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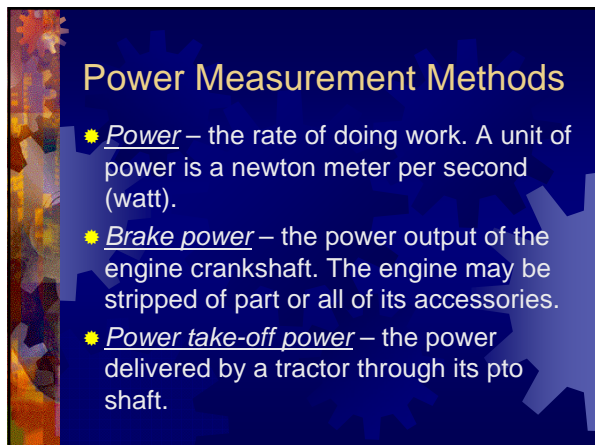
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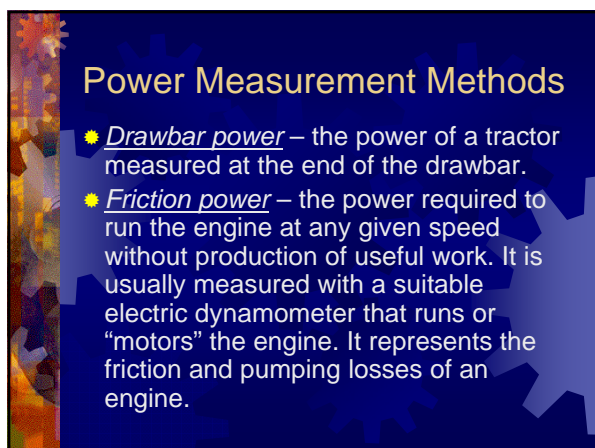
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## Power Measurement Methods

- ☀ Observed power – the power obtained at the dynamometer without any correction for atmospheric temperature, pressure, or water vapor.
- ☀ Corrected power – obtained by correcting observed power to standard conditions of sea-level pressure, 15.5°C temperature, and zero vapor pressure.

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## Power Measurement Methods

- ☀ Dynamometer – an instrument for determining power, usually by the independent measure of force, time, and the distance through which the force is moved. Dynamometers may be classified as brake, drawbar, or torsion, according to the manner in which the work is being applied. Also, they may be classed as absorption or transmission, depending on the disposition of the energy.

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## Dynamometers

- ☀ A dynamometer for testing engines must include the following four essential elements:
  - A means for controlling torque
  - A means for measuring torque
  - A means for measuring speed
  - A means for dissipating power

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## Prony brake

- It is the simplest type of dynamometer – an example of an absorption-type dynamometer.
- The rotor is connected to the crankshaft of the engine and rotates at engine speed. Surrounding the rotor are brake shoes that create torque drag on the rotor. The torque is controlled by tightening or loosening the hand lever. The torque is measured by a scale located at the end of the lever arm. A tachometer must be provided for measuring the rotor speed. After the torque and speed are measured, the power can be calculated.

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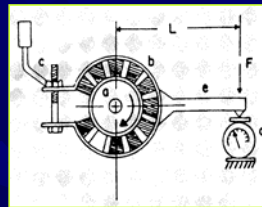
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## Prony Brake Dynamometer

- $P = (2\pi * L * F * n) / 60,000$  ; kW
- Torque is determined by the prony brake through measuring Force and Length.
- $P = 2\pi nT / 60,000$  ; kW



Gooding et al., 2003, Off-road Vehicles, ASABE

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## Hydraulic

- The hydraulic dynamometer operates like a hydraulic turbine/pump. The working medium, usually water, is circulated within the housing creating frictional resistance to turbine rotation. The engine power is converted to heat and the liquid exits at a higher temperature than when it entered. The outer case, which is free to rotate about the input shaft, is connected to and restrained by the torque arm. With the exception of bearing friction, the torque measured is equal to that supplied to the dynamometer.

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## Hydraulic con't

- The power-absorbing capacity for any given type of design varies approximately as the cube of the speed of rotation and the fifth power of the diameter (Culver 1937). The power equation is the same as for the prony brake.
- The accuracy of the hydraulic-brake dynamometer can be expected to be somewhat better than that of the prony brake and should fall between it and the cradled electric type.

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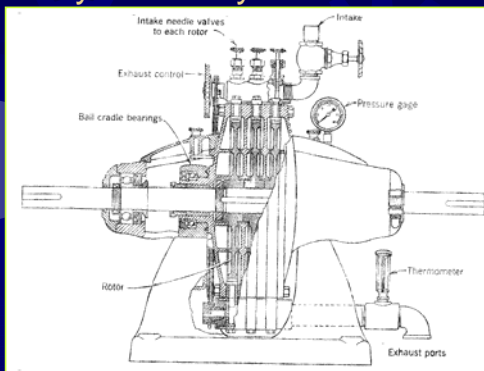
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## Hydraulic Dynamometer



Goering et al., 2003, Offroad Vehicles, ASAE

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## Electric Direct-Current Dynamometers

- The direct-current cradle-mounted dynamometer is a shunt-wound generator with separate field excitation. The field frame is free to rotate, and since any effort to turn the armature causes the field to attempt to revolve, the resultant torque will cause a force to be registered on the scales. The accuracy is independent of the electrical efficiency of the machine. Accuracy within 0.25 percent is possible.

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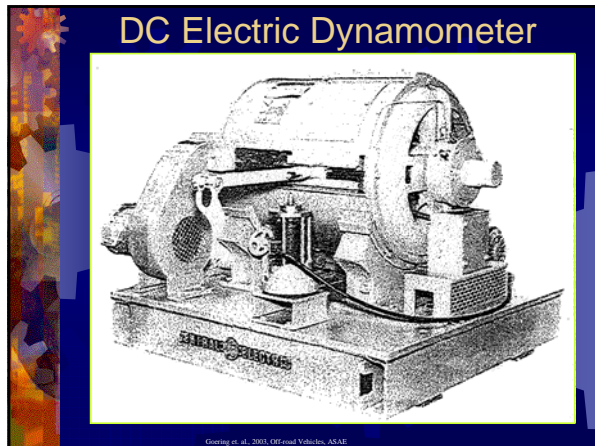
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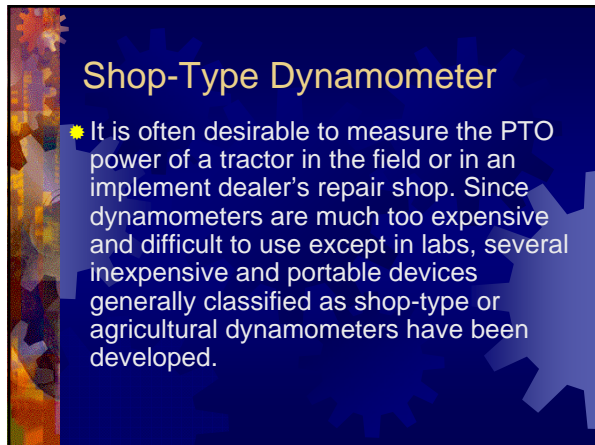
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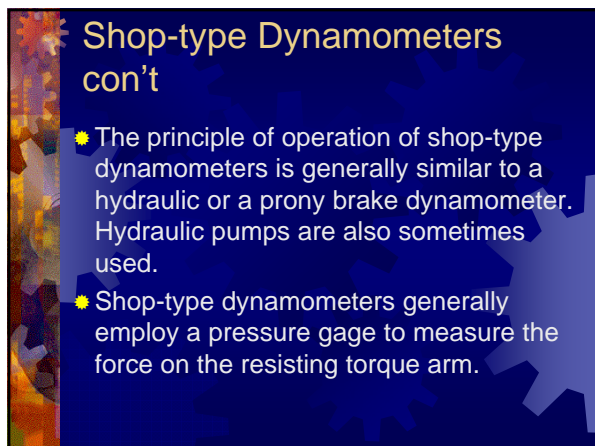
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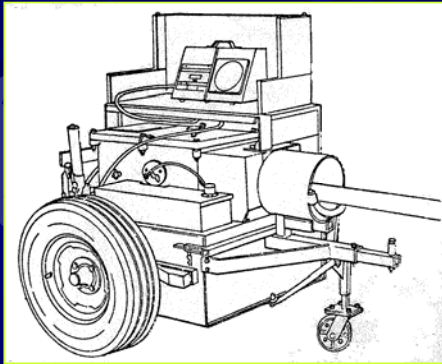
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## Shop-type Dynamometer



Goering et al., 2003, Off-road Vehicles, ASAE

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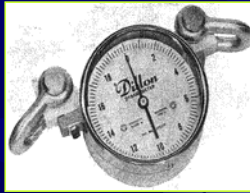
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## Spring Dynamometer

- The simplest and most obvious type of drawbar unit consists of a spring that elongates under tension or shortens under compression. Such a dynamometer is suitable for rough measurements of forces.



Goering et al., 2003, Off-road Vehicles, ASAE

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## Torsion Dynamometers

- With the advent of machinery operated by tractor power-take-off shafts a great deal of interest has been displayed in devices for the measurement of power as transmitted by rotating shafts.
- *Torque Meter, Strain-Gage Type:*
  - The development of the electrical resistance strain gage has made practical the measurement of torque and force on farm tractors and machines. Many torque meters employing strain gages have been developed.

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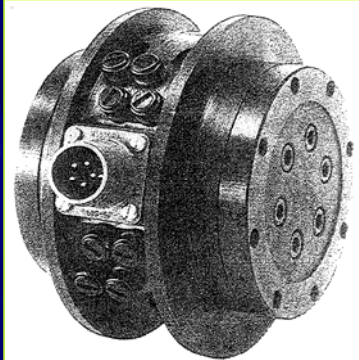
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## Torque Meter



Goring et al., 2003, Off-road Vehicles, ASAE

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## Volume-Based Fuel Flowmeters

- Fuel consumption is frequently measured during an engine test; the measurement can be on a volume or mass basis.

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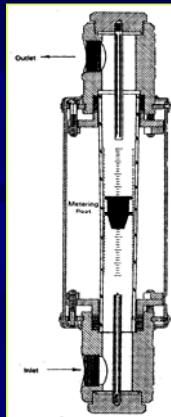
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- This *rotameter* measures fuel consumption on a volume basis. The transparent tube has a slight taper (its diameter increases toward the top). Fuel enters the bottom of the tube, flows upward around the float in the tube, and exits at the top. The higher the flow rate, the higher the flow must rise to allow sufficient space around the edges of the float to allow fuel to pass. Thus, a scale inscribed directly on the outside of the tube can be calibrated directly in terms of volumetric flow rate.



Goring et al., 2003, Off-road Vehicles, ASAE

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## Standardized Tractor Tests

- Data from standardized tests may be used in comparing the performances of various makes and models of tractors. When comparative test are administered by agencies independent of the tractor manufacturers, the resulting competition among the manufacturers also tends to promote improvements in tractors design. The original independent agency to do tractor testing was the University of Nebraska Tractor Testing Laboratory (NTTL).

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## Standardized Tractor Tests

- Three standard test procedures are now widely recognized for testing tractors. They include the standard ASAE/SAE/ISO test, the OECD restricted test, and the OECD long test. The OECD tests are described by code designations, as follows:

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- Compulsory Tests:**

  - Main PTO
  - Hydraulic power and lifting force
  - Drawbar power, ballasted tractor
  - Turning area and turning circle
  - Position of center of gravity
  - Braking (wheeled tractors only)
  - External (bystander) noise (wheeled tractors only)

- Tests performed and reported at manufacturer's option:**

  - Engine
  - Performance at the belt or belt pulley shaft
  - Performance in a hot atmosphere
  - Low temperature starting
  - Drawbar power and fuel consumption for unballasted tractor

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POWER TAKE-OFF PERFORMANCE									
Power HP (kW)	Crab shaft speed rpm	Oil/hr (l/h)	hp/gal (l/hpA)	hp/gal (l/hpA)	hp/gal (l/hpA)	hp/gal (l/hpA)	hp/gal (l/hpA)	hp/gal (l/hpA)	hp/gal (l/hpA)
MAXIMUM POWER AND FUEL CONSUMPTION									
Rated Engine Speed—(PTO speed—1800 rpm)									
94.02 (69.12)	2099	5.40 (20.14)	0.402 (1.54)	17.42 (65.51)					
Maximum Power (2 hours)									
95.06 (70.48)	1900	5.31 (20.12)	0.383 (1.45)	18.26 (69.00)					
VARYING POWER AND FUEL CONSUMPTION									
94.02 (70.12)	2099	5.40 (20.14)	0.402 (1.54)	17.42 (65.51)					
82.93 (61.84)	2184	5.02 (19.00)	0.423 (1.57)	16.52 (62.27)					
63.10 (47.50)	2209	4.29 (16.24)	0.475 (1.83)	14.71 (55.99)					
42.07 (31.37)	2227	3.39 (12.83)	0.563 (2.13)	12.41 (46.33)					
21.16 (15.78)	2245	2.53 (9.58)	0.856 (3.24)	8.56 (31.63)					
0.90 (0.67)	2260	1.72 (6.51)	1.206 (4.58)	0.55 (2.05)					
Maximum Torque 311 lb.-ft. (422 Nm) at 1400 rpm									
Maximum Torque Rise 32.3%									
Torque rise at 1700 engine rpm 20%									

Location of Test: Tractor Testing Laboratory,  
University of Nebraska, Lincoln, Nebraska 68583-0832

Date of Test: May 10 to June 1, 1994

Manufacturer: John Deere Tractor Works, P.O.  
Box 270, Waterloo, Iowa 50704

FUEL OIL and TIME: Fuel No. 2 Diesel/Geshe  
No. 55.9 Specific gravity converted to 60°F/15.6°C  
F (15.6°C) 0.860 Fuel weight 6.994 lb/gal  
(0.818 kg/l) Oil SAE 15W-40 API service  
classification SUCCE To motor 1.551 gal  
(16.093 l) Drained from motor 4.178 gal  
(15.817 l) Transmission and hydraulic lubricant  
John Deere Hy-Gard fluid Front axle lubricant  
John Deere GL-5 Gear Lubricant Total time engine  
was operated 20.0 hours

ENGINE: Make John Deere Model Type six  
cylinder vertical with turbocharger Serial No.  
TC062074311197 Crankshaft length Base Rated  
engine speed 2100 Revs and stroke (in specified)  
4.19" x 4.531" (106.5 mm x 115.0 mm) Compression  
ratio 17.8 to 1 Displacement 209 cu in (3440 ml)  
Starting system 12 volt Lubrication pressure 40  
psi (2.75 bar) Oil filter one paper element and  
one full flow cartridge Oil cooler engine coolant heat  
exchanger for coolant oil, radiator for hydraulic and  
transmission oil Fuel filter one paper element and  
one pressure/pressure relief filter for fuel filter  
underhood Exhaust vertical Cooling medium  
temperature control two thermostats and variable  
speed fan

DRAWBAR PERFORMANCE									
FUEL CONSUMPTION CHARACTERISTICS									
Power hp (kW)	Drawbar pull lb (N)	Speed mph (km/h)	Crab shaft speed rpm	Slip %	Fuel Consumption hp/gal (l/hpA)	hp/gal (l/hpA)	Temp °F (°C)	Air dry bulb °F (°C)	Barom. in. Hg (kPa)
Maximum Power—6th (C1) Gear									
82.70 (61.07)	6456 (28.73)	4.80 (7.75)	2101	3.9 (0.278)	0.457 (1.74)	15.31 (57.4)	196 (75)	70 (21)	28.75 (97.29)
75% of Pull at Maximum Power—6th (C1) Gear									
65.16 (48.59)	4838 (21.52)	5.05 (8.13)	2196	3.49 (0.307)	0.505 (1.93)	13.86 (51)	190 (72)	70 (21)	28.74 (97.52)
50% of Pull at Maximum Power—6th (C1) Gear									
44.59 (33.10)	3229 (14.30)	5.16 (8.30)	2221	3.33 (0.307)	0.603 (2.28)	11.60 (43)	186 (70)	70 (21)	28.74 (97.52)
75% of Pull at Reduced Engine Speed—8th (C2) Gear									
65.26 (48.67)	4843 (21.54)	5.05 (8.13)	1572	3.49 (0.256)	0.440 (1.68)	15.90 (59)	192 (73)	70 (21)	28.74 (97.52)
50% of Pull at Reduced Engine Speed—8th (C2) Gear									
44.54 (33.00)	3225 (14.30)	5.16 (8.30)	1589	2.41 (0.259)	0.491 (1.84)	14.25 (52)	194 (73)	70 (21)	28.74 (97.52)

ENGINE OPERATING PARAMETERS: Fuel  
rate: 37.5-40.3 lb/h (16.5-18.3 kg/h) High Idle:  
2225-2325 rpm Turbo boost nominal 8.7-10.2 psi  
(60-70 kPa) as measured 9.0 psi (63 kPa)

CHASSIS: Type front wheel drive Serial No.  
\*R2W7000001437\* Tread width rear 50.0" (1269  
mm) to 100.5" (2540 mm) front 60.0" (1524 mm) to  
80.0" (2032 mm) Wheel base 103.3" (2629 mm)

Hydraulic control system direct engine drive  
Transmission selective gear fixed ratio Nominal  
travel speeds mph (km/h) first 1.43 (2.30) second  
2.00 (3.22) third 2.64 (4.25) fourth 3.05 (4.87) fifth  
4.24 (6.82) sixth 4.82 (7.75) seventh 5.59 (9.00) eighth  
6.74 (10.85) ninth 8.90 (14.33) tenth 9.99 (16.08)  
eleventh 13.98 (22.50) twelfth 18.46 (29.71) reverse  
1.75 (2.81), 3.70 (5.96), 5.88 (9.48), 12.21 (19.63)  
Clutch multiple wet disc hydraulically actuated by  
foot pedal Brakes wet multiple disc hydraulically  
actuated by two foot pedals which can be locked  
together Steering hydrostatic Power take-off 540  
rpm at 2000 engine rpm and 1000 rpm at 2000 engine  
rpm Unladen tractor mass 12522 lb (5680 kg)

REPAIRS AND ADJUSTMENTS: No repairs or  
adjustments

DRAWBAR PERFORMANCE									
MAXIMUM POWER IN SELECTED GEARS									
Power hp (kW)	Drawbar pull lb (N)	Speed mph (km/h)	Crab shaft speed rpm	Slip %	Fuel Consumption hp/gal (l/hpA)	hp/gal (l/hpA)	Temp °F (°C)	Air dry bulb °F (°C)	Barom. in. Hg (kPa)
2nd (A2) Gear									
60.51 (45.13)	1224 (54.51)	1.85 (2.98)	2101	14.65 (0.196)	0.553 (2.08)	12.85 (50)	186 (70)	63 (19)	28.77 (97.42)
3rd (A3) Gear									
28.25 (21.38)	1158 (51.59)	2.55 (4.07)	2126	8.87 (0.282)	0.485 (1.82)	14.58 (54)	190 (72)	66 (19)	28.76 (97.38)
4th (B1) Gear									
81.84 (61.07)	1005 (45.29)	2.83 (4.55)	2060	8.14 (0.286)	0.460 (1.74)	15.22 (57)	193 (73)	59 (17)	28.74 (97.20)
5th (B2) Gear									
81.15 (60.01)	8240 (36.74)	3.78 (6.08)	1903	5.25 (0.267)	0.438 (1.64)	15.85 (59)	197 (73)	70 (21)	28.73 (97.26)
6th (C1) Gear									
83.22 (62.00)	7209 (32.57)	4.55 (7.33)	1903	6.43 (0.267)	0.439 (1.64)	15.93 (59)	197 (73)	70 (21)	28.73 (97.26)
7th (B3) Gear									
83.14 (62.00)	6471 (29.45)	5.55 (8.93)	1901	5.81 (0.268)	0.441 (1.65)	15.90 (59)	198 (74)	71 (21)	28.68 (97.12)
8th (C2) Gear									
79.99 (59.40)	4876 (21.83)	6.15 (9.93)	1805	2.99 (0.272)	0.432 (1.63)	15.46 (58)	197 (73)	71 (21)	28.71 (97.28)
9th (C3) Gear									
79.14 (58.40)	3642 (16.30)	8.15 (13.10)	1803	2.54 (0.270)	0.435 (1.63)	15.46 (58)	198 (73)	71 (21)	28.75 (97.28)


REMARKS: All test results were determined from  
observed data obtained in accordance with official  
OECD, SAE and Nebraska test procedures. For the  
maximum power tests, the fuel temperature at the  
injection pump return was maintained at 150° F  
(65°C). This tractor did not meet manufacturers claim  
of 72-hp (52-kW) at 2000 rpm. The performance results  
on this summary were taken from OECD tests  
conducted under the Code of Recommended Standard Test  
Code procedure.

We, the undersigned, certify that this is a true and  
correct report of official Tractor Test No. 1478,  
Summary 150, July 21, 1994.

LOUIS I. LEVITICUS  
Engineer-in-Charge

R.D. GRISIO  
M.F. KOCHER  
K. VON BARGEN  
Board of Tractor Test Engineers





## Correcting Power for Atmospheric Conditions

- The density of air changes with temperature and barometric pressure. Such density changes affect the rate at which an engine can consume air and, since it is air consumption that limits engine power, the power output varies with atmospheric conditions.
- Power correction begins with the use of the ideal gas law to correct for atmospheric conditions:  $pV = MRT$

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## Power Correction

- Because mass density is the mass per unit volume, the ideal gas law can be restated as:
  - $\rho = M / V = BP / RT$
  - Where  $\rho$  = air density, kg/m<sup>3</sup>
  - BP = barometric pressure, kPa
  - T = absolute temperature of air, K
  - R = ideal gas constant
- This equation can be used to obtain the ratio of air densities at observed and standard conditions.

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## Power Correction

- The gas constant cancels out in obtaining the ratio, with the following result:
  - $\rho_s / \rho_o = (BP_s / BP_o)(T_o / T_s)$
  - Where  $\rho_o$  = air density at observed conditions, kg/m<sup>3</sup>
  - $\rho_s$  = air density at standard conditions, kg/m<sup>3</sup>
  - BP<sub>o</sub> = barometric pressure at observed conditions, kPa
  - BP<sub>s</sub> = barometric pressure at standard conditions, kPa
  - T<sub>o</sub> = absolute temperature of the air at observed conditions, K
  - T<sub>s</sub> = absolute temperature of the air at standard conditions, K

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## Power Correction

- Power correction factor:

- $f_a = (BP_s / BP_o)(T_o / T_s)^n$

- Theoretically, the correction should be applied to the indicated power, then

- $P_{bs} + P_{fs} = f_a (P_{bo} + P_{fo})$

- But  $P_{fs} = P_{fo}$ , because friction power is not affected by atmospheric conditions:

- $P_{bs} = f_a P_{bo} + P_f (f_a - 1)$

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## Power Correction

- Because  $P_f$  is often much smaller than  $P_b$  and  $f_a$  is close to 1, the last term is usually dropped. The final power correction equation is then:

- $P_{bs} = f_a P_{bo}$

- That is, the correction is applied directly to the brake power. The usual choice of standard conditions is  $B_{pa} = 99 \text{ kPa}$  and  $T_s = 298 \text{ K}$  (25°C).

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