NFPA Technical Committee on Lightning Protection

NFPA 780 (A2019 cycle) Second Draft Meeting

AGENDA

Savanah, Georgia

October 15-17, 2018

Item No.	Subject
17-9-1	Call to Order
17-9-2	Introduction of Members and Guests
17-9-3	Approval of Previous Meeting Minutes
17-9-4	Review of Regulations and Committee Actions
17-9-5	Task Group Reports
17-9-6	Processing of Public Comments
17-9-7	Old Business
17-9-8	New Business
17-9-9	Adjournment

Christine T. Porter	RT 8/9/2011	Daniel Ashton	U 04/04/2017
Chair	LIG-AAA		LIG-AAA
Intertek Testing Services		Centurylink	
702 North 86th Street		120 West MLK Drive	
Seattle, WA 98103-3830		San Marcos, TX 78666	
Intertek Testing Services Alternate: Luis M. Bas			
Samuel Barrack	U 10/29/2012	Christopher Batchelor	E 10/28/2008
Principal	LIG-AAA		LIG-AAA
Consolidated Nuclear Security, LLC		US Department of the Navy	
PO Box 2009, MS 8107		Naval Ordnance Safety & Security Activity	
Oak Ridge, TN 37831		Farragutt Hall, Suite 108	
		3817 Strauss Avenue	
		Indian Head, MD 20640-5151	
Matthew Caie	M 1/14/2005	Joanie A. Campbell	E 8/5/2009
Principal	LIG-AAA	Principal	LIG-AAA
Pentair/ERICO, Inc.		US Department of the Air Force	
34600 Solon Road		908 Kristanna Drive	
Solon, OH 44139		Panama City, FL 32405-3278	
Alternate: Brian Liederbach			
Josephine Covino	E 3/21/2006	Ignacio T. Cruz	SE 1/1/1986
Principal	LIG-AAA	Principal	LIG-AAA
US Department of Defense		Cruz Associates, Inc.	
Policy Development Division		955 Harpersville Road, Apt. 2059	
DOD Explosives Safety Board		Newport News, VA 23601-1090	
4800 MARK Center Drive, Suite 16E12			
Alexandria, VA 22350-3606			
Joseph P. DeGregoria	RT 7/14/2004	Chuck Graves	E 04/11/2018
Principal	LIG-AAA	Principal	LIG-AAA
UL LLC		US Federal Aviation Administration	
1285 Walt Whitman Road		Power Services Group/Systems Engineering	Branch
Melville, NY 11747-3085		6201 SW 61st Street	
Alternate: Eric S. Boettcher		Building 260 AJW-222	
		Oklahoma City, OK 73169	
Mitchell Guthrie	SE 1/1/1980	Mark S. Harger	M 7/14/2004
Principal	LIG-AAA	Principal	LIG-AAA
Engineering Consultant		Harger Lightning & Grounding	
234 Guthrie Road		301 Ziegler Drive	
Blanch, NC 27212		Grayslake, IL 60030-1664	
		Alternate: Andrew S. McElroy	

William E. Heary	IM 1/1/1978	Stephen Humeniuk	IM 4/17/2002
Principal	LIG-AAA	Principal	LIG-AAA
Heary Brothers Lightning Protection		Warren Lightning Rod Company	
561 Dill Road		2 Richey Avenue	
Union Springs, NY 13160		Collingswood, NJ 08107	
Alternate: Kenneth P. Heary		United Lightning Protection Association,	Inc.
		Alternate: George Portfleet	
Mark E. Johnson	M 08/17/2017	Carl S. Johnson II	U 3/1/2011
Principal	LIG-AAA	Principal	LIG-AAA
Thomas and Betts		AVCON, Inc.	
815 T&B Boulevard		5555 East Michigan Street, Suite 200	
Memphis, TN 38125		Orlando, FL 32822	
National Electrical Manufacturers Associa	tion		
Bruce A. Kaiser	M 1/1/1990	Simon C. Larter	IM 10/28/2014
Principal	LIG-AAA	Principal	LIG-AAA
Lightning Master Corporation		Dobbyn Lightning Protection	
PO Box 6017		#123 11769 - 40th Street SE	
Clearwater, FL 33758-6017		Calgary, AB T2Z 4M8 Canada	
Alternate: Morris Kline			
David E. McAfee	SE 4/1/1994	Robley B. Melton, Jr.	U 1/1/1989
Principal	LIG-AAA	Principal	LIG-AAA
Lightning & Fire Protection Consultant		CSI Telecommunications	
325 E. Washington Street		5165 South Trimble Road, NE	
Belding, MI 48809		Atlanta, GA 30342-2124	
		Alliance for Telecommunications Industry Alternate: Ernest J. Gallo	y Solutions
Mark P. Morgan		Luke Pettross	M 8/9/2011
Principal	LIG-AAA	Principal	LIG-AAA
East Coast Lightning Equipment, Inc.		Lightning Eliminators & Consultants Inc.	
24 Lanson Drive		6687 Arapahoe Road	
Winsted, CT 06098 Alternate: Charles H. Ackerman		Boulder, CO 80303	
Alternate: Charles H. Ackerman		Alternate: Joseph A. Lanzoni	
Robert W. Rapp	M 1/1/1996	Lon D. Santis	SE 01/15/1999
Principal	LIG-AAA	Principal	LIG-AAA
National Lightning Protection Corporation		Explosives Risk Managers, LLC	
13550 Smith Road, Suite 150		11104 Innsbrook Way	
Aurora, CO 80011		Ijamsville, MD 21754-9058	
Alternate: Paul R. Svendsen			
Ewen Thomson	SE 03/03/2014	John M. Tobias	U 4/1/1995
Principal	LIG-AAA	Principal	LIG-AAA
Marine Lightning Protection Inc.		US Department of the Army	
3215 NW 17th Street		CECOM, Attn: Amsel-SFS-I	
Companyille EL 22(05 2511		3200 Raritan Avenue	
Gainesville, FL 32605-2511		Aberdeen Proving Grounds, MD 21005	

IM 1/1/1988	Allan P. Steffes	M 1/1/1985
LIG-AAA	Voting Alternate	LIG-AAA
	Thompson Lightning Protection Inc.	
	St. Paul, MN 55118-1792	
U 03/07/2013	Charles H. Ackerman	M 4/1/1993
LIG-AAA	Alternate	LIG-AAA
	East Coast Lightning Equipment Inc.	
	24 Lanson Drive, RFD 4	
	Winsted, CT 06098	
	Principal: Mark P. Morgan	
RT 04/04/2017	Eric S. Boettcher	RT 08/17/2017
LIG-AAA	Alternate	LIG-AAA
	UL LLC	
	9535 Butternut Court	
	New Port Richey, FL 34654	
	UL LLC	
	Principal: Joseph P. DeGregoria	
U 08/17/2017	Kenneth P. Heary	IM 1/1/1978
LIG-AAA	Alternate	LIG-AAA
	Heary Brothers Lightning Protection	
	11291 Moore Road	
	Springville, NY 14141	
ry Solutions	Principal: William E. Heary	
M 03/05/2012	Joseph A. Lanzoni	M 1/16/2003
LIG-AAA	Alternate	LIG-AAA
	Lightning Eliminators & Consultants Inc.	
	6687 Arapahoe Road	
	Boulder, CO 80303-1453	
	Principal: Luke Pettross	
M 10/29/2012	Andrew S. McElroy	M 04/05/2016
	Andrew S. McElroy Alternate	
	Alternate	
	Alternate Harger Lightning & Grounding	
	Alternate	M 04/05/2016 LIG-AAA
	LIG-AAA U 03/07/2013 LIG-AAA RT 04/04/2017 LIG-AAA U 08/17/2017 LIG-AAA ry Solutions M 03/05/2012	LIG-AAAVoting Alternate Thompson Lightning Protection Inc. 901 Sibley Highway St. Paul, MN 55118-1792U 03/07/2013Charles H. AckermanLIG-AAAAlternate East Coast Lightning Equipment Inc. 24 Lanson Drive, RFD 4 Winsted, CT 06098 Principal: Mark P. MorganRT 04/04/2017Eric S. BoettcherLIG-AAAAlternate UL LLC 9535 Butternut Court New Port Richey, FL 34654 UL LLC Principal: Joseph P. DeGregoriaU 08/17/2017Kenneth P. HearyLIG-AAAAlternate Heary Brothers Lightning Protection 11291 Moore Road Springville, NY 14141 Principal: William E. HearyM 03/05/2012Joseph A. Lanzoni LIG-AAALIG-AAAAlternate HearyBitting Eliminators & Consultants Inc. 6687 Arapahoe Road Boulder, CO 80303-1453

George Portfleet	M 08/17/2015	Paul R. Svendsen	M 4/17/2002
Alternate	LIG-AAA	Alternate	LIG-AAA
Michigan Lightning Protection		National Lightning Protection Corporation	
2401 O'Brien Road SW		13550 Smith Road, Suite 150	
Grand Rapids, MI 49534-7009		Aurora, CO 80011	
United Lightning Protection Association, Inc.		Principal: Robert W. Rapp	
Principal: Stephen Humeniuk			
Philip E. Youtsey	M 08/09/2012	Christopher Coache	4/12/2017

Philip E. Youtsey	IM 08/09/2012	Christopher Coache	4/12/2017
Alternate	LIG-AAA	Staff Liaison	LIG-AAA
Guardian Equipment Company		National Fire Protection Association	
44375 Grand River Avenue		One Batterymarch Park	
Novi, MI 48375		Quincy, MA 02169-7471	
Lightning Protection Institute			
Principal: Harold VanSickle, III			

Chairman's Report for the TC on Lightning Protection

NFPA 780 First Draft Meeting

1) Date(s) and location of meeting: October 17 – 20, 2017, Fort Collins, CO.

2) List names of guests in attendance:

Porter, Christine Barrack, Samuel	Chair Principal	Intertek Testing Services Consolidated Nuclear Security, LLC
Batchelor, Christopher	•	US Department of the Navy
Campbell, Joanie	Principal	US Department of the Air Force
Covino, Josephine	Principal	US Department of Defense
DeGregoria, Joseph	Principal	UL LLC
Guthrie, Mitchell	Principal	Engineering Consultant
Harger, Mark	Principal	Harger Lightning & Grounding
Heary, William	Principal	Heary Brothers Lightning Protection
Humeniuk, Stephen	Principal	United Lightning Protection Association,
Johnson II, Carl	Principal	AVCON, Inc.
Kaiser, Bruce	Principal	Lightning Master Corporation
Larter, Simon	Principal	Dobbyn Lightning Protection
Melton, Robley	Principal	Alliance for Telecommunications Industry
Morgan, Mark	Principal	East Coast Lightning Equipment, Inc.
Pettross, Luke	Principal	Lightning Eliminators & Consultants Inc.
Thomson, Ewen	Principal	Marine Lightning Protection Inc.
Tobias, John	Principal	US Department of the Army
VanSickle, Harold	Principal	Lightning Protection Institute
Bas, Luis	Alternate	Intertek Testing Services
Boettcher, Eric	Alternate	UL LLC
Gallo, Ernest	Alternate	Alliance for Telecommunications Industry
McElroy, Andrew	Alternate	, Harger Lightning & Grounding
Portfleet, George	Alternate	United Lightning Protection Association,

Svendsen, Paul	Alternate	National Lightning Protection Corporation
Youtsey, Philip	Alternate	Lightning Protection Institute
Coache, Christopher	Staff Liaison	National Fire Protection Association
Roux, Richard	Staff Liaison	National Fire Protection Association
GUESTS:		

Dobbyn, Tom	Dobbyn Lightning Protection
Graves, Chuck	FAA
Carlson, Chris	Harger Lightning & Grounding
Choi, Younjin	OMNI LPS CO, LTD.
Chung, Youngki	OMNI LPS CO, LTD.
Bouchard, Rich	ULLC
Kohnken, Ken	Orica
Kithil, Richard	National Lightning Safety Inst.

3) List names of guests addressing the Panel/TC, the subject of their address, and the length of time they spoke:

Youngki Chung of Omni LPS speaking in support of several of his submitted inputs (early streamer emissions), 15 minutes with additional 15 minutes for questions.

- 4) Number of Public Inputs acted upon: 284
- 5) Number of First Revisions created: 131
- 6) List any Task Groups appointed to work subsequent to the Second Draft Meeting, along with the names of members of the Task Group(s): none
- 7) List any Public Inputs or First Revisions, in your opinion that needs to be referred to another TC for information or correlation: none
- 8) List any Public Inputs or First Revisions that should be referred to the Toxicity Advisory Committee: none

- 9) List all Public Inputs or First Revisions related to combustibles in plenums or other air handling spaces: none
- 10) Identify any issues that should be brought to the attention of the NFPA Research Foundation for their input and assistance: The CSST grounding/lighting strike issue is still ongoing with not only NFPA 780 but also NEC and NFPA 54.

Public Comn	nent No. 20-NFPA 780-2018 [New Section after 4.6.1.5]
Add a new A.4	1615
	re handrails are designed to be an intended strike termination device it is important to caution
	sideflash issues could result. Signage or other methods should be provided to warn the
public not to tou	uch or stand near the handrails when lightning is probable.
touch and sideflash	clause to allow handrails to serve as a strike termination device, it is important to point out the n safety issues associated with being near the handrail when lightning is in the area. LEMP will source of touch voltages that will be a personal safety threat.
Submitter Informa	tion Verification
	tion Verification me: Mitchell Guthrie
Submitter Full Na	me: Mitchell Guthrie
Submitter Full Nar Organization:	me: Mitchell Guthrie
Submitter Full Nar Organization: Street Address:	me: Mitchell Guthrie
Submitter Full Nat Organization: Street Address: City:	me: Mitchell Guthrie

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Public Comm	nent No. 22-NFPA 780-2018 [Section No. 4.7.11.3]
4.7.11.3	
connect the stril	strike termination device is required on an object, at least one main-size conductor shall ke termination device to a main-roof_conductor providing two or more paths to ground from accordance with Section 4.9 and 4.9.2.
Statement of Prob	lem and Substantiation for Public Comment
Primarily editorial c	comment that further clarifies which main conductor the 2nd main conductor refers to.
Related Ite	<u>em</u>
• FR-55	
ubmitter Informa	tion Verification
Submitter Full Nar	me: Mitchell Guthrie
Organization:	Engineering Consultant
Street Address:	
City:	
State:	
State: Zip:	

<u>4.19.1</u> Genera	al.
protection syste	ework of a structure shall be permitted to be utilized as the main conductor of a lightning em if it is equal to or greater than $\frac{3}{16}$ in. (4.8 mm) in thickness and is electrically continuous, ectrically continuous by methods specified in 4.19.3.
and the air term	aragraph 4.19.1 of NFPA 780 is to eliminate the requirement for both the main conductor inals on the lightning protection system, then I believe that Paragraph 4.19.1 should read
as follows:	
main conductor structure is equ metal roof struc	The metal roof structural members of a structure shall be permitted to function as the and air terminals of a lightning protection system if each metal roof structural member of a al to or greater than 3/16 inches (4.8 mm) in thickness and is electrically continuous. Or the tural members noted above in this paragraph (paragraph 4.19.1) are made electrically he methods specified in 4.19.3.
ment of Prob	lem and Substantiation for Public Comment
	lem and Substantiation for Public Comment
clarify the intent	of 4.19.1
o clarify the intent	
o clarify the intent	of 4.19.1
clarify the intent <u>R</u> no related item	of 4.19.1
o clarify the intent R no related item mitter Informa	of 4.19.1 <u>elated Item</u> tion Verification
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o clarify the intent R no related item mitter Informa ubmitter Full Nat rganization: ffilliation: treet Address:	of 4.19.1 elated Item tion Verification me: albert ondic Eglin Air Force Base
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o clarify the intent R no related item mitter Informa ubmitter Full Nar	of 4.19.1 elated Item tion Verification me: albert ondic Eglin Air Force Base

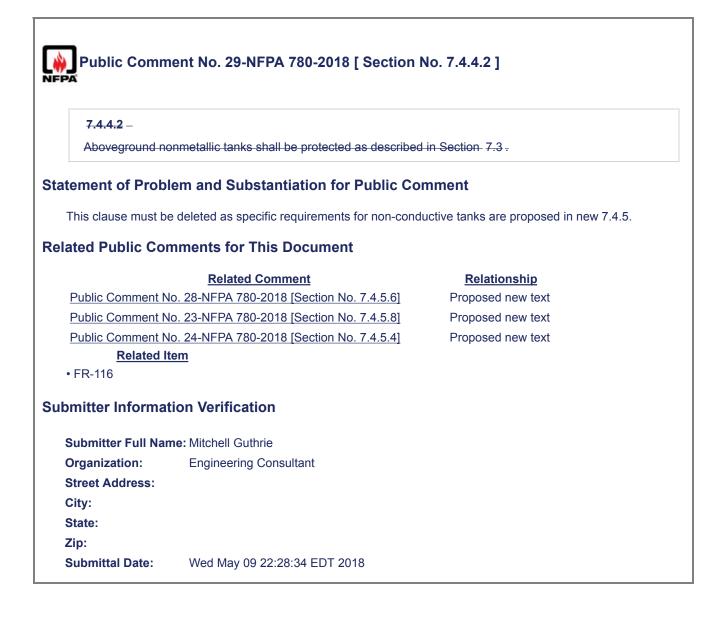
	nent No. 2-NFPA 780-2018 [Section No. 7.2.1 [Excluding any Sub-Sections]
	nent No. 2-NFFA 780-2018 [Section No. 7.2.1 [Excluding any Sub-Sections]
]	
	ns to reduce the ignition of flammable vapors shall be to minimize the exposure of locations
	e a direct strike- or-, Lightning Electromagnetic Pulse (LEMP), or secondary arcing. -vapor mixtures shall be prevented, to the greatest possible extent, from accumulating
outside such str	
Statement of Prob	plem and Substantiation for Public Comment
The comment ackr	nowledges that LEMP is also a threat that can result in arcing in a space containing a flammable
atmosphere, espec	cially in non-metallic tanks.
Related I	<u>item</u>
• FR 116	
Submittor Informa	
	tion Verification
Submitter morma	ation Verification
	ation Verification
Submitter Full Na	me: Mitchell Guthrie
Submitter Full Nation:	me: Mitchell Guthrie
Submitter Full Nat Organization: Street Address:	me: Mitchell Guthrie
Submitter Full Nat Organization: Street Address: City:	me: Mitchell Guthrie

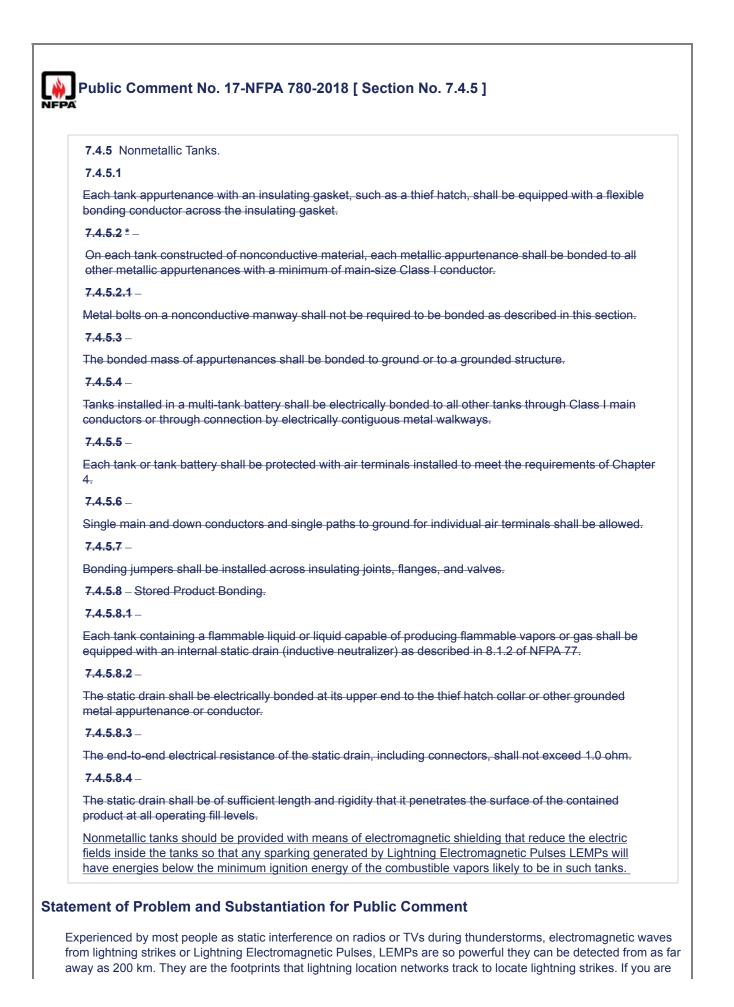
Put	olic Comment No. 25-NFPA 780-2018 [Section No. 7.3.7.3]
7.3	.7.3
A m	netal tank shall be grounded by one of the following methods:
(1)	A tank shall be connected without insulated joints to a grounded metallic piping system [i.e., electrically continuous, buried, and in direct contact with earth- for at least 10 ft (3 m)].
(2)	A vertical cylindrical tank shall rest on earth or concrete and shall be at least 20 ft (6 m) in diameter, or shall rest on bituminous pavement and shall be at least 50 ft (15 m) in diameter.
(3)	A tank shall be grounded through a minimum of two grounding electrodes, as described in Section 4.13, at maximum 100 ft (30 m) intervals along the perimeter of the tank.
(4)	A tank installation using an insulating membrane beneath for environmental or other reasons shall be grounded as in 7.3.7.3(4).
The Co	nt of Problem and Substantiation for Public Comment
The Co piping metalli length It also	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the buric c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes
The Co piping metalli length It also	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the buri c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes
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The Co piping metallii length It also which i • FR-2 bmitte Submi	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the burie c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes Related Item 9 er Information Verification
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The Co piping metallii length It also which i • FR-2 bmitte Submi Organi	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the burial c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes Related Item 9 er Information Verification tter Full Name: Mitchell Guthrie ization: Engineering Consultant
The Co piping metallii length It also which i • FR-2 bmitte Submi Organi Street City: State:	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the burial c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes Related Item 9 er Information Verification tter Full Name: Mitchell Guthrie ization: Engineering Consultant
The Co piping metallii length It also which i • FR-2: bmitte Submit Organi Street City: State: Zip:	ommittee Statement adding the text deleted by this comment provides a description of "grounded metallic system" that is consistent with 4.13.2.3.1. However, this statement uses the burial depth value but the burial c piping is seldom buried at a depth of 10 feet. A more realistic comparison would be to use the 12 foot for radials. infers only one grounding electrode of minimum length is necessary, which is in conflict with 7.3.7.3 (3), requires a minimum of 2 electrodes Related Item 9 er Information Verification tter Full Name: Mitchell Guthrie ization: Engineering Consultant

Public Comm	ent No. 26-NFPA 780-2018 [Secti	ion No. 7.4.3.2.3.1]
7.4.3.2.3.1		
that are not fully	seal assembly components, including sprir submerged shall be electrically insulated f the requirements of Section 4 <u>.</u> 16.	ngs, scissor assemblies, and seal membranes, from the tank roof or bonded to the roof- in
atement of Probl	em and Substantiation for Public	Comment
energies that will no		ure there would be no arcing but to limit any arcing this case, procedures should be implemented to in a flammable atmosphere.
lated Public Cor	nments for This Document	
	Related Comment	Relationship
Public Comment N	o. 27-NFPA 780-2018 [Section No. 7.4.3.2	2.4.1]
Public Comment N	o. 30-NFPA 780-2018 [Section No. 7.4.3.3	9.3]
Related Ite	<u>m</u>	
• FR-32		
ıbmitter Informat	ion Verification	
Submitter Full Nan	ne: Mitchell Guthrie	
Organization:	Engineering Consultant	
Street Address:	-	
City:		
State:		
Zip:		
Submittal Date:	Wed May 09 21:47:13 EDT 2018	

7.4.3.2.4.1		
	uide pole components, telescoping legs, or assemble ally insulated from the roof or bonded to the roof-in-	
tement of Prob	lem and Substantiation for Public Comn	nent
energies that will ne	ements of 4.16 were not developed to ensure there ot result in ignition of building materials. It should be ning flammable vapor.	
lated Public Co	mments for This Document	
	Related Comment	Relationship
Public Comment N	lo. 26-NFPA 780-2018 [Section No. 7.4.3.2.3.1]	Similar application
Public Comment N	lo. 30-NFPA 780-2018 [Section No. 7.4.3.3.3]	
Related I	tem	
• FR-110		
	tion Verification	
bmitter Informa		
	me: Mitchell Guthrie	
	ne: Mitchell Guthrie Engineering Consultant	
Submitter Full Na		
Submitter Full Nar Organization:		
Submitter Full Nar Organization: Street Address:		
Submitter Full Nan Organization: Street Address: City:		

no arcing but to limit any arcing to there is no arcing in an
ationship





close enough to the strike, these LEMPs can induce very large electric potentials that can destroy electronic equipment and are the principal cause of lightning related power failures on distribution lines. LEMPs from nearby lightning strikes go right through the non-conducting body of nonmetallic tanks and can induce potentials onto metallic components within the tank that can trigger sparking with energies far in excess of the minimum ignition energies of combustible vapors. If the tank contains such combustible vapors in the vicinity of these sparking metallic components, fires become inevitable. Lightning strikes falling within a half-mile or so from nonmetallic tanks represent a serious threat of fire.

LEMPs are also of particular interest for EFRTs and various sources of venting on many other types of tanks including metallic tanks.

Related Item

• FR 116

Submitter Information Verification

Submitter Full Name: amir rizkOrganization:Lightning ElectrotechnologiesStreet Address:City:State:Zip:Submittal Date:Mon May 07 14:00:11 EDT 2018

7.4.5 Nonmetallic Non-metallic Tanks.
7.4.5.1
Each tank appurtenance with an insulating gasket, such as a thief hatch, including, but not limited to, thie hatches, joints, flanges, and valves, shall be equipped with a flexible bonding conductor across the insulating gasket.
7.4.5.2*
On each tank constructed of nonconductive material, each metallic appurtenance shall be bonded to all other metallic appurtenances with a minimum of main-size Class I conductor.
7.4.5.2.1
Metal bolts on a nonconductive manway shall not be required to be bonded as described in this section.
7.4.5.3 <u>*</u>
The bonded mass of appurtenances shall be bonded to ground or to a grounded structure.
7.4.5.4
Tanks- <u>The grounding system for each tank</u> installed in a multi-tank battery shall be electrically bonded to the grounding systems for all other tanks through Class I main conductors or through connection by connections to electrically contiguous continuous metal walkways.
7.4.5.5
Each tank or tank battery shall be protected with air terminals strike termination devices installed to mee the requirements of Chapter 4.
7.4.5.6 –
Single main and down conductors and single paths to ground for individual air terminals shall be allowed.
7.4.5.7 –
Bonding jumpers shall be installed across insulating joints, flanges, and valves.
7.4.5.8 – Stored Product Bonding.
7.4.5.8.1 –
Each tank containing a flammable liquid or liquid capable of producing flammable vapors or gas shall be equipped with an internal static drain (inductive neutralizer) as described in 8.1.2 of NFPA 77.
7.4.5.8.2 –
The static drain shall be electrically bonded at its upper end to the thief hatch collar or other grounded metal appurtenance or conductor.
7.4.5.8.3 –
The end-to-end electrical resistance of the static drain, including connectors, shall not exceed 1.0 ohm.
7.4.5.8.4 –
The static drain shall be of sufficient length and rigidity that it penetrates the surface of the contained product at all operating fill levels.

Related Public Comments for This Document

	Related Comment	<u>Relationship</u>			
Public Comment No. 5-NFPA 780-2018 [New Section after A.7.4.5.2]					
	Related Item				
• PI-274 and PI-35	PI-274 and PI-350 as addressed in FR-116				
Submitter Informa	ation Verification				
Submitter Full Name: Simon Larter					
Organization:	Dobbyn Lightning Protection				
Street Address:					
City:					
State:					
Zip:					
Submittal Date:	Fri Apr 27 12:55:46 EDT 2018				

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Public Comm	Public Comment No. 3-NFPA 780-2018 [Section No. 7.4.5.2.1]		
7.4.5.2.1			
Metal bolts on a	Metal bolts on a nonconductive manway shall not be required to be bonded as described in this section.		
Statement of Prob	lem and Substantiation for Public Comment		
	All metallic components (including hardware & fasteners) on a non-conductive tank / or component must be bonded to ground. This is required in API Standard 650 Annex H and Specification 12P, and the intent is to avoid static discharge.		
	Related Item		
 potential hazard, 	not LP related		
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Public Comment No. 14-NFPA 780-2018 [Section No. 7.4.5.5]

7.4.5.5 –

Each tank or tank battery shall be protected with air terminals installed to meet the requirements of Chapter 4.

Statement of Problem and Substantiation for Public Comment

When an air terminal is struck by lightning, a voltage is impressed upon the air terminal that is dependent on the peak current associated with the lightning strike, it's time rate of change, the inductance of the down conductor system and the footing resistance. Side flashes occur whenever the voltage appearing on the down conductor exceeds the breakdown voltage of the gap between the down conductor and some other grounded body.

Similarly, when an air terminal on a fiberglass tank is struck, a voltage will be impressed upon the air terminal. Since these tanks are frequently used in areas of poor soil resistivity, the footing resistance will be high and so will the voltage appearing on the air terminal, in the hundreds of kV or more. Since the tank is made of a thin nonconducting material, from an electrical point of view, the air terminal is effectively suspended in mid-air and thus will produce intense sparking at it's lower end that could go right into the tank. Additionally any metallic components near the tank top, which are bonded to the air terminal, like piping that may enter into the tank, will be exposed to similar voltages and sparking. If there are any combustible vapors within the tank they could be susceptible to ignition from sparking from the air terminal or other metallic components bonded to the air terminal. In this respect the air terminal provides little to no protection against fires, particularly since these tanks typically contain many grounded metallic components at or near the top which can provide the same "protection/hazard" in the absence of an air terminal.

Additionally, the intense magnetic fields generated by the down conductors, when the system is struck by lightning, can induce enormous potentials that can generate hazardous sparking inside the tank. This would also be true for any masts or the down conductors of a catenary system.

The thermal energy associated with a spark of approximately 8" in length is about 0.25mJ. The minimum ignition energy of hydrogen sulfide in air is 0.077mJ (2003) Ignition Handbook. For metallic components installed at the top of a 30ft high tank and using Rusck's Equations for calculating inducing potentials from nearby lightning strikes; for each of the following current levels, the distance from which such a strike can induce potentials sufficient to produce sparking with thermal energy in the 0.25mJ range is given.

3kA -120m, 5kA - 154m, 10kA - 212m, 16kA - 263m

Clearly anything that can provide a protective zone from direct lightning strikes, if struck will be a source of intense fields that can generate hazardous sparking within the tank.

Therefore, air terminals should not be installed on nonmetallic tanks and masts or catenary systems should not be used.

Related Public Comments for This Document

Related Comment

Relationship

Public Comment No. 15-NFPA 780-2018 [Section No. 7.4.5.6]

Related Item

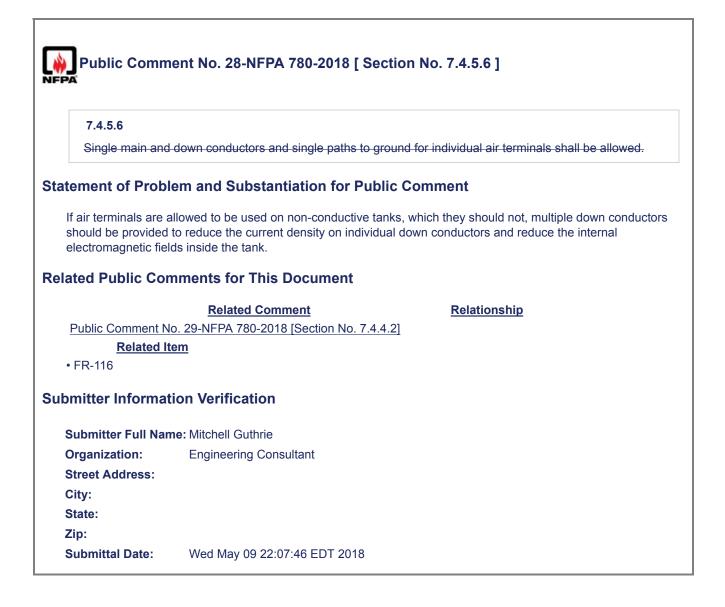
• FR 116

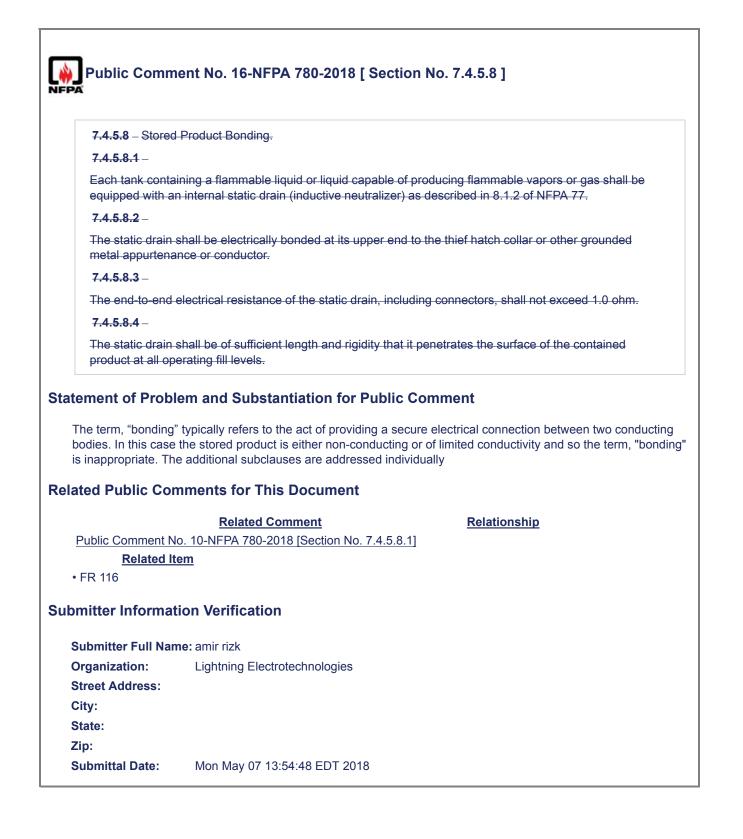
Submitter Information Verification

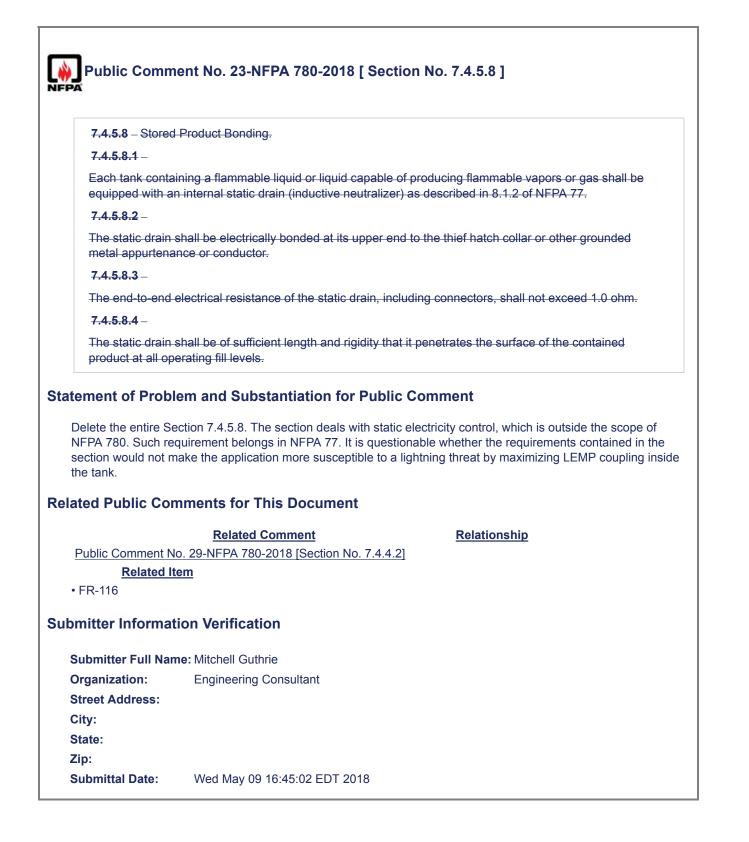
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Submittal Date: Mon May 07 13:48:52 EDT 2018









Public Comment No. 10-NFPA 780-2018 [Section No. 7.4.5.8.1]

7.4.5.8.1

Each tank containing a flammable liquid or liquid capable of producing flammable vapors or gas shall be equipped with an internal static drain (inductive neutralizer) as described in 8.1.2 of NFPA 77.

Statement of Problem and Substantiation for Public Comment

Inductive neutralizers, as described in NFPA 77 8.1.2 are intended for placement in static electric fields to neutralize static electric charge by ionization of air. The generated ions of opposite polarity to the static charge will move towards the static charge and neutralize them upon contact. Sharp tipped points are particularly useful in this regard because, by virtue of their geometry and ability to concentrate the electric field, they are prone to the production of electric discharges (ions) at the comparatively low and localized electric fields associated with static charges.

However for the same reasons that inductive neutralizers are prone to electric discharges under the low level, localized electric fields associated with static charge, they will also be highly prone to intense and hazardous sparking under the far more powerful and pervasive electric fields associated with lightning strikes and due to their characteristics, they will do so at lower field levels than any other metallic objects within the tank. The sparking from an inductive neutralizer under the influence of the electric fields produced by lightning strikes a half-mile away or more can easily exceed the minimum ignition energy of combustible vapors inside the tank making the presence of an inductive neutralizer inside a non-conducting tank a severe lightning hazard.

Related Public Comments for This Document

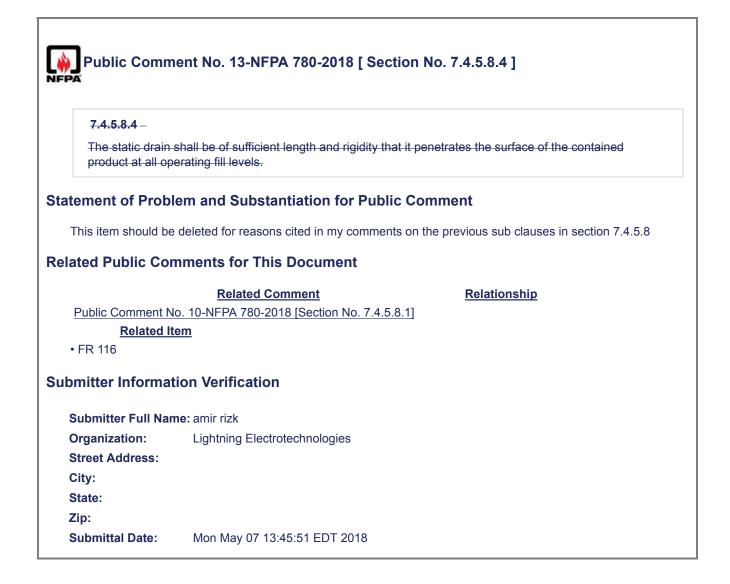
Related CommentPublic Comment No. 11-NFPA 780-2018 [Section No. 7.4.5.8.2]Public Comment No. 12-NFPA 780-2018 [Section No. 7.4.5.8.3]Public Comment No. 13-NFPA 780-2018 [Section No. 7.4.5.8]Public Comment No. 16-NFPA 780-2018 [Section No. 7.4.5.8]Related Item• FR 116Submitter Information Verification

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Relationship

Public Comme	ent No. 11-NFPA 780-2018 [Section No. 7.4.5.8.2]
NFPA	
7.4.5.8.2 –	
The static drain s metal appurtenar	shall be electrically bonded at its upper end to the thief hatch collar or other grounded nee or conductor.
Statement of Proble	em and Substantiation for Public Comment
may be bonded to th comparable to that ir upon the inductive n	e neutralizer to the thief hatch collar or any other metallic component at the tank top, which he air terminal if one is used, is also very hazardous. If the tank is struck, a potential mpressed upon the air terminal or other bonded components at the tank top will be impressed eutralizer. This could result in the direct application of hundreds of kV or more, which will sparking inside the tank with energies far in excess of the minimum ignition energy of the e vapors.
Related Public Com	nments for This Document
	Related Comment Relationship
	o. 10-NFPA 780-2018 [Section No. 7.4.5.8.1]
Related Ite	<u>m</u>
• FR 116	
Submitter Informati	on Verification
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Submittal Date:	Mon May 07 13:39:05 EDT 2018

Public Commo	ent No. 12-NFPA 780-2018 [Section No. 7.4.5.8.3]
7.4.5.8.3 –	
The end-to-end e	electrical resistance of the static drain, including connectors, shall not exceed 1.0 ohm.
tatement of Proble	em and Substantiation for Public Comment
This item should be	deleted for reasons sited in my comments on the previous sub clauses in section 7.4.5.8
Furthermore there appears to be a general misconception among some lightning protection practitioners which may have prompted such recommendations, the belief that the induced image or bound charges on grounded objects due to the free charges in the clouds or descending lightning leader can be removed or bled-off by method similar to those used to neutralize static charges. This notion is of course incorrect. Induced image charge or bound charge on grounded objects are just that, induced images. Attempting to remove the induced image charge while the inducing free charges remain in place is akin to removing the reflection in a mirror while the object producing the reflection remain in place.	
elated Public Com	ments for This Document
Public Comment No Related Ite • FR 116	Related CommentRelationshipb. 10-NFPA 780-2018 [Section No. 7.4.5.8.1]em
ubmitter Informati	on Verification
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Zip: Submittal Date:	Mon May 07 13:43:00 EDT 2018



Public Comment No. 18-NFPA 780-2018 [Section No. A.1.7]

A.1.7

Keeping the lightning protection system up-to-date with current standards is the best practice. However, periodic inspection and maintenance are often neglected. Facilities that have lightning protection systems older than twenty years, that have undergone additions, or that have had-<u>ensures the greatest level of safety.</u> Facilities that have undergone additions_alterations should be brought into compliance with the current standards. When a lightning protection system is upgraded, as-built drawings are recommended so the AHJ has a record of the <u>drawings should be revised to document the modifications.</u> These_drawing drawings_should include_testing_test_point locations_, if installed where applicable. Where required by the AHJ, test records of the new configured system should be provided to establish a new baseline for future test measurements. - If no modifications have occurred since construction, at a minimum, conduct a visual inspection. Re-evaluate the need to improve the lightning protection system based on the current use and contents of the facility. If the system, as previously installed, provides adequate coverage, no additional changes are required. The AHJ is advised to maintain the applicable drawings and test records. If the system is in disrepair and is no longer deemed necessary by the AHJ based on the structure's use, occupancy, and content, the facility would be better off having the lightning protection system removed than to have a nonfunctional system._

Statement of Problem and Substantiation for Public Comment

The proposed revision, as written, infers too much responsibility on the AHJ. For example, very few AHJs maintains drawings or test records. These should be maintained locally at the site so they can be used. The suggestions in the text should be applicable regardless of whether an AHJ is involved. Much of this text is more applicable to Annex D.

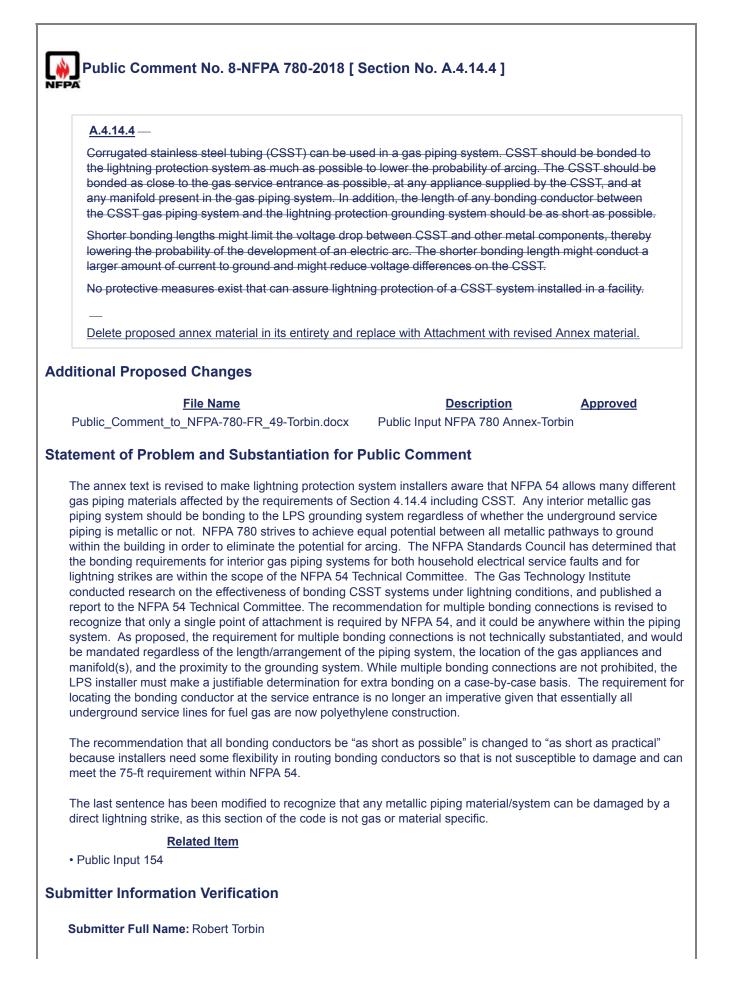
The annex material adds new recommendations not consistent with the normative text of the referenced clause and may not be necessary for all applications. It infers that acceptable grandfather clauses should not be implemented.

Related Item

• FR-75

Submitter Information Verification

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Submittal Date:	Thu May 03 21:06:20 EDT 2018	

Delete proposed Annex material (A.4.14.4) in its entirety and replace with the following:

Corrugated stainless steel tubing (CSST) is one of many gas piping materials allowed by NFPA 54 (National Fuel Gas Code) that can be affected by Section 4.14.4. Where a lightning protection system (LPS) is installed on a building containing fuel gas piping, the piping system should be bonded to the lightning protection system to lower the probability of arcing from a direct strike. NFPA 54 includes specific electrical bonding requirements to minimize damage to the CSST by lightning strikes:

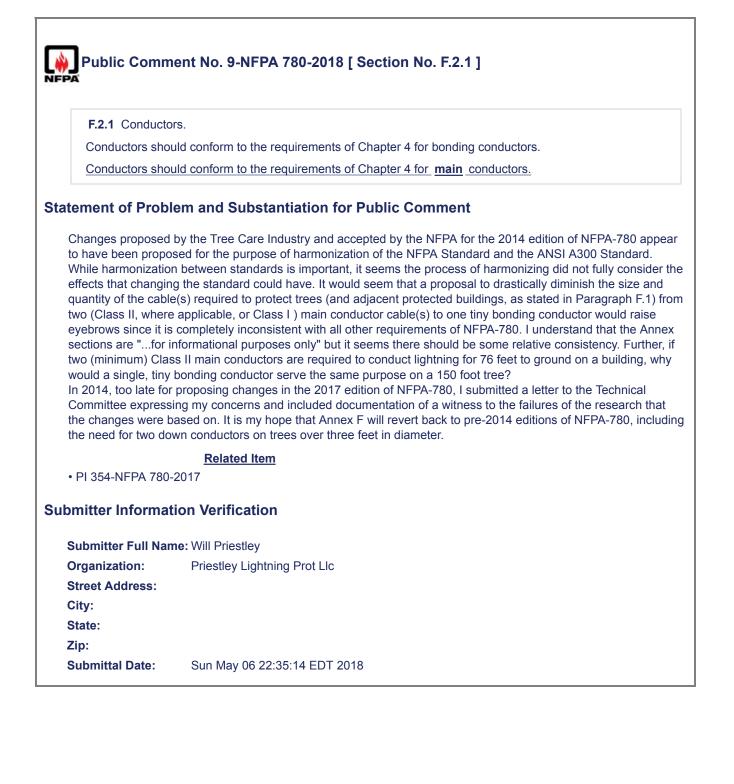
- 1. The CSST system must be bonded at one location in accordance with the requirements of NFPA 54 (Section 7.12.2). This location may be on the customer's gas piping near the service entrance, near a gas appliance with a metallic vent installed through the roof and/or above the roofline, or at any manifold present in the gas piping system.
- 2. <u>The bonding clamp must never be mounted directly on the CSST or its jacket.</u>
- 3. <u>The length of any bonding conductor between the CSST gas piping system and the LPS grounding system should be as short as practical, but in no case longer than 75-ft (22.86-m) in accordance with the National Fuel Gas Code (7.12.2).</u>
- 4. <u>The installation of additional bonding clamps and conductors at multiple locations are not</u> required unless the installing LPS contractor determines the need for extra connections for a given building and gas piping system.

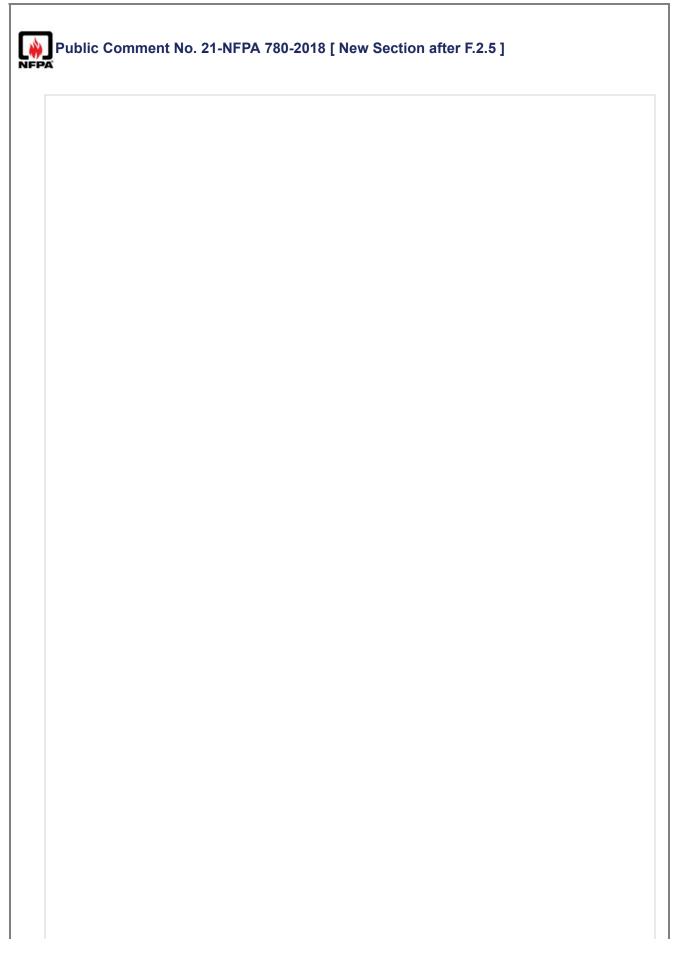
Shorter lengths for the bonding conductor will help minimize the voltage differential between the gas piping and other nearby metal components, and, thereby lowering the probability that an electric arc will be initiated or damage incurred to the piping system.

No protective measures exist that can assure protection of any metallic piping system installed in a building from damage due to lightning.

A.7.4.5.3 Bonding of the c	contained product to grounded metal tan	k components should be considered. If not
equalized, the c	harge on the product may arc to another	r mass at a different potential during a direct or
		a conductive appliance with low electrical resistance to the thief hatch collar and extending to the bottom
of the tank, pen	etrating the surface of the product at all f	fill levels. This will not equalize charge in all areas of
the product, but	can serve to equalize charge local to the	e appliance.
atement of Prob	lem and Substantiation for Pub	lic Comment
		iic ooninient
Wording submitted	is in support of the Flammables Working	g Group edits to 7.4.5.
lated Public Co	nments for This Document	
Dublic Oceano at N	Related Comment	Relationship
7.4.5]	lo. 4-NFPA 780-2018 [Section No.	Tight. Like, bros, dude. They hang out on the reg.
	Related Item	ů – Elektrik
• PI-274 and PI-350), as addressed in FR-116.	
• PI-274 and PI-350		
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A.11.4.4.1	
To maintain all of bonded at all or elevations. All of <u>separation dista</u> greater the brea	counterpoise conductors at the same potential, all counterpoise conductors should be ossings and intersections. Crossing counterpoise conductors could be at different counterpoise conductors within 5 ft (1.5 m) of each other should be bonded. The actual safe ance in soil is dependent upon the local earth resistivity. The higher the earth resistivity, the akdown distance of the soil. Every reasonable and prudent means should be utilized to ecting or crossing counterpoise conductors.
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separation distance Related Ite • FR-61	e) and earth resistivity but does not change the recommended value.
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	Annex G: Protection for Bridges
<u>G.</u>	1 General. This annex provides guidance for the protection of bridges from lightning damage.
<u>G.</u>	1.1 <u>The guidelines in this annex should apply to the following types of structure:</u>
<u>(1)</u>	Beam bridges
<u>(2)</u>	Arch bridges
<u>(3)</u>	Cantilever bridges
<u>(4)</u>	Cable stayed bridges
<u>(5)</u>	Suspension bridges
<u>(6)</u>	Truss bridges
<u>G.</u>	1.2 All of the requirements of Chapter 4 should apply, except as modified by this chapter.
	1.3 <u>Piers, in this chapter, refers to a supporting tower for a bridge structure, as found in cable</u> yed and suspension bridges.
<u>G.:</u>	2 Protection for Bridges
	2.1 Where required by construction, down conductors and grounding electrodes should be rmitted to be spaced at greater than the 100 foot (30 m) average required by 4.9.10.
	2.2 <u>Grounding electrodes should be placed at each end of the bridge, and at each pier, where</u> ch are present.
inte	2.3 Bridges should be provided with deck–level potential equalization networks consisting of erconnected cables and/or conductors running along these structures to provide erconnection of all permanently installed metal objects on the bridge.
suc	2.4 <u>Where expansion joints are installed on a bridge, adequate jumpers should be provided</u> <u>ch that the lightning protection will not be damaged by thermal movement of the bridge</u> mponents.
	2.5 <u>Strike termination devices should be provided to protect all appurtenances that extend</u> tside the zone of protection, including aircraft hazard lights, antennas, railings, etc.
<u>G.:</u>	2.4 Beam and Cantilever bridges.
	2.4.1 Consideration should be given to protecting beam and cantilever bridges with elevated ike termination devices on poles or light standards.
	2.4.2 <u>Handrails and/or guardrails should be permitted to serve as strike termination devices,</u> bject to the requirements of section 4.7.
<u>G.:</u>	2.5 Arch bridges.
	2.5.1 Where the supporting arch is of any material other than structural metal that meets the puirements of section 4.19, strike termination devices should be provided.
<u>G.</u> 2	2.6 Cable stayed bridges.
	2.6.1 Where the supporting piers are of any material other than structural metal that meets the
	uirements of 4.19, strike termination devices should be provided.
	2.6.2 <u>Strike termination devices should not be required on the uppermost cable stay where their</u> ovision would interfere with the operation or maintenance of the bridge.
	2.6.3 The cable stays and their anchoring boxes should be grounded at their top and bottom tremities to the down conductors and deck-level potential equalization network.
	2.6.4 Intermediate equipotential loops shall be provided for the pier(s) in accordance with ction 4.15.
<u>G.:</u>	2.7 Suspension bridges.
<u>G.</u> 2	2.7.1 Suspension bridges should be protected in the same manner as cable stayed bridges.
<u>G.:</u>	2.8 Truss bridges.
	2.8.1 Where the trusses are constructed of any material other than structural metal that meets erequirements of section 4.19, strike termination devices should be provided for the top chord.
<u>G.:</u>	3 Surge protection.
G .:	3.1 Surge protection devices should be installed for all electrical power and communications

	k-level potential equalization network should be permitted to serve as the ground reference point for SPDs protecting communications systems.
atement of Probl	em and Substantiation for Public Comment
There is currently n annex material to the	o guidance for protection of bridges from lightning. This remedies the situation by providing nat end.
Related Ite	<u>em</u>
• PI-328	
bmitter Informat	ion Verification
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M.2	2.1
This the mea	Ightning strike victims are struck before or after the rain that usually accompanies thunderstorms. swould indicate that most people have the good sense to get out of the rain, but are not as conscious of life-threatening hazards presented by lightning. Atmospheric conditions that cause lightning can be asured and the probability of a lightning event predicted. However, it is not possible to predict the exact ation where lightning will strike since it has been known to attach to earth beyond the visible horizon.
-	ntning is extremely dangerous, and unnecessary exposure should be avoided. The following ommendations are advisable:
(1)	When possible, plan outdoor activities around the weather forecast. Although it is difficult to know exactly if a storm will occur, the conditions that create lightning storms, such as the meeting of high- and low-pressure systems, are predicted days in advance. On days when such weather patterns are forecast, avoid planning activities where shelter is not readily available, such as boating or camping.
(2)	Check the forecast the night before and the morning of planned outdoor activities to see if lightning is a possibility.
(3)	Check weather maps online before you leave. Most weather websites will have recent satellite and radar images of the area of your activity.
(4)	When you arrive at the area of your activity, devise a plan on where to go in the event of an approaching lightning storm. Tell all persons in your party, especially children, where to go in accordance with M.2.2. Also, tell your party where you will meet half an hour- <u>30 minutes</u> after thunder is last heard, since you may not be together when the threat of a storm arises.
(5)	Carry a weather radio with an "Alert" feature or set your mobile device to receive severe weather warnings.
(6)	Respond accordingly when warnings are issued.
emer	nt of Problem and Substantiation for Public Comment ersonal safety safety documents require 30 minutes as the waiting time since the the last lightning strike
	hunder has occurred before resuming operations. Thirty minutes should be used here.
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time between th	der, seek shelter immediately. Do not try to predict how close lightning is by counting the e flash of lightning and the sound of thunder. Seek shelter in one of the following structures e until half an hour <u>30 minutes</u> after you last hear thunder:
(1) A dwelling	or other building that is protected against lightning
(2) A large met	al-framed building
(3) An enclose	d automobile, bus, or other vehicle with a metal top and body
(4) An enclose	d metal train or street car
30 minutes is the te	lem and Substantiation for Public Comment
	erm used most often in personnel safety rules
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