

RF simulations with COMSOL

ICPS 2017

Politecnico di Torino

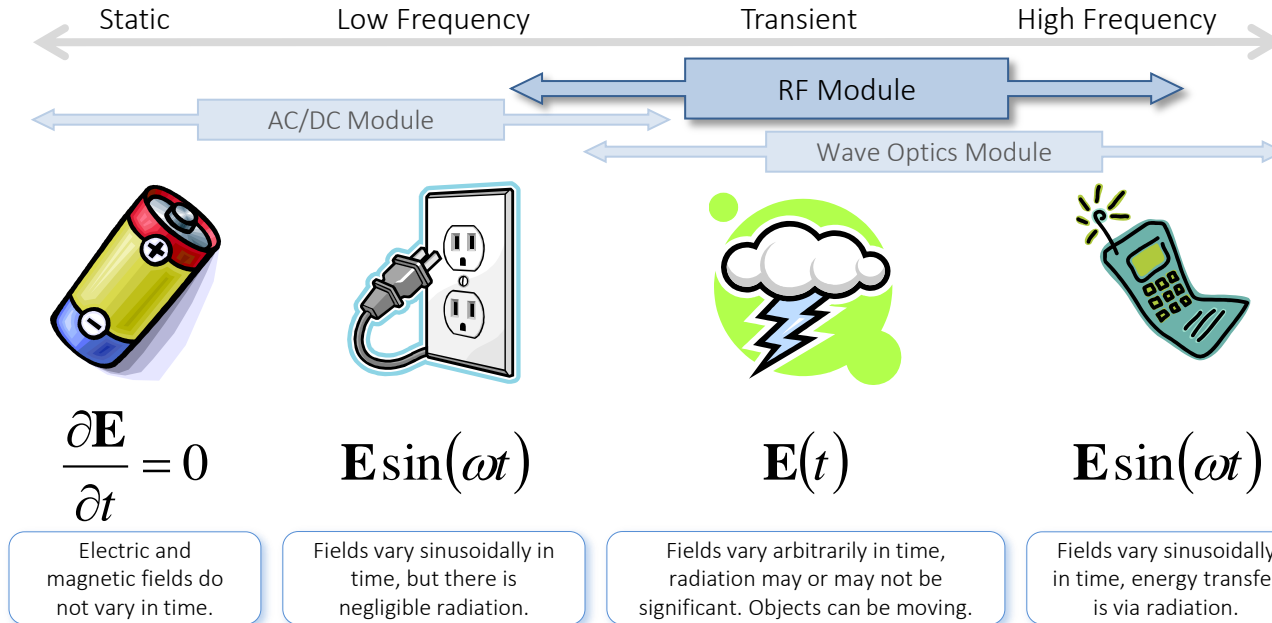
Aug. 10th, 2017

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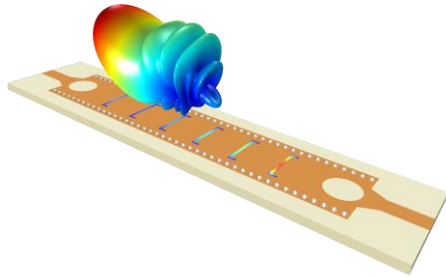
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Types of Electromagnetics Modeling

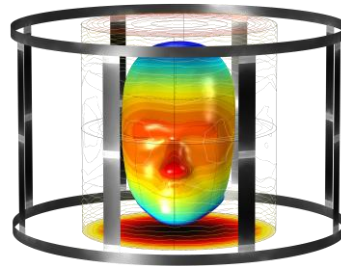


High Frequency Modeling

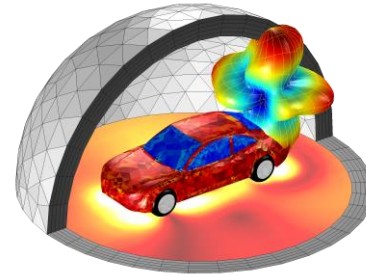
- Electromagnetic Waves formulation solves for the electric and magnetic fields with Frequency domain and Eigenfrequency (resonant mode) analysis



Substrate Integrated Waveguide
Slot Antenna



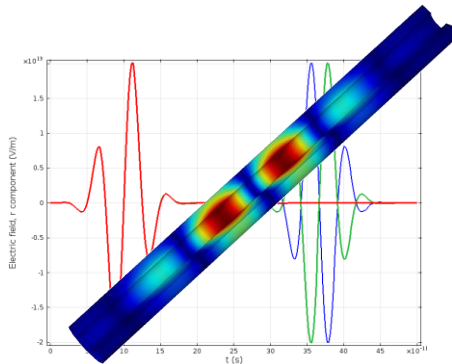
MRI Birdcage Coil



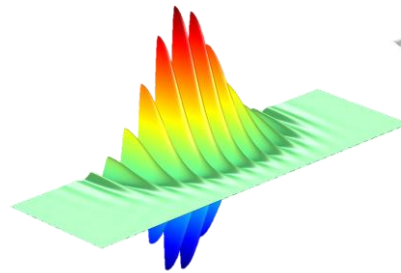
Automotive
EMI/EMC

Transient Modeling

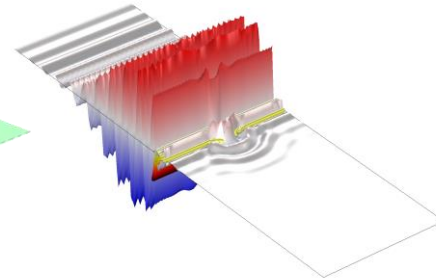
- Transient electromagnetics solves for nonlinear wave phenomena
- For transient phenomena such as signal propagation as a function of time



Coaxial Cable Transient



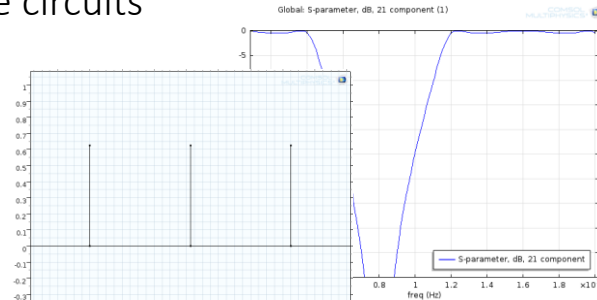
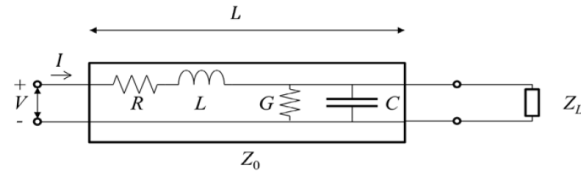
Second Harmonic Generation



Dispersive Drude-Lorentz media

Additional Formulations: Transmission Line Equations

- The Transmission Line Equation formulation solves for the electric potential along transmission lines
- For fast prototyping of transmission line circuits



0.5dB Equal-ripple Low Pass Filter

Feature Overview: Material Models

- All material properties can be:
 - Constant or nonlinearly dependent upon the fields
 - Isotropic, Diagonal, or Fully Anisotropic
 - Real or complex properties (losses)
 - Bi-directionally coupled to any other physics, e.g. Temperature, Strain
 - Fully User-Definable
- RF Module supports loss tangents and dispersion models
 - Drude-Lorentz, and Debye dispersion

$$\mathbf{D} = \varepsilon_0 \varepsilon_r \mathbf{E}$$

$$\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P}$$

$$\mathbf{D} = \varepsilon_0 \varepsilon_r \mathbf{E} + \mathbf{D}_r$$

$$\mathbf{B} = \mu_0 \mu_r \mathbf{H}$$

$$\mathbf{B} = \mu_0 \mathbf{H} + \mu_0 \mathbf{M}$$

$$\mathbf{B} = \mu_0 \mu_r \mathbf{H} + \mathbf{B}_r$$

$$\mathbf{J} = \sigma \mathbf{E}$$

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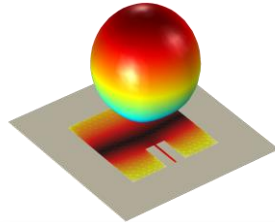
$$\mathbf{B} = \mu_0 \mathbf{H} + \mu_0 \mathbf{M}$$

$$\mathbf{B} = \mu_0 \mu_r \mathbf{H} + \mathbf{B}_r$$

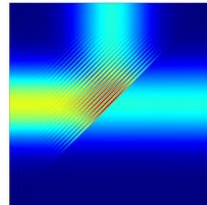
$$\mathbf{J} = \sigma \mathbf{E}$$

Modeling of Conductive Geometries

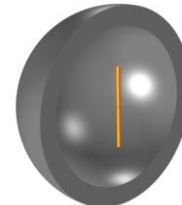
- Geometrically very thin, highly conductive, electrically thicker than skin-depth
 - Perfect Electric Conductor (PEC) Boundary Condition, lossless, non-penetrable
- Geometrically very thin, conductive, and lossy
 - Transition Boundary Condition, lossy, skin-depth dependent penetration, modeled in 2D
- Conductive, electrically much thicker than skin-depth
 - Impedance Boundary Condition, lossy, non-penetrable



Thin copper layer modeled as PEC at 1.6 GHz



Very thin silver layer modeled via Transition Boundary Condition at 428 THz



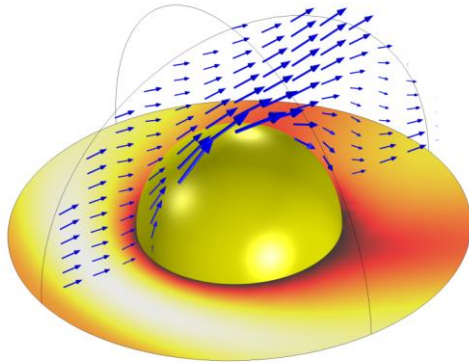
Copper rod represented by Impedance Boundary Condition

Feature Overview: Boundary Conditions

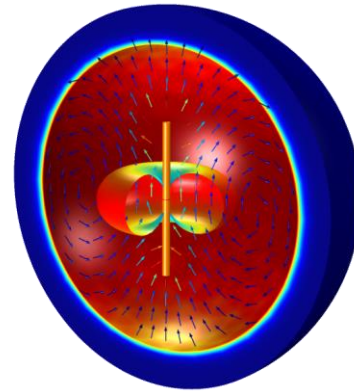
- Voltage source, Current source, & Insulating surfaces
- Thick volumes of electrically resistive, or conductive, material
- Thin layers of electrically resistive, or conductive, material
- Perfectly conducting boundaries
- Periodicity conditions
- Connections to external circuit models
- Lumped, Coaxial, and other Waveguide feeds
- Electromagnetic wave excitations
- Absorbing (Radiating) boundaries

Feature Overview: Domain Conditions

- Background Field excitation for scattering problems
- Perfectly Matched Layer for modeling of free space



PEC Sphere illuminated by
a background plane wave



Half-wave dipole antenna, surrounded
by Perfectly Matched Layer

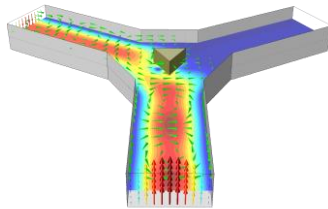
Feature Overview: Data Extraction

- Impedance, Admittance, and S-parameters
- Smith plot
- Touchstone file export
- Far-field plots for radiation

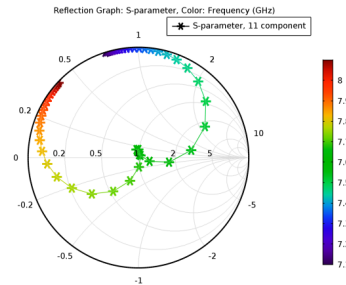
$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$

Lumped Parameters

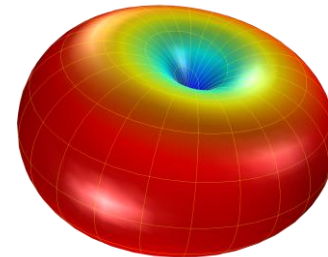
```
#GHZ S MA R 50  
3.0000 0.058933797960767496  
0.03765980464082293 -  
0.9259133092646515 -j
```



Touchstone File Export



Smith Plot



Far-Field Radiation Pattern

Waveguides and Transmission Lines

- Any structure that guides electromagnetic waves along its structure can be considered a waveguide
- COMSOL can compute propagation constants, impedance, S-parameters

$$\begin{aligned}\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2(\epsilon_r - j\sigma/\omega\epsilon_0)\mathbf{E} &= \mathbf{0} \\ \mathbf{E} &= \mathbf{E}(x, y)\exp(\lambda z) \\ \lambda &= -j\beta - \delta_z\end{aligned}$$

- COMSOL also solves the time-harmonic transmission line equation for the electric potential for electromagnetic wave propagation along one-dimensional transmission lines.

$$\frac{\partial}{\partial x} \left(\frac{1}{R + i\omega L} \frac{\partial V}{\partial x} \right) - (G + i\omega C)V = 0$$

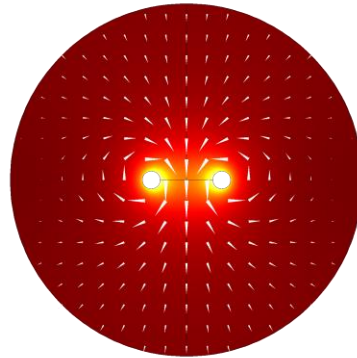
Typical examples

Coaxial cable
Optical fibers and waveguides

Impedance of a Parallel Wire Transmission Line

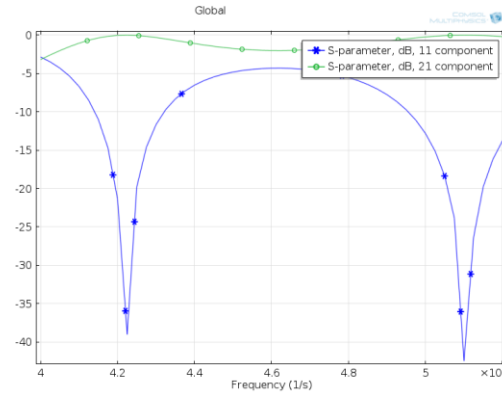
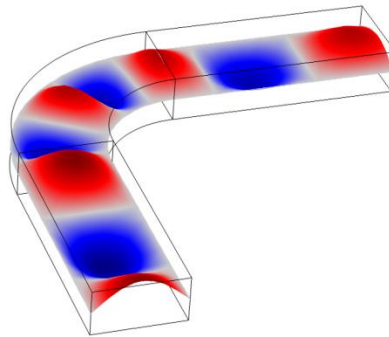
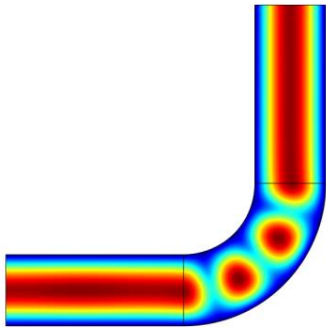
- The impedance of a parallel wire transmission line has an analytic solution
- A cross-sectional model is used to find the fields
- The transmission line is unshielded, so the fields extend to infinity, associated modeling issues are addressed
- The computed impedance agrees with the analytic solution

$$Z_{0, \text{analytic}} = \frac{1}{\pi} \sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_r}} \operatorname{acosh}\left(\frac{r_d}{r_a}\right)$$



H-bend Waveguide 2D & 3D Model

- The transmission of a TE_{10} wave through a 90° bend in a waveguide is modeled



Passive Devices Example Models

- Passive devices like couplers, power dividers, and filters can be realized by combining resonant structures and transmission lines. COMSOL calculates the fields distribution, impedance, and S-parameters

$$\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2(\epsilon_r - j\sigma/\omega\epsilon_0)\mathbf{E} = \mathbf{0}$$

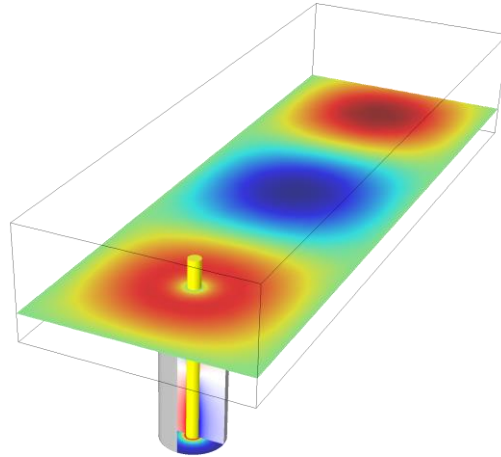
$$S = \begin{bmatrix} S_{11} & S_{12} & \dots & S_{1n} \\ S_{21} & S_{22} & \dots & \cdot \\ \vdots & \vdots & \ddots & \vdots \\ S_{n1} & \cdot & \dots & S_{nn} \end{bmatrix}$$

Typical examples

3dB Couplers and Power Dividers
Band-pass Filters

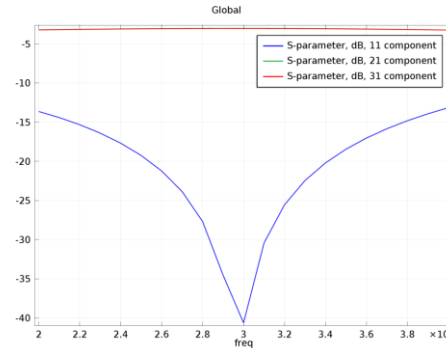
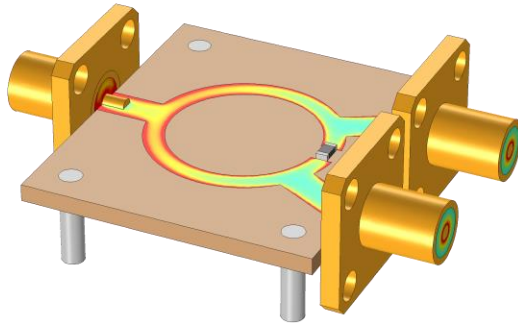
Coaxial Cable to Waveguide Coupling

- A model of a coaxial cable feed that excites a propagating wave inside a rectangular waveguide
- S-parameters for transmission and reflection are computed



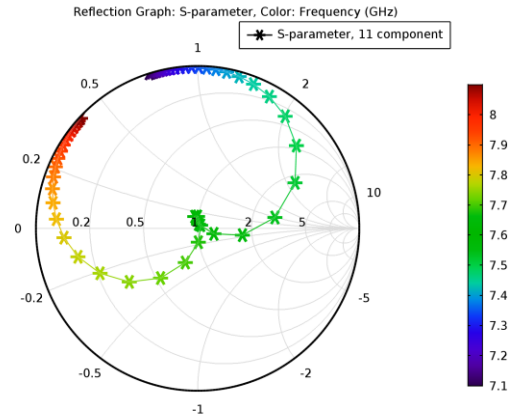
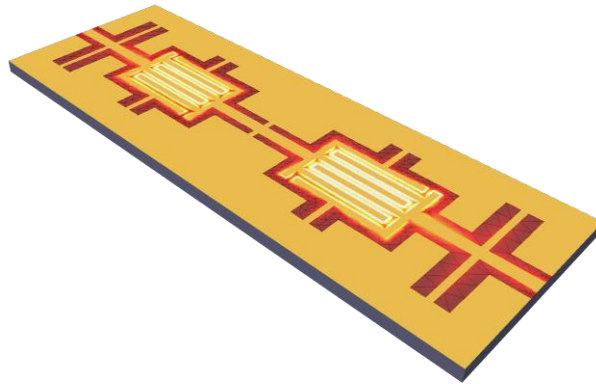
Wilkinson Power Divider

- A Wilkinson power divider is a three-port lossless device and outperforms a T-junction divider and a resistive divider
- Computed S-parameters show good input matching and -3 dB evenly split output
- 100 Ohm resistor modeled via lumped element feature



Coplanar Waveguide (CPW) Bandpass Filter

- Excite and terminate two slots equally using multi-element uniform lumped ports
- Combination of interdigital capacitors (IDCs) and short-circuited stub inductors (SSIs)



Antenna Example Models

- Antennas transmit and/or receive radiated electromagnetic energy. COMSOL can compute the radiated energy, far field patterns, losses, gain, directivity, impedance and S-parameters by solving the linear problem for the E -field

$$\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2(\epsilon_r - j\sigma/\omega\epsilon_0)\mathbf{E} = \mathbf{0}$$

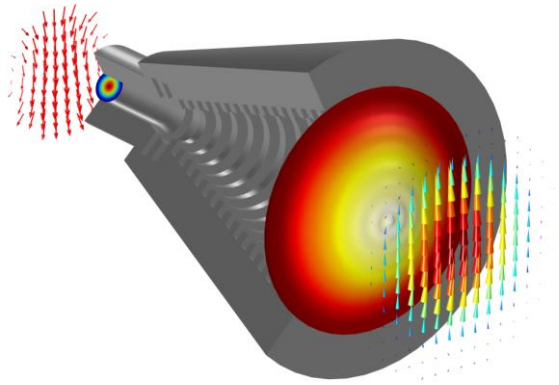
$$\mathbf{E}_{far} = -\frac{jk}{4\pi} \mathbf{r}_0 \times \int [\mathbf{n} \times \mathbf{E} - \eta \mathbf{r}_0 \times (\mathbf{n} \times \mathbf{H})] \exp(jk\mathbf{r} \cdot \mathbf{r}_0) dS$$

Typical examples

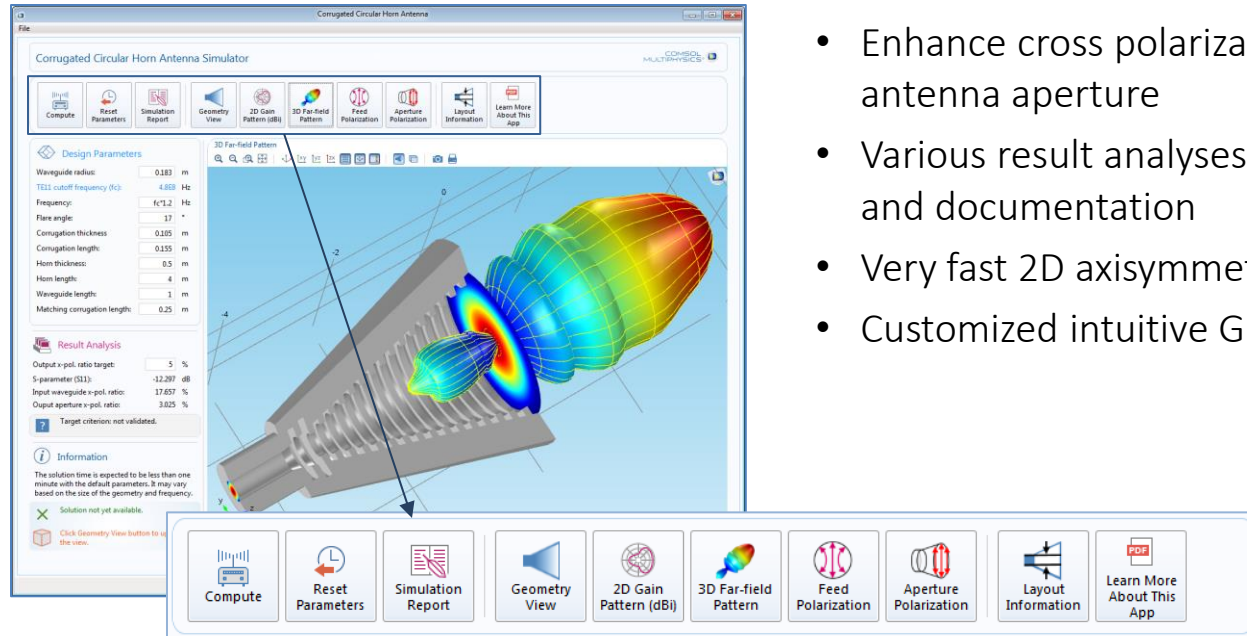
Microstrip Patch Antenna
Vivaldi Antenna
Dipole Antenna

Corrugated Circular Horn Antenna

- Designed using a 2D axisymmetric model
- Low cross-polarization at the antenna aperture by combining TE mode excited at the circular waveguide feed and TM mode generated from the corrugated inner surface



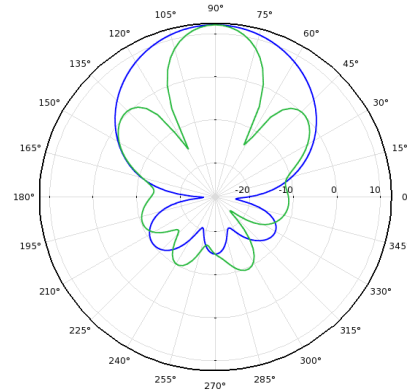
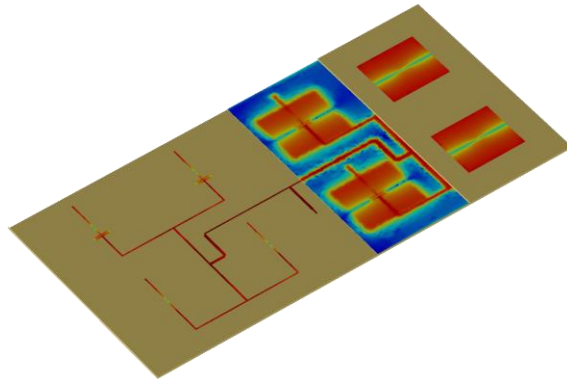
Corrugated Circular Horn Antenna Simulator



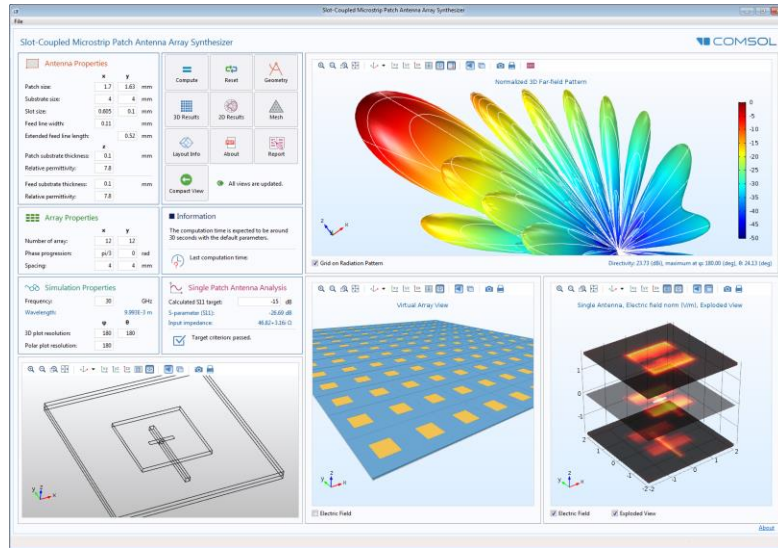
- Enhance cross polarization ratio at the antenna aperture
- Various result analyses, simulation report, and documentation
- Very fast 2D axisymmetric simulation
- Customized intuitive GUI

4 x 2 Microstrip Patch Antenna Array

- Slot-coupled 4x2 array of patch antennas
- Controlling the phase and magnitude assigned to each element can steer the beam
- Far-Field radiation pattern is computed



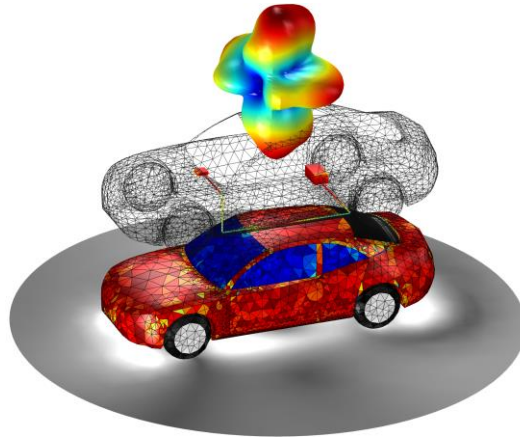
Slot-Coupled Microstrip Patch Antenna Array Synthesizer



- Single slot-coupled microstrip patch antenna fabricated on a multilayered low temperature co-fired ceramic (LTCC) substrate
- Far-field radiation pattern of the antenna array and directivity.
- Approximated by multiplying the array factor and the single antenna radiation
- Phased antenna array prototypes for 5G mobile networks

Car Antenna Effect on a Cable Harness

- Printed FM antenna on a real windshield
- Far-field pattern with a ground plane
- Electric field intensity affected on a cable harness



Examples of Periodic Problems

- Any structure that repeats in one, two, or all three dimensions can be treated as periodic, which allows for the analysis of a single unit cell, with Floquet Periodic boundary conditions

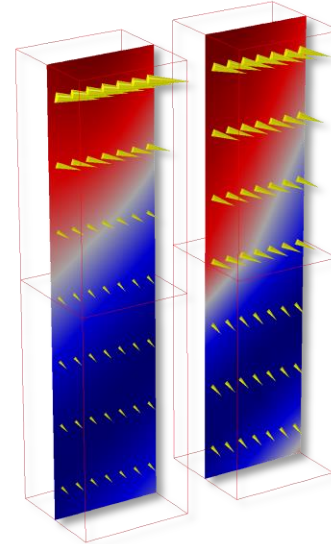
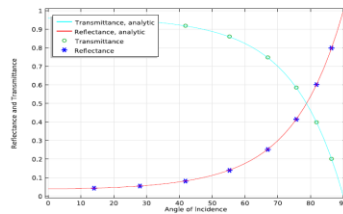
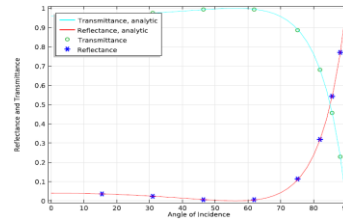
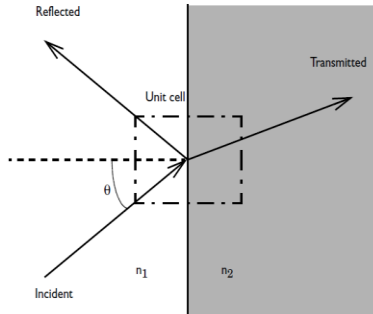
$$\mathbf{E}_d = \mathbf{E}_s \exp(-j\mathbf{k}_F \cdot (\mathbf{r}_d - \mathbf{r}_s))$$

Typical examples

Optical Gratings
Frequency Selective Surfaces
Electromagnetic Band Gap Structures

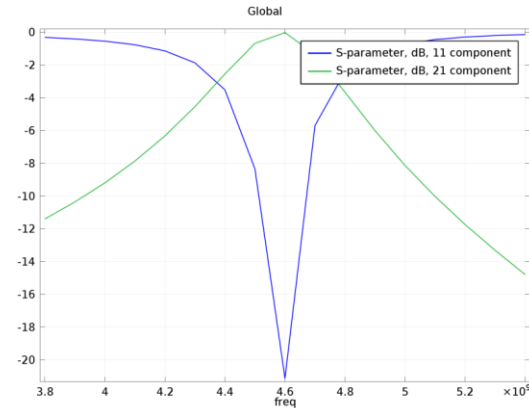
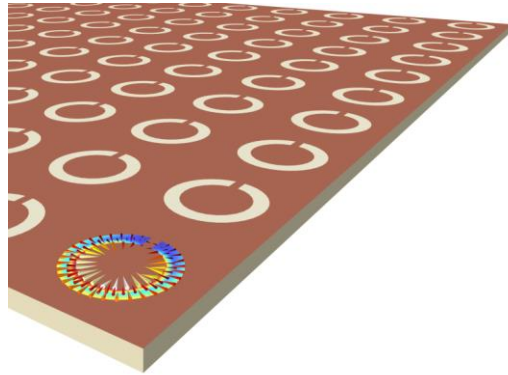
Verification of Fresnel Equations

- TE- and TM-polarized light incident upon an infinite dielectric slab
- 3D model uses Floquet Periodicity
- Results agree with analytic solution

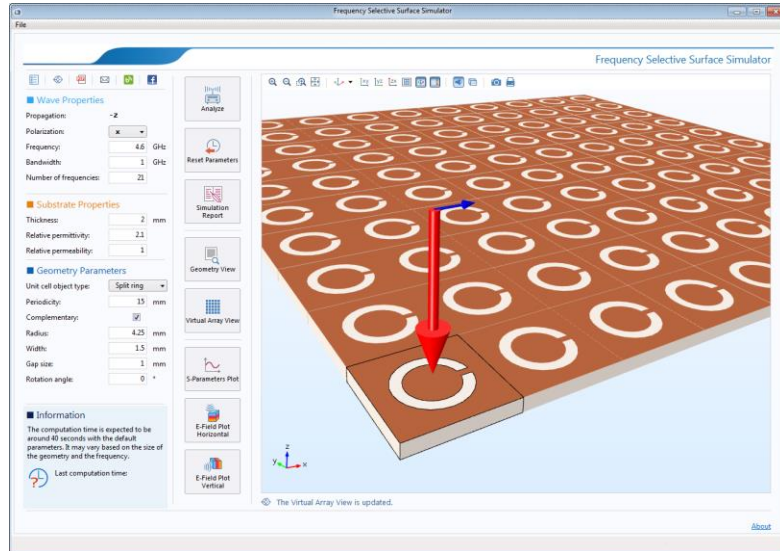


Frequency Selective Surface, CSRR

- One unit cell of the complementary split ring resonator (CSRR) with periodic boundary conditions to simulate an infinite 2D array
- Interior port boundaries combined with perfectly matched layer absorbing higher order modes



Frequency Selective Surface Simulator



- Periodic structures that generate a bandpass or a bandstop frequency response
- Built-in unit cell types: five popular FSS types, with two predefined polarizations and propagation at normal incidence
- The reflection and transmission spectra, the electric field norm on the top surface of the unit cell, and the dB-scaled electric field norm

Electromagnetic Heating Examples

- An electromagnetic wave interacting with any materials will have some loss that leads to rise in temperature over time. Any losses computed from solving the electromagnetic problem can be bi-directionally coupled to the thermal equation

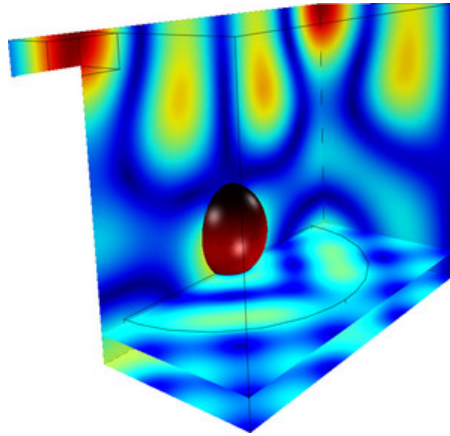
$$\rho C_p \frac{\partial T}{\partial t} - \nabla \cdot (k \nabla T) = Q_{\substack{\text{Electromagnetic} \\ \text{Losses}}}$$

Typical examples

Thermal Drift in a Microwave Filter Cavity
Microwave Ovens
Absorbed Radiation in Living Tissue
Tumor Ablation

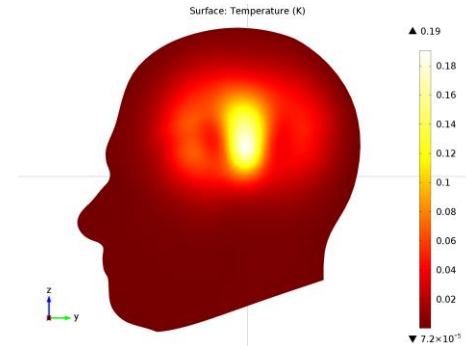
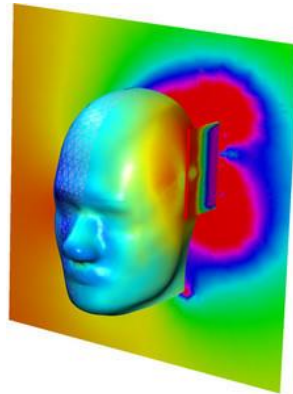
Potato in a Microwave Oven

- A half-symmetry model of a potato in a microwave oven
- The electromagnetic fields are solved in the frequency domain
- The thermal problem is solved transiently



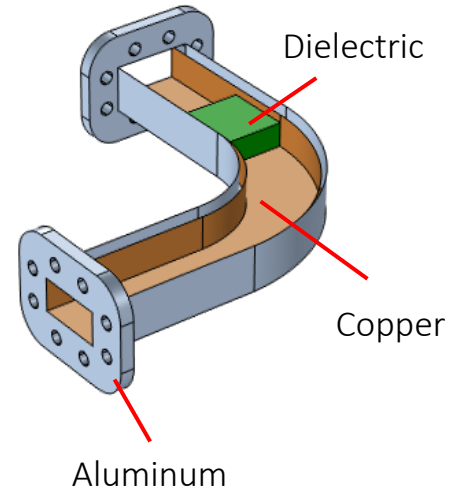
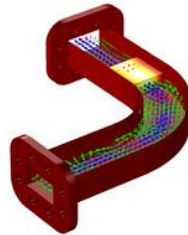
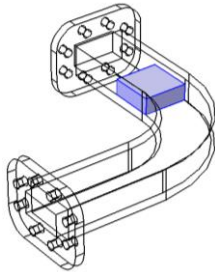
Absorbed Radiation (SAR) in the Human Brain

- A representative cell phone antenna is placed next to a head
- The dielectric properties of the head are from scan data
- Absorbed radiation and temperature rise is computed
- Pennes Bioheat equation models living tissue



Live Demo

- EM heating of a lossy dielectric in a rectangular waveguide
- RF solved in frequency domain; HT solved in time domain



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