### **Dynamic Process Modeling**

Process Dynamics and Control

### Description of process dynamics

- Classes of models
- ► What do we need for control?
- Modeling for control
  - Mechanical Systems Modeling
  - Electrical circuits and electrochemical systems
  - ► Fluid and heat flow models

Brief intro to Matlab and Simulink tools (Tutorials 1 and 2)

#### Motivation:

- Develop understanding of process
  - ➡ a mathematical hypothesis of process mechanisms
- Match observed process behavior
  - → useful in design, optimization and *control* of processes

#### Control:

- Interested in description of process dynamics
  - Dynamic model is used to predict how process responds to given input
  - ➡ Tells us how to react

#### What kind of model do we need?

Dynamic vs. Steady-state (Static)

► Steady-state (Static)

➡Variables not a function of time

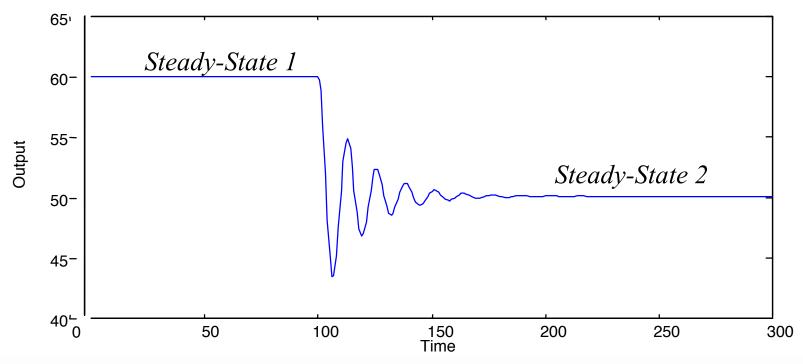
→useful for design calculation

► Dynamic

➡Variables are a function of time

Control requires dynamic model

#### Dynamic vs. Steady-state



Step change in input to observe

- ➤ Starting at steady-state, we made a step change
- ► The system oscillates and finds a new steady-state
- > Dynamics describe the transient behavior

What kind of model do we need?

Experimental vs Theoretical

► Experimental

Derived from tests performed on actual process

Simpler model forms

Easier to manipulate

► Theoretical

Application of fundamental laws

more complex but provides understanding

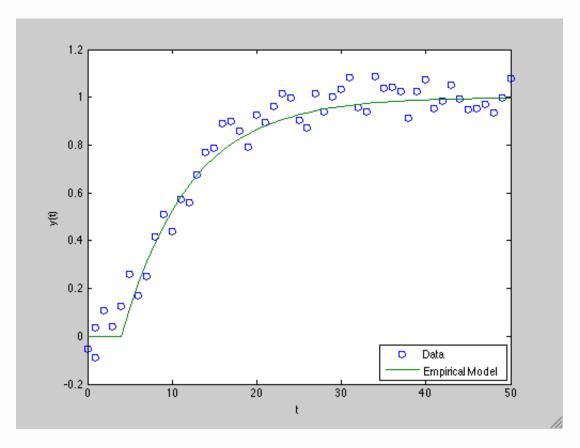
Required in design stages

#### Empirical vs. Mechanistic models

- ► Empirical Models
  - only local representation of the process
    - (no extrapolation)
  - model only as good as the data
- Mechanistic Models
  - Rely on our understanding of a process
  - Derived from first principles
  - Observing physical laws
  - Useful for simulation and exploration of new operating conditions
  - May contain unknown constants that must be estimated

#### Empirical vs Mechanistic models

- ► Empirical models
  - do not rely on underlying mechanisms
  - ➡Fit specific function to match process



#### Mechanistic modeling procedure

Identify modeling objectives

➡end use of model (e.g. control)

Apply fundamental physical and chemical laws

Mass, Energy and/or Momentum balances

- ➤ Make appropriate assumptions (Simplify)
  - ideality (e.g. isothermal, adiabatic, ideal gas, no friction, incompressible flow, etc,...)
- Develop the model equations

#### Modeling procedure

- ► Check model consistency
  - →do we have more unknowns than equations
- Determine unknown constants
  - ▶e.g. friction coefficients, fluid density and viscosity
- Solve model equations
  - →typically nonlinear ordinary (or partial) differential equations
  - ➡initial value problems
- Check the validity of the model
  - compare to process behavior

#### For control applications:

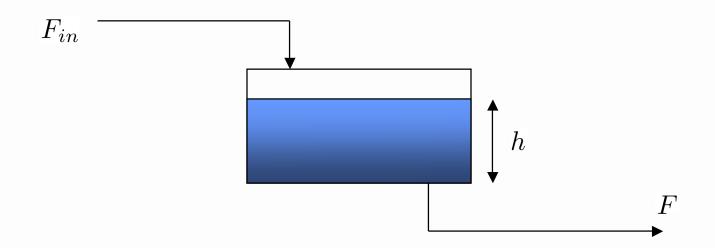
 Modeling objectives is to describe process dynamics based on the laws of conservation of mass, energy and momentum

The balance equation

$$\begin{array}{c} Rate \ of \ Accumulation \\ of \ fundamental \ quantity \end{array} \end{array} \right) = \left( \begin{array}{c} Flow \\ In \end{array} \right) - \left( \begin{array}{c} Flow \\ Out \end{array} \right) \\ + \left( \begin{array}{c} Rate \ of \\ Production \end{array} \right) \end{array}$$

- 1. Mass Balance
- 2. Energy Balance
- 3. Momentum Balance (Newton's Law)

Application of a mass balance *Holding Tank* 



- Modeling objective: Control of tank level
- *Fundamental quantity:* Mass

Assumptions: Incompressible flow

Total mass in system  $= \rho V = \rho Ah$ Flow in  $= \rho F_{in}$ Flow out  $= \rho F$ 

Balance equation:

$$\frac{d\rho Ah}{dt} = \rho F_{in} - \rho F$$

► For constant density

$$\rho A \frac{dh}{dt} = \rho F_{in} - \rho F$$

$$\downarrow \left( \times \frac{1}{\rho A} \right)$$

$$\frac{dh}{dt} = \frac{1}{A} \left( F_{in} - F \right)$$

Taking Laplace transform

$$sH(s) = \frac{1}{A}F_{in}(s) - \frac{1}{A}F(s)$$
$$\downarrow \left(\times \frac{1}{s}\right)$$
$$H(s) = \frac{1}{As}F_{in}(s) - \frac{1}{As}F(s)$$

If the outlet flow is zero (F = 0)

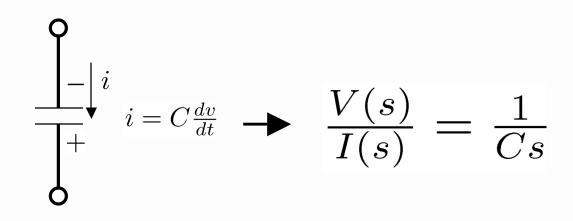
$$H(s) = \frac{1}{As}F_{in}(s)$$

Interesting parallel with capacitor

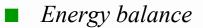
► Holding tank (assume F = 0)

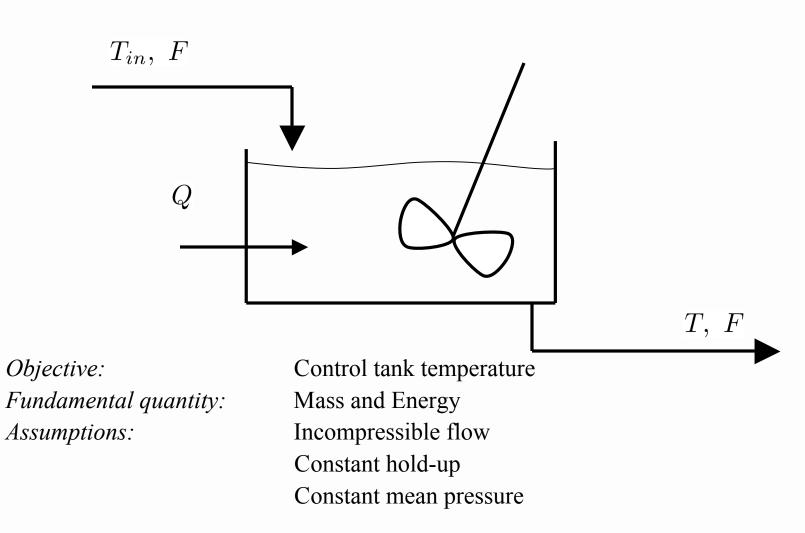
$$\frac{H(s)}{F_{in}(s)} = \frac{1}{As}$$

► Capacitor



> Dynamics of both systems are equivalent





#### Under constant hold-up and constant density

► Mass balance equation

➡ Total Mass ρV➡ Mass In ρF➡ Mass Out ρF

$$\frac{d\rho V}{dt} = \rho F - \rho F = 0$$
$$\frac{dV}{dt} = 0$$

► Constant volume

I Under constant hold-up and constant mean pressure changes

► Energy Balance leads to an enthalpy balance

$$\frac{dH}{dt} = \dot{H}_{in} - \dot{H}_{out} + Q + W_s$$

Inlet Enthalpy
 Outlet Enthalpy
 Heat flow to the system
 Work done on system
 Total enthalpy in the system
 Hin =  $\rho FC_p(T_{in} - T_{ref})$   $\dot{H}_{out} = \rho FC_p(T - T_{ref})$   $W_s(= 0)$   $H = \rho VC_p(T - T_{ref})$ 

$$\frac{d\rho V C_p(T - T_{ref})}{dt} = \rho F C_p(T_{in} - T_{ref}) - \rho F C_p(T - T_{ref}) + Q$$

After substitution, with  $T_{ref}$  fixed and assuming constant  $\rho$ ,  $C_p$ 

$$\rho C_p V \frac{dT}{dt} = \rho C_p F(T_{in} - T) + Q$$

Divide by  $\rho C_p V$ 

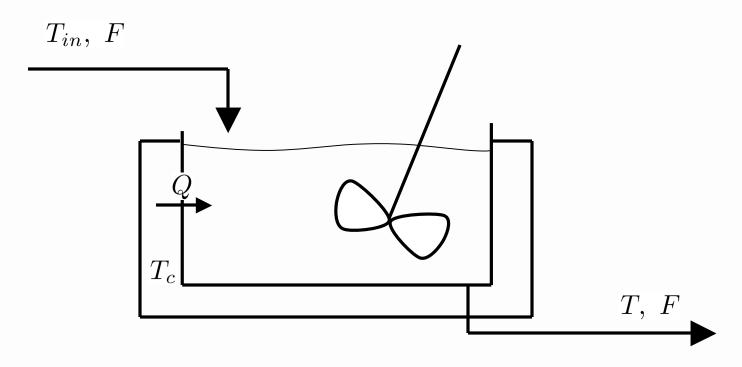
$$\frac{dT}{dt} = \frac{F}{V}(T_{in} - T) + \frac{Q}{\rho C_p V}$$

 $\blacktriangleright$  Heat input from a hot (or cold source) at temperature  $T_c$ 

$$Q = UA(T_c - T)$$

where U is a heat-transfer coefficient A is the effective area for heat transfer

### Modeling heat input



➤ Heat input is proportional to the difference in temperature

$$Q = UA(T_c - T)$$

Assume F is fixed then the ODE is linear, use Laplace Transforms

$$sT(s) - T(0) = \frac{F}{V}T(s) + \frac{1}{\rho C_p V}Q(s)$$

where  $\tau = V/F$  is the tank residence time (or time constant)

Isolating and solving for T(s) gives

$$T(s) = \frac{1}{\tau s + 1} T(0) + \frac{\frac{1}{\rho C_p V}}{\tau s + 1} Q(s)$$

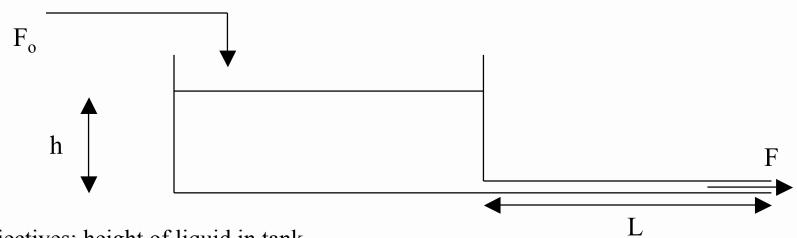
If F changes with time then the differential equation does not have a closed form solution.

$$\frac{dT}{dt} = \frac{F(t)}{V} \left( T_{in}(t) - T(t) \right) + \frac{Q(t)}{\rho C_p V}$$

Products  $F(t)T_{in}(t)$  and F(t)T(t) makes this differential equation *nonlinear*.

Solution will need numerical integration.

#### Gravity tank



Objectives: height of liquid in tank Fundamental quantity: Mass, momentum

Assumptions:

- Outlet flow is driven by head of liquid in the tank
- ► Incompressible flow
- Plug flow in outlet pipe
- ► Turbulent flow

From mass balance and Newton's law,

dh	 $F_{o}$	$A_p v$
$\overline{dt}$	 $\overline{A}$	$\overline{A}$
dv	 hg	$K_f v^2$
$\overline{dt}$	 $\overline{L}$	$\overline{\rho A_p L}$

A system of simultaneous ordinary differential equations results

Linear or nonlinear?

# Solution of ODEs

Mechanistic modeling results in (sets of) nonlinear ordinary differential equations

Solution requires numerical integration

- To get solution, we must first:
  - ► specify all constants
  - specify all initial conditions
  - ► specify types of perturbations of the input variables

For the heated stirred tank,

$$\frac{dT}{dt} = \frac{F}{V}(T_{in} - T) + \frac{Q}{\rho C_p V}$$

specify ρ, C<sub>p</sub>, V
specify T(0)

► specify Q(t), F(t)

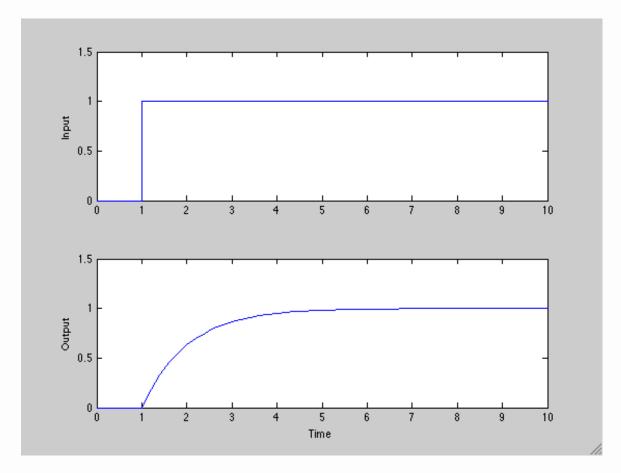
# Input Specifications

#### Study of control system dynamics

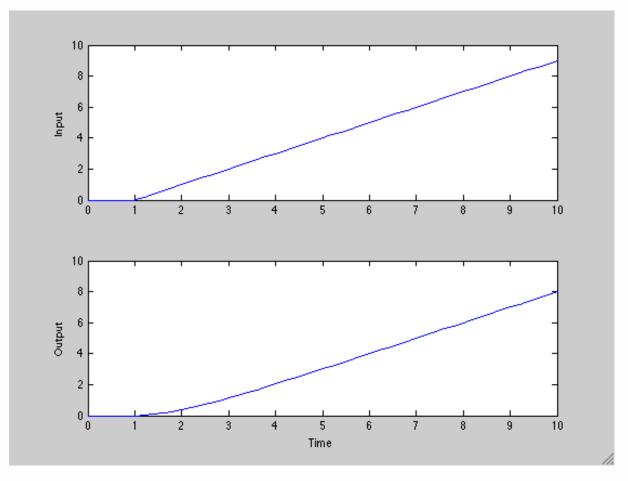
- Observe the time response of a process output in response to input changes
- Focus on specific inputs
  - 1. Step input signals
  - 2. Ramp input signals
  - 3. Pulse and impulse signals
  - 4. Sinusoidal signals
  - 5. Random (noisy) signals

1. Step Input Signal: a sustained instantaneous change

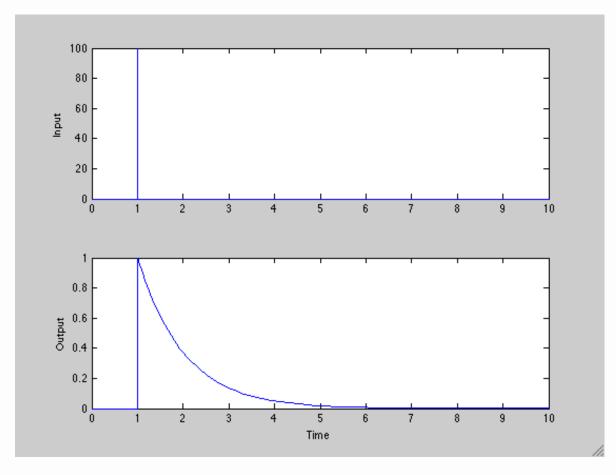
e.g. Unit step input introduced at time 1



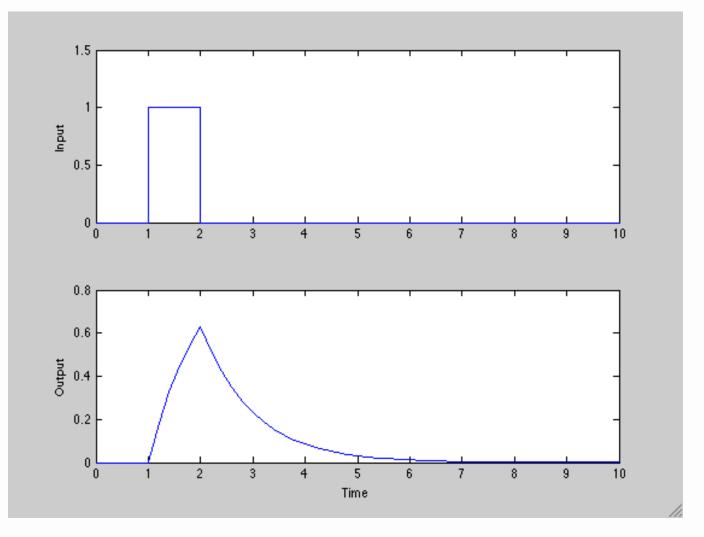
2. Ramp Input: A sustained constant rate of changee.g. Ramp input at time t=1



3. Pulse: An instantaneous temporary changee.g. Fast pulse (unit impulse) at t=1

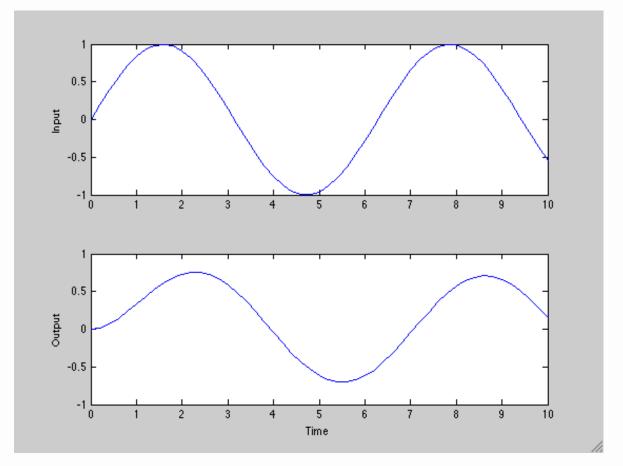


- 3. Pulses:
- e.g. Rectangular Pulse



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4. Sinusoidal input, e.g.  $u(t) = \sin t$ 



### 5. Random Input, e.g. white noise

