

Physics impact of target & horn design updates

John Back
University of Warwick


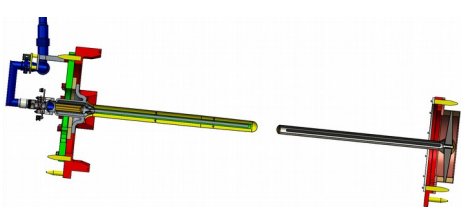
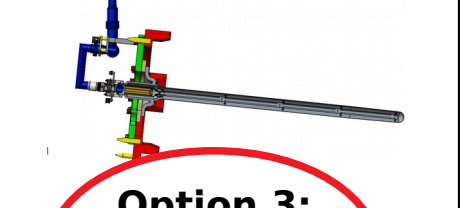
23 July 2020

DUNE-doc-20072

Introduction

- Geant4 simulations of neutrino beamline: graphite target & 3 focusing horns
 - Using geometry based on beam optimization task force (BOTF) report
 - DUNE-doc-2901, Summer 2017
 - 2 m long cylindrical graphite target, extended to 2.2 m: used for TDR fluxes
 - RAL downstream-support (DS) conceptual design: DUNE-doc-5207, Sept. 2017
 - proton beam: 120 GeV, 1.2 MW, 1.1×10^{21} POT/yr; QGSP_BERT hadronic model
- Overview of physics impact of various engineering changes since TDR:
 - Cylindrical graphite target design: cantilever, $L = 1.5 - 1.8$ m, $r = 8$ mm $= 3\sigma_{\text{beam}}$
 - Using cone for upstream horn A inner conductor
 - Allows bigger, stiffer target support (to make target longer)
 - Standardizing horn B and C engineering design
 - Equalization sections, striplines, structural support requirements
- Plots of unoscillated neutrino signal & bkgnd fluxes extrapolated to far detector (40 kt)
- Plots of CP sensitivity and exposure (GLOBES, NuFit 4.0 parameters), using:
 - https://github.com/DUNE/lblpwgtools/tree/master/deprecated/inputs/MVAtoGLOBES/tdr_globes_final

Target concept selection summary: DUNE-doc-15490

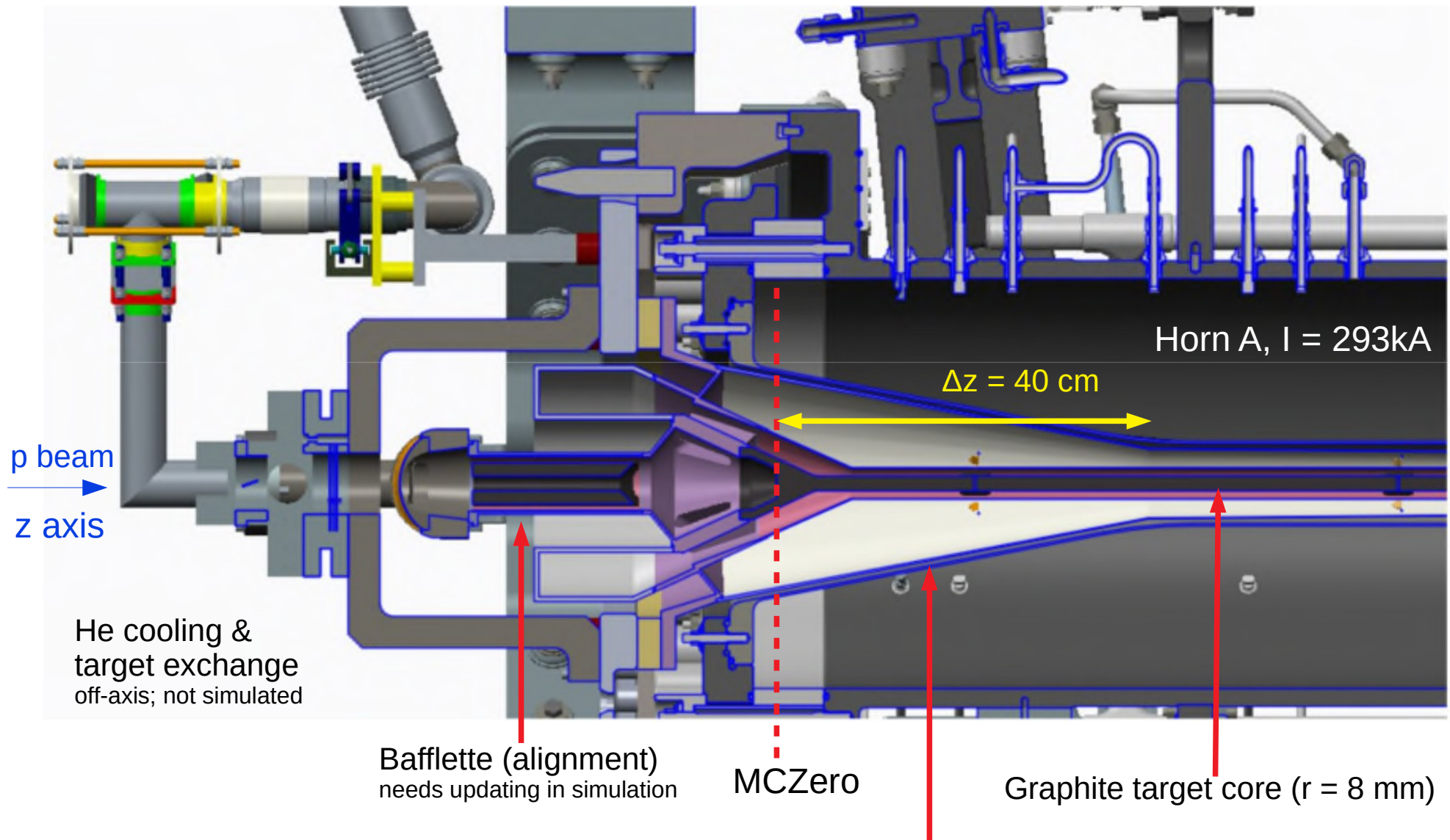
	 <p>Option 1: 1x2m long</p>	 <p>Option 2: 2x1m long</p>	 <p>Option 3: intermediate cantilever</p>
Instantaneous physics	Best instantaneous physics.	Needs an extra 19 days/yr to match option 1.	1.5m needs an extra 19 days/yr (13 days/yr at 1.6m).
Engineering performance	High heat load. Unstable until supported.	High heat load but divided between 2 targets	Pushing at the limits on cantilever length.
Manufacturability	Difficult to make long tubes. DS support adds complexity.	2 nd target low-mass manifold is complex.	Difficult to make long tubes.
Ease of remote maintenance	≈3 weeks exchange time, DS support adds time and risk.	≈2 weeks exchange time, 2 nd target adds some time and risk.	≈1 week exchange time, lowest complexity and risk.
Cost and schedule impacts	DS support somewhat increases cost and time.	2 nd target greatly increases cost and time.	Cheapest and fastest to produce.

LBNF target conceptual design selection review: 24 July 2019 @ Fermilab

Target performance = physics x reliability

⇒ Consensus to use option 3: cantilever with L = 1.5 m (prototype) up to 1.8 m (goal)

Target and Horn A integration



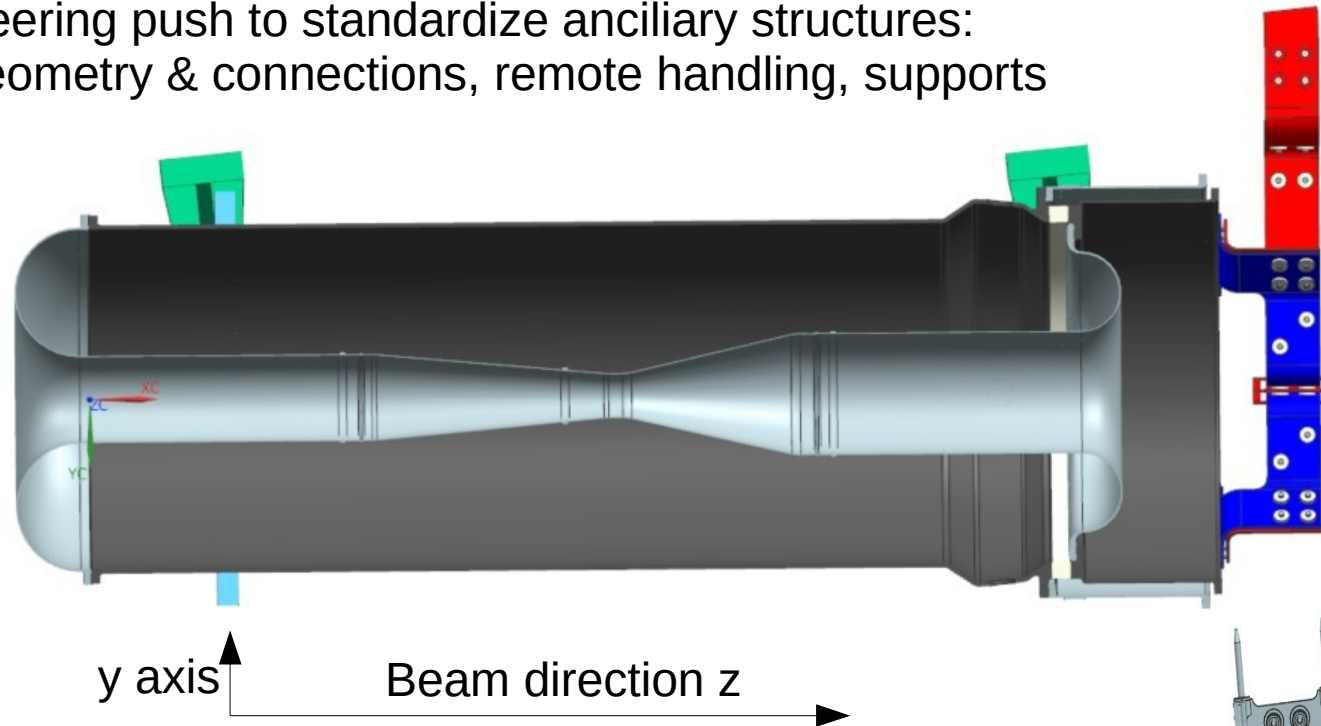
Horn A inner conductor cone ($r_{\text{base}} = 14 \text{ cm}$, $\Delta z = 40 \text{ cm}$)
to allow space for upstream target support structure

Horn B (& C) standardization

Need to reduce heating of current equalization sections.

Major engineering push to standardize ancillary structures:
stripline geometry & connections, remote handling, supports

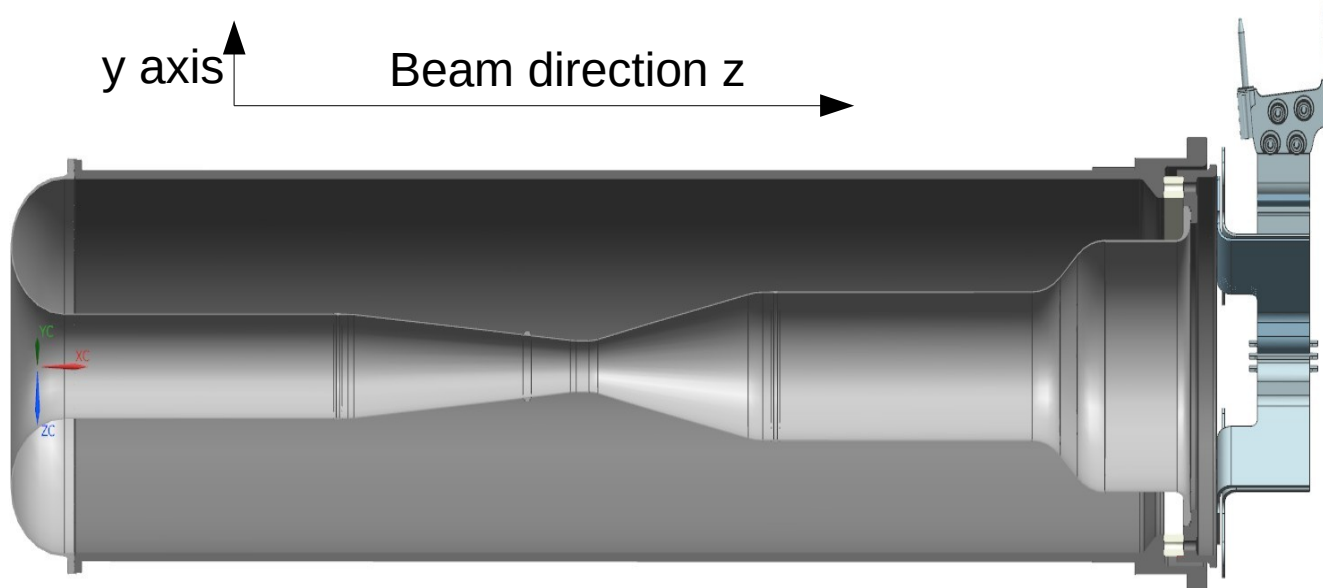
TDR
conceptual
enr. design
 $r_{oc} = 63.4 \text{ cm}$



Striplines
not simulated

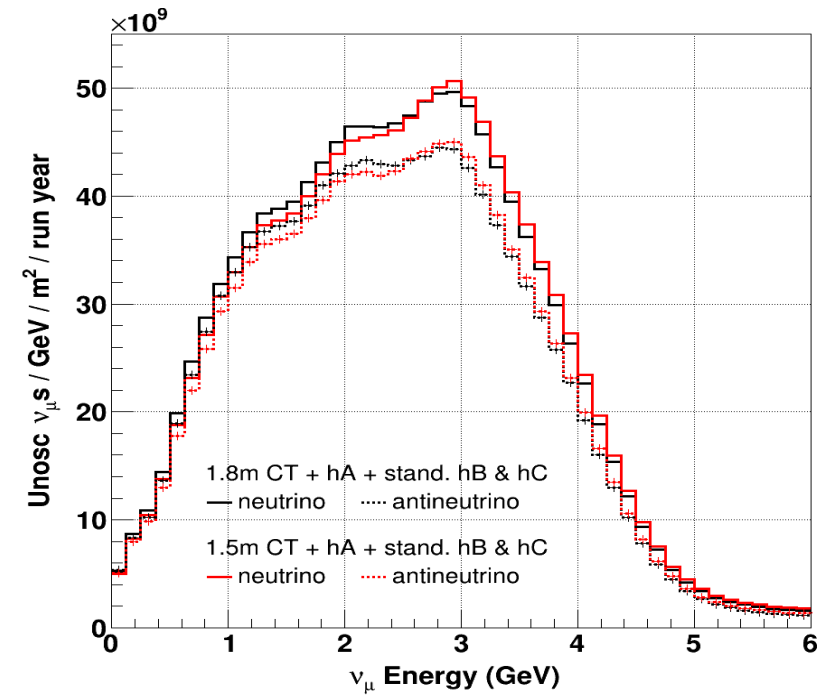
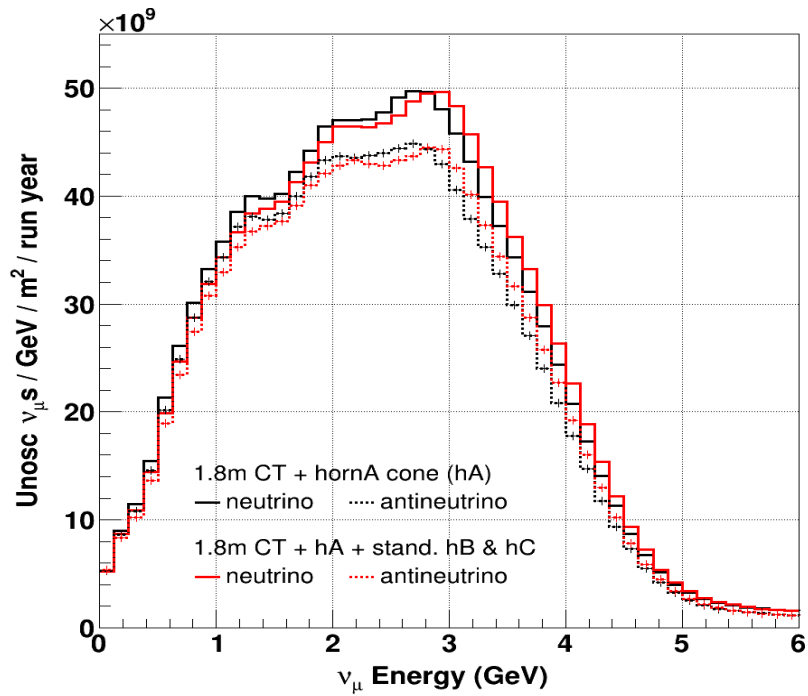
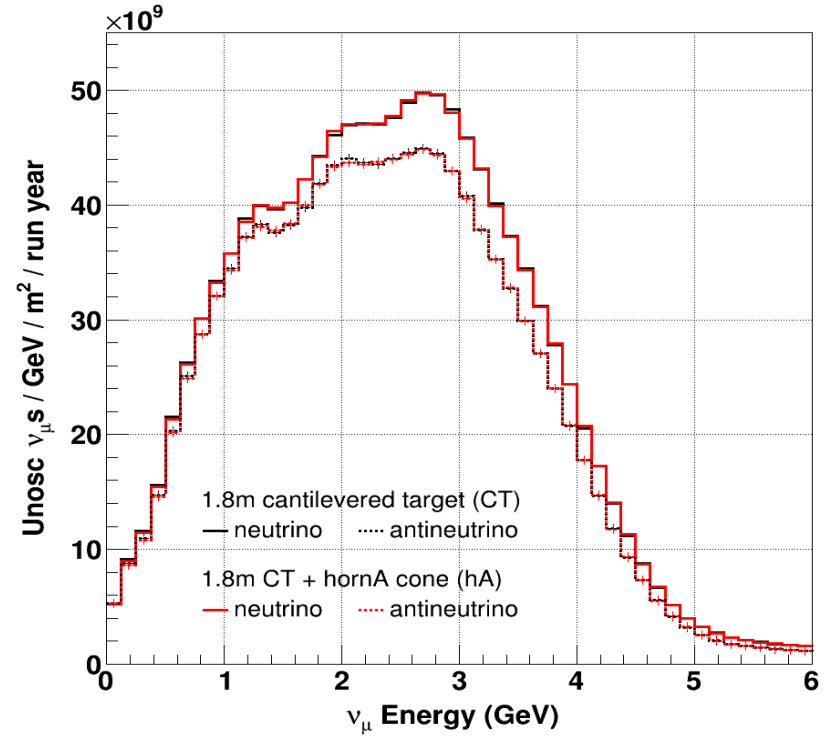
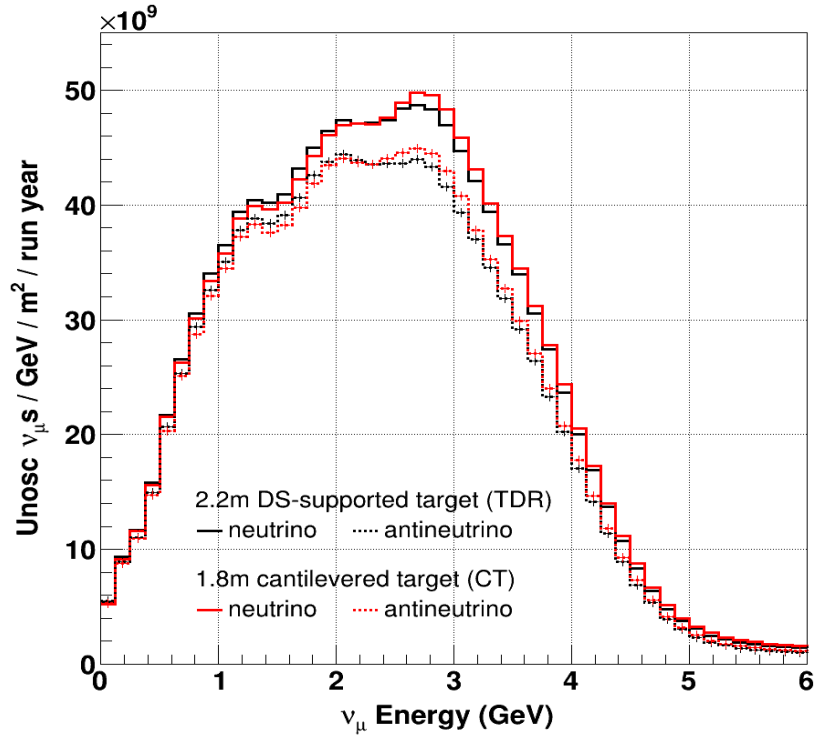
$I_B = I_C = 293 \text{ kA}$

Current
standardized
enr. design
 $r_{oc} = 60 \text{ cm}$
maximum radius

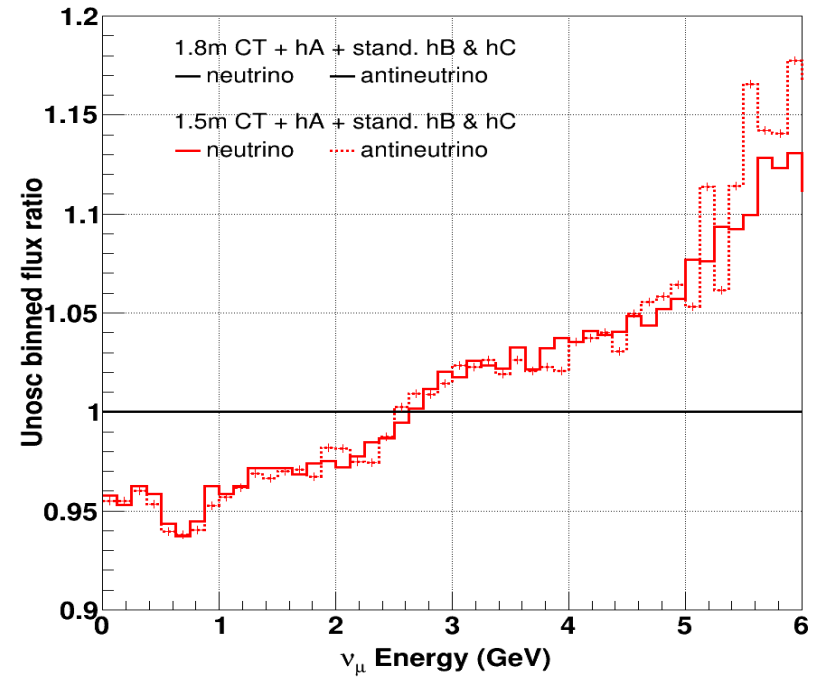
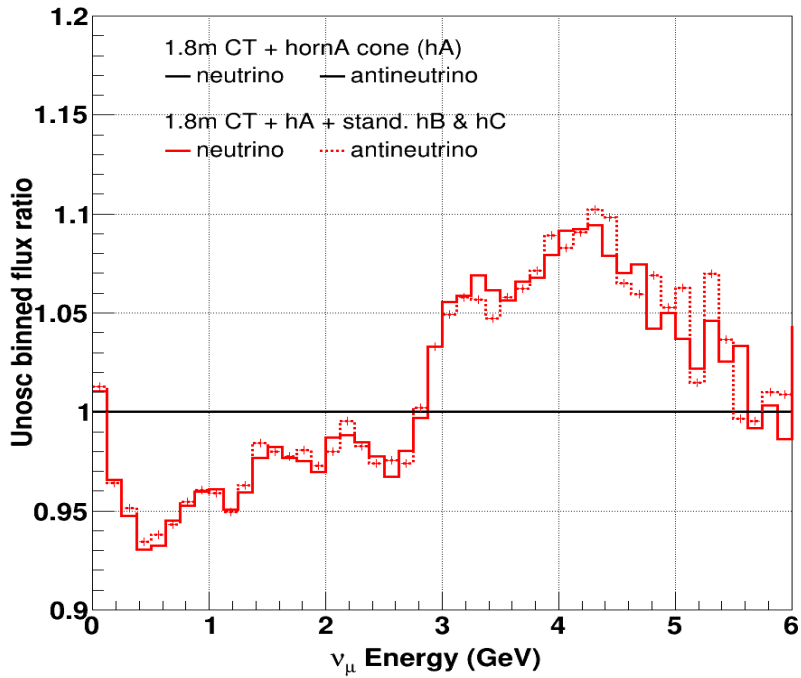
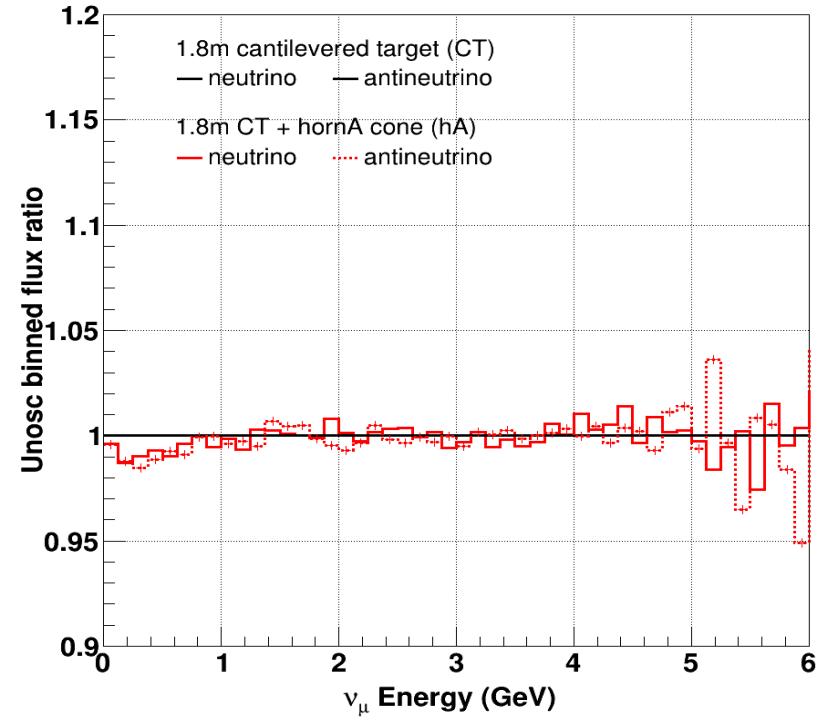
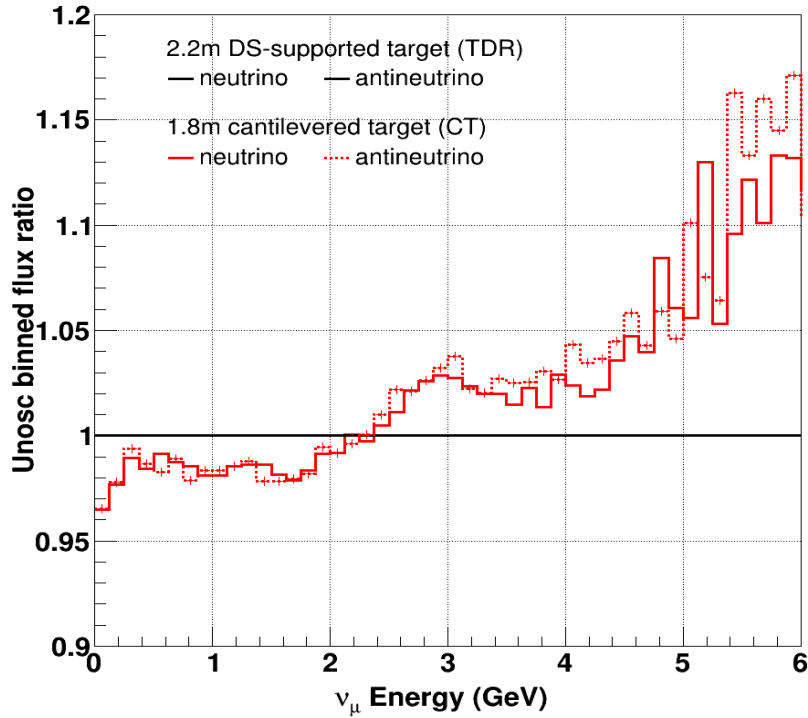


Striplines & **B**
fields included

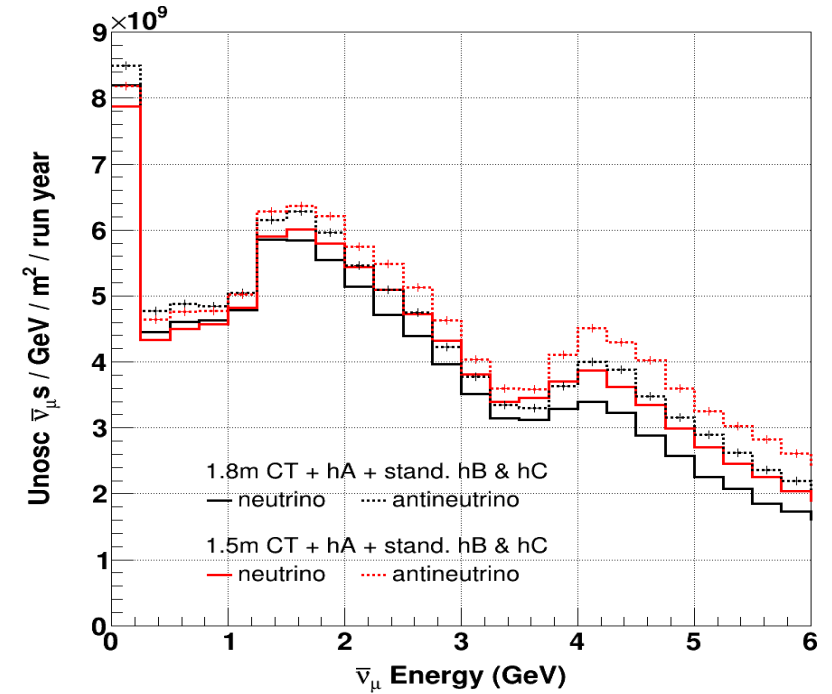
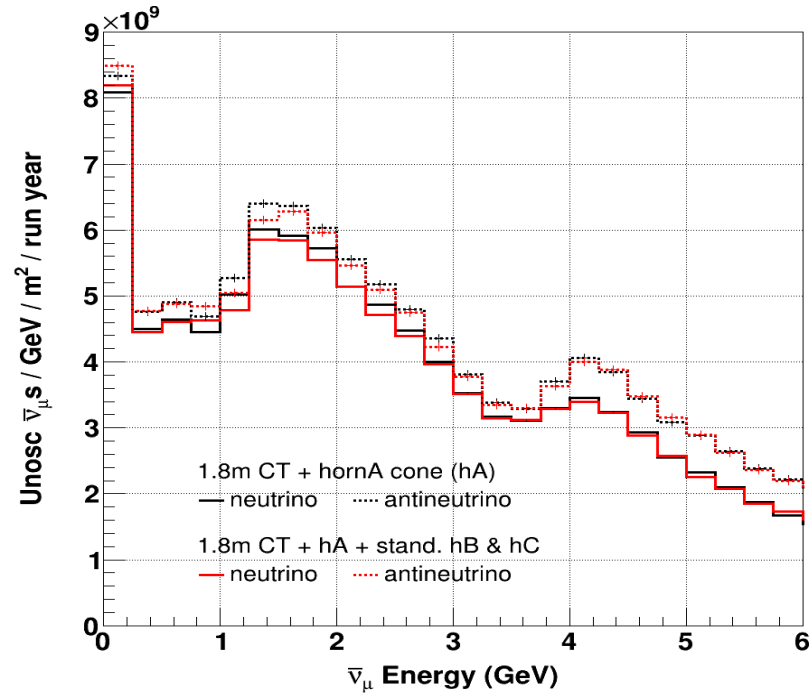
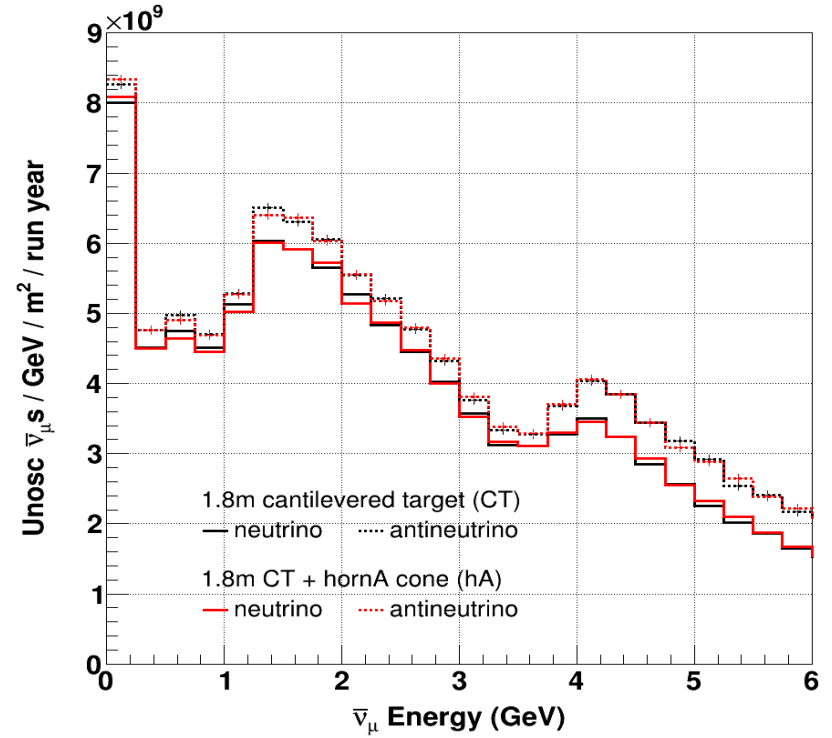
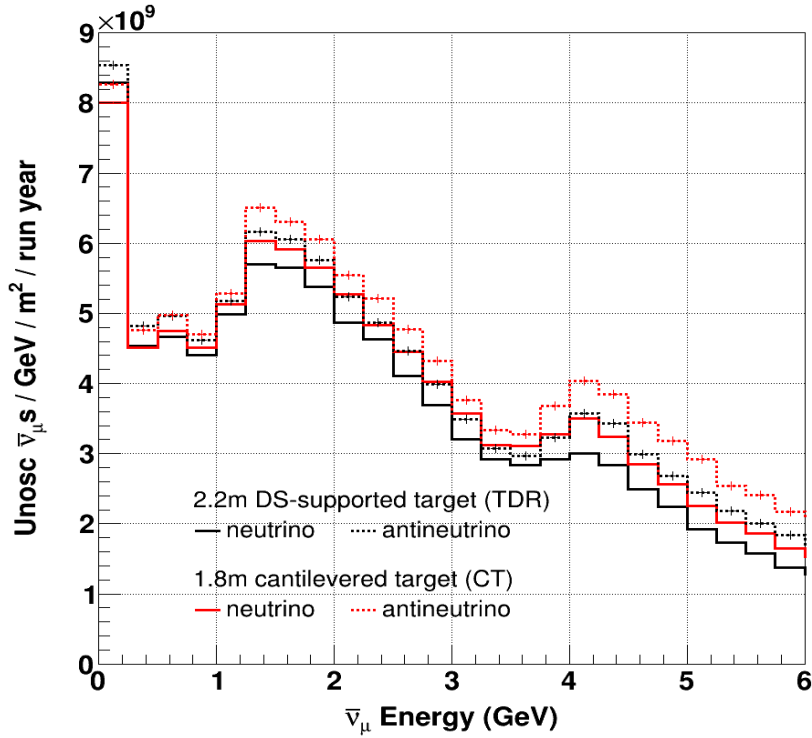
Signal: ν_μ (solid) & anti- ν_μ (dotted)



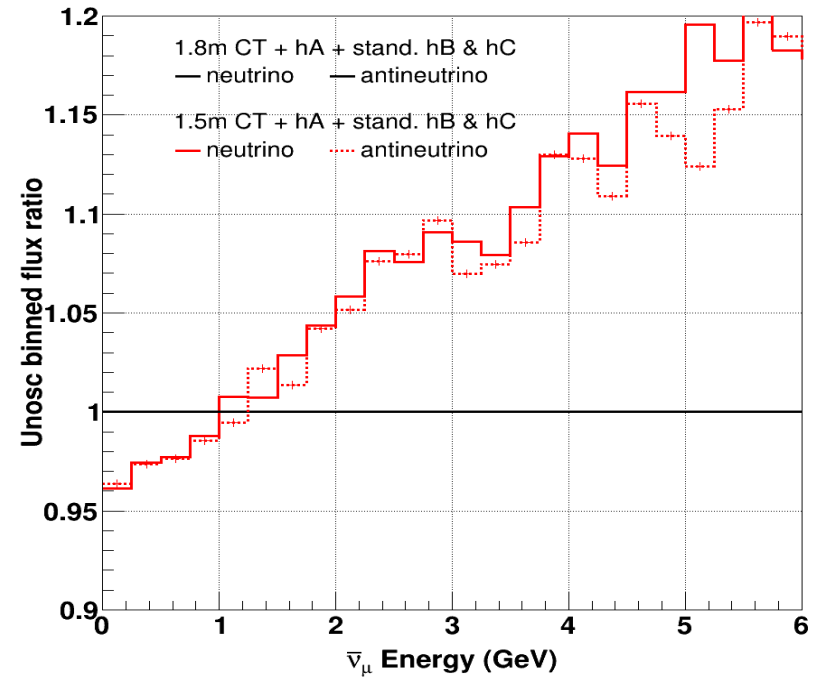
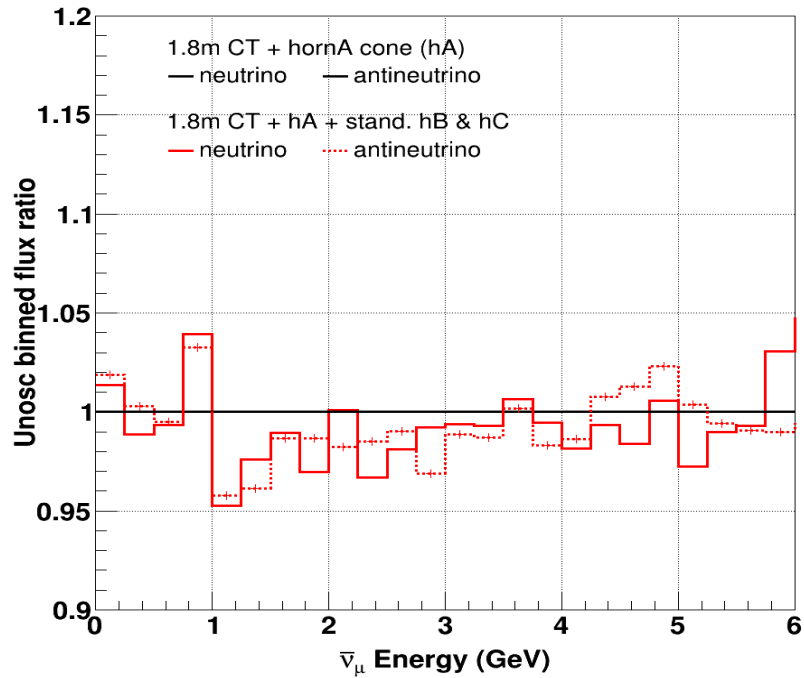
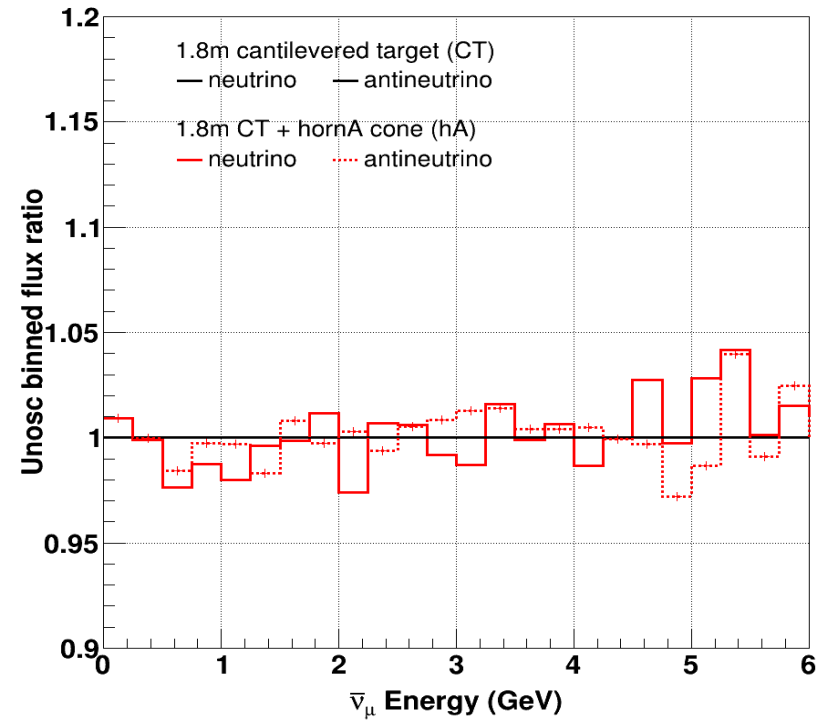
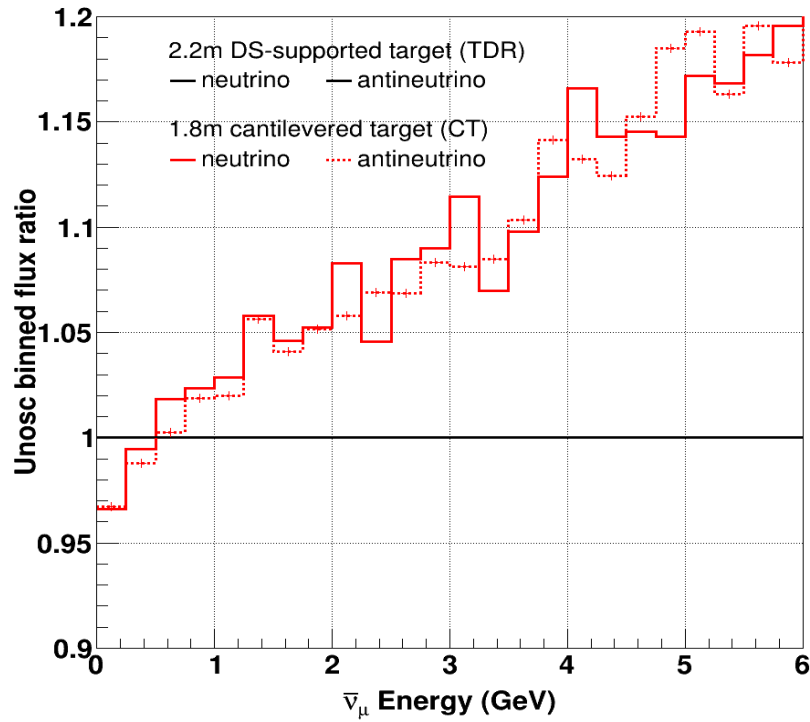
Signal: ν_μ (solid) & anti- ν_μ (dotted)



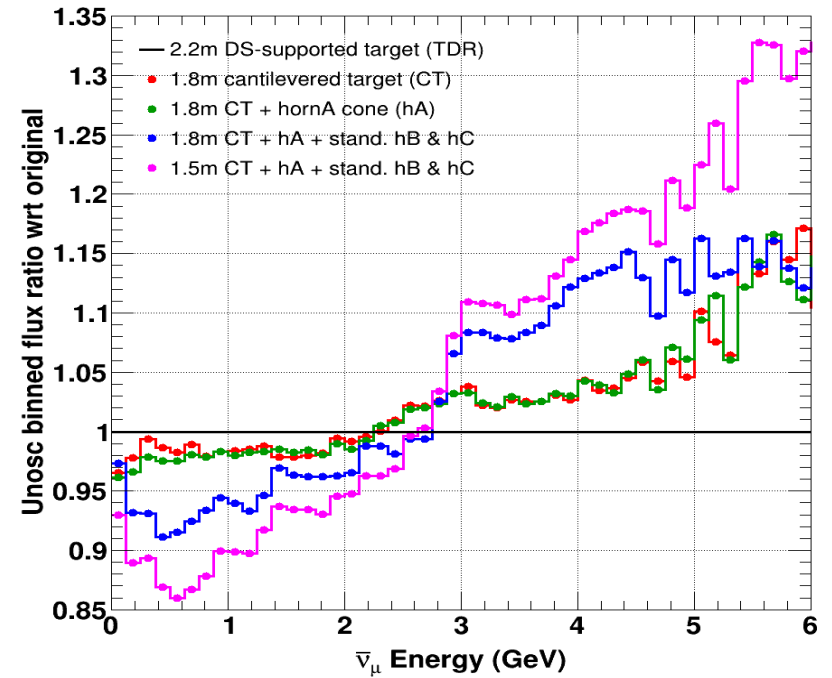
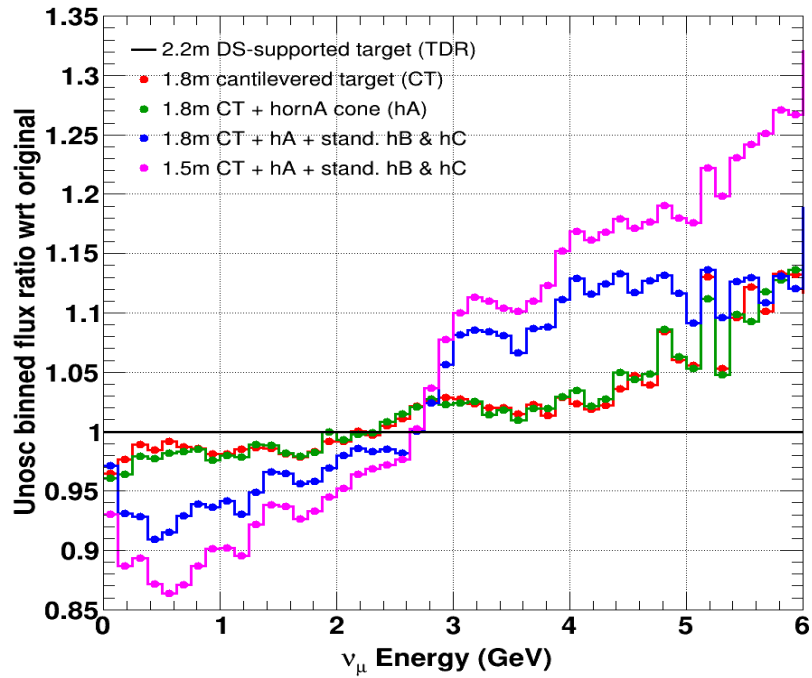
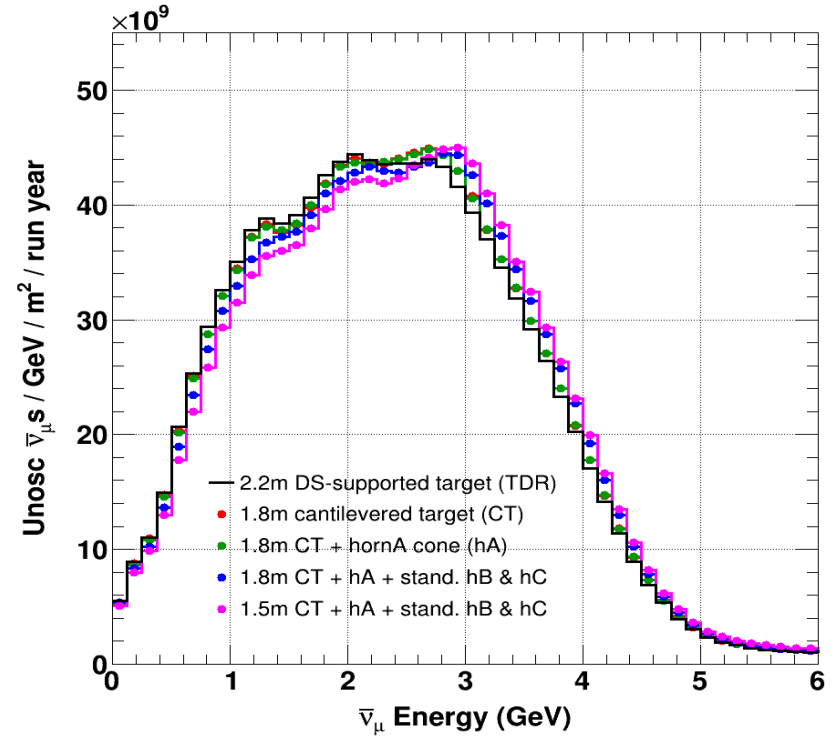
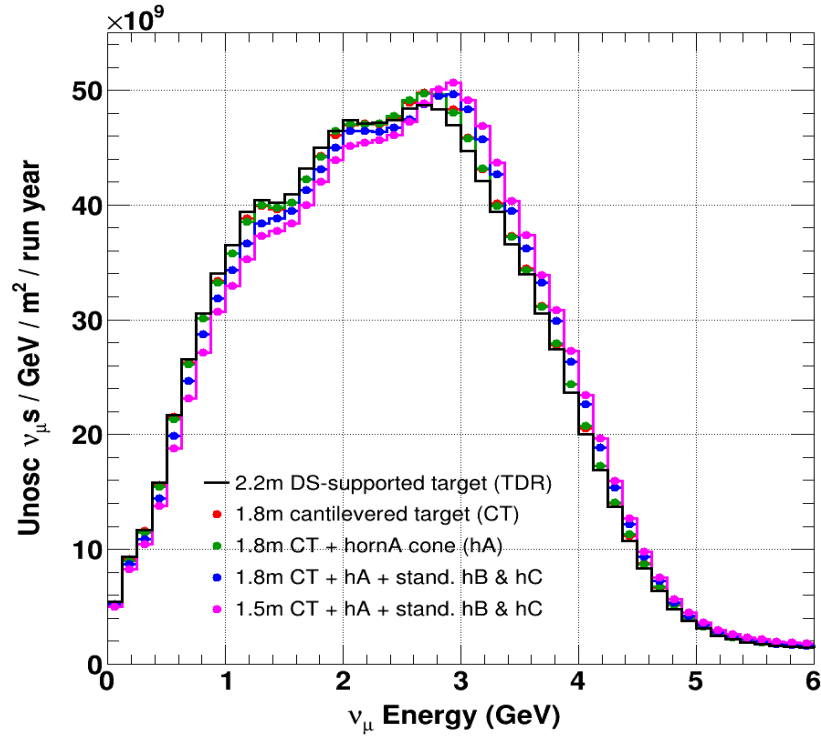
Wrong-sign bkgnd: anti- $\bar{\nu}_\mu$ (solid) & ν_μ (dotted)



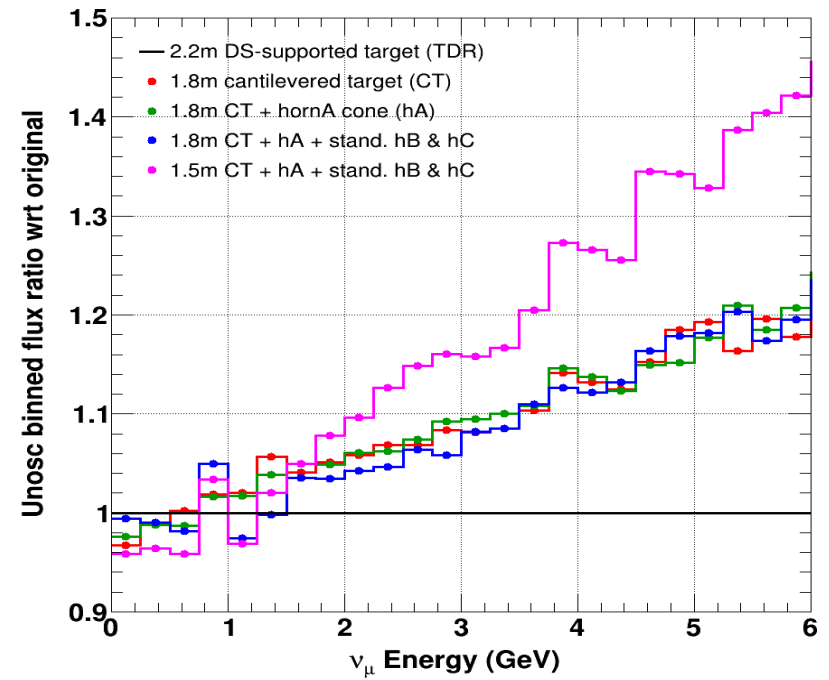
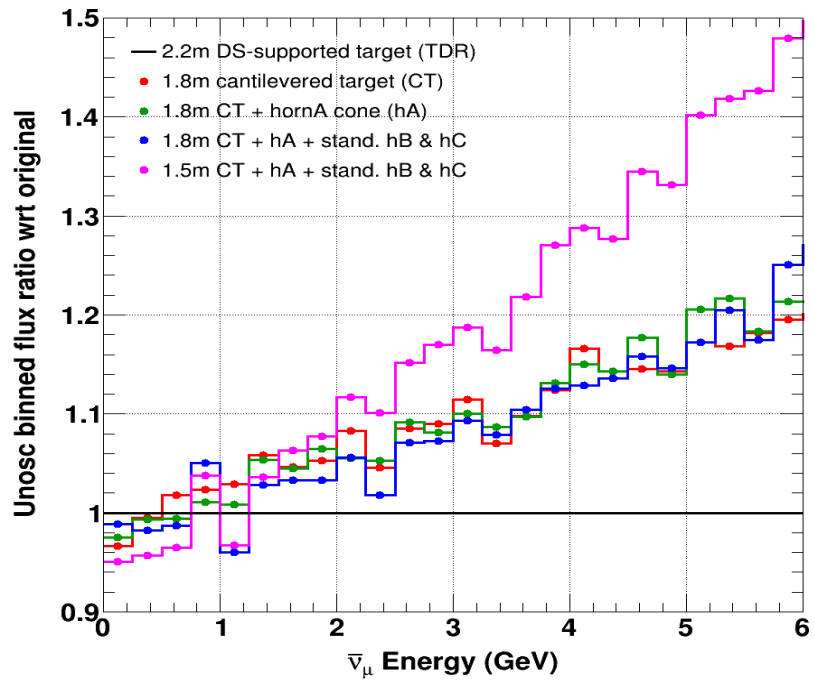
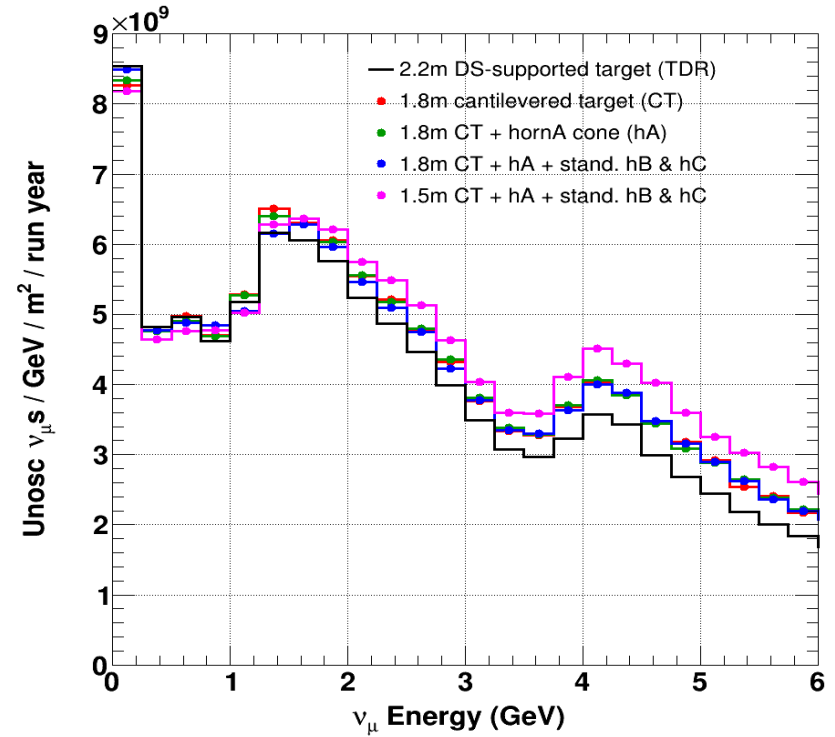
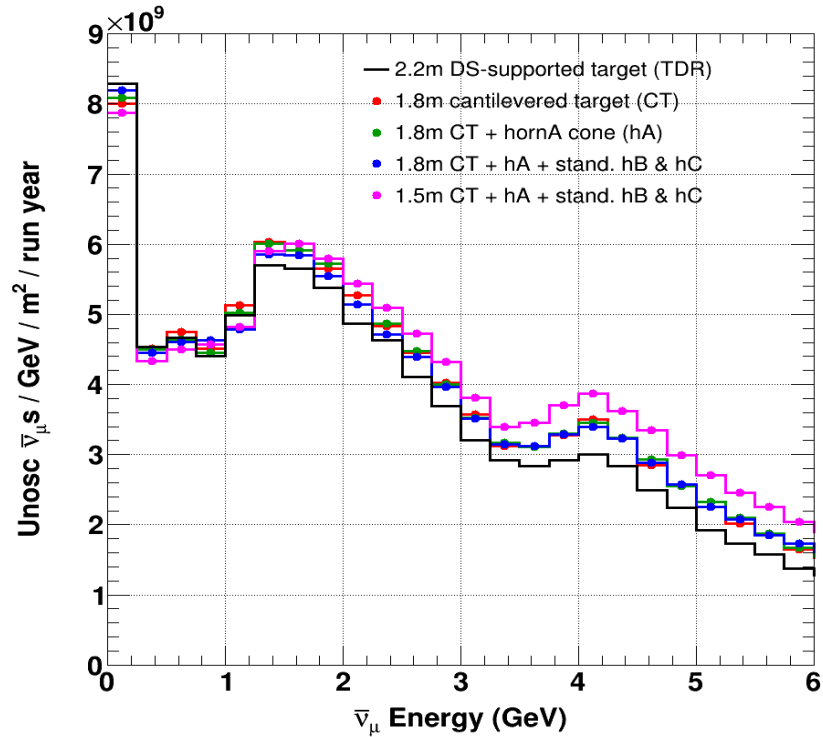
Wrong-sign bkgnd: anti- $\bar{\nu}_\mu$ (solid) & ν_μ (dotted)



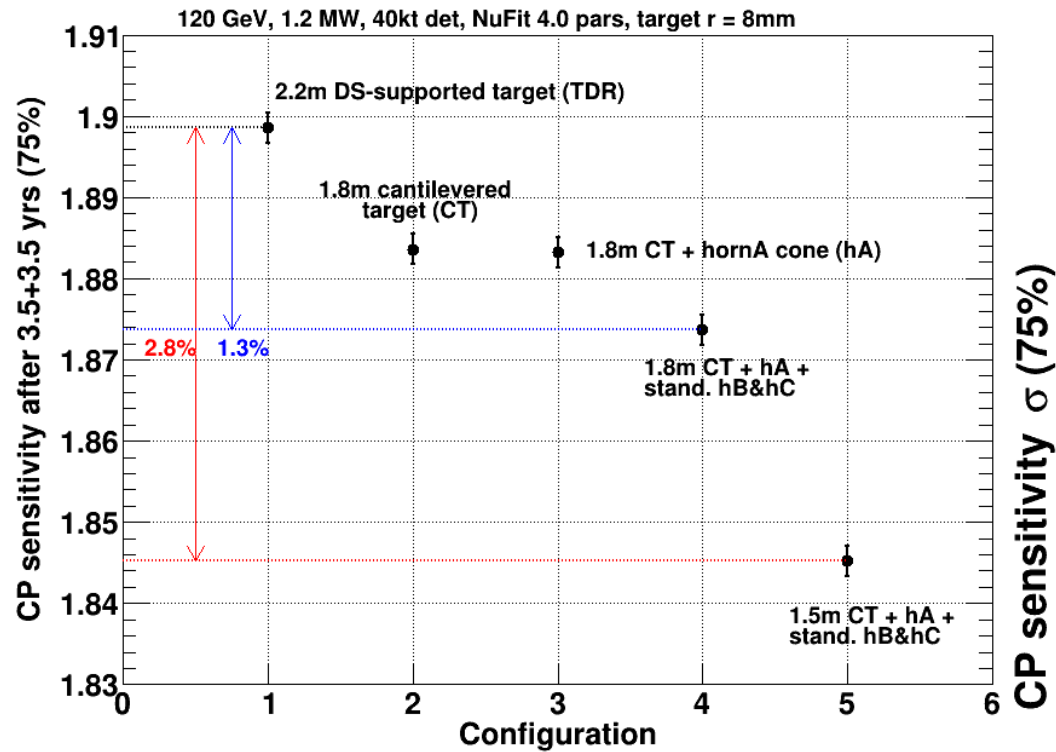
Signal: ν_μ (left) & anti- ν_μ (right)



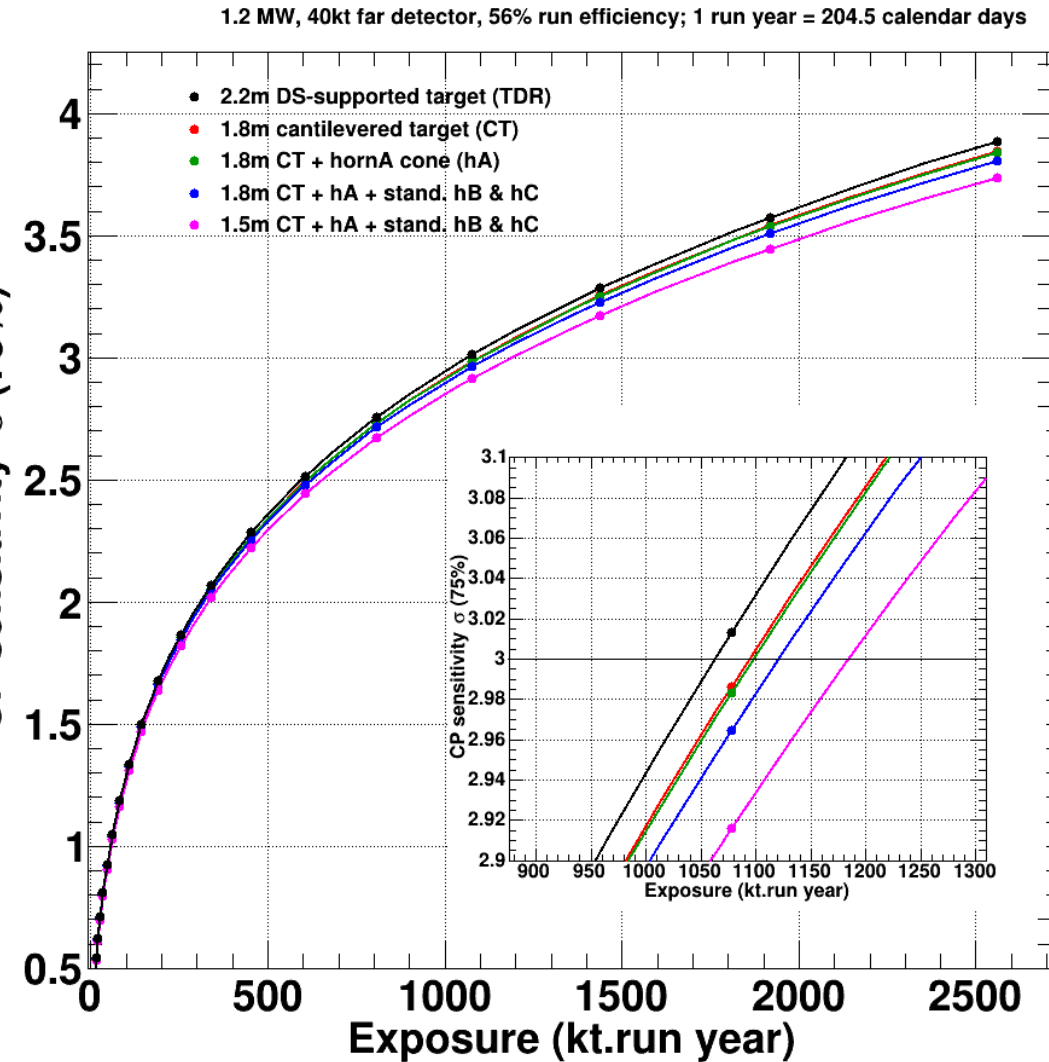
Wrong-sign bkgnd: anti- ν_μ (left) & ν_μ (right)



CP sensitivities (75% δ_{CP} range) and exposures



Configuration	Extra time per run year (1 run year = 204.5 days)
1.8m cantilevered target (CT)	6 days (3 %)
1.8m CT + horn A cone (hA)	6 days (3 %)
1.8m CT + hA + standardized horns B & C	11 days (5 %)
1.5m CT + hA + standardized horns B & C	23 days (11 %)



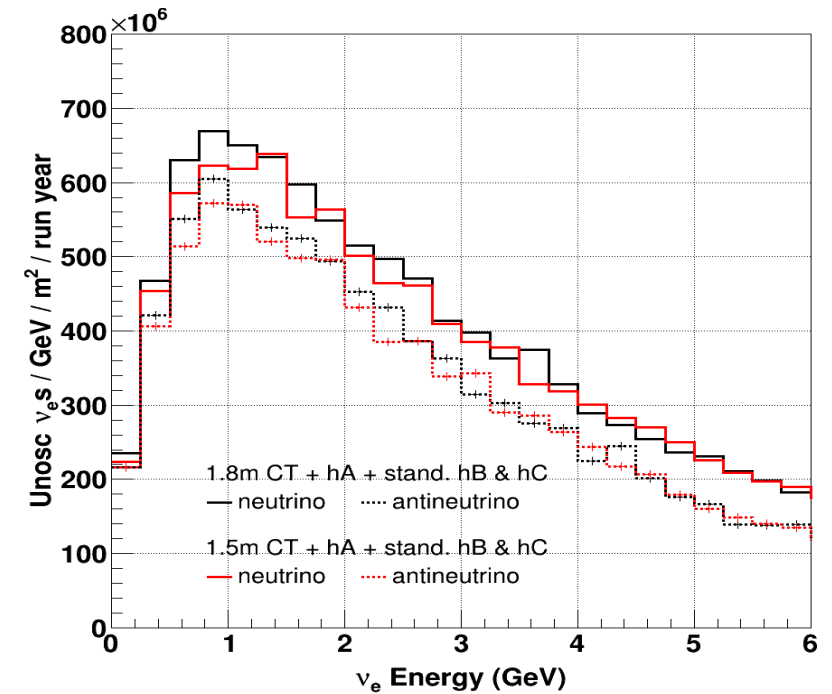
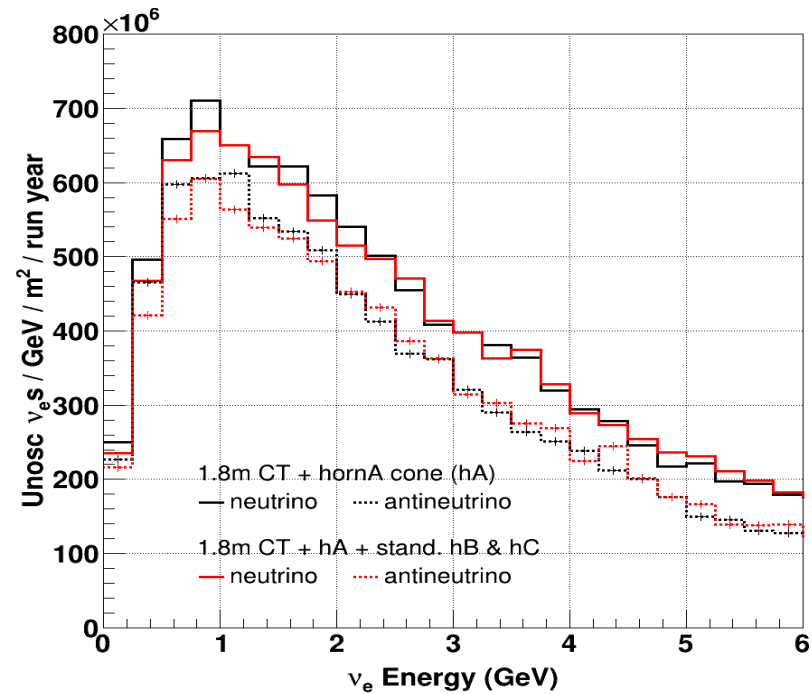
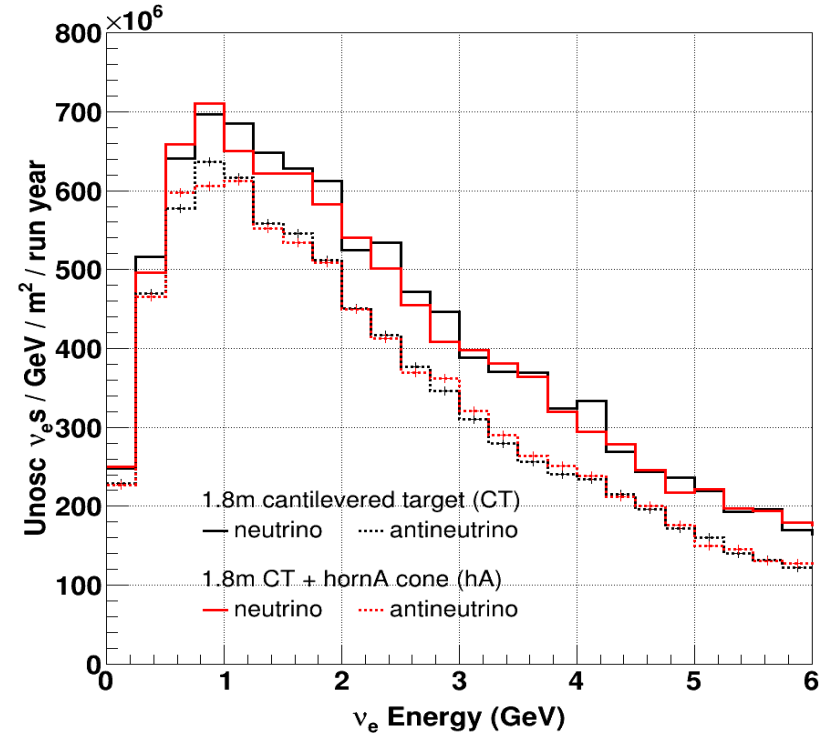
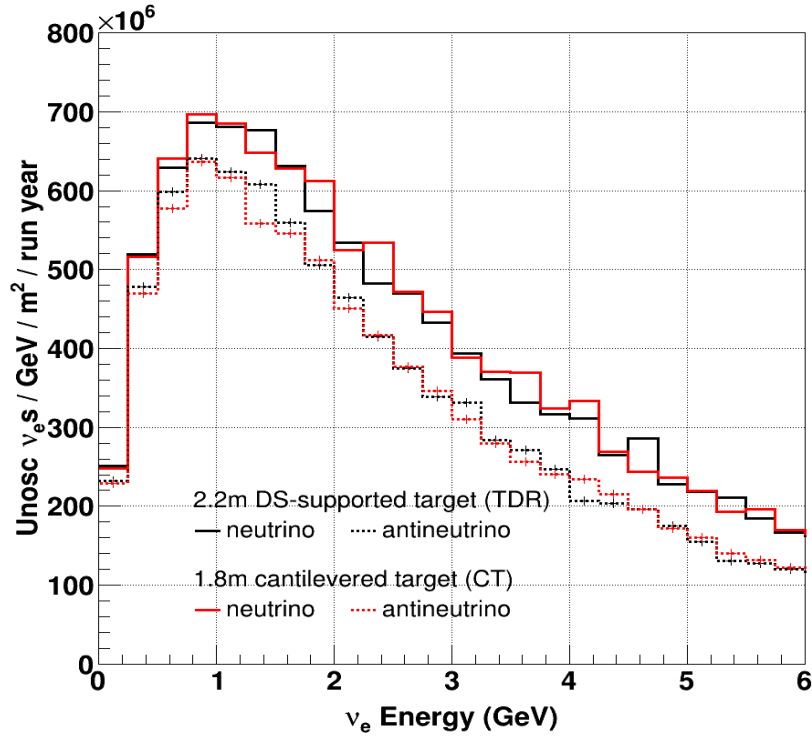
Approx extra time needed to reach 3σ level of CP exposure performance of TDR 2.2 m target

Excludes target exchange downtime variations

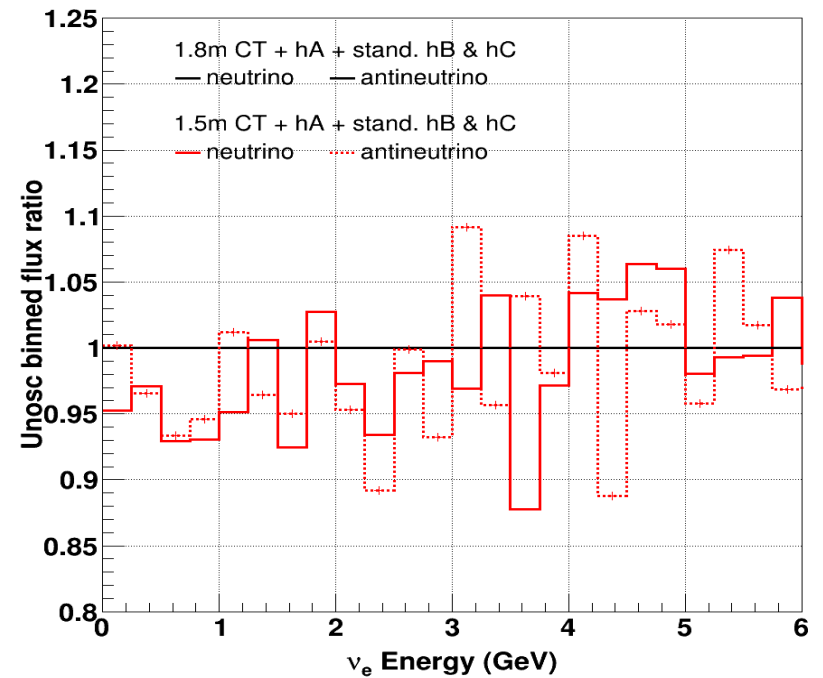
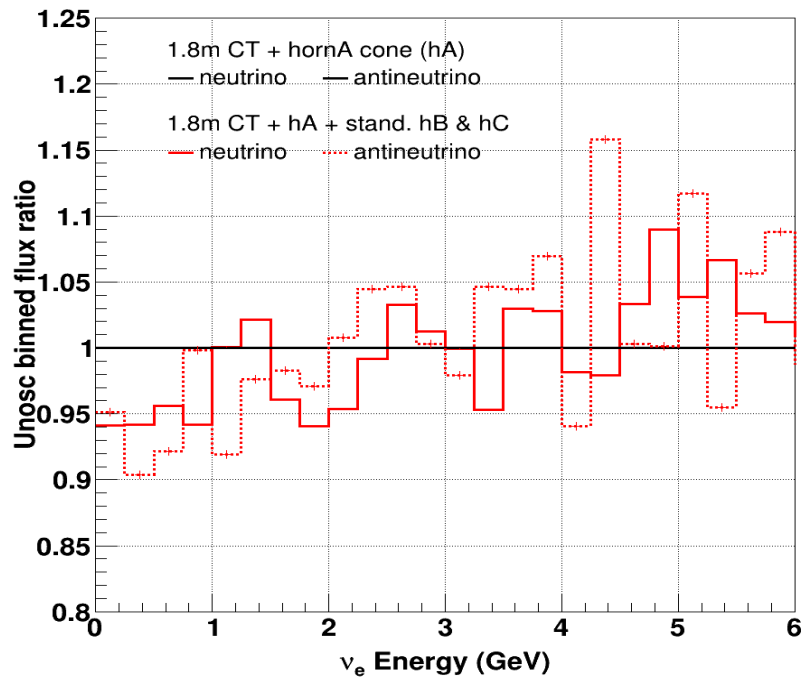
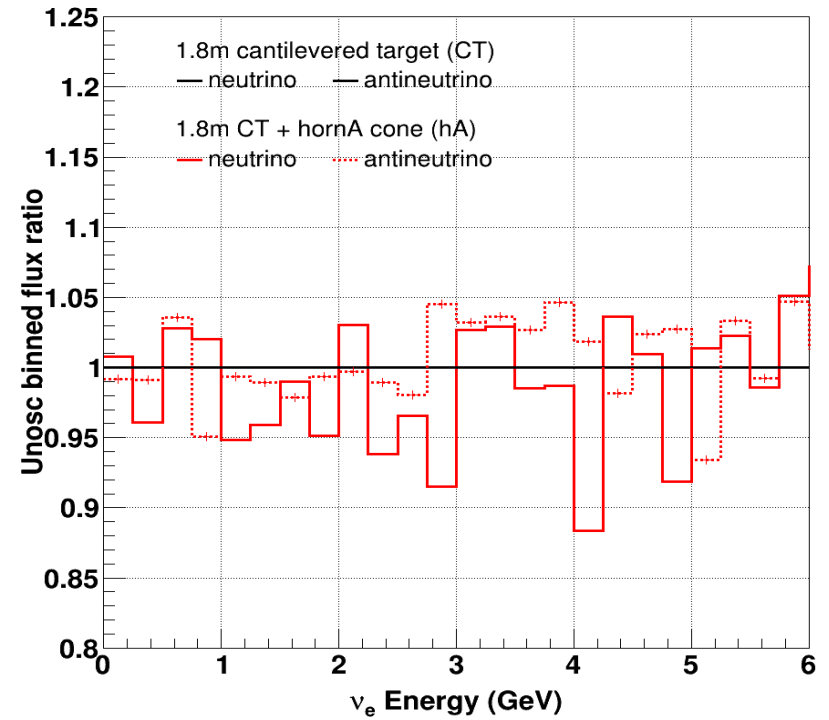
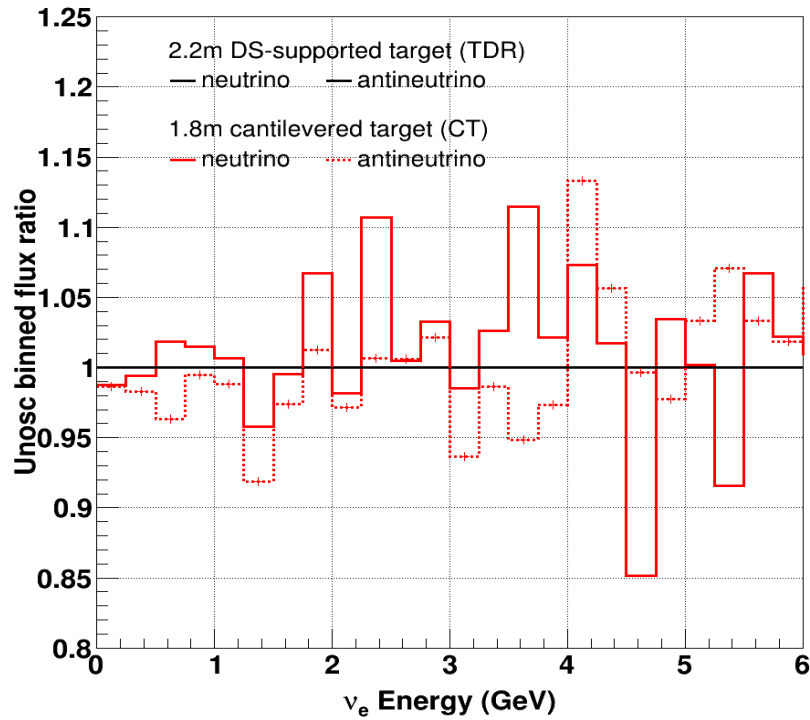
Summary

- Evolution of target & horn engineering design has affected physics performance:
 - Loss (gain) of signal flux at low (high) neutrino energy
 - Increase of wrong-sign backgrounds, especially at high energy
- Biggest change from target length reduction:
 - TDR L = 2.2 m has more engineering (reliability) risks: ~21 days exchange downtime
 - Cantilevered target has lower risk & cost, more reliable: ~7 days exchange downtime
 - Production target (aim) L = 1.8 m needs ~+6 days/run year to match TDR exposure (same horns)
 - Cantilevered L = 1.8 m with standardized horns ~ +11 days/run year to match TDR exposure
 - This is the current target & horn design we are aiming for
 - Initial target prototype, cantilevered L = 1.5 m ~ +23 days/run year to match TDR exposure
- Horn A upstream inner conductor cone gives no significant change:
 - Potentially allows target length up to 1.8 m $\sim 4\lambda_{\text{int}}$ (max limit from gravitational bending)
- Horn B & C standardization requirements increase exposure time by an extra ~5 days/run year:
 - Striplines & their B fields give ~1% signal flux reduction (DUNE-doc-19219)
 - Varying horn lengths & foci does not significantly improve performance (DUNE-doc-19885)

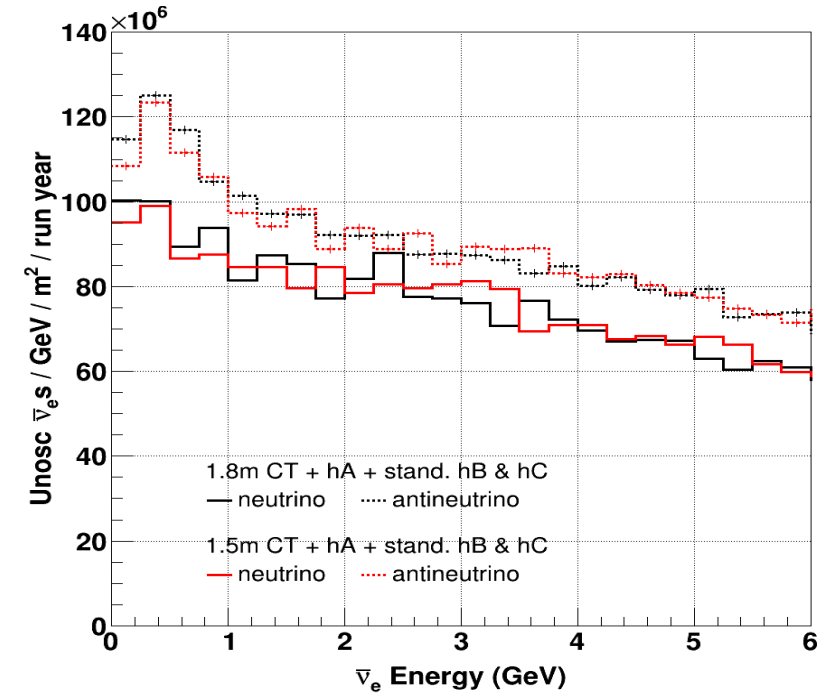
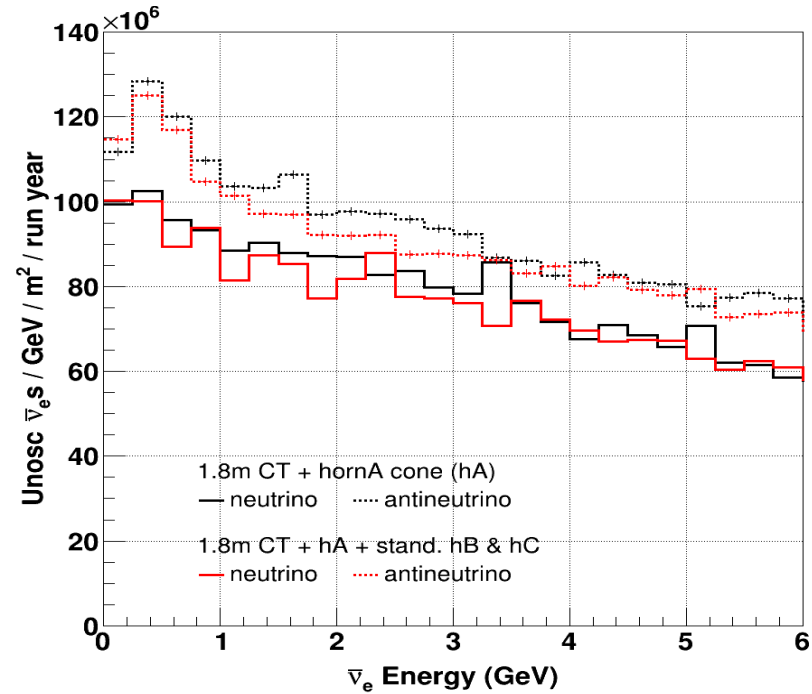
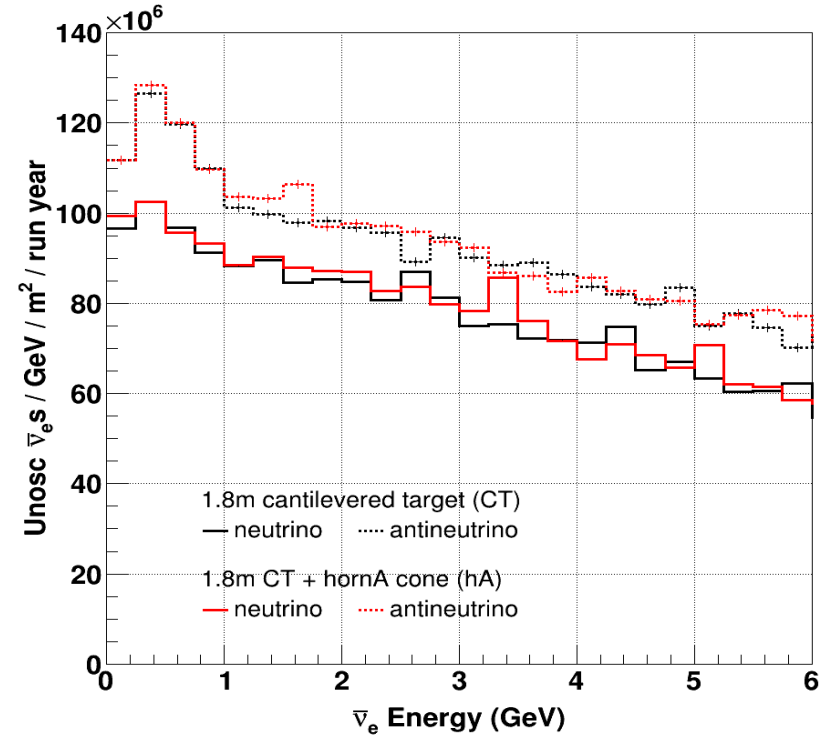
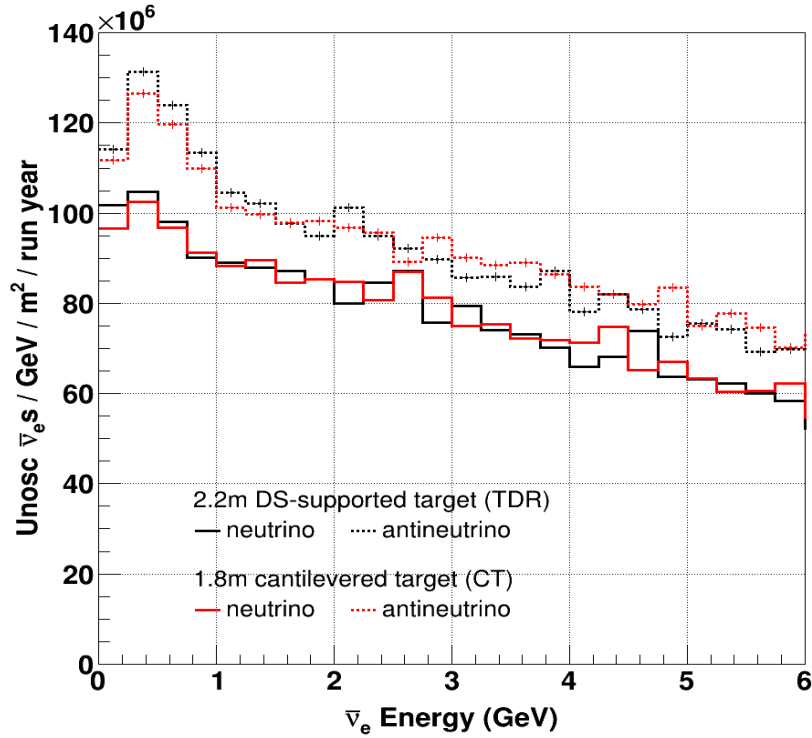
$\nu_\mu \rightarrow \nu_e$ (solid) & anti- $\nu_\mu \rightarrow$ anti- ν_e (dotted) bkgnd



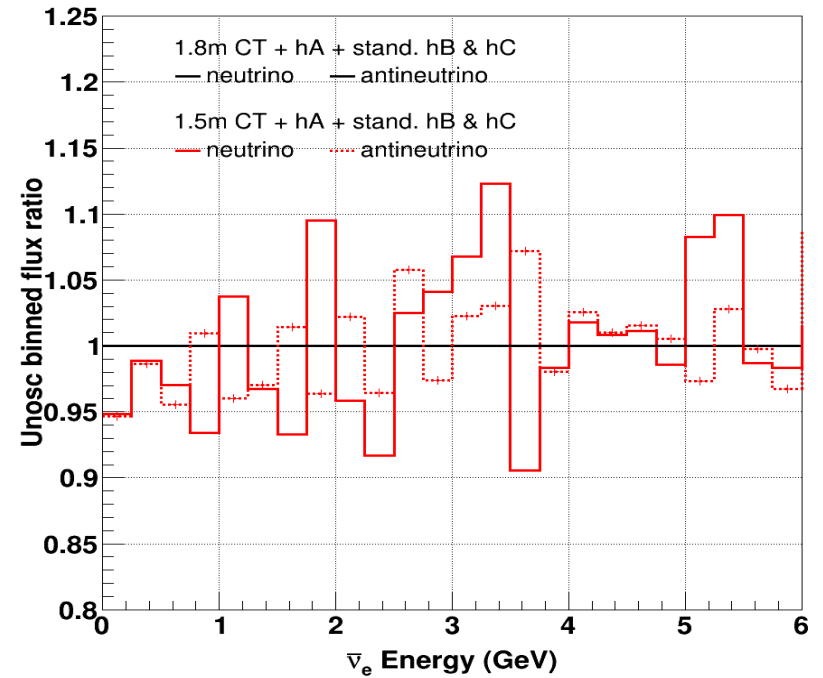
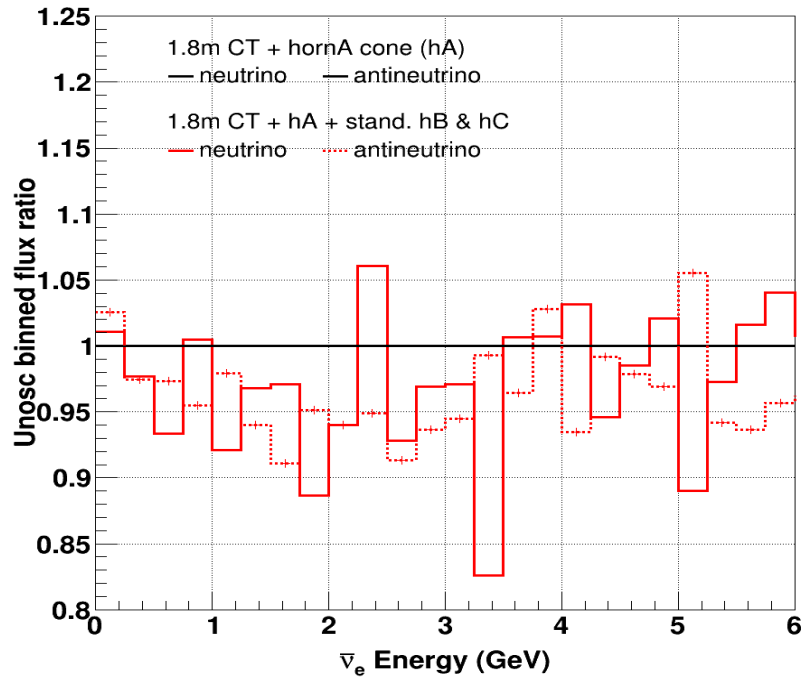
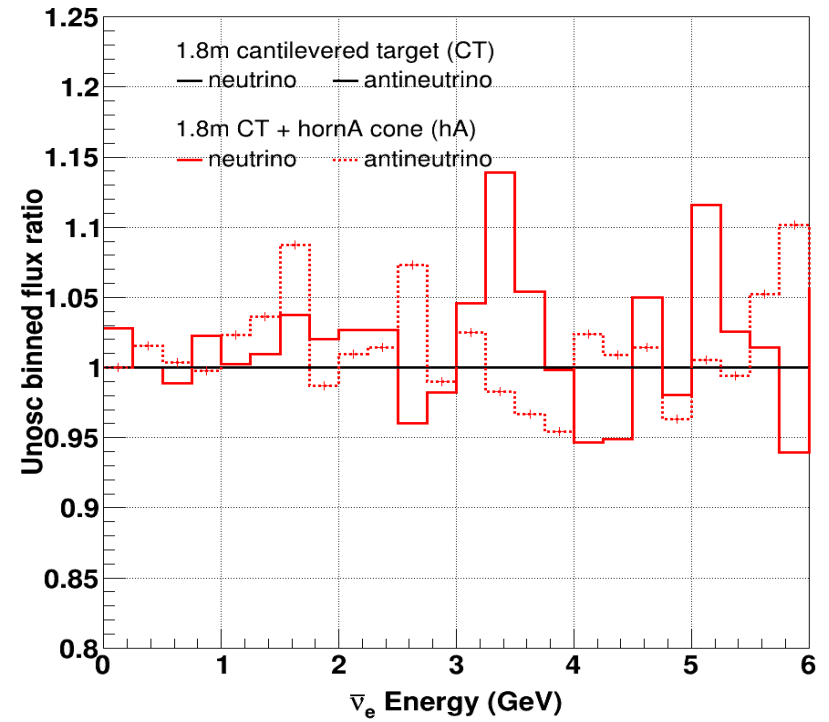
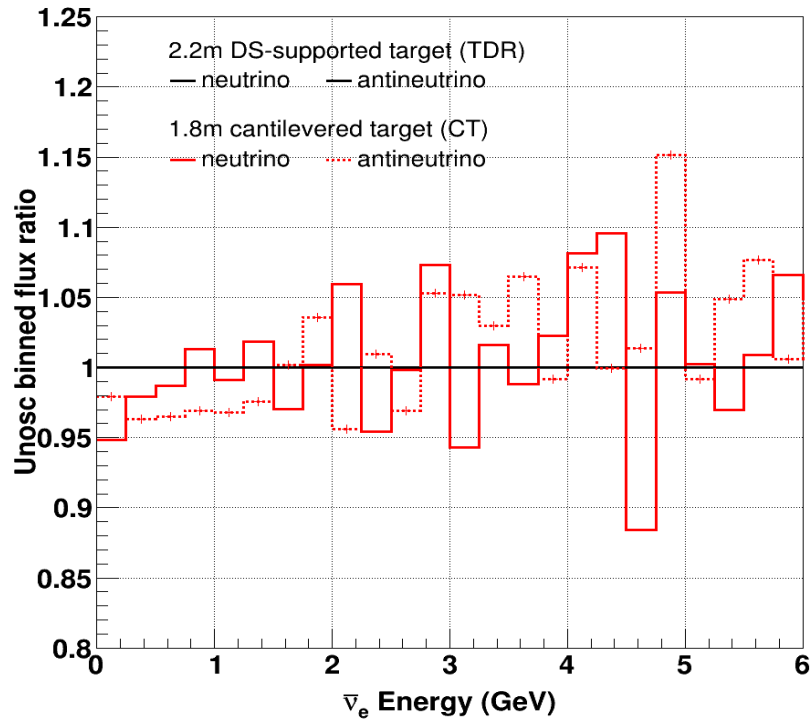
$\nu_\mu \rightarrow \nu_e$ (solid) & anti- $\nu_\mu \rightarrow$ anti- ν_e (dotted) bkgnd



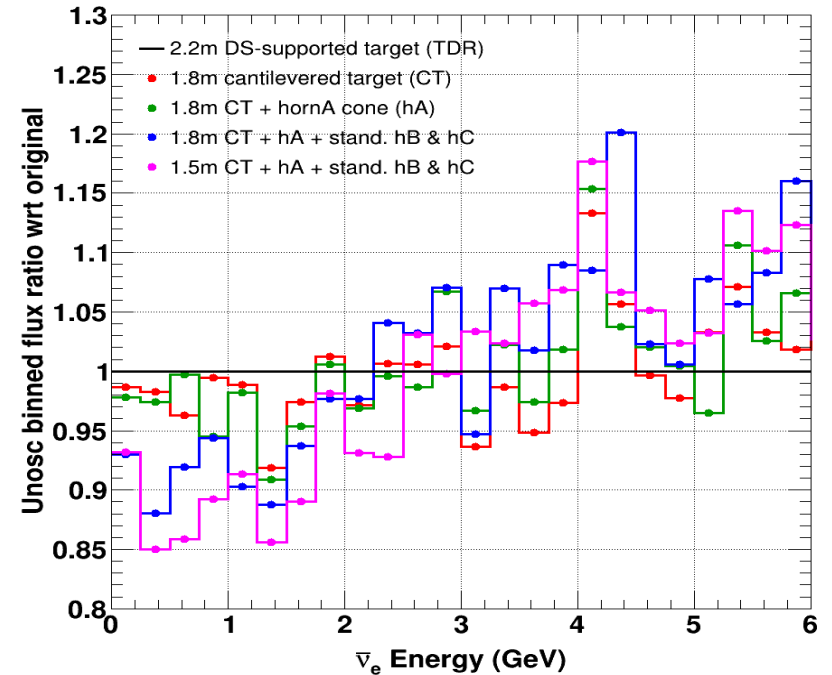
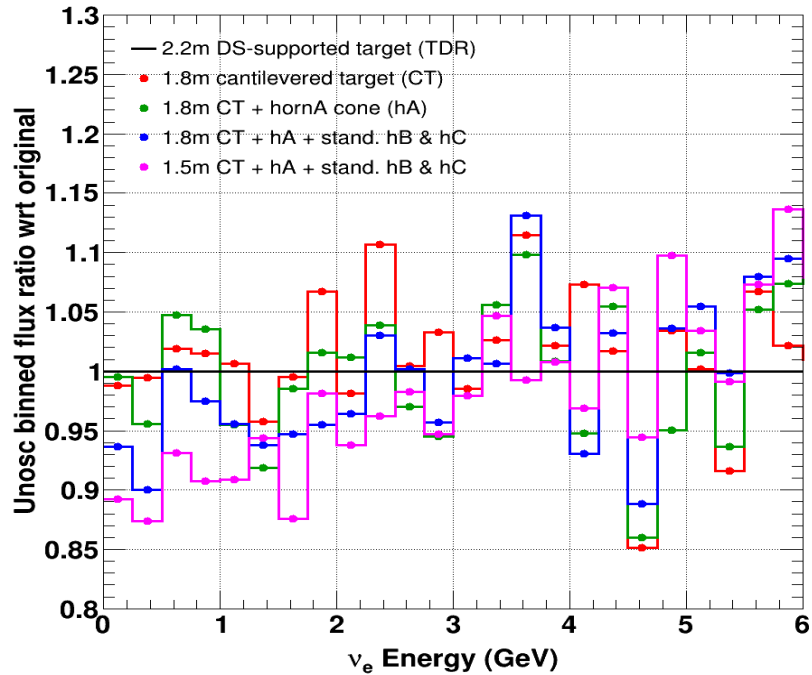
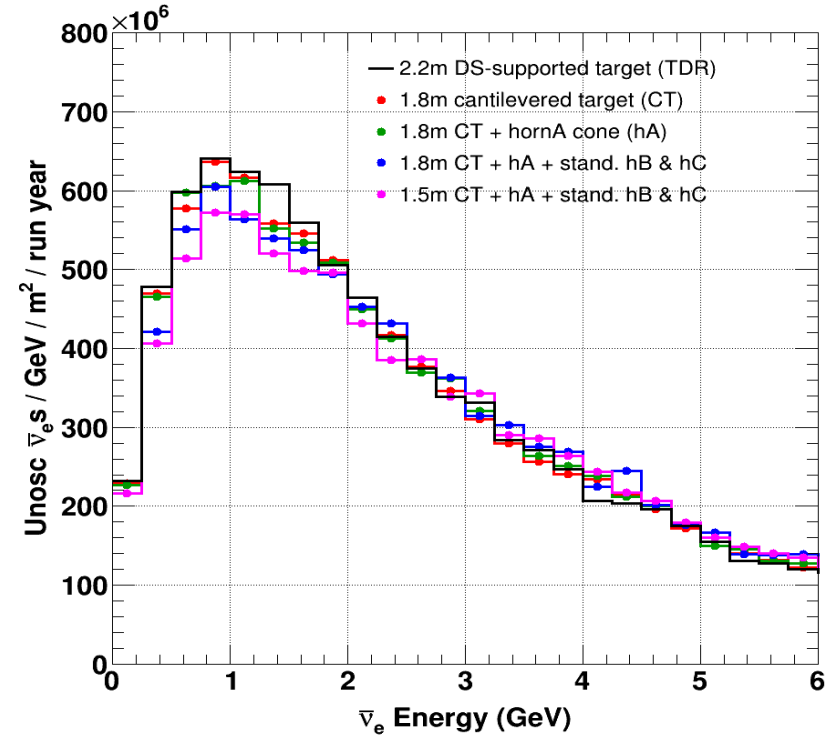
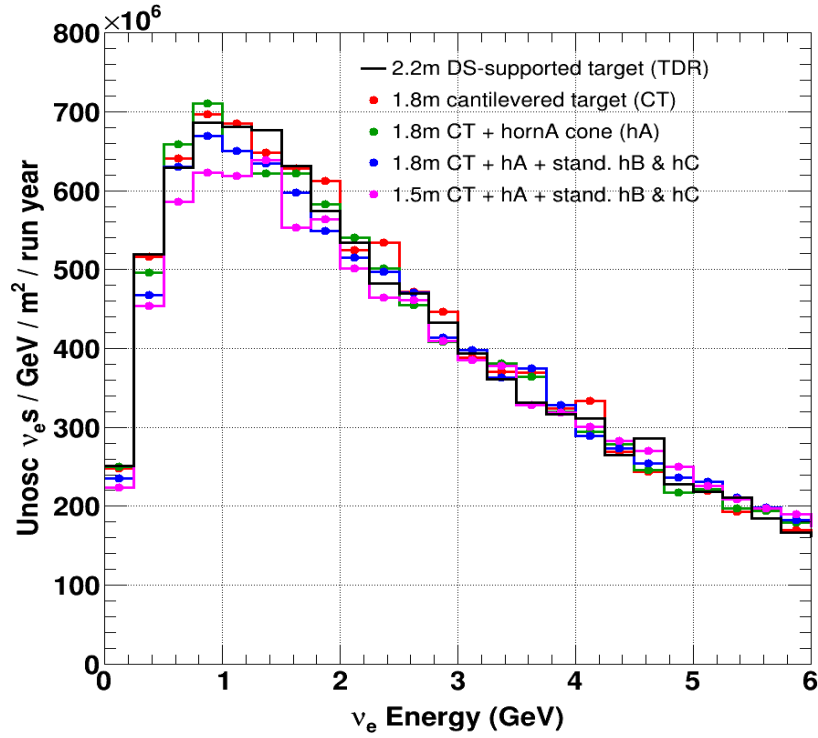
$\nu_\mu \rightarrow \text{anti-}\nu_e$ (solid) & $\text{anti-}\nu_\mu \rightarrow \nu_e$ (dotted) bkgnd



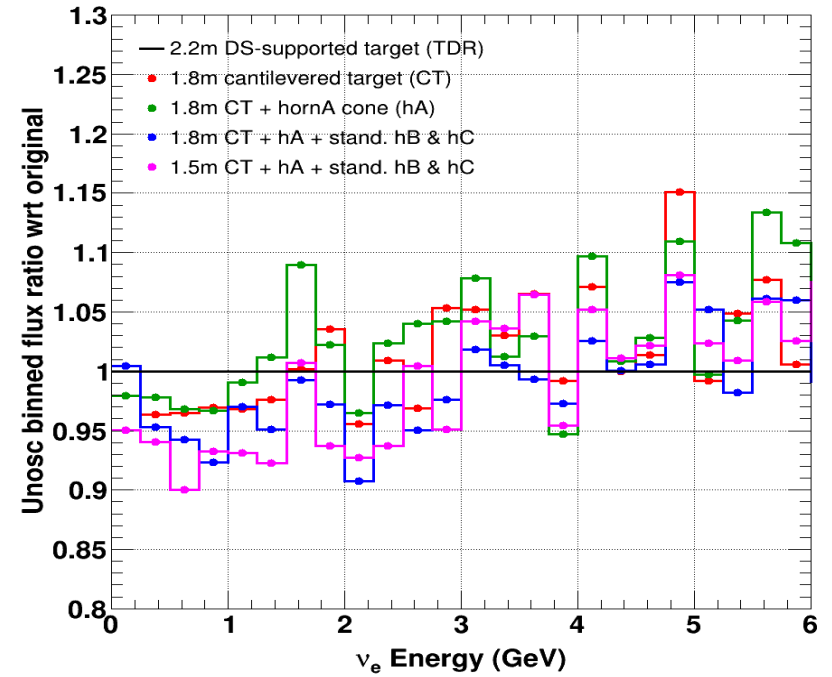
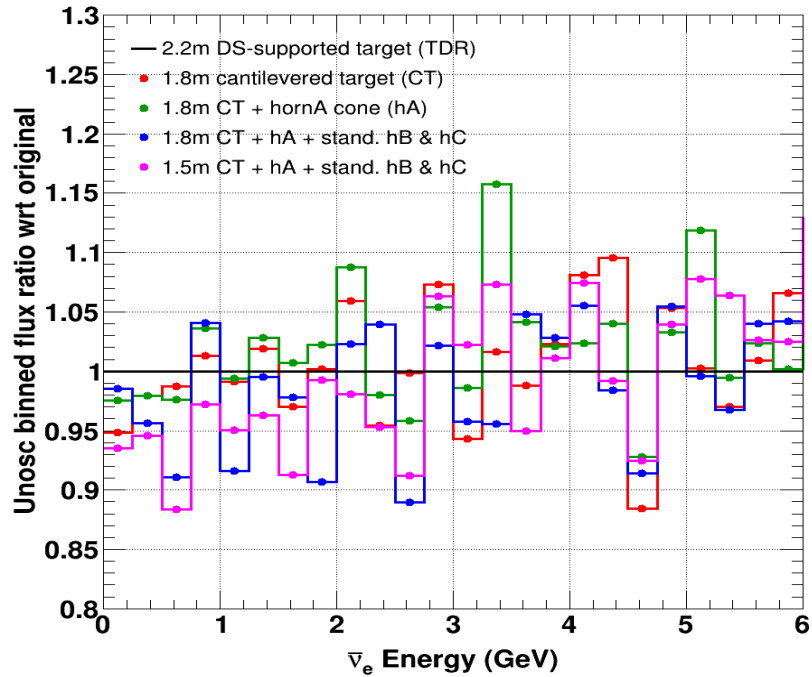
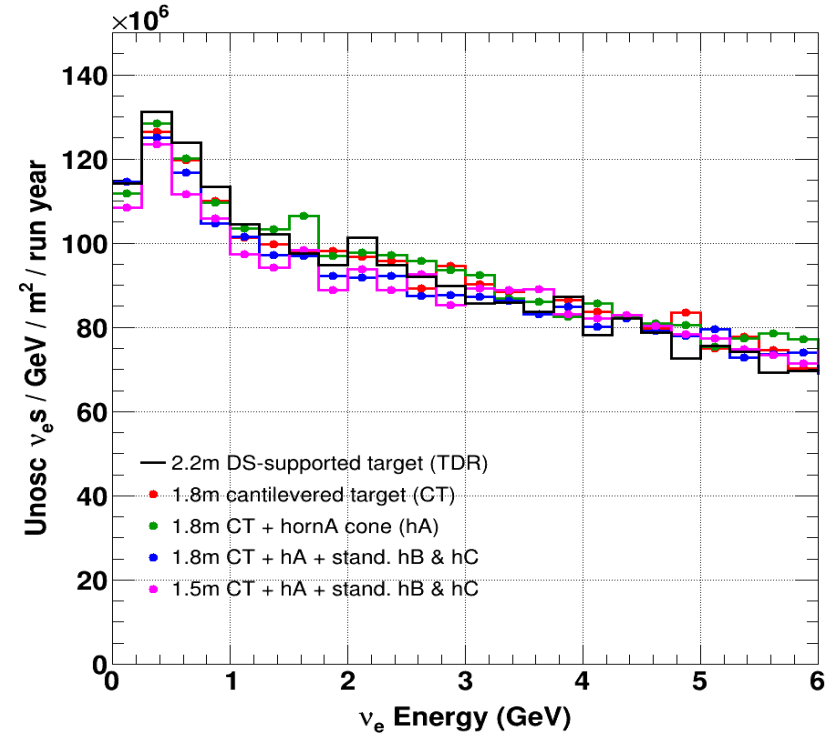
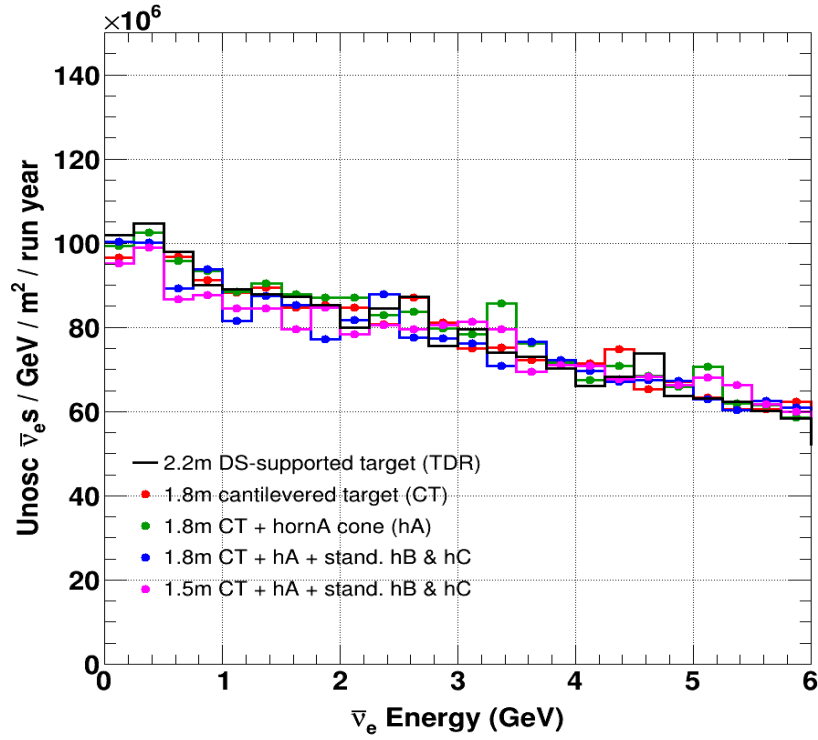
$\nu_\mu \rightarrow \text{anti-}\nu_e$ (solid) & $\text{anti-}\nu_\mu \rightarrow \nu_e$ (dotted) bkgnd



$\nu_\mu \rightarrow \nu_e$ (left) & anti- $\nu_\mu \rightarrow$ anti- ν_e (right) bkgnd

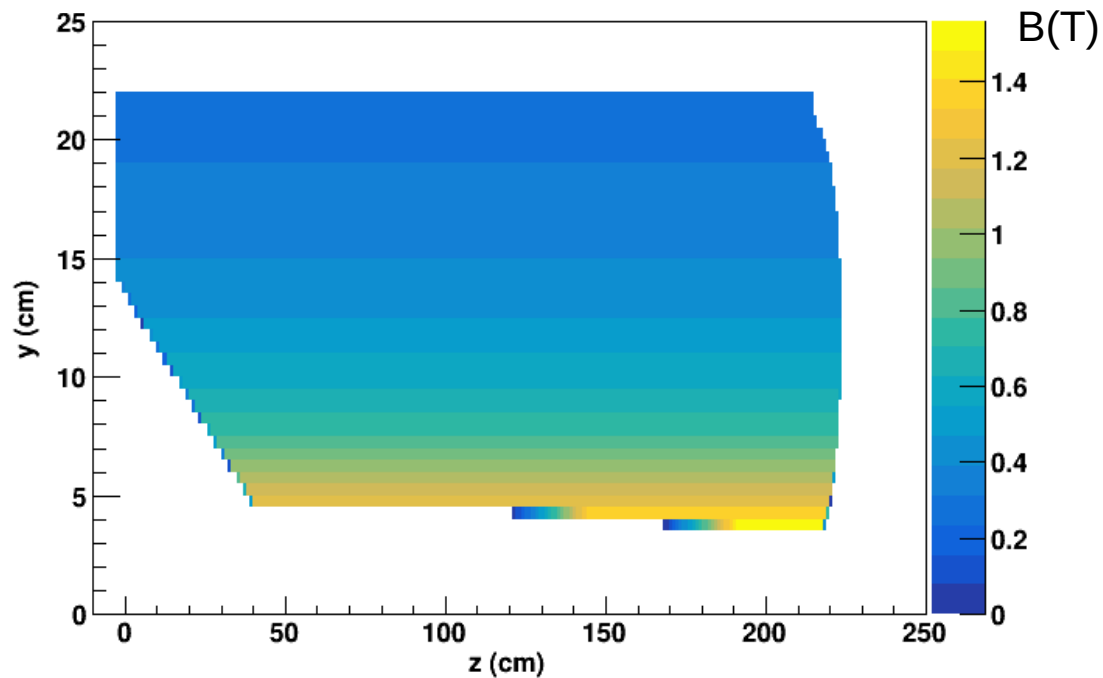
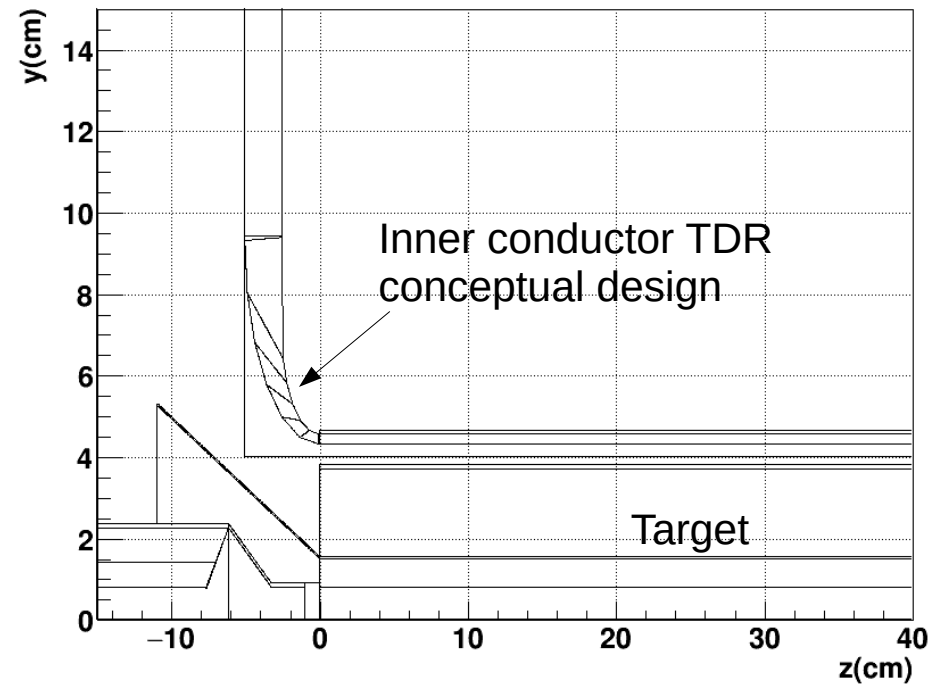
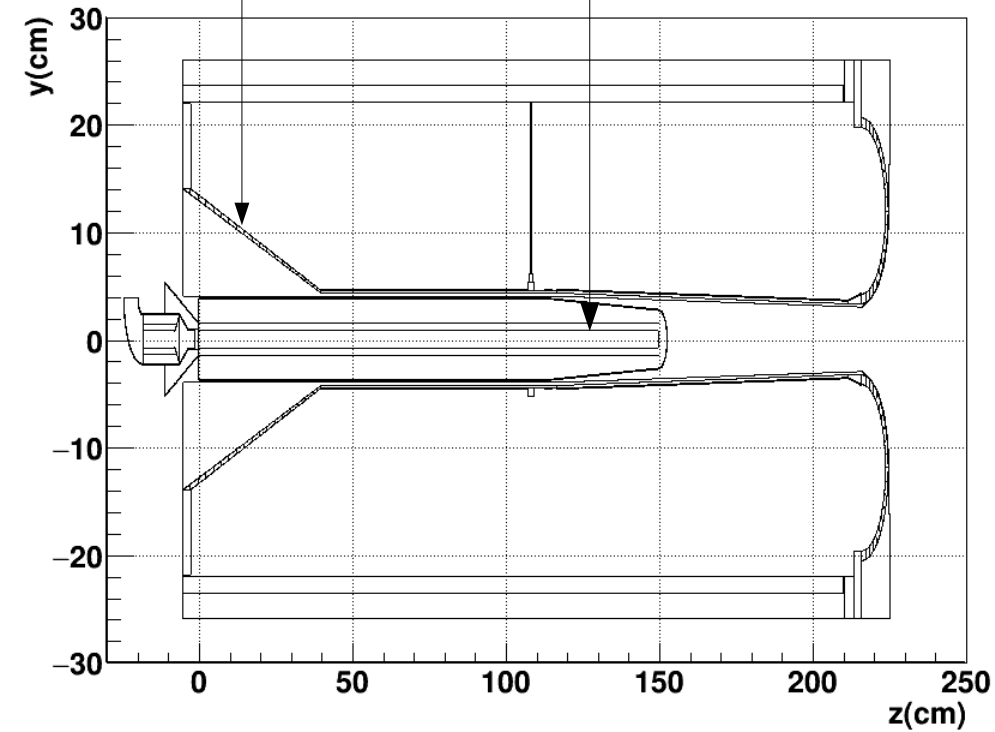


$\nu_\mu \rightarrow \text{anti-}\nu_e$ (left) & $\text{anti-}\nu_\mu \rightarrow \nu_e$ (right) bkgnd



Horn A geometry & B field

Cone: $r=14\text{cm}$, $L=40+5\text{cm}$ Target

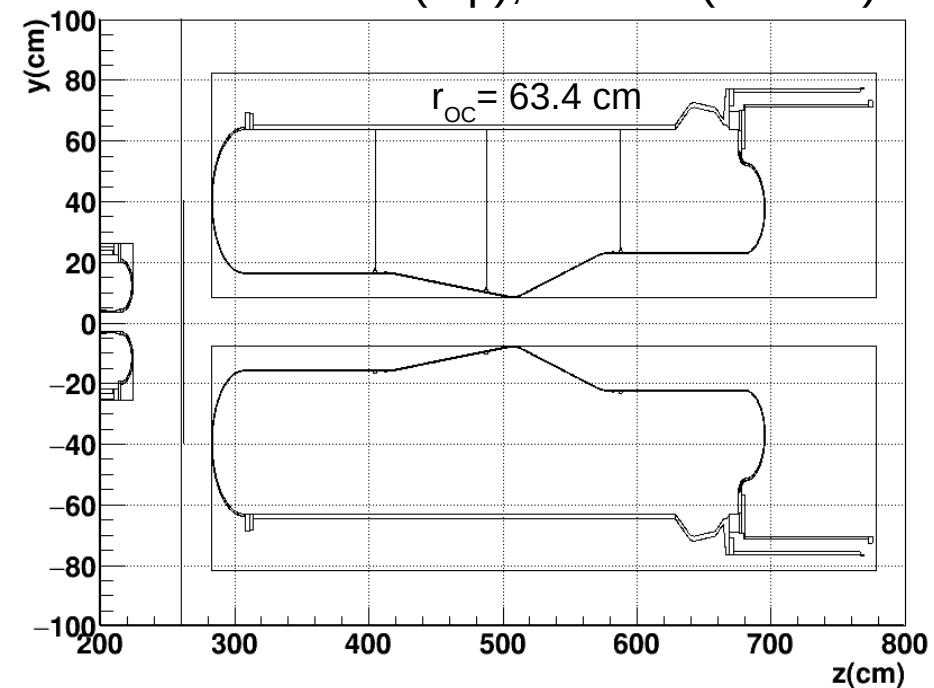


$$B = \mu I / 2\pi r = 0.02 [I(\text{kA}) / r(\text{cm})] \text{ T}$$

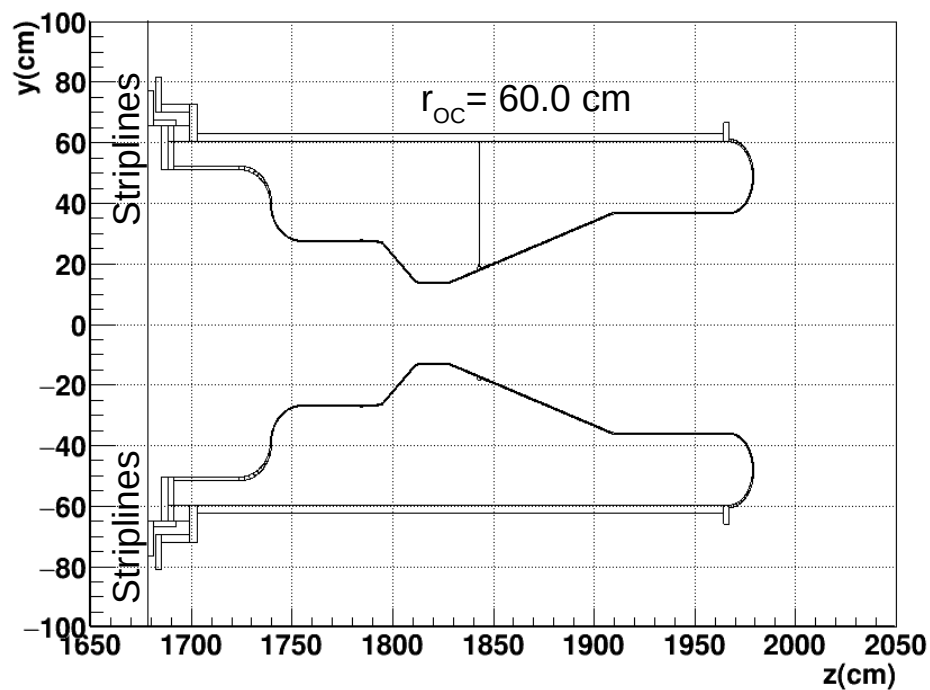
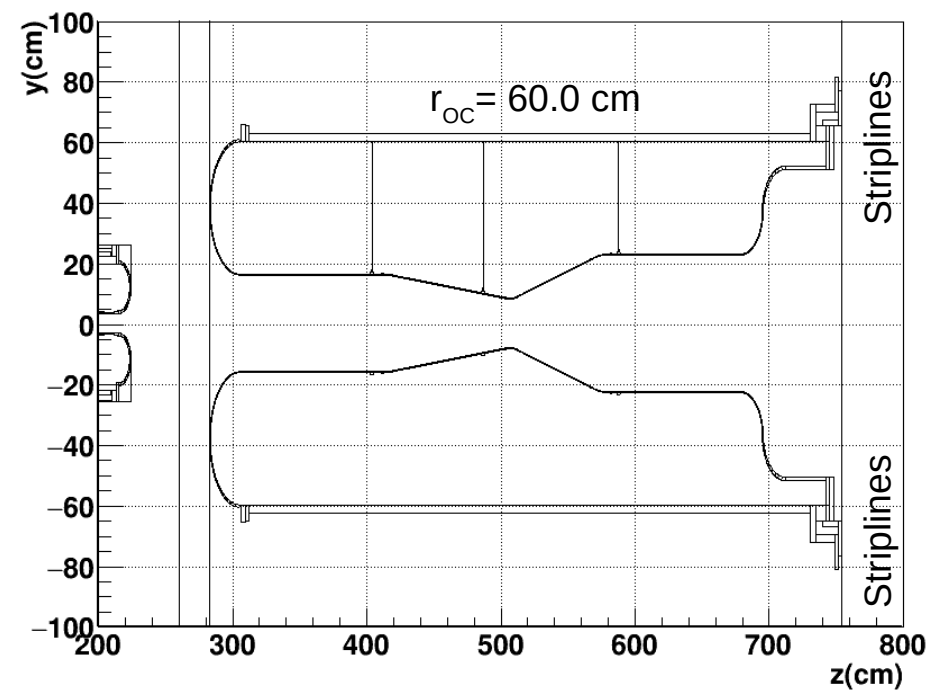
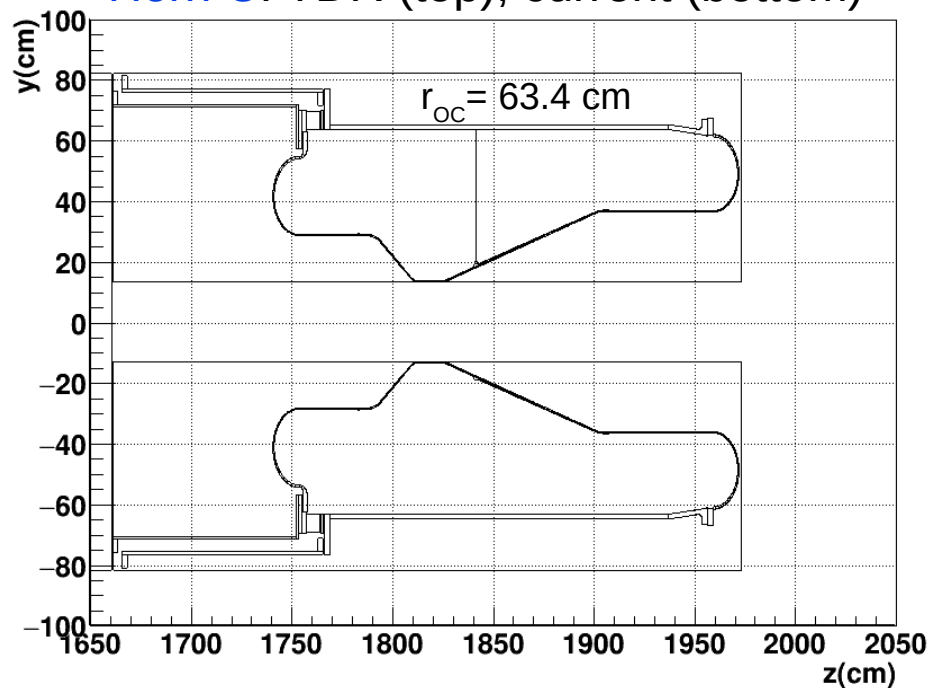
$$I_A = 293 \text{ kA} = I_B = I_C$$

Horn B & C geometry changes

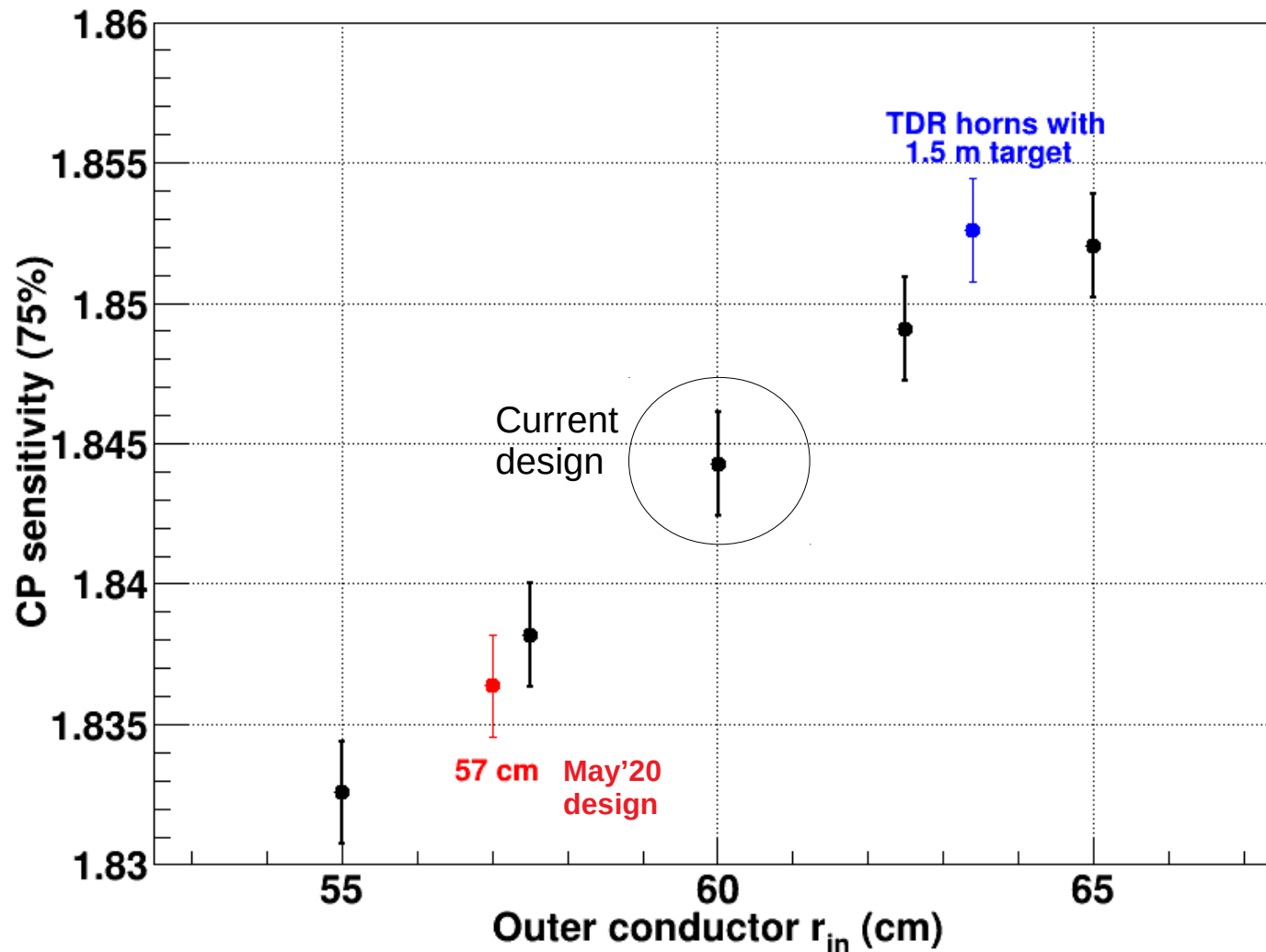
Horn B: TDR (top), current (bottom)



Horn C: TDR (top), current (bottom)

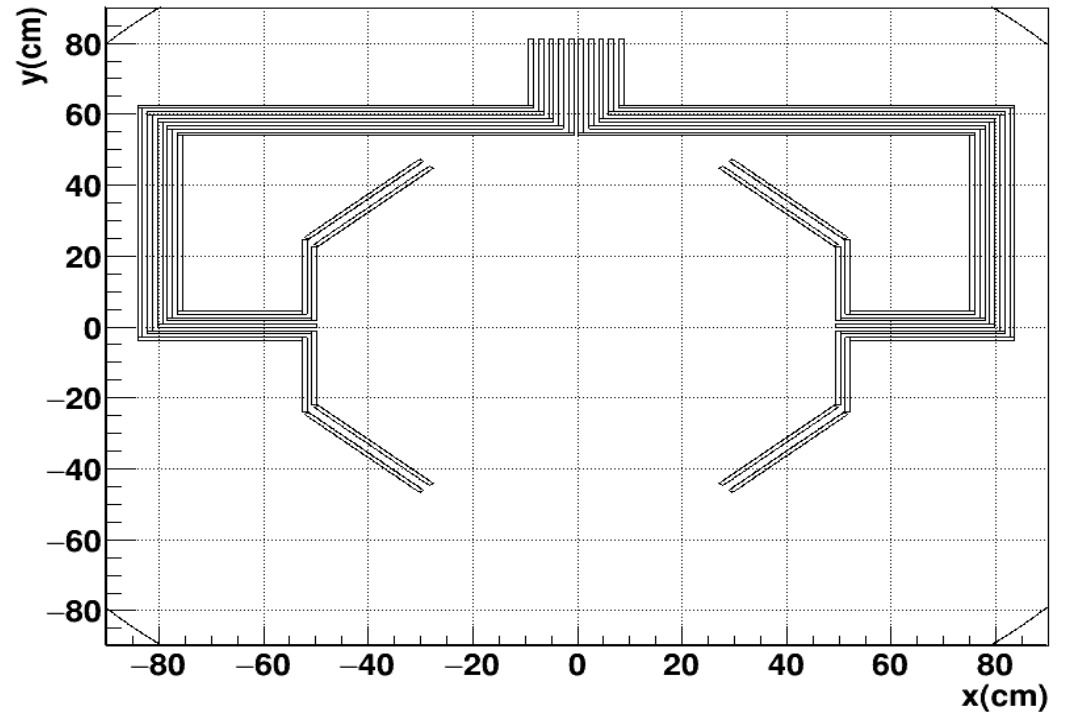
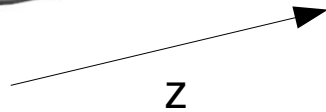
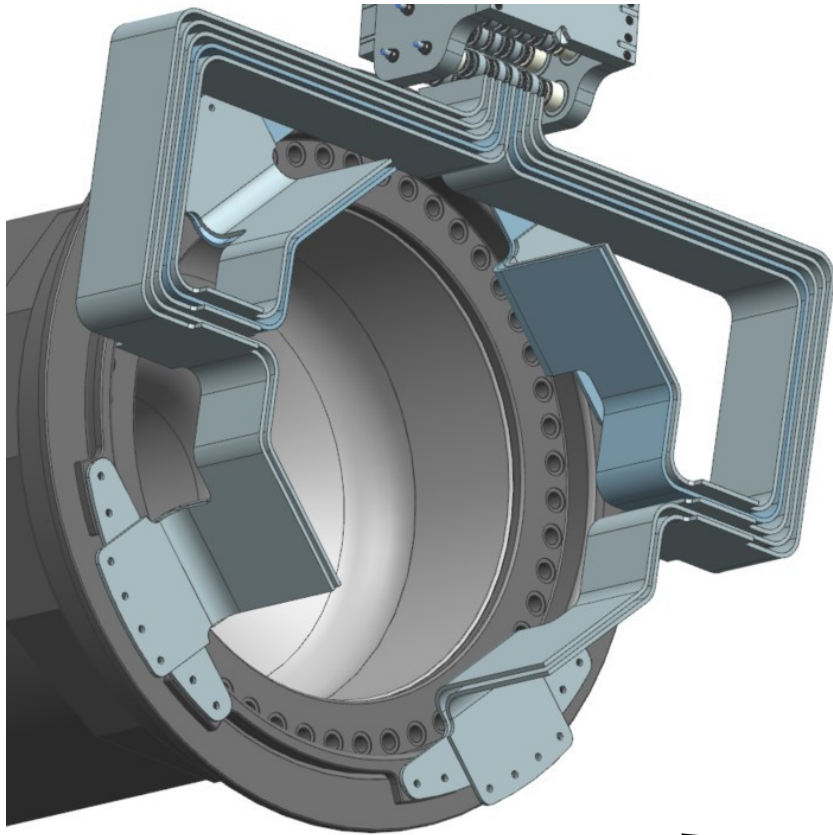


CP sensitivity vs standardized Horn B & C outer conductor inner radius

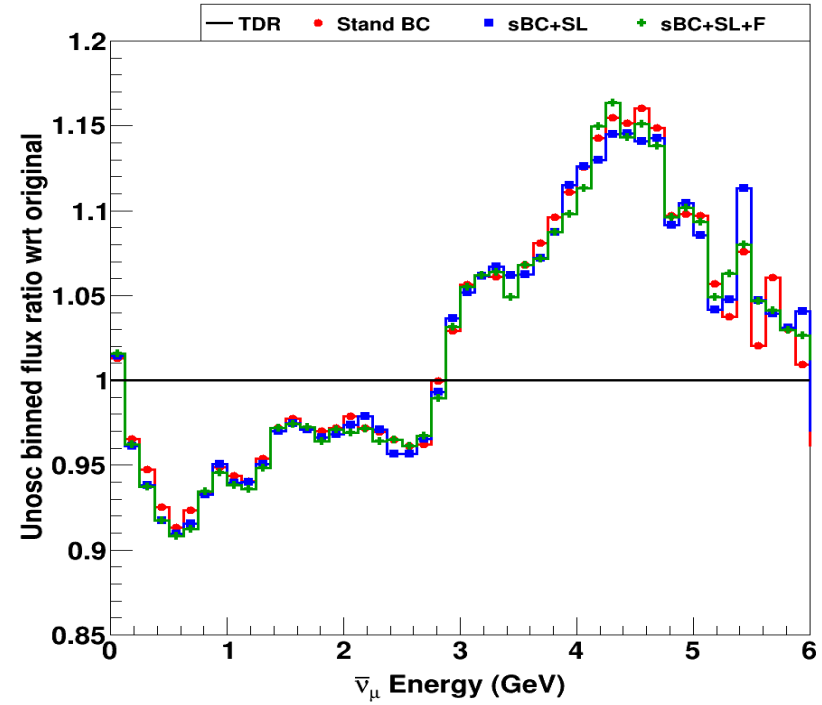
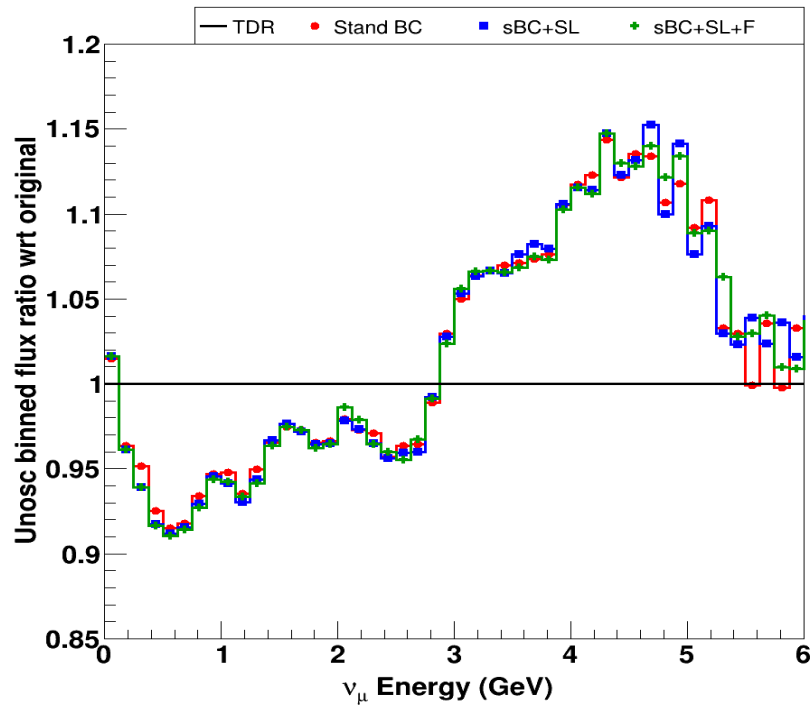
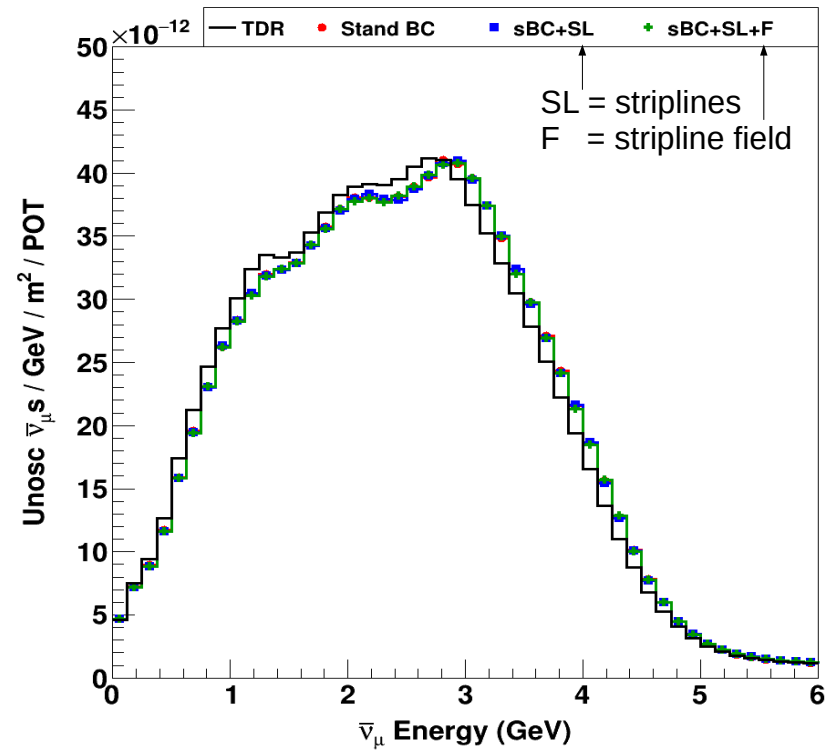
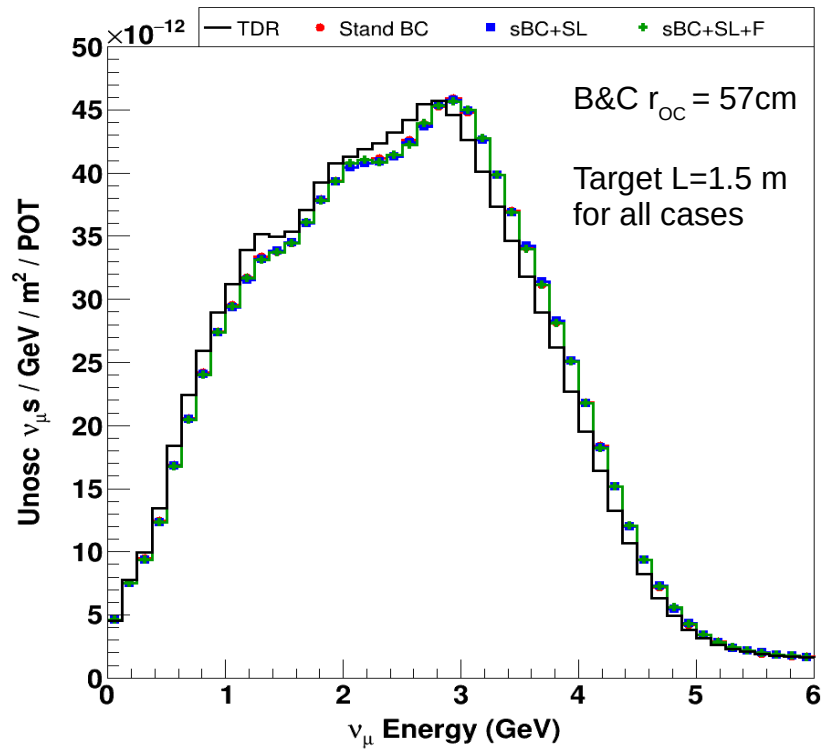


1.5 m cantilever target, horn A cone, DUNE-doc-19219
Horns B & C outer conductor radii are equal

Current Horn B & C striplines



Including Horn B&C striplines: signal ν_μ (left) and anti- $\bar{\nu}_\mu$ (right)

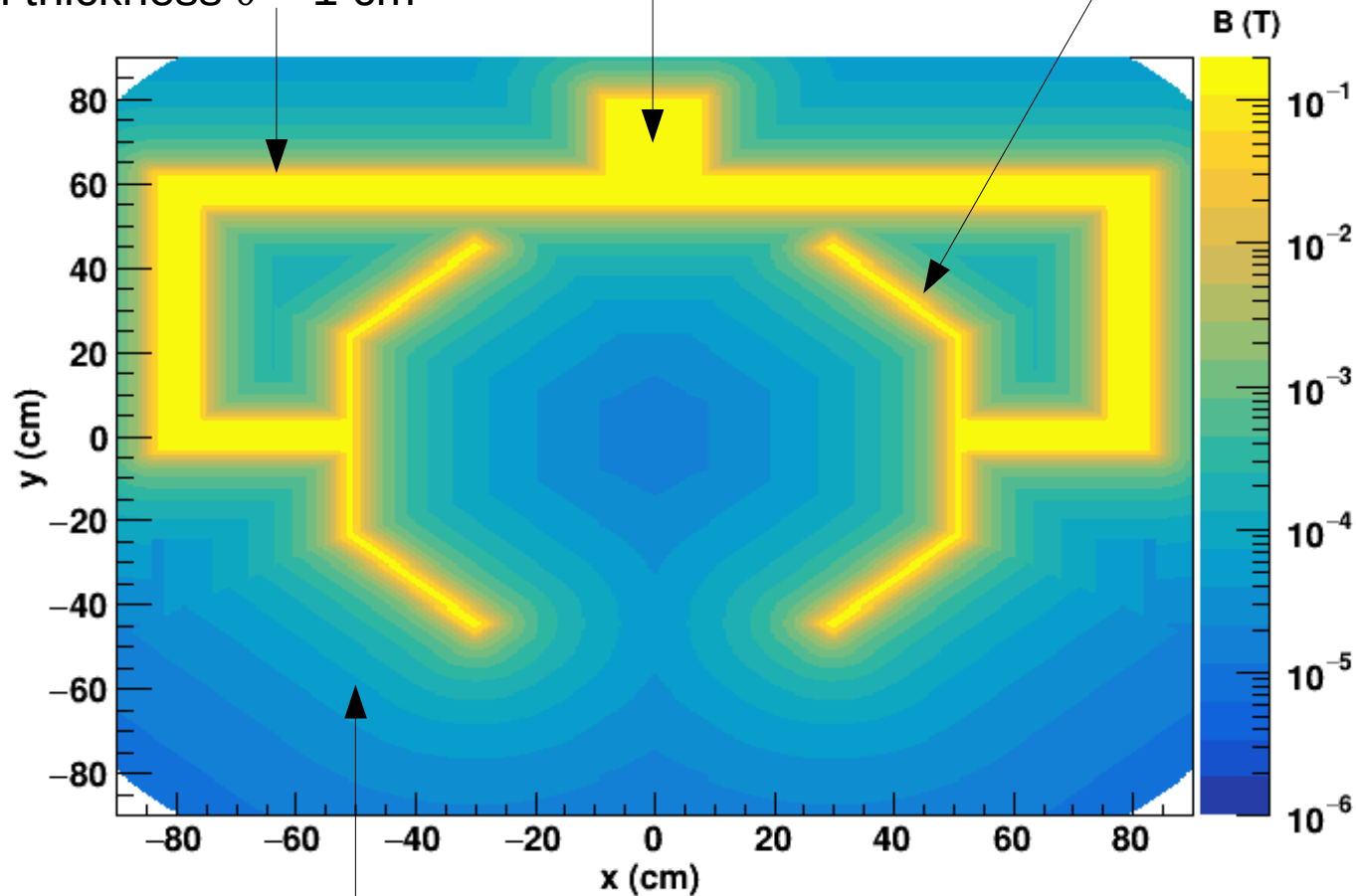


Stripline field

surface $B_z = 0.04$ T
within thickness $\delta = 1$ cm

Inside $B_z = 0.2$ T

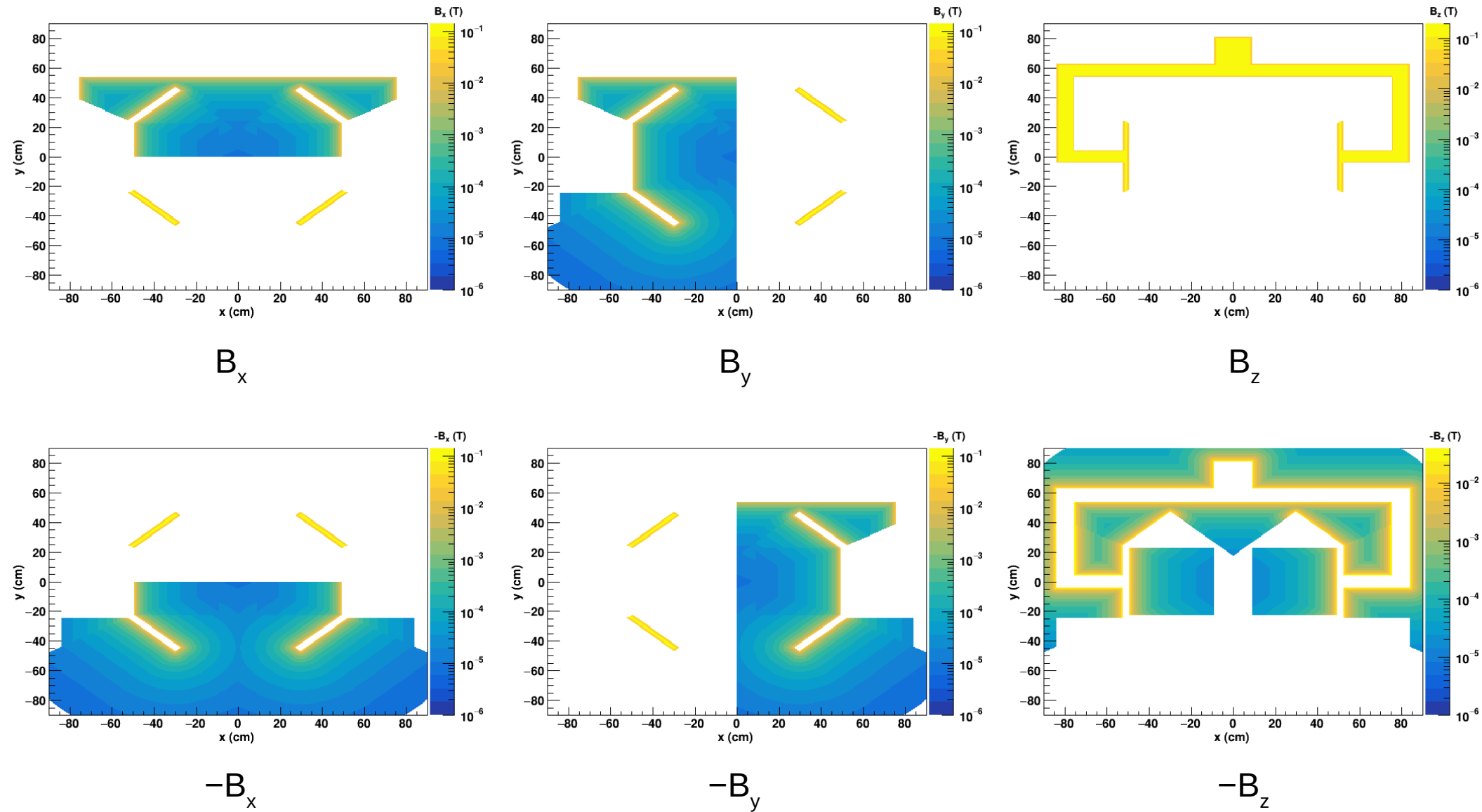
B_x & B_y parallel to planes (I along z)



outside dipole $B_{x,y \text{ or } z} = 0.04 [\delta/(r + \delta)]^2$ T, where r = nearest perp. distance from planes

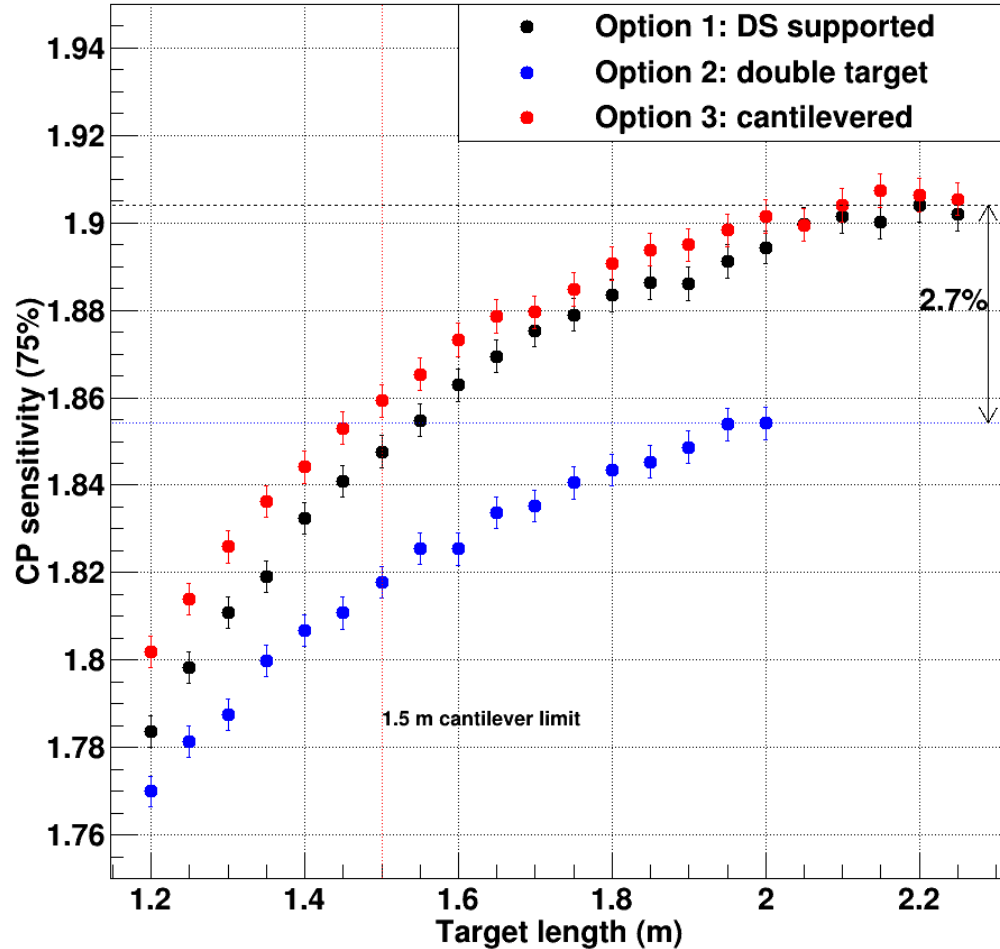
Not a real field map but an approximation

Stripline field components

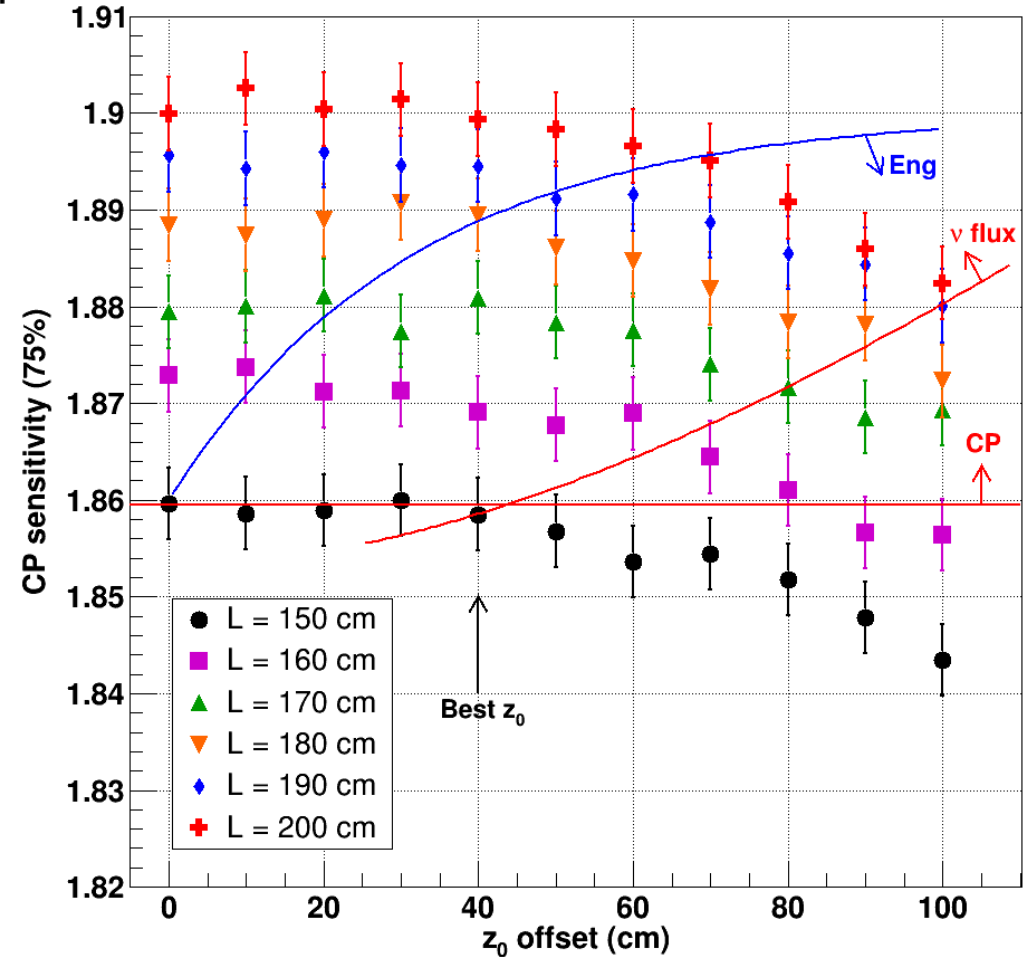


CP sensitivity vs target length & horn A cone length

120 GeV, 1.2 MW, 3.5+3.5 run yrs, 40kt det, NuFit 4.0 pars, $r = 8\text{mm}$



TDR horns A, B & C
DUNE-doc-14944



Horn A cone:

$r_{\text{base}} = 14\text{ cm}$, $L_z = z_0 + 5\text{ cm}$; $z_0 = \Delta z$ from MCZero

1.5 m cantilevered target; TDR horns B & C
DUNE-doc-17052