |  |  |  |  |  | 63 | 65:40 |  |
| 280 | 2:00 |  |  |  |  |  |  | 67 | 69:40 |  |
| 270 | 2:00 |  |  |  |  |  |  | 70 | 72:40 |  |
| 280 | 2:00 |  |  |  |  |  |  | 74 | 78:40 |  |
| 290 | 2:00 |  |  |  |  |  |  | 77 | 79:40 |  |
| 300 | 2:00 |  |  |  |  |  |  | 81 | 83:40 |  |
| 310 | 2:00 |  |  |  |  |  |  | 84 | 88:40 |  |
| 320 | 2:00 |  |  |  |  |  |  | 87 | 89:40 |  |

Table 18-11. MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw)Stop times (min) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 90 FSW |  |  |  |  |  |  |  |  |  |  |
| 50 | 3:00 |  |  |  |  |  |  | 0 | 3:00 | K |
| 55 | 220 |  |  |  |  |  |  | 3 | 6:00 | K |
| 60 | $2 \cdot 20$ |  |  |  |  |  |  | 6 | 9:00 | L |
| 65 | 2-20 |  |  |  |  |  |  | 8 | 11:00 | L |
| 70 | 220 |  |  |  |  |  |  | 11 | 14:00 | M |
| 75 | 2-20 |  |  |  |  |  |  | 13 | 18:00 | M |
| 80 | 220 |  |  |  |  |  |  | 14 | 17:00 | N |
| 85 | $2 \cdot 20$ |  |  |  |  |  |  | 16 | 18:00 | N |
| 90 | 2.20 |  |  |  |  |  |  | 18 | 21:00 | 0 |
| 95 | 2-20 |  |  |  |  |  |  | 21 | 24:00 | 0 |
| 100 | 2.20 |  |  |  |  |  |  | 24 | 27:00 | 0 |
| 110 | 2-20 |  |  |  |  |  |  | 30 | 33:00 | 0 |
| 120 | 220 |  |  |  |  |  |  | 35 | 38:00 | z |
| 130 | 2.20 |  |  |  |  |  |  | 40 | 43:00 | z |
|  |  |  |  |  |  |  |  |  |  |  |
| 140 | 2-20 |  |  |  |  |  |  | 45 | 48:00 |  |
| 150 | 2.20 |  |  |  |  |  |  | 51 | 54:00 |  |
| 160 | $2 \cdot 20$ |  |  |  |  |  |  | 57 | 80:00 |  |
| 170 | 2.00 |  |  |  |  |  | 1 | 62 | 85:40 |  |
| 180 | 2:00 |  |  |  |  |  | 2 | 66 | 70:40 |  |
| 190 | 2.00 |  |  |  |  |  | 2 | 71 | 75:40 |  |

## 100 FSW

| 39 | 3:20 |  | 0 | 3:20 | J |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | 2-40 |  | 1 | 4:20 | J |
| 45 | 2-40 |  | 5 | 8:20 | K |
| 50 | 2-40 |  | 9 | 12-20 | L |
| 55 | 2.40 |  | 12 | 15:20 | L |
| 60 | 2-40 |  | 15 | 18:20 | M |
| 65 | $2 \cdot 40$ |  | 18 | 21:20 | M |
| 70 | 2-40 |  | 21 | 24:20 | N |
| 75 | 2.40 |  | 23 | 28:20 | N |
| 80 | 2-40 |  | 28 | 29:20 | 0 |
| 85 | 2-40 |  | 30 | 33:20 | $\bigcirc$ |
| 90 | $2 \cdot 40$ |  | 34 | 37:20 | 0 |
| 95 | 2.20 | 1 | 37 | 41:00 | 0 |
| 100 | 220 | 3 | 39 | 45:00 | 0 |
|  |  |  |  |  |  |
| 110 | 2-20 | 6 | 43 | 52-00 |  |
| 120 | 2-20 | 8 | 47 | 58:00 |  |

Table 18-11. MK 16 MOD $1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 80 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw) Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 110 FSW |  |  |  |  |  |  |  |  |  |  |
| 32 | 3:40 |  |  |  |  |  |  | 0 | 3:40 | J |
| 35 | 3:00 |  |  |  |  |  |  | 3 | 6:40 | J |
| 40 | 3:00 |  |  |  |  |  |  | 8 | 11:40 | K |
| 45 | 3:00 |  |  |  |  |  |  | 13 | 16:40 | L |
| 50 | 3:00 |  |  |  |  |  |  | 17 | 20:40 | L |
| 55 | 3:00 |  |  |  |  |  |  | 21 | 24:40 | M |
| 60 | 3:00 |  |  |  |  |  |  | 25 | 28:40 | M |
| 65 | 3:00 |  |  |  |  |  |  | 28 | 31:40 | N |
| 70 | 2:40 |  |  |  |  |  | 1 | 30 | 34:20 | $\bigcirc$ |
| 75 | 2:40 |  |  |  |  |  | 4 | 32 | 39:20 | 0 |
| 80 | 2:40 |  |  |  |  |  | 7 | 34 | 44:20 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |
| 85 | 2:40 |  |  |  |  |  | 9 | 37 | 49:20 |  |
| 90 | 2.40 |  |  |  |  |  | 11 | 39 | 53:20 |  |
| 95 | 2.40 |  |  |  |  |  | 13 | 42 | 58:20 |  |
| 100 | 2.40 |  |  |  |  |  | 15 | 44 | 62:20 |  |
| 110 | 2:20 |  |  |  |  | 3 | 15 | 49 | 70:00 |  |
| 120 | 2:20 |  |  |  |  | 6 | 15 | 56 | 80:00 |  |

## 120 FSW

| 27 | 4:00 |  |  | 0 | 4:00 | J |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | $3: 20$ |  |  | 4 | 8:00 | J |
| 35 | 3:20 |  |  | 10 | 14:00 | K |
| 40 | 3:20 |  |  | 16 | 20:00 | L |
| 45 | 3:20 |  |  | 21 | 25:00 | L |
| 50 | $3: 20$ |  |  | 26 | 30:00 | M |
| 55 | 3:20 |  |  | 30 | 34:00 | M |
| 60 | 3:00 |  | 4 | 31 | 38:40 | N |
| 65 | 3:00 |  | 8 | 30 | 41:40 | 0 |
|  |  |  |  |  |  |  |
| 70 | 3:00 |  | 12 | 32 | 47:40 |  |
| 75 | 3:00 |  | 15 | 35 | 53:40 |  |
| 80 | $2: 40$ | 3 | 15 | 38 | 59:20 |  |
| 85 | 2.40 | 6 | 15 | 41 | 65:20 |  |
| 90 | 2.40 | 8 | 15 | 44 | 70:20 |  |
| 95 | 2.40 | 10 | 15 | 47 | 75:20 |  |
| 100 | 2:40 | 12 | 15 | 51 | 81:20 |  |

Table 18-11. MK $16 \mathrm{MOD} 1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued). (DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| $\begin{aligned} & \text { Bottom Time } \\ & (\mathrm{min}) \end{aligned}$ | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw) Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 130 FSW |  |  |  |  |  |  |  |  |  |  |
| 23 | 4:20 |  |  |  |  |  |  | 0 | 4:20 | 1 |
| 25 | 3.40 |  |  |  |  |  |  | 2 | $6: 20$ | J |
| 30 | 3:40 |  |  |  |  |  |  | 10 | 14:20 | K |
| 35 | 3:40 |  |  |  |  |  |  | 17 | 21:20 | K |
| 40 | 3:40 |  |  |  |  |  |  | 23 | 27:20 | L |
| 45 | 3:40 |  |  |  |  |  |  | 29 | 33:20 | M |
| 50 | 320 |  |  |  |  |  | 4 | 30 | 38:00 | N |
| 55 | 3:20 |  |  |  |  |  | 9 | 30 | 43:00 | N |
|  |  |  |  |  |  |  |  |  |  |  |
| 60 | 3.20 |  |  |  |  |  | 14 | 30 | 48:00 |  |
| 85 | 3.00 |  |  |  |  | 3 | 15 | 33 | 54:40 |  |
| 70 | 3:00 |  |  |  |  | 7 | 15 | 36 | 61:40 |  |
| 75 | 3:00 |  |  |  |  | 11 | 15 | 39 | 68:40 |  |
| 80 | 3:00 |  |  |  |  | 14 | 15 | 42 | 74.40 |  |

140 FSW

| 21 | 4:40 |  |  |  | 0 | 4:40 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 4:00 |  |  |  | 7 | 11:40 | J |
| 30 | 4:00 |  |  |  | 16 | 20:40 | K |
| 35 | 4:00 |  |  |  | 23 | 27:40 | L |
| 40 | $3: 40$ |  |  | 2 | 29 | 35:20 | L |
| 45 | 3:40 |  |  | 7 | 30 | 41:20 | M |
|  |  |  |  |  |  |  |  |
| 50 | 320 |  | 1 | 12 | 30 | 47:00 |  |
| 55 | 3:20 |  | 4 | 15 | 30 | 53:00 |  |
| 60 | 320 |  | 9 | 15 | 33 | 81:00 |  |
| 65 | 3:20 |  | 13 | 15 | 36 | 68:00 |  |
| 70 | 3:00 | 3 | 15 | 15 | 40 | 76.40 |  |
| 75 | 3:00 | 7 | 15 | 15 | 44 | 84:40 |  |
| 80 | 3:00 | 10 | 15 | 15 | 50 | 93:40 |  |

Table 18-11. MK $16 \mathrm{MOD} 1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued). (DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw)Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 150 FSW |  |  |  |  |  |  |  |  |  |  |
| 17 | 5:00 |  |  |  |  |  |  | 0 | 5:00 | H |
| 20 | 4:20 |  |  |  |  |  |  | 3 | 8:00 | 1 |
| 25 | 4:20 |  |  |  |  |  |  | 13 | 18:00 | J |
| 30 | 4:20 |  |  |  |  |  |  | 22 | 27:00 | K |
| 35 | 4:00 |  |  |  |  |  | 3 | 27 | 34:40 | L |
| 40 | 4:00 |  |  |  |  |  | 8 | 30 | 42:40 | M |
|  |  |  |  |  |  |  |  |  |  |  |
| 45 | 3:40 |  |  |  |  | 4 | 11 | 30 | 49:20 |  |
| 50 | $3: 40$ |  |  |  |  | 7 | 15 | 30 | 56:20 |  |
| 55 | 3:20 |  |  |  | 2 | 11 | 15 | 33 | 65:00 |  |
| 60 | 3:20 |  |  |  | 4 | 14 | 15 | 37 | 74:00 |  |
| 65 | 3:20 |  |  |  | 8 | 15 | 15 | 40 | 82:00 |  |
| 70 | 3:20 |  |  |  | 13 | 15 | 15 | 46 | 93:00 |  |
| 75 | 3:00 |  |  | 2 | 15 | 15 | 15 | 52 | 102:40 |  |
| 80 | 3:00 |  |  | 6 | 15 | 15 | 15 | 59 | 113:40 |  |

160 FSW

|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 5:20 |  |  |  |  |  | 0 | 5:20 | H |
| 20 | 4:40 |  |  |  |  |  | 7 | 12:20 | J |
| 25 | 4:20 |  |  |  |  | 1 | 17 | 23:00 | K |
| 30 | 4:20 |  |  |  |  | 3 | 25 | 33:00 | L |
| 35 | 4:00 |  |  |  | 1 | 8 | 28 | 41:40 | M |
| 40 | 4:00 |  |  |  | 5 | 10 | 30 | 49:40 |  |
| 45 | $3: 40$ |  |  | 2 | 7 | 14 | 30 | 57:20 |  |
| 50 | $3: 40$ |  |  | 5 | 10 | 15 | 33 | 67:20 |  |
| 55 | 3:40 |  |  | 8 | 14 | 15 | 30 | 77:20 |  |
| 60 | $3: 20$ |  | 3 | 10 | 15 | 15 | 41 | 88:00 |  |
| 65 | $3: 20$ |  | 5 | 13 | 15 | 15 | 48 | 100:00 |  |
| 70 | $3: 20$ |  | 8 | 15 | 15 | 15 | 55 | 112:00 |  |
| 75 | $3: 20$ |  | 13 | 15 | 15 | 15 | 61 | 123:00 |  |
| 80 | $3: 00$ | 3 | 15 | 15 | 15 | 15 | 68 | 134:40 |  |

Table 18-11. MK $16 \mathrm{MOD} 1 \mathrm{~N}_{2} \mathrm{O}_{2}$ Decompression Tables (Continued). (DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw) <br> Stop times ( $\mathbf{m i n}$ ) include travel time, except first stop |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 170 FSW |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 13 | 5:40 |  |  |  |  |  |  | 0 | 5:40 | H |
| 15 | 5:00 |  |  |  |  |  |  | 2 | 7:40 | 1 |
| 20 | 5:00 |  |  |  |  |  |  | 12 | 17:40 | J |
| 25 | 4:40 |  |  |  |  |  | 3 | 20 | 28:20 | K |
| 30 | 4:20 |  |  |  |  | 3 | 5 | 28 | 39:00 | L |
| 35 | 4:00 |  |  |  | 1 | 5 | 8 | 30 | 48:40 |  |
| 40 | 4:00 |  |  |  | 4 | 7 | 12 | 30 | 57:40 |  |
| 45 | 4:00 |  |  |  | 8 | 8 | 15 | 32 | 67:40 |  |
| 50 | 3.40 |  |  | 4 | 7 | 13 | 15 | 36 | 79:20 |  |
| 55 | $3: 40$ |  |  | 7 | 9 | 15 | 15 | 41 | 91:20 |  |
| 60 | 320 |  | 2 | 7 | 14 | 15 | 15 | 48 | 105:00 |  |

180 FSW

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 8:00 |  |  |  |  |  |  | 0 | 6:00 | H |
| 15 | 5:20 |  |  |  |  |  |  | 4 | 10:00 | I |
| 20 | 5:00 |  |  |  |  |  | 2 | 14 | 21:40 | K |
| 25 | 4:40 |  |  |  |  | 3 | 3 | 23 | 34:20 | L |
| 30 | 4:20 |  |  |  | 2 | 4 | 7 | 27 | 45:00 |  |
| 35 | 4:00 |  |  | 1 | 3 | 8 | 9 | 30 | 55:40 |  |
| 40 | 4:00 |  |  | 2 | 7 | 8 | 14 | 30 | 65:40 |  |
| 45 | 4:00 |  |  | 6 | 7 | 11 | 15 | 35 | 78:40 |  |
| 50 | 3:40 |  | 2 | 8 | 8 | 15 | 15 | 40 | 92-20 |  |
| 55 | 3:40 |  | 5 | 8 | 12 | 15 | 15 | 48 | 108:20 |  |
| 80 | 320 | 1 | 7 | 9 | 15 | 15 | 15 | 57 | 123:00 |  |

190 FSW

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 6.20 |  |  |  |  |  |  | 0 | 6:20 | G |
| 15 | 5:40 |  |  |  |  |  |  | 6 | 12:20 | J |
| 20 | 5:00 |  |  |  |  | 1 | 4 | 16 | 28:40 | K |
| 25 | 4:40 |  |  |  | 2 | 4 | 4 | 24 | 39.20 | L |
| 30 | 4.20 |  |  | 2 | 3 | 5 | 8 | 29 | 52:00 |  |
| 35 | 4.20 |  |  | 4 | 5 | 8 | 11 | 30 | 63:00 |  |
| 40 | 4:00 |  | 2 | 5 | 8 | 8 | 15 | 34 | 78:40 |  |
| 45 | 4:00 |  | 4 | 8 | 7 | 14 | 15 | 39 | 91:40 |  |
| 50 | 3.40 | 1 | 7 | 8 | 11 | 15 | 15 | 47 | 108:20 |  |
| 55 | 3:40 | 4 | 8 | 8 | 15 | 15 | 15 | 56 | 125:20 |  |
| 60 | 3.40 | 7 | 7 | 13 | 15 | 15 | 15 | 65 | 141:20 |  |

Table 18-12. No Decompression Limits and Repetitive Group Designators for MK 16 MOD 1 HeO ${ }_{2}$ Dives.

| Depth (fsw) | No-Stop Limit | Repetitive Group Designator |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | D | E | F | G | H | 1 | J | K | 1 | M | N | 0 | Z |
| 10 | Unlimited | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 15 | Unlimited | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | Unlimited | 129 | 269 | * |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | Unlimited | 45 | 72 | 106 | 146 | 200 | 278 | 425 | * |  |  |  |  |  |  |  |  |
| 30 | 332 | 27 | 43 | 60 | 78 | 100 | 124 | 152 | 185 | 227 | 281 | 332 |  |  |  |  |  |
| 35 | 190 | 19 | 30 | 41 | 54 | 67 | 81 | 97 | 114 | 133 | 154 | 178 | 190 |  |  |  |  |
| 40 | Unlimited | 122 | 246 | * |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | 325 | 27 | 43 | 59 | 78 | 99 | 123 | 150 | 183 | 223 | 276 | 325 |  |  |  |  |  |
| 60 | 134 | 15 | 23 | 32 | 41 | 51 | 61 | 71 | 83 | 95 | 108 | 123 | 134 |  |  |  |  |
| 70 | 86 | 11 | 16 | 22 | 28 | 34 | 41 | 47 | 54 | 61 | 69 | 77 | 85 | 86 |  |  |  |
| 80 | 63 | 8 | 12 | 17 | 21 | 26 | 30 | 35 | 40 | 45 | 51 | 56 | 62 | 63 |  |  |  |
| 90 | 44 | 6 | 10 | 13 | 17 | 20 | 24 | 28 | 32 | 36 | 40 | 44 |  |  |  |  |  |
| 100 | 31 | 5 | 8 | 11 | 14 | 17 | 20 | 23 | 25 | 30 | 31 |  |  |  |  |  |  |
| 110 | 24 | 4 | 7 | 9 | 12 | 14 | 17 | 20 | 22 | 24 |  |  |  |  |  |  |  |
| 120 | 20 | 4 | 6 | 8 | 10 | 13 | 15 | 17 | 19 | 20 |  |  |  |  |  |  |  |
| 130 | 17 | 3 | 5 | 7 | 9 | 11 | 13 | 15 | 17 |  |  |  |  |  |  |  |  |
| 140 | 15 | 3 | 4 | 6 | 8 | 10 | 12 | 13 | 15 |  |  |  |  |  |  |  |  |
| 150 | 13 | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 |  |  |  |  |  |  |  |  |
| 160 | 12 |  | 3 | 5 | 6 | 8 | 9 | 11 | 12 |  |  |  |  |  |  |  |  |
| 170 | 11 |  | 3 | 4 | 6 | 7 | 9 | 10 | 11 |  |  |  |  |  |  |  |  |
| 180 | 10 |  | 3 | 4 | 5 | 6 | 8 | 9 | 10 |  |  |  |  |  |  |  |  |
| 190 | 9 |  |  | 4 | 5 | 6 | 7 | 8 | 9 |  |  |  |  |  |  |  |  |
| 200 | 8 |  |  |  | 4 | 5 | 7 | 8 |  |  |  |  |  |  |  |  |  |

- Diver does not acquire a repetitive group designator during dives to these depths.
* Highest repetitive group that can be achieved at this depth regardless of bottom time.

Table 18-13. Residual Helium Timetable for MK 16 MOD $1 \mathrm{HeO}_{2}$ Dives.


## REPETITIVE DIVE WORKSHEET FOR MK 16 MOD $1 \mathrm{HeO}_{2}$ DIVES

Part 1. Previous Dive:
minutes
feet
repetitive group designator from Table $18-12$ if
the dive was a no-decompression dive, or from
Table 18-14 if the dive was a decompression
dive.

Part 2. Surface Interval:
Enter the top section of Table 18-13 at the row for the repetitive group designator from Part 1 and move horizontally to the right to the column in which the time equal to or just greater than the actual or planned surface interval time lies. Read the final repetitive group designator from the bottom of this column.
$\qquad$ hours $\qquad$ minutes on the surface
___ final repetitive group from Table 18-13

Part 3. Equivalent Single Dive Time for the Repetitive Dive:
Enter the bottom section of Table 18-13 at the row for the maximum depth of the planned repetitive dive. Move horizontally to the right to the column of the final repetitive group designator from Part 2 to find the Residual Helium Time (RHT). Add this RHT to the planned bottom time for the repetitive dive to obtain the equivalent single dive time.
$\qquad$ minutes: RHT
$\qquad$ minutes: planned bottom time
$=$ $\qquad$ minutes: equivalent single dive time

## Part 4. Decompression Schedule for the Repetitive Dive:

Locate the row for the depth of the planned repetitive dive in Table 18-12. Move horizontally to the right to the column with bottom time equal to or just greater than the equivalent single dive time and read the surfacing repetitive group for the repetitive dive from the top of the column. If the equivalent single dive time exceeds the no-decompression limit, locate the row for the depth and equivalent single dive time in Table 18-14. Read the required decompression stops and surfacing repetitive group from the columns to the right along this row.
$\qquad$ minutes: equivalent single dive time from Part 3
$\qquad$ feet: depth of the repetitive dive
$\qquad$ Schedule (depth/bottom time) from Table 18-12 or Table 18-14

Ensure RHT Exception Rule does not apply.
Figure 18-6. Repetitive Dive Worksheet for MK 16 MOD $1 \mathrm{HeO}_{2}$ Dives.

Table 18-14. MK $16 \mathrm{MOD} 1 \mathrm{HeO}_{2}$ Decompression Tables.
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw)Stop times $(\mathrm{min})$ include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total <br> Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | $(\mathrm{M}: \mathbf{S})$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 30 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 332 | 1:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1:00 |  |
| 340 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 5:00 |  |
| 360 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13 | 14:00 |  |
| 420 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 34 | 35:00 |  |
| 480 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 48 | 49:00 |  |
| 540 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 59 | 60:00 |  |
| 600 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 70 | 71:00 |  |
| 660 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 87 | 88:00 |  |
| 720 | 0:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 101 | 102:00 |  |

35 FSW

| 190 | $1: 10$ | 0 | $1: 10$ |
| :--- | :--- | ---: | ---: |
| 200 | $0: 30$ | 12 | $13: 10$ |
| 210 | $0: 30$ | 23 | $24: 10$ |
| 220 | $0: 30$ | 33 | $34: 10$ |
| 230 | $0: 30$ | 42 | $43: 10$ |
| 240 | $0: 30$ | 50 | $51: 10$ |
| 270 | $0: 30$ | 71 | $72: 10$ |
| 300 | $0: 30$ | 89 | $90: 10$ |
| 330 | $0: 30$ | 103 | $104: 10$ |
| 360 | $0: 30$ | 115 | $116: 10$ |
| 390 | $0: 30$ | 126 | $127: 10$ |
| 420 | $0: 30$ | 145 | $148: 10$ |
| 450 | $0: 30$ | 182 | $183: 10$ |
| 480 | $0: 30$ | 177 | $178: 10$ |

## 50 FSW

| 325 | $1: 40$ | 0 | $1: 40$ | K |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 330 | $1: 00$ | 1 | $2: 40$ | K |
| 340 | $1: 00$ | 2 | $3: 40$ | K |
| 350 | $1: 00$ | 3 | $4: 40$ | K |
| 360 | $1: 00$ | 5 | $6: 40$ | K |
| 420 | $1: 00$ | 11 | $12: 40$ |  |
| 480 | $1: 00$ | 15 | $16: 40$ |  |
| 540 | $1: 00$ | 18 | $19: 40$ |  |
| 600 | $1: 00$ | 21 | $22: 40$ |  |
| 60 | $1: 00$ | 25 | $28: 40$ |  |
| 720 | $1: 00$ | 28 | $30: 40$ |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time $(\mathrm{min})$ | $\begin{gathered} \text { Time } \\ \text { to First } \\ \text { Stop } \\ \text { (M:S) } \end{gathered}$ | DECOMPRESSION STOPS (fsw) <br> Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 60 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 134 | 2.00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2.00 | L |
| 140 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 | 5:00 | L |
| 150 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8 | 10:00 | L |
| 160 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 | 14:00 | L |
| 170 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 16 | 18:00 | L |
| 180 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 20 | 22.00 |  |
| 190 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 24 | 26:00 |  |
| 200 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 27 | 29:00 |  |
| 210 | $1: 20$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 31 | 33-00 |  |
| 220 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 34 | 36:00 |  |
| 230 | $1: 20$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 37 | 39-00 |  |
| 240 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 40 | 42:00 |  |
| 250 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 42 | 44:00 |  |
| 260 | 1:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 | 47-00 |  |
| 270 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 47 | 49:00 |  |
| 280 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 49 | 51:00 |  |
| 290 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 51 | 53-00 |  |
| 300 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 53 | 55:00 |  |
| 310 | 1:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 55 | 57-00 |  |
| 320 | 1220 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 57 | 59:00 |  |
| 330 | 120 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 59 | 61:00 |  |
| 340 | 1:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 61 | 63:00 |  |
| 350 | 1220 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 64 | 68:00 |  |
| 380 | 1:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 66 | 88:00 |  |

## 70 FSW

| 86 | $2: 20$ | 0 | $2: 20$ | $M$ |
| :--- | :--- | :--- | ---: | :---: | :---: |
| 90 | $1: 40$ | 3 | $5: 20$ | $M$ |
| 95 | $1: 40$ | 8 | $10: 20$ |  |
| 100 | $1: 40$ | 12 | $14: 20$ |  |
| 110 | $1: 40$ | 19 | $21: 20$ |  |
| 120 | $1: 40$ | 28 | $28: 20$ |  |
| 130 | $1: 40$ | 33 | $35: 20$ |  |
| 140 | $1: 40$ | 39 | $41: 20$ |  |
| 150 | $1: 40$ | 45 | $47: 20$ |  |
| 160 | $1: 40$ | 50 | $52: 20$ |  |
| 170 | $1: 40$ | 55 | $57: 20$ |  |
| 180 | $1: 40$ | 60 | $62: 20$ |  |
| 180 | $1: 40$ | 64 | 6620 |  |
| 200 | $1: 40$ | 68 | $70: 20$ |  |
| 210 | $1: 40$ | 72 | $74: 20$ |  |
| 220 | $1: 40$ | 78 | $78: 20$ |  |

Table 18-14. MK $16 \mathrm{MOD} 1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min) | Time to First Stop (M:S) | DECOMPRESSION STOPS (fsw) <br> Stop times ( $\mathbf{m i n}$ ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 80 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 63 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2:40 | M |
| 65 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 4:40 | M |
| 70 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8 | 10:40 |  |
| 75 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 14 | 16:40 |  |
| 80 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 19 | 21:40 |  |
| 85 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 24 | 26:40 |  |
| 90 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 29 | $31: 40$ |  |
| 95 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 34 | 38:40 |  |
| 100 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 39 | 41:40 |  |
| 110 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 48 | 50:40 |  |
| 120 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 56 | 58:40 |  |
| 130 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 63 | 65:40 |  |
| 140 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 70 | 72:40 |  |
| 150 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 76 | 78:40 |  |
| 160 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 82 | 84:40 |  |
| 170 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 88 | 90:40 |  |
| 180 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 93 | 95:40 |  |
| 190 | 2:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 98 | 100:40 |  |

## 90 FSW

| 44 | 3:00 | 0 | 3:00 | K |
| :---: | :---: | :---: | :---: | :---: |
| 45 | 2.20 | 1 | 4:00 | K |
| 50 | $2: 20$ | 2 | 5:00 | L |
| 55 | 2:20 | 7 | 10:00 | M |
| 60 | 2:20 | 15 | 18:00 |  |
| 65 | 2:20 | 22 | 25:00 |  |
| 70 | 2:20 | 29 | 32:00 |  |
| 75 | 2:20 | 35 | 38:00 |  |
| 80 | 2:20 | 41 | 44:00 |  |
| 85 | 2:20 | 47 | 50:00 |  |
| 90 | 2:20 | 53 | 56:00 |  |
| 95 | 2:20 | 58 | 61:00 |  |
| 100 | 2:20 | 63 | 68:00 |  |
| 110 | 2:20 | 73 | 78:00 |  |
| 120 | 2:20 | 82 | 85:00 |  |
| 130 | 2:20 | 90 | 93:00 |  |
| 140 | 2:20 | 97 | 100:00 |  |
| 150 | 2:20 | 105 | 108:00 |  |
| 180 | 2:20 | 112 | 115:00 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw)Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | $(\mathrm{M}: \mathrm{S})$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 100 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | 3:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 3:20 | J |
| 35 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 5-20 | K |
| 40 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 7:20 | L |
| 45 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 9:20 | M |
| 50 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 16 | 19:20 |  |
| 55 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 24 | 27-20 |  |
| 60 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 33 | 36:20 |  |
| 65 | $2 \cdot 40$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 41 | 44:20 |  |
| 70 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 48 | 51:20 |  |
| 75 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 55 | 58-20 |  |
| 80 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 62 | 65-20 |  |
| 85 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 68 | 71:20 |  |
| 90 | 2-40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 74 | 77.20 |  |
| 95 | 2-40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 80 | 83-20 |  |
| 100 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 85 | 88:20 |  |
| 110 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 96 | 99.20 |  |
| 120 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 105 | 108:20 |  |
| 130 | 2:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 114 | 118:00 |  |
| 140 | $2 \cdot 20$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 124 | 128:00 |  |

110 FSW

| 24 | 3.40 |  |  | 0 | 3:40 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 3:00 |  |  | 1 | 4:40 | 1 |
| 30 | 3:00 |  |  | 4 | 7:40 | J |
| 35 | 3:00 |  |  | 7 | 10:40 | L |
| 40 | 3:00 |  |  | 10 | 13:40 | M |
| 45 | 3.00 |  |  | 21 | 24:40 |  |
| 50 | 3-00 |  |  | 31 | 34:40 |  |
| 55 | 3:00 |  |  | 40 | 43:40 |  |
| 60 | 2.40 |  | 1 | 48 | 53-20 |  |
| 65 | 2.40 |  | 2 | 57 | 62:20 |  |
| 70 | 2-40 |  | 3 | 64 | 70-20 |  |
| 75 | 2.40 |  | 4 | 71 | 78:20 |  |
| 80 | 2.40 |  | 5 | 77 | 85:20 |  |
| 85 | 2-40 |  | 5 | 84 | 92:20 |  |
| 90 | 2.40 |  | 6 | 89 | 98:20 |  |
| 95 | 2.40 |  | 6 | 95 | 104:20 |  |
| 100 | 2.40 |  | 6 | 101 | 110-20 |  |
| 110 | 2.40 |  | 7 | 112 | 122-20 |  |
|  |  |  |  |  |  |  |
| 120 | 2:40 |  | 7 | 123 | 133:20 |  |
| 130 | 2-40 |  | 7 | 136 | 146:20 |  |
| 140 | 2:20 | 1 | 7 | 149 | 180-00 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw) <br> Stop times (min) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $(\min )$ | $(M: S)$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 120 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 4:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 4:00 | 1 |
| 25 | 3:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 8:00 | $J$ |
| 30 | 3:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8 | 12:00 | K |
| 35 | 3:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 | 16:00 | M |
| 40 | 3:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 23 | 27:00 |  |
| 45 | 3:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 34 | 39:40 |  |
| 50 | 3:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 43 | 50:40 |  |
| 55 | 3:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 52 | 61:40 |  |
| 60 | 3:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 60 | 70:40 |  |
| 65 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 7 | 68 | 80:20 |  |
| 70 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 | 7 | 76 | 89:20 |  |
| 75 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 | 8 | 83 | 97:20 |  |
| 80 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 7 | 91 | 105:20 |  |
| 85 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 7 | 97 | 112:20 |  |
| 90 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 8 | 103 | 119:20 |  |
| 95 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 7 | 110 | 128:20 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 7 | 117 | 133:20 |  |
| 110 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 7 | 131 | 148:20 |  |
| 120 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 7 | 145 | 162:20 |  |

## 130 FSW

| 17 | 4:20 |  |  |  | 0 | 4:20 | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 3:40 |  |  |  | 3 | 7:20 | 1 |
| 25 | 3:40 |  |  |  | 8 | 12:20 | K |
| 30 | 3:40 |  |  |  | 13 | 17:20 | L |
| 35 | 3:20 |  |  | 2 | 21 | 27:00 | L |
| 40 | 3:20 |  |  | 5 | 32 | 41:00 | L |
| 45 | 3:00 |  | 1 | 7 | 43 | 54:40 | L |
| 50 | 3:00 |  | 3 | 7 | 53 | 68:40 |  |
| 55 | 3:00 |  | 5 | 7 | 63 | 78:40 |  |
| 60 | 3:00 |  | 6 | 8 | 71 | 88:40 |  |
| 65 | 2:40 | 1 | 7 | 7 | 81 | 99:20 |  |
| 70 | 2:40 | 2 | 7 | 7 | 89 | 108:20 |  |
| 75 | 2.40 | 3 | 7 | 7 | 97 | 117:20 |  |
| 80 | 2:40 | 3 | 8 | 7 | 104 | 125:20 |  |
| 85 | 2:40 | 4 | 8 | 7 | 111 | 133:20 |  |
| EXCEPTIONAL EXPOSURE |  |  |  |  |  |  |  |
| 90 | 2:40 | 5 | 7 | 7 | 119 | 141:20 |  |
| 95 | 2:40 | 5 | 8 | 7 | 127 | 150:20 |  |
| 100 | 2:40 | 6 | 7 | 7 | 136 | 159:20 |  |
| 110 | 2:40 | 6 | 8 | 7 | 152 | 176:20 |  |
| 120 | 2:40 | 7 | 7 | 18 | 159 | 194:20 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 80 FPM-ASCENT RATE 30 FPM)


150 FSW

| 13 | 5:00 |  |  |  |  |  | 0 | 5:00 | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 4:20 |  |  |  |  |  | 3 | 8-00 | H |
| 20 | 4:20 |  |  |  |  |  | 10 | 15:00 | J |
| 25 | 4:00 |  |  |  |  | 2 | 14 | 20-40 | L |
| 30 | 4:00 |  |  |  |  | 7 | 24 | 35:40 | L |
| 35 | 3:40 |  |  |  | 4 | 8 | 37 | 53:20 | L |
| 40 | 3:20 |  |  | 1 | 7 | 8 | 50 | 70:00 |  |
| 45 | 3:20 |  |  | 4 | 8 | 7 | 63 | 86:00 |  |
| 50 | 3:20 |  |  | 7 | 7 | 8 | 74 | 100:00 |  |
| 55 | 3:00 |  | 2 | 8 | 7 | 7 | 88 | 113:40 |  |
| 60 | 3:00 |  | 4 | 8 | 7 | 7 | 98 | 125:40 |  |
| 65 | 3:00 |  | 6 | 7 | 7 | 8 | 105 | 136:40 |  |
| 70 | 3:00 |  | 7 | 7 | 8 | 7 | 114 | 146:40 |  |
|  |  |  |  |  |  |  |  |  |  |
| 75 | 2:40 | 1 | 8 | 7 | 7 | 8 | 124 | 158-20 |  |
| 80 | 2-40 | 2 | 8 | 7 | 7 | 8 | 135 | 170-20 |  |
| 85 | 2:40 | 3 | 7 | 8 | 7 | 7 | 146 | 181-20 |  |
| 90 | 2-40 | 4 | 7 | 7 | 8 | 9 | 155 | 193-20 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM )

| Bottom | Time to First | DECOMPRESSION STOPS (fsw) Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | (M:S) | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 160 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 5:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 5:20 | H |
| 15 | 4:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 10:20 | 1 |
| 20 | 4:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 13 | 18:20 | K |
| 25 | 4:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 16 | 27:00 | M |
| 30 | 4:00 |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 8 | 31 | 47:40 |  |
| 35 | 3:40 |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 7 | 8 | 46 | 67:20 |  |
| 40 | 3:40 |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 8 | 7 | 80 | 85:20 |  |
| 45 | 3:20 |  |  |  |  |  |  |  |  |  |  |  | 3 | 7 | 7 | 8 | 73 | 102:00 |  |
| 50 | 3:20 |  |  |  |  |  |  |  |  |  |  |  | 6 | 7 | 7 | 8 | 85 | 117:00 |  |
| 55 | 3:00 |  |  |  |  |  |  |  |  |  |  | 1 | 7 | 8 | 7 | 7 | 97 | 130:40 |  |
| 60 | 3:00 |  |  |  |  |  |  |  |  |  |  | 3 | 7 | 8 | 7 | 8 | 107 | 143:40 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 65 | 3:00 |  |  |  |  |  |  |  |  |  |  | 5 | 7 | 8 | 7 | 7 | 118 | 155:40 |  |
| 70 | 3:00 |  |  |  |  |  |  |  |  |  |  | 6 | 8 | 7 | 7 | 8 | 130 | 169:40 |  |
| 75 | 3:00 |  |  |  |  |  |  |  |  |  |  | 8 | 7 | 7 | 8 | 7 | 142 | 182:40 |  |
| 80 | 2:40 |  |  |  |  |  |  |  |  |  | 2 | 7 | 7 | 8 | 7 | 7 | 154 | 195:20 |  |
| 85 | 2:40 |  |  |  |  |  |  |  |  |  | 2 | 8 | 7 | 8 | 7 | 16 | 158 | 209:20 |  |
| 90 | 2:40 |  |  |  |  |  |  |  |  |  | 3 | 8 | 7 | 7 | 8 | 25 | 161 | 222:20 |  |

## 170 FSW

| 11 | 5:40 |  |  |  |  |  |  |  | 0 | 5:40 | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 5:00 |  |  |  |  |  |  |  | 8 | 13:40 | I |
| 20 | 4:40 |  |  |  |  |  |  | 2 | 15 | 22:20 | K |
| 25 | 4:20 |  |  |  |  |  | 2 | 8 | 22 | 37:00 | L |
| 30 | 4:00 |  |  |  |  | 2 | 7 | 7 | 39 | 59:40 | L |
| 35 | 4:00 |  |  |  |  | 7 | 7 | 8 | 55 | 81:40 |  |
| 40 | $3: 40$ |  |  |  | 4 | 8 | 7 | 7 | 70 | 100:20 |  |
| 45 | 3:20 |  |  | 1 | 7 | 8 | 7 | 7 | 84 | 118:00 |  |
| 50 | $3: 20$ |  |  | 4 | 7 | 8 | 7 | 8 | 96 | 134:00 |  |
| 55 | $3: 20$ |  |  | 7 | 7 | 7 | 8 | 7 | 108 | 148:00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | 3:00 |  | 2 | 7 | 8 | 7 | 7 | 8 | 120 | 162:40 |  |
| 65 | 3:00 |  | 4 | 7 | 8 | 7 | 7 | 8 | 134 | 178:40 |  |
| 70 | 3:00 |  | 5 | 8 | 7 | 8 | 7 | 7 | 148 | 193:40 |  |
| 75 | 3:00 |  | 7 | 7 | 8 | 7 | 7 | 12 | 157 | 208:40 |  |
| 80 | 2:40 | 1 | 7 | 8 | 7 | 7 | 8 | 22 | 160 | 223:20 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM -ASCENT RATE 30 FPM )

| Bottom | $\begin{gathered} \text { Time } \\ \text { to First } \end{gathered}$ | DECOMPRESSION STOPS (fsw)Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $(\mathrm{min})$ | (M:S) | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 180 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 6.00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 6:00 | H |
| 15 | 5:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 11 | 17:00 | $J$ |
| 20 | 5:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 14 | 25:40 | L |
| 25 | 4:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 8 | 29 | 48:20 | L |
| 30 | 4.20 |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 7 | 8 | 47 | 73:00 |  |
| 35 | 4:00 |  |  |  |  |  |  |  |  |  |  |  | 4 | 8 | 7 | 8 | 64 | 95:40 |  |
| 40 | 3:40 |  |  |  |  |  |  |  |  |  |  | 2 | 8 | 7 | 7 | 8 | 80 | 116-20 |  |
| 45 | 3:40 |  |  |  |  |  |  |  |  |  |  | 6 | 8 | 7 | 7 | 8 | 94 | 134:20 |  |
| 50 | 3:20 |  |  |  |  |  |  |  |  |  | 3 | 7 | 7 | 8 | 7 | 7 | 108 | 151:00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | 3:20 |  |  |  |  |  |  |  |  |  | 5 | 8 | 7 | 8 | 7 | 7 | 121 | 167-00 |  |
| 60 | 3:00 |  |  |  |  |  |  |  |  | 1 | 7 | 8 | 7 | 7 | 8 | 7 | 136 | 184:40 |  |
| 65 | 3:00 |  |  |  |  |  |  |  |  | 3 | 7 | 8 | 7 | 7 | 8 | 7 | 151 | 201:40 |  |
| 70 | 3:00 |  |  |  |  |  |  |  |  | 5 | 7 | 7 | 8 | 7 | 7 | 16 | 158 | 218-40 |  |

## 190 FSW

| 9 | 6:20 |  |  |  |  |  |  |  |  |  |  | 0 | 6-20 | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 5:40 |  |  |  |  |  |  |  |  |  |  | 2 | $8: 20$ | H |
| 15 | 5:40 |  |  |  |  |  |  |  |  |  |  | 14 | 20-20 | J |
| 20 | 4:40 |  |  |  |  |  |  |  | 1 | 1 | 8 | 16 | 31:20 | M |
| 25 | 3:20 |  |  |  | 1 | 0 | 0 | 0 | 4 | 7 | 7 | 38 | 61:00 |  |
| 30 | 3.00 |  |  | 1 | 0 | 0 | 2 | 2 | 7 | 7 | 8 | 57 | 87:40 |  |
| 35 | 2.40 |  | 1 | 0 | 0 | 2 | 0 | 8 | 7 | 8 | 7 | 75 | 111:20 |  |
| 40 | 220 | 1 | 0 | 0 | 0 | 2 | 6 | 8 | 7 | 7 | 8 | 91 | 133:00 |  |
| 45 | 2.20 | 1 | 0 | 0 | 0 | 5 | 7 | 8 | 7 | 7 | 8 | 105 | 151:00 |  |
| 50 | 2:20 | 1 | 0 | 0 | 0 | 8 | 8 | 7 | 8 | 7 | 7 | 120 | 169-00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | $2: 20$ | 1 | 0 | 0 | 4 | 8 | 7 | 7 | 8 | 7 | 7 | 138 | 190-00 |  |
| 60 | 2.20 | 1 | 0 | 0 | 7 | 7 | 8 | 7 | 7 | 8 | 7 | 153 | 208-00 |  |
| 65 | 2.20 | 1 | 0 | 2 | 7 | 7 | 8 | 7 | 7 | 8 | 19 | 159 | 228:00 |  |
| 70 | 2:20 | 1 | 0 | 3 | 8 | 7 | 8 | 7 | 7 | 8 | 31 | 164 | 247-00 |  |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw) Stop times (min) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (min) | $(\mathrm{M}: \mathrm{S})$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 200 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | 6:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 6:40 | G |
| 10 | 6:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 11:40 | H |
| 15 | 5:20 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 1 | 15 | 23:00 | K |
| 20 | 3:20 |  |  |  |  |  |  |  | 1 | 0 | 0 | 2 | 0 | 0 | 5 | 7 | 25 | 44:00 | L |
| 25 | 2:00 |  |  |  | 1 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 1 | 7 | 7 | 7 | 47 | 75:40 | L |
| 30 | 1:20 |  | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 1 | 7 | 7 | 8 | 7 | 69 | 108:00 |  |
| 35 | 1:20 |  | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 7 | 7 | 7 | 8 | 7 | 87 | 130:00 |  |
| 40 | 1:00 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 5 | 8 | 7 | 7 | 8 | 7 | 104 | 152:40 |  |
| 45 | 1:00 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 2 | 7 | 8 | 7 | 8 | 7 | 7 | 120 | 172:40 |  |
| EXCEPTIONAL EXPOSURE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | 1:00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 6 | 7 | 7 | 8 | 7 | 8 | 7 | 139 | 195:40 |  |
| 55 | 1:00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 2 | 8 | 7 | 7 | 8 | 7 | 8 | 8 | 155 | 215:40 |  |
| 60 | 1:00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 5 | 7 | 8 | 7 | 7 | 8 | 7 | 22 | 161 | 237:40 |  |

210 FSW

| 5 | 7:00 |  |  |  |  |  |  |  |  |  |  | 0 | 7:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 6:20 |  |  |  |  |  |  |  |  |  |  | 5 | 12:00 |
| 15 | 6:00 |  |  |  |  |  |  |  |  |  | 7 | 5 | 18:40 |
| 20 | 5:00 |  |  |  |  |  |  | 5 | 3 | 2 | 2 | 28 | 45:40 |
| 25 | 4:20 |  |  |  |  | 3 | 3 | 3 | 2 | 3 | 3 | 57 | 79:00 |
| 30 | 4:20 |  |  |  |  | 6 | 3 | 2 | 2 | 6 | 12 | 76 | 112:00 |
| 35 | 3:40 |  |  | 3 | 3 | 3 | 2 | 3 | 5 | 12 | 12 | 95 | 142:20 |
| 40 | 3:20 |  | 3 | 2 | 3 | 2 | 3 | 5 | 12 | 11 | 12 | 113 | 170:00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 3:20 |  | 4 | 2 | 3 | 2 | 4 | 11 | 12 | 12 | 11 | 131 | 196:00 |
| 50 | 3:20 |  | 4 | 3 | 2 | 3 | 10 | 11 | 12 | 12 | 11 | 149 | 221:00 |
| 55 | 3:00 | 3 | 2 | 3 | 2 | 7 | 11 | 11 | 12 | 11 | 12 | 185 | 242:40 |
| 60 | 3:20 |  | 5 | 3 | 2 | 11 | 12 | 11 | 11 | 12 | 21 | 173 | 285:00 |

Table 18-14. MK 16 MOD $1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 80 FPM-ASCENT RATE 30 FPM)

| Bottom | $\begin{gathered} \text { Time } \\ \text { to First } \end{gathered}$ | DECOMPRESSION STOPS (fsw)Stop times (min) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Time } \\ & (\mathrm{min}) \end{aligned}$ | $\begin{aligned} & \text { Stop } \\ & \text { (M:S) } \end{aligned}$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 220 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 7:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 7.20 |  |
| 10 | 6.40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 12:20 |  |
| 15 | 5-40 |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 3 | 2 | 6 | 21:20 |  |
| 20 | 5.00 |  |  |  |  |  |  |  |  |  |  | 4 | 3 | 2 | 3 | 2 | 37 | 56.40 |  |
| 25 | 5:00 |  |  |  |  |  |  |  |  |  |  | 7 | 3 | 3 | 2 | 8 | 65 | 93.40 |  |
| 30 | 4:00 |  |  |  |  |  |  |  | 3 | 3 | 2 | 3 | 3 | 3 | 10 | 12 | 84 | 127:40 |  |
| 35 | $4: 20$ |  |  |  |  |  |  |  |  | 8 | 2 | 3 | 2 | 12 | 12 | 11 | 106 | 161:00 |  |
| 40 | 4:20 |  |  |  |  |  |  |  |  | 9 | 3 | 2 | 12 | 11 | 12 | 11 | 126 | 191:00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 3:40 |  |  |  |  |  |  | 6 | 2 | 3 | 2 | 10 | 12 | 11 | 12 | 11 | 144 | 217:20 |  |
| 50 | 4:00 |  |  |  |  |  |  |  | 8 | 3 | 8 | 11 | 12 | 11 | 11 | 12 | 164 | 244:40 |  |
| 55 | 4:00 |  |  |  |  |  |  |  | 9 | 4 | 12 | 11 | 12 | 11 | 11 | 18 | 177 | 269:40 |  |

230 FSW

| 5 | 7:40 |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 7:40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 7:00 |  |  |  |  |  |  |  |  |  |  |  |  | 6 | 13:40 |
| 15 | 6.00 |  |  |  |  |  |  |  |  |  | 5 | 3 | 2 | 9 | 25:40 |
| 20 | 5-00 |  |  |  |  |  |  | 3 | 3 | 2 | 3 | 3 | 2 | 48 | 67-40 |
| 25 | 4:40 |  |  |  |  |  | 5 | 2 | 3 | 3 | 2 | 3 | 12 | 71 | 106:20 |
| 30 | 4:00 |  |  |  | 3 | 3 | 2 | 3 | 2 | 3 | 6 | 12 | 12 | 93 | 143:40 |
| 35 | 4:00 |  |  |  | 5 | 3 | 2 | 3 | 2 | 8 | 12 | 12 | 11 | 116 | 178:40 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 3:20 |  | 2 | 3 | 2 | 3 | 2 | 3 | 8 | 12 | 11 | 12 | 11 | 137 | 210:00 |
| 45 | 4:00 |  |  |  | 8 | 2 | 3 | 7 | 12 | 11 | 11 | 12 | 11 | 159 | 240.40 |
| 50 | 3:20 |  | 4 | 3 | 2 | 3 | 5 | 11 | 13 | 11 | 11 | 11 | 16 | 174 | 288:00 |
| 55 | 3:00 | 2 | 3 | 2 | 4 | 2 | 12 | 11 | 11 | 11 | 11 | 11 | 38 | 172 | 293:40 |

240 FSW

| 5 | 8:00 |  |  |  |  |  |  |  |  |  |  |  | 0 | 8:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 7:20 |  |  |  |  |  |  |  |  |  |  |  | 8 | 16:00 |
| 15 | 6:00 |  |  |  |  |  |  |  | 4 | 3 | 2 | 4 | 15 | 34.40 |
| 20 | 5:20 |  |  |  |  |  | 5 | 2 | 3 | 2 | 3 | 3 | 54 | 78:00 |
| 25 | $5 \cdot 20$ |  |  |  |  |  | 9 | 3 | 2 | 2 | 8 | 12 | 80 | 122:00 |
| 30 | 4:20 |  |  | 5 | 3 | 2 | 2 | 3 | 3 | 11 | 12 | 12 | 103 | 161:00 |
| 35 | 4:20 |  |  | 7 | 3 | 2 | 3 | 4 | 12 | 11 | 12 | 12 | 127 | 198:00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 4:20 |  |  | 8 | 3 | 3 | 4 | 12 | 12 | 11 | 12 | 12 | 150 | 232:00 |
| 45 | 4:20 |  |  | 10 | 2 | 4 | 12 | 12 | 11 | 12 | 11 | 12 | 173 | 264:00 |
| 50 | $3: 40$ | 6 | 3 | 2 | 3 | 12 | 11 | 11 | 12 | 11 | 11 | 32 | 174 | 292:20 |

Table 18-14. MK $16 \mathrm{MOD} 1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw)Stop times (min) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $(\mathrm{M}: \mathrm{S})$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 250 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 8:20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 8:20 |  |
| 10 | 7:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9 | 17:20 |  |
| 15 | 6:20 |  |  |  |  |  |  |  |  |  |  |  | 5 | 3 | 3 | 2 | 24 | 44:00 |  |
| 20 | 5:40 |  |  |  |  |  |  |  |  |  | 6 | 3 | 2 | 3 | 3 | 6 | 61 | 90:20 |  |
| 25 | 5:00 |  |  |  |  |  |  |  | 6 | 3 | 2 | 2 | 3 | 3 | 12 | 12 | 87 | 135:40 |  |
| 30 | 4:20 |  |  |  |  |  | 4 | 3 | 3 | 2 | 3 | 2 | 8 | 11 | 12 | 12 | 112 | 177:00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 4:40 |  |  |  |  |  |  | 9 | 2 | 3 | 2 | 10 | 12 | 12 | 11 | 12 | 139 | 217:20 |  |
| 40 | 4:20 |  |  |  |  |  | 8 | 3 | 2 | 3 | 11 | 12 | 11 | 11 | 12 | 11 | 164 | 253:00 |  |
| 45 | 4:00 |  |  |  |  | 7 | 3 | 3 | 2 | 11 | 11 | 12 | 11 | 11 | 12 | 25 | 175 | 287:40 |  |
| 50 | 3:40 |  |  |  | 6 | 2 | 3 | 3 | 9 | 12 | 11 | 11 | 12 | 11 | 11 | 49 | 175 | 319:20 |  |

## 260 FSW

| 5 | 8:40 |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 8:40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8:00 |  |  |  |  |  |  |  |  |  |  |  |  | 11 | 19:40 |
| 15 | 6:20 |  |  |  |  |  |  |  | 4 | 3 | 3 | 2 | 3 | 31 | 53:00 |
| 20 | 5:40 |  |  |  |  |  | 5 | 3 | 3 | 2 | 3 | 3 | 10 | 67 | 102:20 |
| 25 | 5:20 |  |  |  |  | 8 | 3 | 2 | 2 | 3 | 7 | 13 | 12 | 96 | 152:00 |
| 30 | 4:40 |  |  | 6 | 3 | 2 | 3 | 2 | 3 | 12 | 12 | 13 | 11 | 123 | 195:20 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 4:40 |  |  | 8 | 3 | 3 | 2 | 6 | 12 | 12 | 11 | 12 | 11 | 151 | 238:20 |
| 40 | $4: 20$ |  | 8 | 3 | 2 | 3 | 7 | 12 | 12 | 11 | 11 | 12 | 14 | 175 | 275:00 |
| 45 | 4:00 | 7 | 3 | 2 | 3 | 8 | 12 | 11 | 11 | 11 | 12 | 11 | 42 | 173 | 310:40 |

## 270 FSW

| 5 | 8:20 |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 14:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8:20 |  |  |  |  |  |  |  |  |  |  |  |  | 13 | 22:00 |
| 15 | 6:20 |  |  |  |  |  |  | 3 | 3 | 3 | 2 | 3 | 3 | 39 | 63:00 |
| 20 | 6:20 |  |  |  |  |  |  | 9 | 3 | 2 | 3 | 5 | 12 | 75 | 116:00 |
| 25 | 5:40 |  |  |  |  | 9 | 3 | 2 | 3 | 3 | 12 | 11 | 12 | 105 | 188:20 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 5:00 |  |  | 8 | 3 | 2 | 3 | 2 | 9 | 11 | 12 | 11 | 12 | 134 | 212:40 |
| 35 | 4:40 |  | 8 | 3 | 2 | 3 | 3 | 11 | 12 | 12 | 11 | 11 | 12 | 183 | 250:20 |
| 40 | 4:20 | 8 | 3 | 3 | 1 | 5 | 12 | 12 | 11 | 11 | 11 | 12 | 30 | 174 | 298:00 |
| 45 | 4:20 | 9 | 3 | 2 | 5 | 12 | 13 | 10 | 11 | 11 | 12 | 11 | 56 | 176 | 336:00 |

Table 18-14. MK $16 \mathrm{MOD} 1 \mathrm{HeO}_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First | DECOMPRESSION STOPS (fsw) Stop times ( min ) include travel time, except first stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Ascent Time (M:S) | Repet Group |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $(\mathrm{M}: \mathrm{S})$ | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |  |
| 280 FSW |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 8:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 14:20 |  |
| 10 | 8:40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 14 | 23-20 |  |
| 15 | 7:00 |  |  |  |  |  |  |  |  |  |  | 7 | 3 | 2 | 3 | 3 | 47 | 72:40 |  |
| 20 | 6.20 |  |  |  |  |  |  |  |  | 9 | 2 | 3 | 2 | 3 | 9 | 12 | 82 | 129:00 |  |
| 25 | 5:20 |  |  |  |  |  | 6 | 3 | 3 | 2 | 3 | 2 | 7 | 12 | 12 | 12 | 114 | 182:00 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | $5 \cdot 20$ |  |  |  |  |  | 10 | 3 | 2 | 3 | 3 | 12 | 12 | 11 | 12 | 12 | 145 | 231:00 |  |
| 35 | 4:40 |  |  |  | 8 | 2 | 3 | 2 | 3 | 8 | 12 | 12 | 11 | 11 | 11 | 13 | 178 | 277:20 |  |
| 40 | 4:40 |  |  |  | 10 | 2 | 3 | 2 | 11 | 12 | 11 | 12 | 12 | 10 | 12 | 45 | 174 | $321: 20$ |  |
| 45 | 4:40 |  |  |  | 11 | 3 | 3 | 11 | 11 | 12 | 11 | 11 | 11 | 12 | 11 | 72 | 178 | 362-20 |  |

## 290 FSW

| 5 | 9:00 |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 14:40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8:00 |  |  |  |  |  |  |  |  |  | 4 | 4 | 2 | 6 | 24:40 |
| 15 | 7:00 |  |  |  |  |  |  | 6 | 3 | 2 | 3 | 3 | 2 | 55 | 81:40 |
| 20 | 6-20 |  |  |  |  | 8 | 2 | 3 | 2 | 3 | 4 | 12 | 12 | 88 | 141:00 |
| 25 | 5:40 |  |  | 8 | 3 | 2 | 3 | 3 | 2 | 12 | 12 | 11 | 12 | 122 | 196:20 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 5:00 | 7 | 3 | 2 | 3 | 3 | 2 | 9 | 12 | 12 | 11 | 11 | 12 | 156 | 248:40 |
| 35 | 5:00 | 10 | 2 | 3 | 2 | 5 | 12 | 11 | 12 | 11 | 11 | 12 | 28 | 178 | 300:40 |
| 40 | 5:00 | 12 | 2 | 3 | 7 | 12 | 11 | 12 | 11 | 11 | 11 | 12 | 59 | 177 | 345:40 |
| 45 | 5:00 | 13 | 3 | 9 | 11 | 12 | 11 | 11 | 11 | 11 | 11 | 18 | 82 | 180 | 388:40 |

## 300 FSW

| 5 | 9:20 |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 15:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8:20 |  |  |  |  |  |  |  |  |  | 6 | 3 | 2 | 9 | 29-00 |
| 15 | 7:00 |  |  |  |  |  | 5 | 3 | 2 | 3 | 2 | 3 | 5 | 61 | 91:40 |
| 20 | 6-20 |  |  |  | 7 | 3 | 2 | 3 | 2 | 4 | 6 | 12 | 12 | 96 | 154:00 |
| 25 | 5.20 | 5 | 3 | 2 | 3 | 3 | 2 | 3 | 7 | 12 | 11 | 12 | 11 | 132 | 212:00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 5:20 | 9 | 3 | 2 | 3 | 2 | 5 | 12 | 12 | 11 | 11 | 12 | 12 | 169 | 269:00 |
| 35 | 5:20 | 12 | 2 | 3 | 2 | 10 | 12 | 11 | 12 | 11 | 11 | 12 | 41 | 176 | 321:00 |
| 40 | 5:20 | 14 | 2 | 4 | 12 | 12 | 11 | 11 | 12 | 11 | 11 | 11 | 74 | 180 | 371:00 |

Table 18-14. MK 16 MOD 1 HeO ${ }_{2}$ Decompression Tables (Continued).
(DESCENT RATE 60 FPM-ASCENT RATE 30 FPM)

| Bottom | Time to First |  |  |  | Stop | time | $\begin{aligned} & \text { DECC } \\ & 5(\mathrm{~min} \end{aligned}$ | OMPR <br> ) incl | ESSI ude tr |  |  |  |  |  |  |  |  | Total Ascent |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time (min) | $\begin{aligned} & \text { Stop } \\ & \text { (M:S) } \end{aligned}$ | 170 | 160 | 150 |  | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 | Time (M:S) | Repet <br> Group |

310 FSW

| 10 | 8:20 |  |  |  |  |  |  |  |  | 5 | 2 | 3 | 3 | 14 | 36:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 7:20 |  |  |  |  |  | 6 | 3 | 3 | 2 | 3 | 2 | 9 | 66 | 102:00 |
| 20 | 6:20 |  |  | 6 | 3 | 2 | 3 | 2 | 3 | 3 | 12 | 11 | 12 | 103 | 167:00 |
| 25 | 6:00 |  | 9 | 3 | 2 | 3 | 3 | 2 | 12 | 11 | 12 | 12 | 11 | 142 | 228:40 |
| 30 | 5:40 | 11 | 3 | 2 | 2 | 3 | 10 | 12 | 11 | 11 | 12 | 12 | 17 | 176 | 288:20 |
| 35 | 5:40 | 14 | 2 | 3 | 6 | 12 | 11 | 12 | 11 | 11 | 11 | 12 | 55 | 178 | 344:20 |
| 40 | 5:40 | 16 | 2 | 10 | 12 | 11 | 12 | 11 | 11 | 11 | 11 | 19 | 83 | 182 | 397:20 |

## 320 FSW

| EXCEPTIONAL EXPOSURE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8:20 |  |  |  |  |  |  |  | 4 | 2 | 3 | 3 | 2 | 21 | 44:00 |
| 15 | 7:40 |  |  |  |  |  | 8 | 3 | 2 | 3 | 2 | 3 | 12 | 71 | 112:20 |
| 20 | 6:20 |  | 6 | 2 | 3 | 2 | 3 | 2 | 4 | 5 | 12 | 12 | 12 | 111 | 181:00 |
| 25 | 6:20 |  | 11 | 3 | 2 | 2 | 3 | 7 | 12 | 11 | 12 | 11 | 12 | 153 | 248:00 |
| 30 | 6:00 | 13 | 2 | 3 | 2 | 6 | 12 | 11 | 12 | 11 | 11 | 12 | 30 | 177 | 308:40 |
| 35 | 6:00 | 15 | 3 | 3 | 11 | 12 | 11 | 12 | 11 | 11 | 11 | 12 | 88 | 182 | 368:40 |
| 40 | 6:00 | 18 | 7 | 11 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 35 | 83 | 185 | 424:40 |

# DECOMPRESSION CHARTS USED IN SURFACE SUPPLIED HELIUMOXYGEN DIVING OPERATIONS 

## HEO2 TABLES

Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table.




Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued). (DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

100
xotxoum
110
120
yano
Max $\mathrm{O}_{2}=26.3 \%$
Min $\mathrm{O}_{2}=14.0 \%$
Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued).
(DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

| Bottom Time (min.) | Time to First Stop (min:sec) | Decompression Stops (fsw) <br> Stop times (min) include travel time, except first $\mathrm{HeO}_{2}$ and first $\mathrm{O}_{2}$ stop |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 190 | 180 | 170 | 160 | 150 | 140 | 130 | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |  |
|  |  | Bottom Mix |  |  |  |  |  |  |  |  |  | $50 \% \mathrm{O}_{2}$ |  |  |  |  |  | $100 \% \mathrm{O}_{2}$ |  |  |
| 10 | 3.00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 | 6 | 8 | 1 |
| 20 | 3.00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 | 12 | 19 | 1 |
| 30 | 3.00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 | 18 | 30 | 2 |
| 40 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 10 | 10 | 22 | 40 | 2 |
| 60 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 10 | 10 | 29 | 52 | 3 |
| 80 | 2.40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 10 | 10 | 33 | 60 | 3 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 10 | 10 | 35 | 64 | 4 |
| 120 | 2:40 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 | 11 | 11 | 35 | 66 | 4 |




## 150 <br> $\mathrm{Max} \mathrm{O}_{2}=23.4 \%$ $\mathrm{Min} \mathrm{O}_{2}=14.0 \%$

160
$\mathrm{Max} \mathrm{O}_{2}=22.2 \%$
$\mathrm{Min} \mathrm{O}_{2}=14.0 \%$
170
$\mathrm{Max} \mathrm{O}_{2}=21.1 \%$
$\mathrm{Min} \mathrm{O}_{2}=14.0 \%$
Table 14-3. Surface-Supplied Hellum-Oxygen Decompression Table (Continued).


Depth (fsw)
180
Max $\mathrm{O}_{2}=20.1 \%$
$\mathrm{Min} \mathrm{O}_{2}=14.0 \%$
190
Max $\mathrm{O}_{2}=19.2 \%$
Min $\mathrm{O}_{2}=14.0 \%$
200
$\mathrm{Max} \mathrm{O}_{2}=18.4 \%$
$\mathrm{Min} \mathrm{O}_{2}=14.0 \%$
210
$\begin{aligned} & \operatorname{Max} \mathrm{O}_{2}=17.7 \% \\ & \operatorname{Min} \mathrm{O}_{2}=10.0 \%\end{aligned}$
Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued).

(msy) uldea
Max $\mathrm{O}_{2}=17.0 \%$
230
Max $\mathrm{O}_{2}=16.3 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
240
Max $\mathrm{O}_{2}=15.7 \%$
Min $\mathrm{O}_{2}=10.0 \%$
250
$\operatorname{Max} \mathrm{O}_{2}=15.2 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued).
(DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)

097
$\operatorname{Max} \mathrm{O}_{2}=14.6 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
270
$\operatorname{Max} \mathrm{O}_{2}=14.2 \%$
$\mathrm{Min} \mathrm{O}_{2}=10.0 \%$

## 280

$\operatorname{Max} \mathrm{O}_{2}=13.7 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
290
$\operatorname{Max} O_{2}=13.3 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
Table 14-3. Surface-Supplied Hellum-Oxygen Decompression Table (Continued).

(msı) uldea
$00 \varepsilon$
$\mathrm{Max} \mathrm{O}_{2}=12.9 \%$
$\mathrm{Min} \mathrm{O}_{2}=10.0 \%$
310
$\operatorname{Max} \mathrm{O}_{2}=12.5 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
320
$\mathrm{Max} \mathrm{O}_{2}=12.2 \%$
Min $\mathrm{O}_{2}=10.0 \%$
330
$\begin{aligned} & M \operatorname{sx} \mathrm{O}_{2}=11.8 \% \\ & \operatorname{Min} \mathrm{O}_{2}=10.0 \%\end{aligned}$
Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued).

$\begin{aligned} & \text { Depth (fsw) } \\ & \mathbf{3 4 0}\end{aligned}$
$\begin{aligned} & M a x \\ & \mathrm{O}_{2}=11.5 \% \\ & \operatorname{Min} \mathrm{O}_{2}=10.0 \%\end{aligned}$

## 350

360
$\mathrm{Max} \mathrm{O}_{2}=10.9 \%$
$\operatorname{Min} \mathrm{O}_{2}=10.0 \%$
Table 14-3. Surface-Supplied Helium-Oxygen Decompression Table (Continued).


380
$\begin{aligned} & M \operatorname{ax} \mathrm{O}_{2}=10.4 \% \\ & \operatorname{Min} \mathrm{O}_{2}=10.0 \%\end{aligned}$
(DESCENT RATE 75 FPM-ASCENT RATE 30 FPM)
$\operatorname{Min} \mathrm{O}_{\mathrm{z}}=10.0 \%$

