

EL5823/BE6203 Medical Imaging

Projection Radiography

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Based on J. L. Prince and J. M. Links, Medical Imaging Signals and Systems, and lecture notes by Prince. Figures are from the textbook.

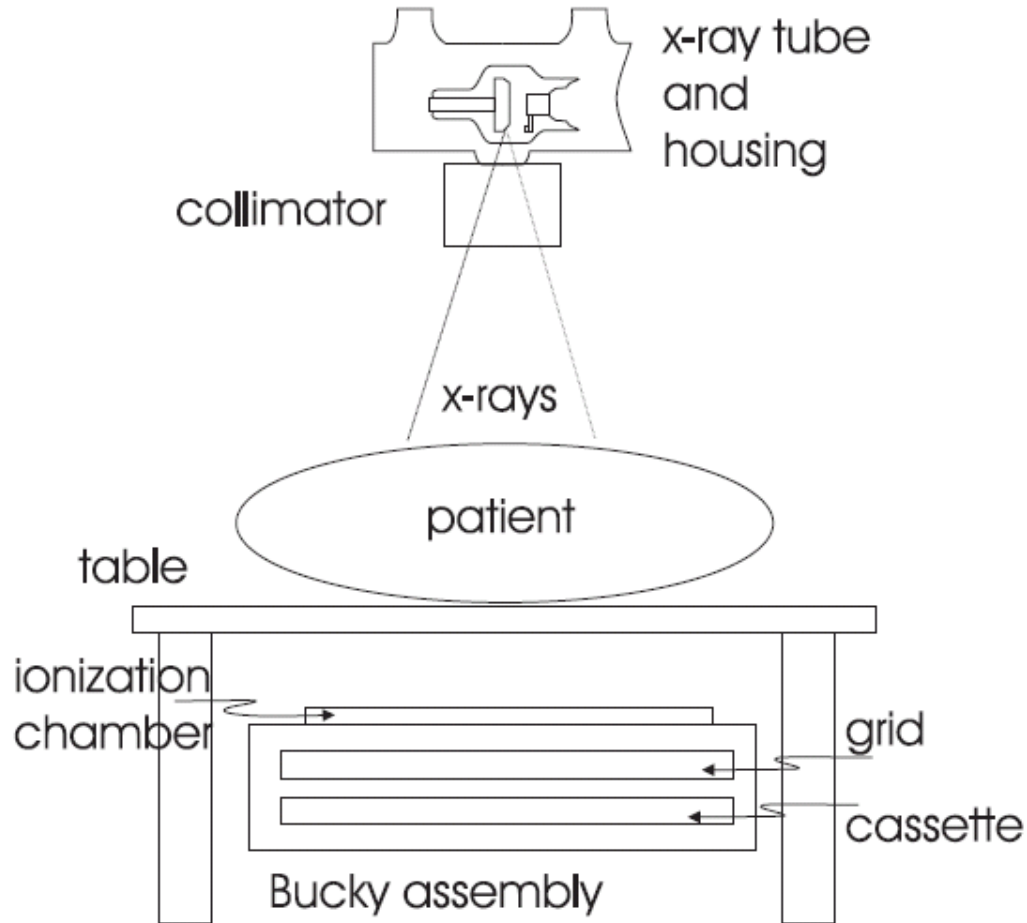
Lecture Outline

- Instrumentation
 - X-ray tube configuration
 - Filtration and restriction of x-ray photons
 - Compensation and Scatter control
 - Film screen detector
- Image formation
 - Geometric effect
 - Extended source
 - Detector/film response
- Image quality
 - Contrast and SNR
 - Effect of noise and Compton scattering

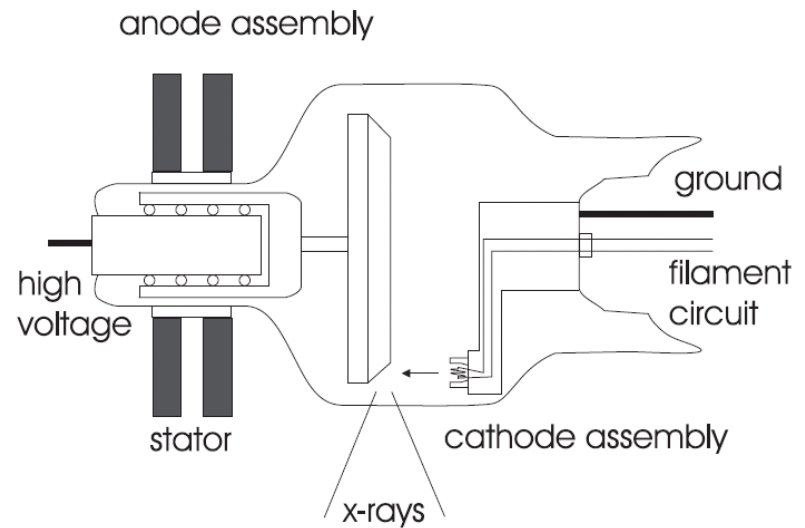
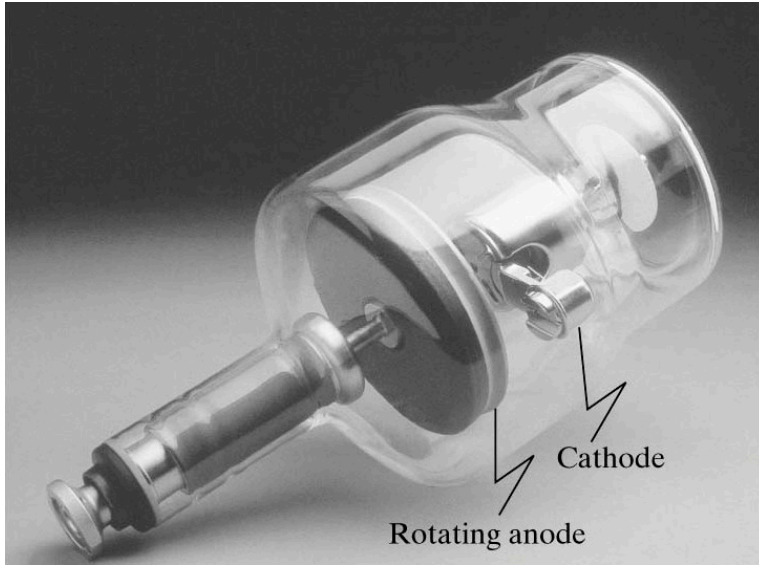
Overview

- Systems:
 - chest x-rays, mammography
 - dental x-rays
 - fluoroscopy, angiography
- Properties
 - high resolution
 - low dose
 - broad coverage
 - short exposure time

Radiographic System



X-ray Tube



X-Ray Tube Components

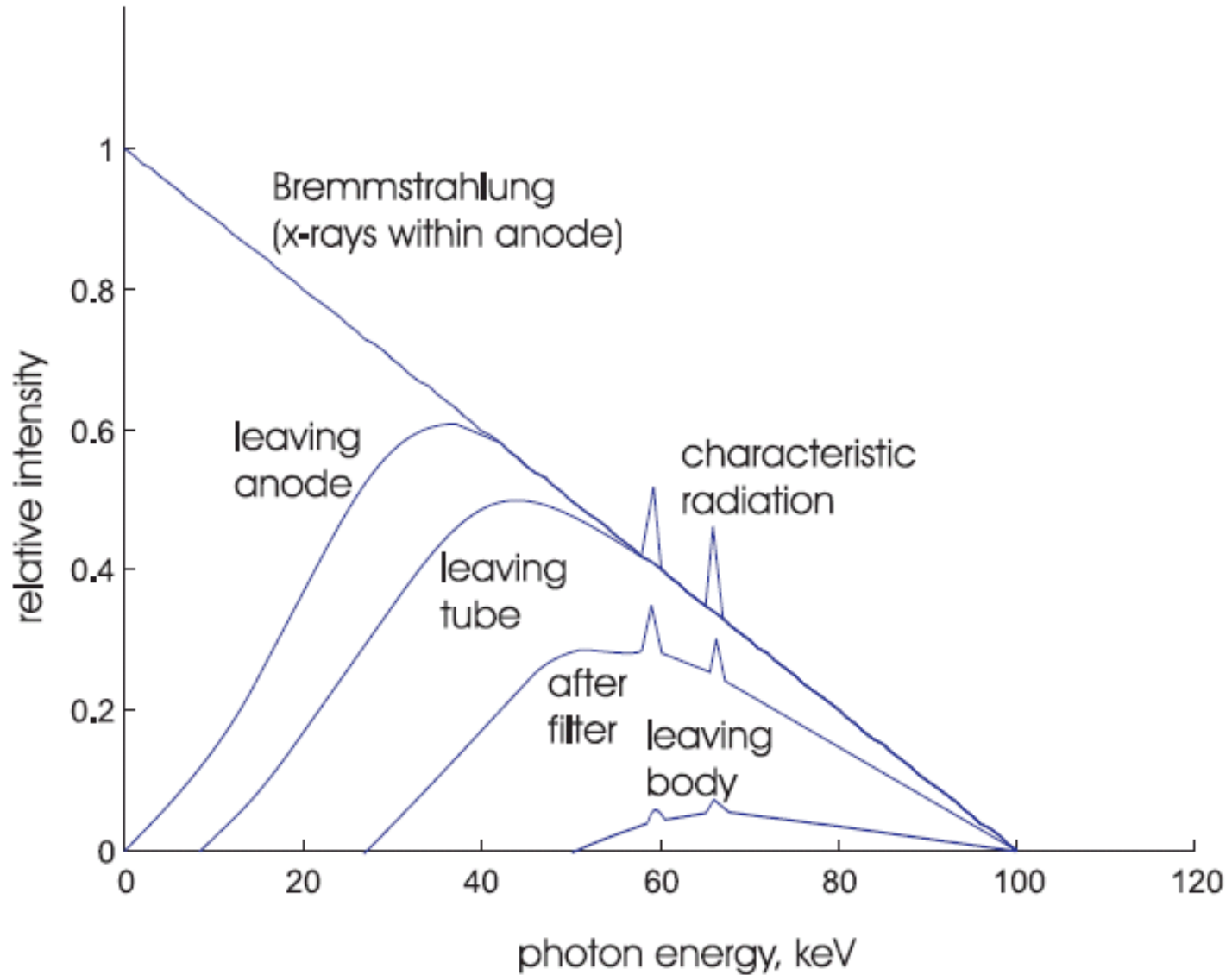
- Filament controls tube current (mA)
- Cathode and focussing cup
- Anode is switched to high potential
 - 30–150 kVp
 - Made of tungsten
 - Bremsstrahlung is 1%
 - Heat is 99%
 - Spins at 3,200–3,600 rpm
- Glass housing; vacuum

Exposure Control

- kVp applied for short duration
 - fixed timer (SCR), or
 - automatic exposure control (AEC), 5 mm thick ionization chamber triggers SCR
- Tube current mA controlled by
 - filament current, and
 - kVp
 - $I_{\text{tube}} = 1\text{-}1000\text{mA}$
- mA times exposure time yields mAs

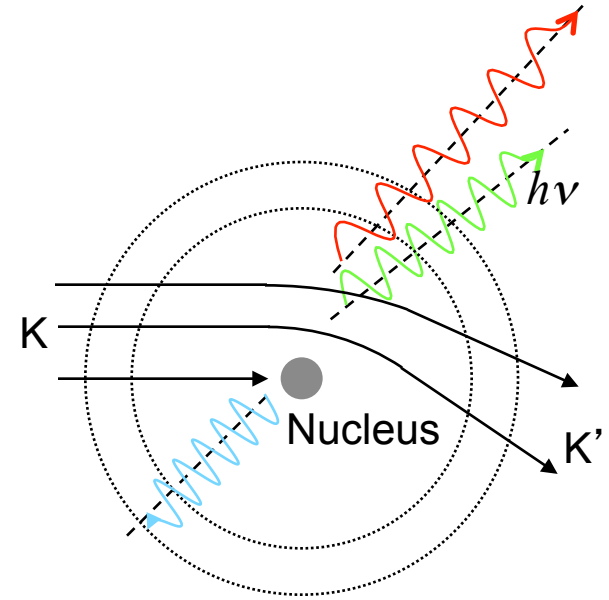
mAs measures x-ray exposure

X-Ray Spectra



Bremsstrahlung

- *Continuous* spectrum of EM radiation is produced by abrupt deceleration of charged particles (“Bremsstrahlung” is German for “braking radiation”).
- Deceleration is caused by deflection of electrons in the Coulomb field of the nuclei
- Most of the energy is converted into heat, ~0.5 % is x-ray
- The energy of the generated x-ray photon is given by energy conservation:
- The maximum energy for the produced photon is given by:



$$h\nu = K_e - K'_e$$

$$E_{p,\max} = h\nu = K_e = eV_{\text{tube}}$$

[From Graber, Lecture Note for BMI1-FS05]

Bremsstrahlung intensity

- Overall Bremsstrahlung intensity I :

$$I \propto V_{tube}^2 I_{tube}$$

Electrical power consumption of tube: $P_{tube} = I_{tube} \times V_{tube}$ [W]

- The produced x-ray power P_x (in[W]) is given by:

$$P_x = k Z V_{tube}^2 I_{tube} = kZ V_{tube} P_{tube} = \eta P_{tube}$$

$$\eta = P_x / P_{tube} = kZ V_{tube} : \text{ x-ray production efficiency}$$

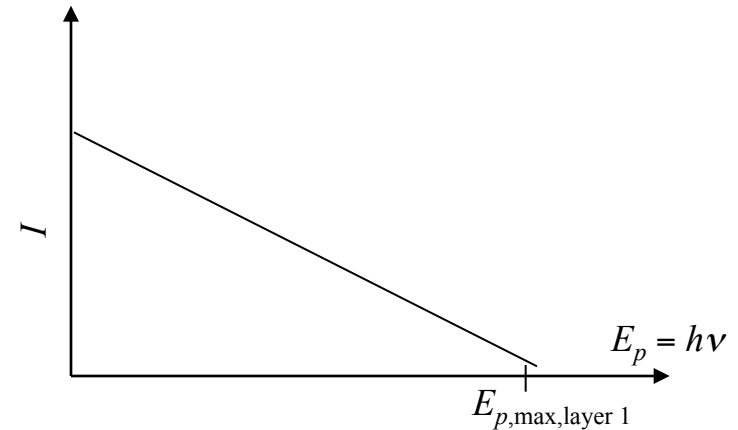
- Material constant $k = 1.1 \times 10^{-9}$ for Tungsten ($Z=74$).

[From Graber, Lecture Note for BMI1-FS05]

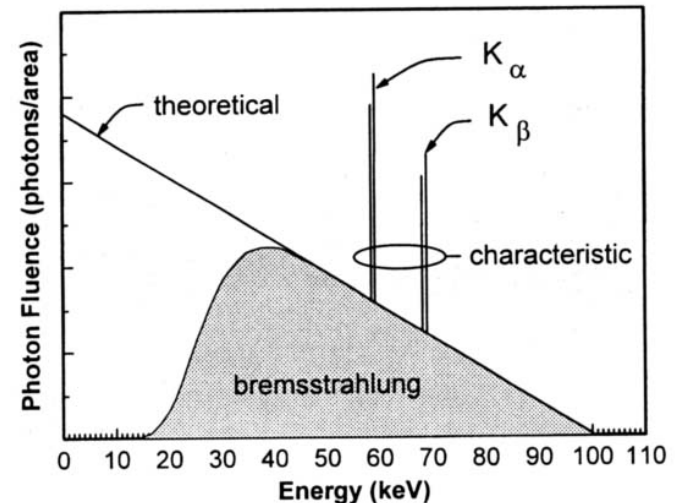
Bremsstrahlung spectrum

- Theoretically, bremsstrahlung from a thick target creates a continuous spectrum from $E = 0$ to E_{max} with intensity I_b :

$$I_b(E) \sim Z(E_{max} - E)$$



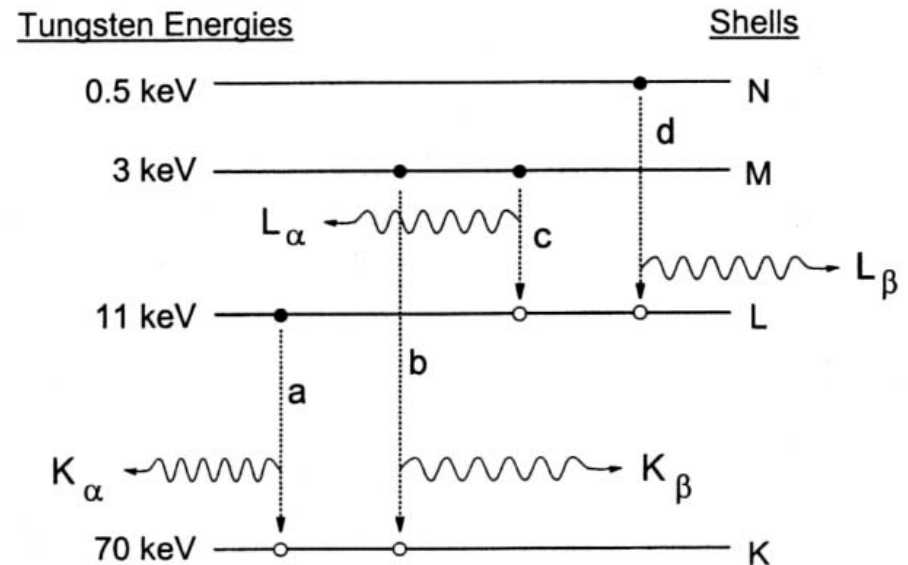
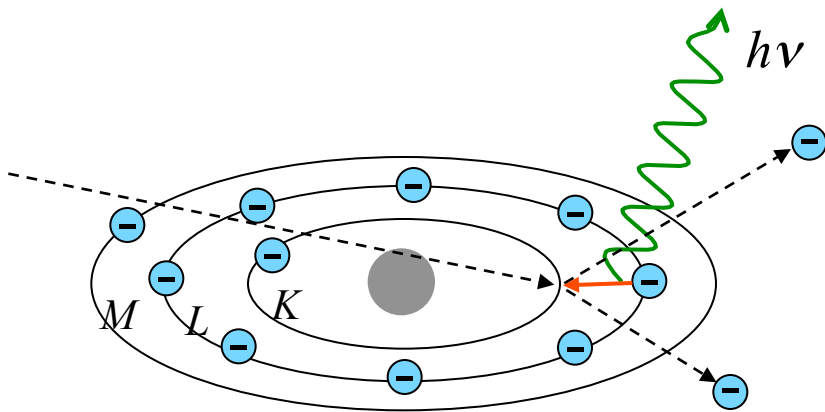
- Actual spectrum deviates from ideal form due to
 - Absorption in window / gas envelope material and absorption in anode
 - Multienenergetic electron beam



[From Graber, Lecture Note for BMI1-FS05]

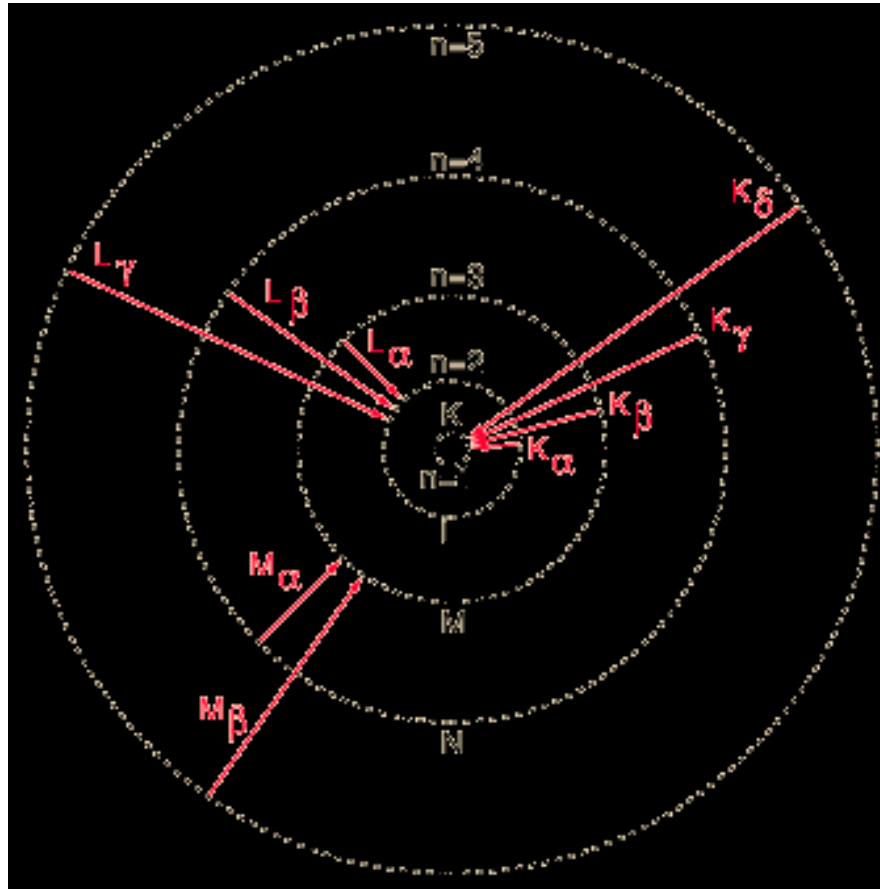
Characteristic radiation

- Narrow lines of intense x-ray at characteristic energies are superimposed on the continuous bremsstrahlung spectrum.
- Caused by removal of inner shell electrons and subsequent filling of hole with electrons from higher shell. The shell-energy difference determines the energy of characteristic rays
- Lines are named after the lower shell involved in the process; the upper shell involved is denoted by Greek letters:
 $\Delta n = 1 \rightarrow \alpha$ -transitions, $\Delta n = 2 \rightarrow \beta$ -transitions, ...



[From Graber, Lecture Note for BMI1-FS05]

Different types of characteristics rays



From <http://hyperphysics.phy-astr.gsu.edu/Hbase/quantum/xterm.html#c1>

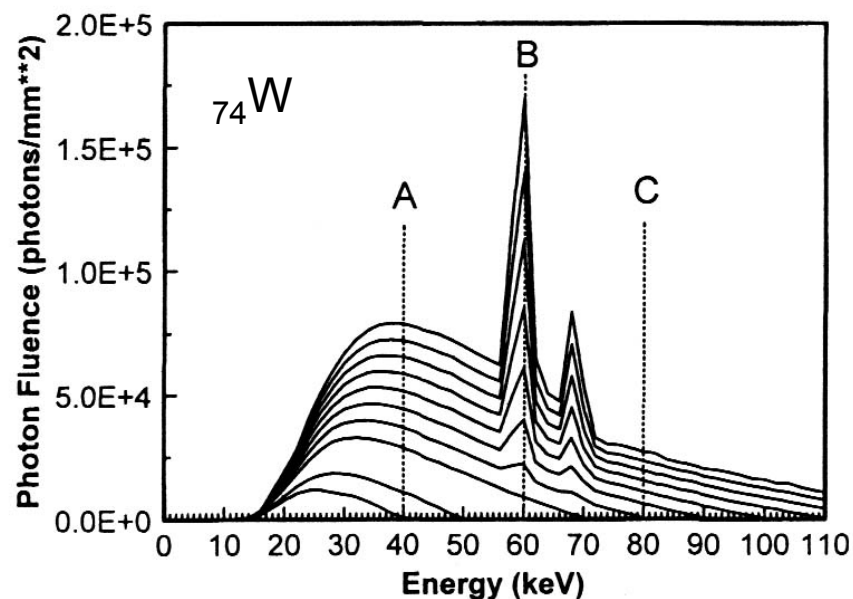
X-ray spectra

- X-ray for general diagnostic radiology produced at 40 – 150 kVp

- Maximum photon energy:
 $E_p[\text{keV}] = h\nu_{\text{max}} = e \times \text{kVp}$

- Characteristic radiation occurs only for anode voltages

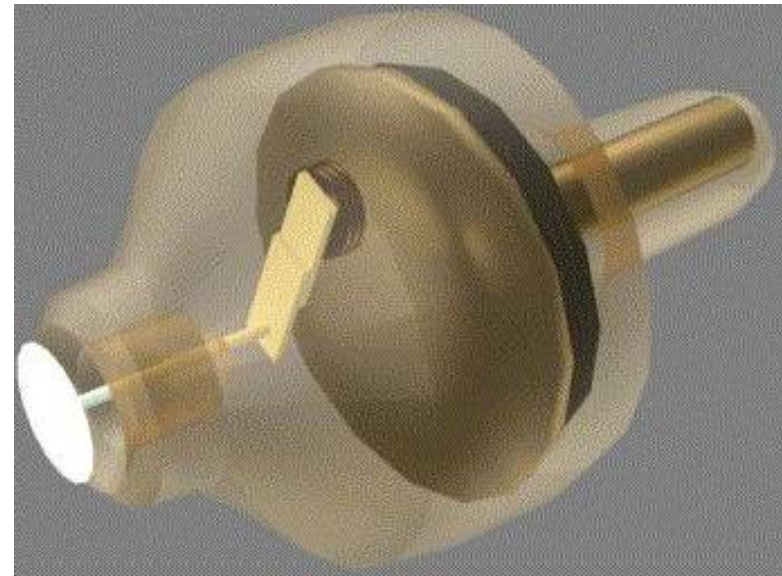
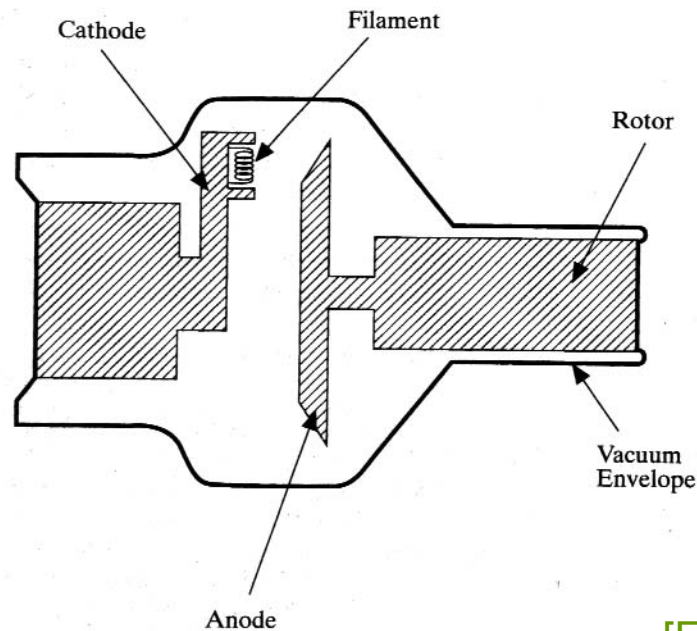
$$e \times \text{kVp} > I_{K,L,M,\dots}$$



[From Graber, Lecture Note for BMI1-FS05]

X-ray tube design

- Cathode w/ focusing cup, 2 filaments (different spot sizes)
- Anode
 - Tungsten, $Z_w = 74$, $T_{\text{melt}} = 2250\text{ }^\circ\text{C}$
 - Embedded in copper for heat dissipation
 - Angled (see next slide)
 - Rotating to divert heat



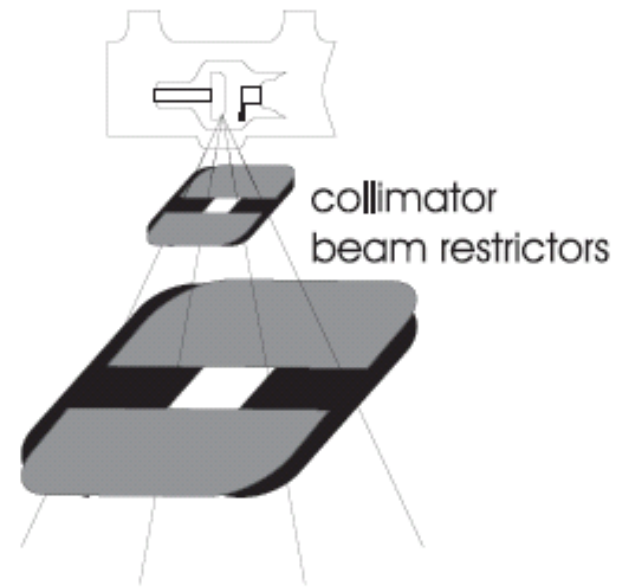
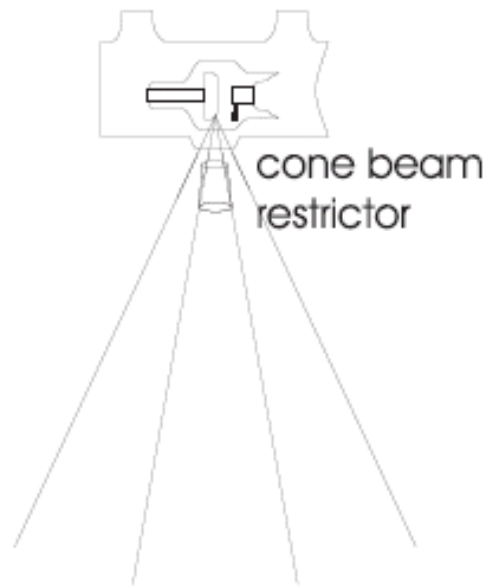
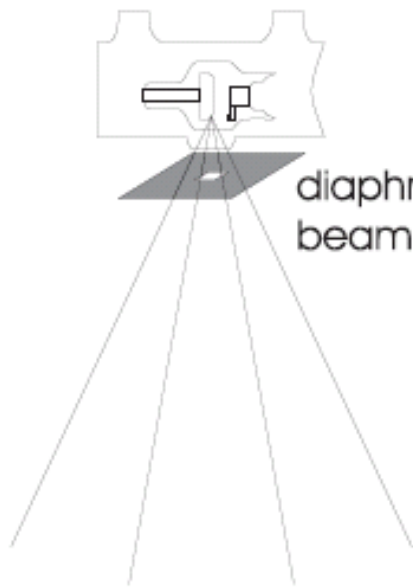
[From Graber, Lecture Note for BMI1-FS05]

Filtration

- Low energy x-ray will be absorbed by the body, without providing diagnostic information
- Filtration: Process of absorbing low-energy x-ray photons before they enter the patient
 - Inherent filtration
 - Within anode
 - Glass housing
 - Added filtration
 - Aluminum
 - Copper/Aluminum
 - Note: Cu has 8keV characteristic xrays
 - Measured in mm Al/Eq

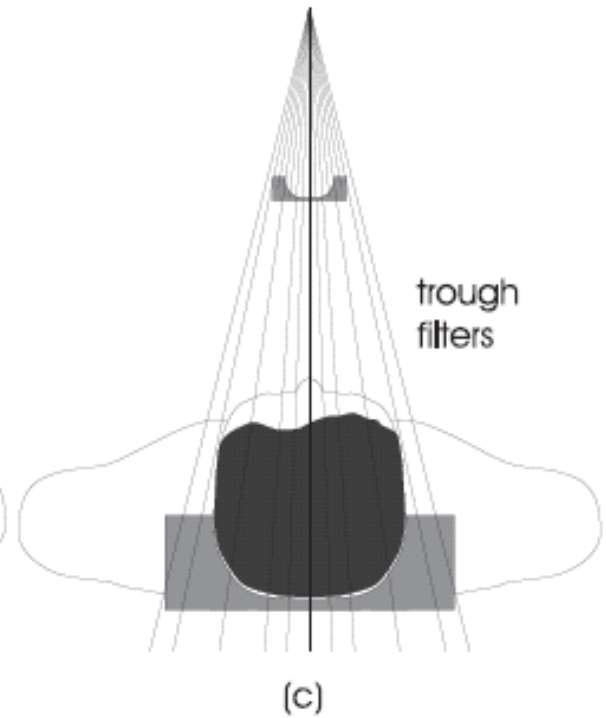
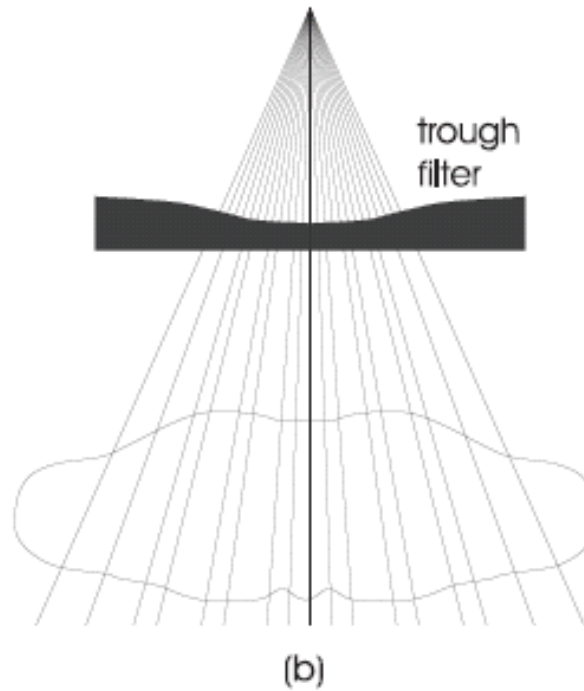
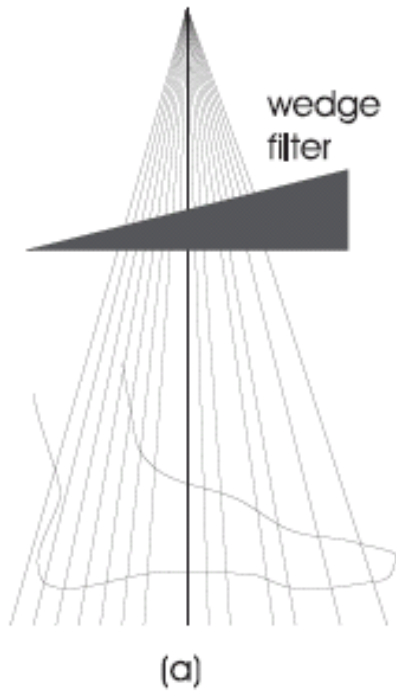
Restriction

- Goal: To direct beam toward desired anatomy



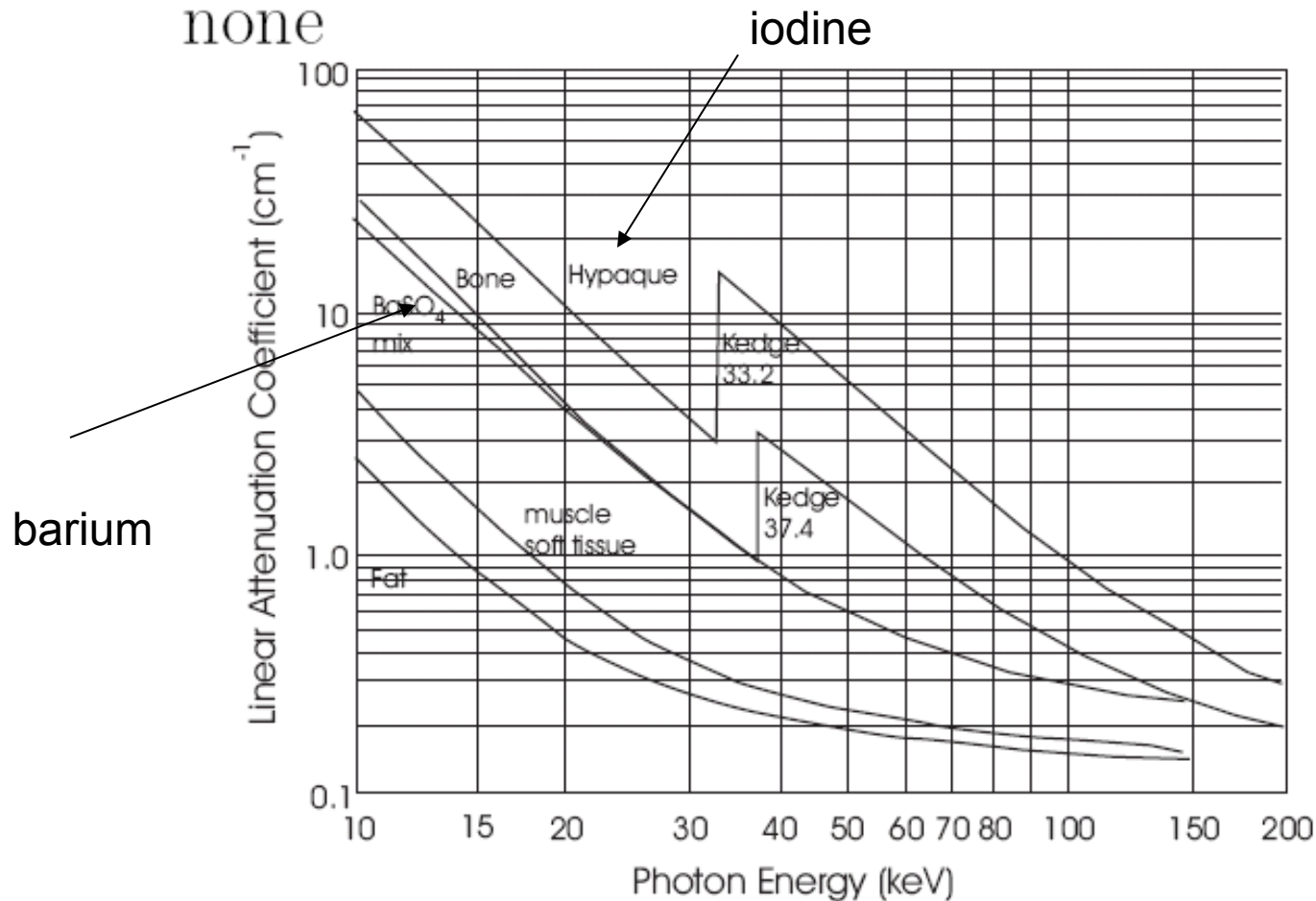
Compensation Filters

- Goal: to even out film exposure



Contrast Agents

- Goal: To create contrast where otherwise



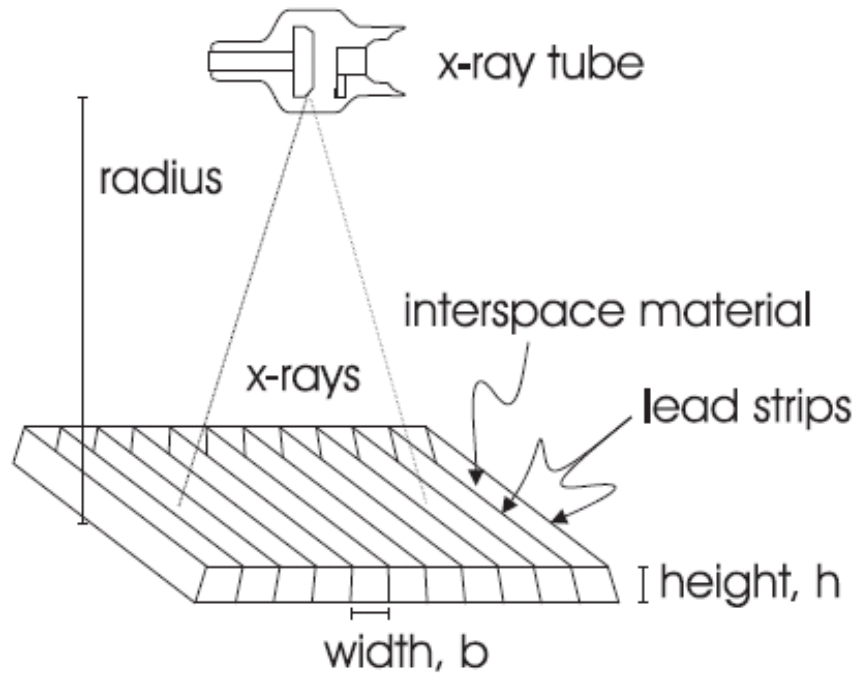
When the x-ray energy exceeds the Kedge (binding energy of K-shell), the μ coefficient is much higher, providing high contrast

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- Iodine:
 - Can be synthesized into soluble compounds that are safely introduced through intravascular injection or ingestion
 - Used for imaging of
 - Blood vessels, heart chambers, tumors, infections
 - Kidneys, bladder
 - Naturally exist in thyroid, and hence X-ray is very good for thyroid imaging
 - Barium
 - Administered as a “chalky milkshake”
 - Used in the gastrointestinal tract,
 - Stomach, bowel
 - Air
 - Does not absorb x-ray
 - “opposite” type of contrast
 - By Inflating the lungs, air provides contrast for lung tissues

Scatter Control

- Ideal x-ray path: a line!
- Compton scattering causes blurring
- How to reduce scatter?
 - airgap
 - scanning slit
 - grid

Grids



- Effectiveness in scatter reduction?

$$\text{grid ratio} = \frac{h}{b}$$

- 6:1 to 16:1 (radiography) or 2:1 (mammo)

Problem with Grids

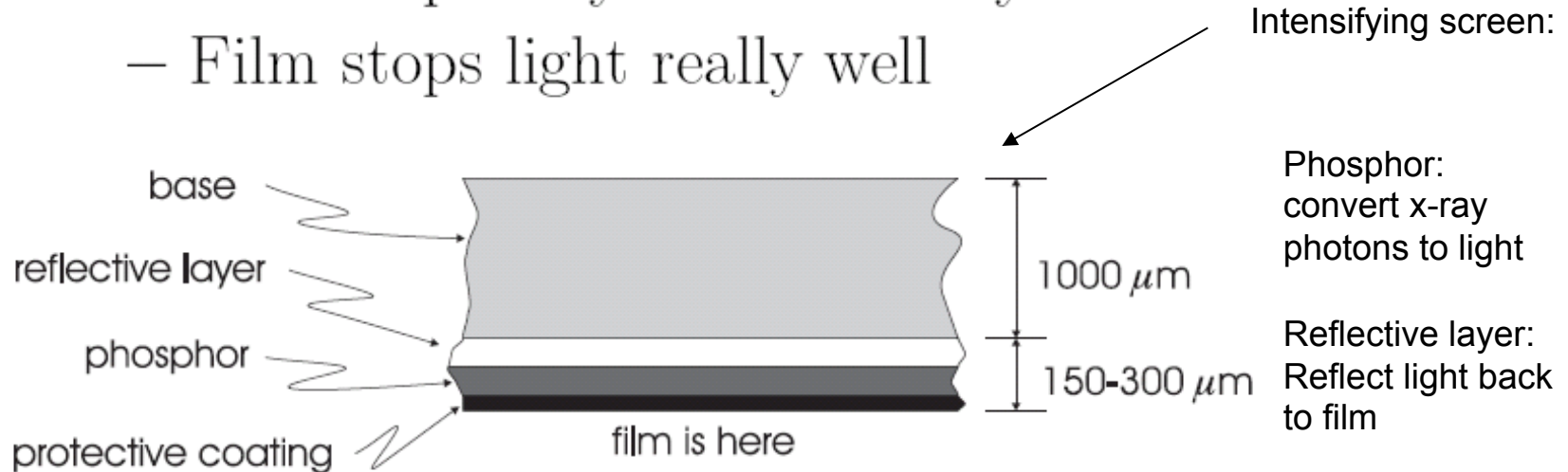
- Radiation is absorbed by grid
 - grid conversion factor

$$\text{GCF} = \frac{\text{mAs w/ grid}}{\text{mAs w/o grid}}$$

- Typical range $3 < \text{GCF} < 8$
- Grid visible on x-ray film
 - move grid during exposure
 - linear or circular motion

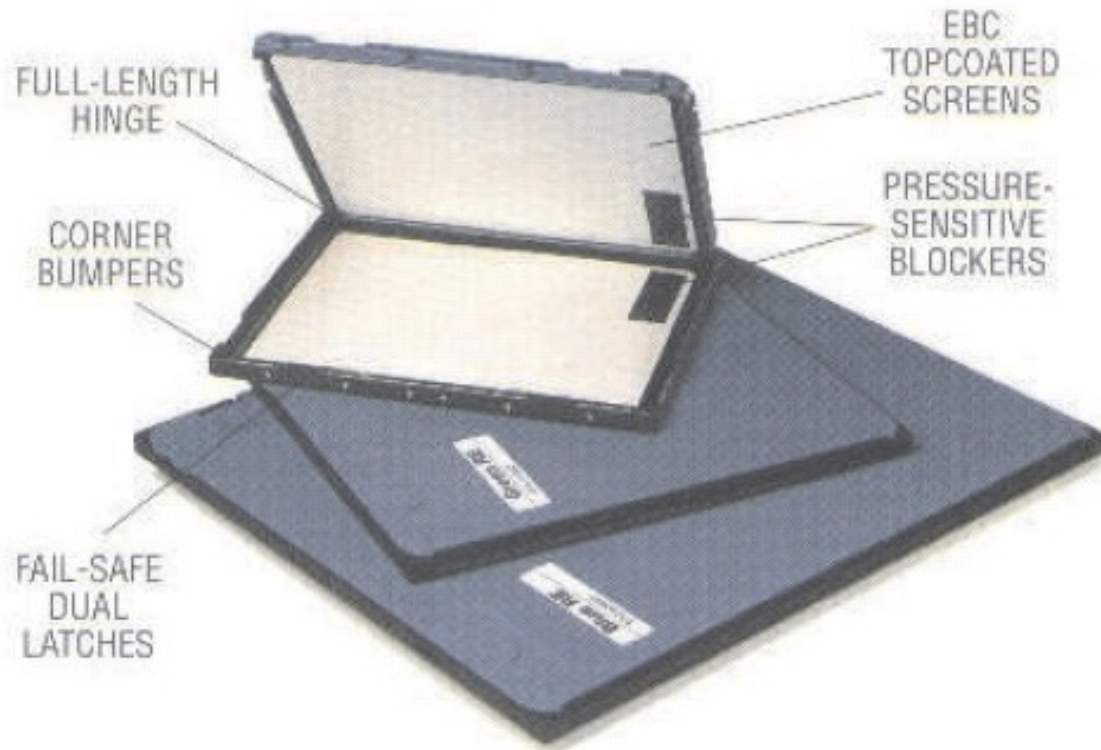
Film-Screen Detector

- Film stops only 1–2% of x-rays
- Film stops light really well



- Phosphor = calcium tungstate
- Flash of light lasts 1×10^{-10} second
- $\sim 1,000$ light photons per 50 keV x-ray photon

Radiographic Cassette



Digital Radiology

- Replace the intensifying screen/X-ray film by
 - flat panel detectors (FPD) using thin-film transistor (TFT) arrays
 - A scintillator
 - Consisting of many thin, rod-shaped cesium iodide (CsI) crystals
- When an X-ray is absorbed in a CsI rod, the CsI scintillates and produces light
- The light is converted into an electrical signal by a photodiode in the TFT array
- The electrical signal is amplified and converted to a digital value using an A/D converter
- A typical commercial DR system has flat panel dimensions of 41x41 cm, with an TFT array of 2048x2048 elements
- Ref: Webb, Introduction to biomedical imaging, Sec. 1.5.5

Biological effects of ionizing radiation

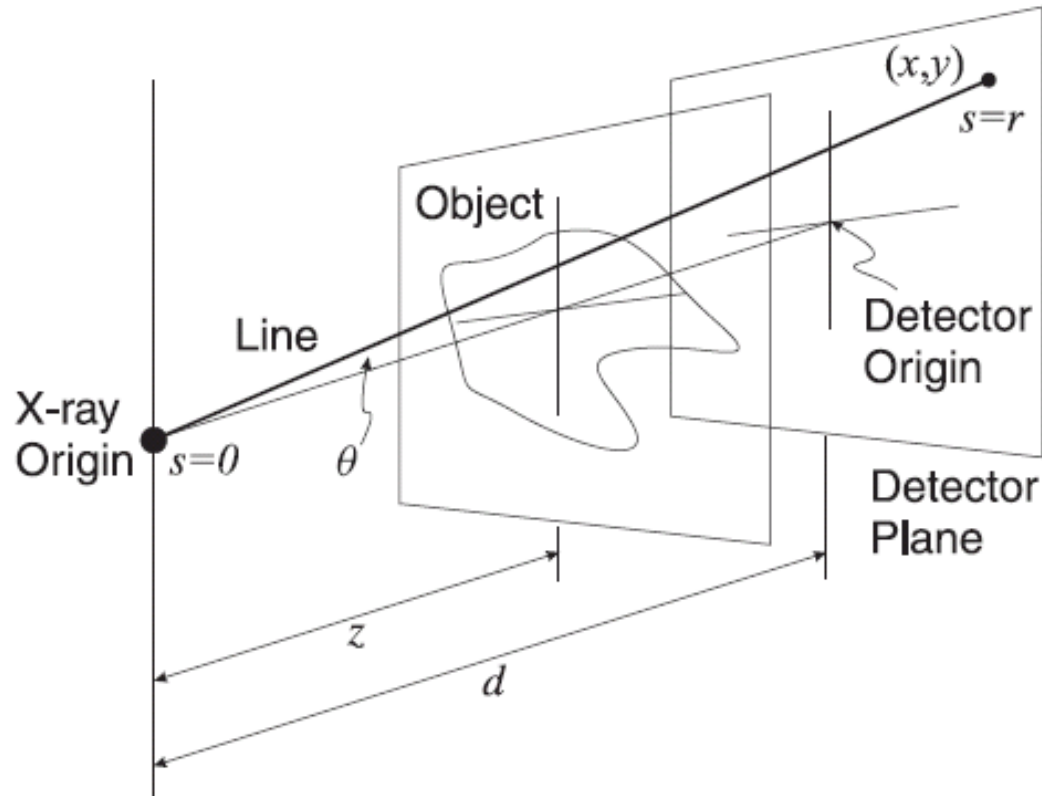
- Damage depends on deposited (= absorbed) energy (intensity \times time) per tissue volume
- Threshold: No minimum level is known, above which damage occurs
- Exposure time: Because of recovery, a given dose is less harmful if divided
- Exposed area: The larger the exposed area the greater the damage (collimators, shields!)
- Variation in Species / Individuals: LD 50/30 (lethal for 50% of a population over 30 days, humans \sim 450 rads / whole body irradiation)
- Variation in cell sensitivity: Most sensitive are nonspecialized, rapidly dividing cells (Most sensitive: White blood cells, red blood cells, epithelial cells. Less sensitive: Muscle, nerve cells)
- Short/long term effects: Short term effects for unusually large (> 100 rad) doses (nausea, vomiting, fever, shock, death); long term effects (carcinogenic/genetic effects) even for diagnostic levels \Rightarrow maximum allowable dose 5 R/yr and 0.2 R/working day [Nat. Counc. on Rad. Prot. and Meas.]

[From Graber, Lecture Note for BMI1-FS05]

Image Formation

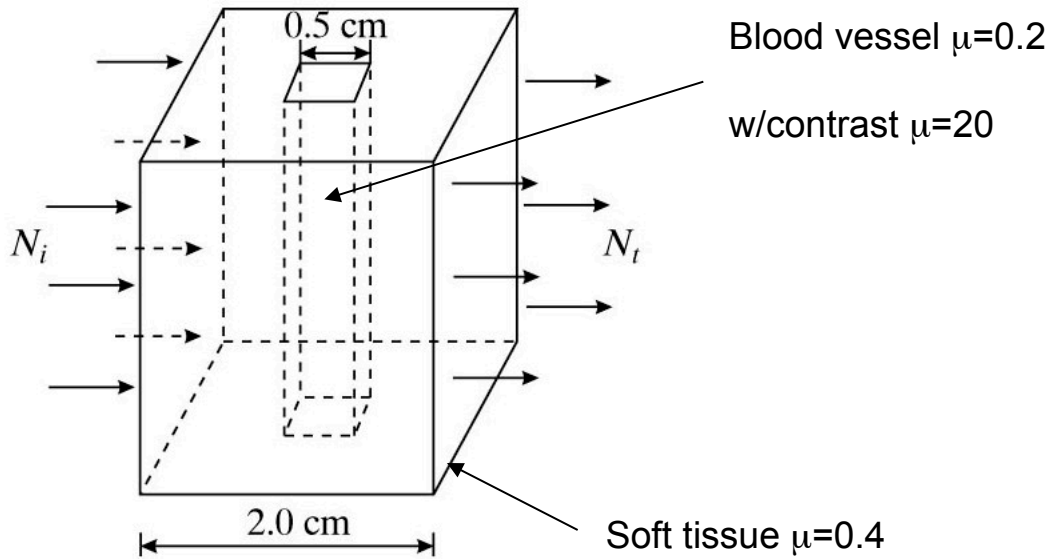
- Basic imaging equation
- Geometric effects
- Extended source
- Film blurring
- Impact of noise and scattering

Basic Imaging Equations



$$I(x, y) = \int_0^{\infty} S_0(E') E' \exp \left\{ - \int_0^{r(x, y)} \mu(s; E', x, y) ds \right\} dE'$$

Example



w/o contrast :

$$I_b = I_{\min} = I_0 e^{-(0.4 \cdot 2.0)};$$

$$I_o = I_{\max} = I_0 e^{-(0.4 \cdot 1.5 + 0.2 \cdot 0.5)}$$

$$\text{Local contrast : } C_1 = \frac{I_o - I_b}{I_b};$$

$$\text{Global contrast : } C = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}}$$

w/ contrast :

$$I_b = I_{\max} = I_0 e^{-(0.4 \cdot 2.0)};$$

$$I_o = I_{\min} = I_0 e^{-(0.4 \cdot 1.5 + 20 \cdot 0.5)}$$

$$\text{Local contrast : } C_1 = \frac{|I_o - I_b|}{I_b};$$

$$\text{Global contrast : } C = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}}$$

- 1) What is the local contrast of the blood vessel?
- 2) What is the local contrast of the blood vessel when contrast agent is injected?

Geometric Effects

- X-rays are diverging from source
- Undesirable effects:
 - $\cos^3 \theta$ falloff across detector
 - anode heel effect
 - pathlength irregularities
 - magnification
- I_0 is intensity at $(0, 0)$
- r is distance from (x, y) to x-ray origin
- θ is angle between $(0, 0)$ and (x, y)

Inverse Square Law

- Net flux of photons decrease as $1/r^2$.

Therefore

$$I_0 = \frac{I_S}{4\pi d^2} \quad I_r = \frac{I_S}{4\pi r^2}$$

- Eliminate source intensity I_S

$$I_r = I_0 \frac{d^2}{r^2}$$

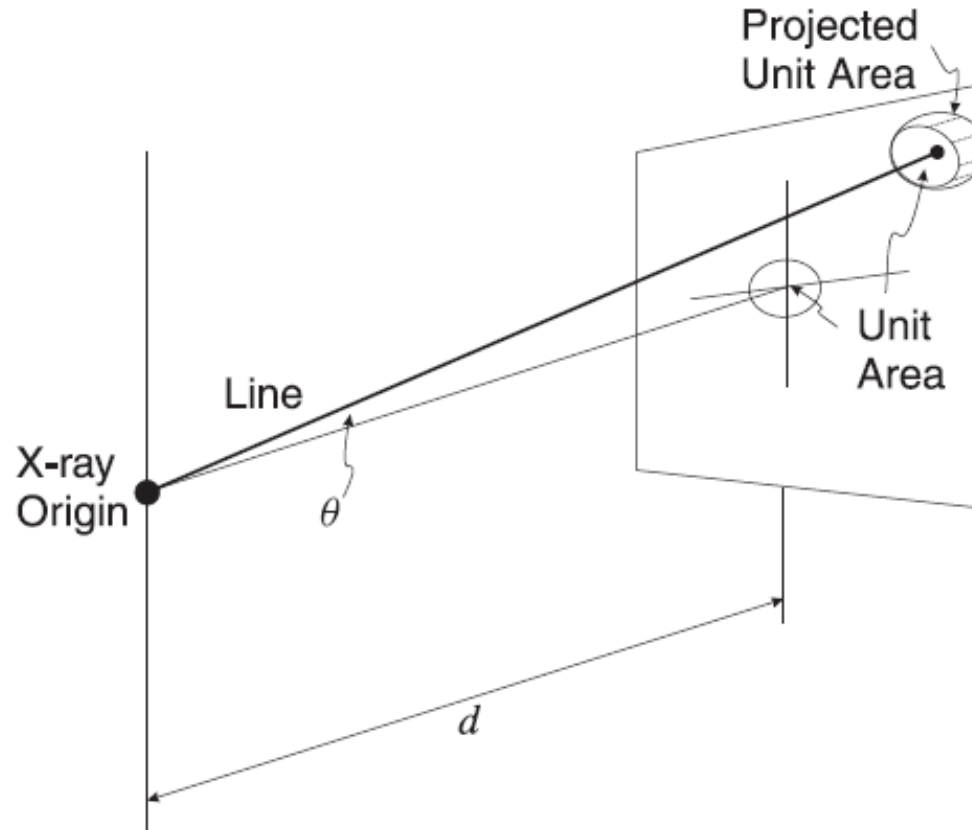
- Since $\cos \theta = d/r$

$$I_r = I_0 \cos^2 \theta$$

I_0 is the detected flux at the origin of the detector plane

I_r is the detected flux at an arbitrary point of the detector plane with angle θ w/o considering the oblique effect discussed in the next page

Obliquity



- Intensity is

I_0 should be replaced by I_r

$$I_d = I_0 \cos \theta$$

Overall Effect of Beam Divergence

- Inverse square law and obliquity combine

$$I_d(x_d, y_d) = I_0 \cos^3 \theta$$

- Can usually be ignored. Why?
 - Detector is far away
 - Field of view (FOV) is often small

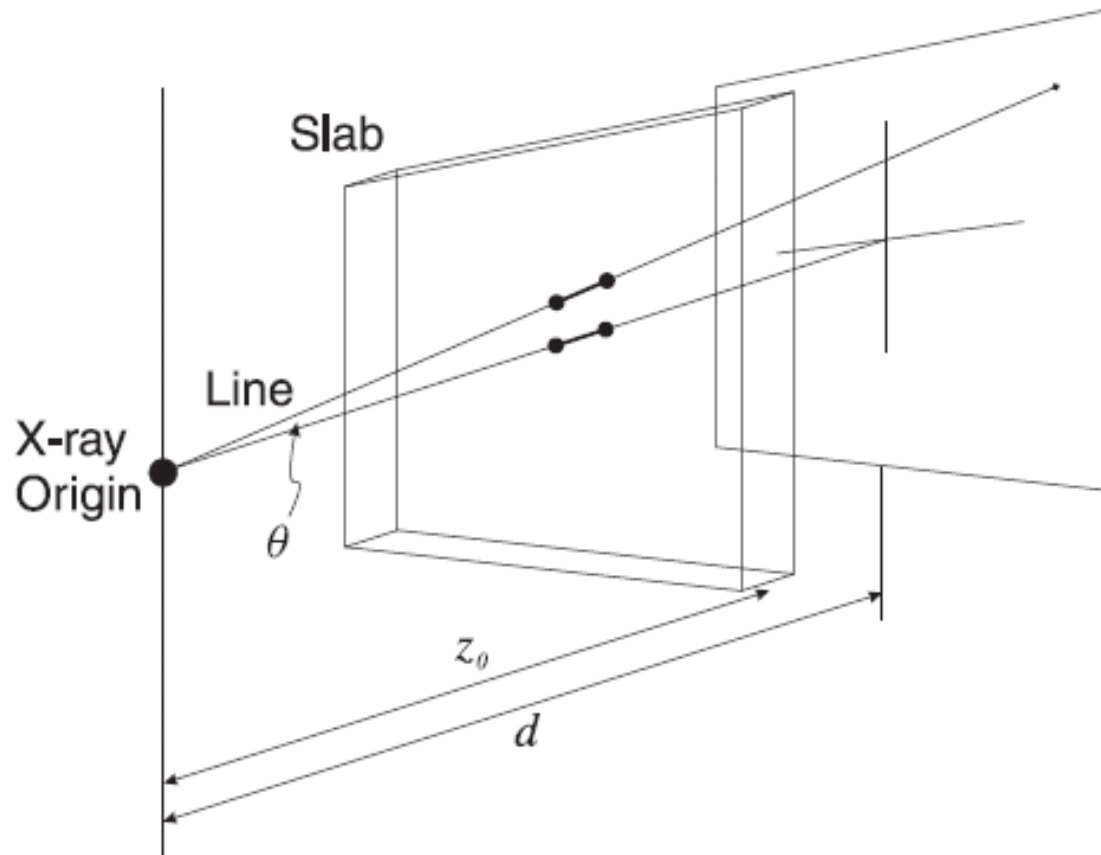
→ θ is small

Anode Heel Effect

- Intensity within the x-ray cone
 - Not uniform
 - stronger in the cathode direction
 - 45% variation is typical
- Compensate, use to advantage, or ignore
- We will ignore in math

Imaging of a Uniform Slab

- Uniform slab yields different intensities



-
- Intensity on detector

$$I_d(x, y) = I_0 \exp\{-\mu L / \cos \theta\}$$

- Including inverse square law and obliquity:

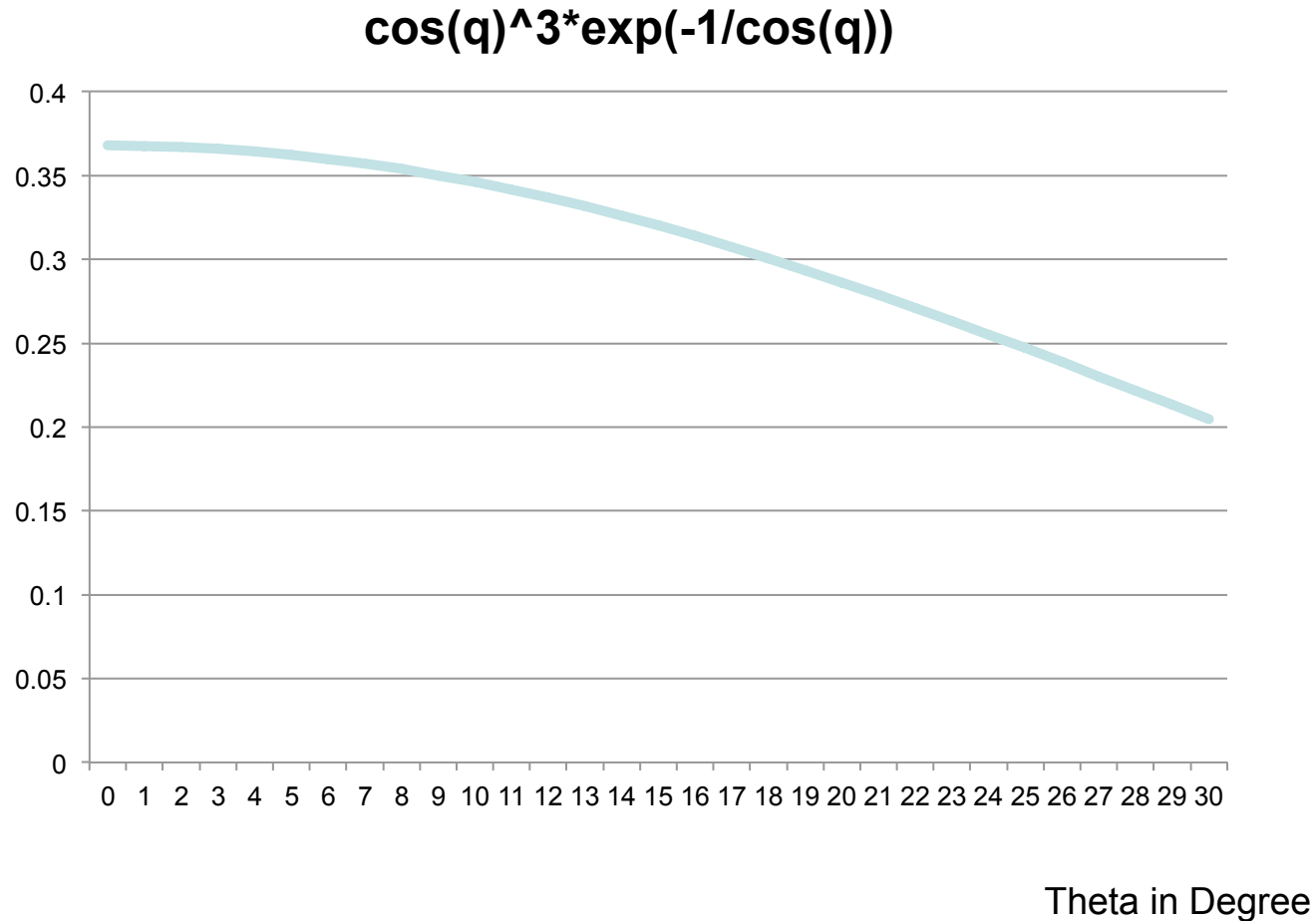
$$I_d(x, y) = I_i \cos^3 \theta \exp\{-\mu L / \cos \theta\}$$

- If $d \approx r$ all effects can be ignored

$$I_i = I_s / (4 \pi d^2)$$

Illustrate the received intensity as function of y or x or θ

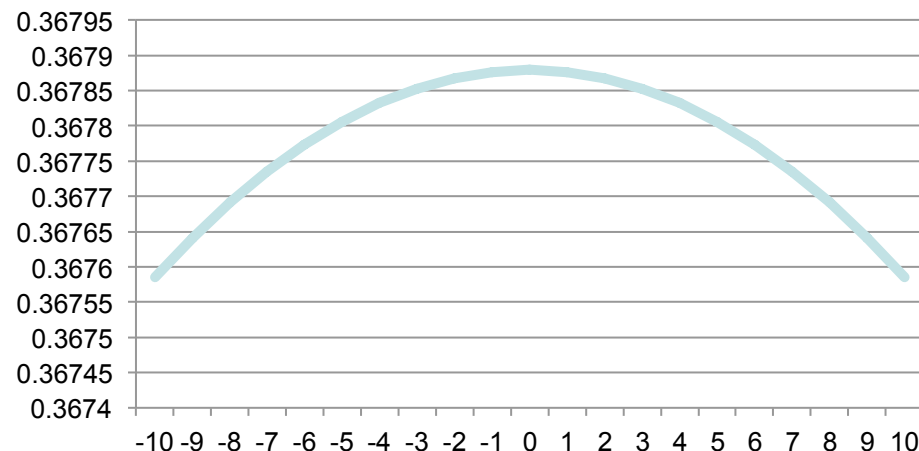
Received Signal as a Function of Theta



This plot assumes $\mu \cdot L = 1$, e.g. $\mu = 1/\text{cm}$, $L = 1\text{cm}$.

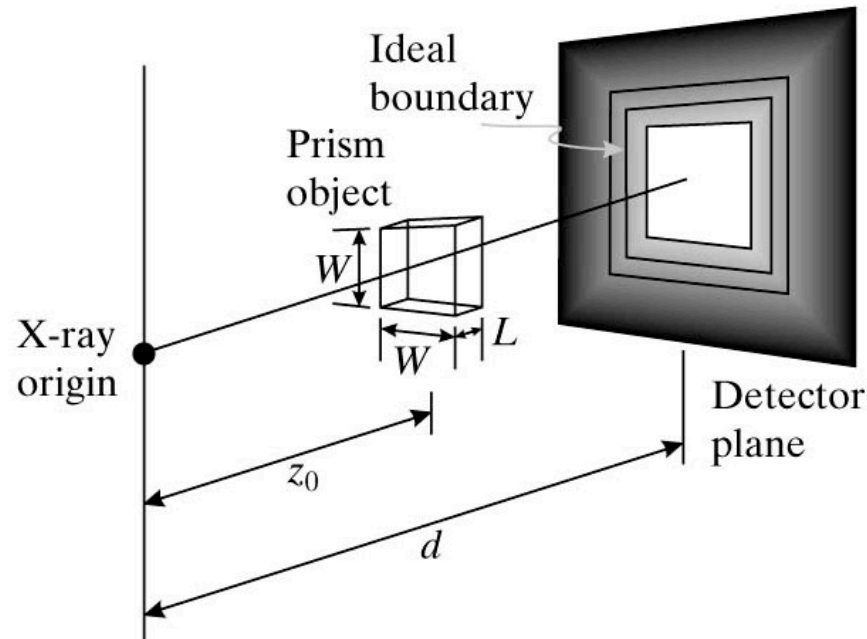
-
- How does it vary as a function of Y when $x=0$ (vertical axis of the detector plain)?
 - $\cos(q) = d/r = d/\sqrt{d^2+y^2}$
 - Assuming $d=5m$, $y= -10cm$ to $10cm$ (q from 0 to 1.14 degree)
 - Vary small relative change in the range of y

intensity as function of y



Example: Image of a prism due to a point source

Consider the x-ray imaging of a cube. Determine the intensity of detected photons along the y axis on the detector plane. Express your solution in terms of the angle q . Sketch this function. You should consider the inverse square law and the oblique effect. Assume the x-ray source is an ideal point source with intensity I_0 , and the object has a constant linear attenuation coefficient m . (Example 5.4 in textbook)

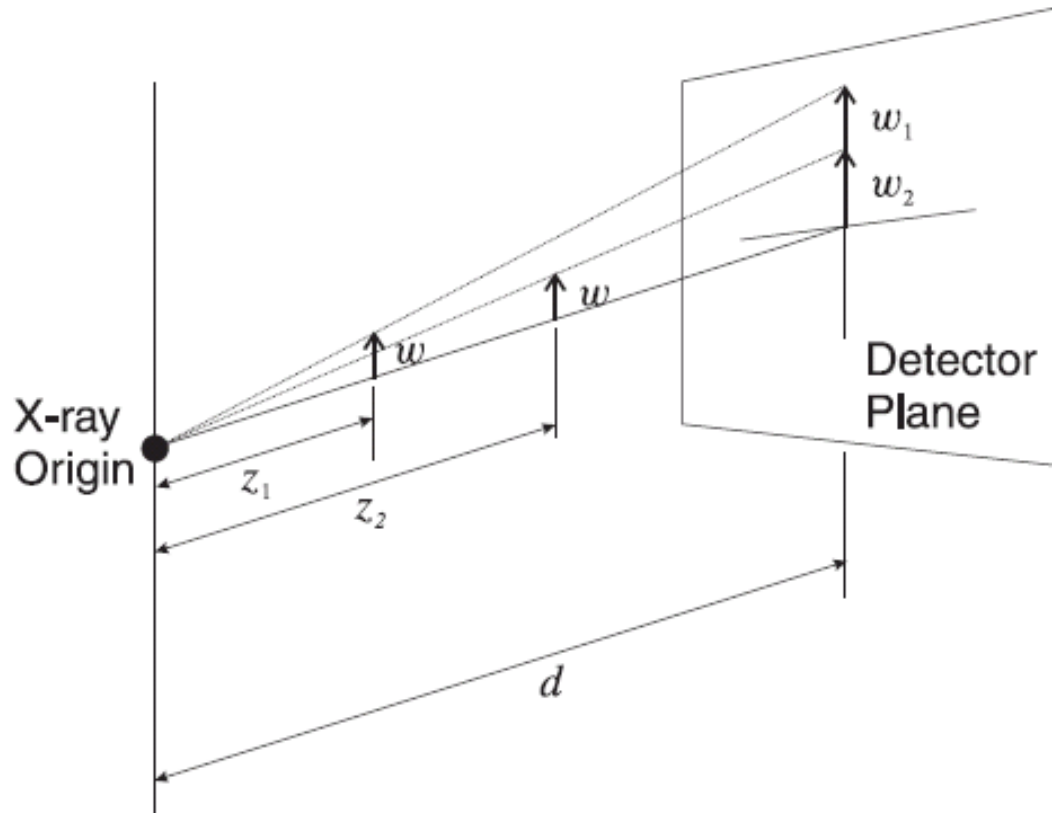


Solution

Sketch over in class. Also see textbook
Must consider different regions separately

Objects Magnification

- Size on detector depends on distance from source



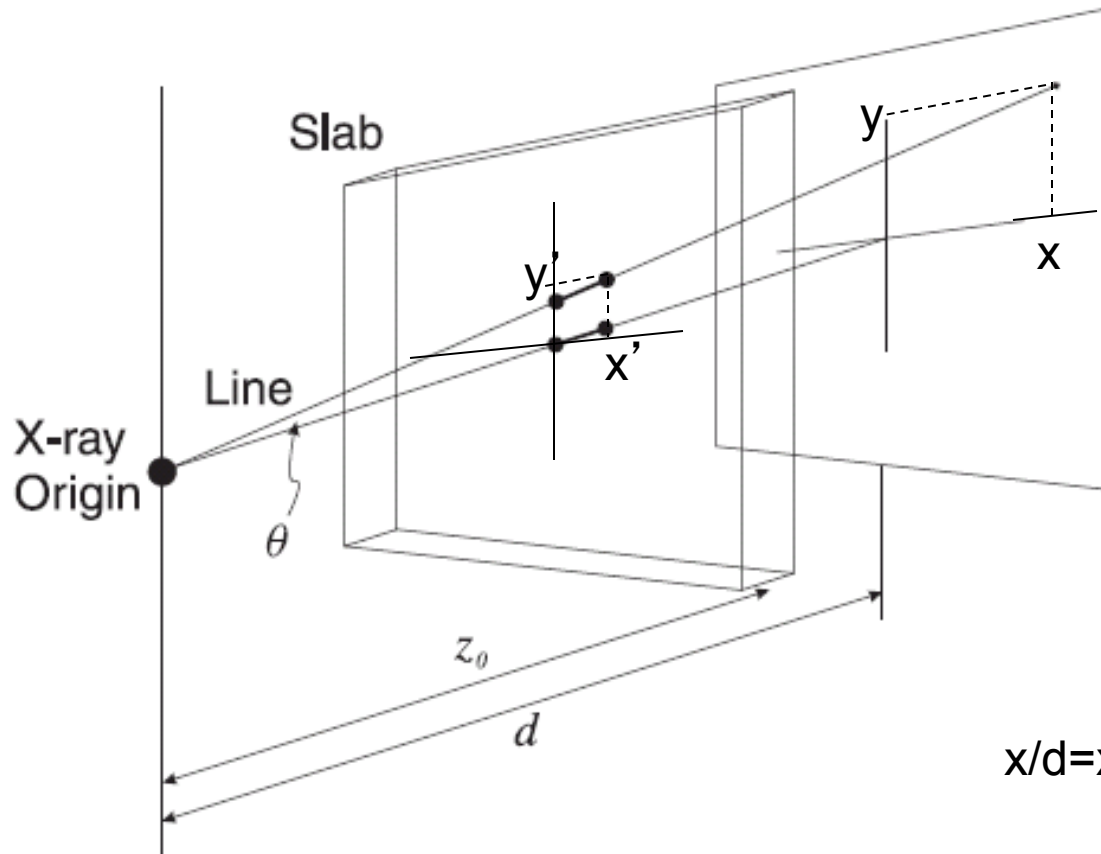
$$w_z = w \frac{d}{z}$$

Magnification factor:

$$M(z) = \frac{d}{z}$$

Imaging of a Thin Non-Uniform Slab

- Assume a very thin slab at z
 - the linear absorption coefficient at (x', y') is $\mu(x', y')$
 - Detector position (x, y) \rightarrow slab position (x', y')



$$x/d = x'/z \rightarrow x' = x z/d = x /M(z)$$

-
- Let “transmittivity” be

$$t_z(x, y) = \exp\{-\mu(x, y)\Delta z\}$$

- On detector, intensity is

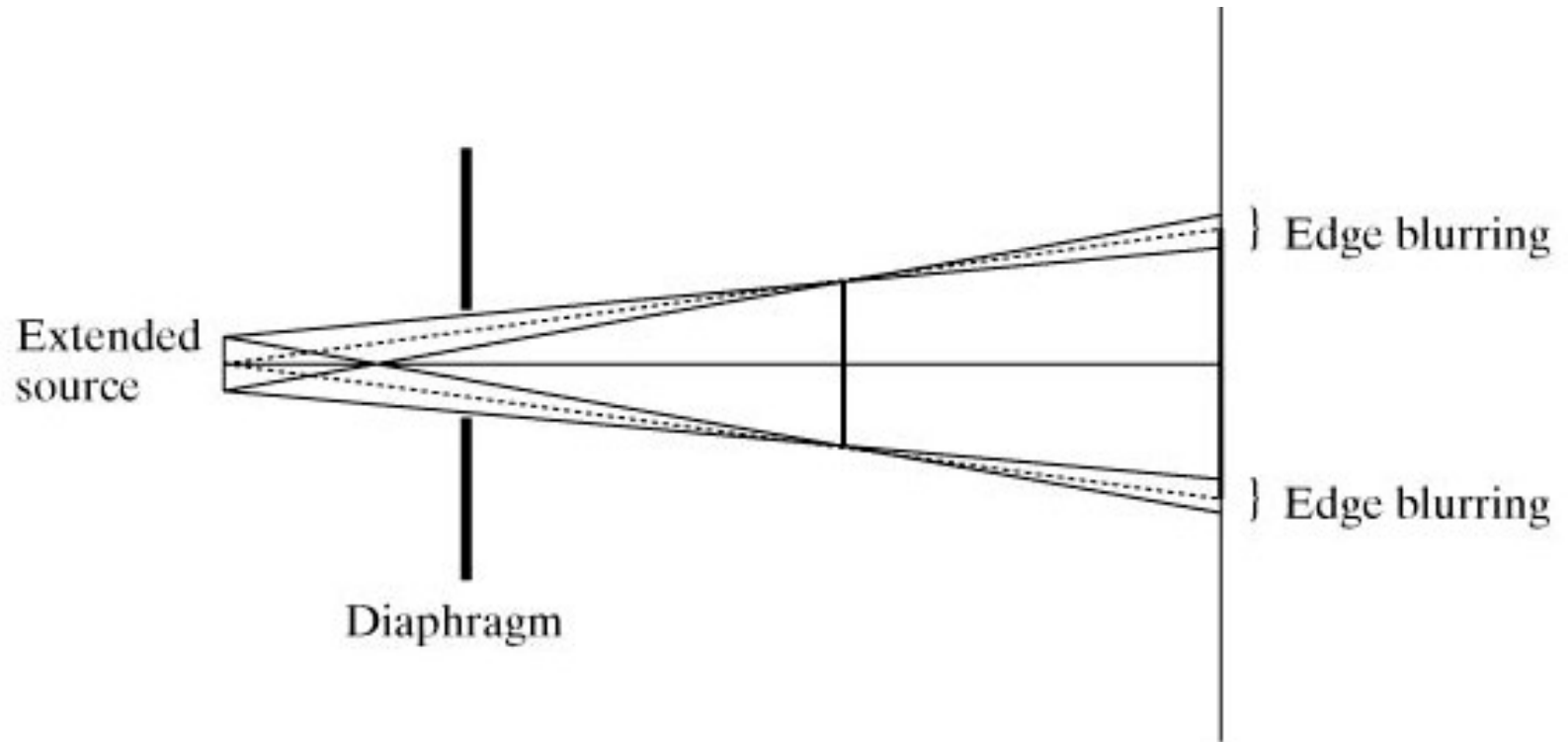
$$I_d(x, y) = I_0 \cos^3 \theta t_z\left(\frac{x}{M(z)}, \frac{y}{M(z)}\right)$$

- After substitution

$$I_d(x, y) = I_0 \left(\frac{d}{\sqrt{d^2 + x^2 + y^2}}\right)^3 t_z\left(\frac{xz}{d}, \frac{yz}{d}\right)$$

$$I_0 = I_s / (4 \pi d^2)$$

Blurring Due to Extended Source



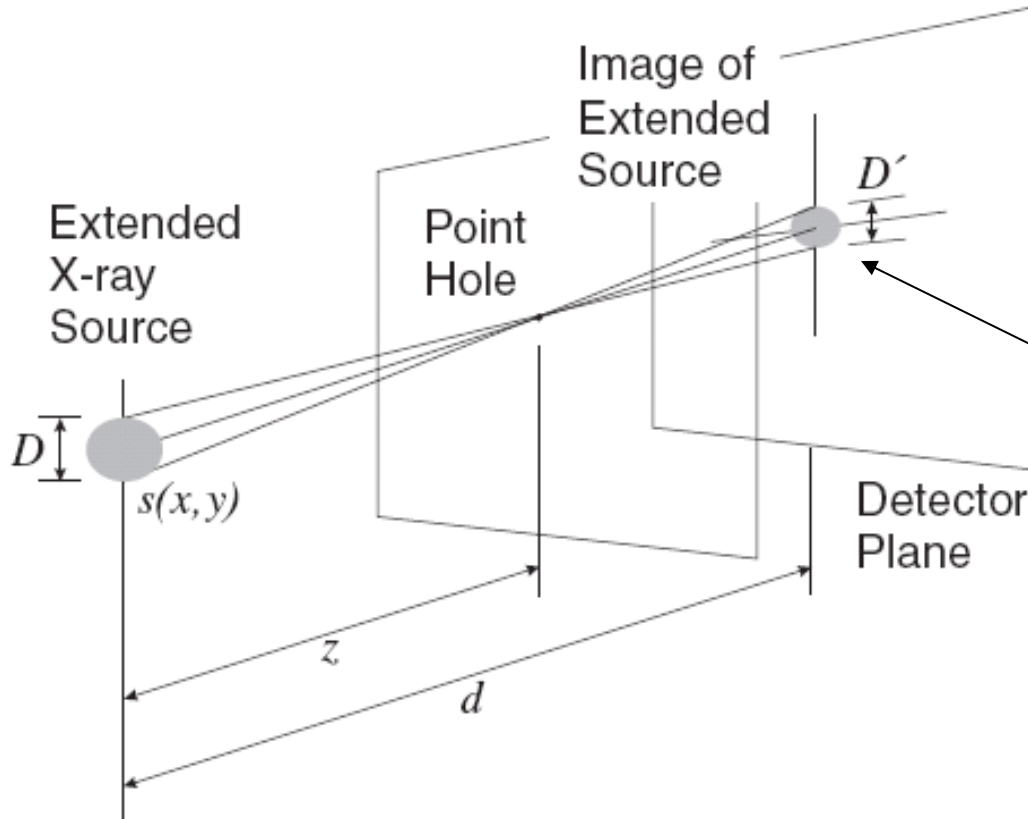
First study the image through a pinhole ^(c)

- Impulse response

Image through an arbitrary objects

- Impulse response * object attenuation profile

Image of source through a pinhole



Pinhole: a infinitesimal hole (area=0) that passes the X-ray source w/o attenuation. Everywhere else the X-ray is completely absorbed

Reversed image

$$D' / (d-z) = -D/z \rightarrow D' = -D (d-z)/z = Dm$$

- Source magnification:

$$m(z) = -\frac{d-z}{z} = 1 - M(z)$$

Call the following $h(x,y)$ (response due to a pinhole at (0,0))

- Image of source through pinhole at z

$$I_d(x, y) = \frac{\cos^3 \theta}{4\pi d^2 m^2} s\left(\frac{x}{m}, \frac{y}{m}\right)$$

Scale factor due to pinhole (See textbook)

Loss of source intensity due to inverse square law

Image of an Arbitrary Slice

- An arbitrary slab at z can be thought of as many pinholes at different locations (x', y') , each with transmittivity $t_z(x', y')$
 - *The received signal due to transmittivity at (x', y') can be written as $h(x-x', y-y') t_z(x', y')$ assuming the system is translation invariant*
- The image of the slab is a sum of individual images of the source through all the pinholes multiplied by the respective transmittivity
 - $I_d(x, y) = \int_{\{x', y'\}} h(x-x', y-y') t_z(x', y') dx' dy'$
- The overall effect can be captured through linear convolution

$$I_d(x, y) = \frac{\cos^3 \theta}{4\pi d^2 m^2} t_z \left(\frac{x}{M}, \frac{y}{M} \right) * s \left(\frac{x}{m}, \frac{y}{m} \right)$$

Note: m depends on z , distance of slab to the source

Example

- Source is a circular disk with diameter D
- Object is square plane with dimension W at distance z
- Detector plane at distance d from source
- How does the detected image look for $d=2Z$ and $d=3Z$
- Note that the blurring of the edge depends on z

- What is $t_z(x,y)$ and $s(x,y)$?
- What is $I_d(x,y)$?
- How is $I_d(x,y)$ related with $t_z(x,y)$?
- How does the image of $I_d(x,y)$ look?

Example: solution

$T_z(x,y)$: a square with width W

$S(x,y)$: a disk with diameter D . Assuming $D \ll W$,

- For $d=2z$, $M=d/z=2$, $m=1-M=-1$

$T_z(x/M,y/M)$: a square with width $2W$

$S(x/m,y/m)$: a disk with diameter D

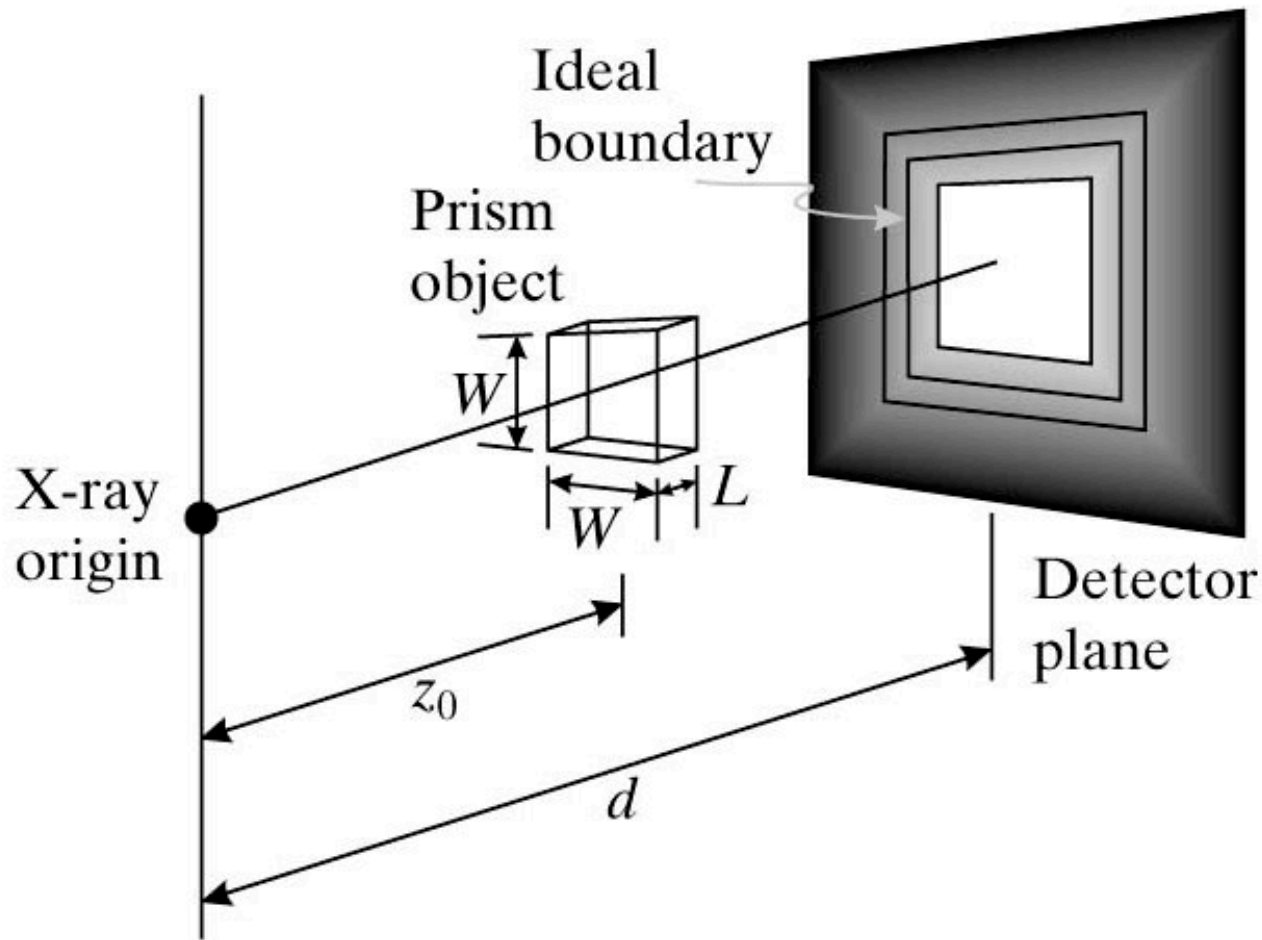
The resulting detector image is a square with width $2W$ but with a blurred edge with blurring width D

- For $d=3z$, $M=d/Z=3$, $m=1-M=-2$

$T_z(x/M,y/M)$: a square with width $3W$

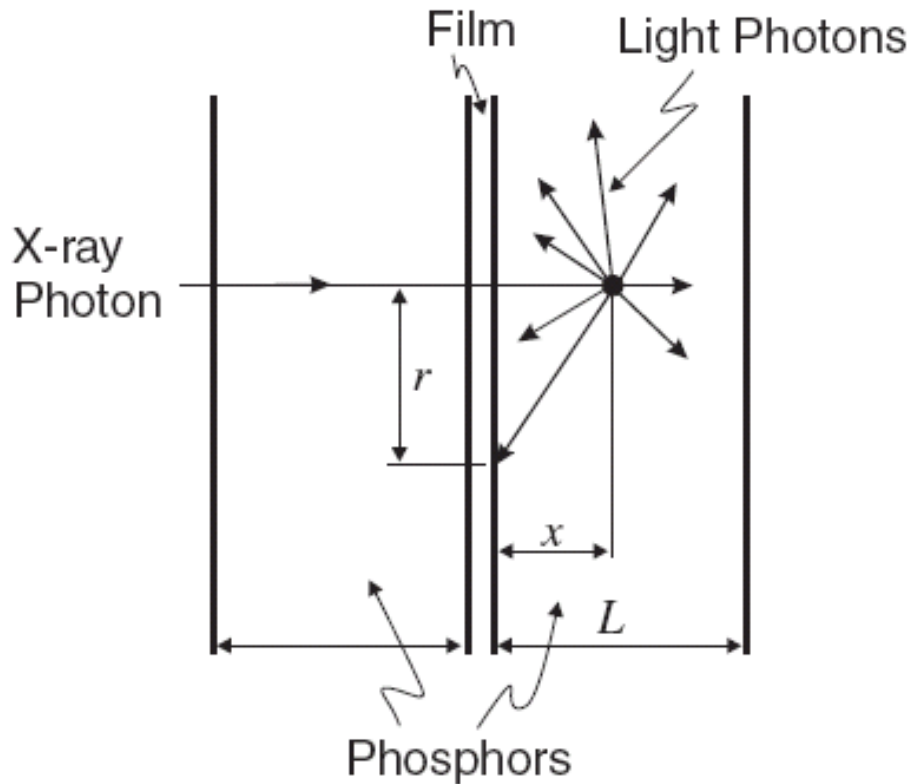
$S(x/m,y/m)$: a disk with diameter $2D$

The resulting detector image is a square with width $3W$ but with a blurred edge with blurring width $2D$



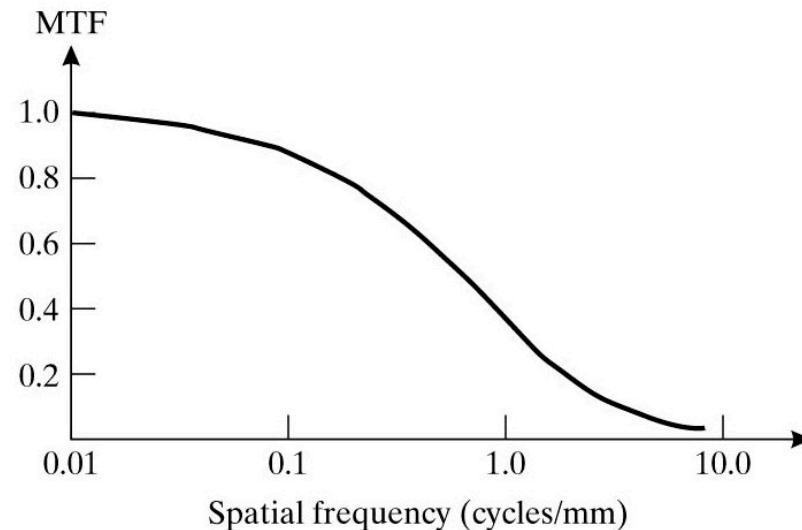
For the previous example, L is very small, but the source has diameter D , blurring is due to the source diameter being non-zero

Film Screen Blurring



A single x-ray photon causes a blurry spot on the film which is effectively the “impulse response” to the x-ray impulse $h(x,y)$

Typical MTF for a film-screen detector



Overall Imaging Equation

- Including all effects (geometric, extended source, film-screen blurring), the image corresponding to a slab at z with transmittivity function $t_z(x,y)$ is

$$I_d(x, y) = \cos^3 \theta \frac{1}{4\pi d^2 m^2} s \left(\frac{x}{m}, \frac{y}{m} \right) * t_z \left(\frac{x}{M}, \frac{y}{M} \right) * h(x, y)$$

- For an object with a certain thickness, the transmittivity function must be modified to reflect the overall attenuation along the z -axis
- When the source is polyenergetic, integration over photon energy is additionally needed

Example

- In the previous example, how would the image look if the film blurring is a box function of width h ?

Film Characteristics

- Film darkening (after development) depends on incident light (which depends on the incident x-ray)

- Optical density

$$D = \log_{10} \frac{I_i}{I_t}$$

- Usable densities $0.25 < D < 2.25$
- Best densities $1.0 < D < 1.5$

Optical Density vs. Exposure

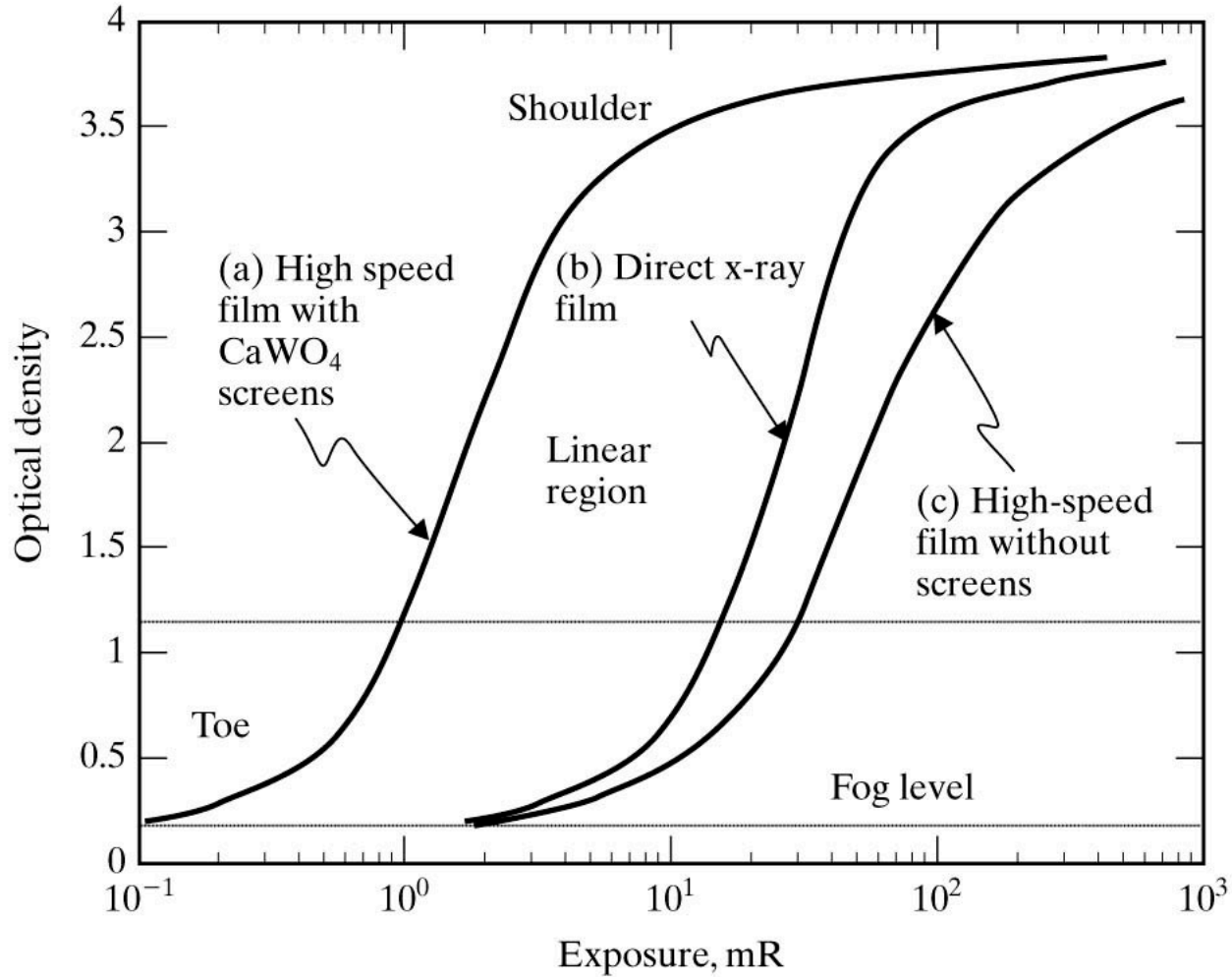
- X-ray exposure yields optical density

$$D = \Gamma \log_{10} \frac{X}{X_0}$$

- Γ is film gamma
- Typical ranges: $0.5 < \Gamma < 3.0$
- Latitude is range exposures where relationship is linear
- Speed is inverse of exposure at which

$$D = 1 + \text{fog level}$$

The H&D Curve



Effect of Noise

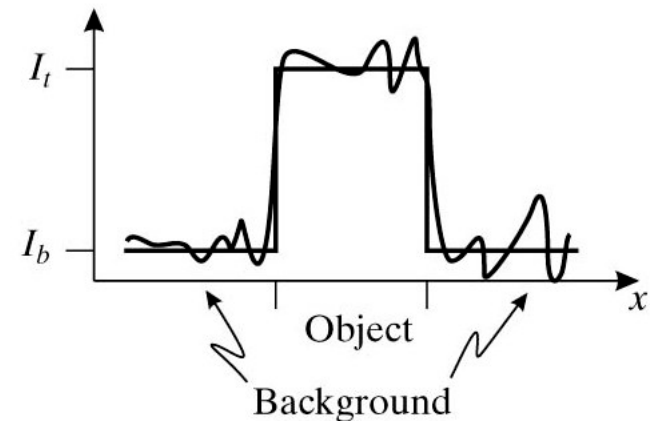
- Source of noise:
 - Detector does not faithfully reproduce the incident intensity
 - X-rays arrive in discrete packets of energy. This discrete nature can lead to fluctuations in the image

- Local contrast

$$C = \frac{I_t - I_b}{I_b}$$

- Signal is $I_t - I_b$
- Noise is due to Poisson behavior
- Variance of noise in background: σ_b^2
- Signal to noise

$$\text{SNR} = \frac{I_t - I_b}{\sigma_b} = \frac{CI_b}{\sigma_b}$$



How is noise related to signal?

- Assuming the number of photons in each burst follows the Poisson distribution
 - $P(N=k) = (a^k / k!) e^{-a}$
 - Variance = mean = a

- Let N_b denotes the average number of photons per burst per area
- Let $h\nu$ denotes the effective energy for the X-ray source
- The average background intensity is

$$I_b = \frac{N_b h\nu}{A\Delta t}$$

- The variance of photon intensity is

$$\sigma_b^2 = N_b \left(\frac{h\nu}{A\Delta t} \right)^2$$

- The SNR is $SNR = C\sqrt{N_b}$

If X is an RV with mean η_x , variance σ_x^2

$Y = aX$ is a RV with mean $\eta_y = a\eta_x$, variance $\sigma_y^2 = a^2\sigma_x^2$

- SNR can be improved by
 - Increasing incident photon count
 - Improving contrast

Detective Quantum Efficiency

- How good is a detector?
- Consider:
 - Potential SNR before detection
 - Actual SNR upon detection
- Detective Quantum Efficiency

$$\text{DQE} = \left(\frac{\text{SNR}_{\text{out}}}{\text{SNR}_{\text{in}}} \right)^2$$

- Degradation of SNR during detection

When a x-ray source has mean intensity $m=N_b$, and variance $s^2=N_b$,
 $\text{SNR} = m/s = \sqrt{N_b}$

Example

- Suppose an X-ray tube is set up to fire bursts of photons each with $N=10000$ photons and the detector's output (# of detected photons per burst) x has a mean = 8000, variance = 40000. What is its DQE?
- Solution:

The actual # of photons fired at the x - ray tube follows the Poisson process (mean = variance = 10000)

$$\text{SNR}_{\text{in}} = \frac{\text{mean}}{\sqrt{\text{variance}}} = \frac{10000}{\sqrt{10000}} = 100$$

The #of detected photons has mean = 8000, variance = 40000

$$\text{SNR}_{\text{out}} = \frac{\text{mean}}{\sqrt{\text{variance}}} = \frac{8000}{\sqrt{40000}} = \frac{8000}{200} = 40$$

$$\text{DQE} = \left(\frac{\text{SNR}_{\text{out}}}{\text{SNR}_{\text{in}}} \right)^2 = 0.16$$

This means that only about 16% of photons are detected correctly

Effect of Compton Scattering

- Compton scattering causes the incident photons to be deflected from their straight line path
 - Add a constant intensity I_s in both target and background intensity (“fog”)
 - Decrease in image contrast
 - Decrease in SNR

W/o scattering :

target intensity : I_t

background intensity : I_b

$$\text{contrast } C = \frac{I_t - I_b}{I_b}$$

$$\text{SNR} = C \frac{I_b}{\sigma_b} = C \sqrt{N_b}$$

W/ scattering :

target intensity : $I_t + I_s$

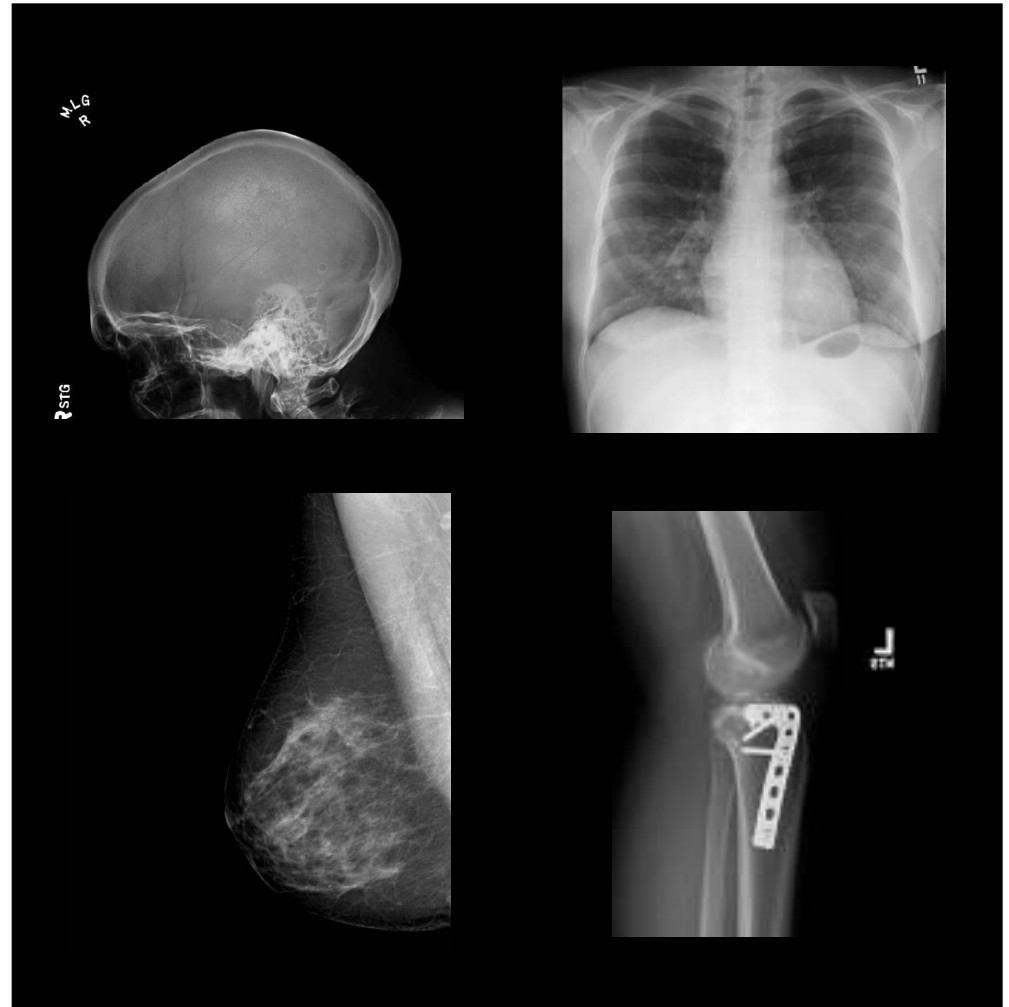
background intensity : $I_b + I_s$

$$\text{contrast } C' = \frac{I_t - I_b}{I_b + I_s} = \frac{I_b}{I_b + I_s} C = \frac{C}{1 + I_s / I_b}$$

$$\text{SNR}' = C \frac{I_b}{\sigma_b'} = C \frac{N_b}{\sqrt{N_b + N_s}} = C \frac{\sqrt{N_b}}{\sqrt{1 + N_s / N_b}} = \text{SNR} \frac{1}{\sqrt{1 + I_s / I_b}}$$

Medical Applications

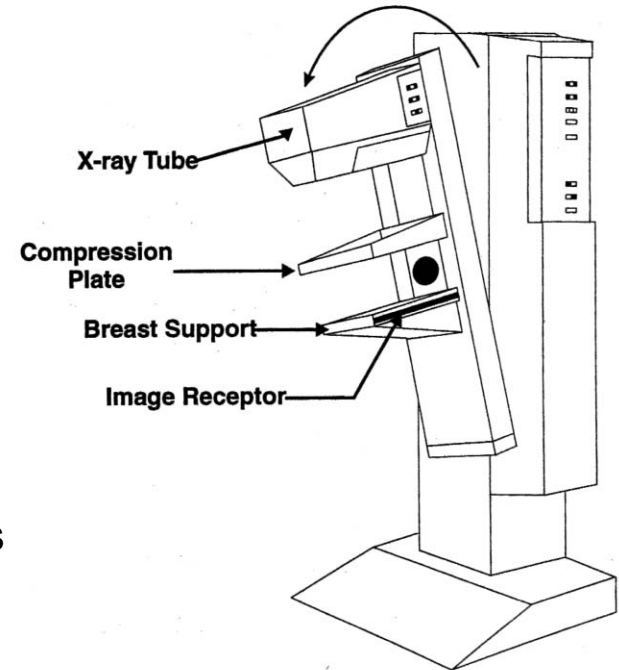
- Orthopedic
- Chest
- Abdomen
- Mammography
- Angiography



[From Graber, Lecture Note for BMI1-FS05]

Mammography

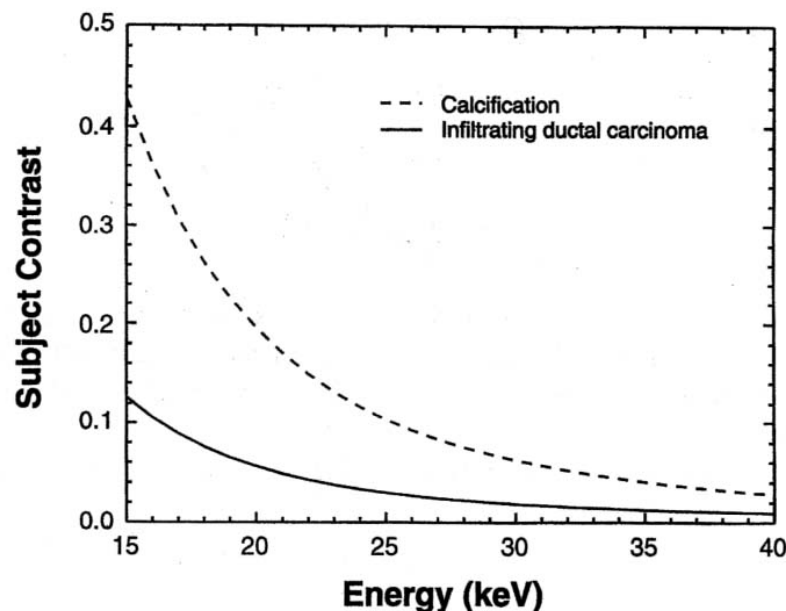
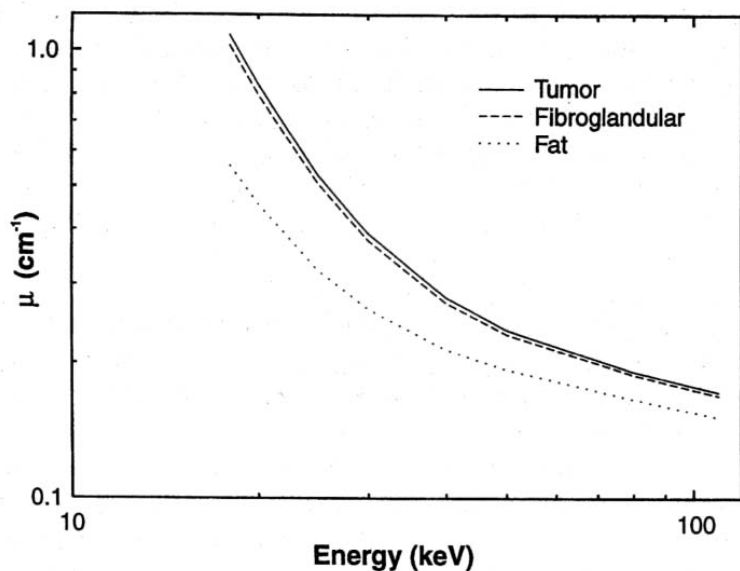
- Detection and diagnosis (symptomatic and screening) of breast cancer
- Pre-surgical localization of suspicious areas
- Guidance of needle biopsies.
- Breast cancer is detected on the basis of four types of signs on the mammogram:
 - Characteristic morphology of a tumor mass
 - Presentation of mineral deposits called microcalcifications
 - Architectural distortions of normal tissue patterns
 - Asymmetry between corresponding regions of images on the left and right breast
- ⇒ Need for good image contrast of various tissue types.
- Simple x-ray shadowgram from a quasi-point source.



[From Graber, Lecture Note for BMI1-FS05]

Mammography contrast

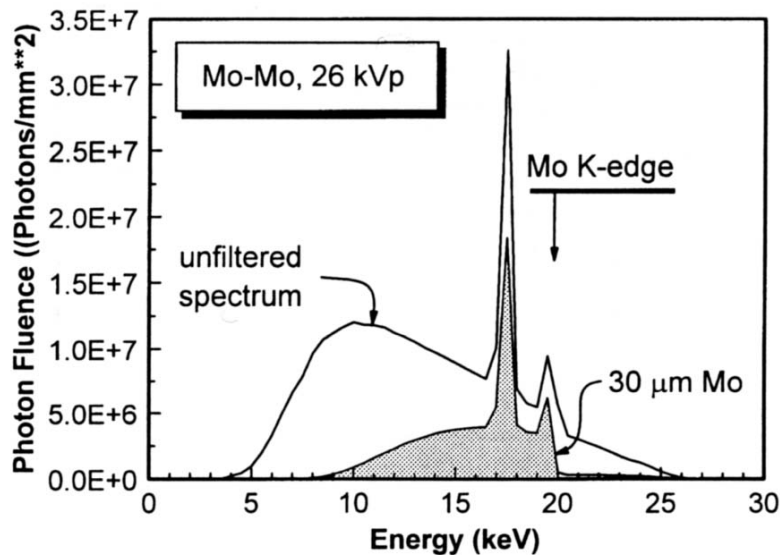
- Image contrast is due to varying linear attenuation coefficient of different types of tissue in the breast (adipose tissue (fat), fibroglandular, tumor).
- Ideal energy distribution of X-ray should be below 20 for average size breast, slightly higher for denser breast



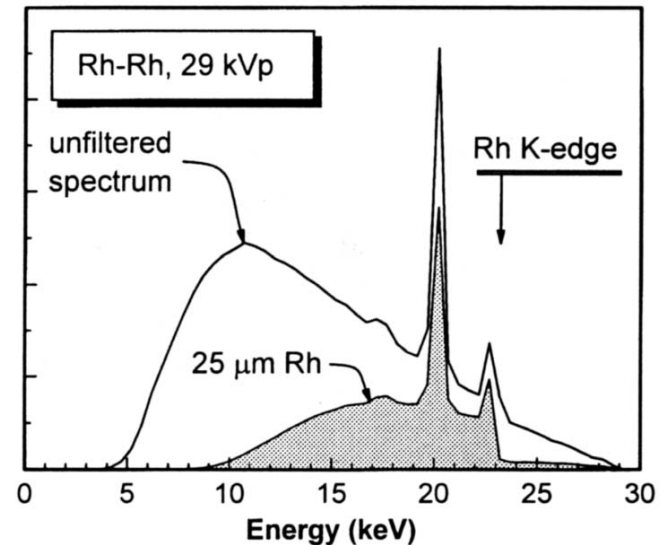
[From Graber, Lecture Note for BMI1-FS05]

Mammography source

- Voltage ~ 25-30 kVp
- Anode material Mo (Molybdenum), Rh (Rhodium) (characteristic peaks at 17.9 and 19 for Mo, and slightly higher for Rh)
- Filtering: use Mo or Rh to absorb energy above 20 or 25Kev



Target Mo, Filter Mo

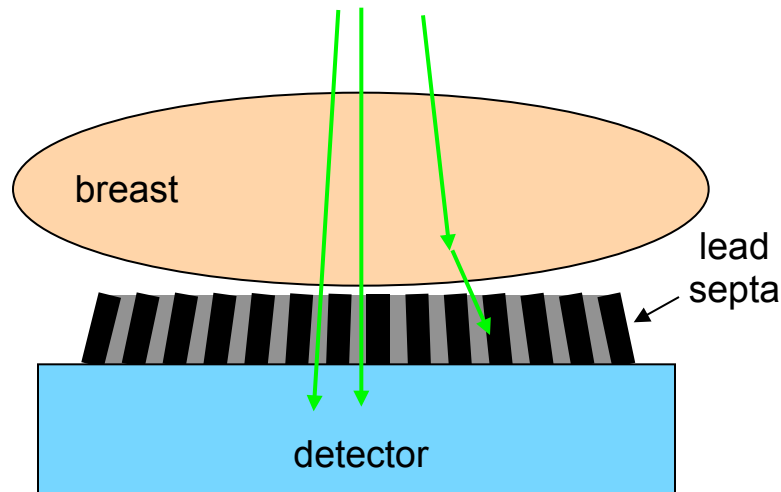


Target Rh, Filter Rh

[From Graber, Lecture Note for BMI1-FS05]

Anti-scatter grid

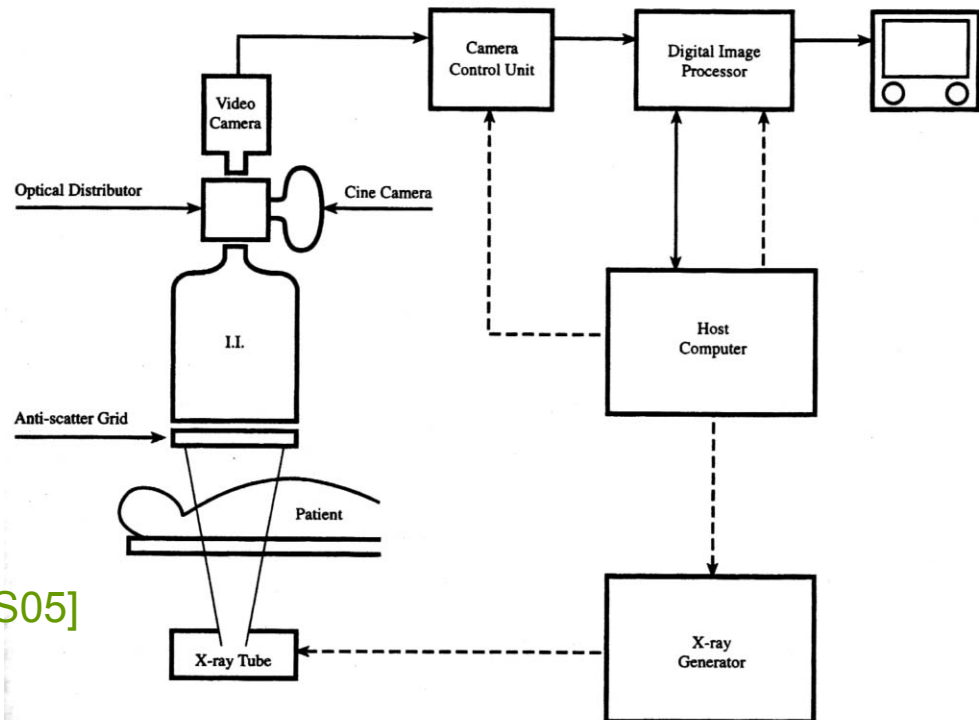
- Significant Compton interaction for low E_p (37-50% of all photons).
- Linear grid: Lead septa + interspace material. Septa focused toward source. Grid ratio ~ 3.5 -5:1. Only scatter correction in one dimension. Scatter-to-primary (SPR) reduction factor ~ 5
- Recently crossed grid introduced
- Grids are moved during exposure
- Longer exposure



[From Graber, Lecture Note for BMI1-FS05]

X-ray projection angiography

- Imaging the circulatory system. Contrast agent: Iodine (Z=53) compound; maximum iodine concentration $\sim 350 \text{ mg/cm}^3$
- Monitoring of therapeutic manipulations (angioplasty, atherectomy, intraluminal stents, catheter placement).
- Short intense x-ray pulses to produce clear images of moving vessels. Pulse duration: 5-10 ms for cardiac studies ... 100-200 ms for cerebral studies



[From Graber, Lecture Note for BMI1-FS05]

Summary

- Projection radiography system consists of an x-ray tube, devices for beam filtration and restriction, compensation filters, grids, and a film-screen detector (or digital detector, filmless)
- The detector reading (or image gray level) is proportional to the number of unabsorbed x-ray photons arriving at the detector, which depends on the overall attenuation in the path from the source to the detector
- The above relation must be modified to take into account of inverse square law, obliquity, anode heel effect, extended source and detector impulse response
- The degree of film darkening is nonlinearly related to the film exposure (detected x-ray) by the H&D curve
- Both detector noise and Compton scattering reduce contrast and SNR of the formed image

Reference

- Prince and Links, Medical Imaging Signals and Systems, Chap 5.
- Webb, Introduction to biomedical imaging, Chap 1.

Homework

- Reading:
 - Prince and Links, Medical Imaging Signals and Systems, Chap 5.
- Note down all the corrections for Ch. 5 on your copy of the textbook based on the provided errata.
- Problems for Chap 5 of the text book:
 - P5.2
 - P5.4
 - P5.5
 - P5.8
 - P5.18
 - P5.19
 - correction: the sentence “Suppose a 5 cm ...” in Part (a) should be moved to the beginning of part (b). Also, intrinsic contrast in part (b) = $(\mu_t - \mu_b) / (\mu_t + \mu_b)$, contrast in part (c) = $(I_{\max} - I_{\min}) / (I_{\max} + I_{\min})$.
 - P5.22

Homework (added problem)

1. Consider the x-ray imaging of a two-layer slab, illustrated below. Determine the intensity of detected photons along the y axis on the detector plane. Express your solution in terms of the y -coordinate. Sketch this function. You should consider the inverse square law and the oblique effect. Assume the x-ray source is an ideal point source with intensity I_0 . For simplicity, assume the slab is infinitely long in the y direction.

