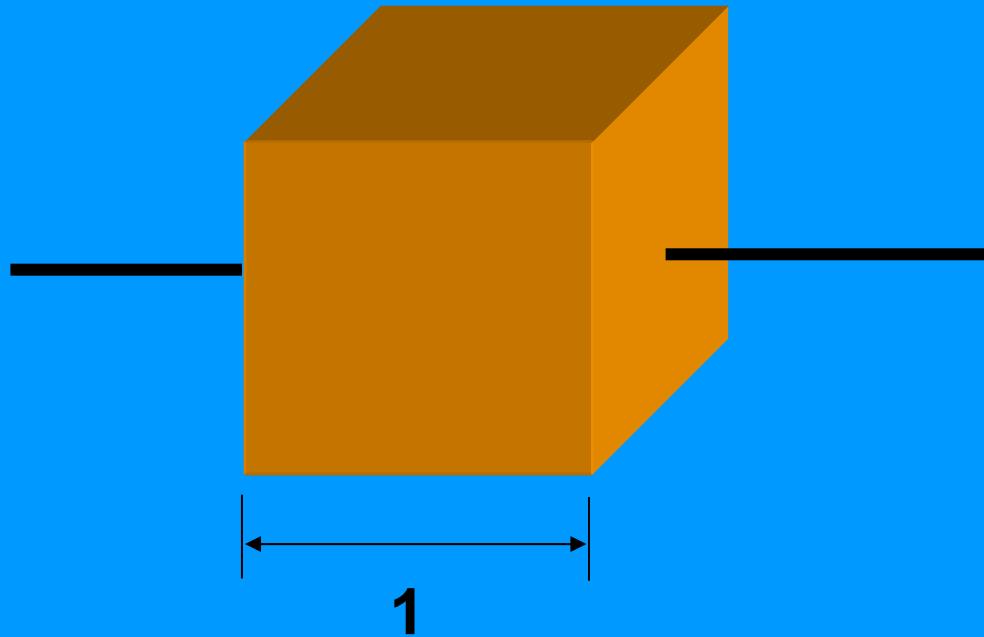


Sistemas de puesta a tierra para instalaciones de baja tensión.

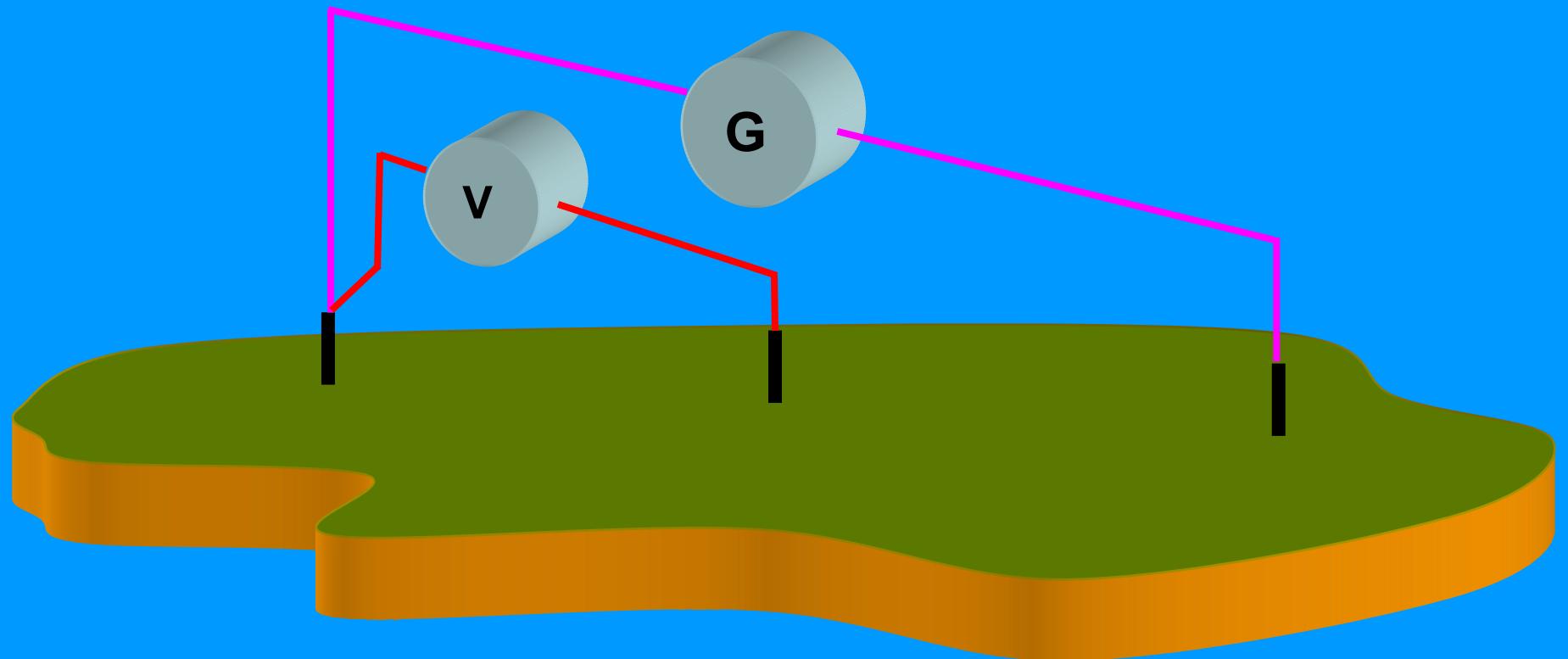
Resistividad – Definición y unidades

$$\left[\Omega \frac{m^2}{m} \right] = [\Omega m]$$

$$R = \rho \times \frac{l}{s}$$



Medición de la resistencia de puesta a tierra



La tierra como conductor

Resistividad del terreno

ITEM	TIPO DE TERRENO	RESISTIVIDAD [Ohm x metro]
1	Terreno de humus húmedo	30
2	Terreno de cultivo	100
3	Terreno arcilloso y arenoso	150
4	Terreno arenoso y húmedo	300
5	Terreno arenoso y seco	1000
6	Argamasa 1:5	400
7	Grava húmeda	500
8	Grava seca	1000
9	Terreno pedregoso	30000
10	Roca	10^7

La tierra como conductor

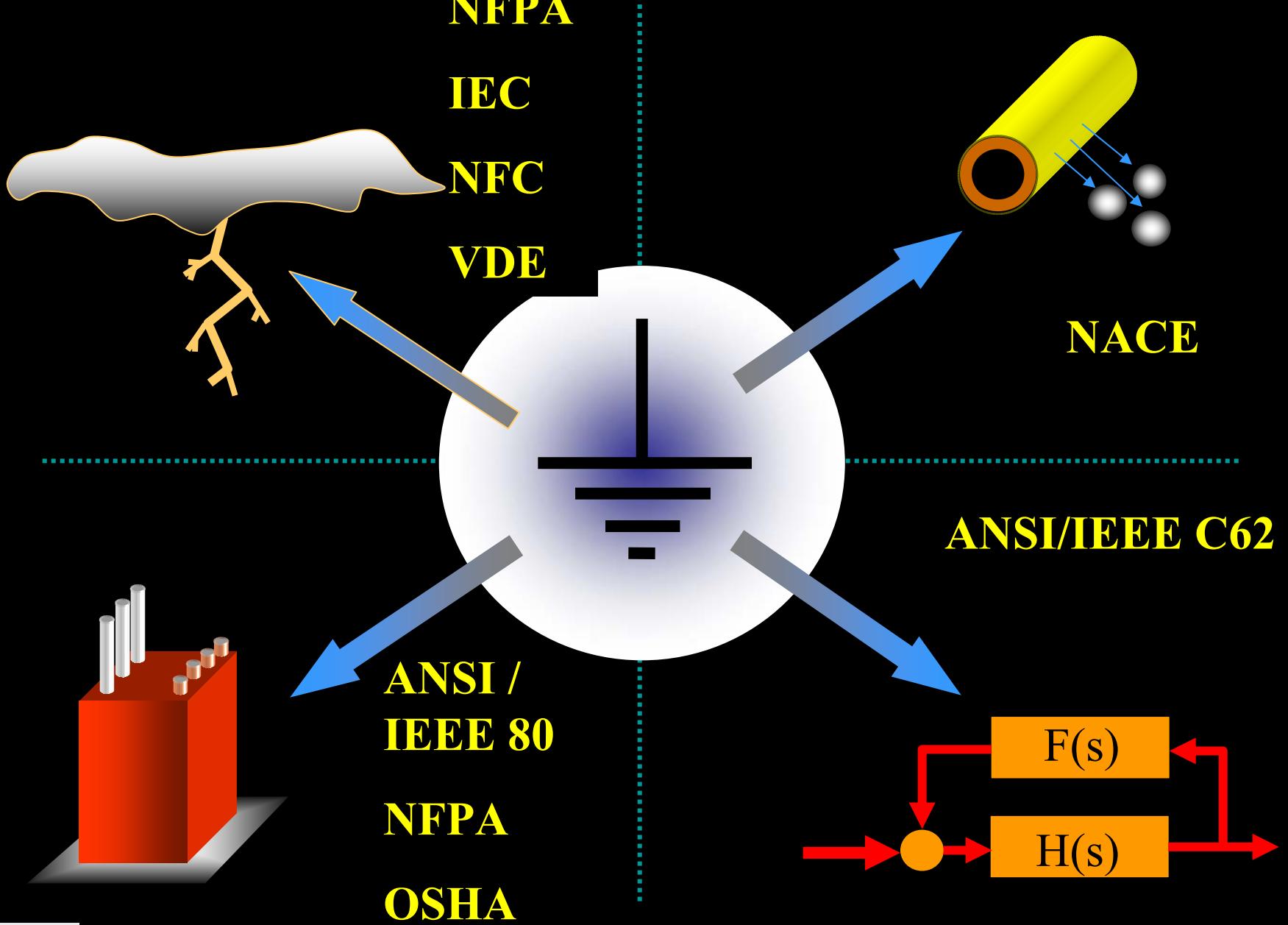
Resistividad del terreno

Variación con la temperatura para un suelo arenoso con una humedad del 15,2%

Temperatura (°C)	Resistividad (Ωm)
20	72
10	99
0 (agua)	138
0 (hielo)	300
-5	790
-15	3300

Conclusiones sobre la tierra

- No posee potencial 0
- Posee resistividad elevada y no es lineal
- Por lo tanto la tierra es un mal conductor y no debe ser utilizado como tal

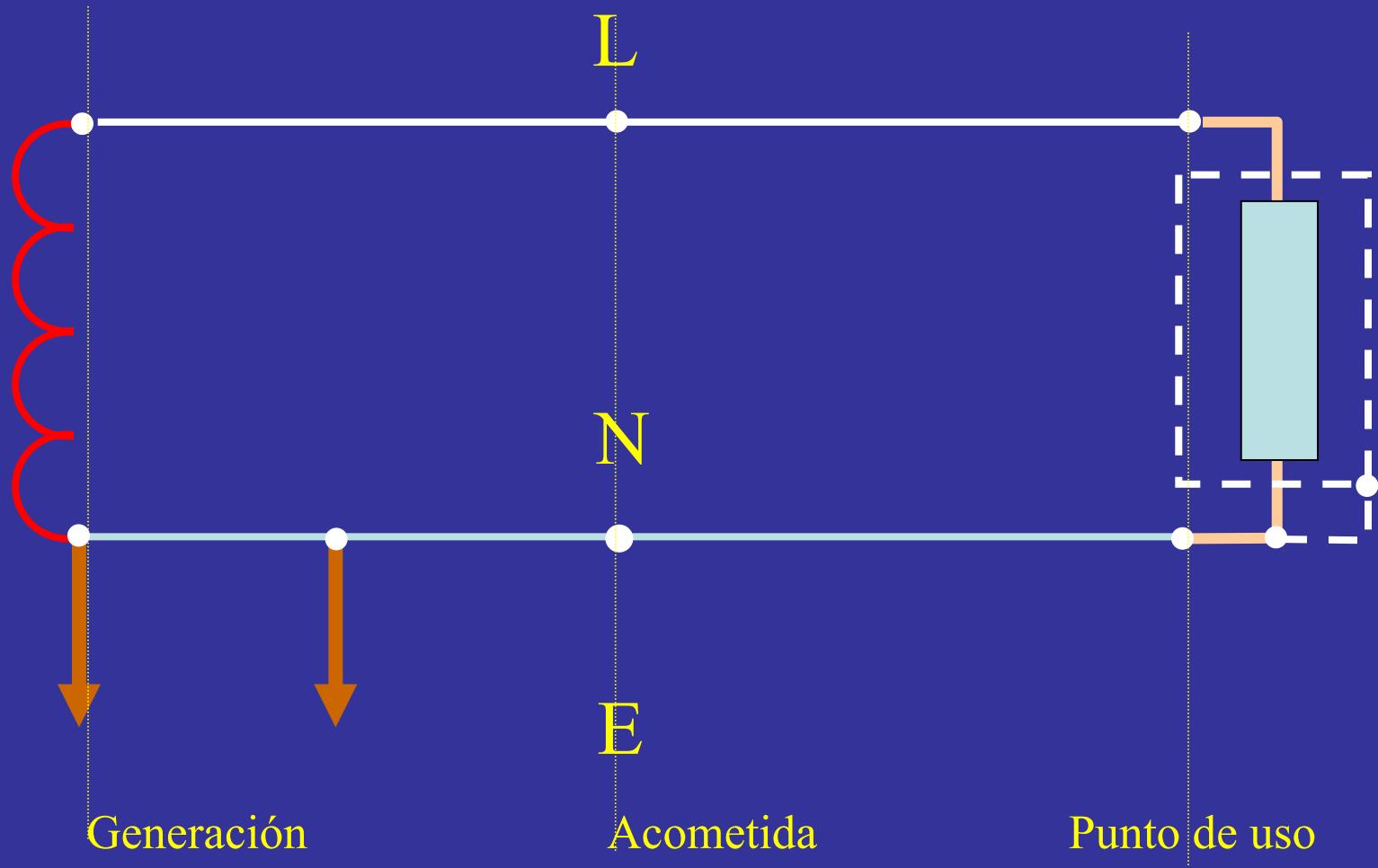


Los tres sistemas de conexión a tierra normalizados. Breve descripción.

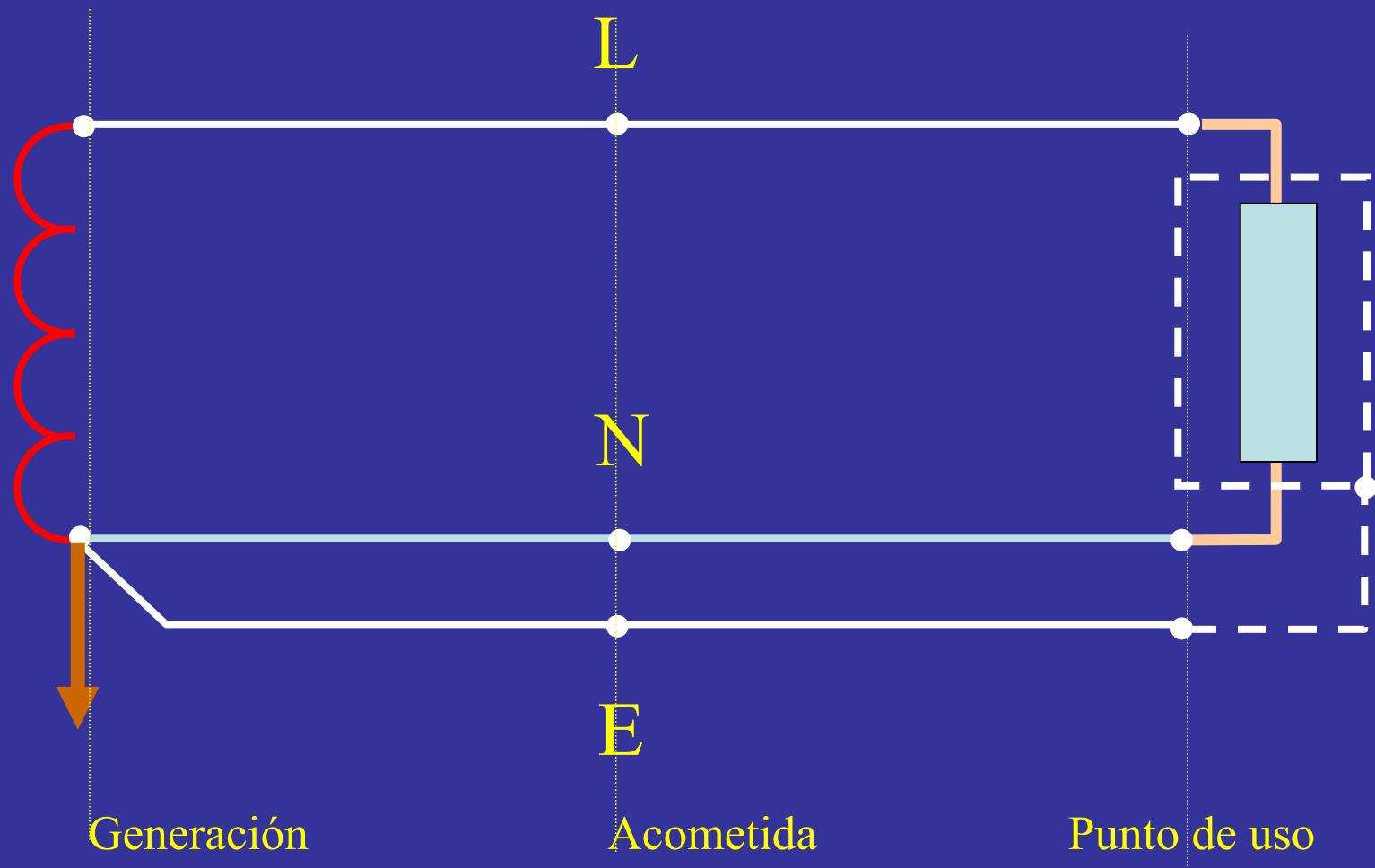
Tierra para seguridad electrica

- Tres grupos; ***TN(TN-S, TN-C, TN-CS) TT e IT.***
- **1^a letra. Situacion de la conexión a tierra**
- ***T- Conexión directa a tierra***
- ***I- Aislado de tierra***
- **2^a letra. Conexión de las masas (a N o a T)**
- **3^a Letra. Unión entre neutro y protección.**
- ***S- Conductores separados***
- ***C- Conductor común***

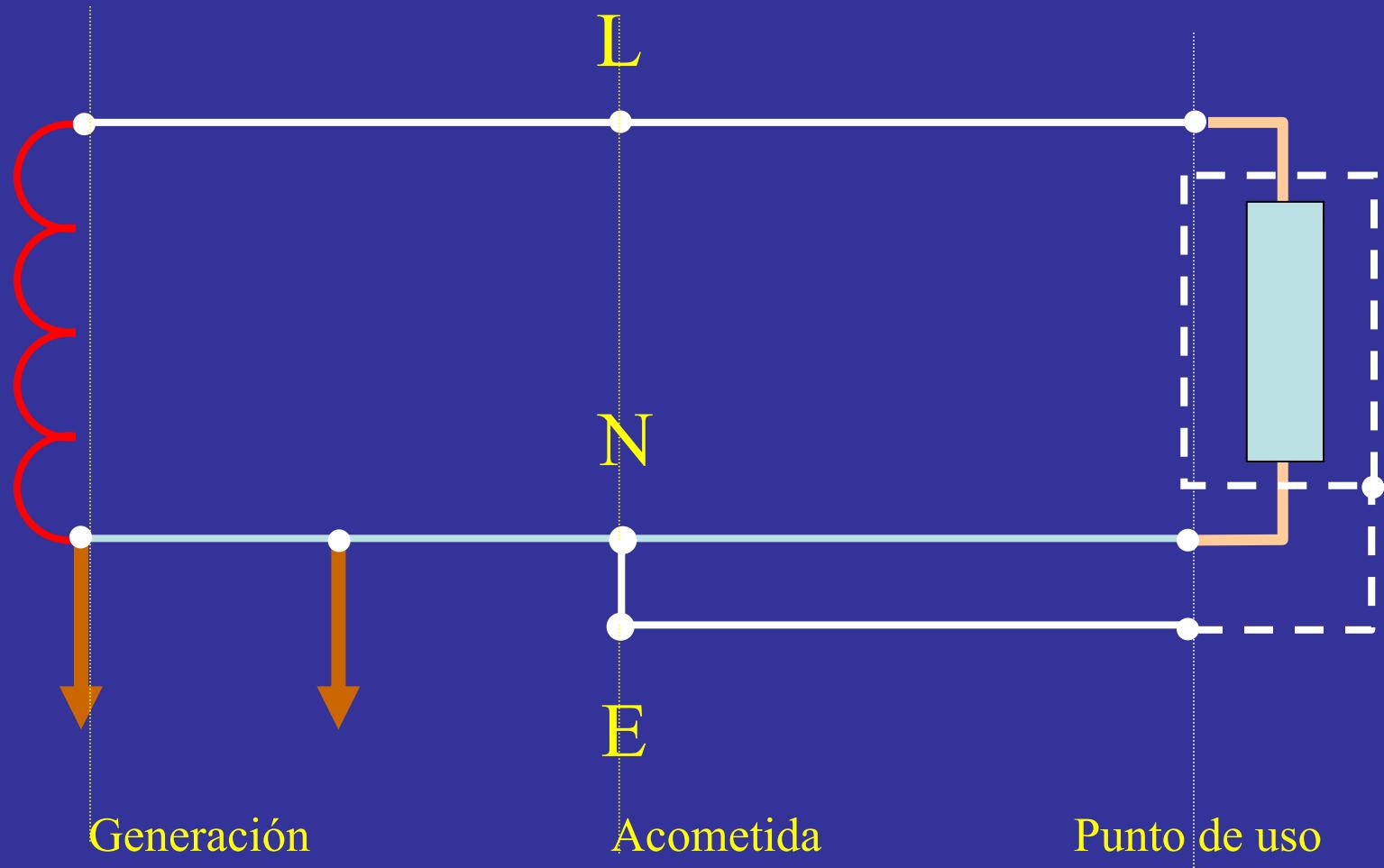
TN-C



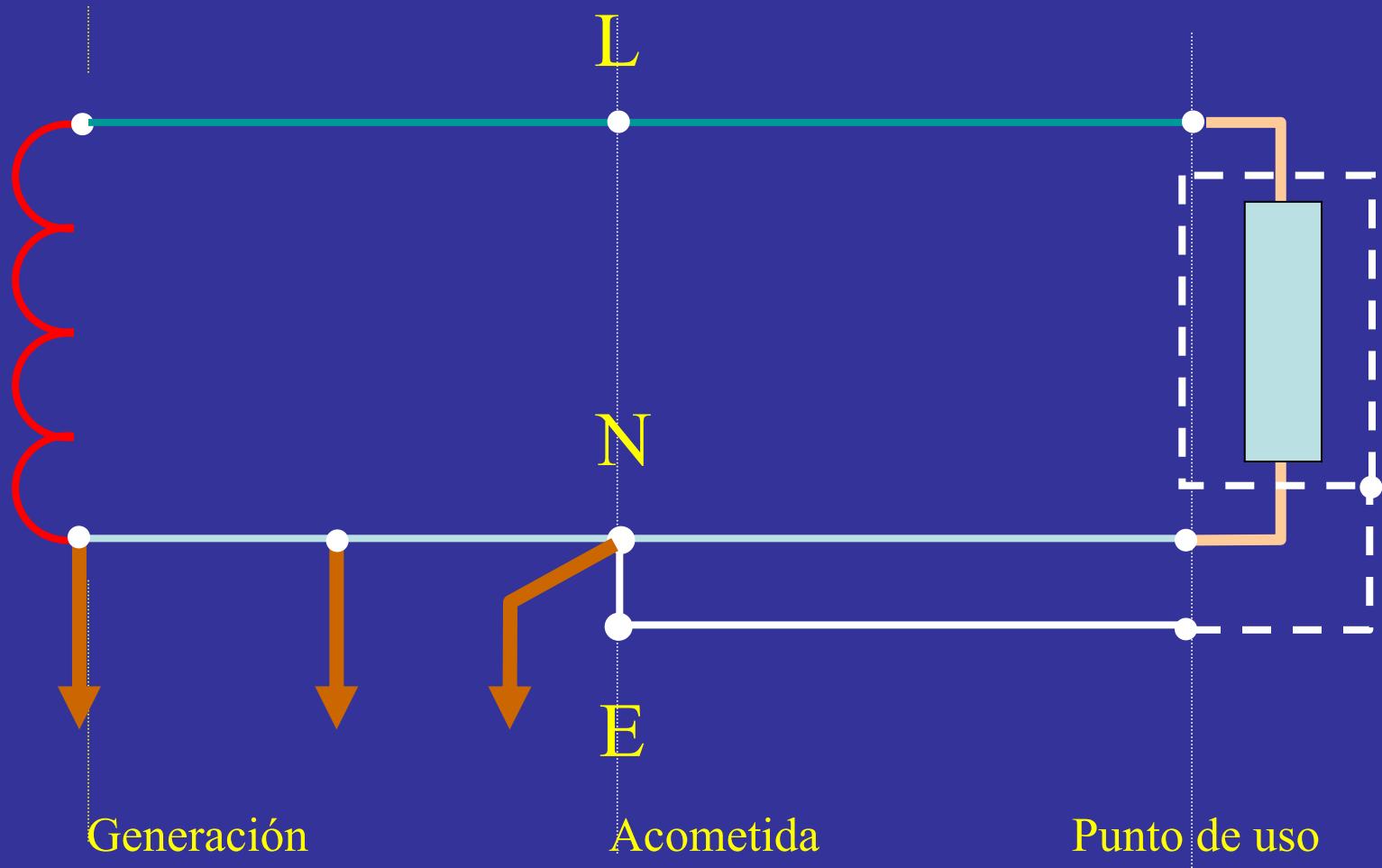
TN-S

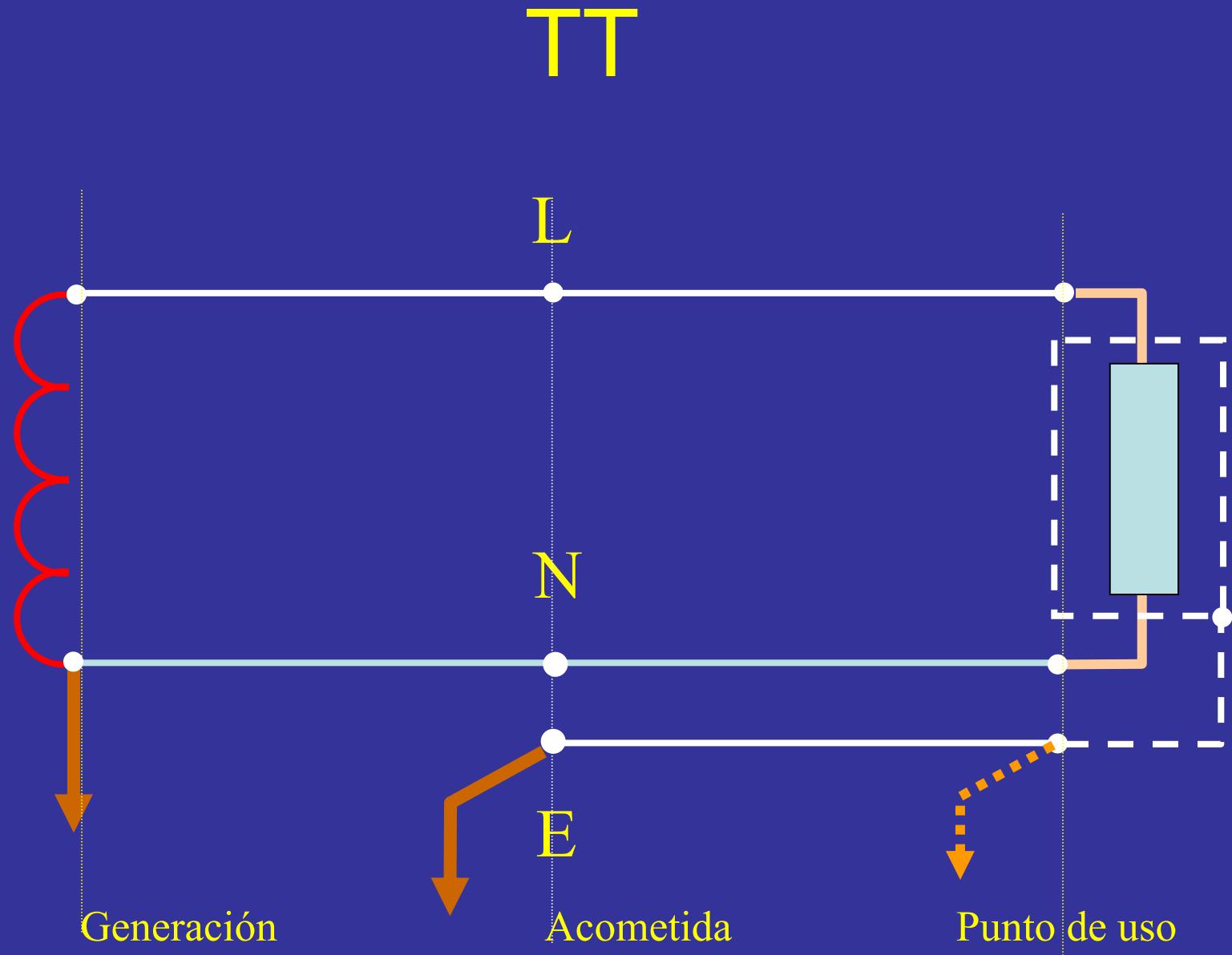


TN-C-S

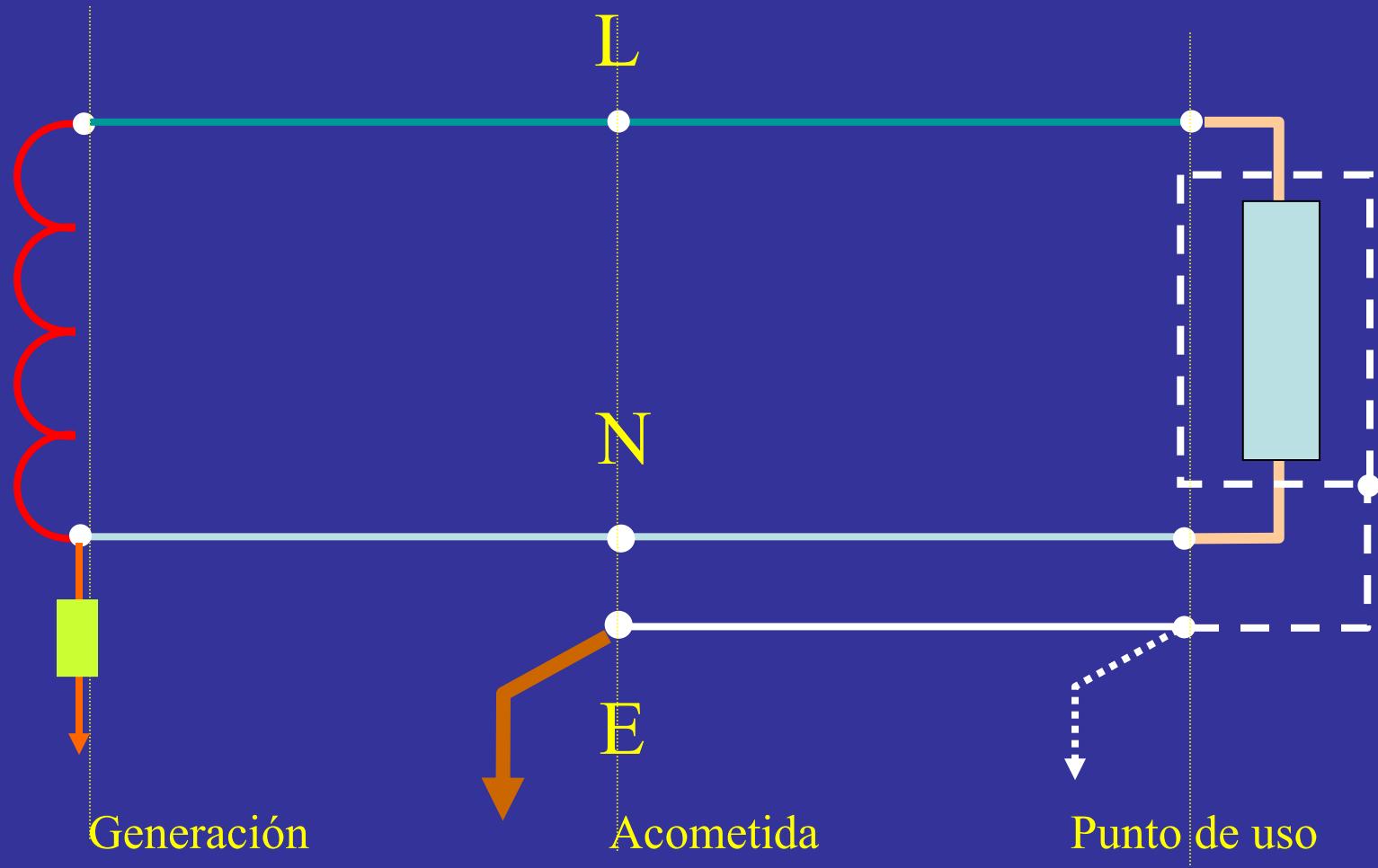


TN-C-S (EE.UU)

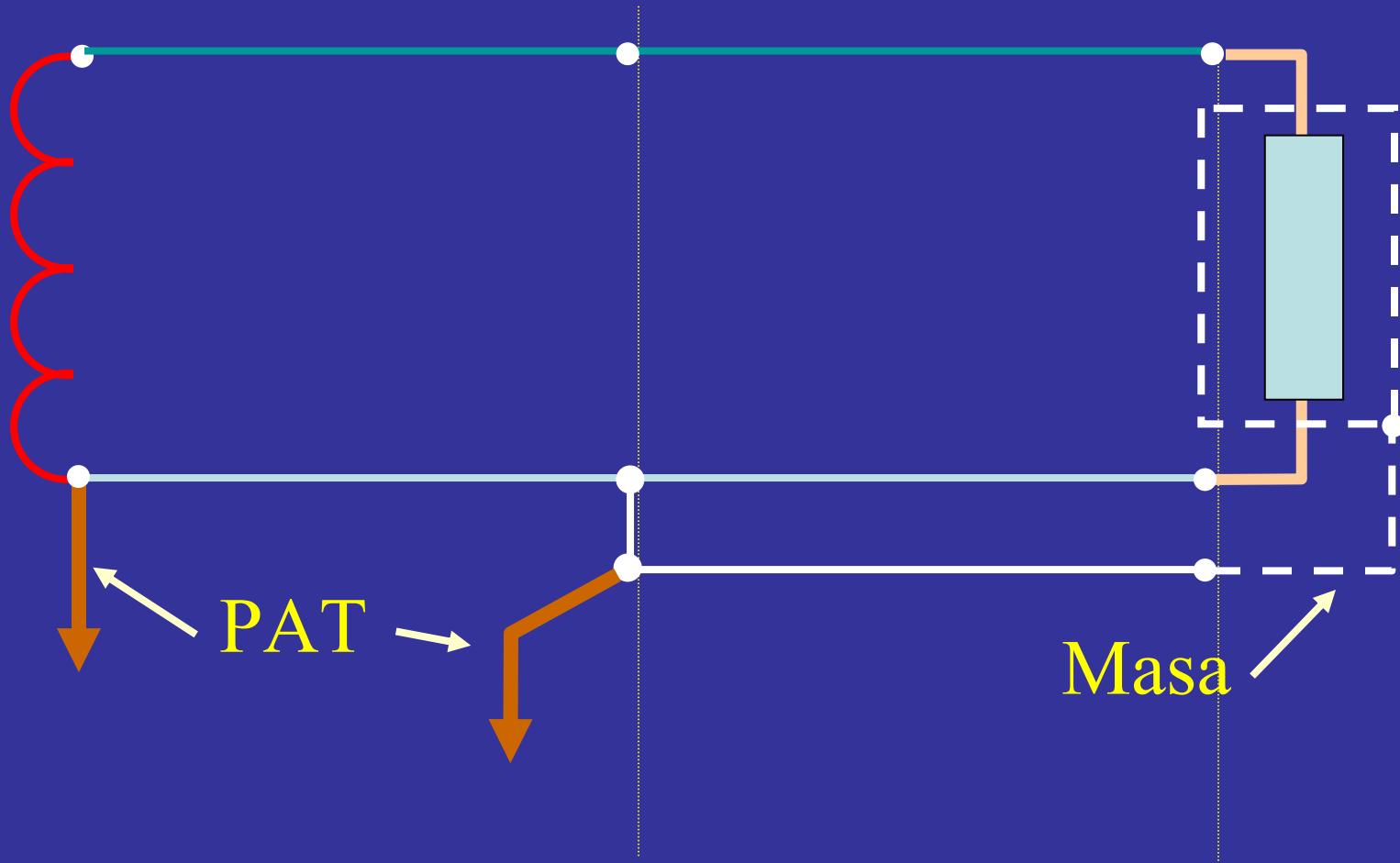




IT



Tierra y masas



Tolerancia a corriente.

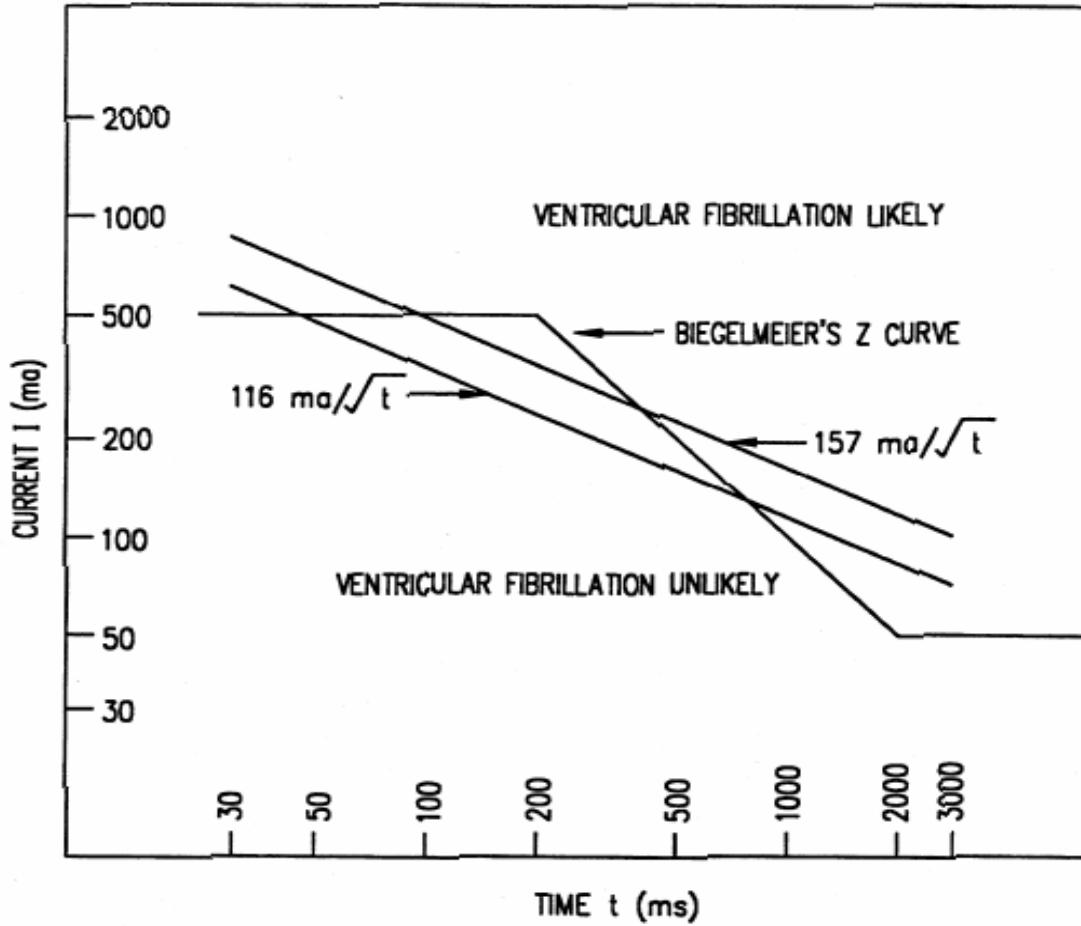
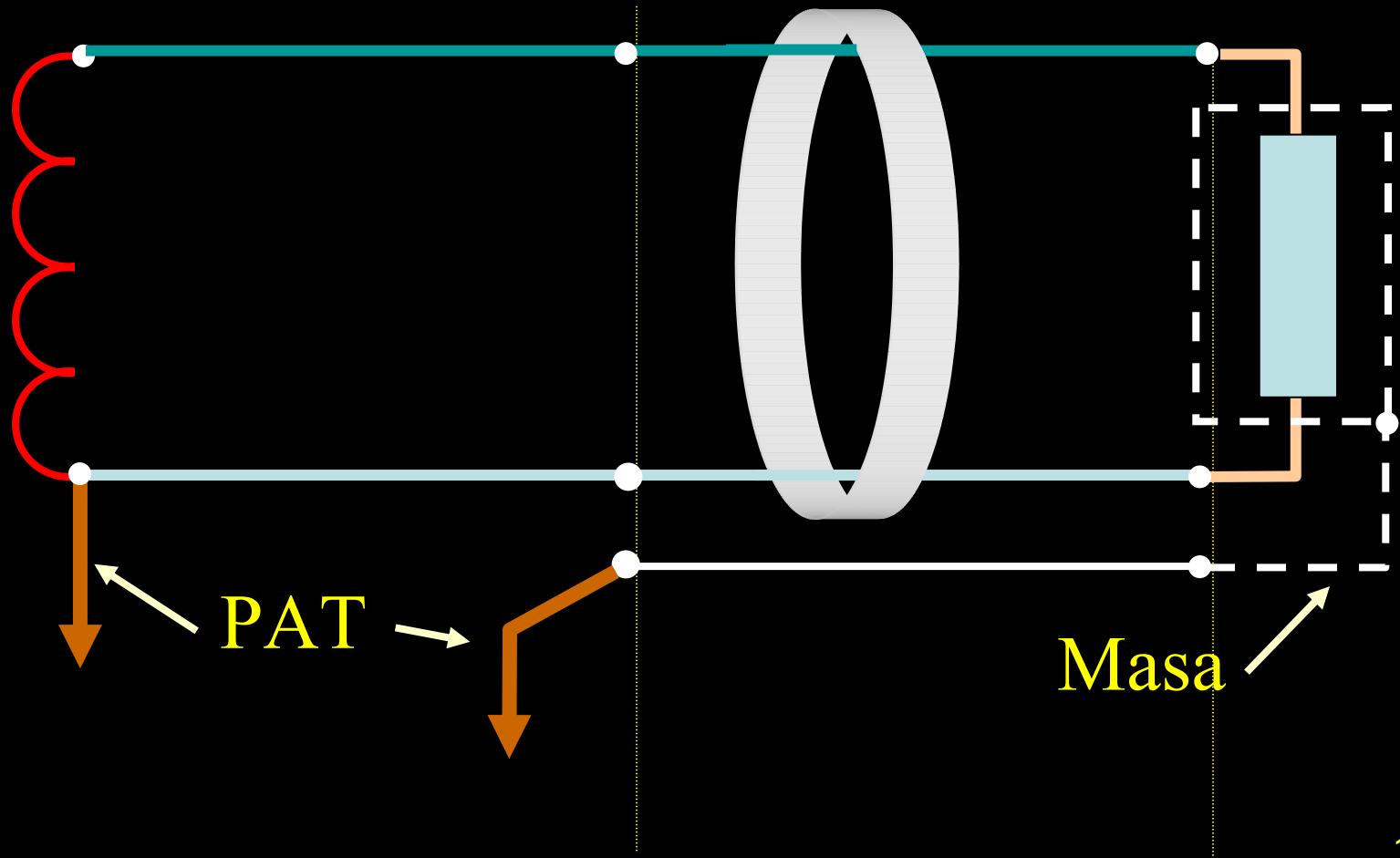


Figure 5—Body current versus time

Disyuntor diferencial



Norma ANSI / IEEE 142.

Recognized as an
American National Standard (ANSI)

IEEE Std 142-1991
(Revision of IEEE Std 142-1982)

IEEE Recommended Practice for Grounding of Industrial and Commercial Power Systems

Sponsor
Power Systems Engineering Committee
of the
IEEE Industry Applications Society

Approved June 27, 1991
IEEE Standards Board

Approved December 9, 1991
American National Standards Institute

Abstract: The problems of system grounding, that is, connection **to** ground of neutral, of the corner of the delta, or of the midtap of one phase, are covered. The advantages and disadvantages of grounded versus ungrounded systems are discussed. Information is given on how to ground the system, where the system should be grounded, and how to select equipment for the grounding of the neutral circuits.

Connecting the frames and enclosures of electric apparatus, such as motors, switchgear, transformers, buses, cables conduits, building frames, and portable equipment, **to** a ground system is addressed. The fundamentals of making the interconnection or ground-conductor system between electric equipment and the ground rods, water pipes, etc. are outlined.

The problems of static electricity-how it is generated, what processes may produce it, how it is measured, and what should be done to prevent its generation or to drain the static charges to earth to prevent sparking-are treated.

Methods of protecting structures against the effects of lightning are also covered.

Obtaining a low-resistance connection to the earth, use of ground rods, connections to water pipes, etc. is discussed. A separate chapter on sensitive electronic equipment is included.

Abstract: The problems of system grounding, that is, connection **to** ground of neutral, of the corner of the delta, or of the mid tap of one phase, are covered.

The advantages and disadvantages of grounded versus ungrounded systems are discussed.

Information is given on how to ground the system, where the system should be grounded, and how to select equipment for the grounding of the neutral circuits.

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Methods of protecting structures against the effects of lightning are also covered.

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A separate chapter on sensitive electronic equipment is included.

Fig. 9
Configuración 1

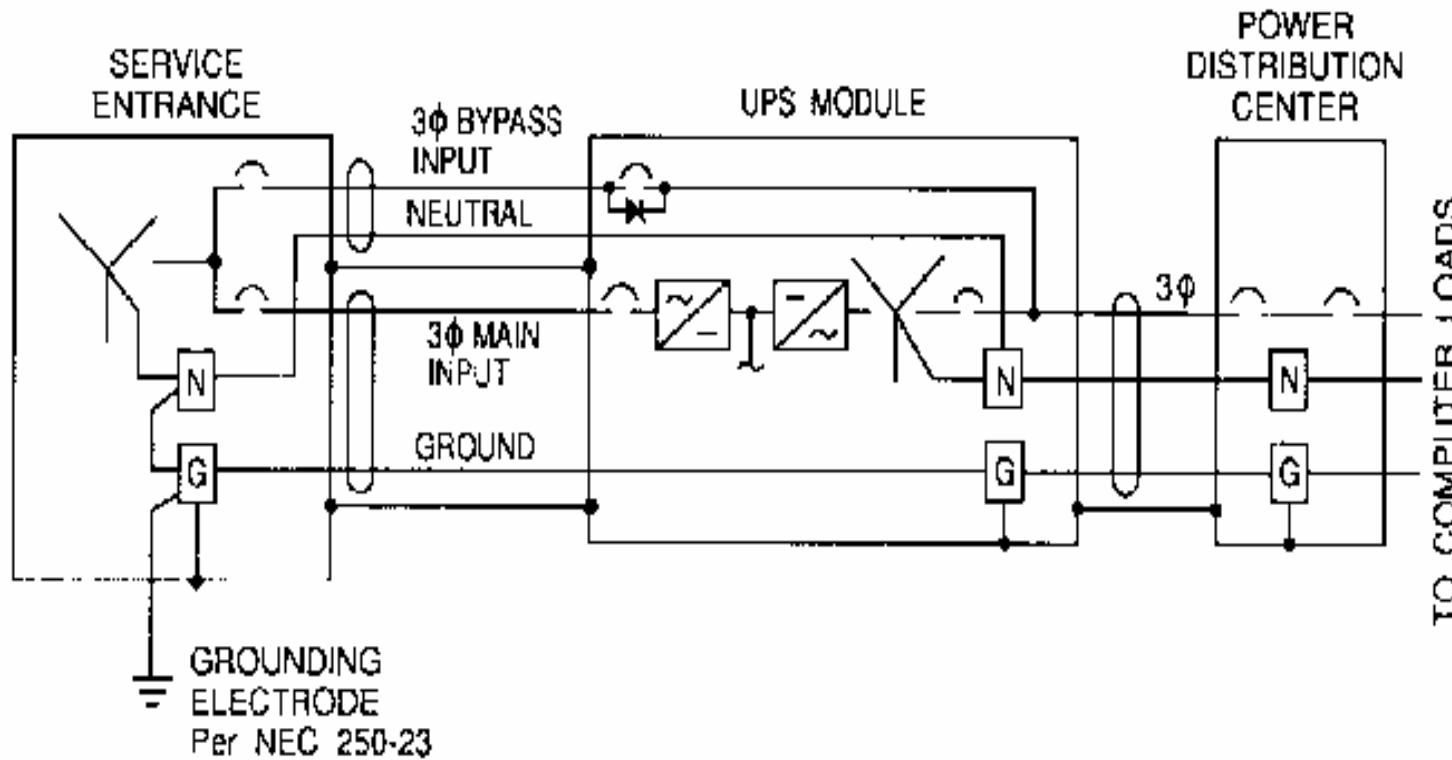


Fig. 10
Configuración 2

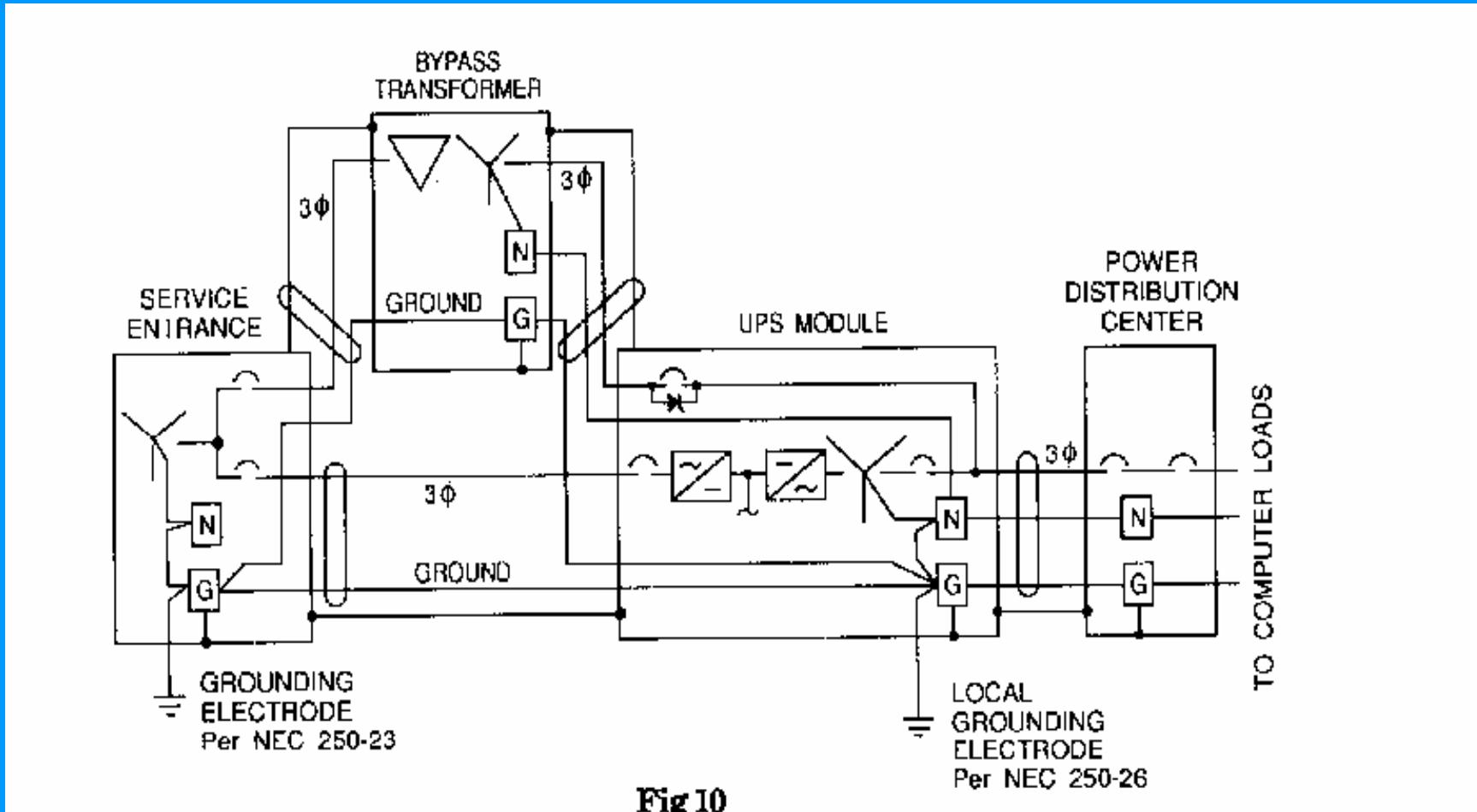


Fig 10



ASOCIACION ELECTROTECNICA ARGENTINA

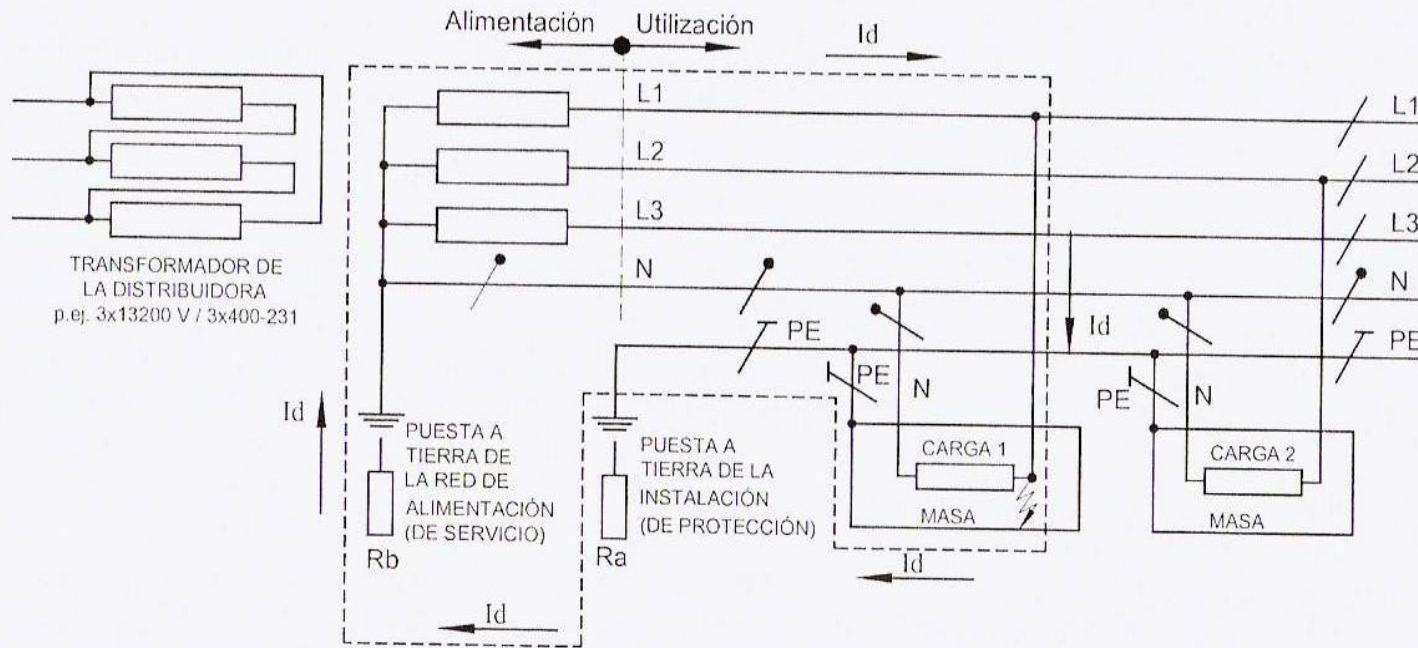


Figura 771.18.B – Lazo de falla esquema TT

**Conexión a tierra de instalaciones
de baja tensión.**

**El verdadero concepto de puestas a
tierra separadas, de acuerdo con
las normas**



ASOCIACION ELECTROTECNICA ARGENTINA

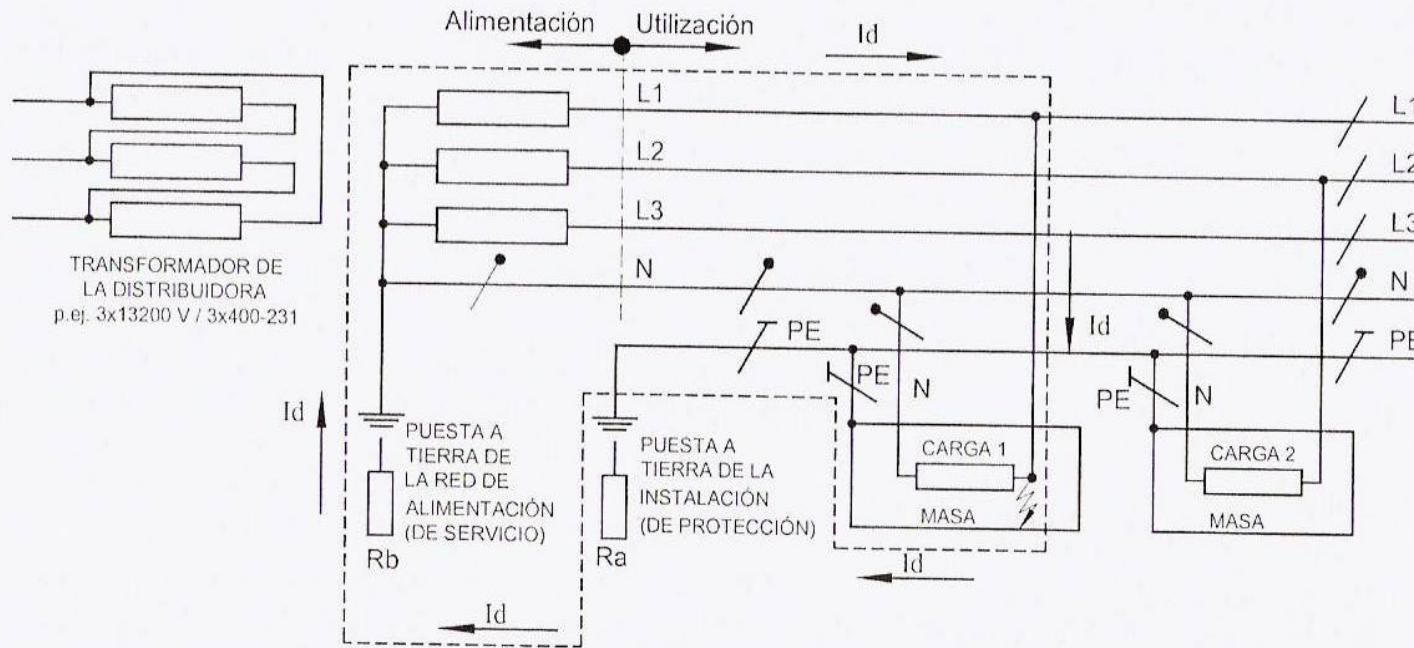
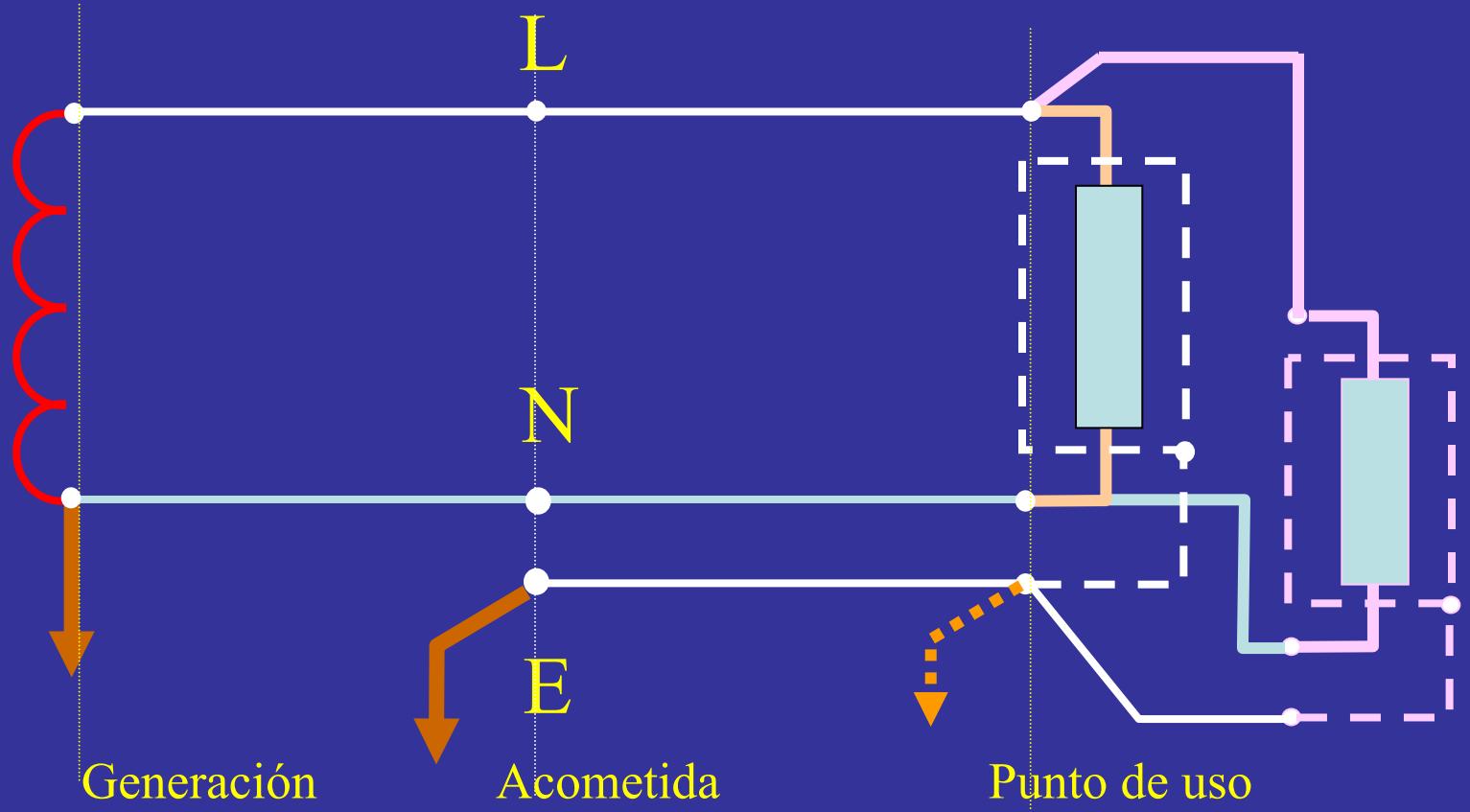


Figura 771.18.B – Lazo de falla esquema TT



El neutro y la puesta a tierra de seguridad.



ASOCIACION ELECTROTECNICA ARGENTINA

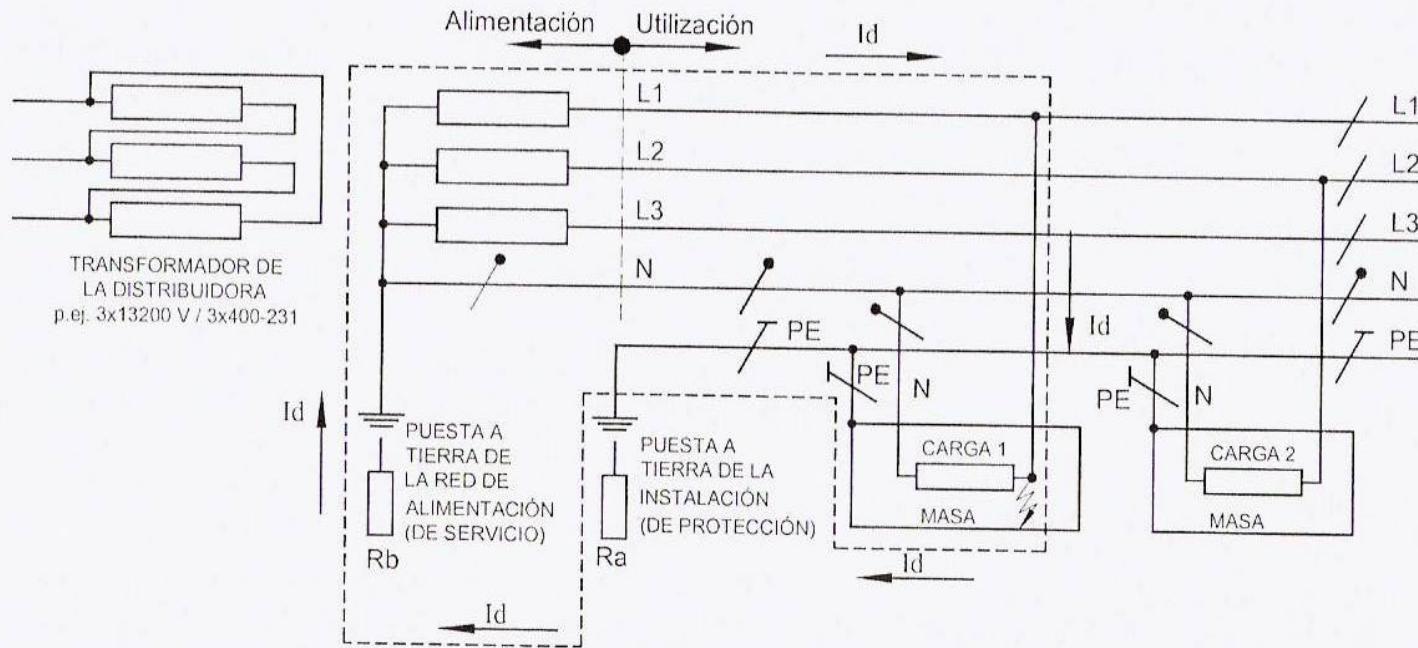


Figura 771.18.B – Lazo de falla esquema TT

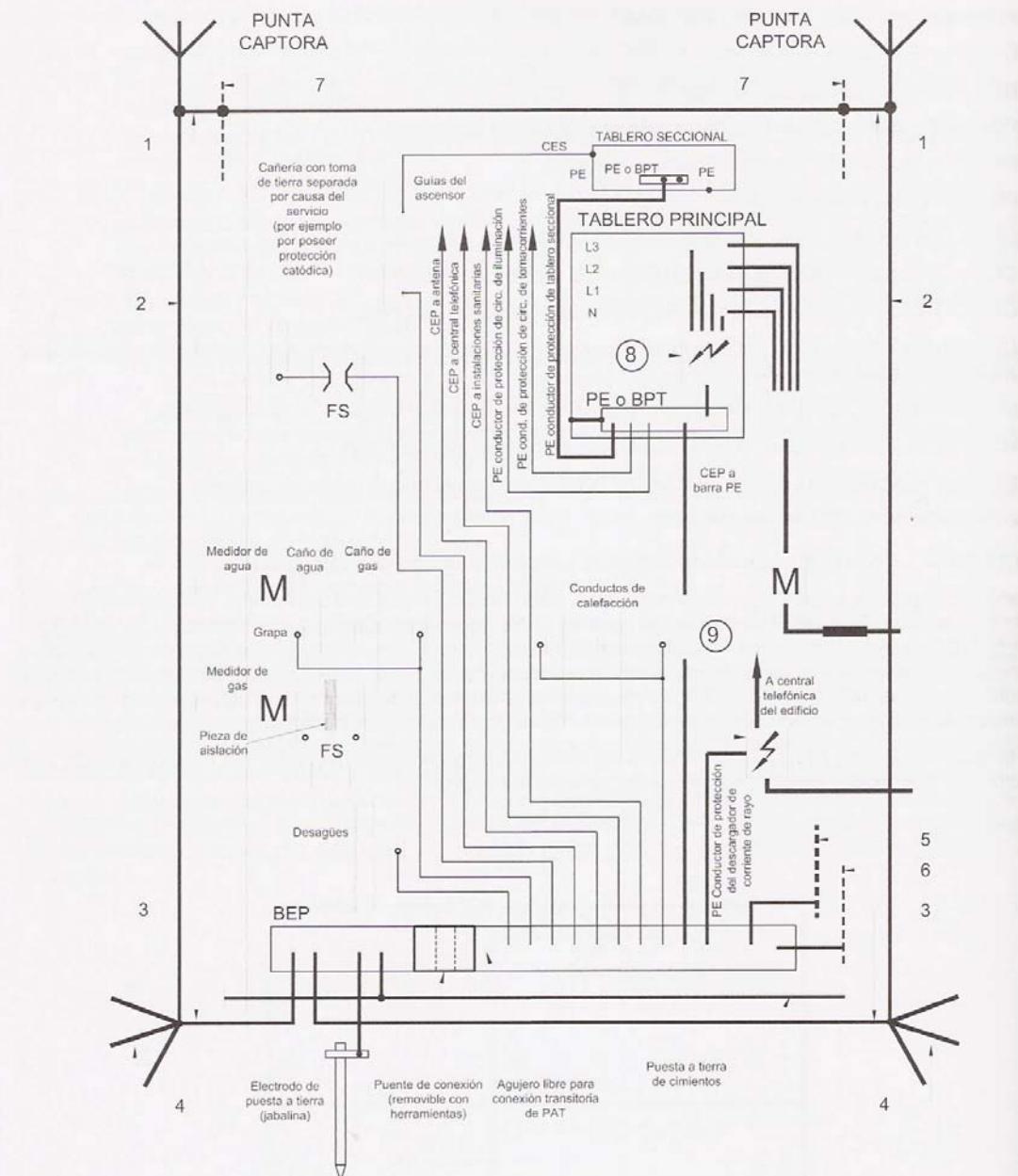
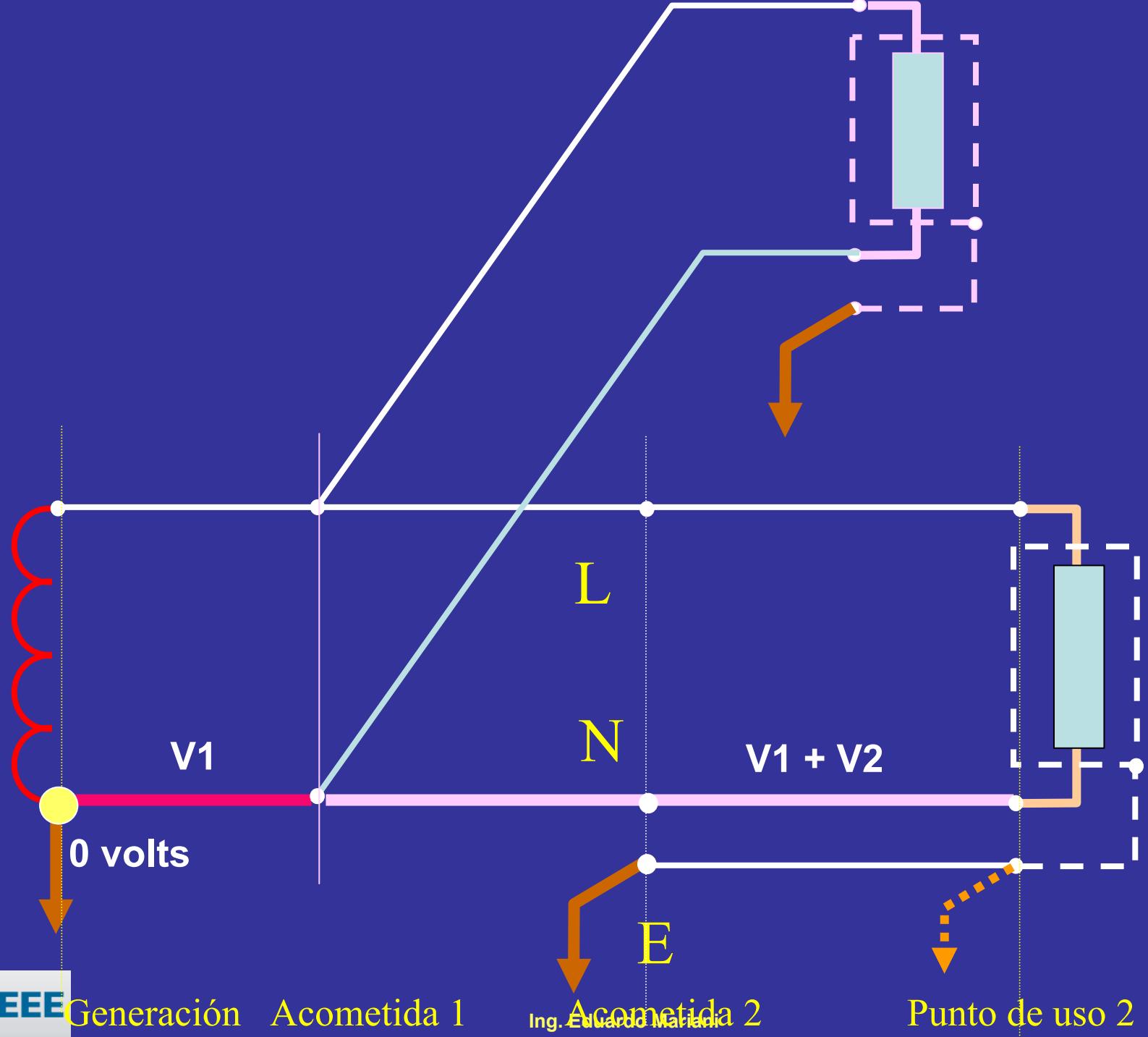


Figura 771.18.D – Equipotencialización típica en un esquema de conexión a tierra TT

Componentes armónicas debido a cargas no lineales.



Ejemplo con 3ra armónica en fase

$$V_r = V_{pr} \times \sin(\omega t + 0) + V_{pr_3} \times \sin 3(\omega t + 0)$$

$$V_s = V_{ps} \times \sin(\omega t + 120) + V_{ps_3} \times \sin 3(\omega t + 120)$$

$$V_s = V_{ps} \times \sin(\omega t + 120) + V_{ps_3} \times \sin 3\omega t$$

$$V_t = V_{pt} \times \sin(\omega t + 240) + V_{pt_3} \times \sin 3(\omega t + 240)$$

$$V_t = V_{pt} \times \sin(\omega t + 240) + V_{pt_3} \times \sin 3\omega t$$

Fin del primer modulo.

Segundo módulo

El “comportamiento” de un sistema de puesta a tierra en altas corrientes.

- Para estudiar el comportamiento de sistemas eléctricos, se los somete a distintos tipos de análisis
- Existe un “analizador” natural, el rayo

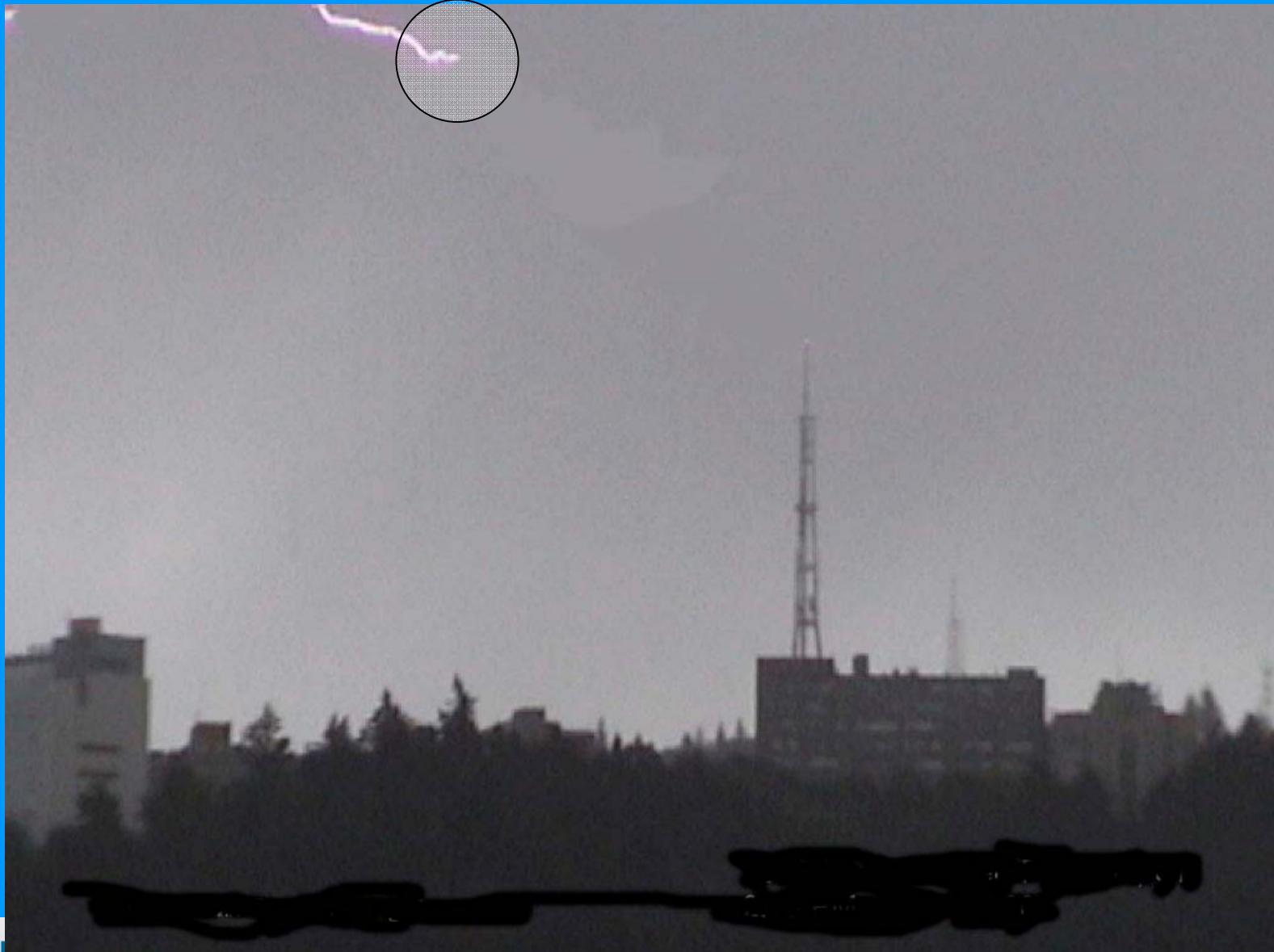
Sistemas de puesta a tierra para descargas atmosféricas, media y alta tensión.

- Parámetros de la corriente de un rayo.
- Normas IEC y NFPA.
- Geometría de la puesta a tierra.
- Cobertura de un pararrayos.

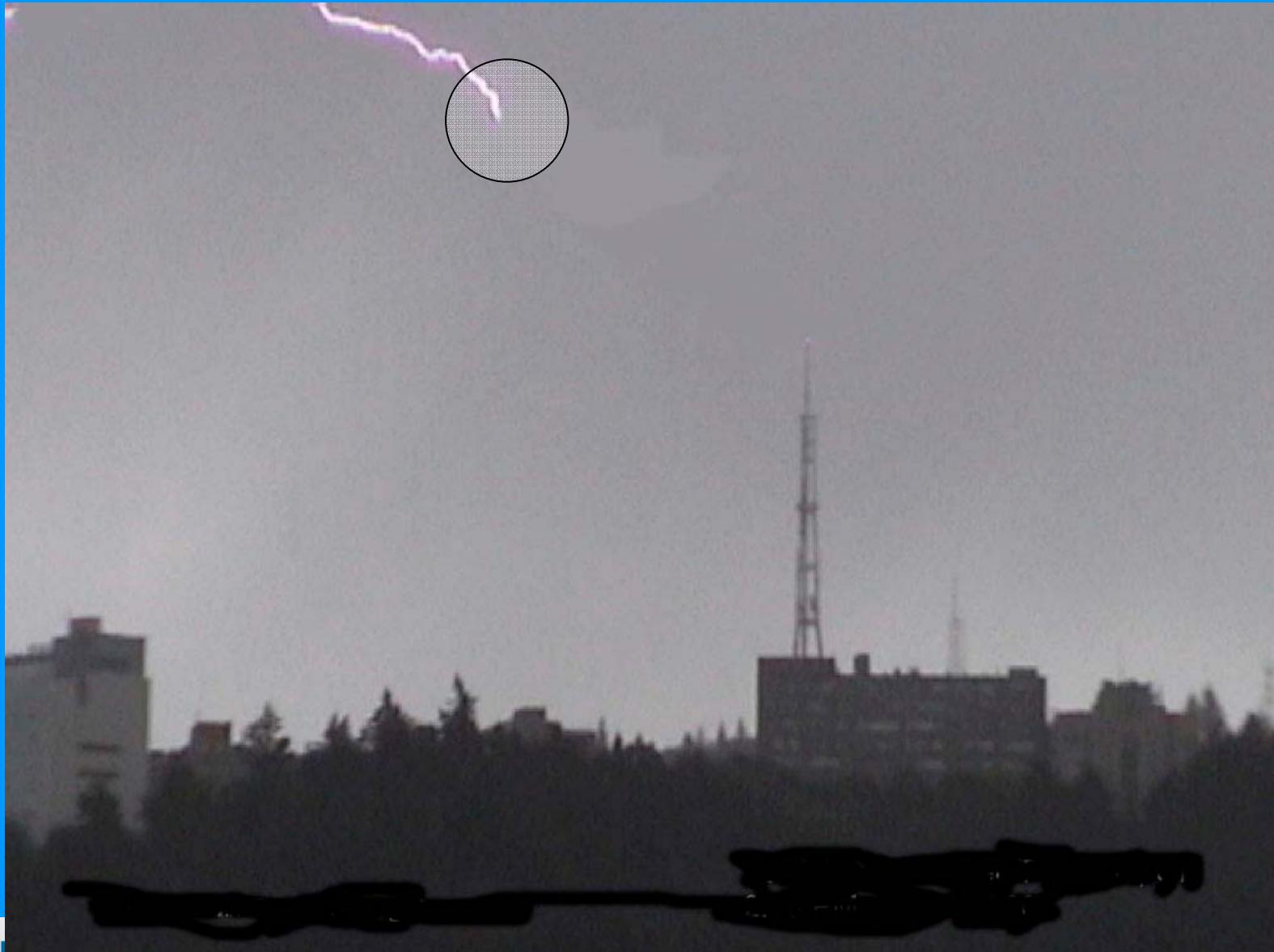
La “caída” de un rayo



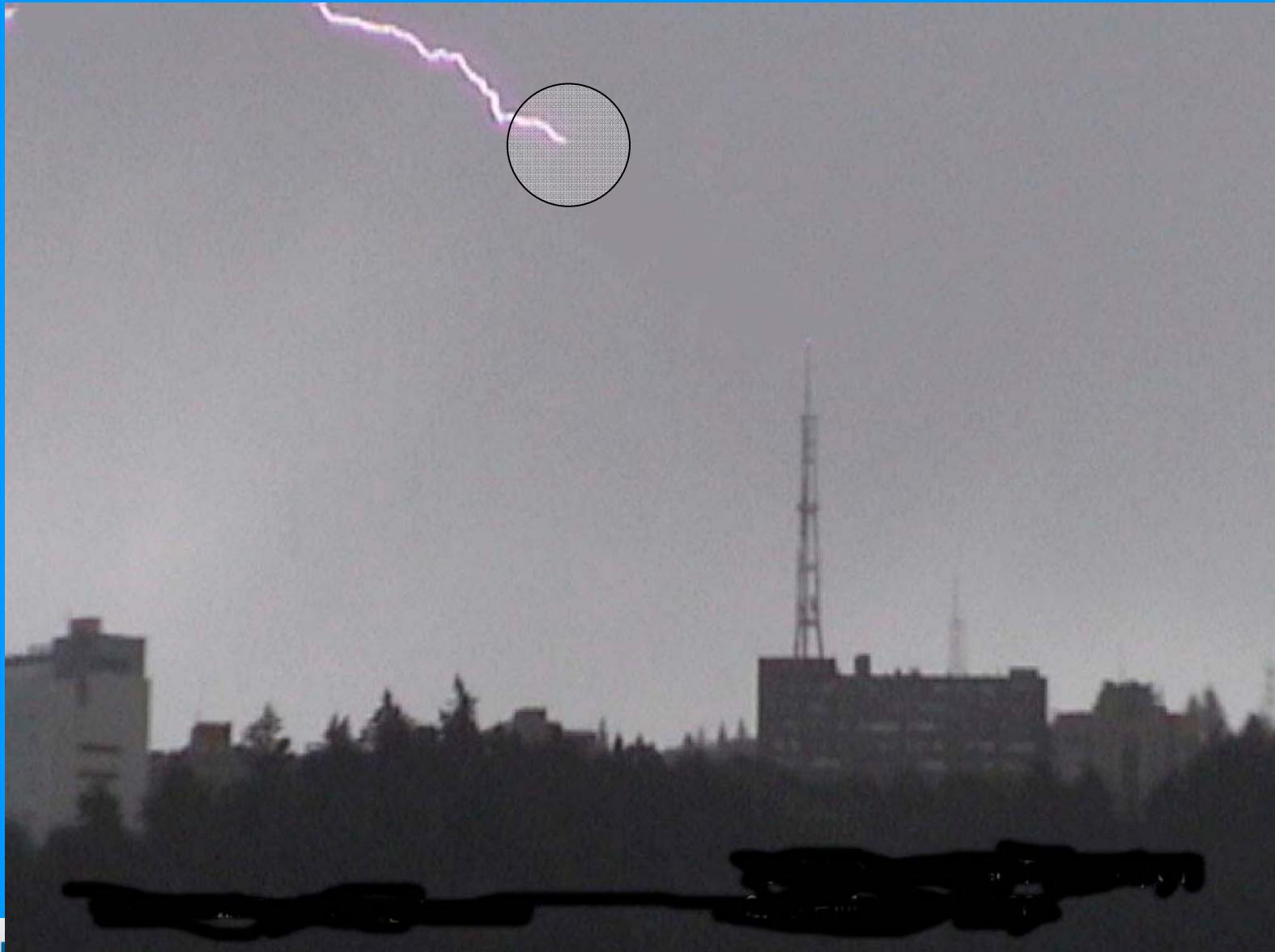
La “caída” de un rayo



La “caída” de un rayo



La “caída” de un rayo



La “caída” de un rayo



La “caída” de un rayo



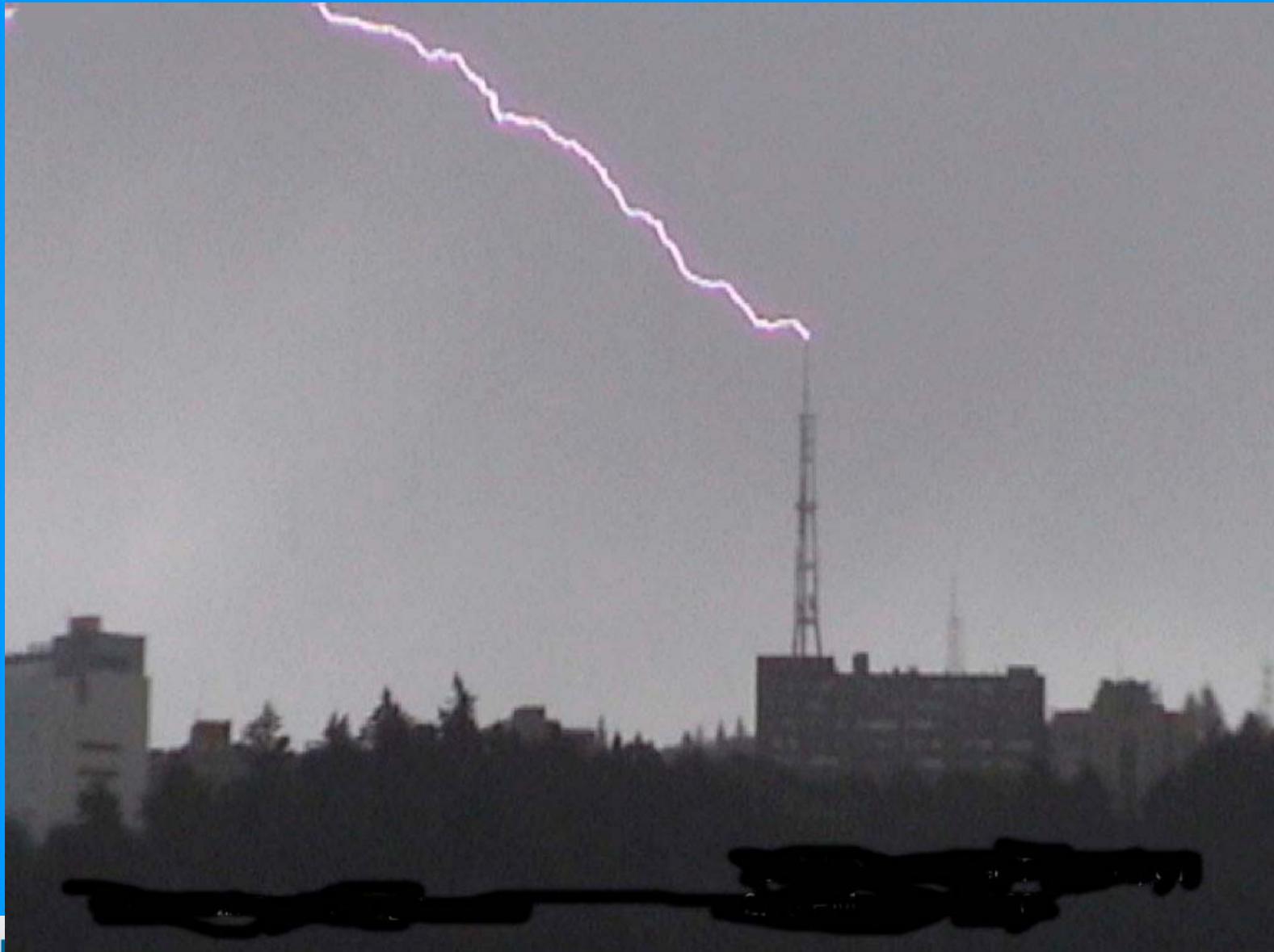
La “caída” de un rayo



La “caída” de un rayo



La “caída” de un rayo



Métodos de Protección (Teoría electrogeométrica)

Sistemas Franklin y Faraday

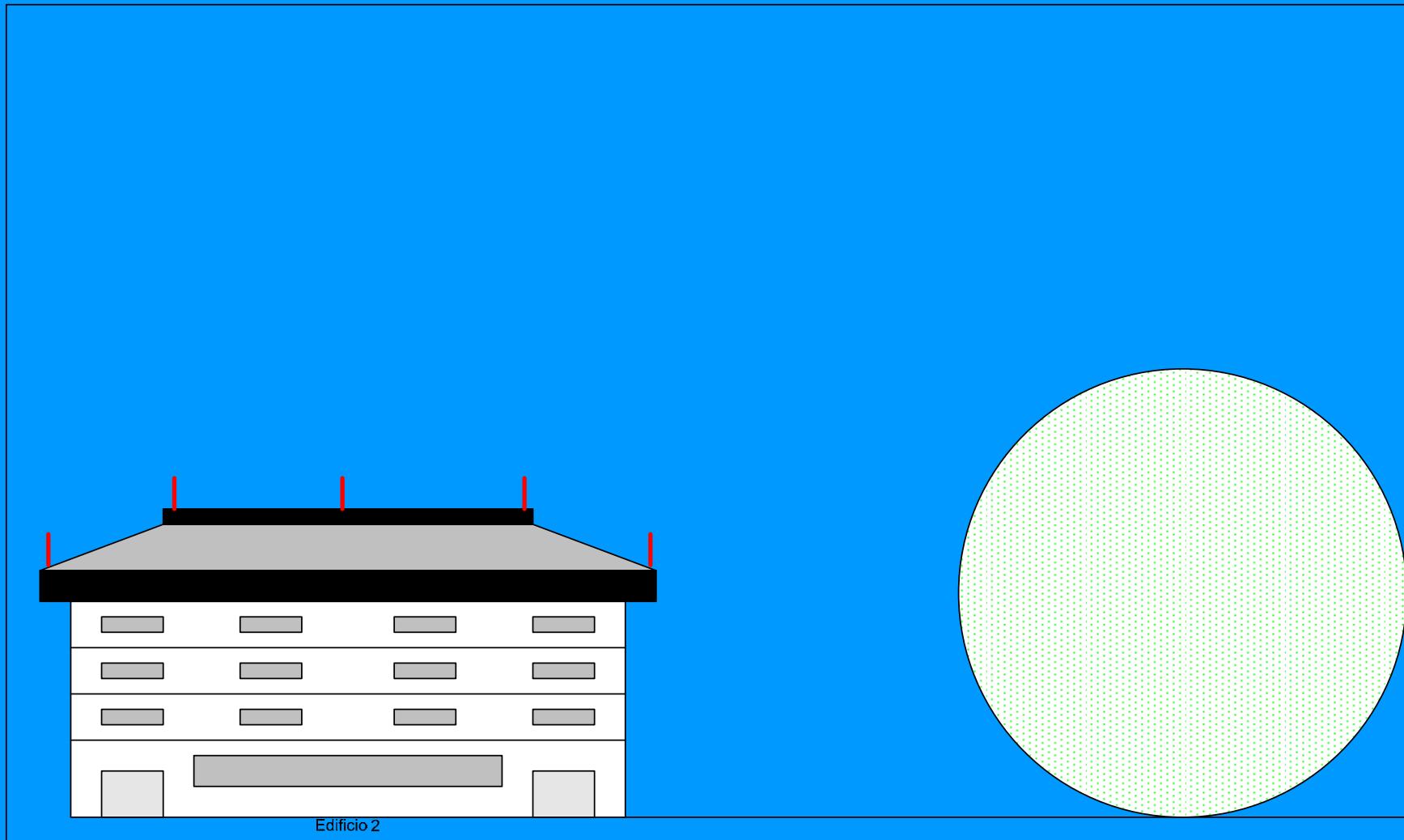
Normas más divulgadas

- IEC 61024
- IRAM 2184
- NFPA 780
- NFC 17100

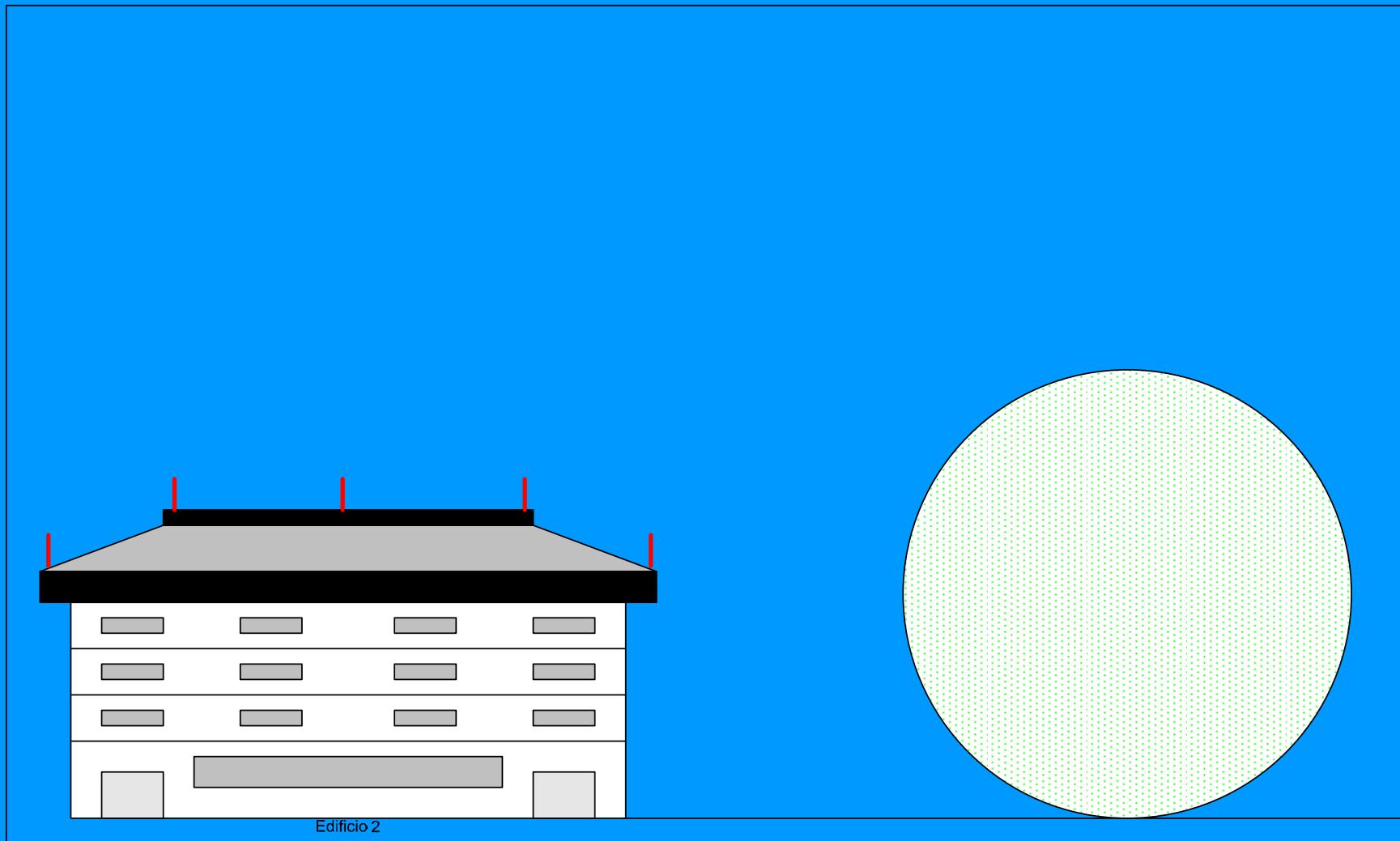
Métodos de Protección (Teoría electrogeométrica)



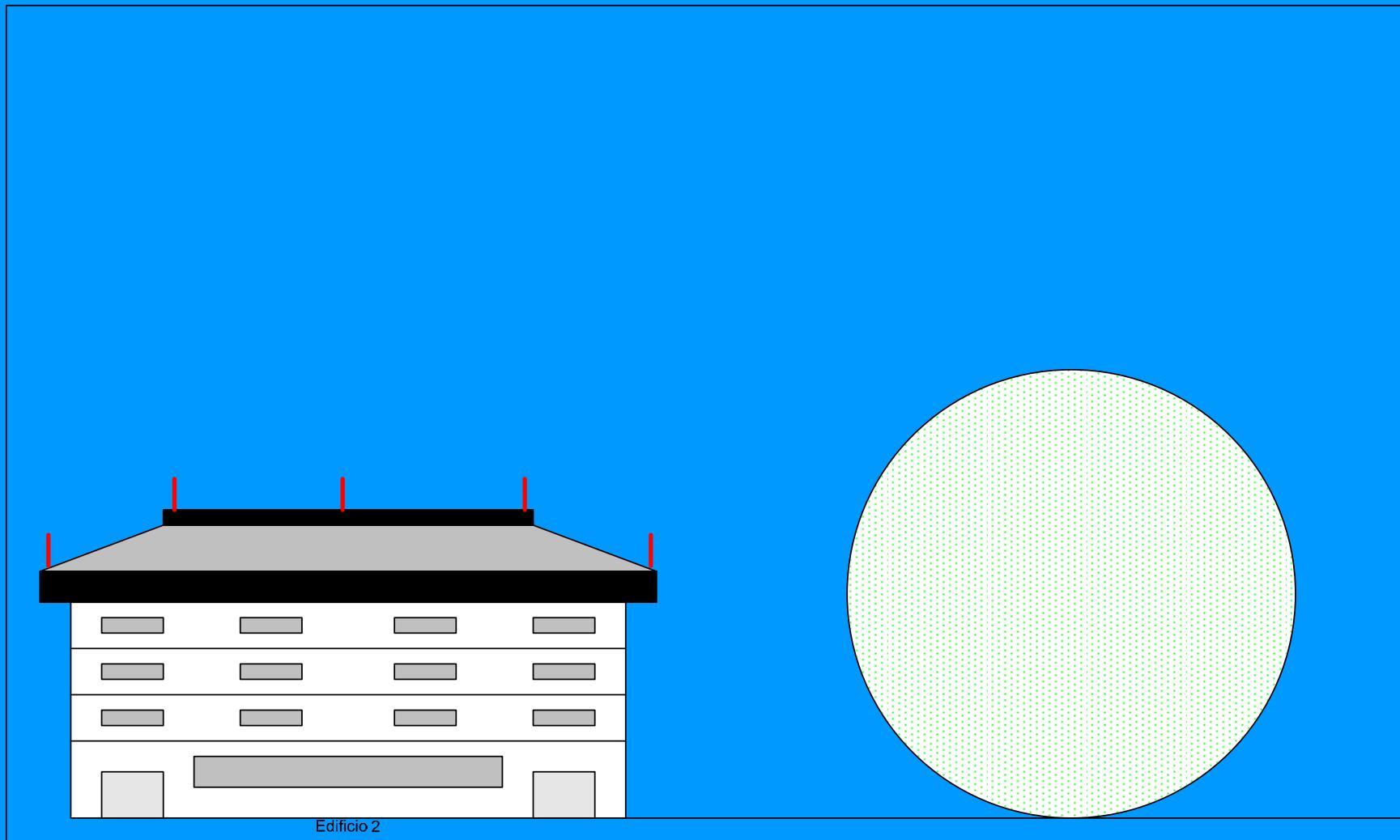
Métodos de Protección (Teoría electrogeométrica)



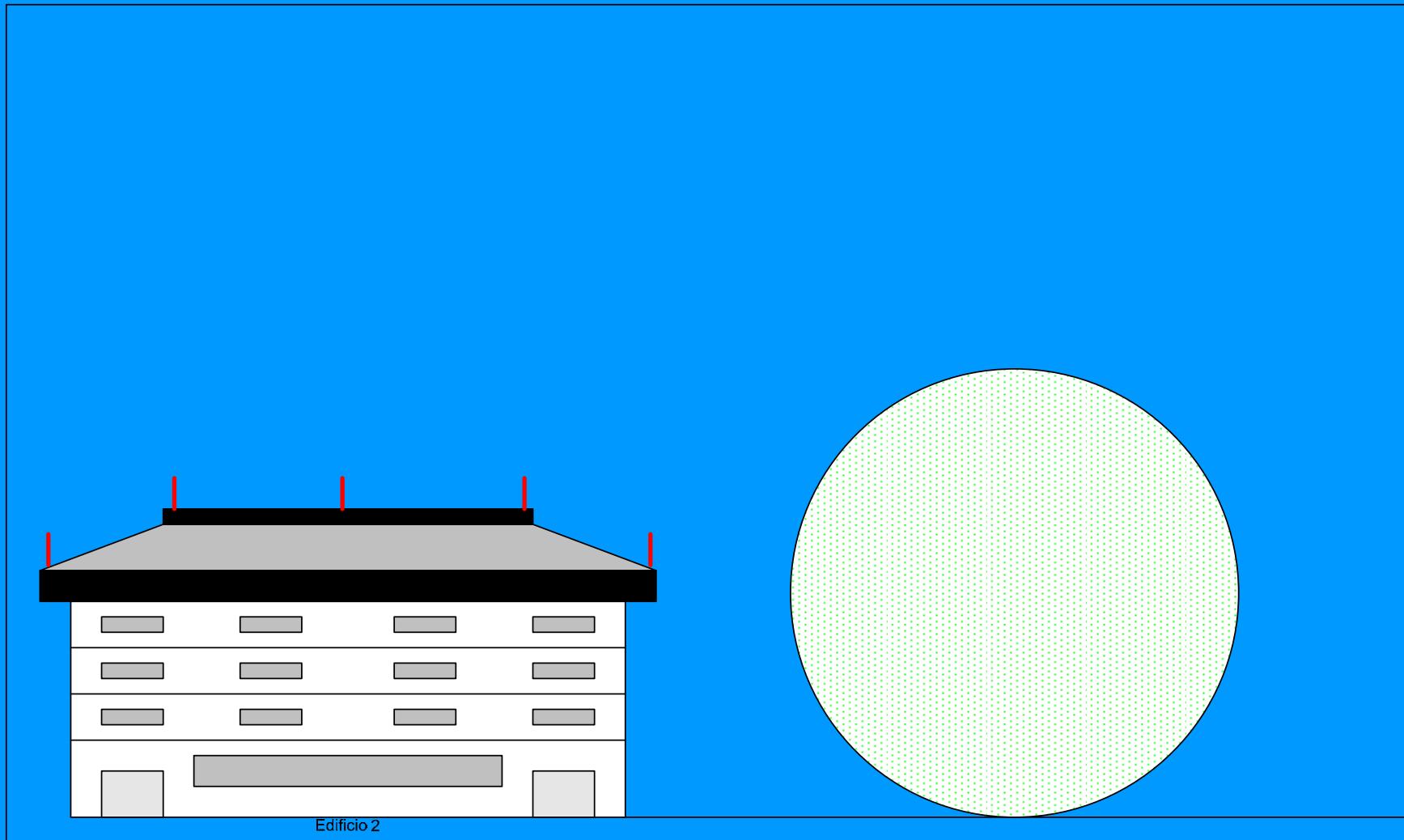
Métodos de Protección (Teoría electrogeométrica)



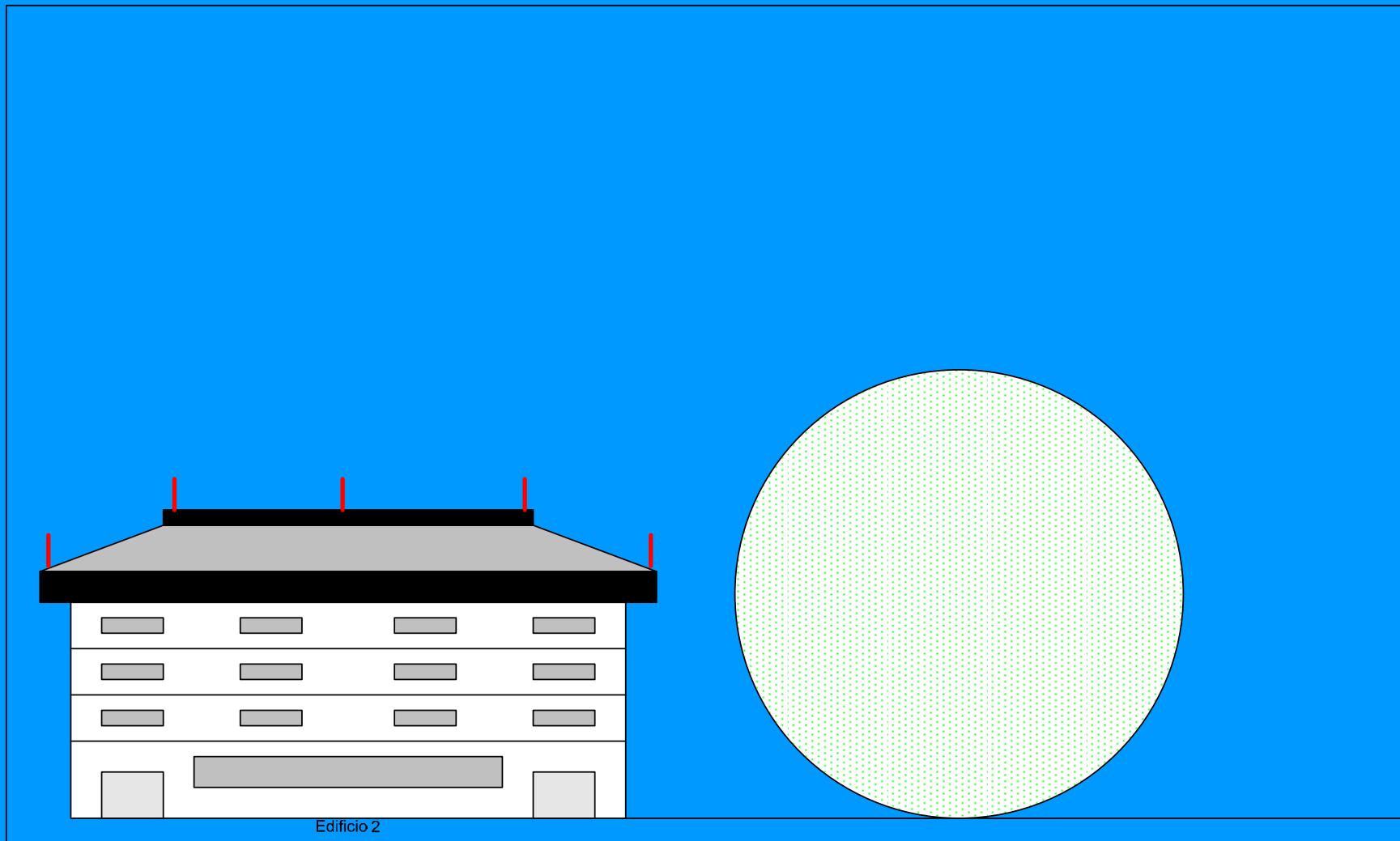
Métodos de Protección (Teoría electrogeométrica)



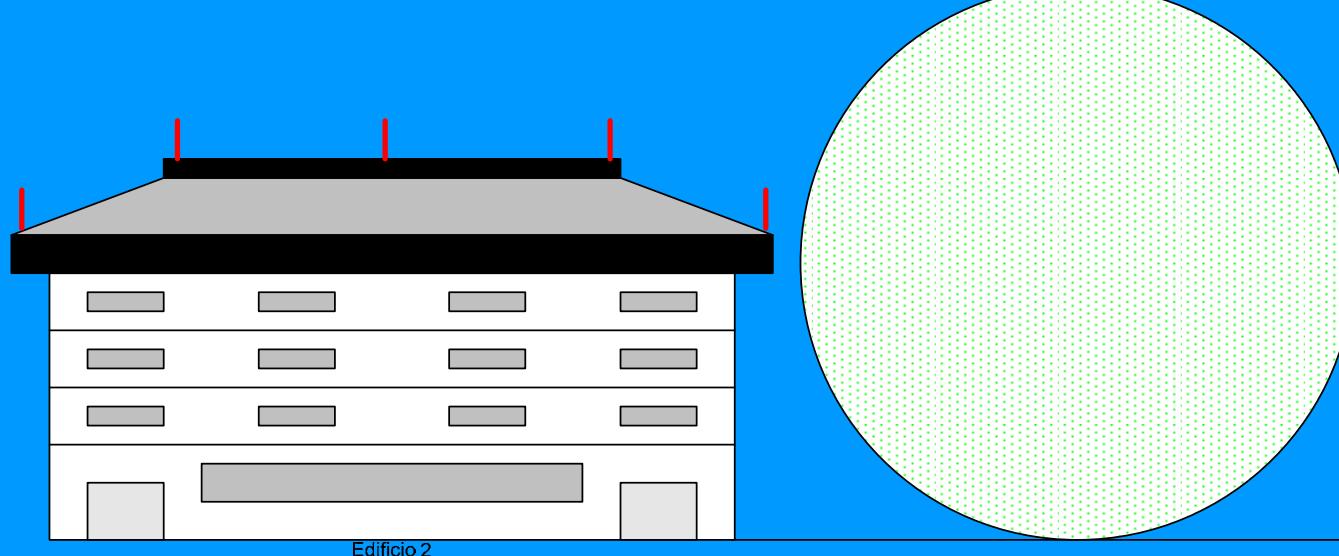
Métodos de Protección (Teoría electrogeométrica)



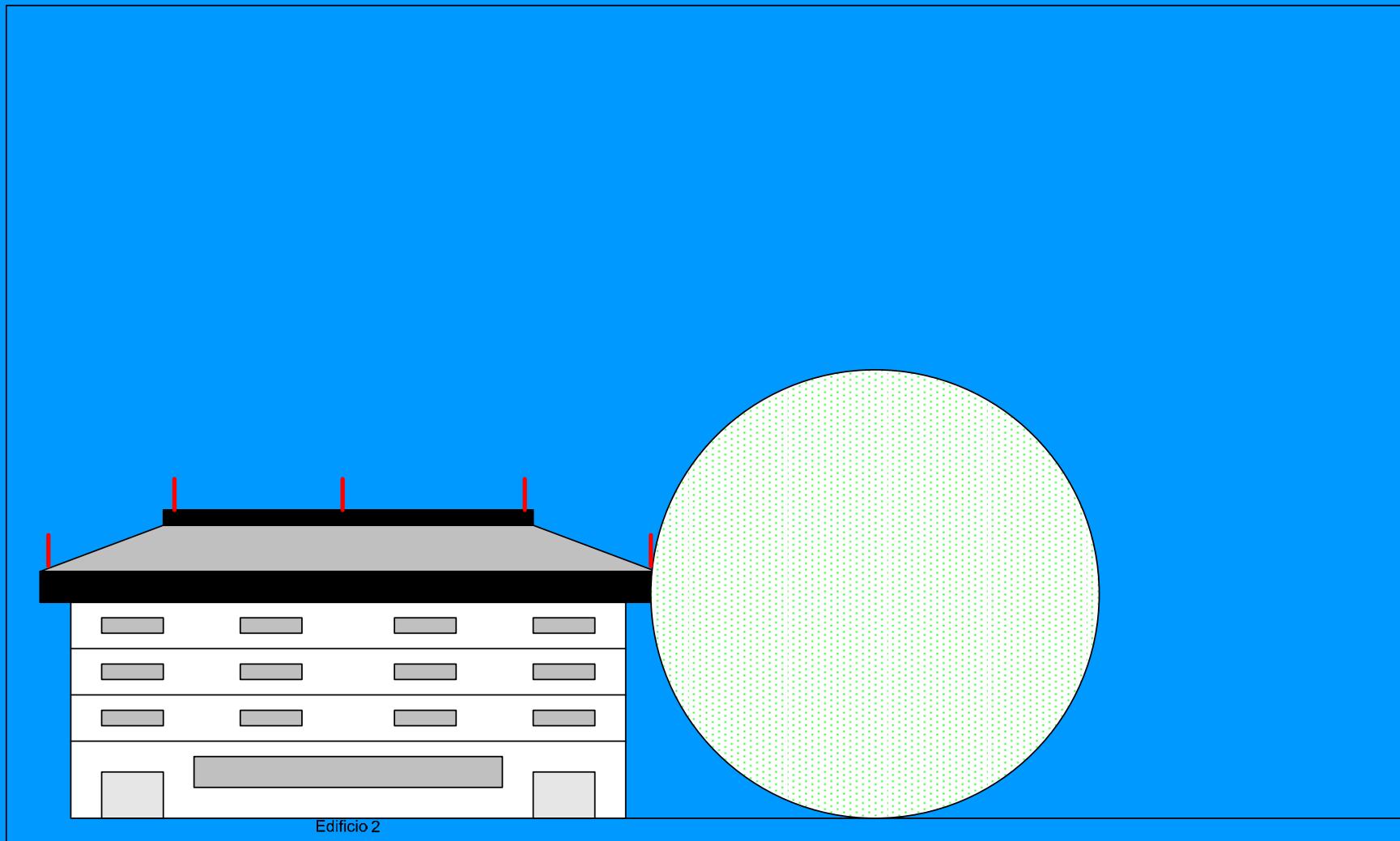
Métodos de Protección (Teoría electrogeométrica)



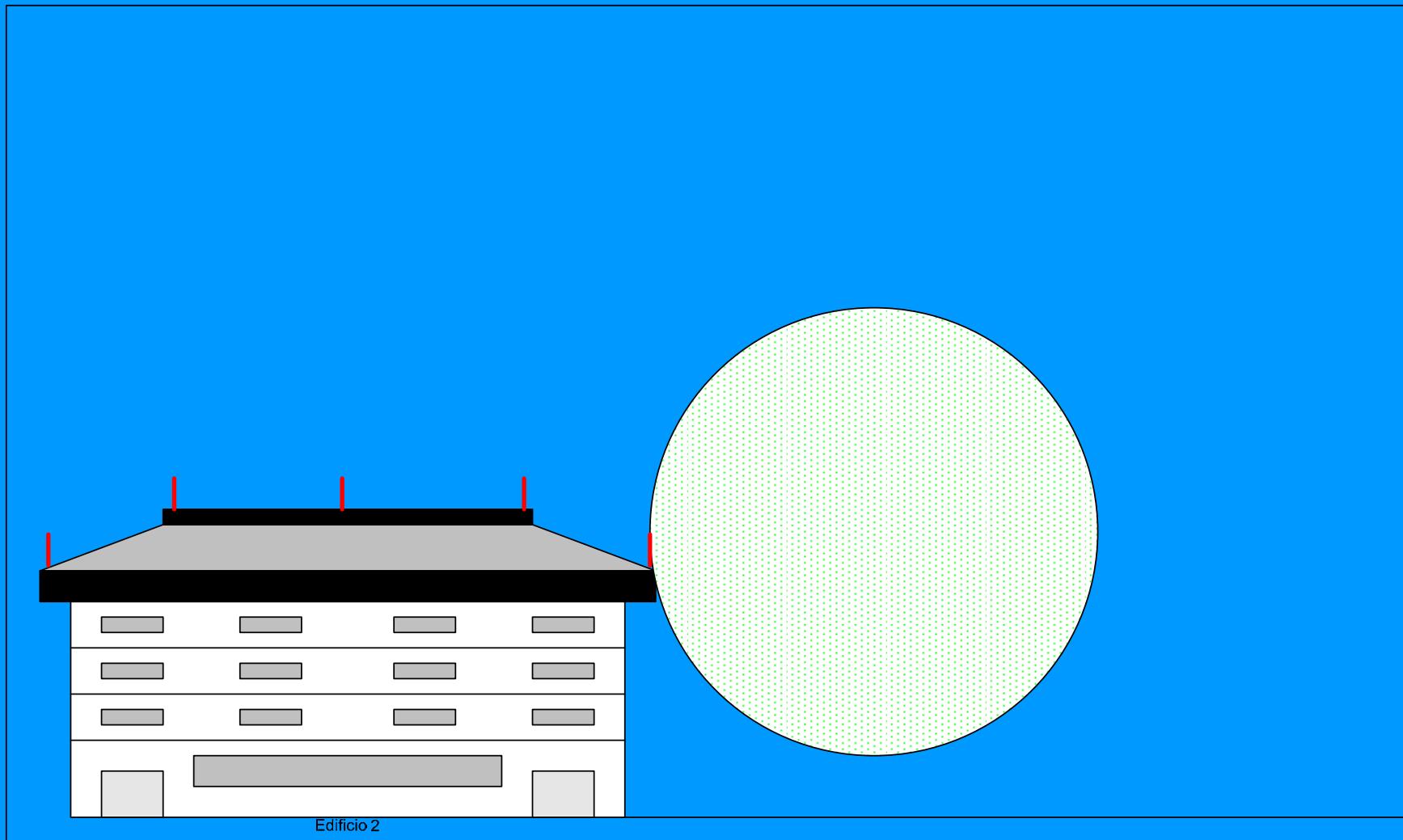
Métodos de Protección (Teoría electrogeométrica)



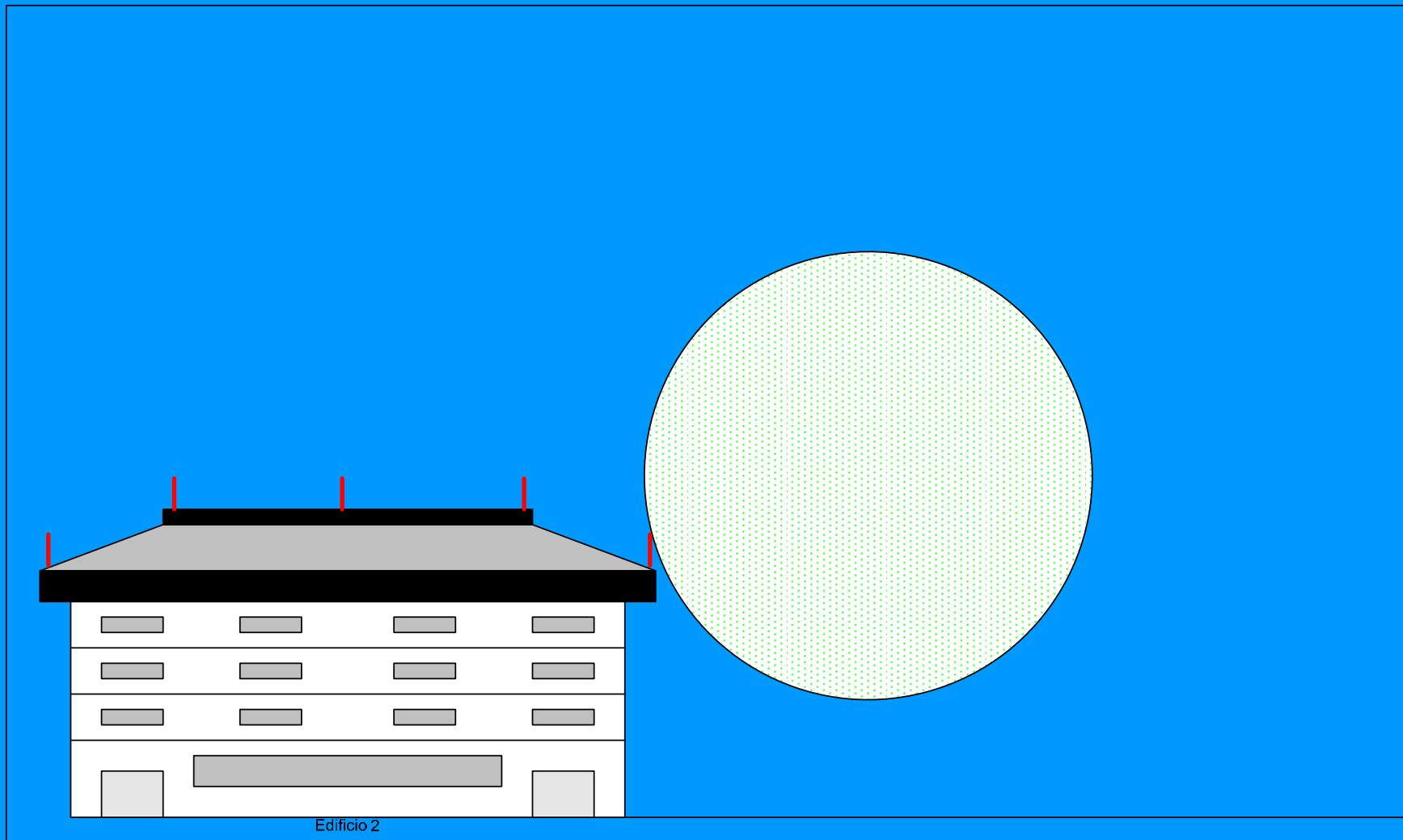
Métodos de Protección (Teoría electrogeométrica)



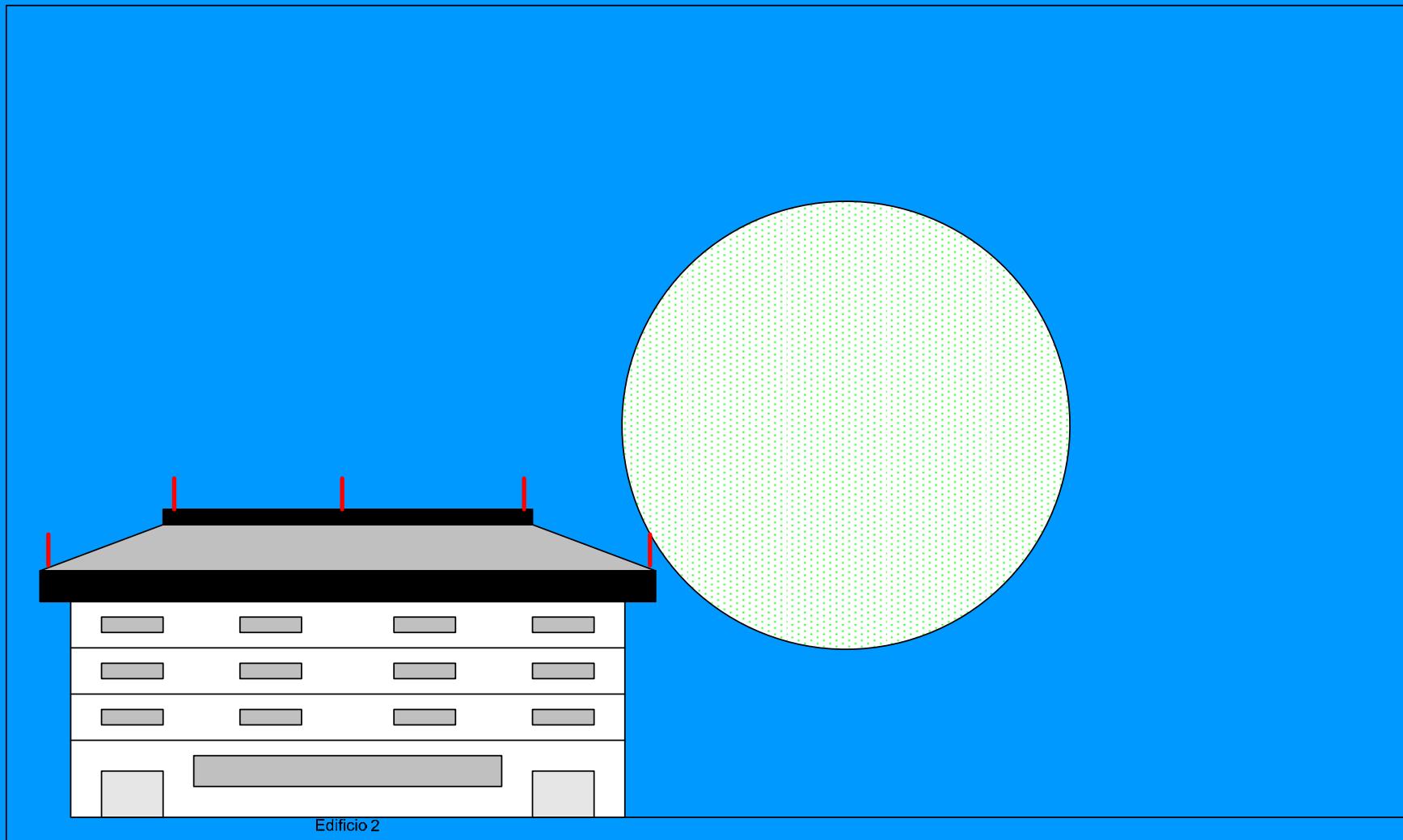
Métodos de Protección (Teoría electrogeométrica)



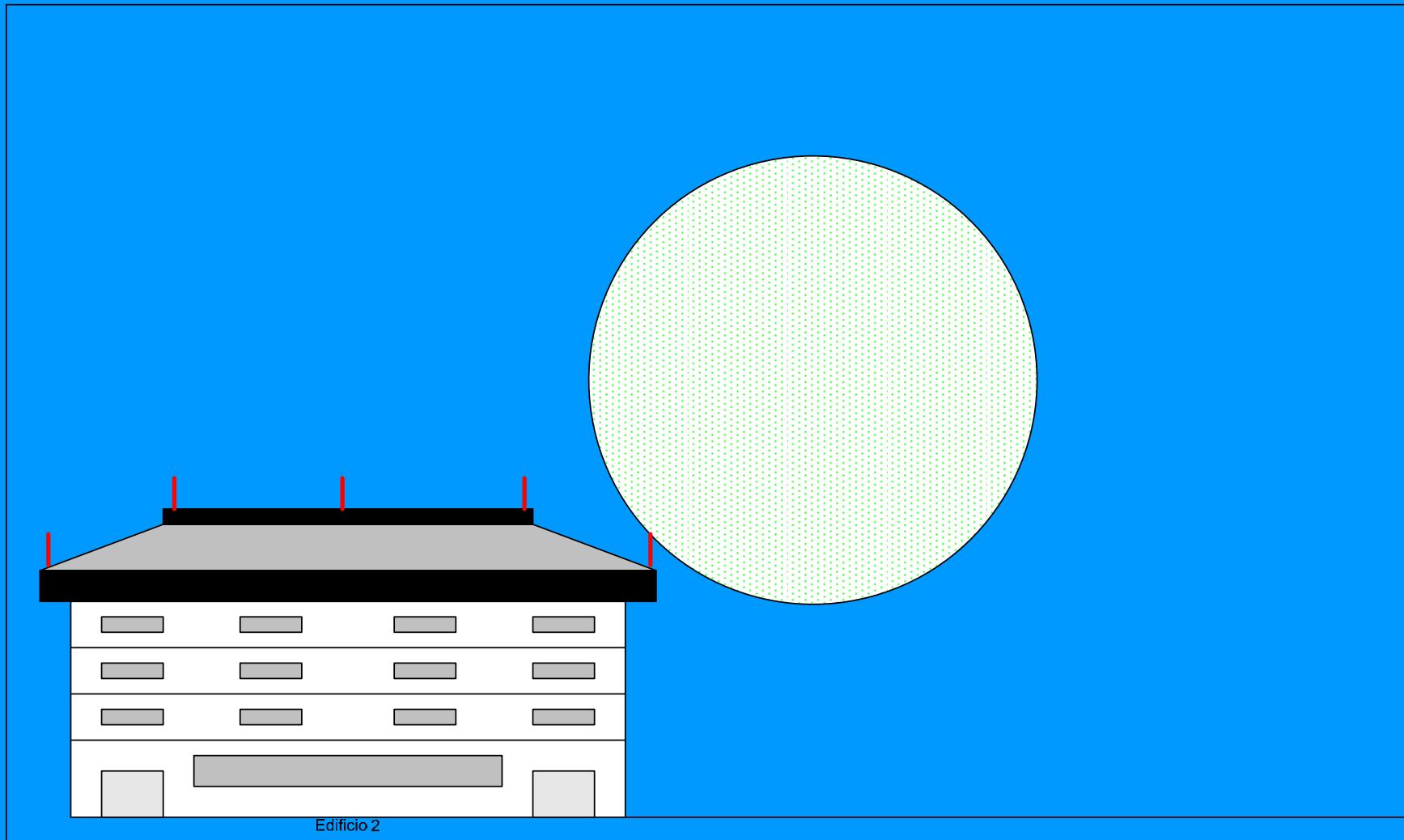
Métodos de Protección (Teoría electrogeométrica)



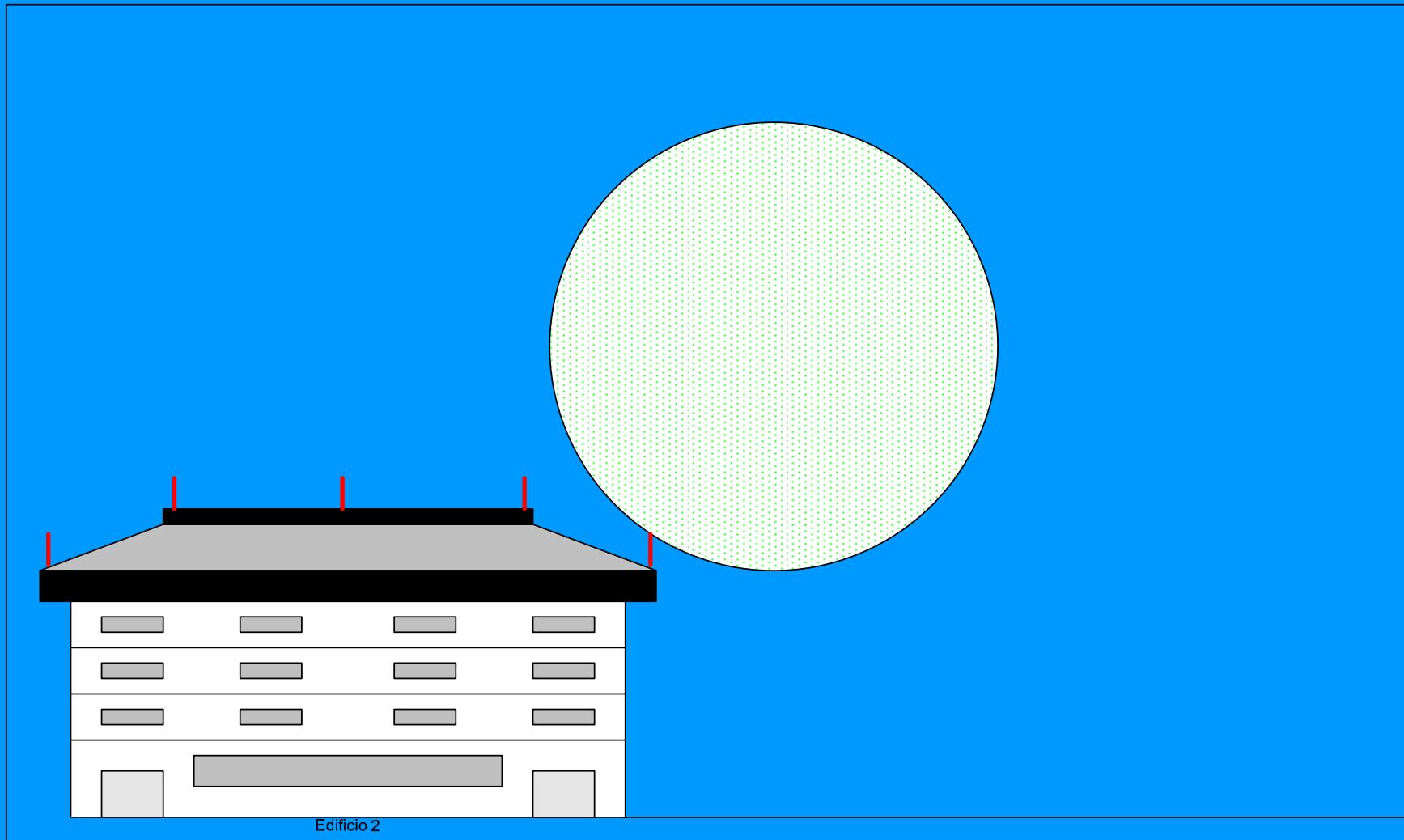
Métodos de Protección (Teoría electrogeométrica)



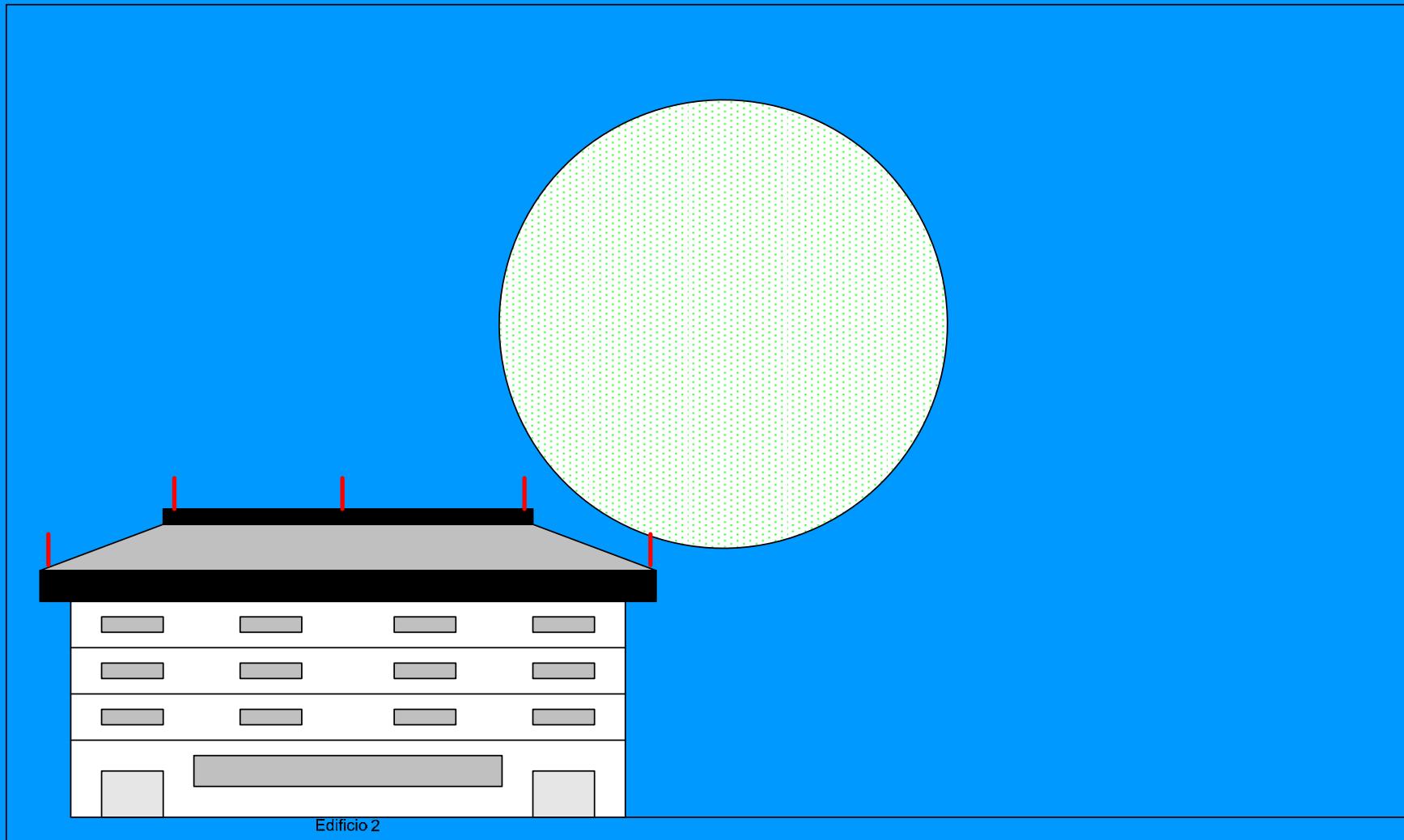
Métodos de Protección (Teoría electrogeométrica)



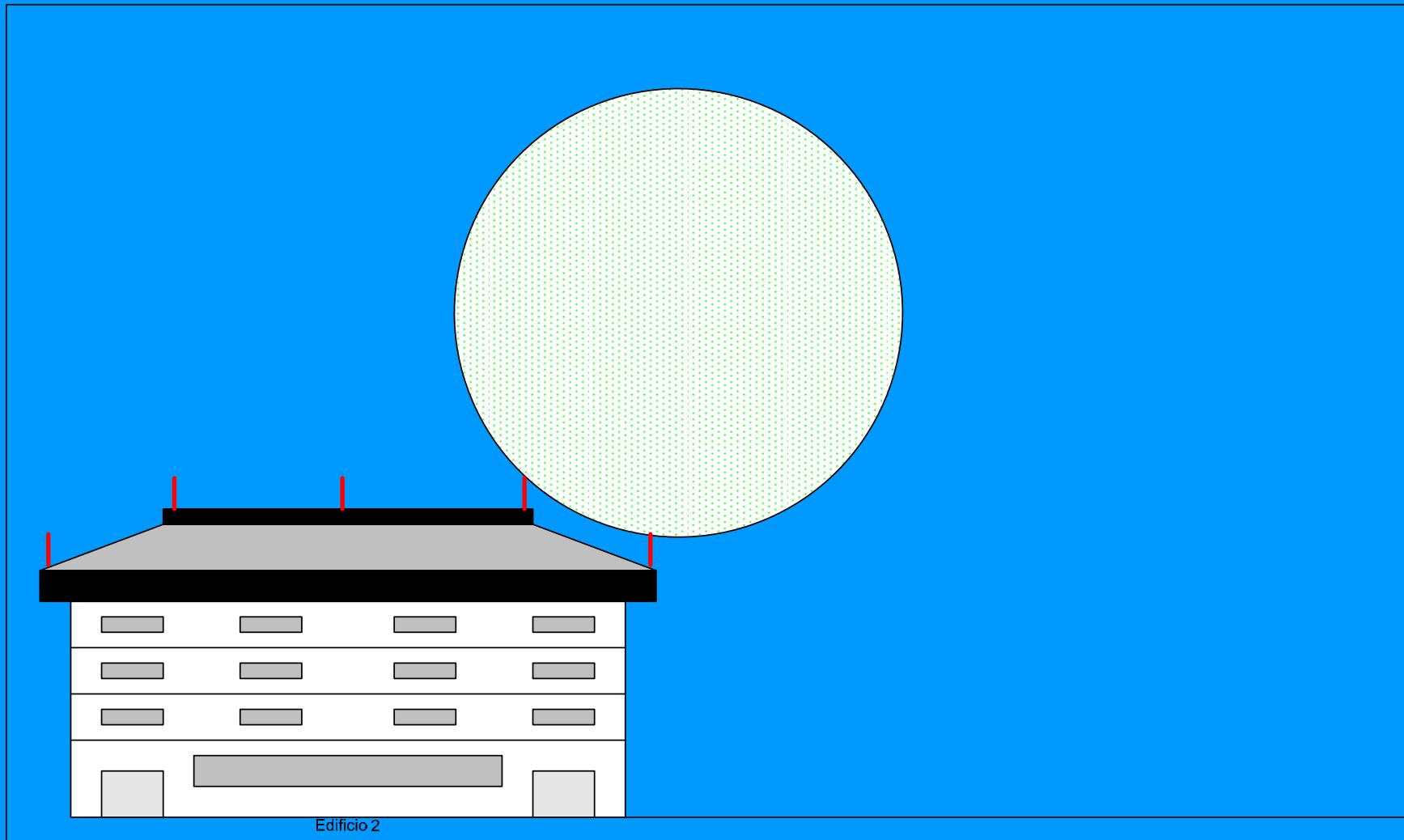
Métodos de Protección (Teoría electrogeométrica)



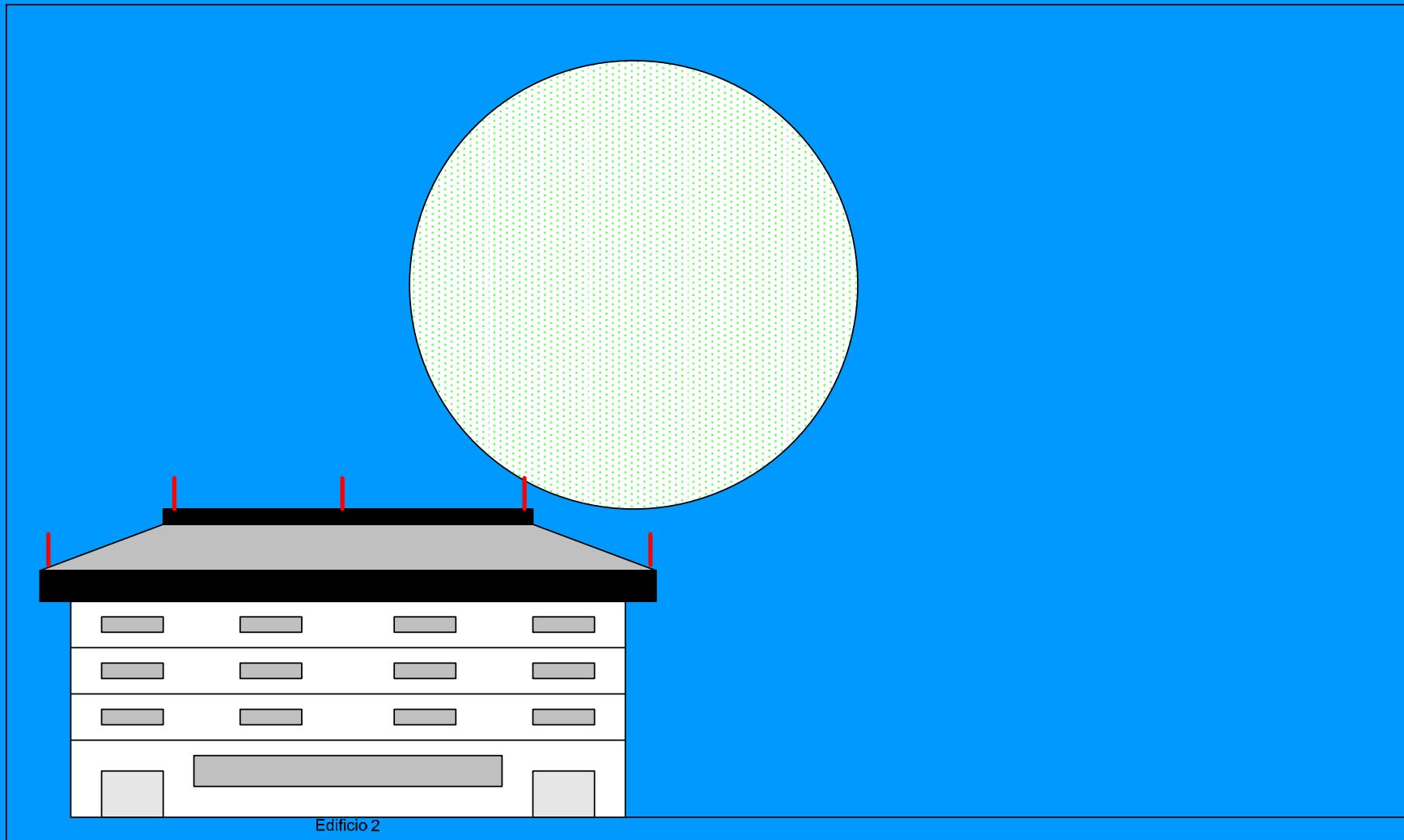
Métodos de Protección (Teoría electrogeométrica)



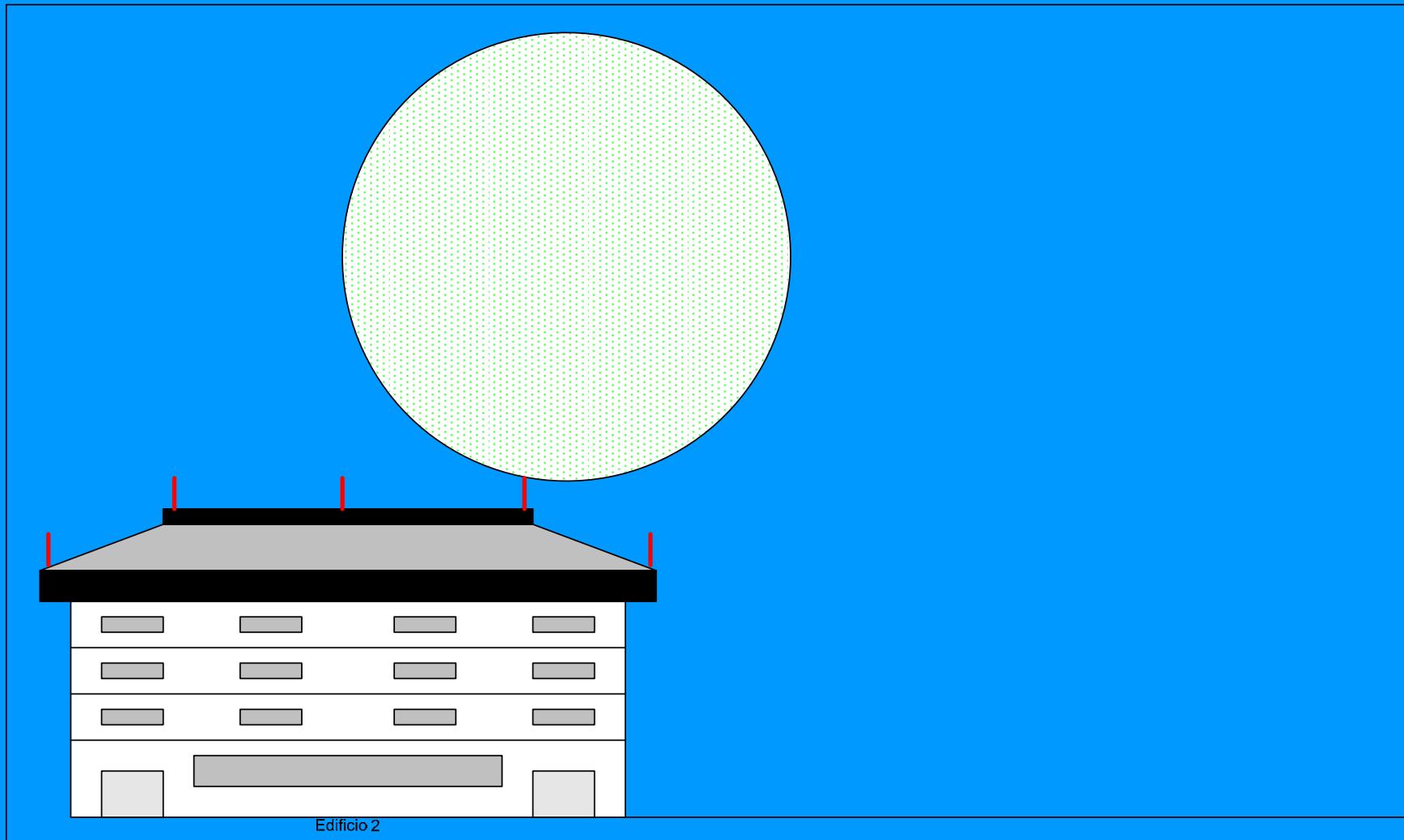
Métodos de Protección (Teoría electrogeométrica)



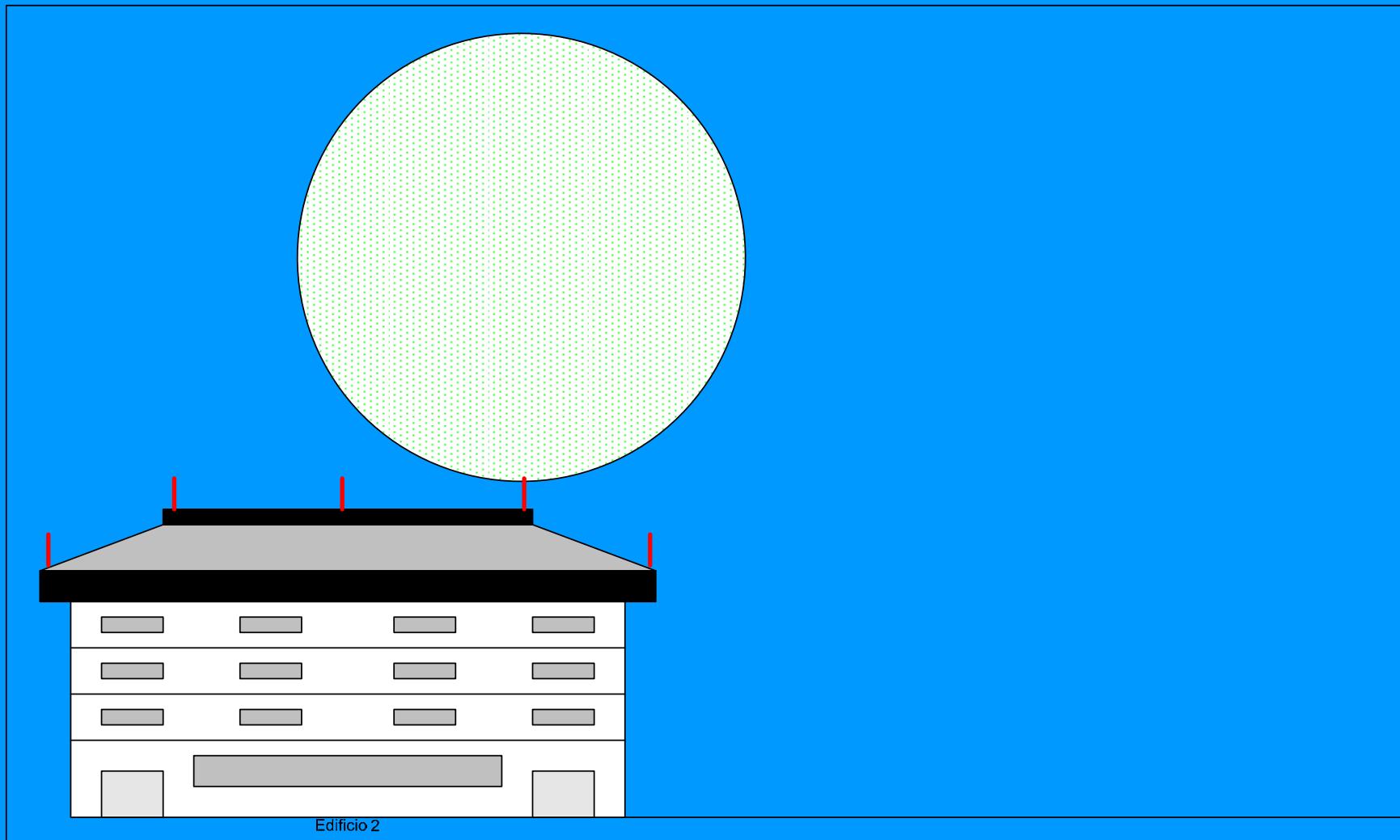
Métodos de Protección (Teoría electrogeométrica)



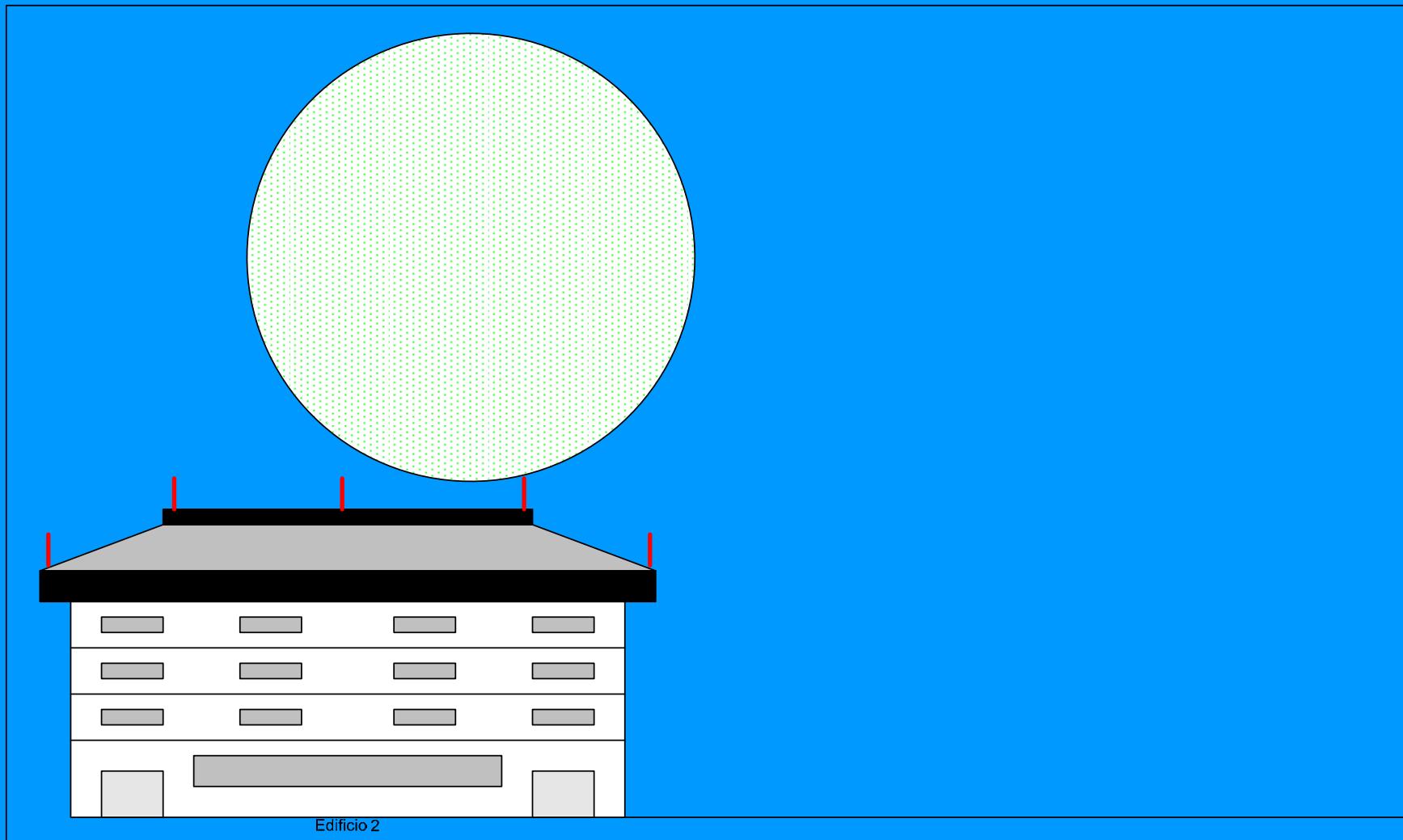
Métodos de Protección (Teoría electrogeométrica)



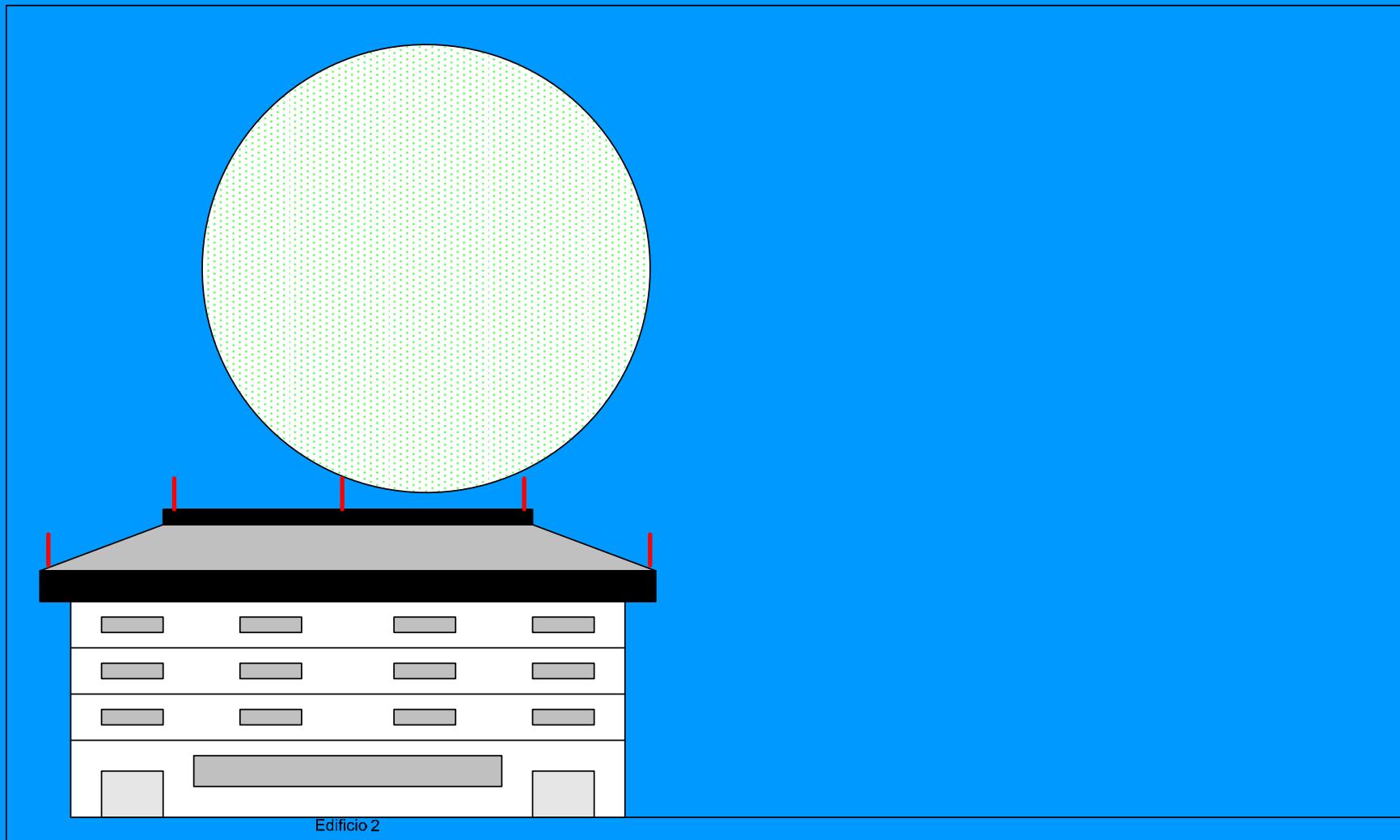
Métodos de Protección (Teoría electrogeométrica)



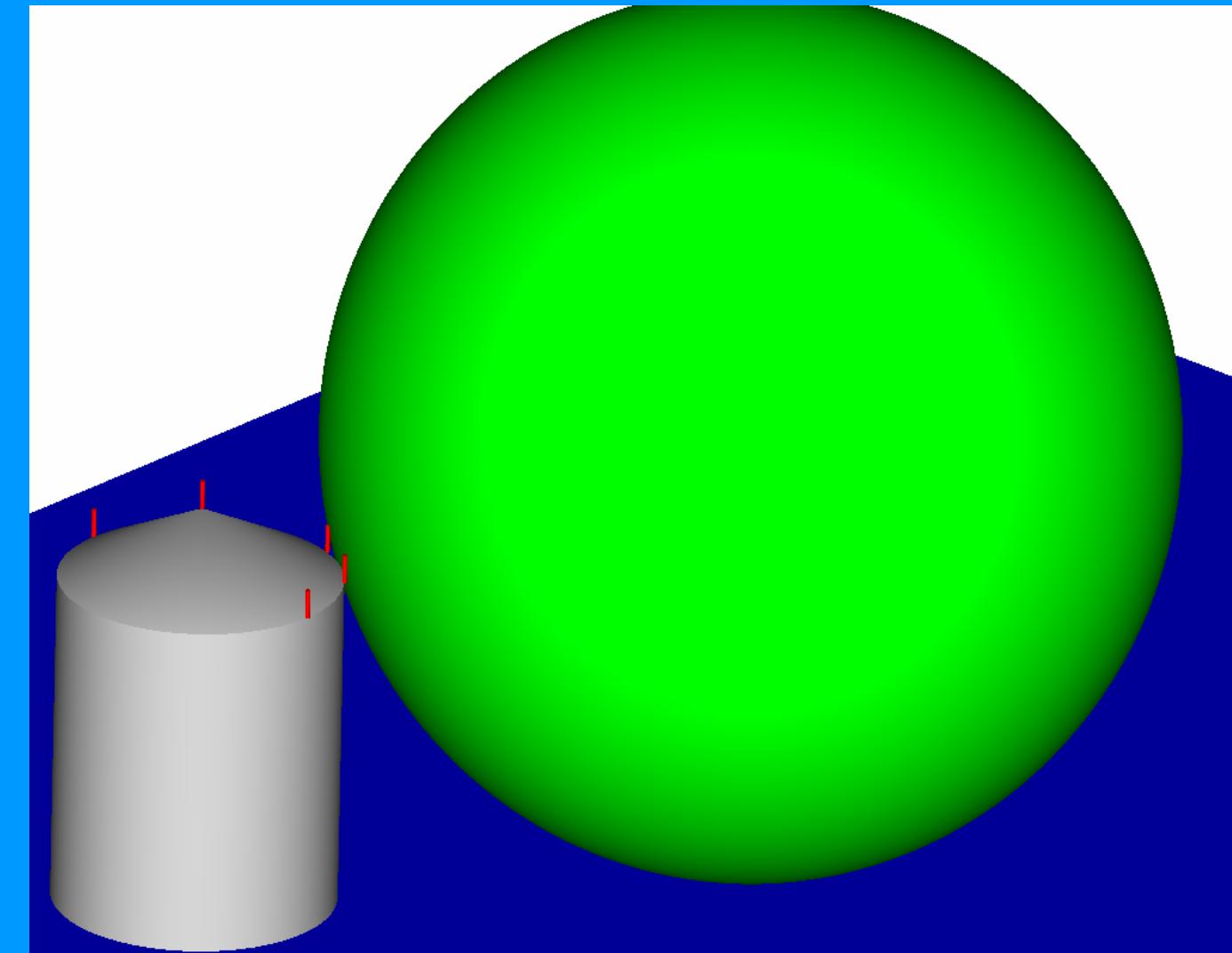
Métodos de Protección (Teoría electrogeométrica)



Métodos de Protección (Teoría electrogeométrica)



Métodos de Protección (Teoría electrogeométrica)



Verificación
mediante
Autocad®

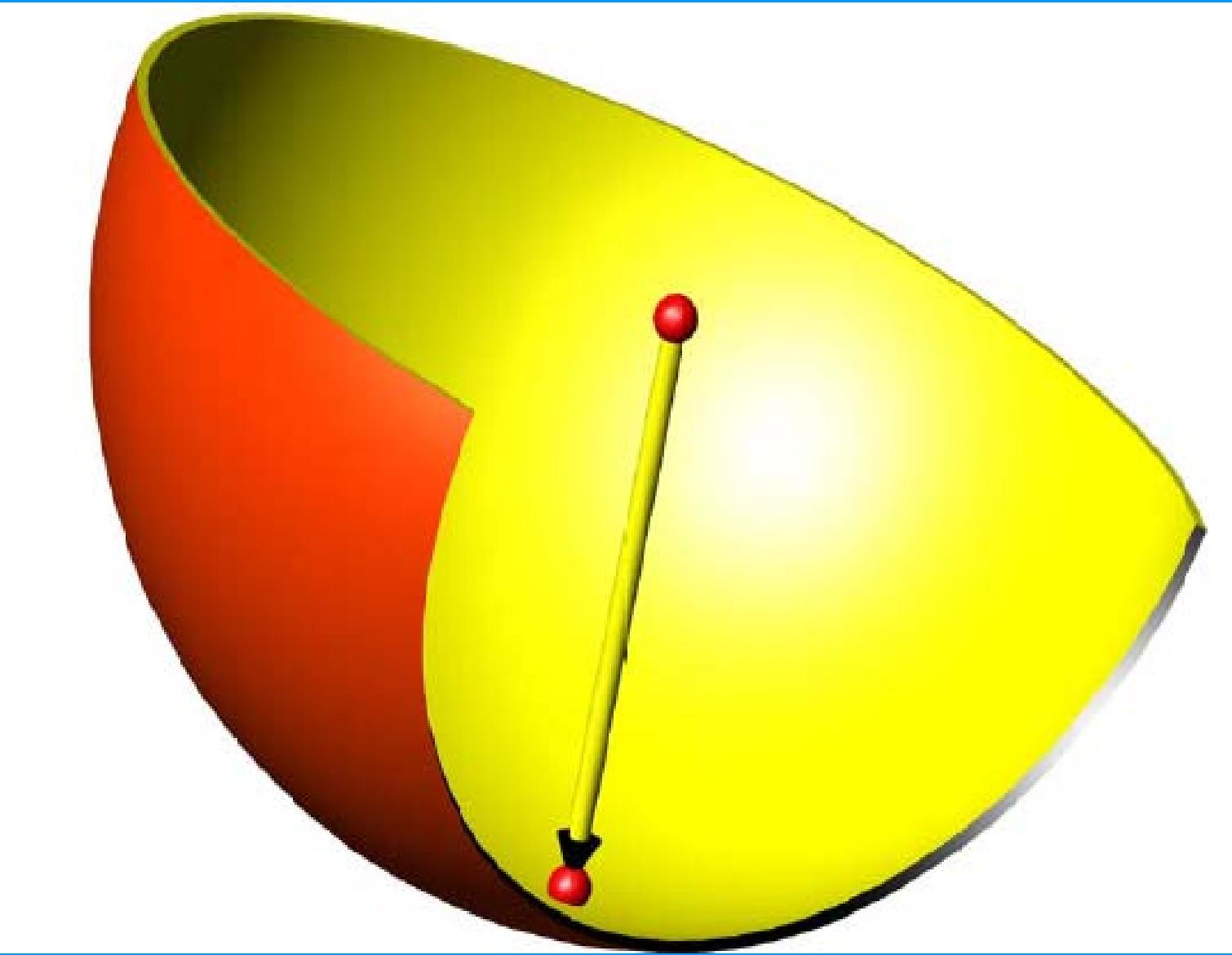
Métodos de Protección (Teoría electrogeométrica)

Punta Franklin
convencional

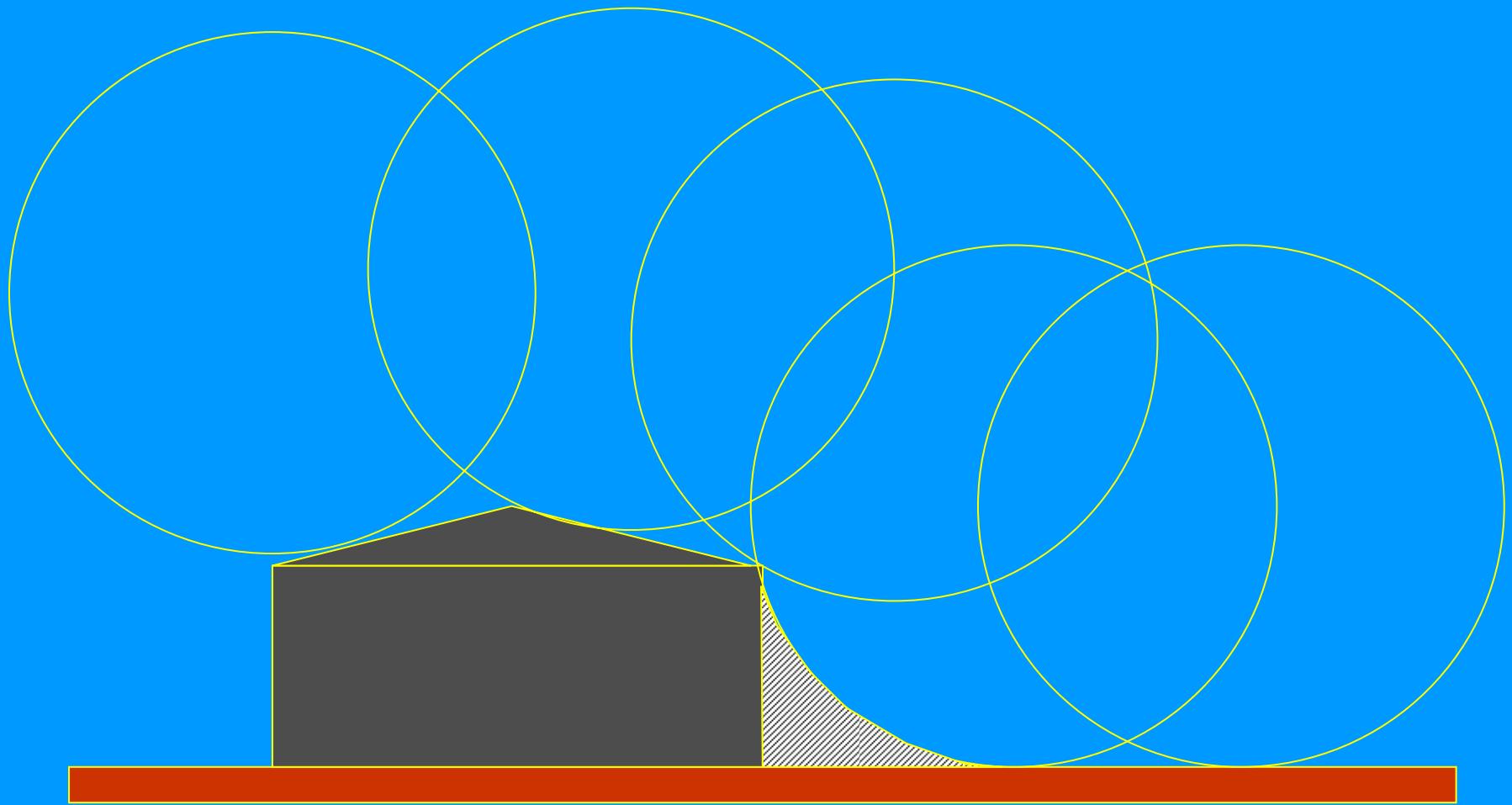


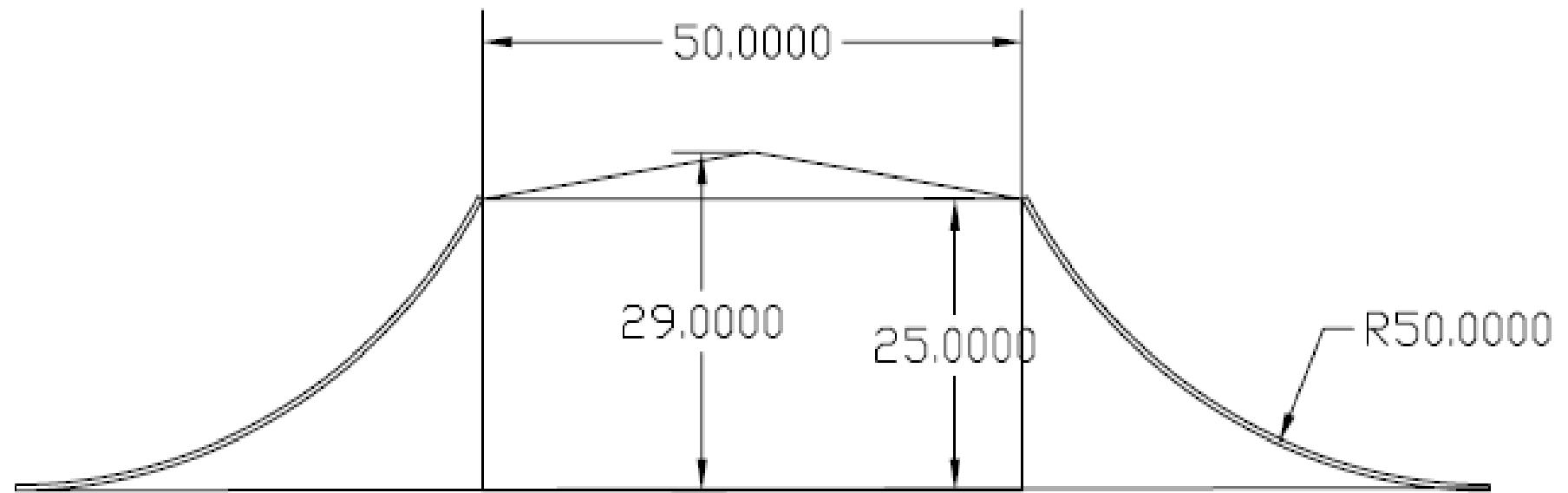
Punta Propuesta por el Prof.
Charlie Moore al Comité NFPA
780. Mencionada en la edición
2000 de NFPA 780

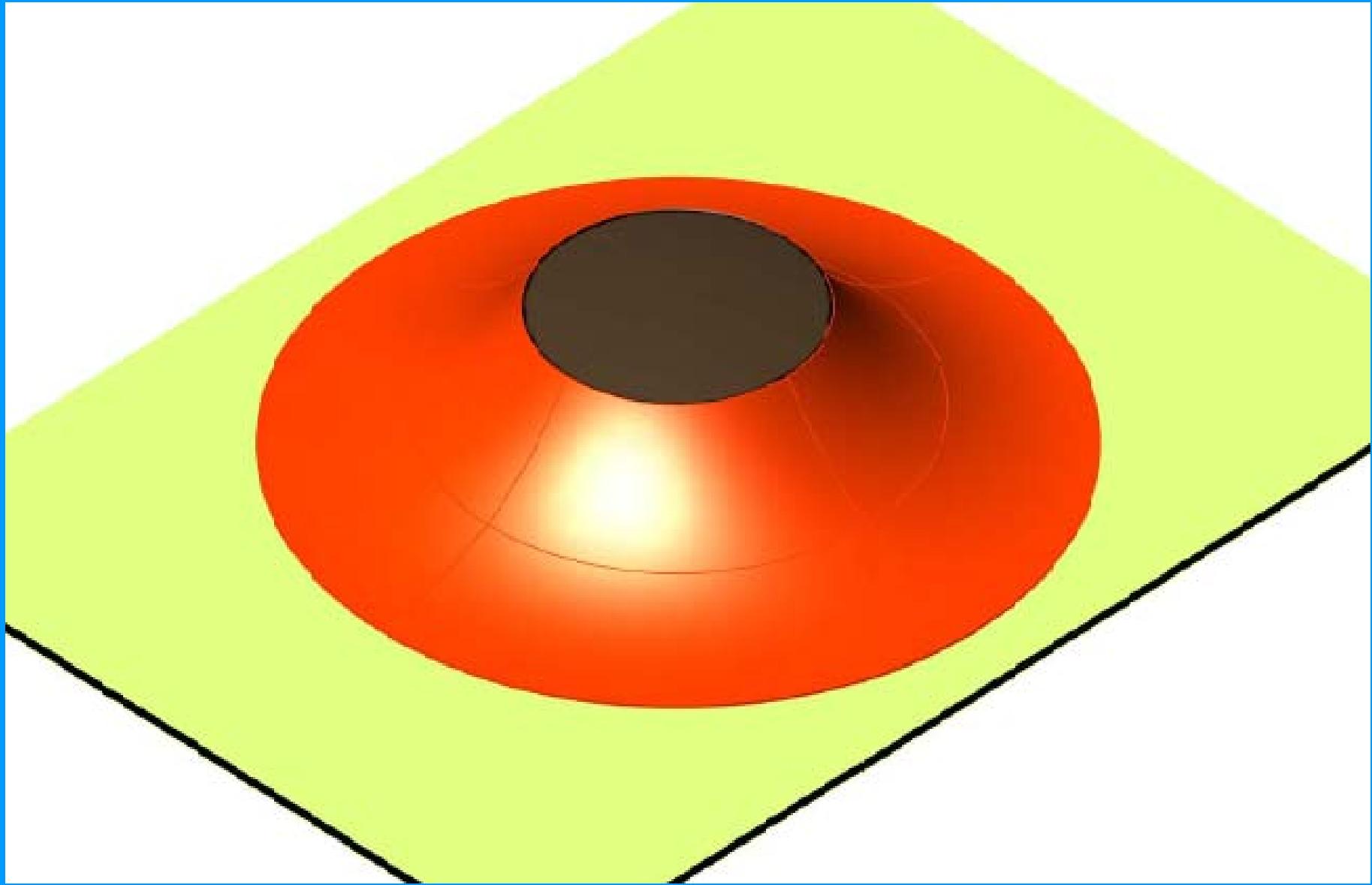




Verificación de la cobertura

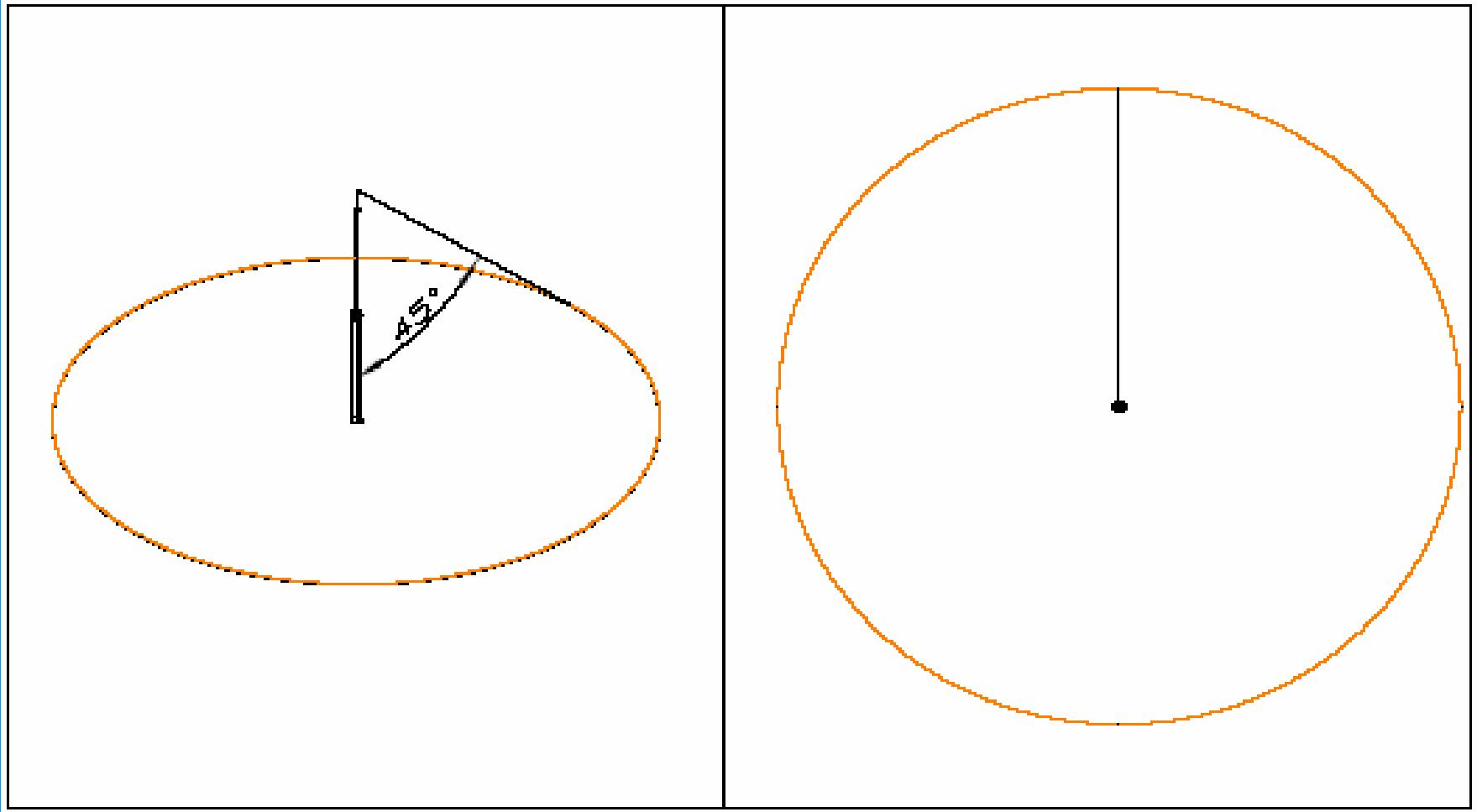


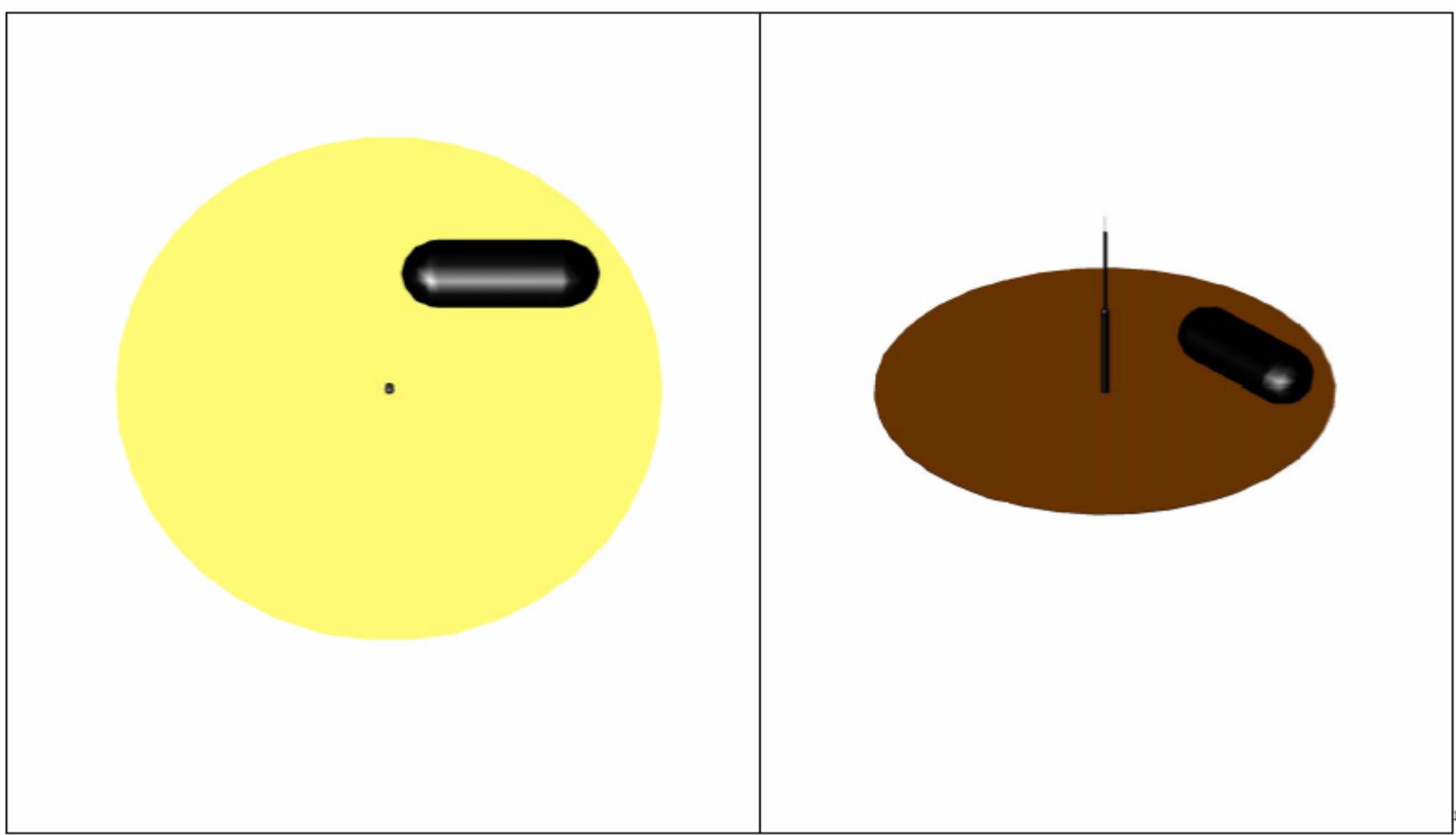


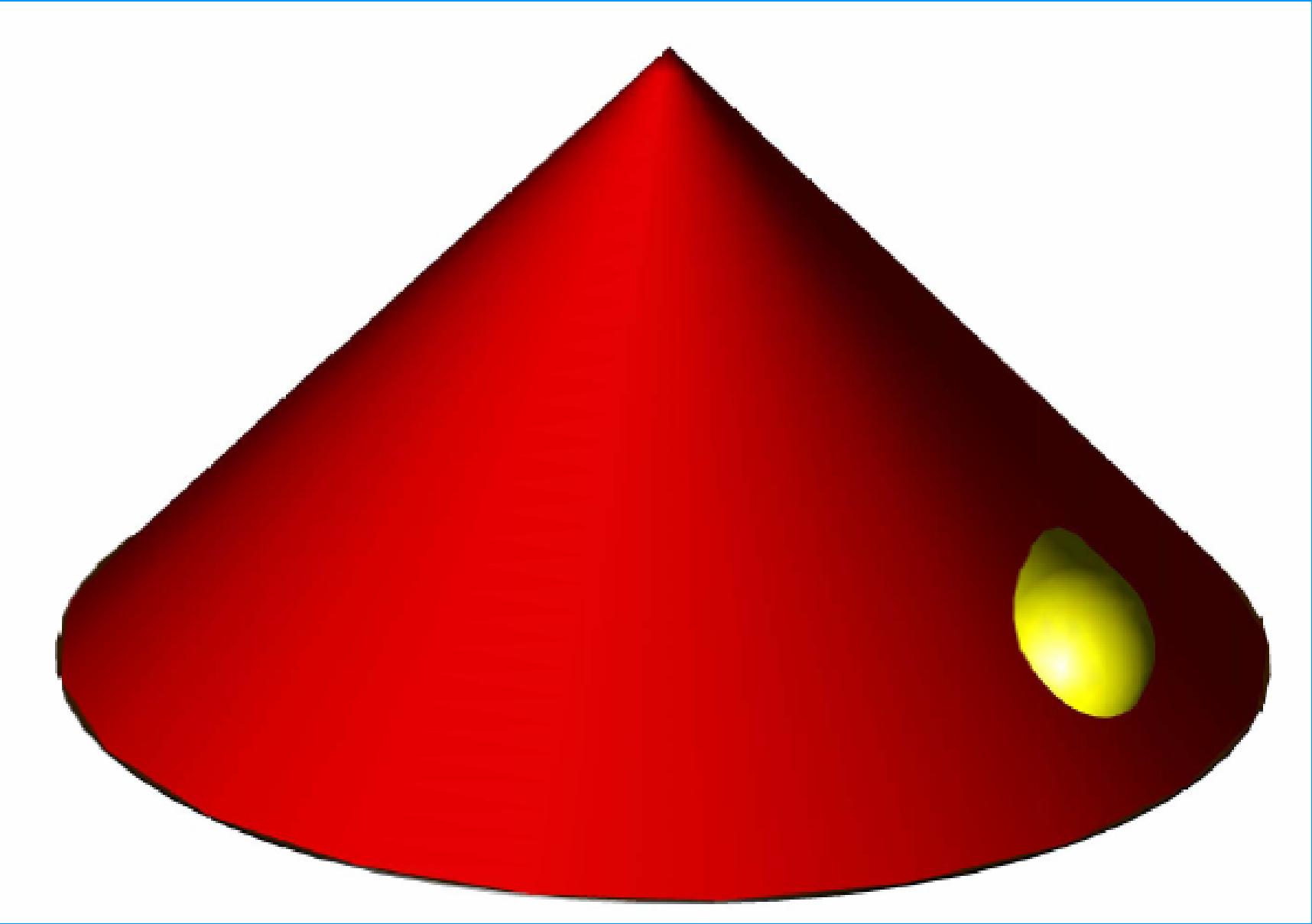


Cono de protección

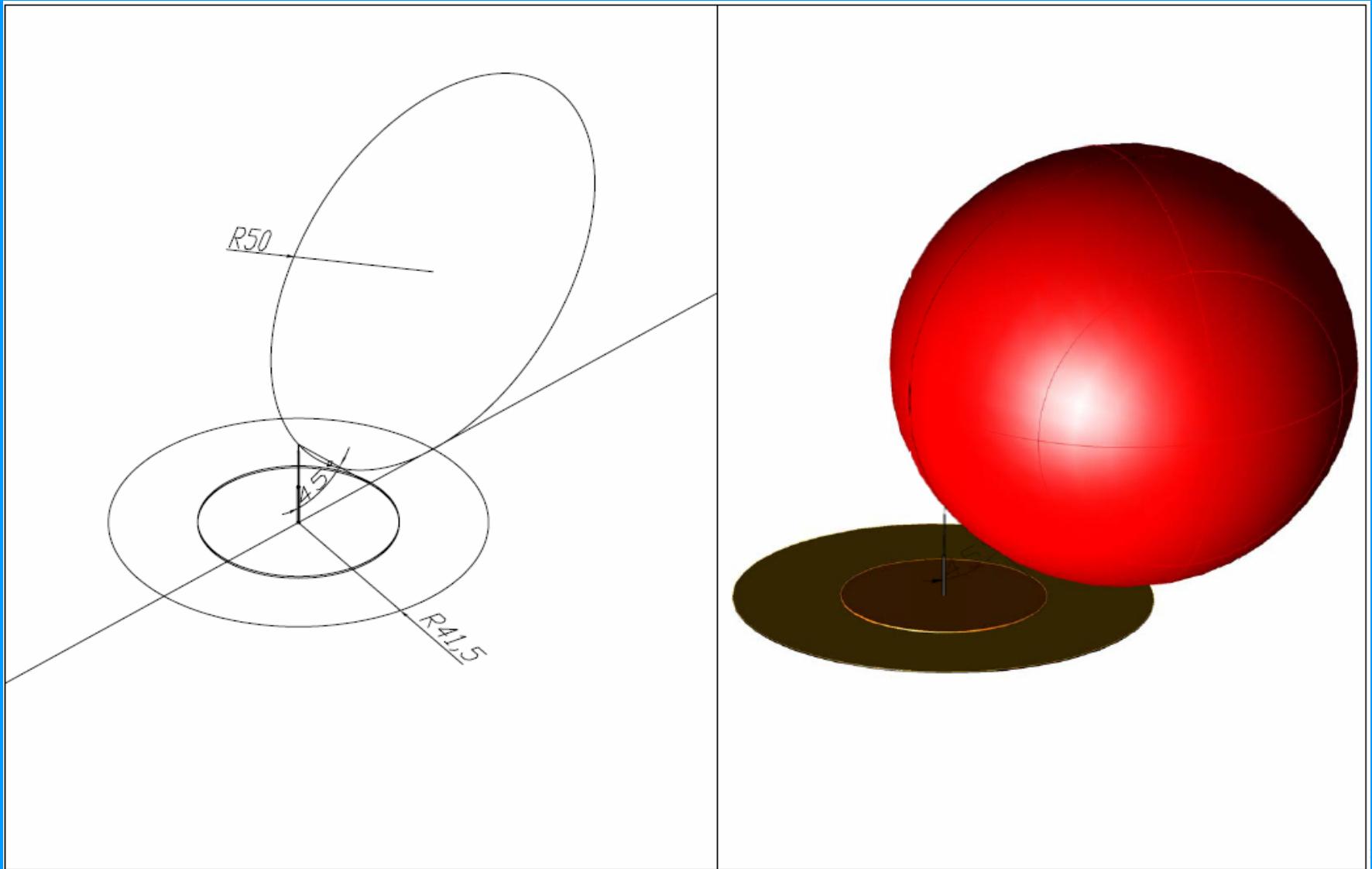
Cono de protección

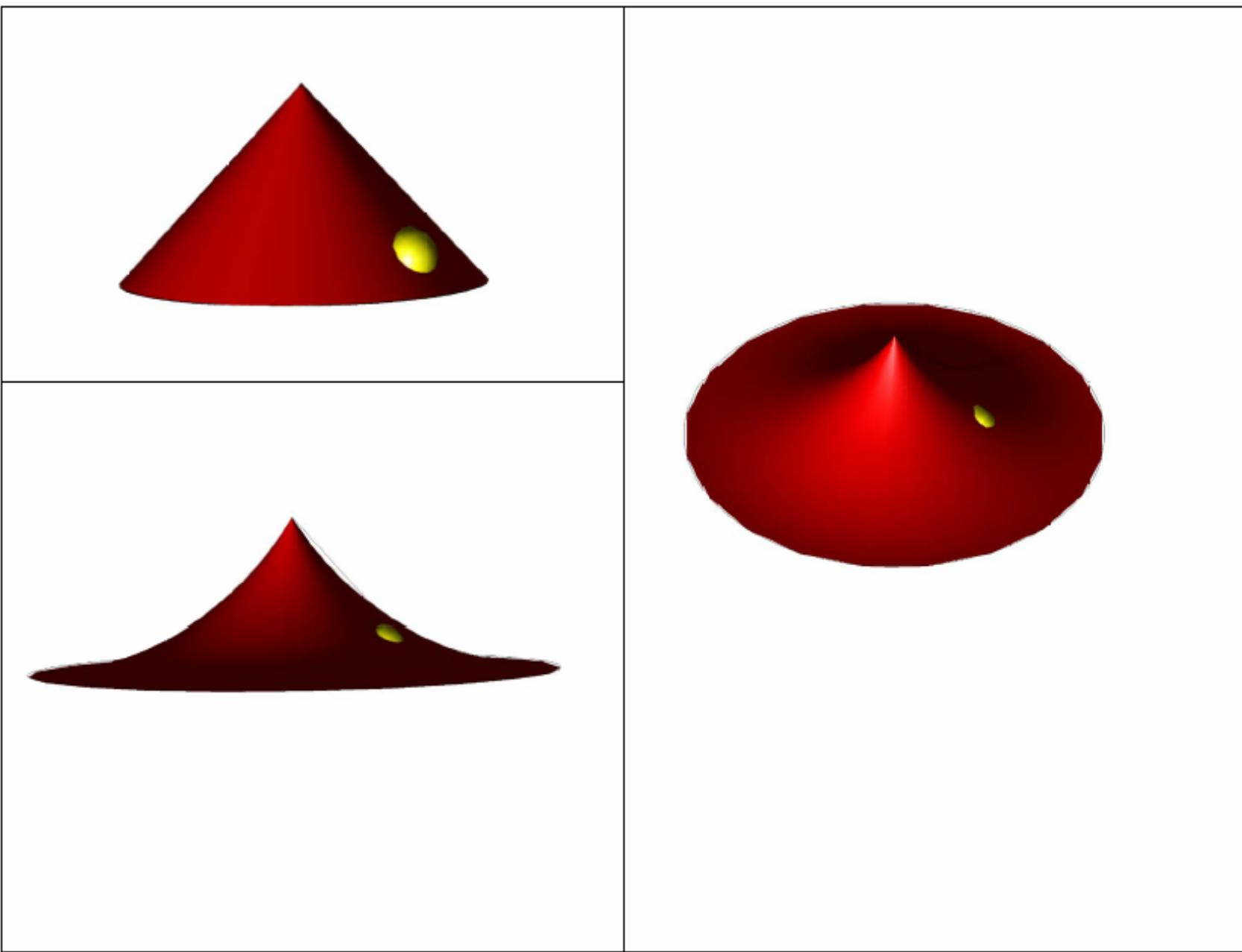




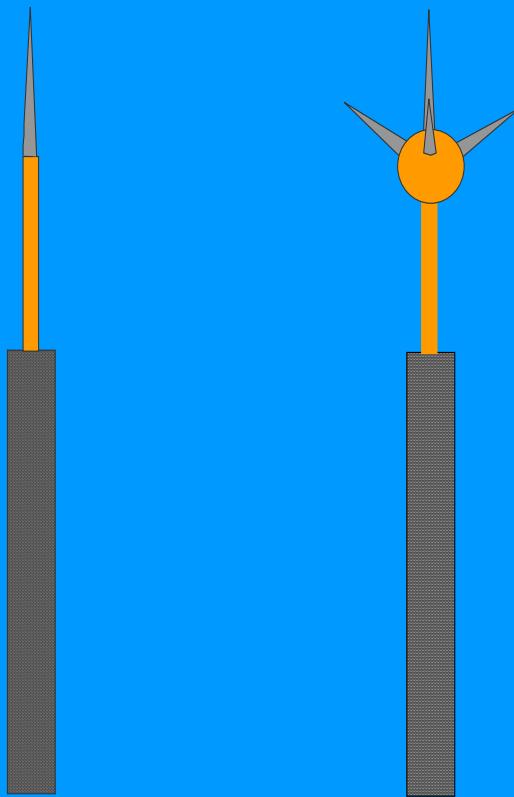


Esfera rodante (teoría electrogeométrica)

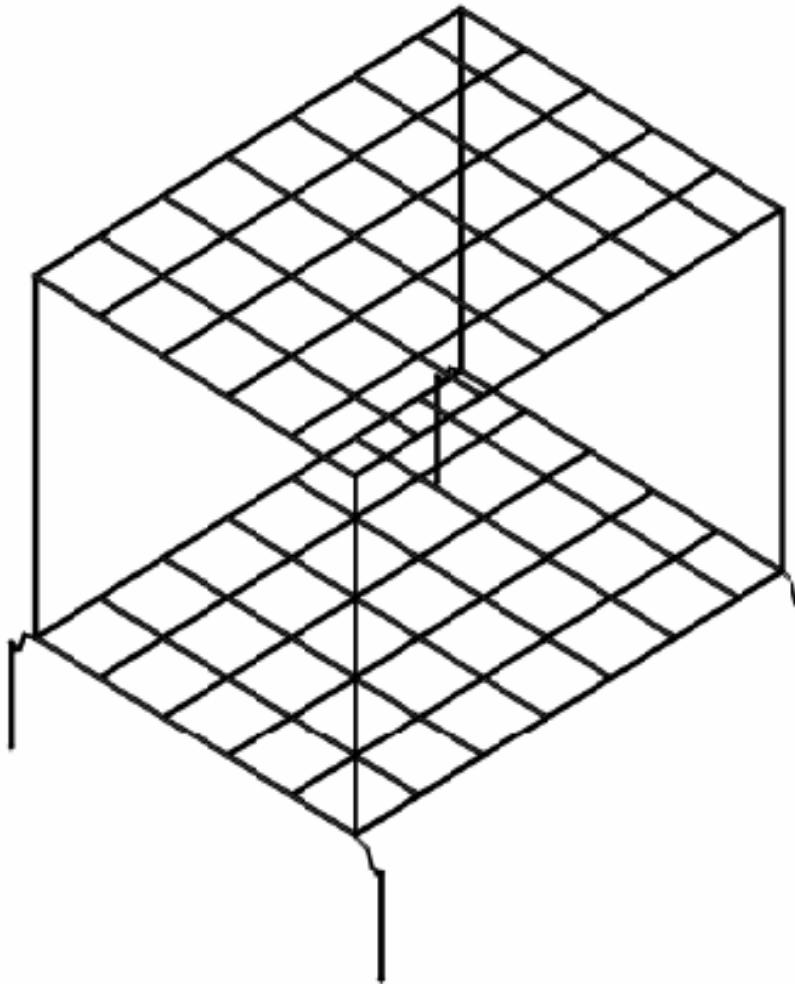




Franklin Normal

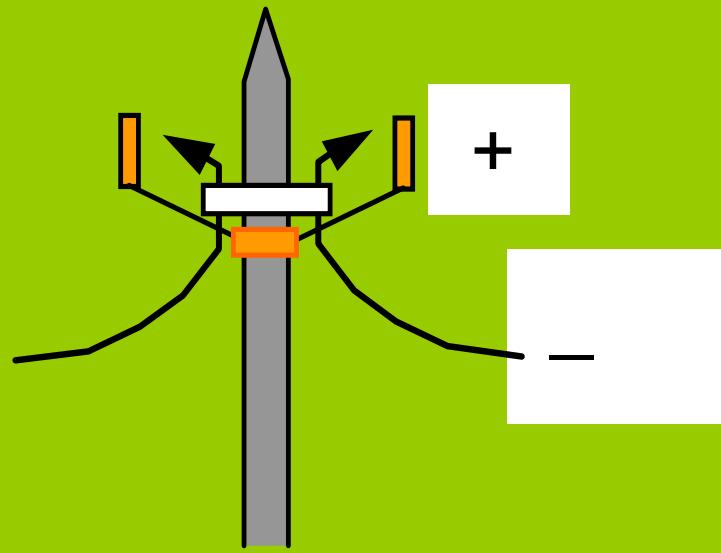


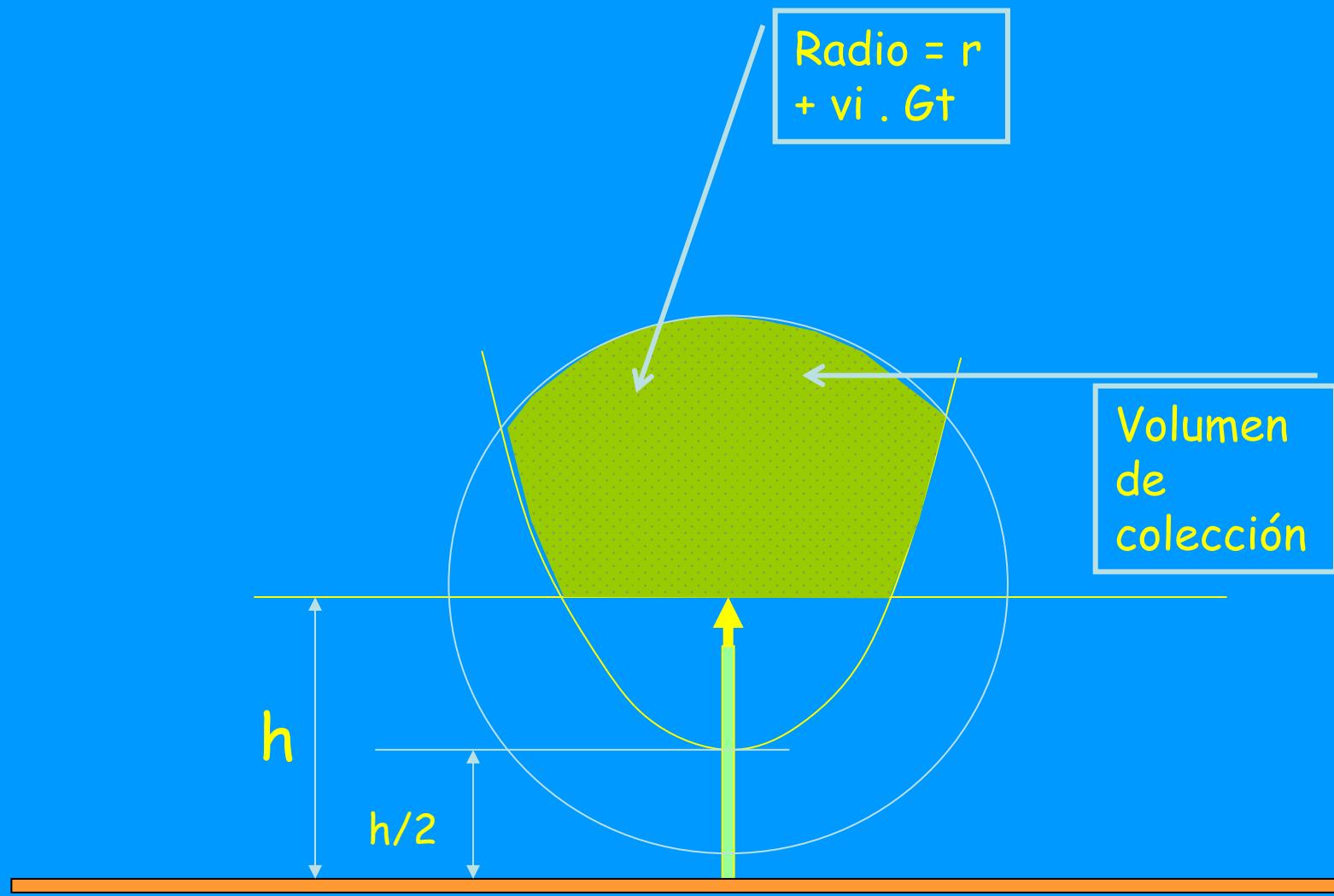
Jaula de Faraday



Norma NFC - 17 102

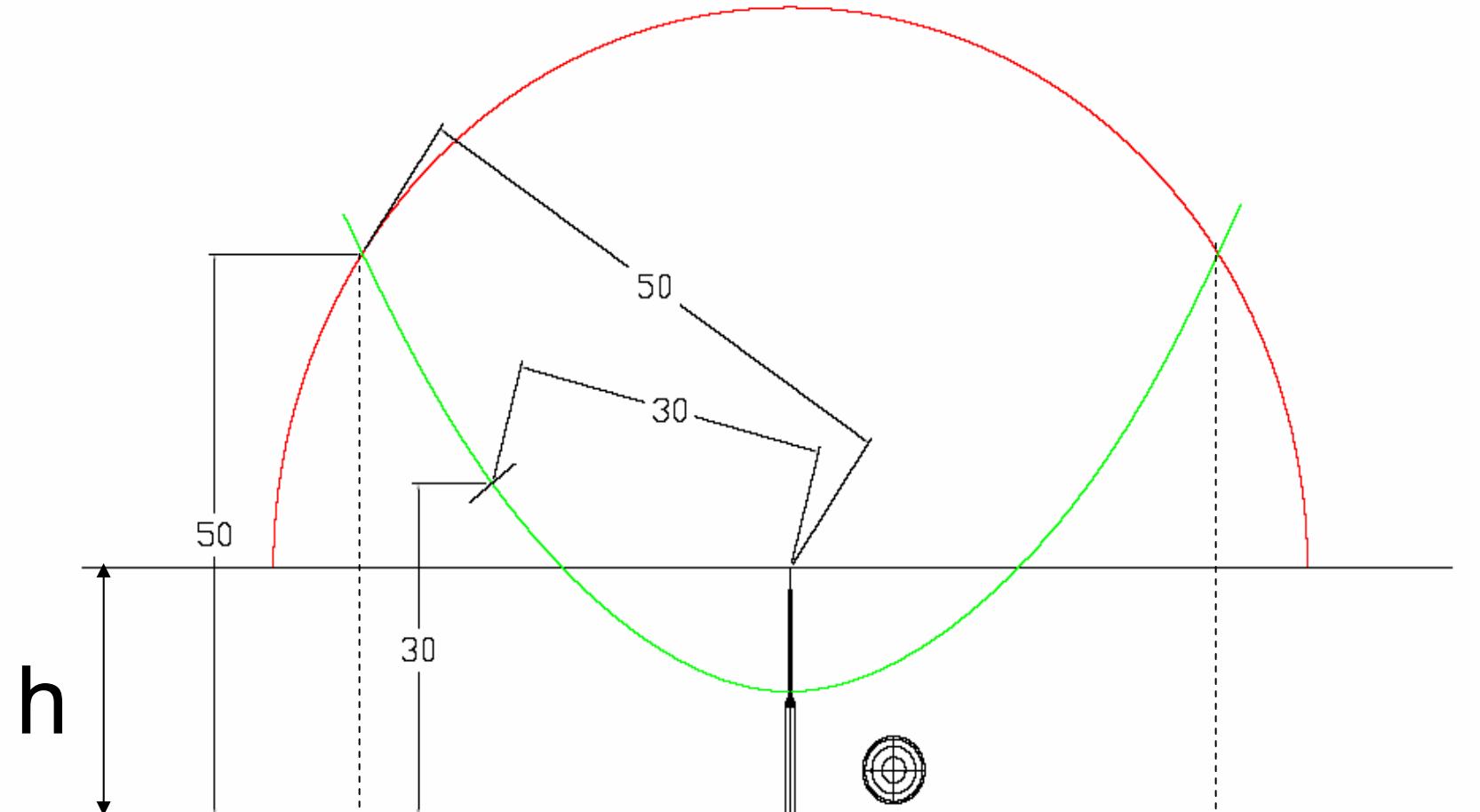
Cebado (E.S.E.)

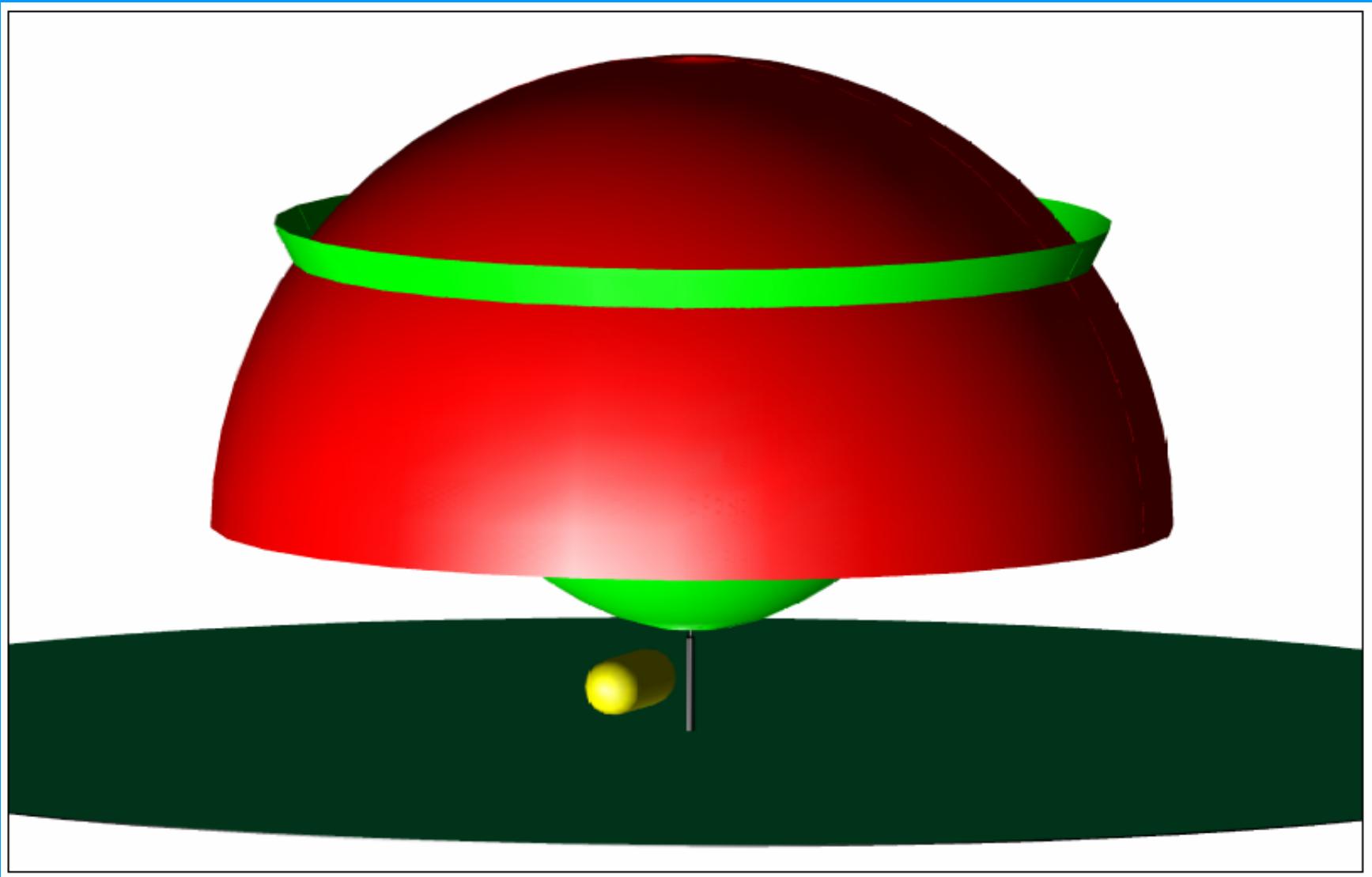




Teoría electrogemétrica modificada

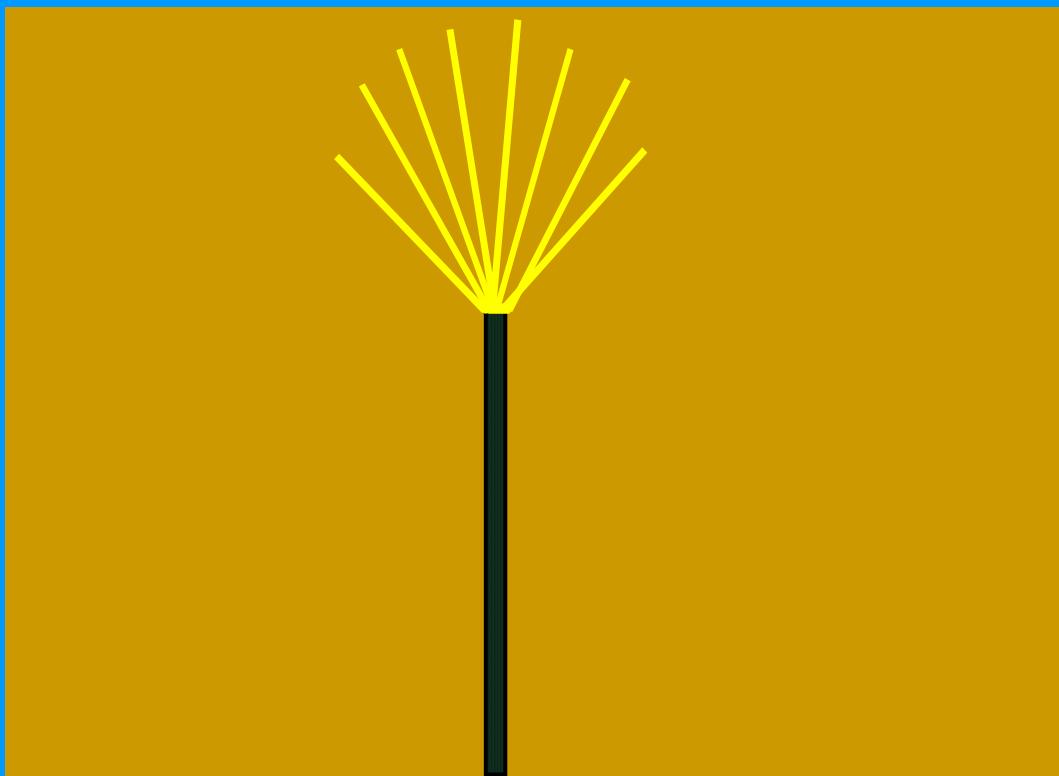
Volumen de colección





Sin normas

D.A.S



Tendencias y resultados de la investigación.

Congresos internacionales.

- ICLP (Europa y Asia) Años pares
- SIPDA (Brasil) Años impares

Posición oficial de ambos grupos

- **El sistema convencional sigue siendo el mas aceptable y requiere investigación mas profunda.**
- **Los pararrayos con sistema de cebado y los sistemas de transferencia de cargas no tiene fundamento científico**

En la última década del siglo XX se realizaron grandes esfuerzo.

- Se trató de demostrar el funcionamiento de los pararrayos de gran radio.
- Se trató de demostrar el sistema de eliminación de rayos o de trasnferencia de cargas.

En ambos casos los experiencias de laboratorio y ensayos en campo fueron desalentadores.

Reseña del trabajo de dos centros de investigación que fueron los responsables la tarea experimental.

Langmuir Laboratory Bald Peak El Socorro. Nueva Mexico





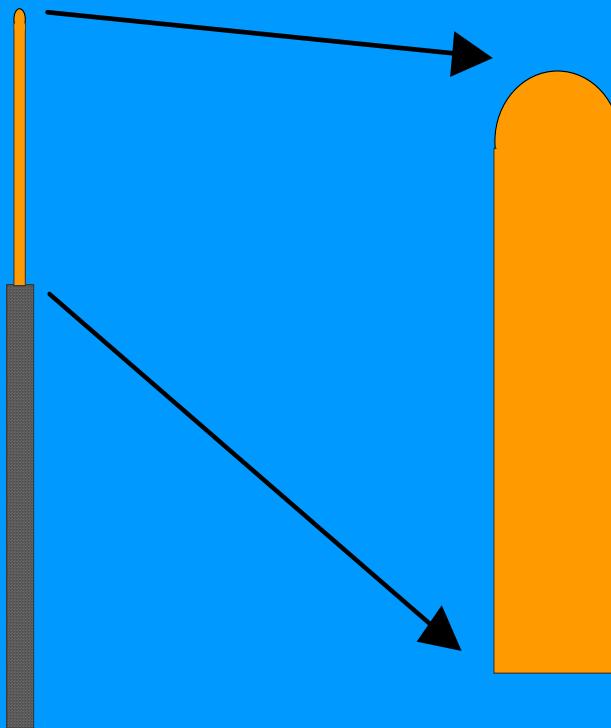




Punta experimental de aluminio
impactada por un rayo. Foto enviada por el Prof.
Charlie Moore



Punta Propuesta por el Prof. Charlie Moore al Comité NFPA 780



Charge Transfer System is Wishful Thinking, Not Science

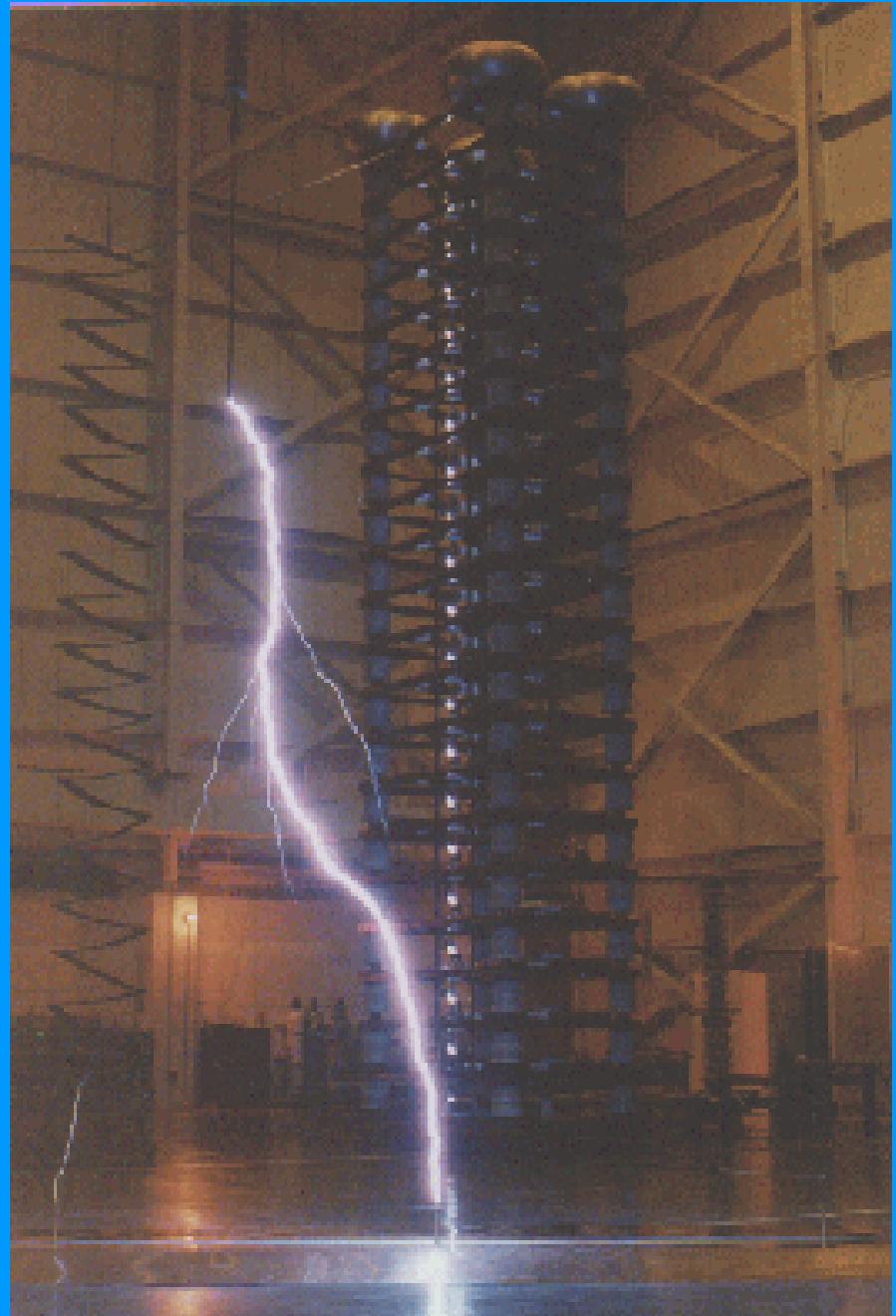
**Charles B. Moore
Professor Emeritus
Atmospheric Physics**

**New Mexico Institute of Mining and Technology, Socorro,
NM 87801
Langmuir Laboratory for Atmospheric Research**

- Universidad Estatal de Mississippi.
Laboratorio de Alta Tensión

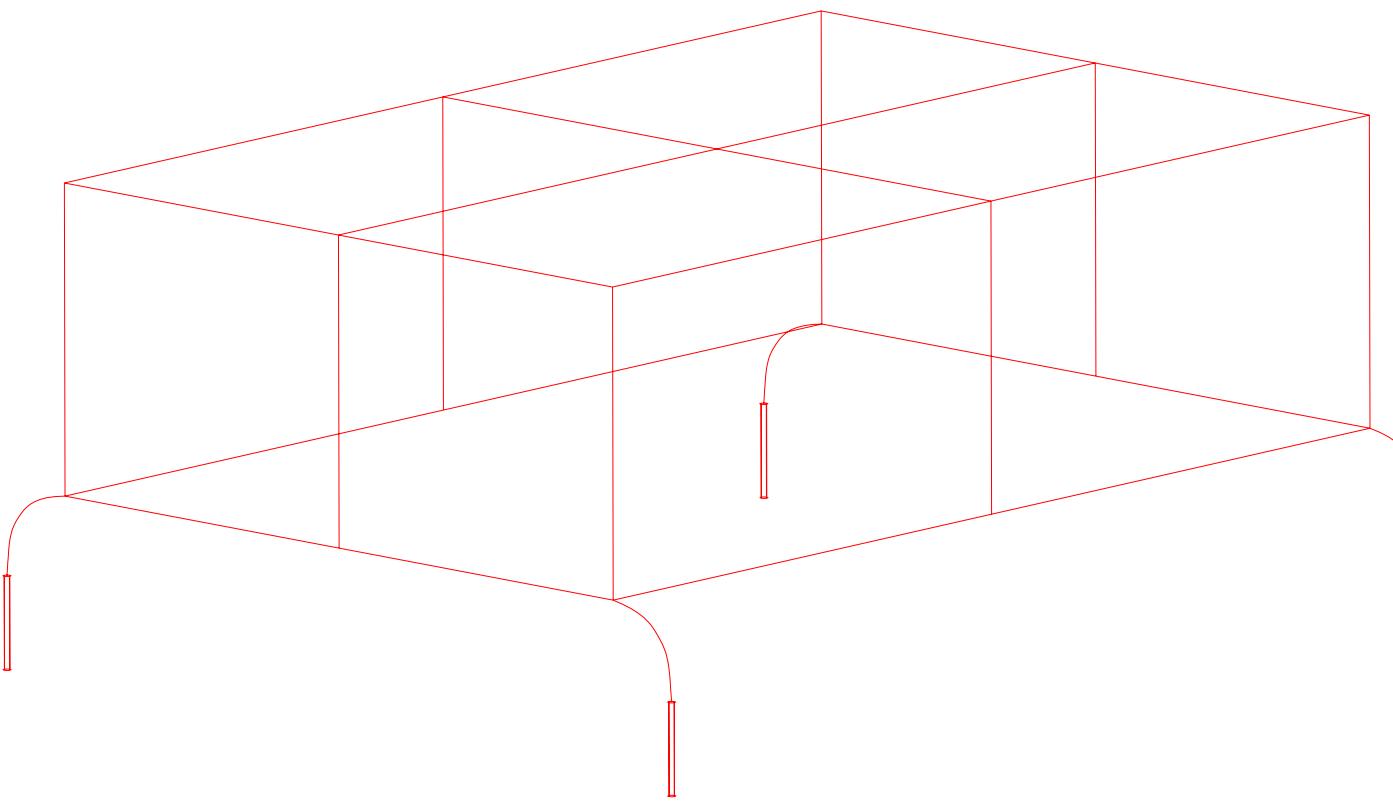
Stanislaw Grzybowski, Dr. Hab., Ph.D., FIEEE





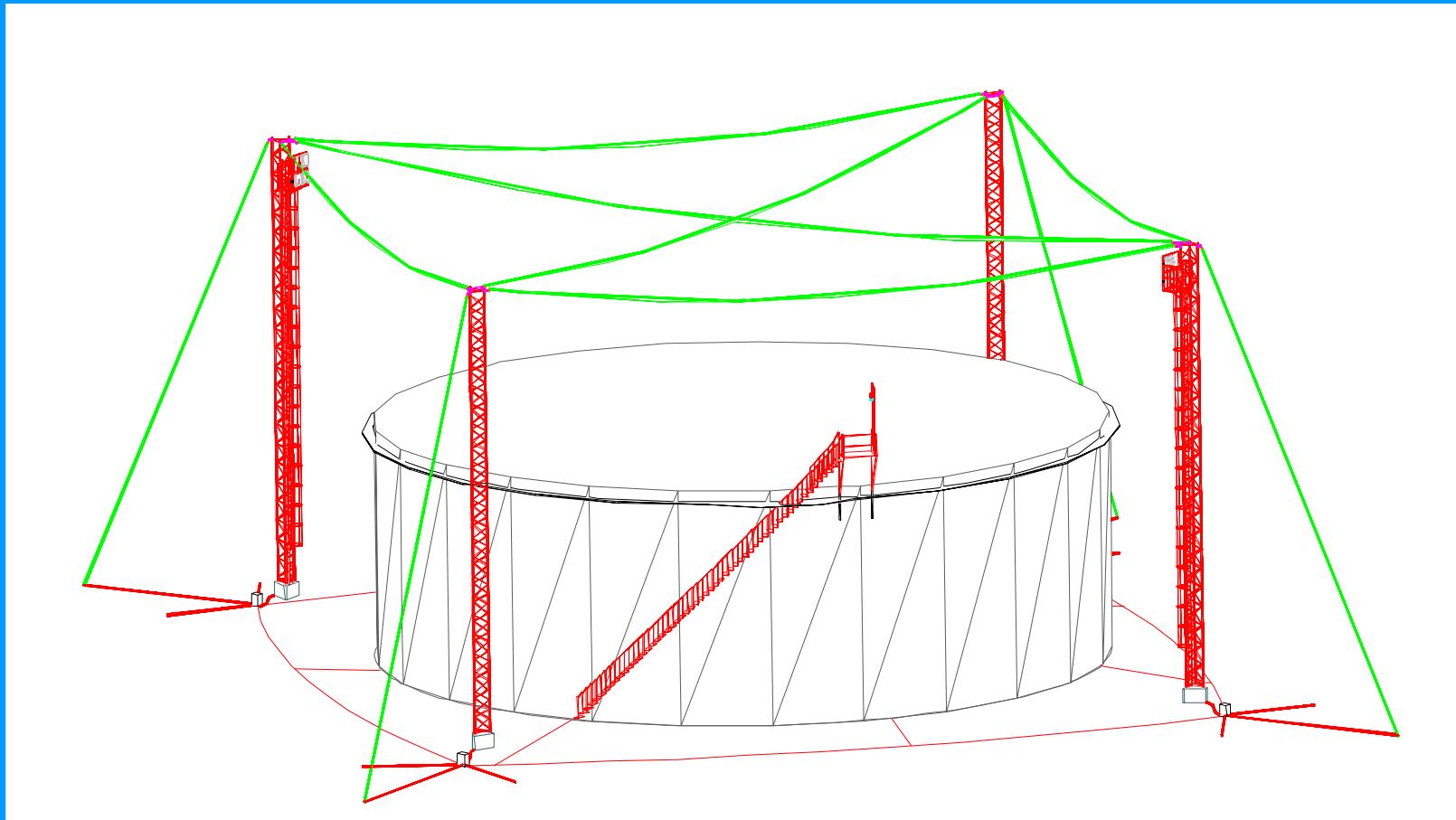
Métodos de Protección (Teoría electrogeométrica)

Jaula de Faraday



Métodos de Protección (Teoría electrogeométrica)

Jaula de Faraday



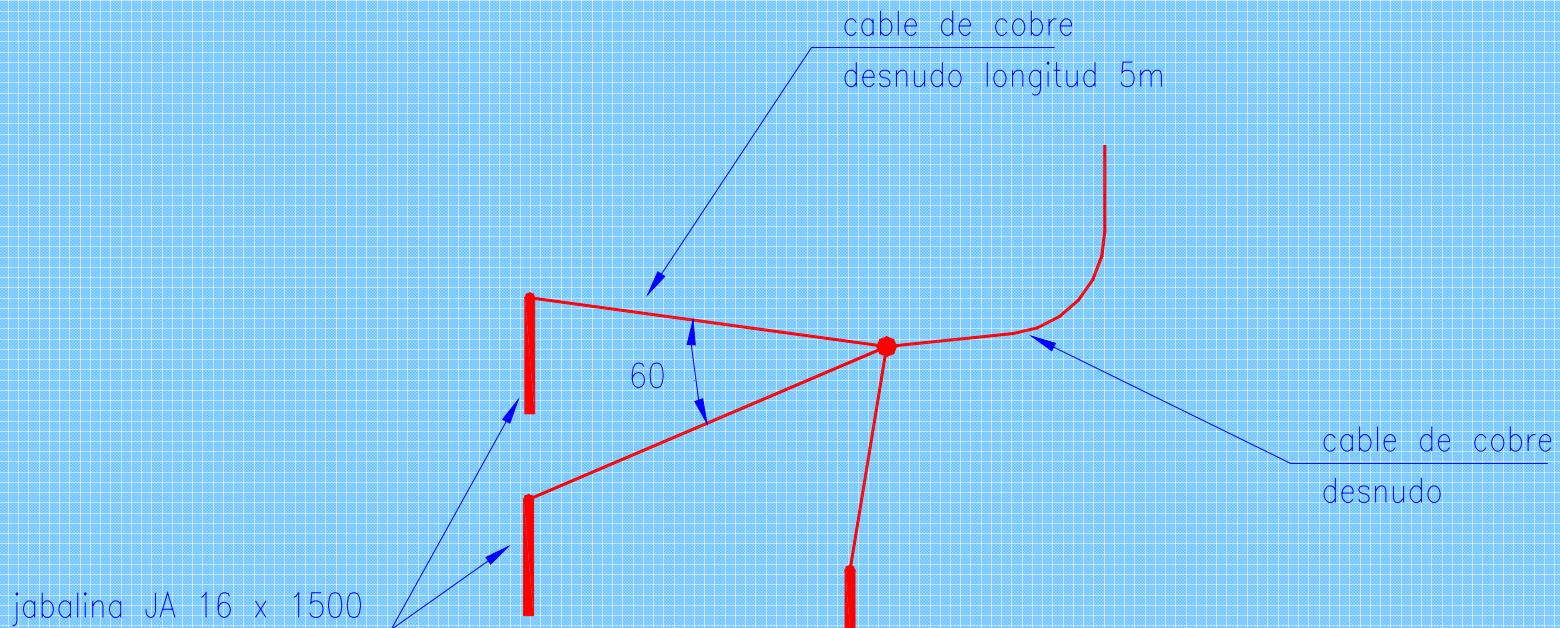
Puesta a Tierra de un pararrayos

Como interconectar jabalinas

- Requiere una geometría tal que asegure baja impedancia (no sólo resistencia)
- Se construye con dispersores radiales y caminos de bajada lo más cortos y rectos posibles

Puesta a Tierra de un pararrayos

Como interconectar jabalinas



Puesta a Tierra de un pararrayos

Como interconectar jabalinas



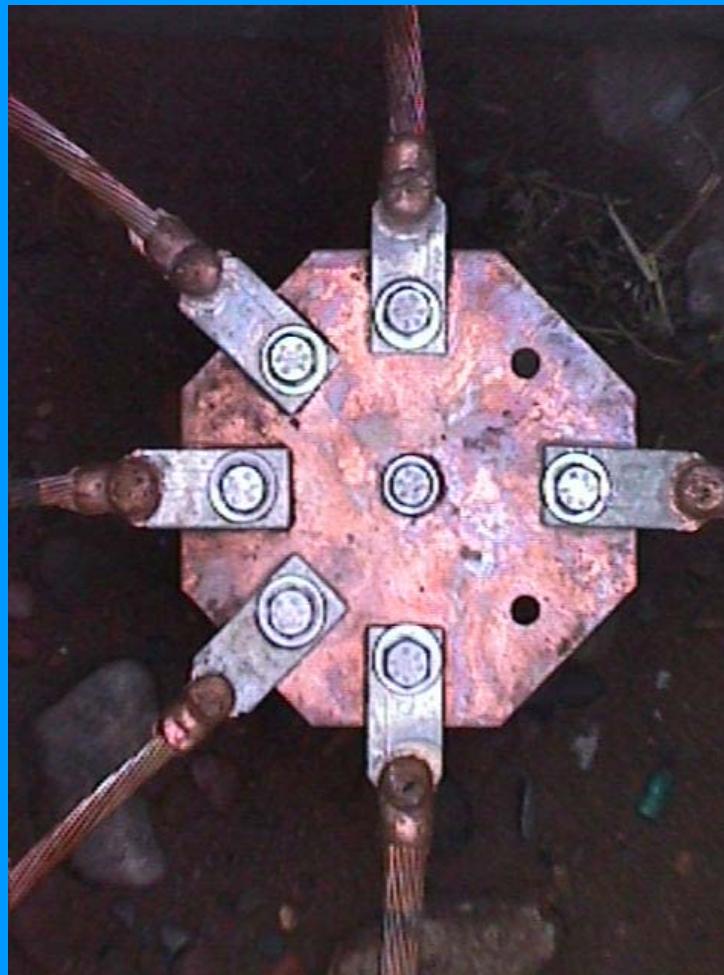
Puesta a Tierra de un pararrayos

Como interconectar jabalinas



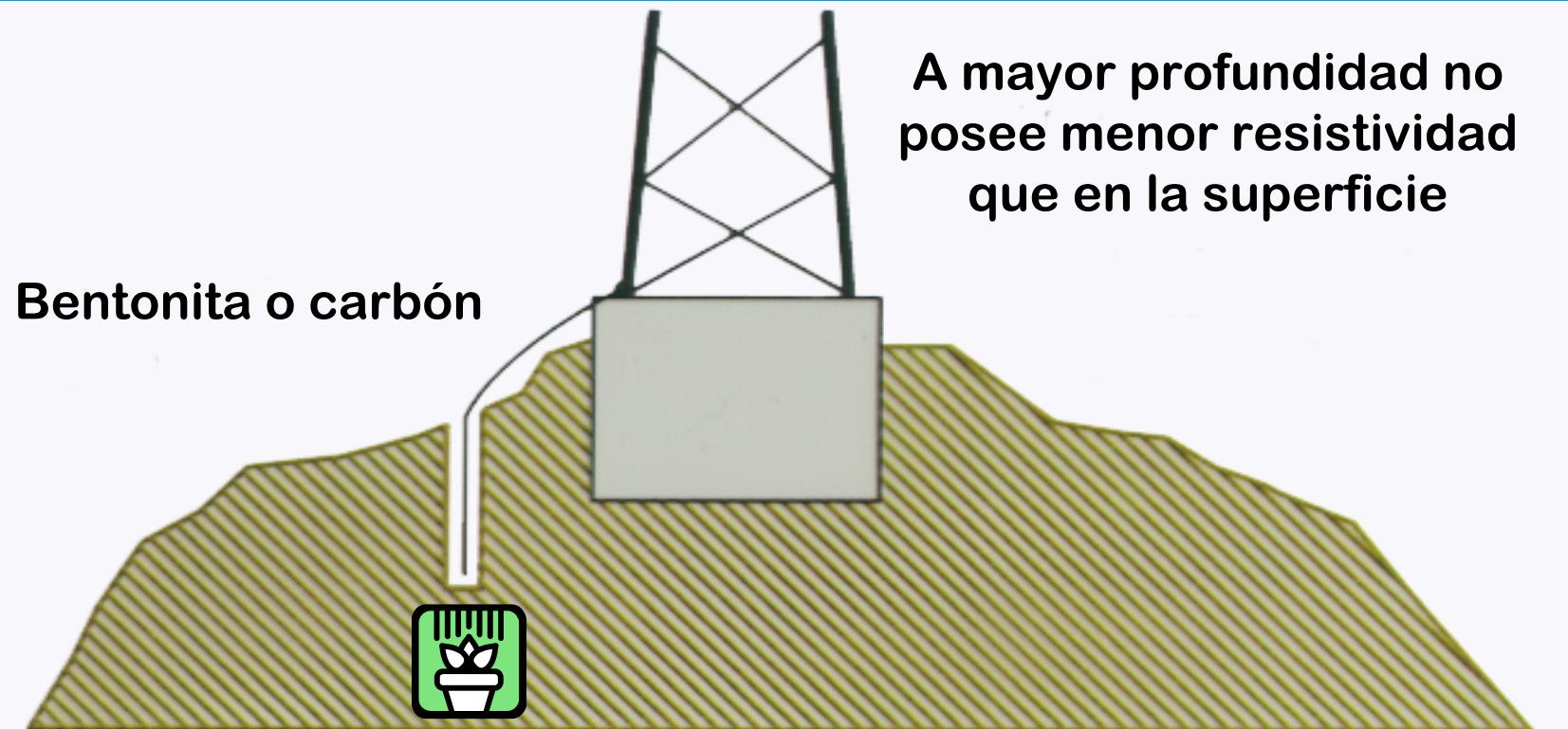
Puesta a Tierra de un pararrayos

Como interconectar jabalinas

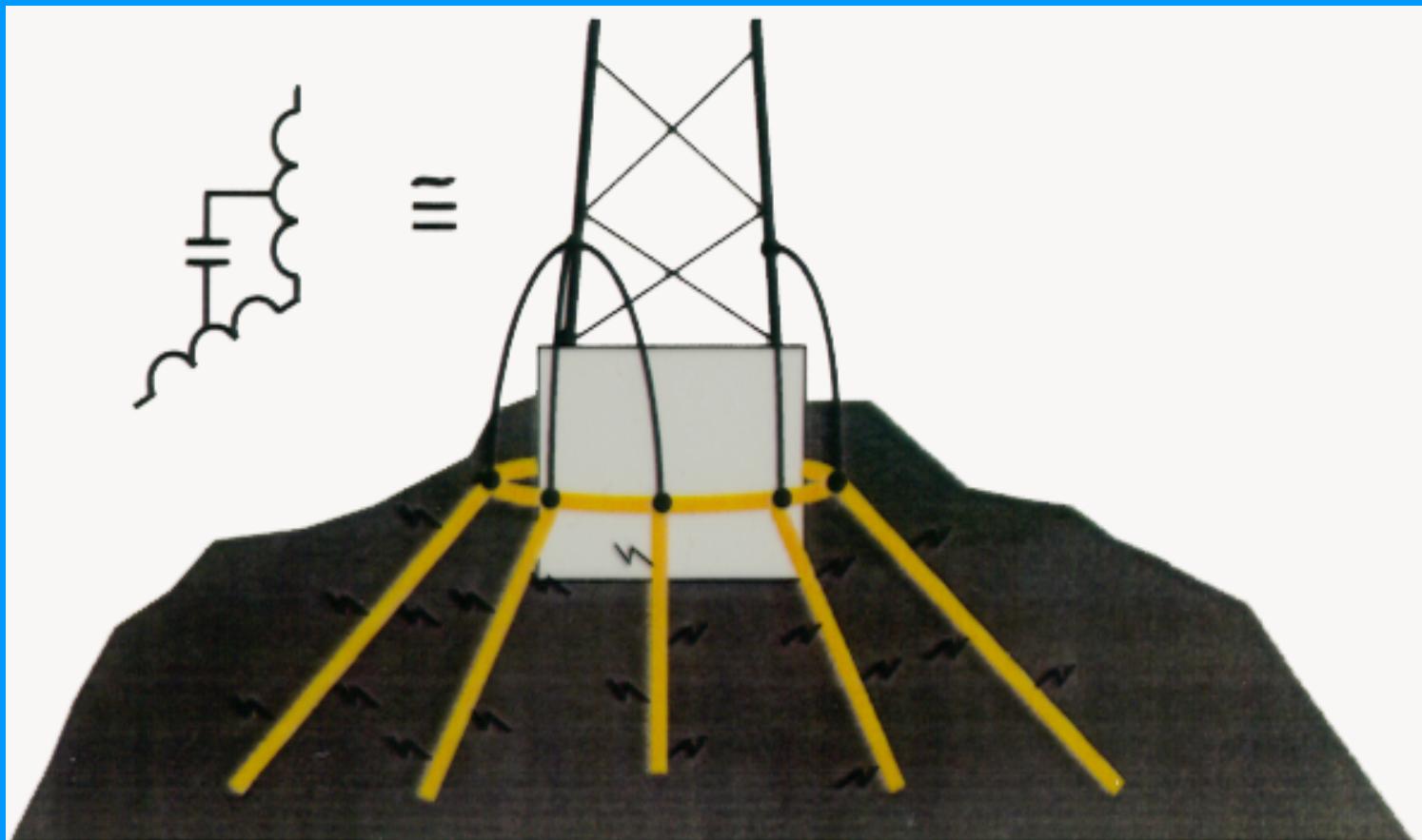


Puesta a Tierra de un pararrayos

Terreno rocoso



Puesta a Tierra de un pararrayos Sin jabalinas



- La norma ANSI / IEEE 80
- La malla de subestación.
- Tensiones de paso y contacto.
- Criterios de dimensionamiento.

IEEE Guide for Safety in AC Substation Grounding

Sponsor

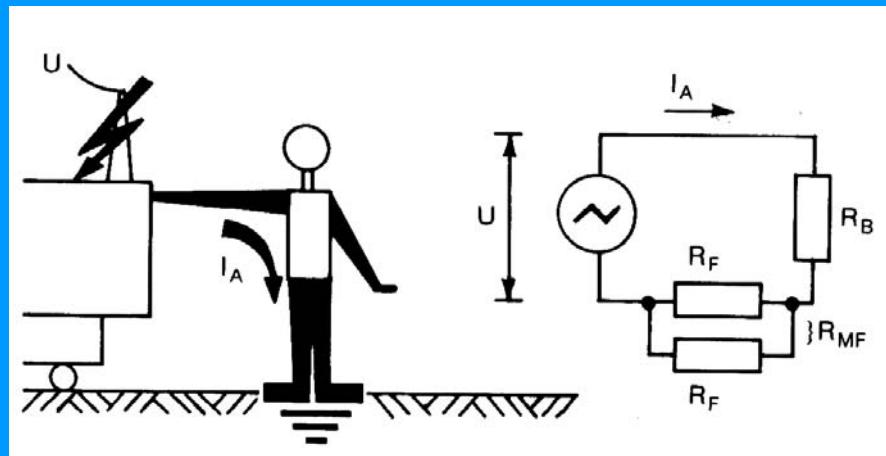
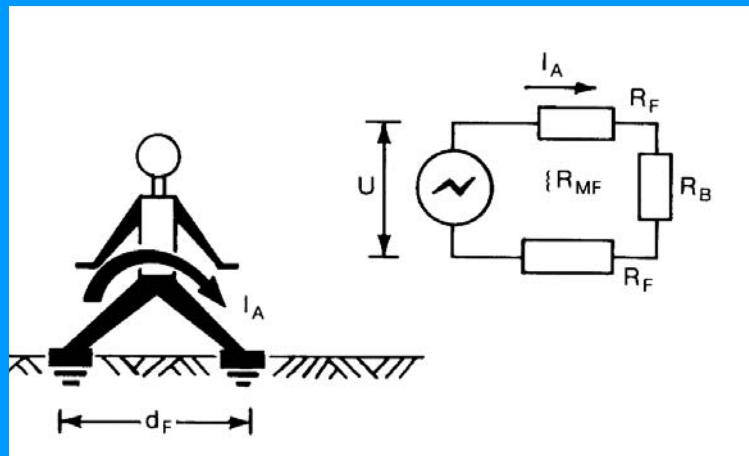
Substations Committee
of the
IEEE Power Engineering Society

Approved 30 January 2000

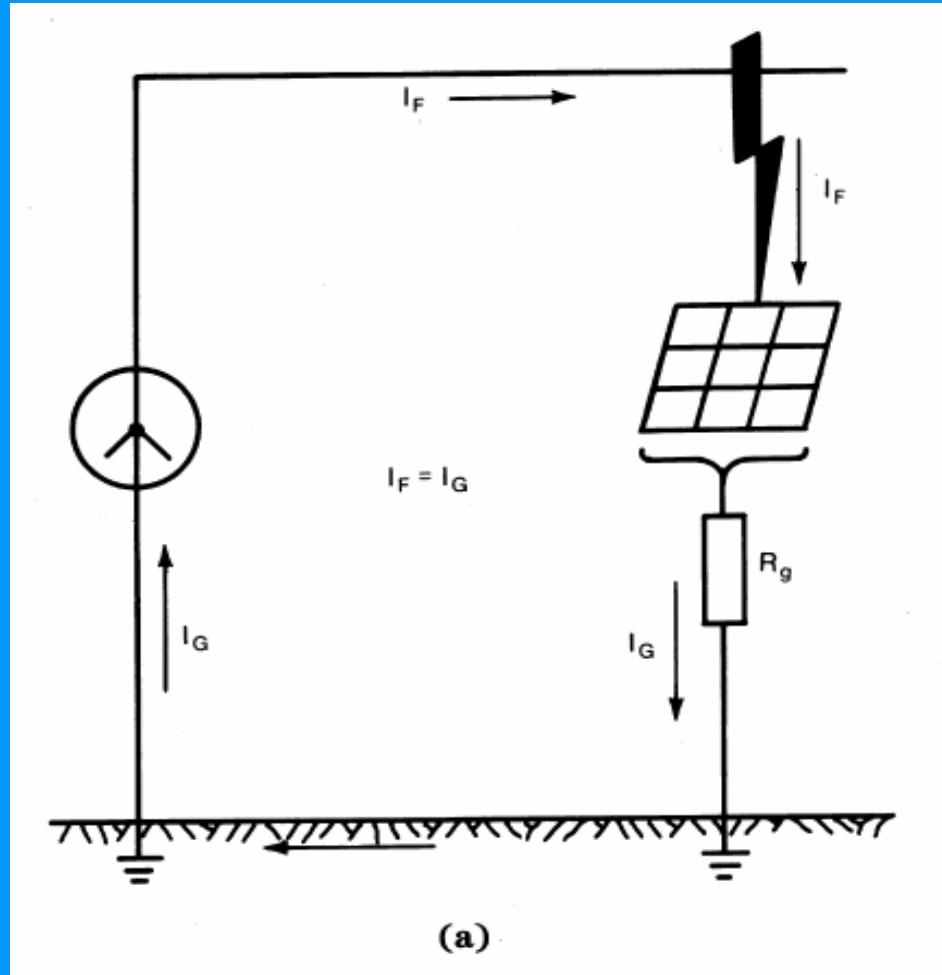
IEEE-SA Standards Board

- **Abstract:**
- Outdoor ac substations, either conventional or gas-insulated, are covered in this guide.
- Distribution, transmission, and generating plant substations are also included.
- With proper caution, the methods described herein are also applicable to indoor portions of such substations, or to substations that are wholly indoors.
- No attempt is made to cover the grounding problems peculiar to dc substations.
- A quantitative analysis of the effects of lightning surges is also beyond the scope of this guide

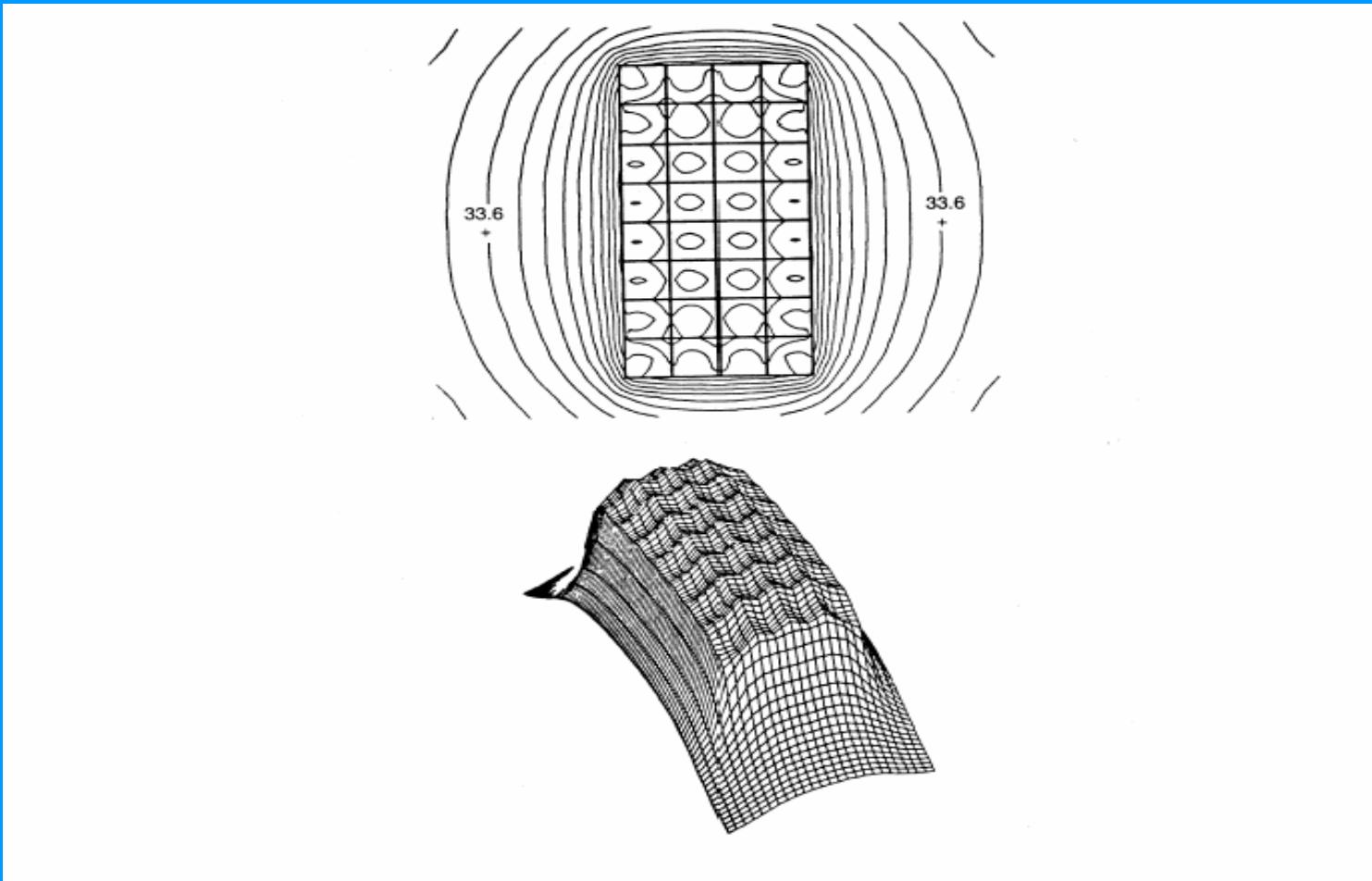
Tensión de paso y de contacto



Falla a tierra.



Potencial del terreno y malla



Tolerancia a corriente.

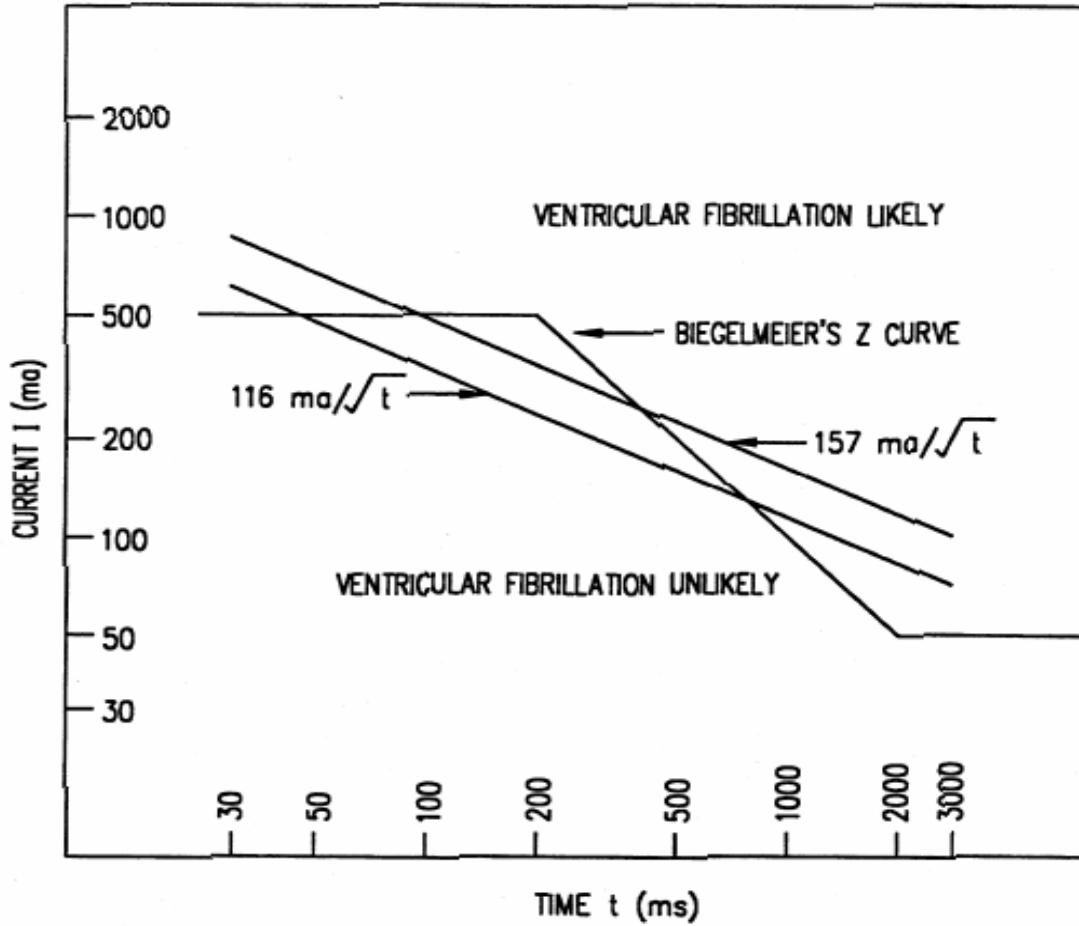


Figure 5—Body current versus time

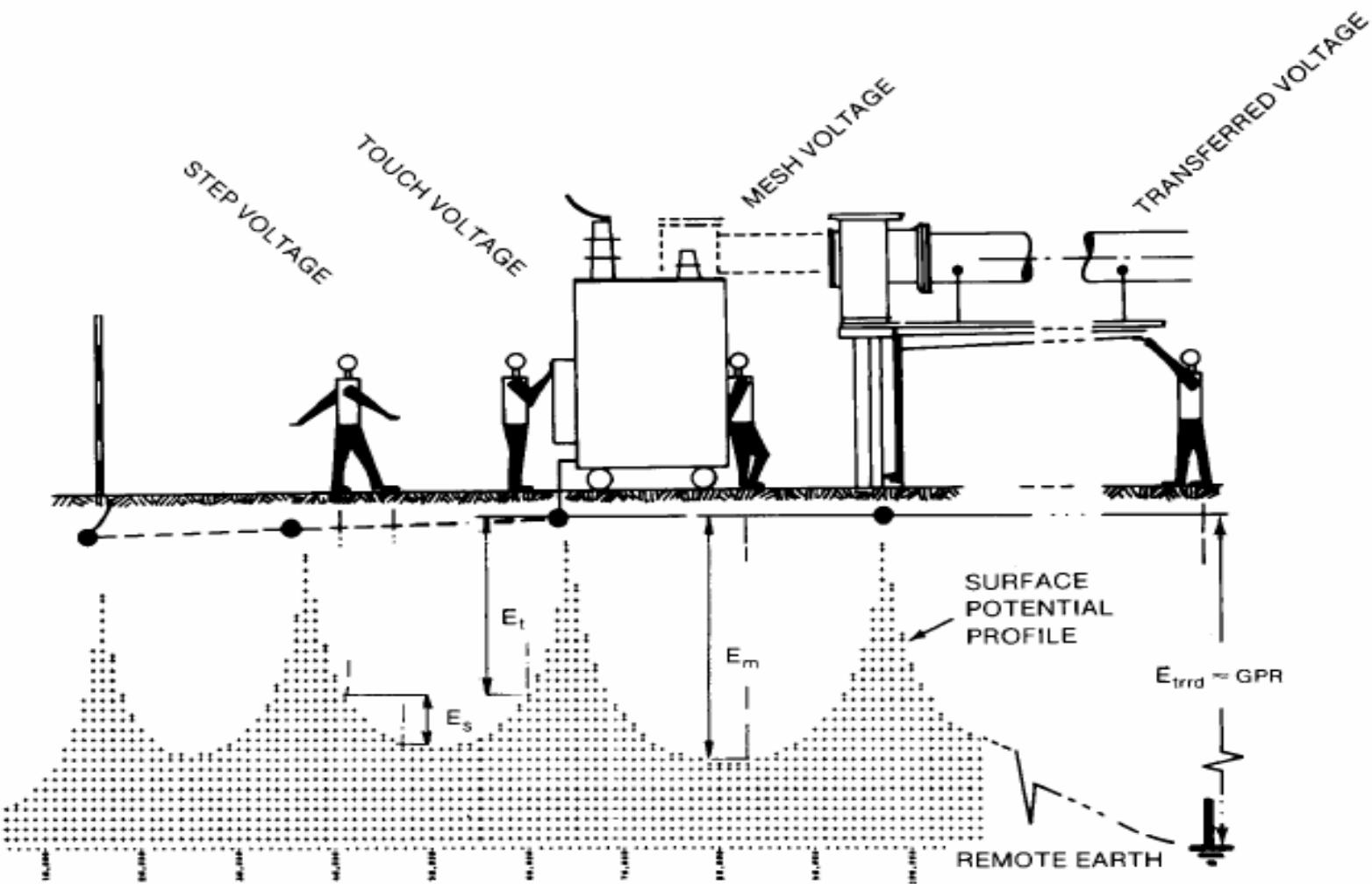


Fig 9
Basic Shock Situations

La tierra en altas corrientes

12.1 Soil as a grounding medium

The behavior of a ground electrode buried in soil can be analyzed by means of the circuit in Figure 17. As shown, most soils behave both as a conductor of resistance, r , and as a dielectric. Except for high-frequency and steep-front waves penetrating a very resistive soil material, the charging current is negligible in comparison to the leakage current, and the earth can be represented by a pure resistance.

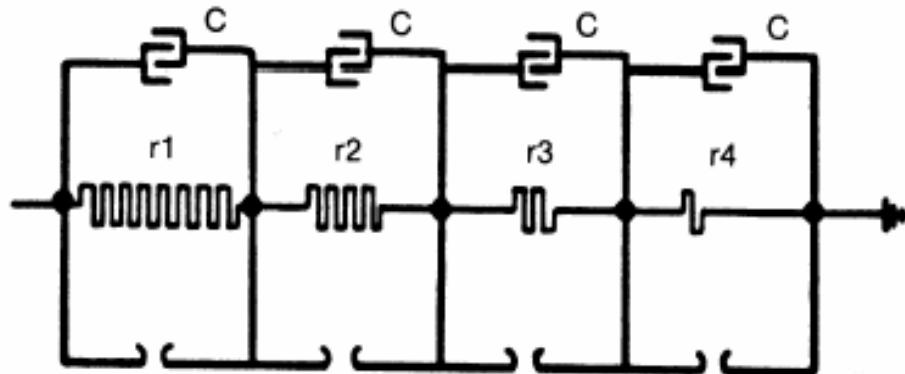


Figure 17—Soil model

Densidad de corriente

- **12.3 Effect of current magnitude**
- Soil resistivity in the vicinity of ground electrodes may be affected by current flowing from the electrodes into the surrounding soil. The thermal characteristics and the moisture content of the soil will determine if a current of a given magnitude and duration will cause significant drying and thus increase the effective soil resistivity. A conservative value of current density, as given by Armstrong [B4], is not to exceed 200 A/m² for 1 s.

Fin de la presentación