



Massachusetts Institute of Technology



MIT Plasma Science & Fusion Center

# SMALLER & SOONER: EXPLOITING NEW TECHNOLOGIES FOR FUSION'S DEVELOPMENT

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**With grateful acknowledgement to MIT colleagues and students**

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C. Haakonsen, H.S. Barnard

***SOFE 2015***

***June 2015***

# It is self-evident that smaller, modular fusion devices will accelerate fusion's development

	Shippingport: 1954 "Pilot" Fission Plant	ITER
<i><math>P_{thermal}</math> (MW)</i>	230	500
<i>Core volume (m<sup>3</sup>)</i>	60	~1000
<i>Cost (2012 US B\$)</i>	0.6	~ 20
<i>Cost / volume (M\$/m<sup>3</sup>)</i>	10	~ 20
<i>Construction time (y)</i>	~ 4	> 20

- Cost & time  $\propto$  unit volume and mass

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- Cost & time  $\propto$  unit volume and mass
- ITER is an invaluable science experiment for burning plasmas but is not an optimized size for modular fusion energy "pilots"
  - ITER is a trial of just one fusion concept, fission pilot tried four different cores!
- **Small size and modularity are self-reinforcing:** pilots of complex engineered systems as small as possible, yet sufficiently capable

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$P_{thermal}$ (MW)	230	500
Core volume ( $m^3$ )	60	~1000

Sounds like a reasonable strategy but how do you do it?

- Cost & t
- ITER is an invaluable science experiment for burning plasmas but is not an optimized size for modular fusion energy "pilots"
  - ITER is a trial of just one fusion concept, fission pilot tried four different cores!
- Small size and modularity are self-reinforcing, make pilots of complex engineered systems as small as possible, yet sufficiently capable

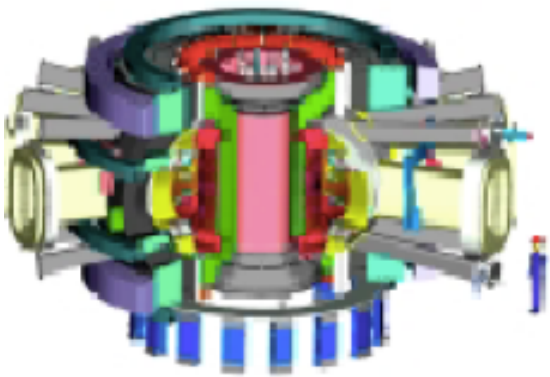
# Confinement physics strongly favors **high B** to produce fusion capable devices at smaller size

**Gain**  $nT \tau_E \sim \frac{\beta_N H}{q_*^2} R^{1.3} B^3$

$V \propto R^3$

$\frac{P_{fusion}}{S_{wall}} \sim \frac{\beta_N^2 \epsilon^2}{q_*^2} R B^4$  **Power density**

Copper coil pulse ~ 10 s



**FIRE**

R (m)	2.14
V (m <sup>3</sup> )	30
B <sub>o</sub> (T)	10
Q <sub>p</sub>	>10
Steady-state	No
Tritium breeding	No
Q <sub>electric</sub>	0

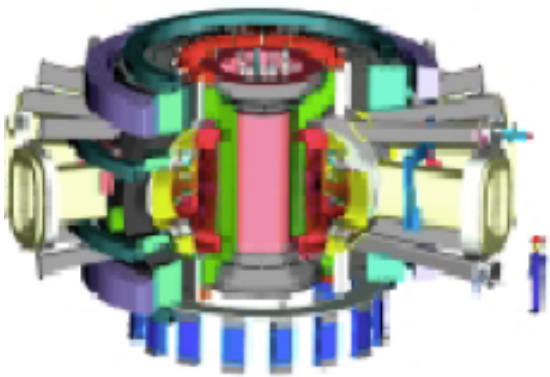
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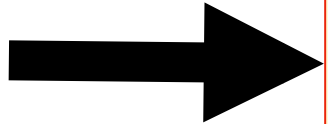
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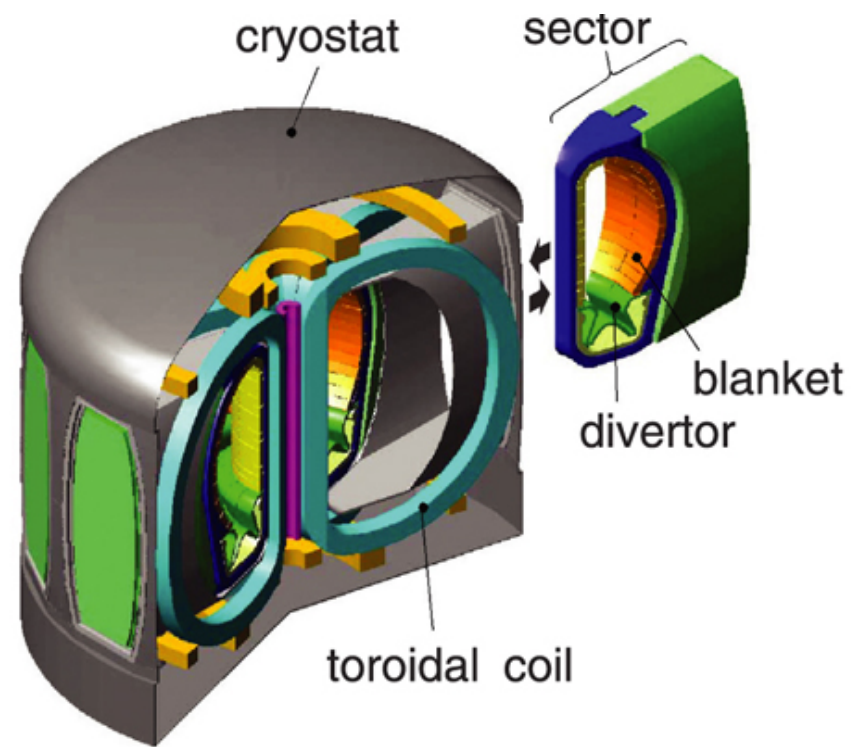
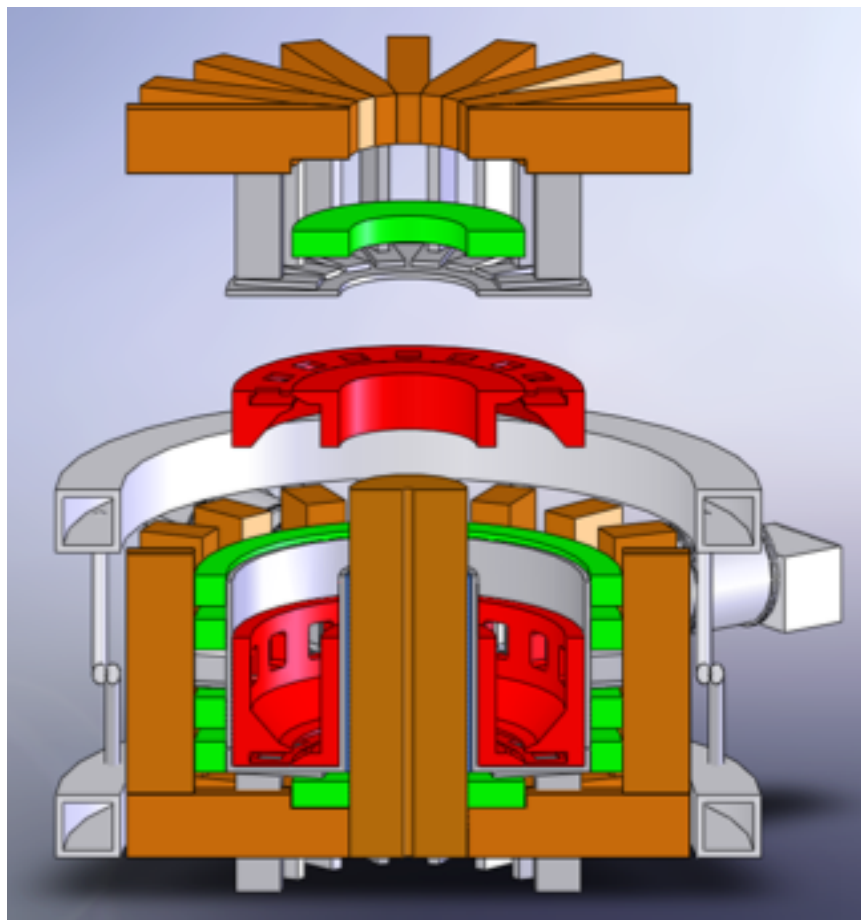
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Continuous /w High-B Superconductors?

# Basic geometry favors demountable magnets to provide modularity for internal components

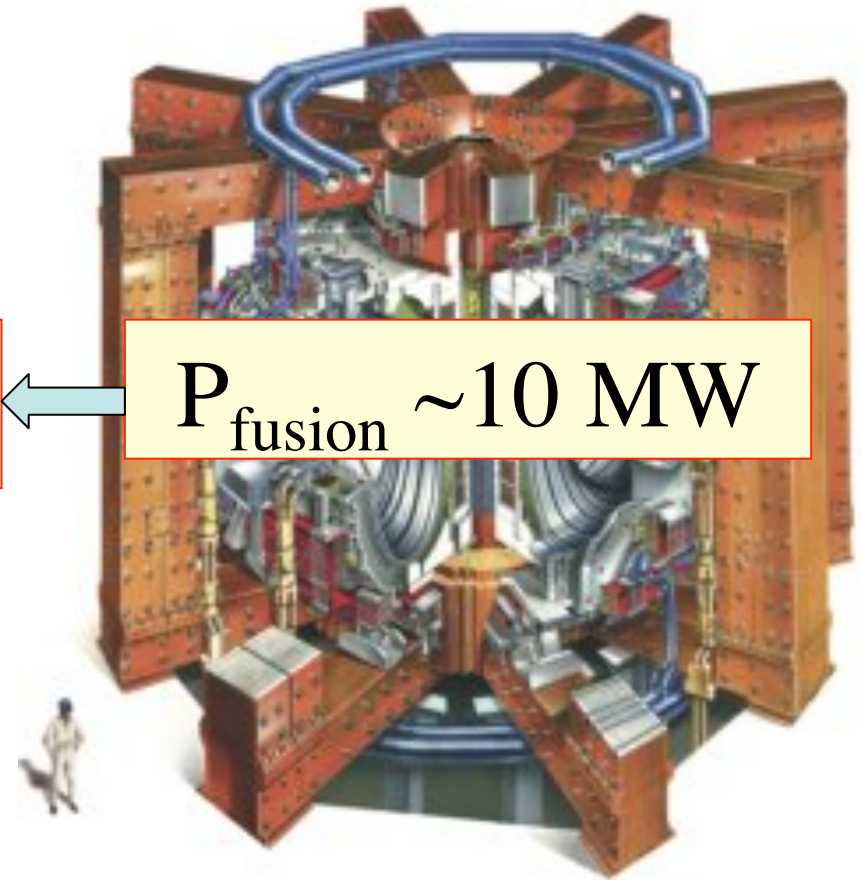
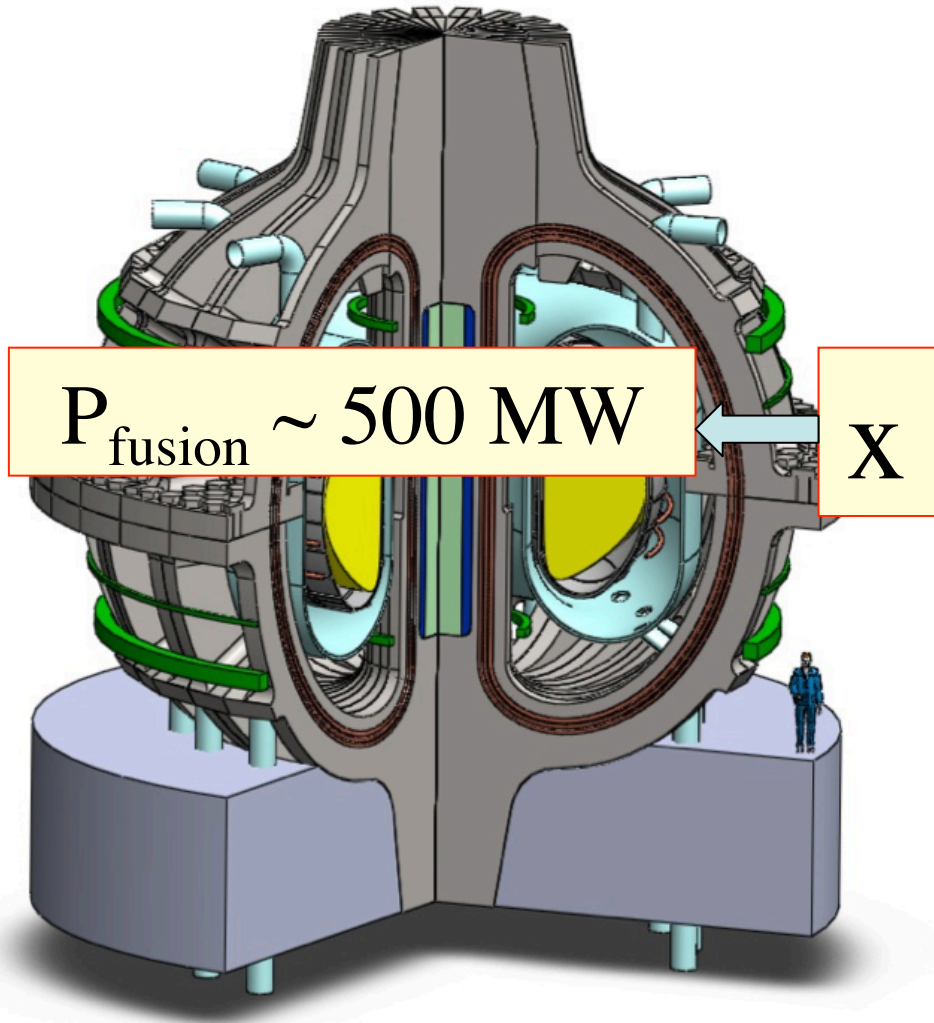


*FNSF-AT V. Chan et al NF 2011*

# ARC conceptual design example of “smaller, sooner” fusion device using new superconductors

REBCO superconductor  $B = 9.2 \text{ T}$

Copper,  $B = 3.5 \text{ T}$



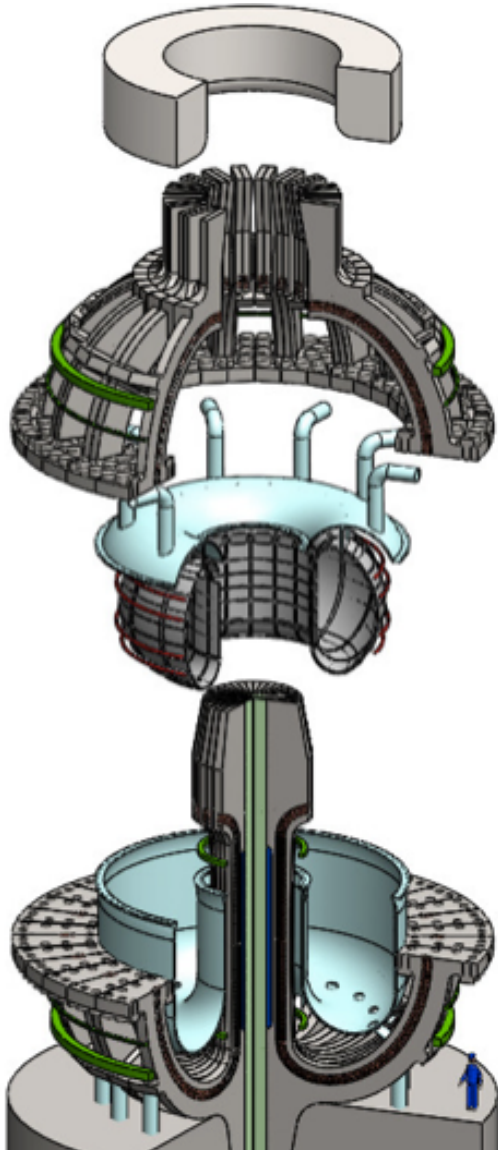
$\times B^4$

ARC:  $R \sim 3.2 \text{ m}$

JET:  $R \sim 3 \text{ m}$   
 $\sim 4 \text{ years construction}$



# ARC conceptual design example of “smaller, sooner” **modular** fusion devices using new superconductors



- Demountable magnetic field coils
- Single-unit vertical lift

Small, modular design features generically attractive to your favorite MFE choice: ST, stellarator, liquid wall etc.

# Multiple, linked engineering design challenges to smaller, modular path

## Challenges

$B_{\text{coil}} > 20 \text{ T}$

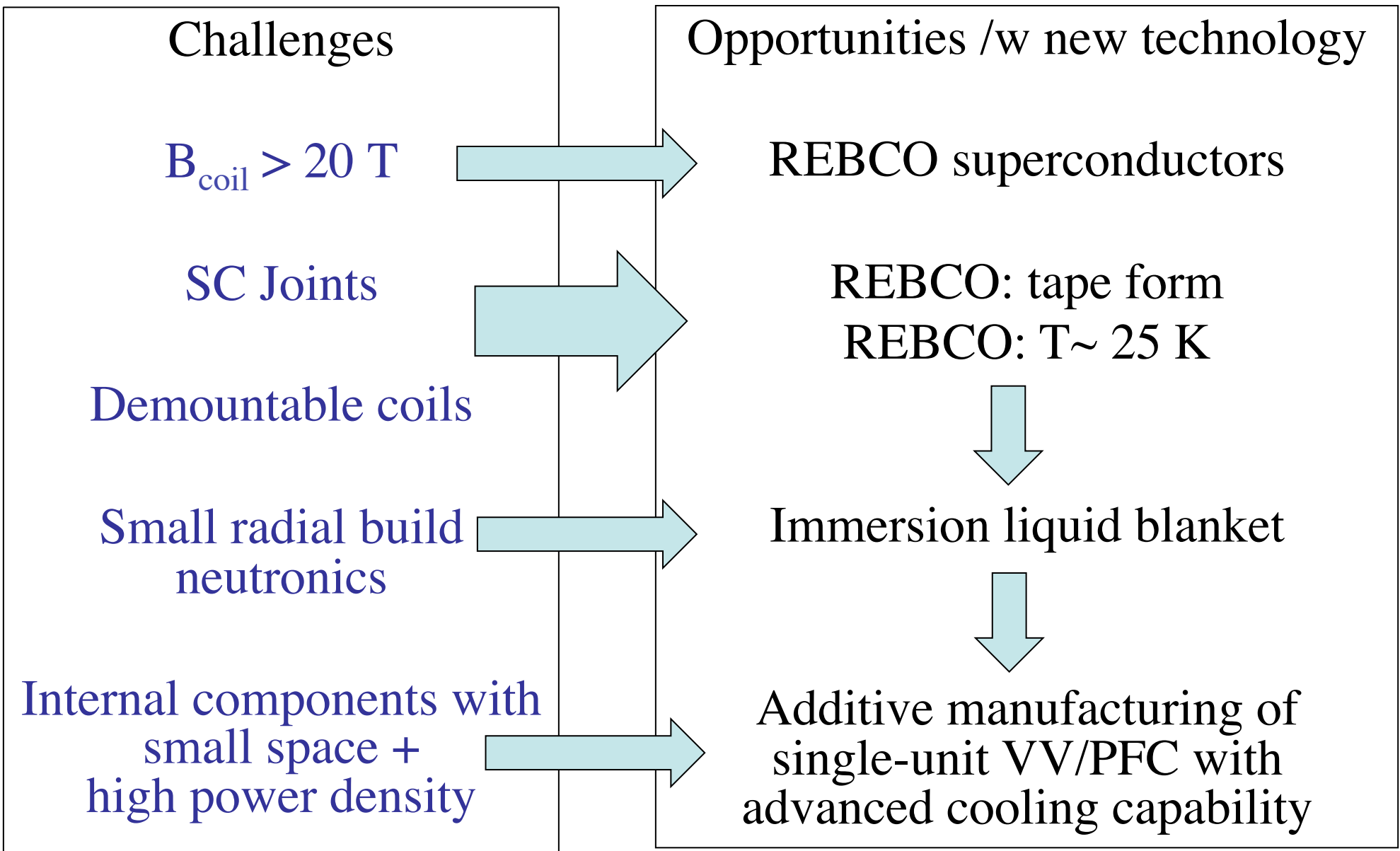
SC Joints

Demountable coils

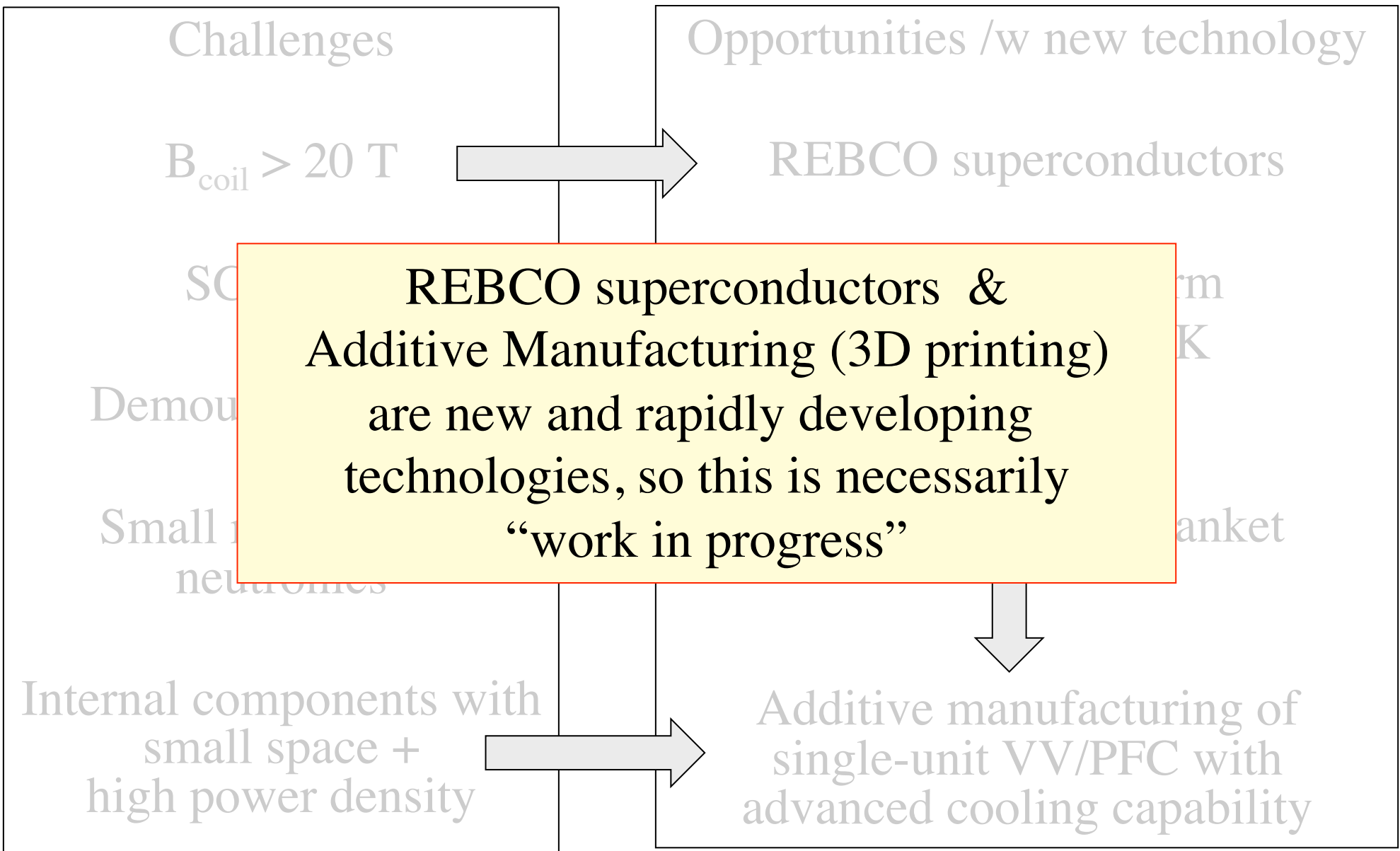
Small radial build  
neutronics

Internal components with  
small space +  
high power density

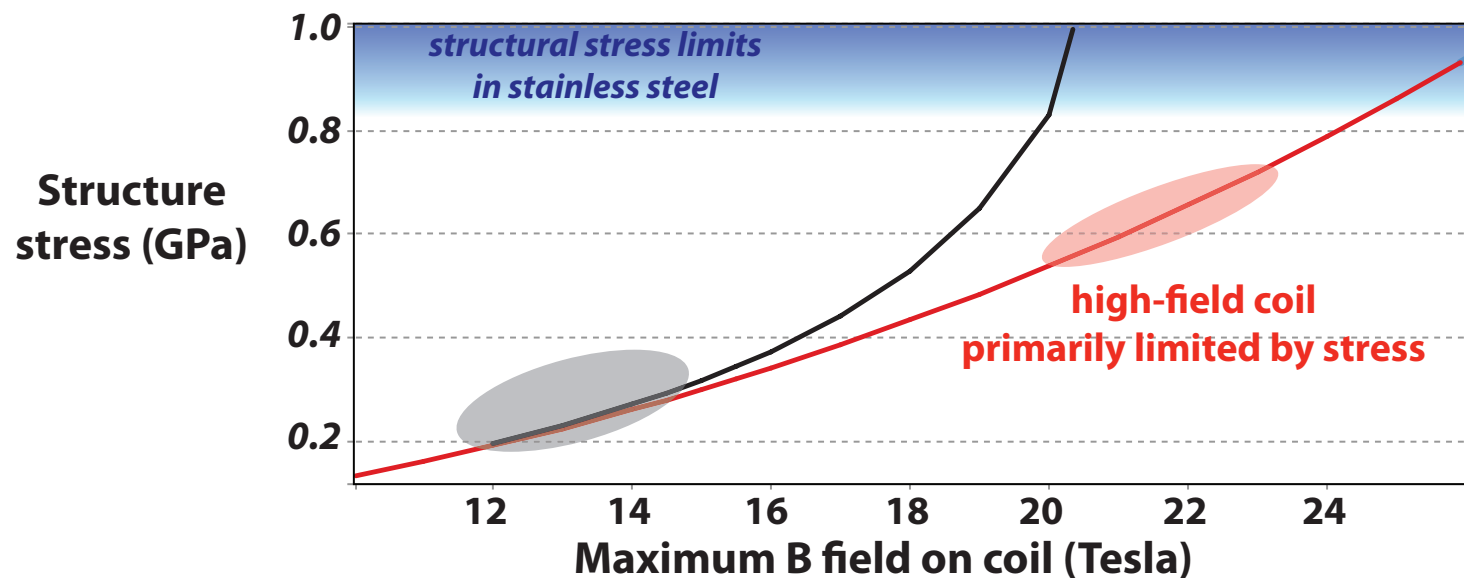
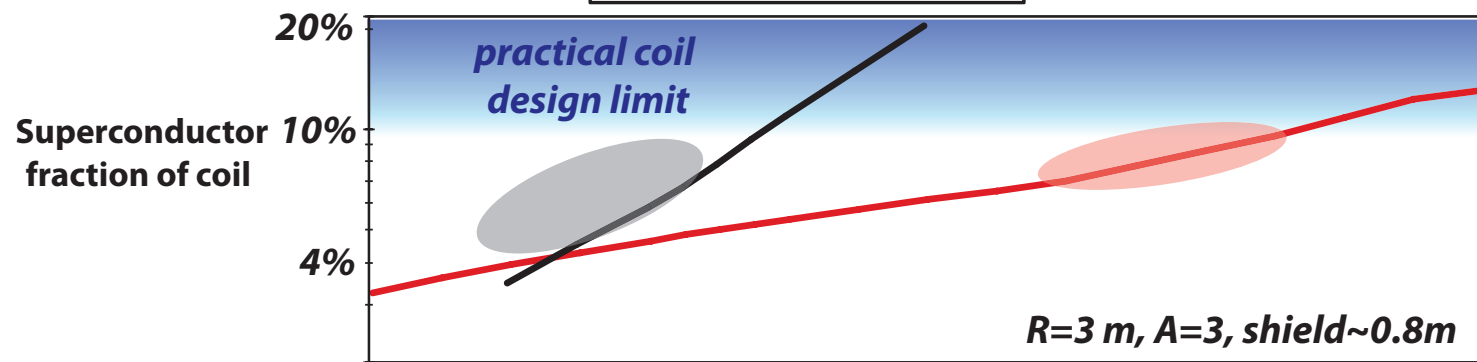
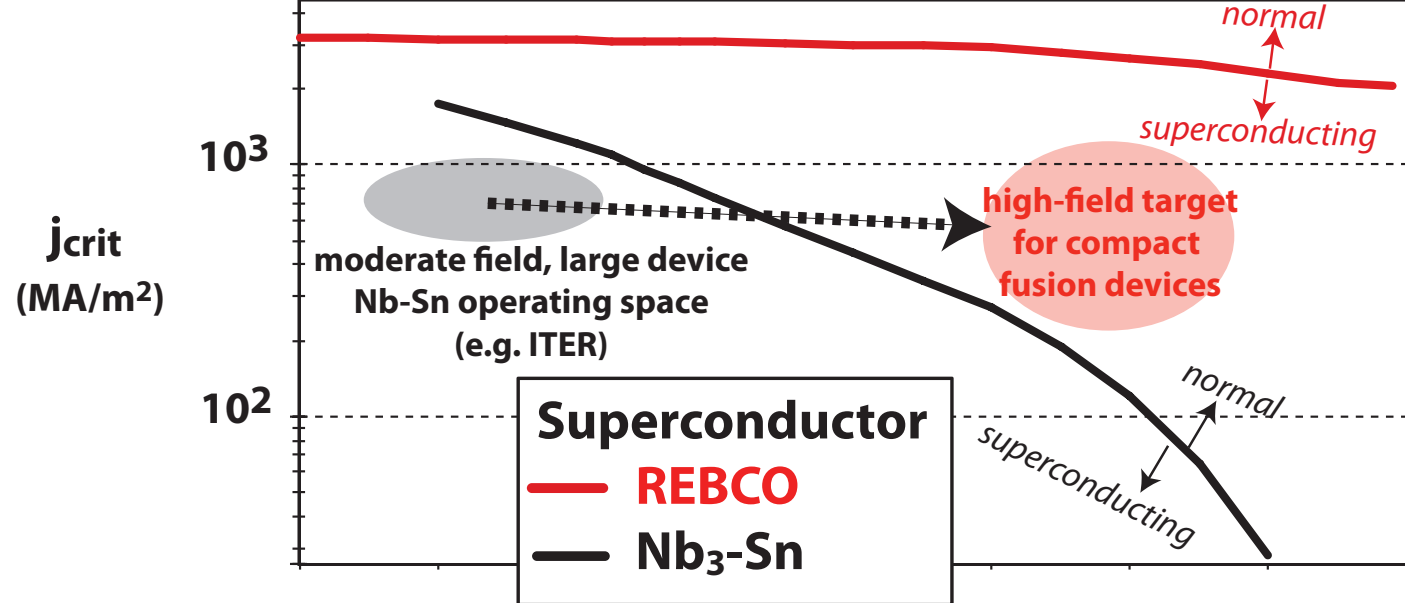
# Multiple, linked engineering design challenges to smaller, modular path



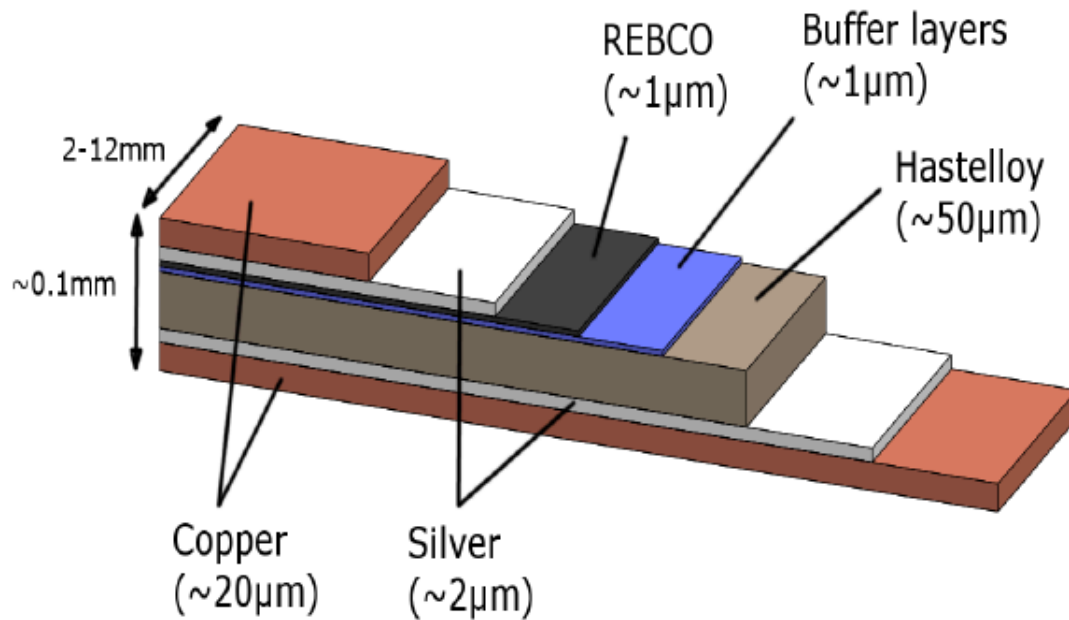
# Multiple, linked engineering design challenges to smaller, modular path



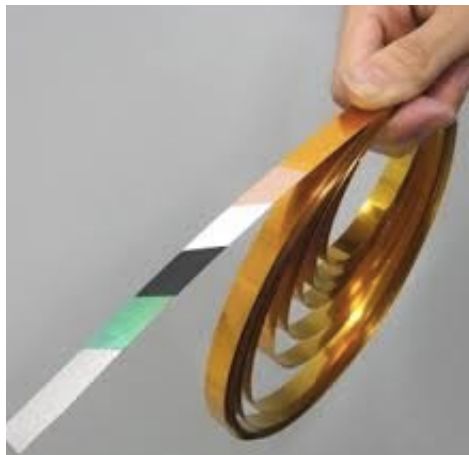
**A revolution in superconductors in last 5 years: REBCO (Rare-Earth Barium Cu Oxide) remain superconducting at VERY high B-field and above liquid He temperatures**



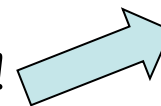
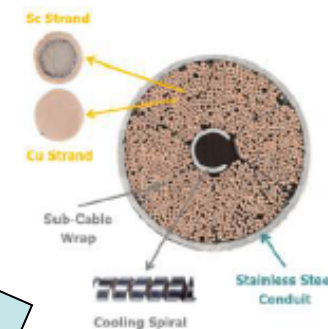
# REBCO: coated superconductors in robust tape form, commercially available



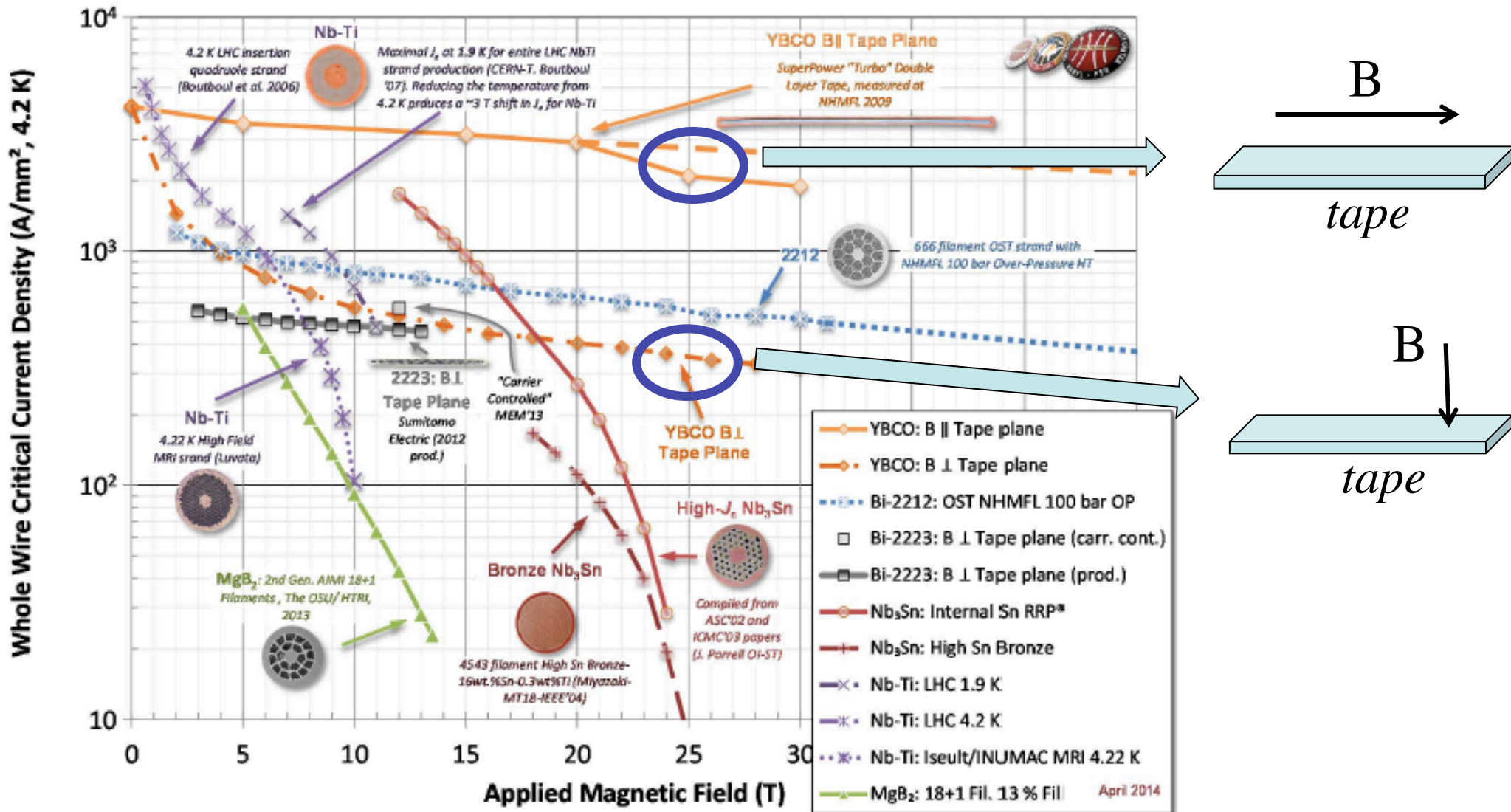
REBCO tape composition  
(*not to scale*)



- Strong in tension due to steel
- Flexible
- Outer Cu coating  $\rightarrow$  simple solder low-resistance joint
- Stark contrast with NbSn superconductor strand & CIC!



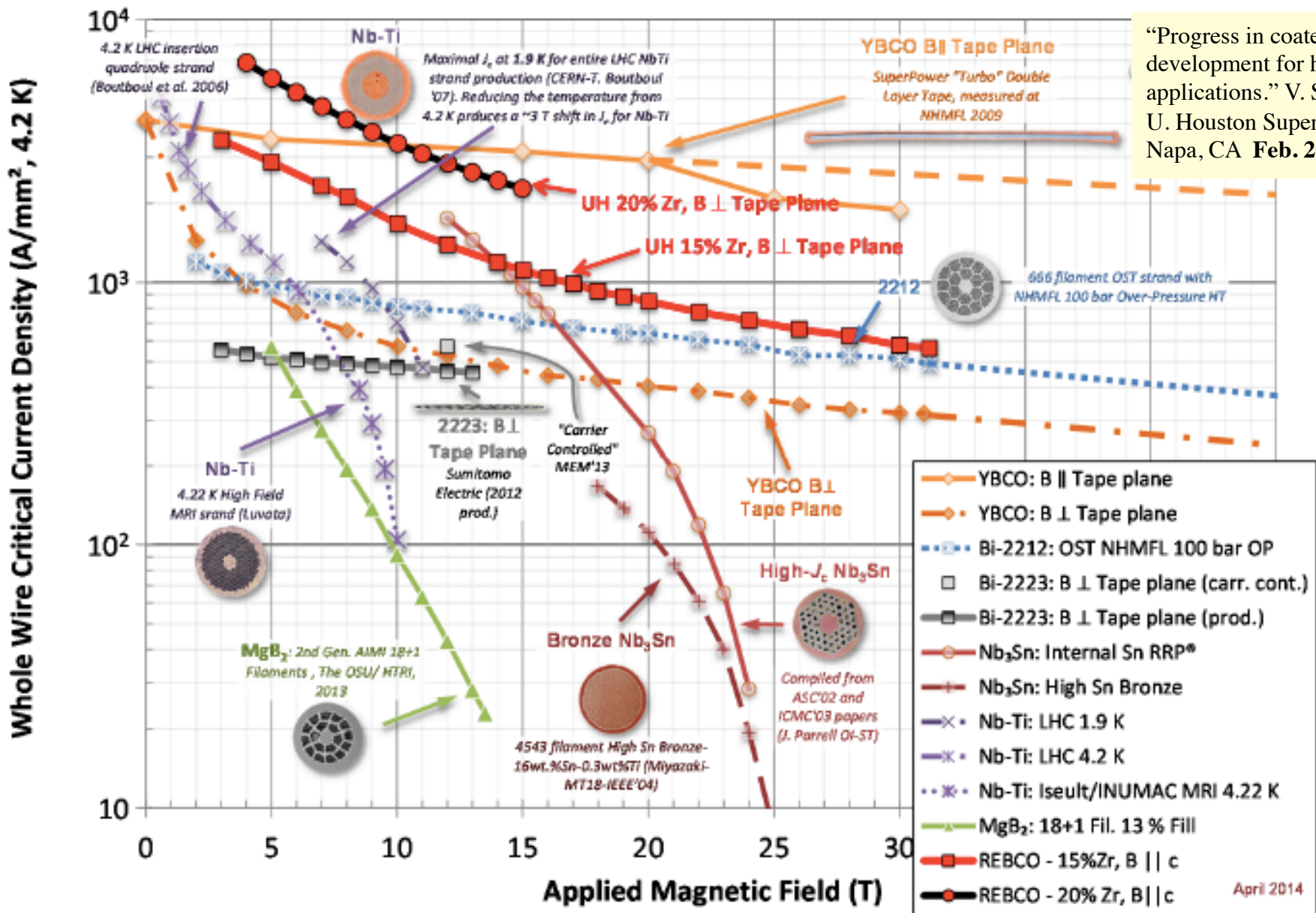
# REBCO superconductors performance is constantly improving for application in high-B coils: E.g. Challenge of field anisotropy in $j_{crit}$



Data maintained by Peter Lee, NHMFL, <http://fs.magnet.fsu.edu/~lee/plot/plot.htm>

# REBCO superconductors performance is constantly improving for application in high-B coils:

E.g. Field anisotropy in  $j_{crit}$  nearly eliminated last year

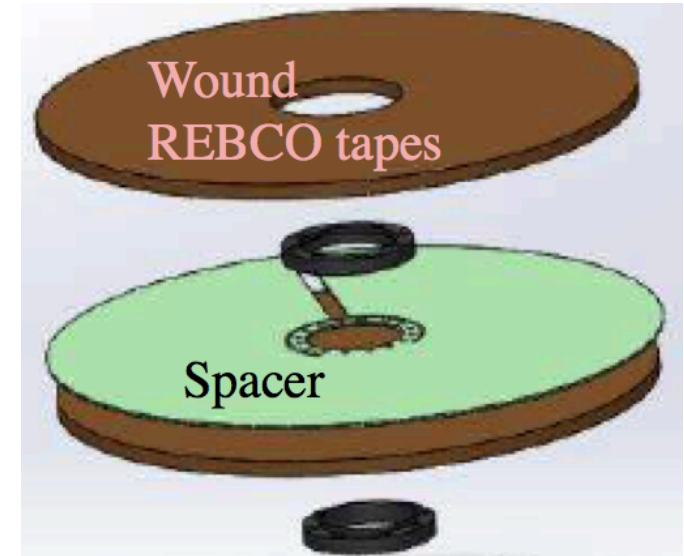
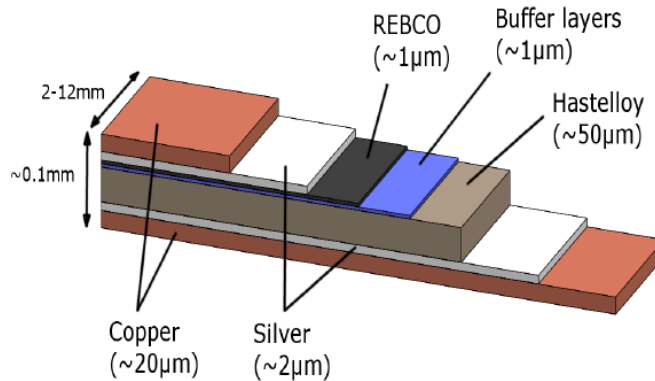


“Progress in coated conductor development for high magnetic field applications.” V. Selvamanickam, et al. U. Houston Superconductor Workshop, Napa, CA Feb. 2015

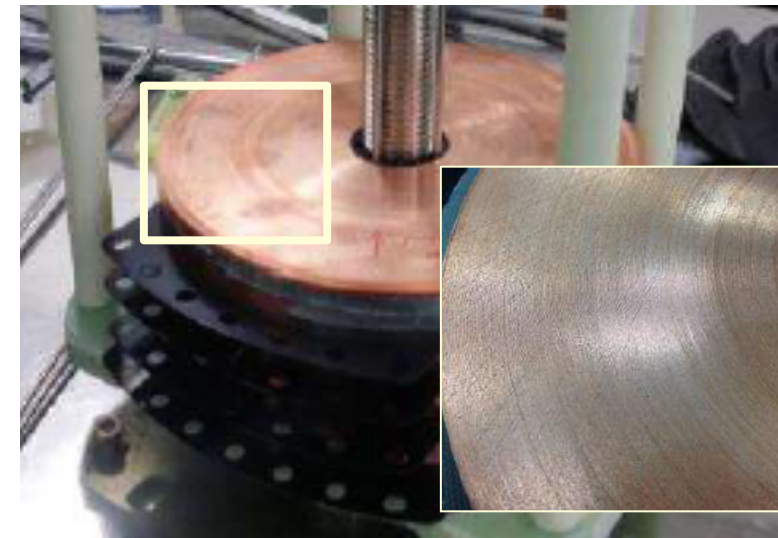
April 2014



# Making coils from REBCO: “No-insulator” tape winding highly attractive

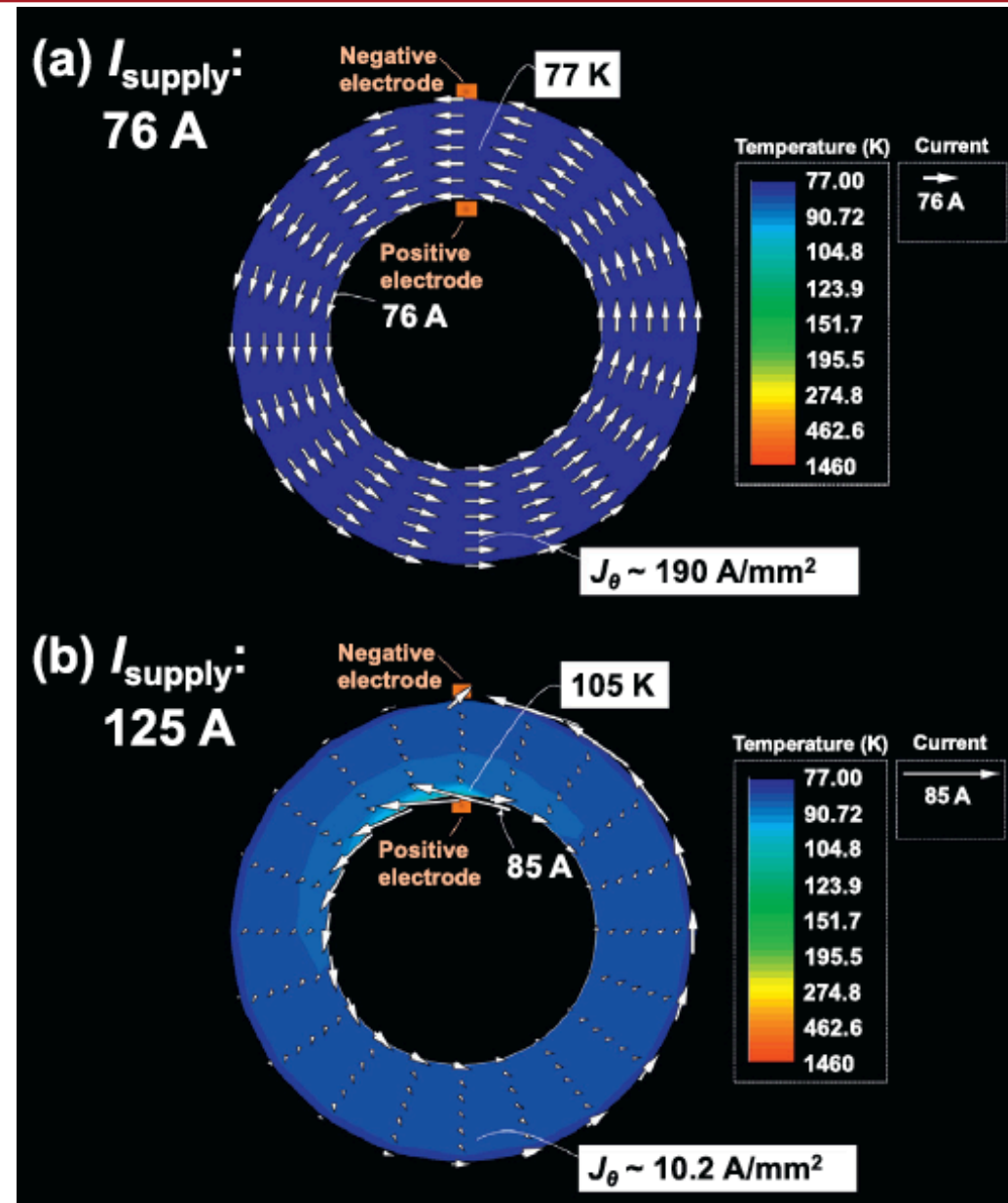
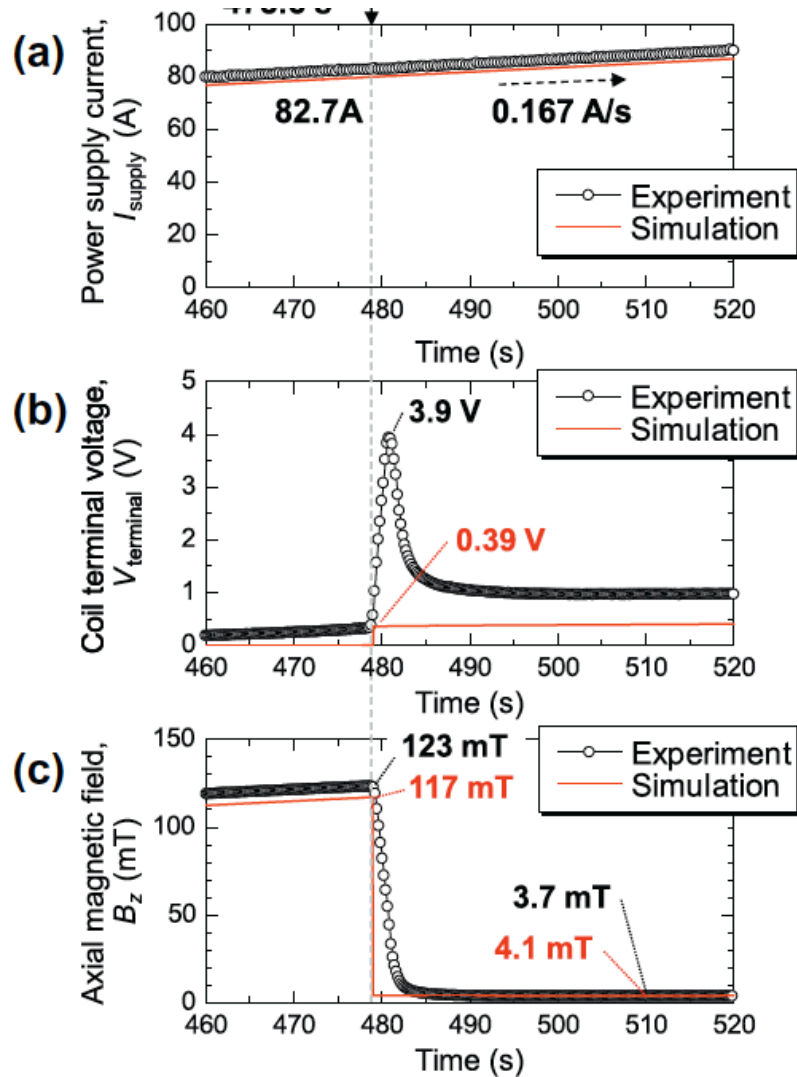


- Steel is “internal” insulator for each turn
- Benefits
  - Simple
  - Improved mechanical strength
  - Radiation resistance (insulators weakest link)
  - Self-protecting in quenches



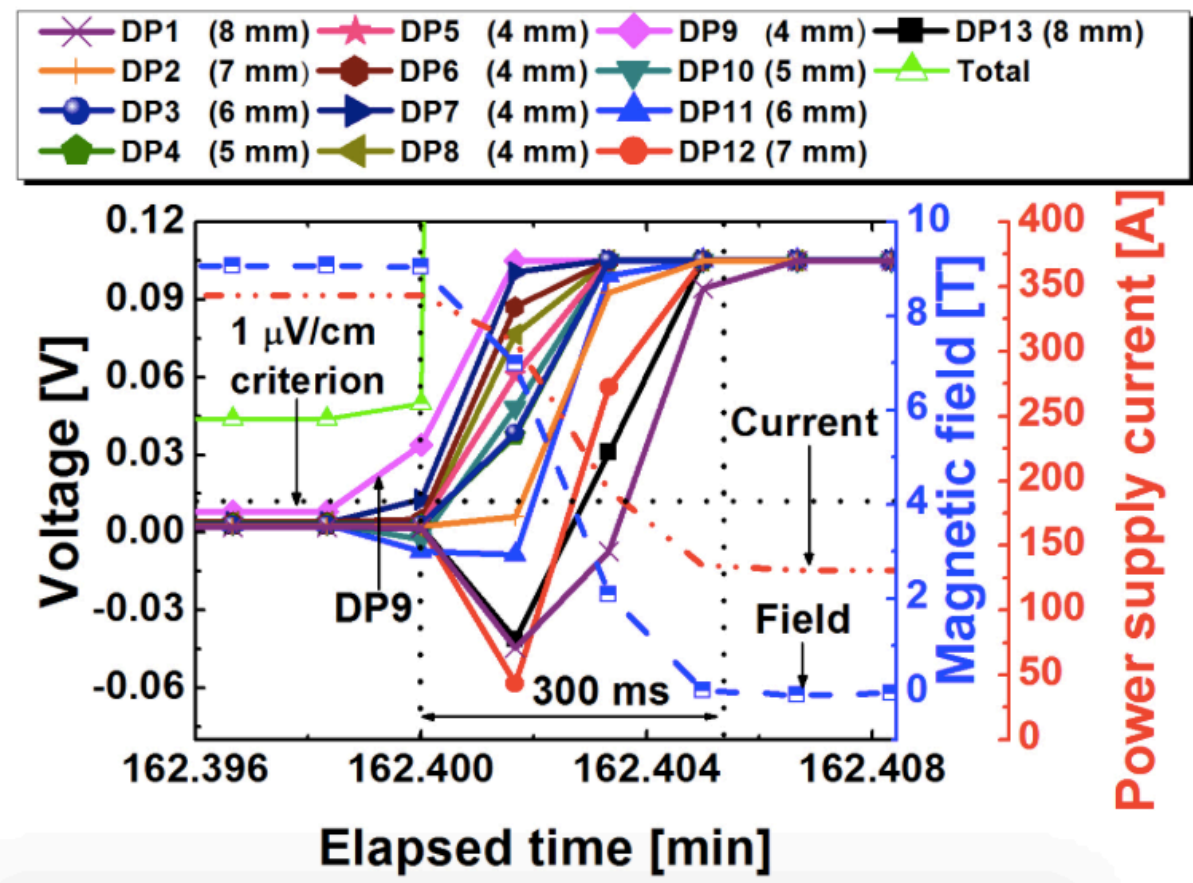
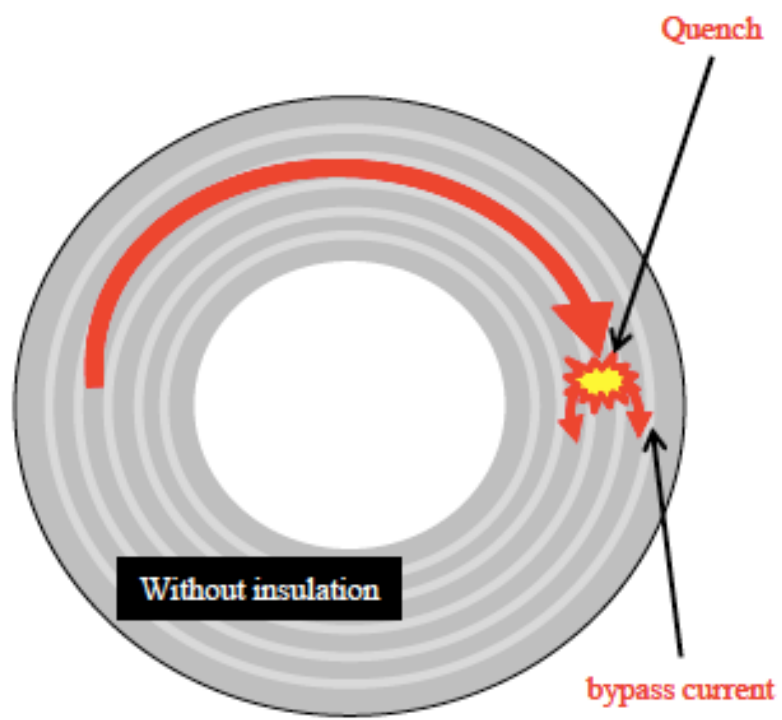
*S. Hahn et al. App Phys Lett 173511 (2013)*

# No-insulator coil self-heals via internal redistribution of $j \rightarrow$ “Single-turn mode” $\rightarrow$ Immediate drop in $B$ , energy distributed in coil



Yanagisawa et al. *Physica Scripta C* (2014) 40

# “No-insulator” winding provides intrinsic quench protection in coil.



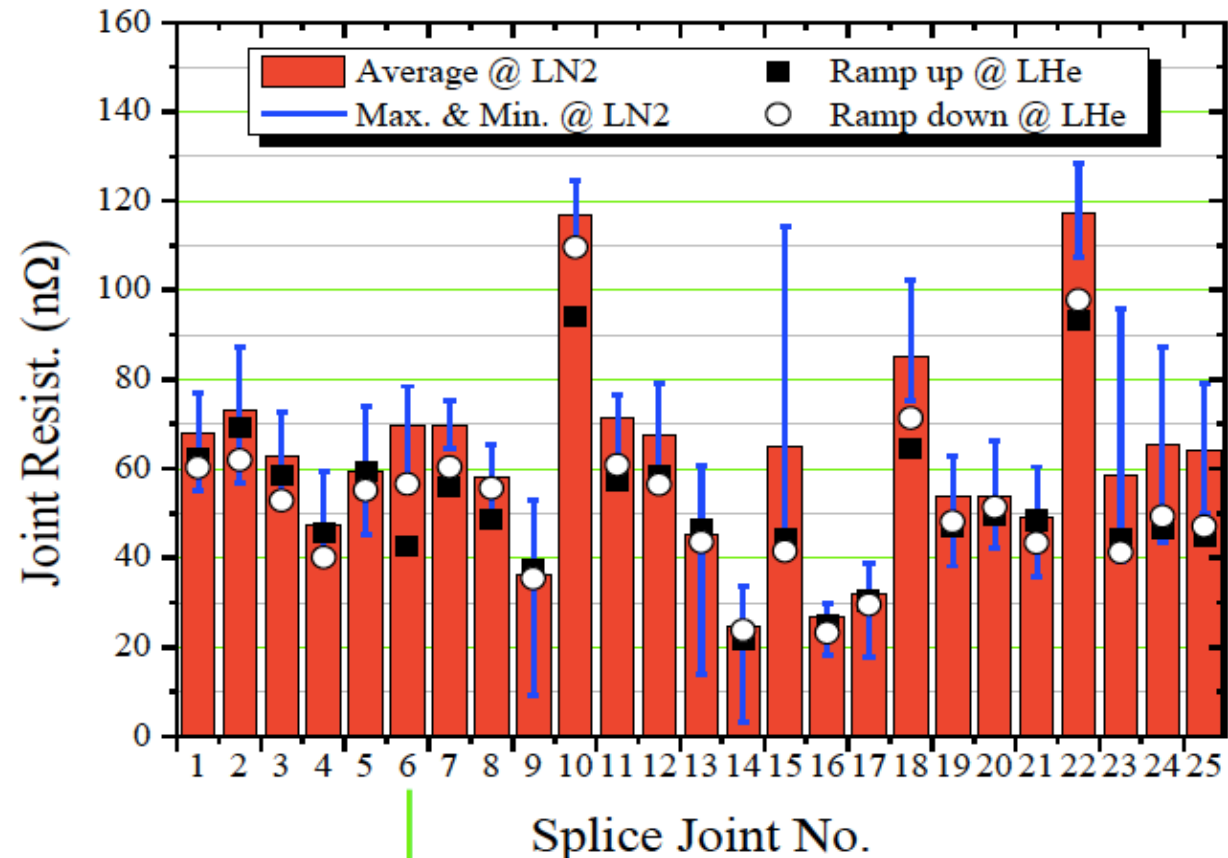
*Quench at 9 Tesla: No damage to stacked double pancake coil (2014)*

S. Hahn et al. Bitter Magnet Lab, MIT

# Large coils made with REBCO actually *require* joints: Contact resistance at low-T is acceptable



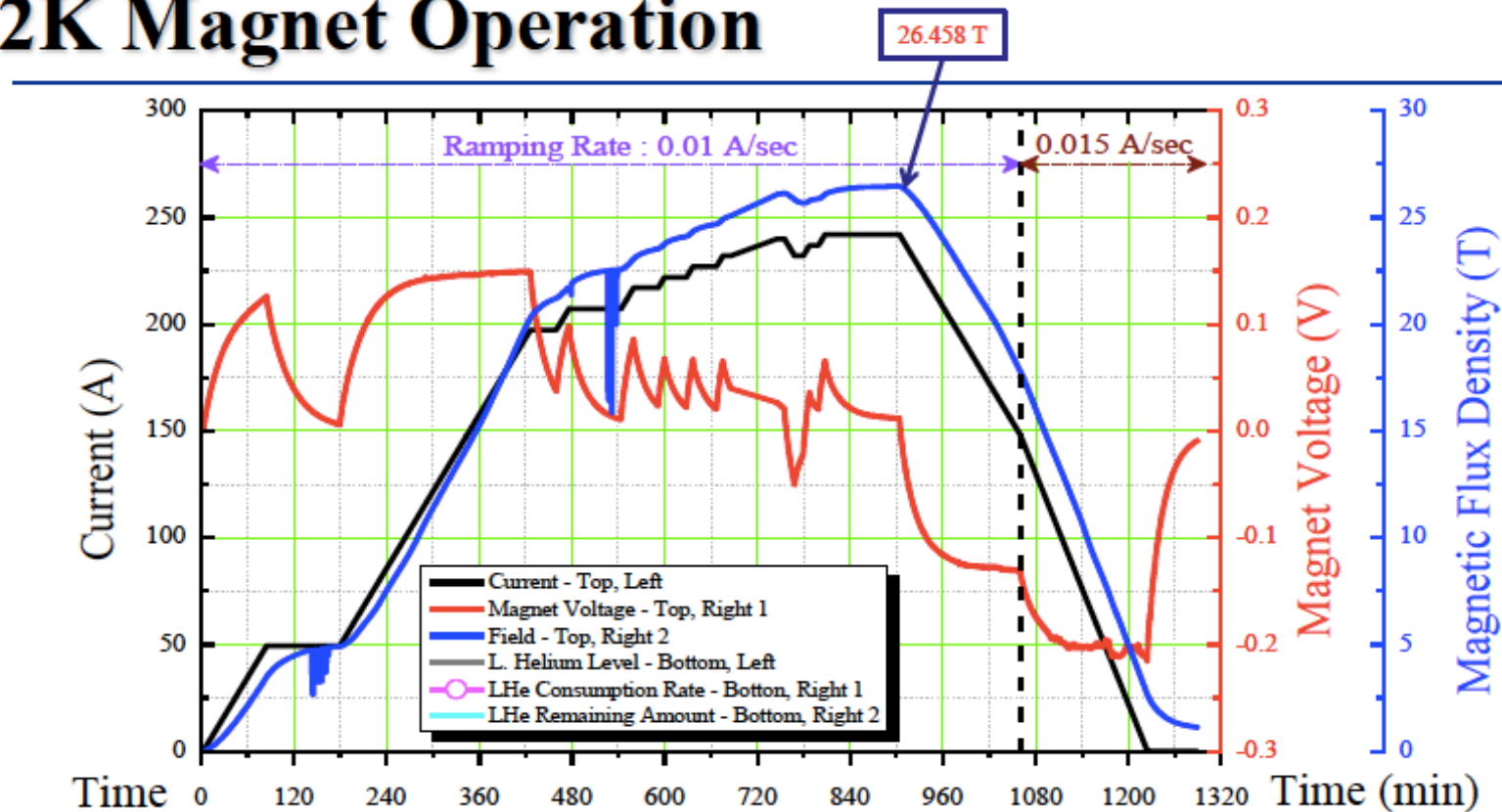
26 stacked coils  
~300 m/coil consistent  
with maximum  
continuous length of  
high-performance tape



- Soldered joints!
- Mechanical attachment lowers resistance

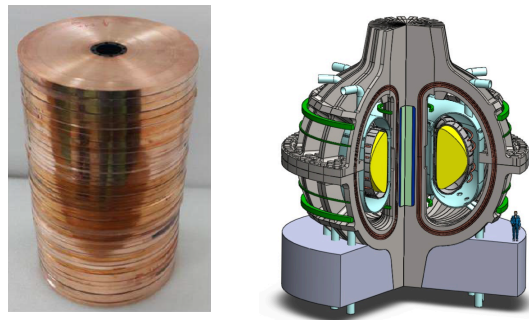
# April 2015: New record of 26.5 Tesla with REBCO-only, “no-insulation” coil

## 4.2K Magnet Operation



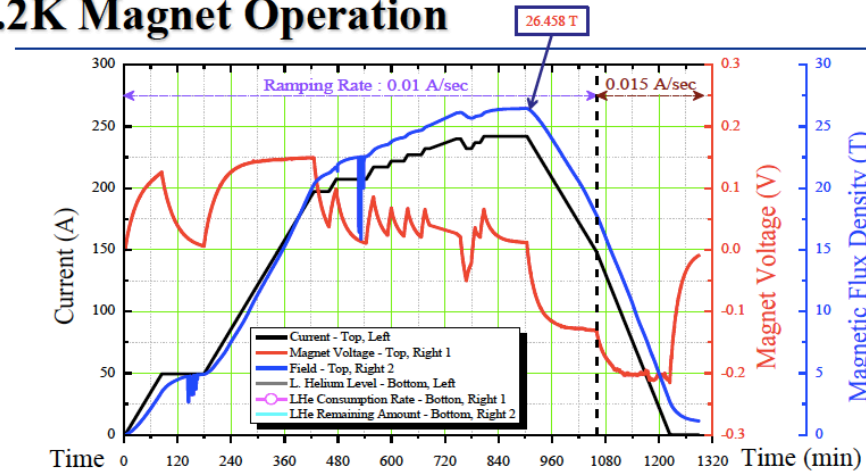
*S. Hahn, J.M. Kim, et al.  
NNFML, FSU, SUNAM, MIT*

# Scaled-down REBCO coil matches most requirements for ARC design

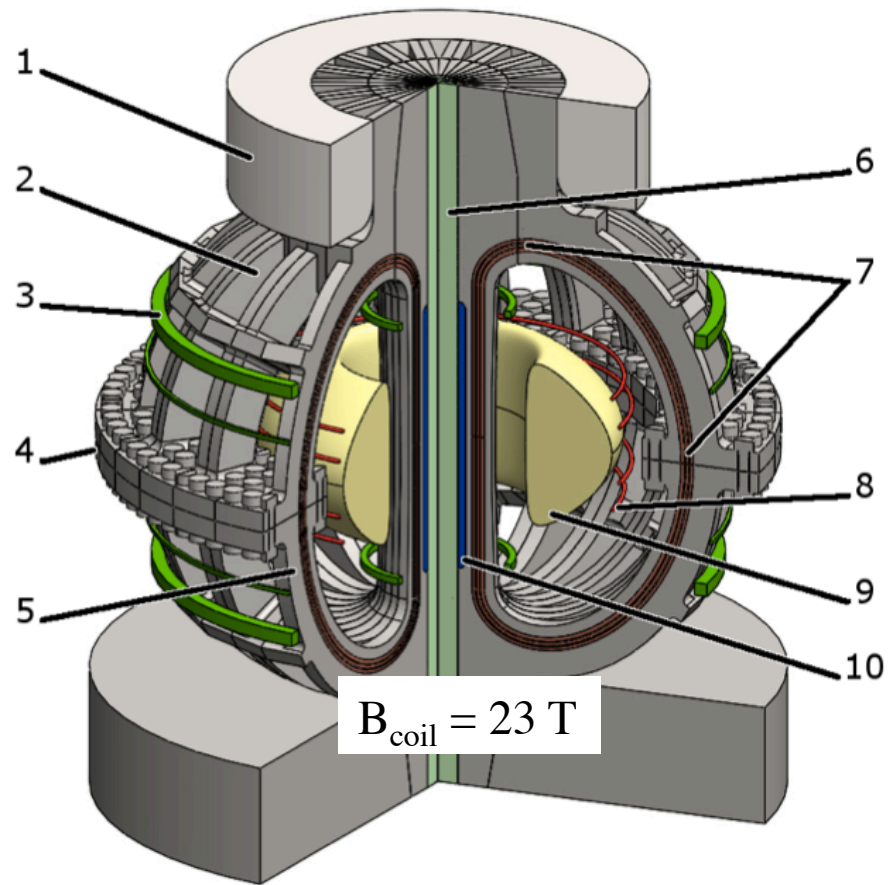


$B_{\text{coil}}(\text{T})$	<b>26.5</b>	<b>23</b>
$J_e (\text{A}/\text{mm}^2)$	400	400-500
T (K)	4.2	25
Materials	REBCO, SS316L	
$\sigma_{\text{max}} (\text{MPa})$	593	660
Diameter (m)	0.03	~ 6

## 4.2K Magnet Operation

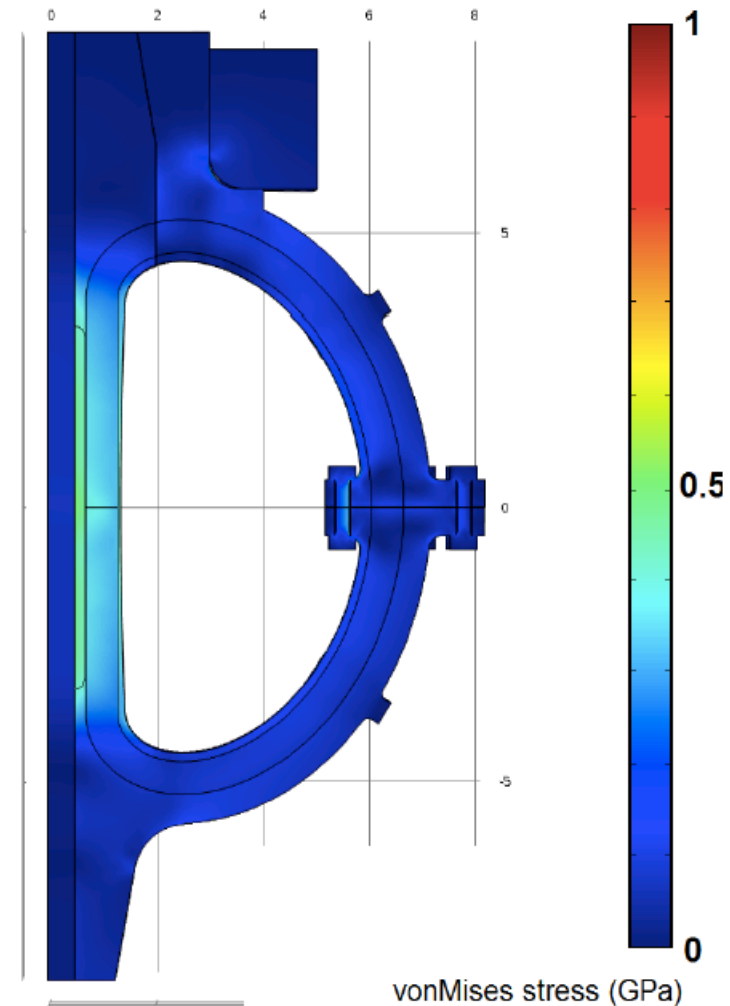


# Large-bore challenge for high-B MFE magnet: requires optimized geometry & superstructure

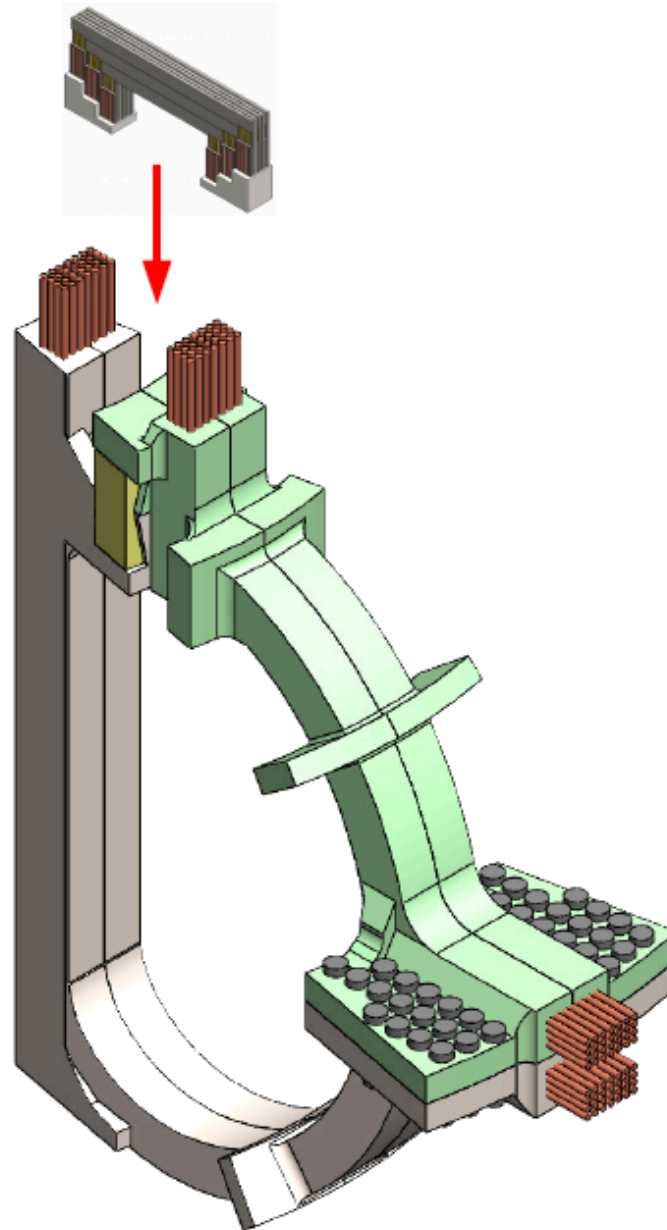


- 1. Support ring, 2. Top TF leg
- 4. Mechanical joint
- 6. Epoxy enforcement

Peak stress  $\sim 0.67 \text{ GPa}$   
 $\sim 65\%$  of limit for 316SS LN



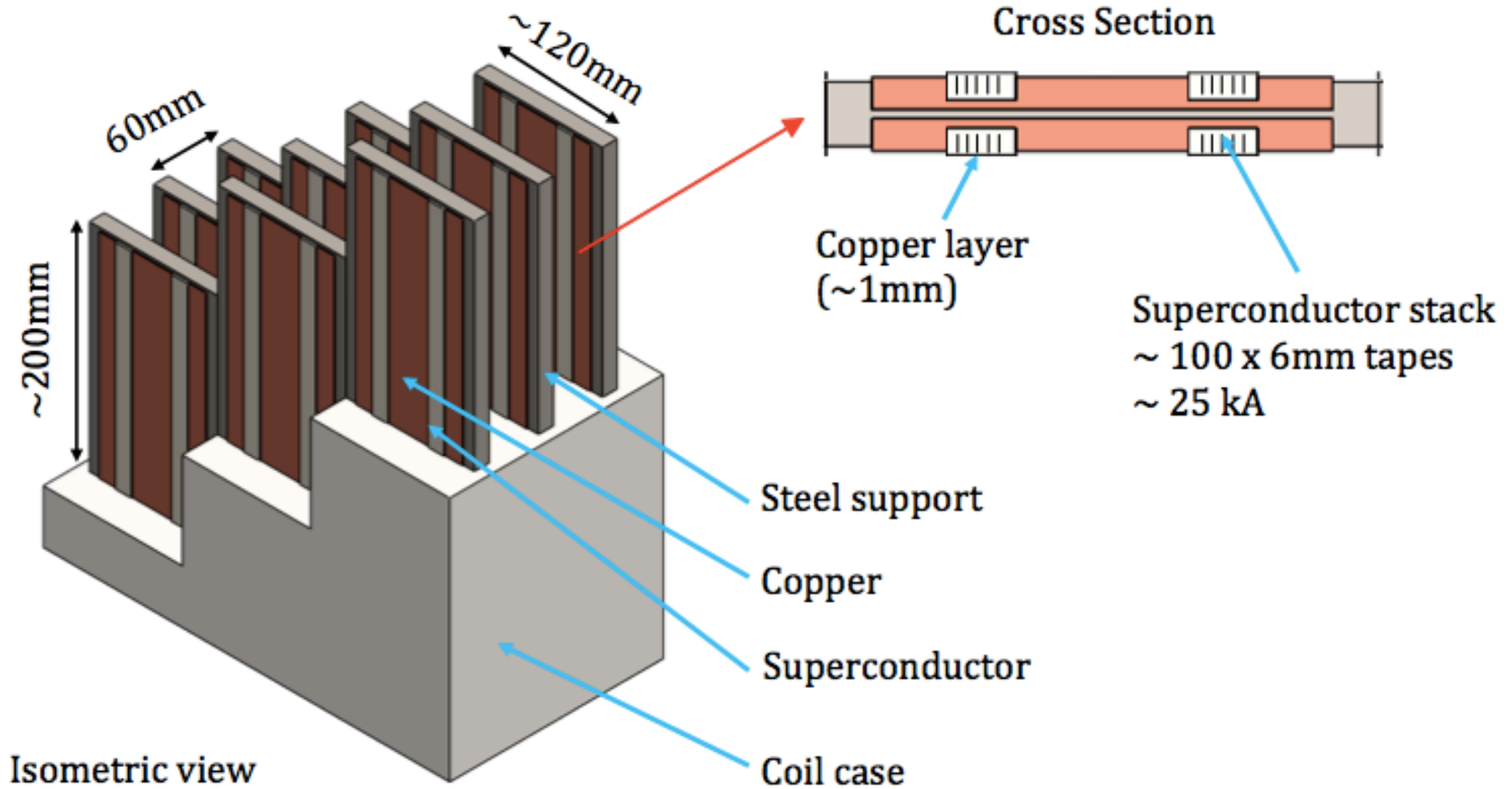
# Demountable TF coil: Evolving strategy → Separation of mechanical and electrical joints



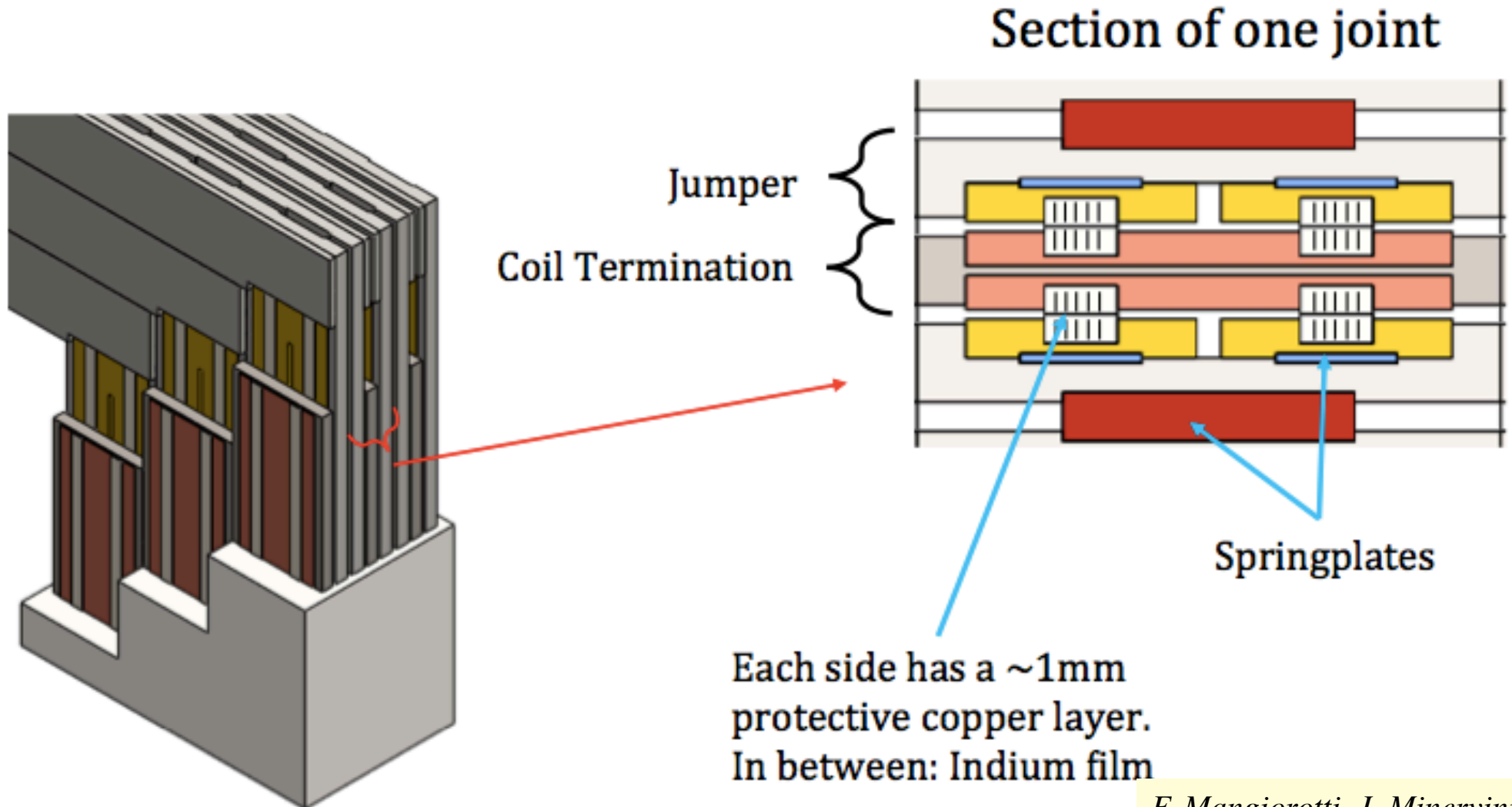
*F. Mangiorotti, J. Minervini  
MIT Ph.D. thesis*



# One design example: Plate terminations with edge joints



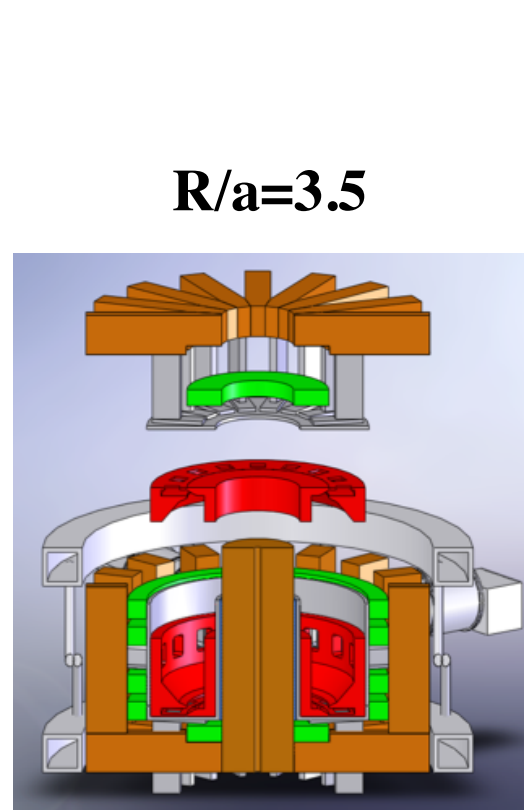
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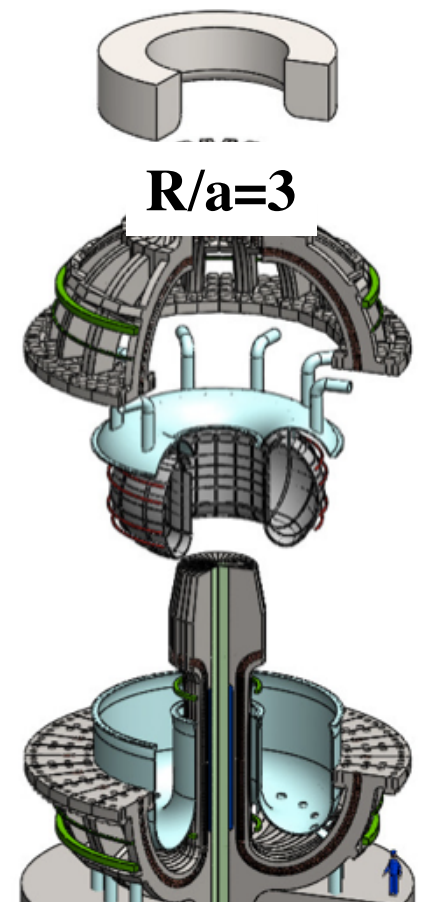
*F. Mangiorotti, J. Minervini  
MIT Ph.D. thesis*

# Operation of joints above 4 K liquid He temperatures is highly advantageous

- Greatly reduces required cooling power (Carnot).
- Thermal stability due to higher heat capacity.
- Operation or ARC at  $T \sim 25$  K
  - Small power to joints
  - Liquid H or Ne for cooling options



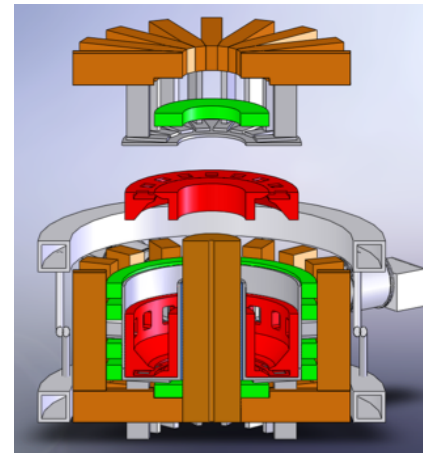
**Copper FNSF-AT**  
Coil  $P_{\text{coil}} \sim 500$  MW



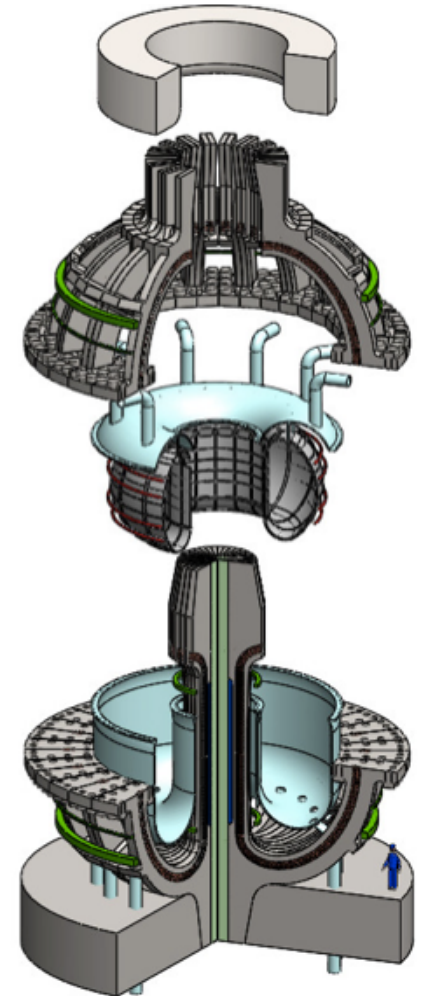
**ARC: Resistive joints /w REBCO superconductors**  
Coil  $P_{\text{coil}} \sim 1$  MW

# Demountability seems complicated... is it really worth it? Yes, for FNSF/Pilot

- Demountable design transfers complex, integrated risk away from the speculative nuclear components and places it on “non-nuclear” mechanical/electrical engineering.
  - Nuclear components have “Catch-22” problem: needs FNSF to test its own components!
  - Can demonstrate demountable joints at small scale.
  - Device maintenance with modular coils: single leg failure of TF can be tolerated



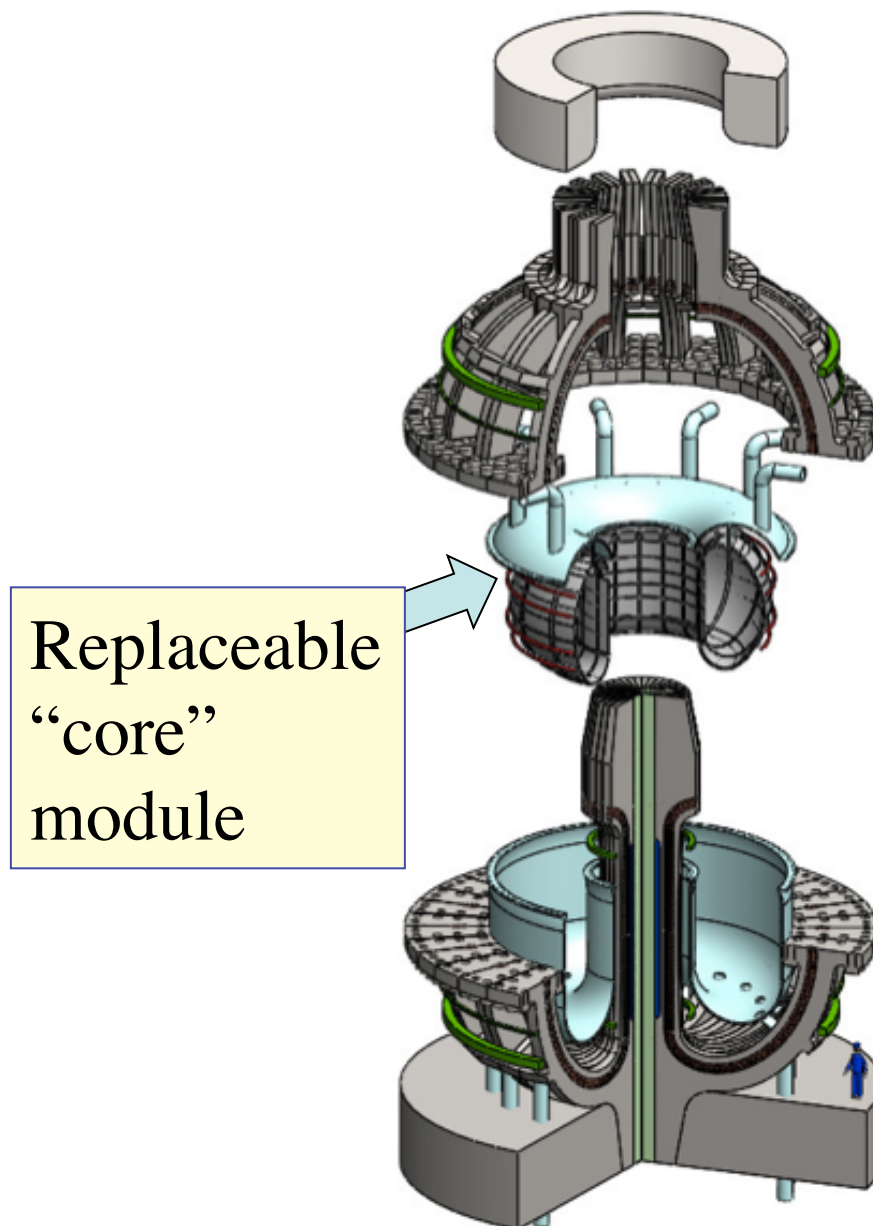
Copper FNSF



ARC

# Demountable coils have a profound effect on modularity and design of interior fusion “core”

- Core is designed as a single integrated unit
  - PFCs, vacuum vessel, blankets
  - Synergy with keeping design of small total mass and volume
- **Fabrication + qualification done completely off-site**
  - **Vacuum**
  - **Heating**
  - **Cooling**
- No connections made inside TF

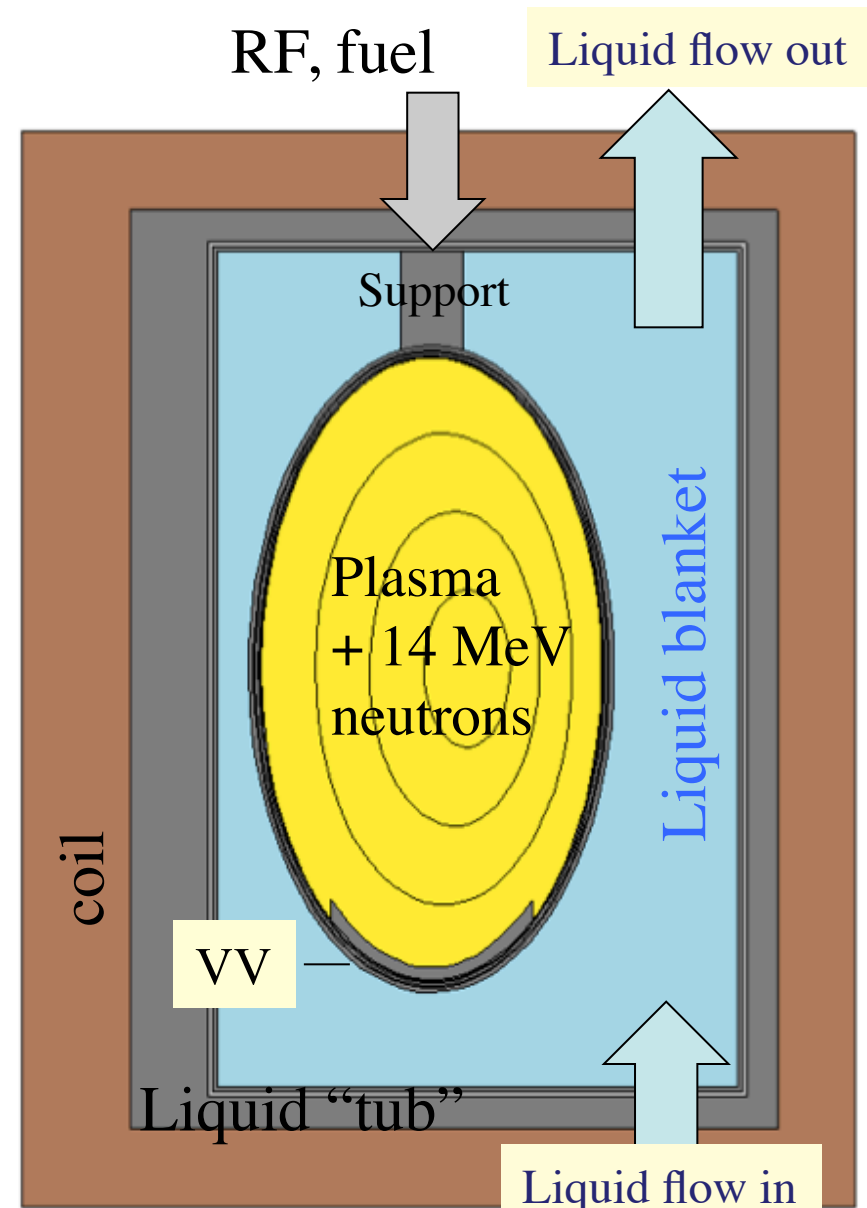


# Modular core can have a profound effect on fusion design: e.g. the immersion blanket

- VV is right beside plasma
- VV is immersed in liquid blanket

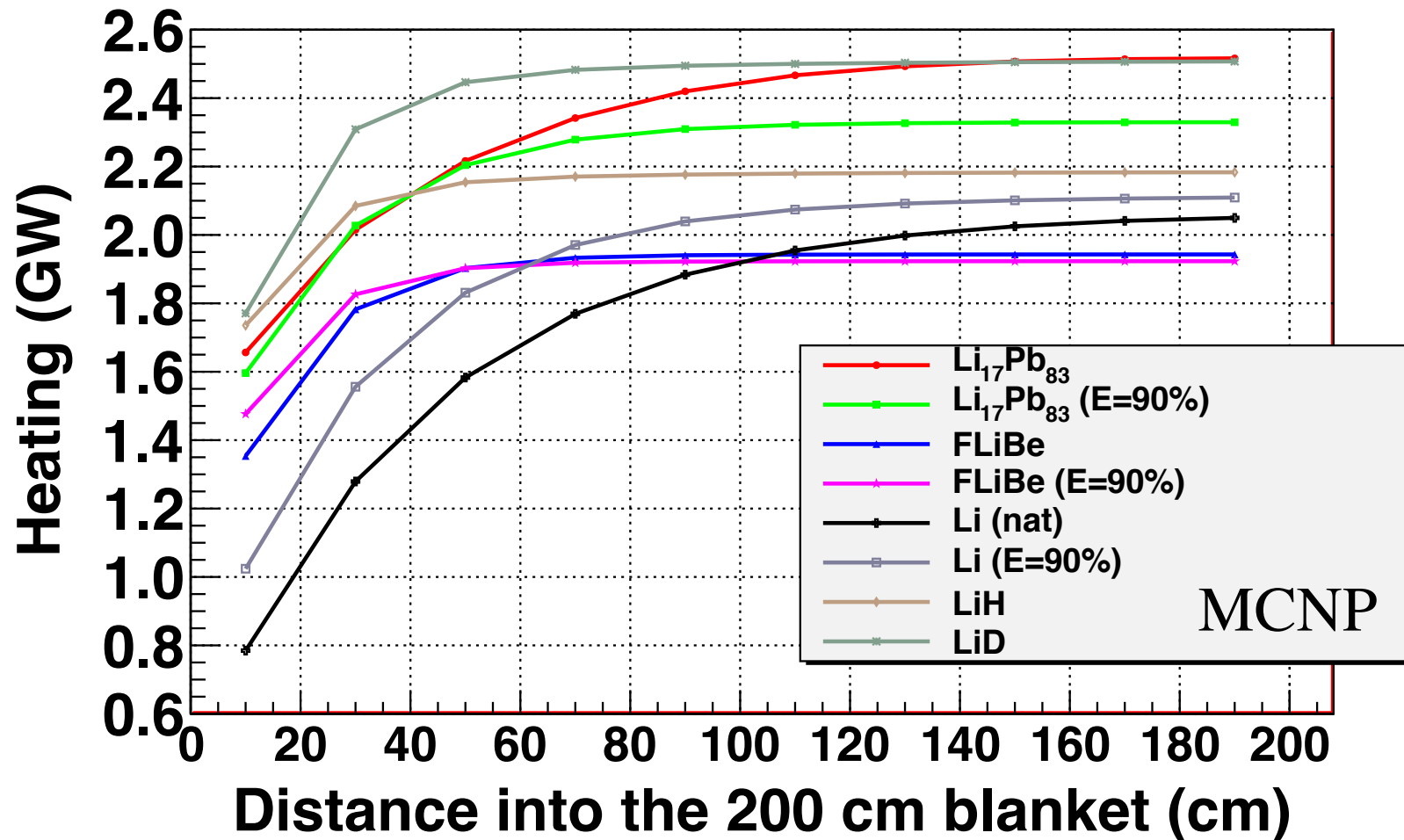
## Advantages

- Simple
- Neutronics/nuclear engineering at atmospheric pressure.
- No gaps
- Energy & tritium extraction with single-phase low-velocity flow
- No DPA limits in blanket
- Minimized solid waste
- Tub is robust safety boundary



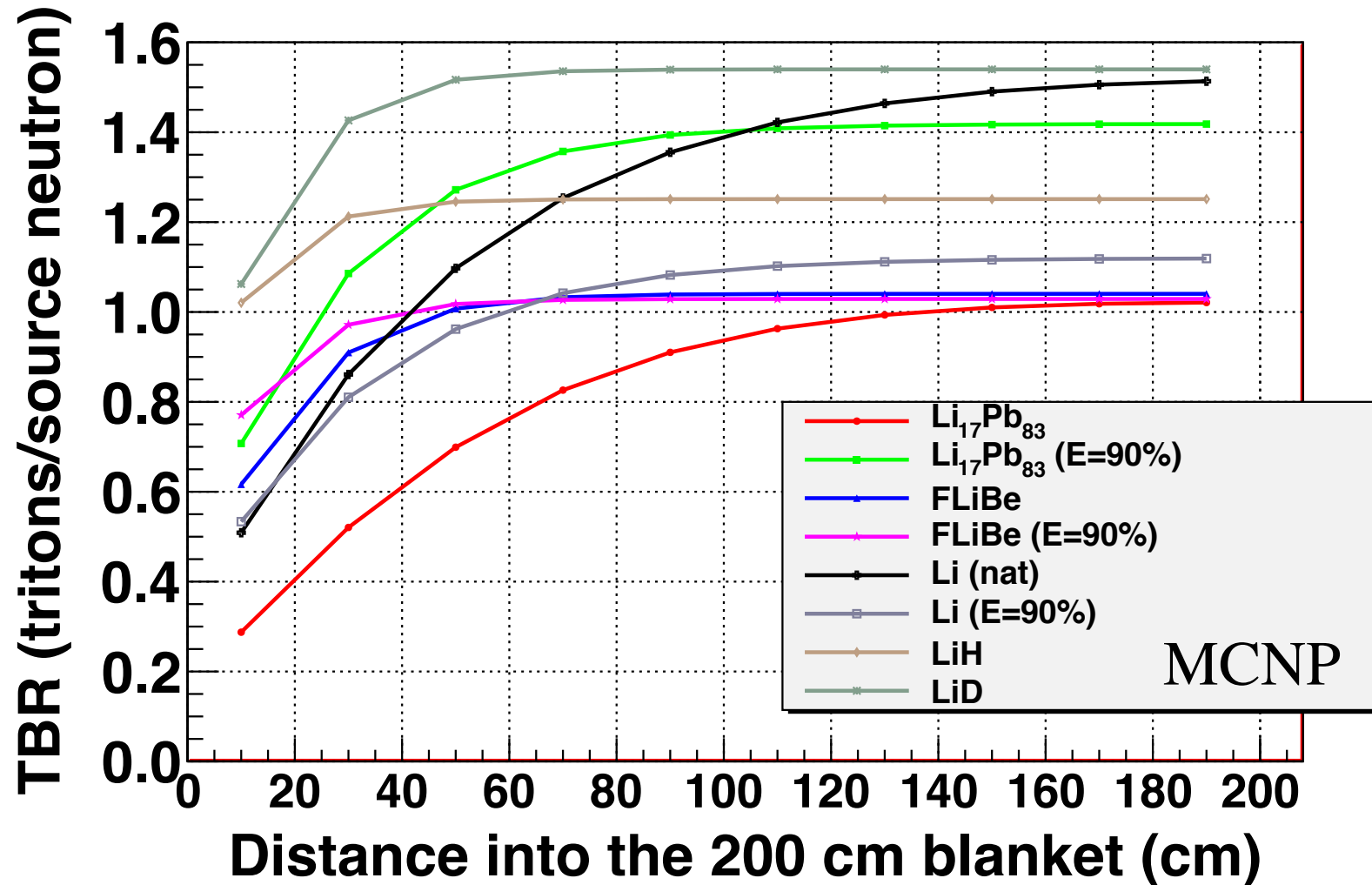
# Immersion blanket: Many liquid choices & lack of internal structure optimize neutron thermalization, energy capture and tritium breeding → Small radial build

Heating with 2mm W first wall, 2.54cm Inconel-625 vessel



# Immersion blanket: Many liquid choices & lack of internal structure optimize neutron thermalization, energy capture and tritium breeding → Small radial build

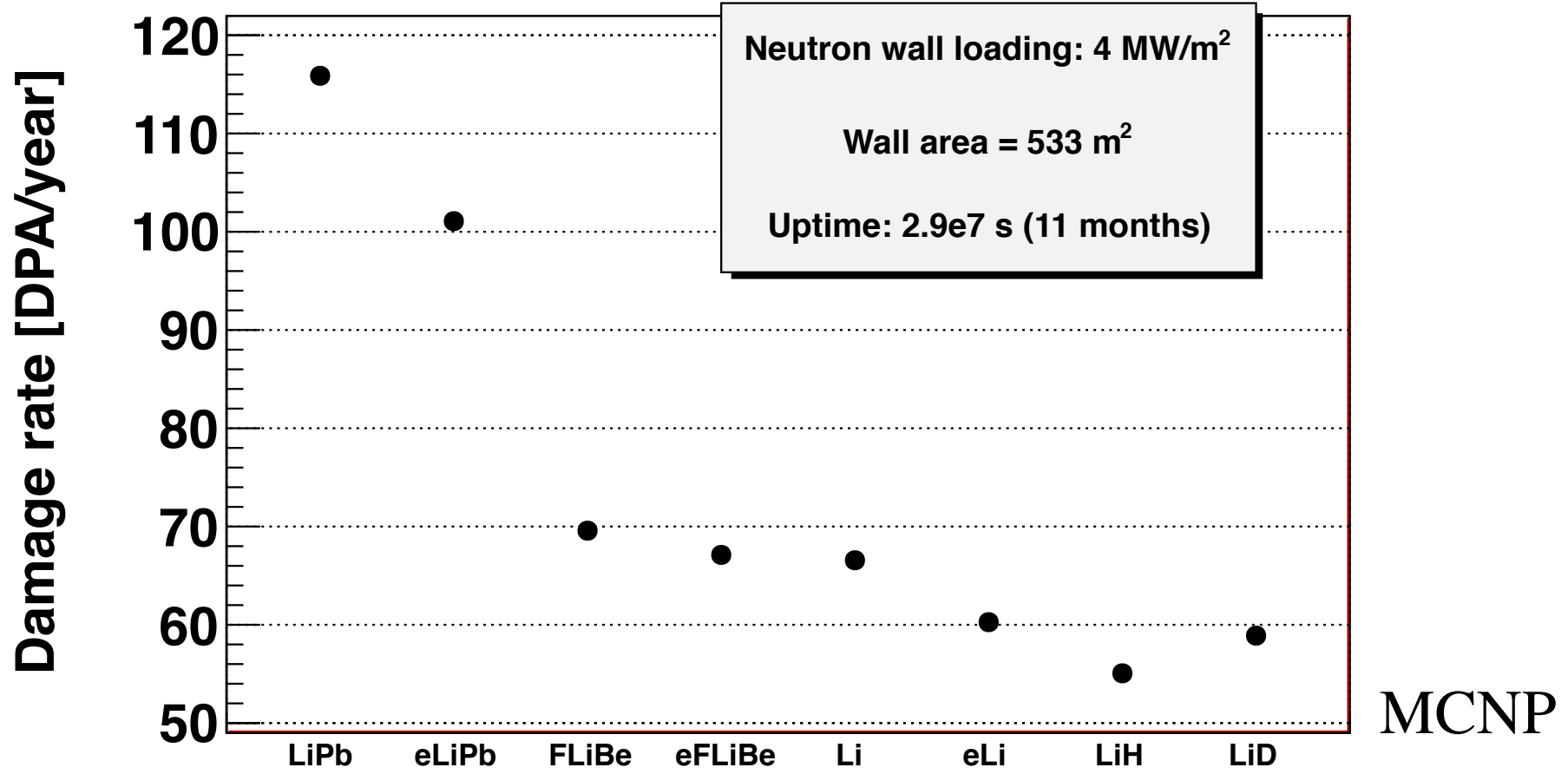
TBR with 2mm W first wall, 2.54cm Inconel-625 vessel





# Immersion blanket: Solid, replaceable components (plasma-facing materials, vacuum vessel) receive minimized neutron damage immersed in low-Z fluid

## Damage to the Inconel-625 primary vacuum vessel

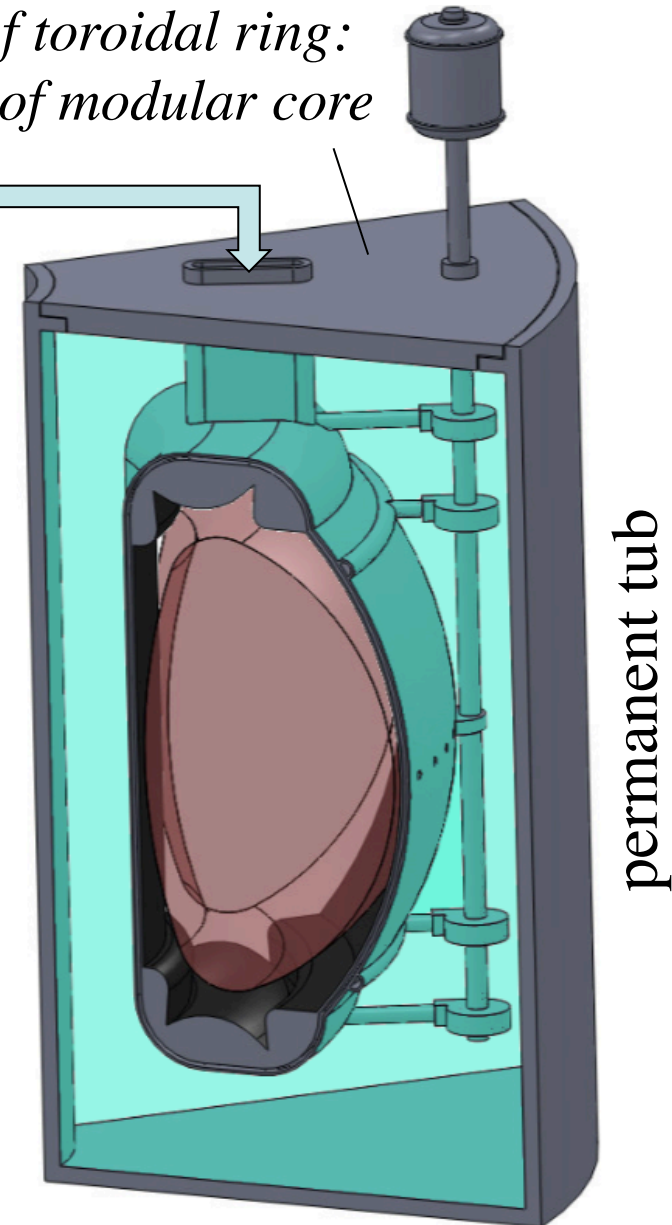


Z. Hartwig, C. Haakonsen MIT

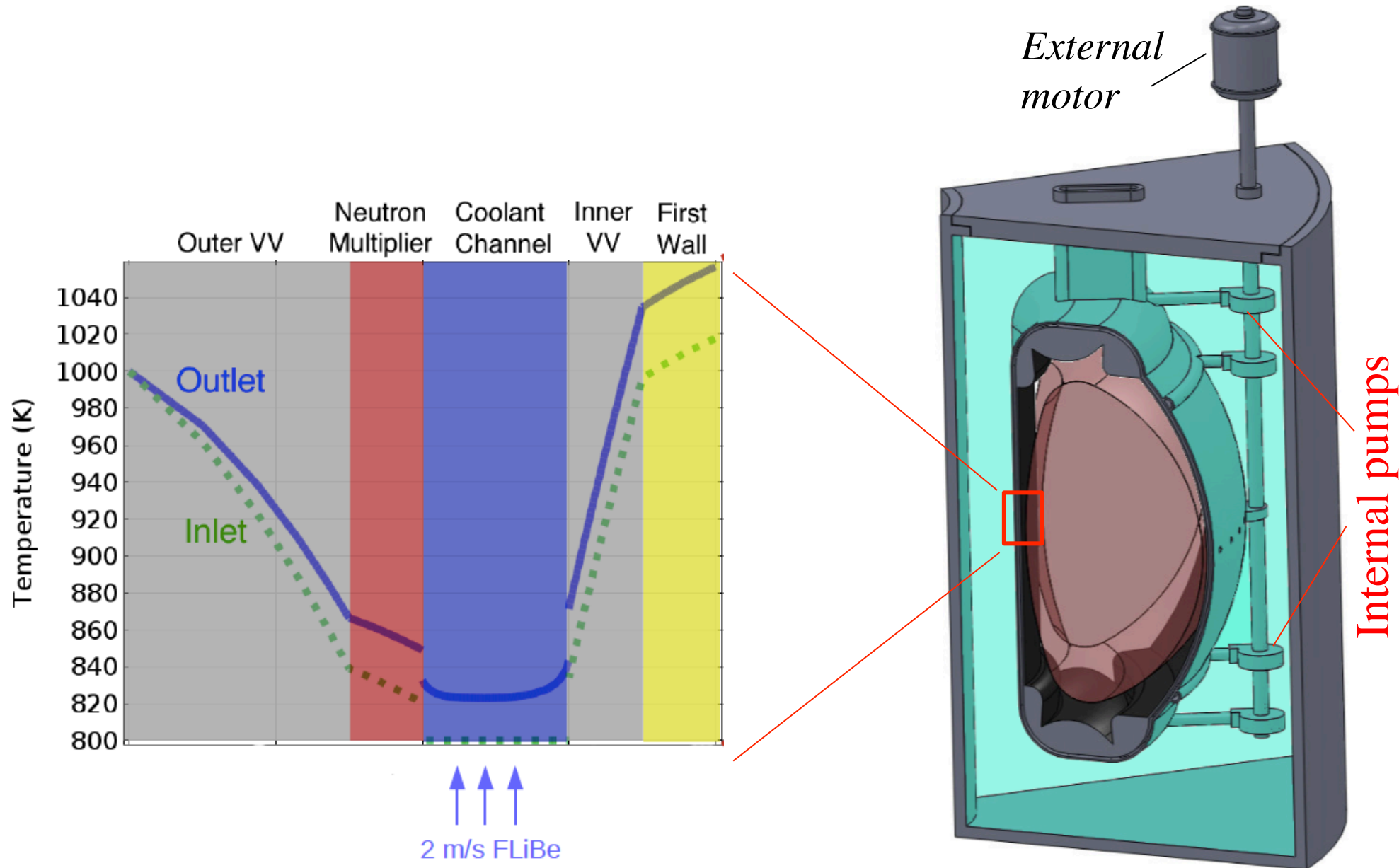
# While in many ways, immersion blanket is ideal (see fission!) it does limit areal access to plasma

- Heating, pumping, diagnostics must wind through supports
- ARC: Total  $\sim 4\text{-}5\text{ m}^2$ 
  - RF heating:  $\sim 1\text{ m}^2$
  - Support:  $\sim 1\text{-}2\text{ m}^2$
  - Pumping  $\sim 0.5\text{ m}^2$
- Tradeoff: more port area vs. TBR, neutron streaming

*Section of toroidal ring:  
Top part of modular core*



# Immersion blanket: Very large heat sink in close proximity to internals provides fundamental improvement in heat exhaust

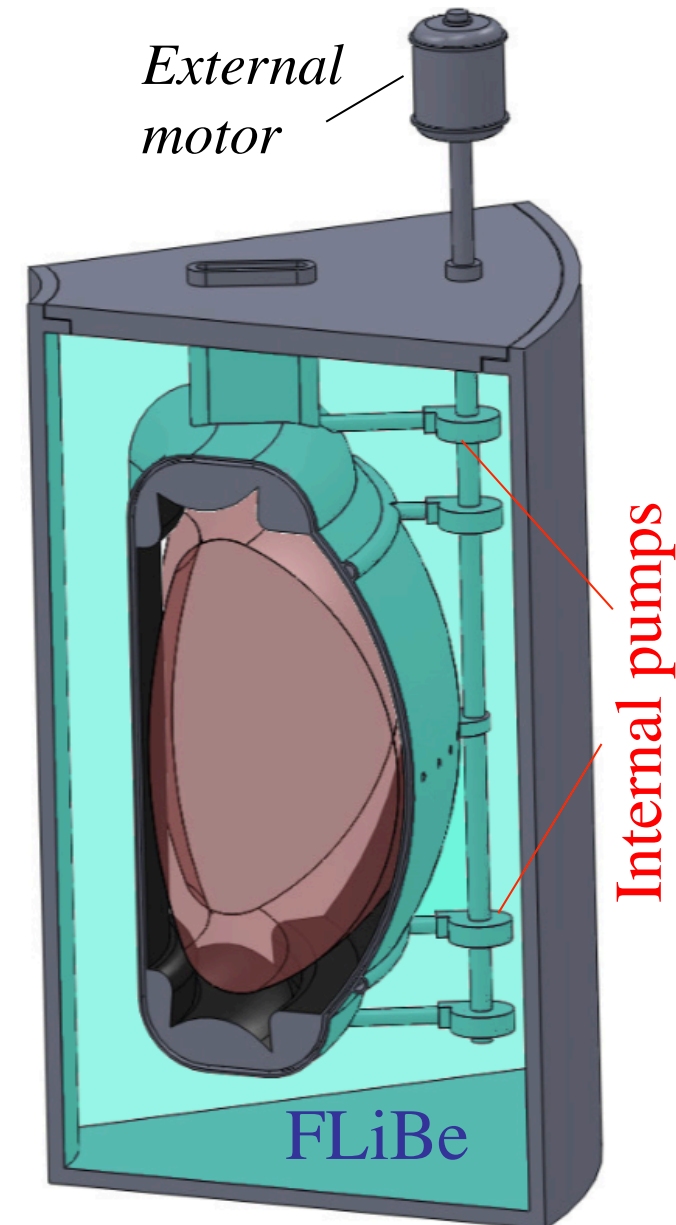


# Immersion blanket: high-T molten salt FLiBe

## Single-phase, low-pressure flow with minimum MHD effects

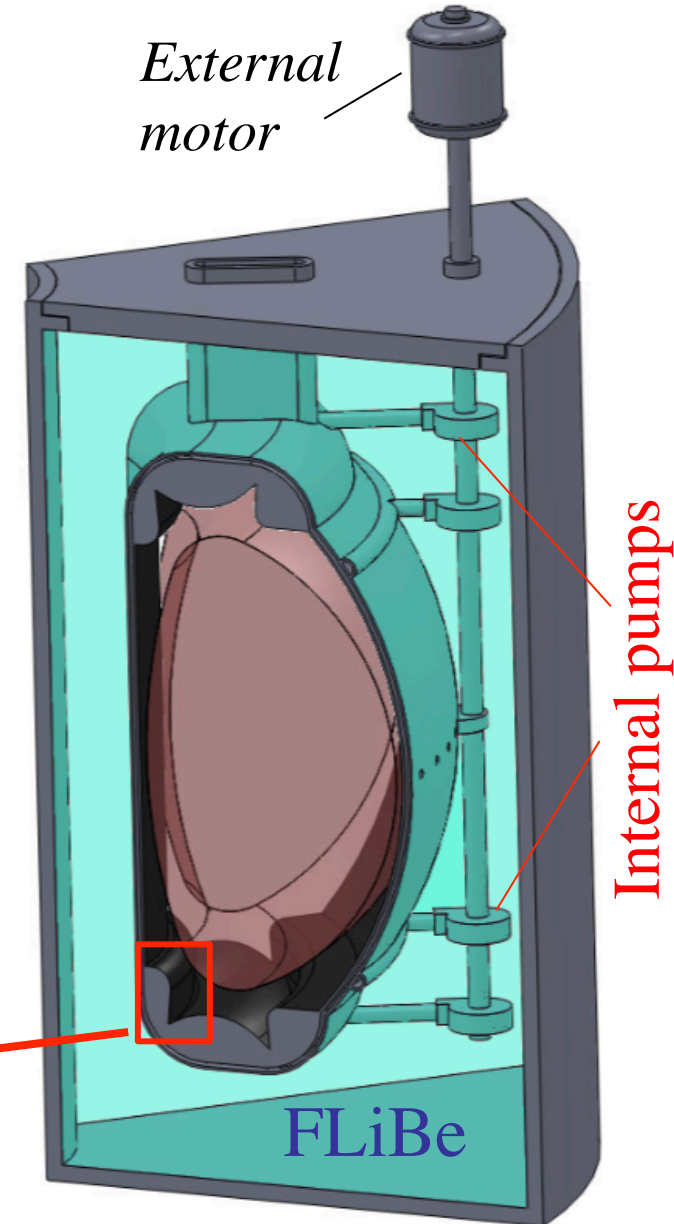
Property	FLiBe [7]	Water
Melting Point (K)	732	273
Boiling Point (K)	1700	373
Density (kg/m <sup>3</sup> )	1940	1000
Specific Heat (kJ/kg/K)	2.4	4.2
Thermal Conductivity (W/m/K)	1	0.58
Viscosity (mPa-s)	6	1

- TBR ~ 1.14
- High thermal efficiency ~ 0.4 - 0.5
- Shielding: ~10 FPY coil lifetime



# Immersion blanket: high-T molten salt FLiBe

## Single-phase, low-pressure flow with minimum MHD effects

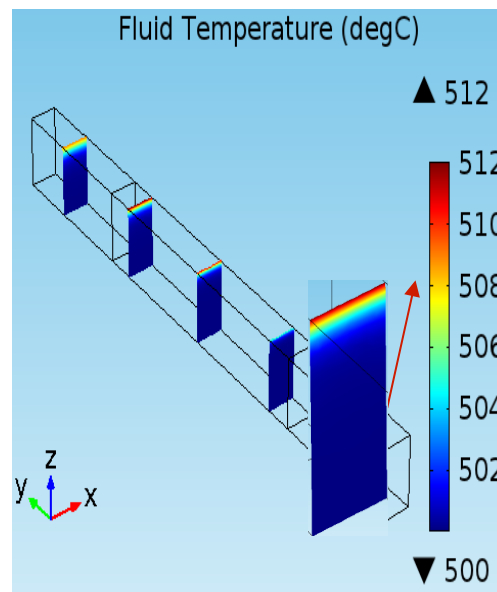
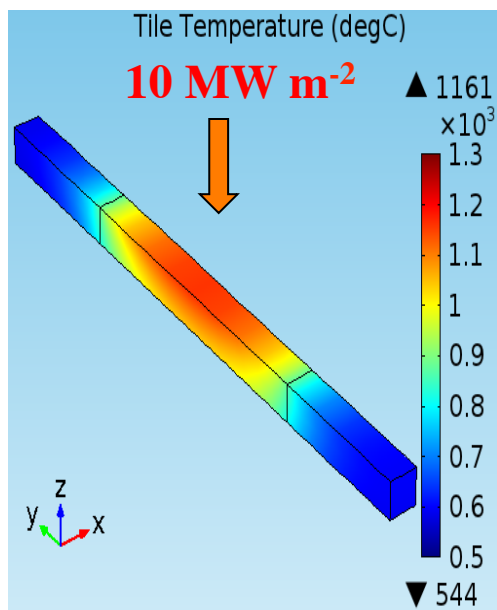
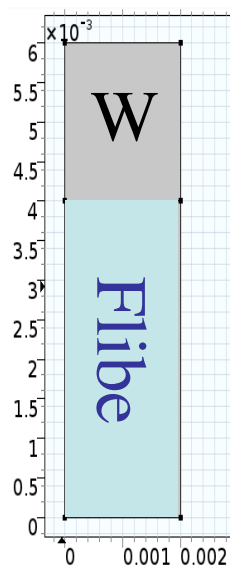


- TBR  $\sim 1.14$
- High thermal efficiency  $\sim 0.4 - 0.5$
- Shielding: 10 full-power coil lifetime
- **Exploit FLiBe + Immersion blanket + Additive manufacturing to address high heat flux regions?**

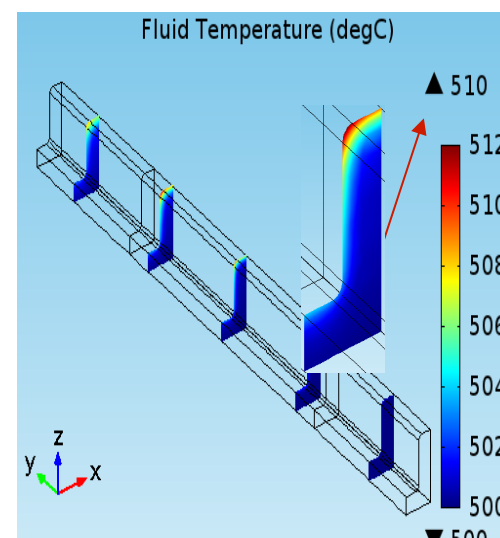
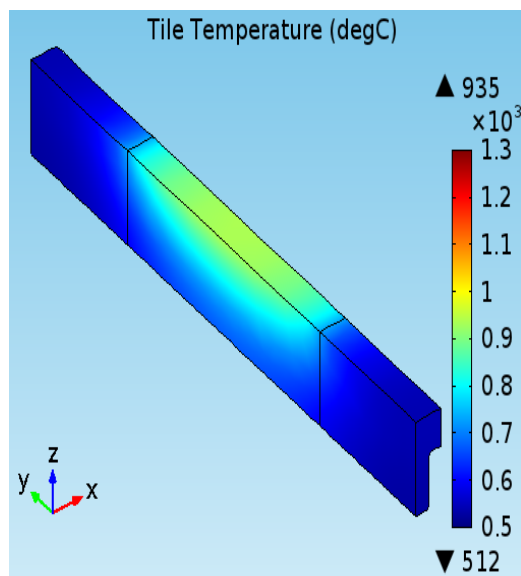
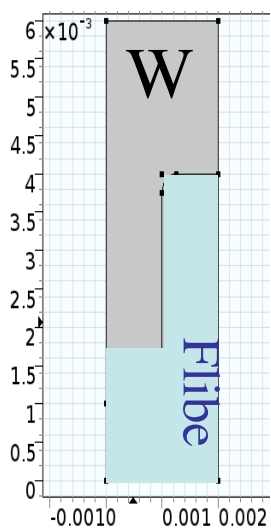
# Preliminary study: Improved surface heat removal with FLiBe + 3-D printed cooling channels

*Next major design study: ARC divertor & cooling*

2 mm thick W tile



2 mm thick W tile + Internal Fin



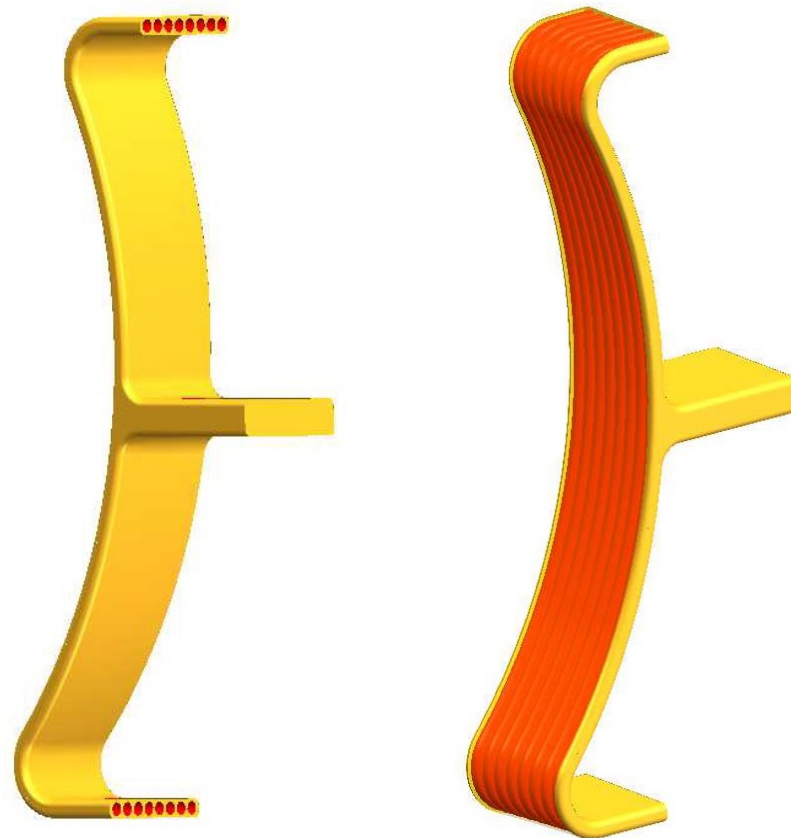
**10 m/s**  
**~ 1 bar pressure drop**

L. Zhou, R. Vieira MIT

# Strong benefits of 3D printing for actively cooled launchers too

## Example RF antennae strap

Integrated, near-surface cooling channels impossible /w standard manufacturing

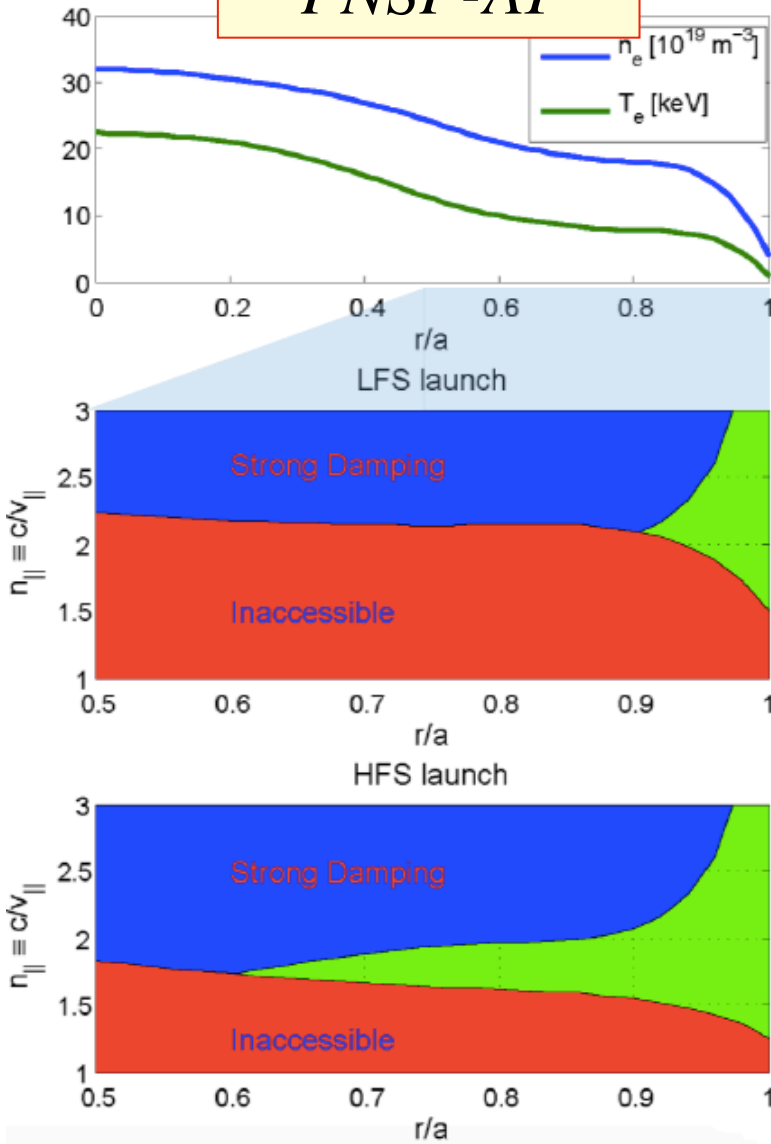


S. Wukitch  
Tue pm  
SO15

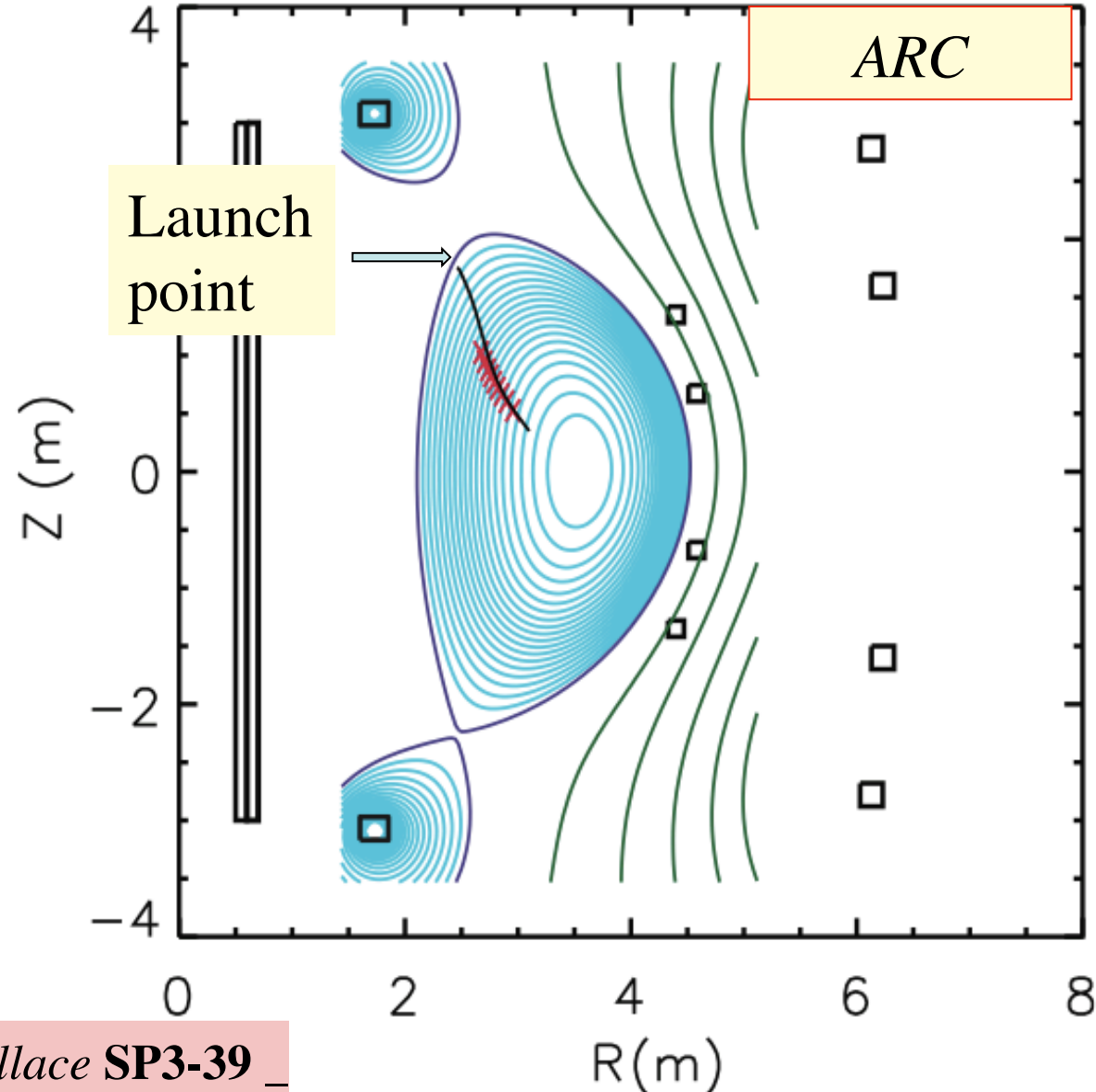
# New technologies provide access to synergistic physics design advantages at high-B and small size:

## High-field side launch $\rightarrow$ + 50% CD efficiency

*FNSF-AT*



*ARC*



Wallace SP3-39



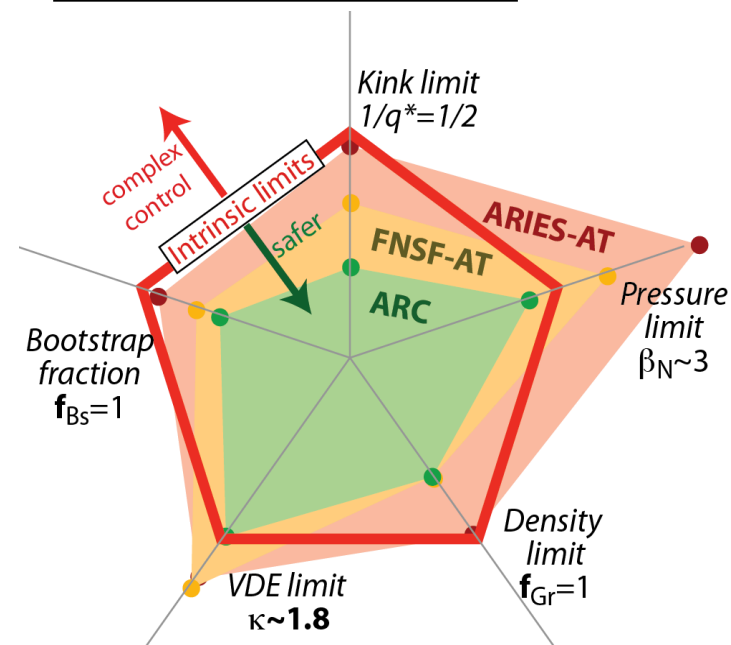
# New technologies provide access to synergistic design advantages at high-B and small size: Robust steady-state far from disruptive limits

	DIII-D	ARIES-AT	ARC
$q_{95}$	6.3	3	7.2
$H_{98}$	1.5	1.7	1.7
$\beta_N$	3.7	5.4	2.6
$G = \beta_N H_{98} / q^2$	0.14	0.90	0.09
$f_{\text{bootstrap}}$	0.65	0.91	0.63
$n / n_{\text{Greenwald}}$	0.5	0.9	0.65

$$\frac{P_{\text{fusion}}}{S_{\text{wall}}} \sim \frac{\beta_N^2 \epsilon^2}{q_*^2} R B^4$$

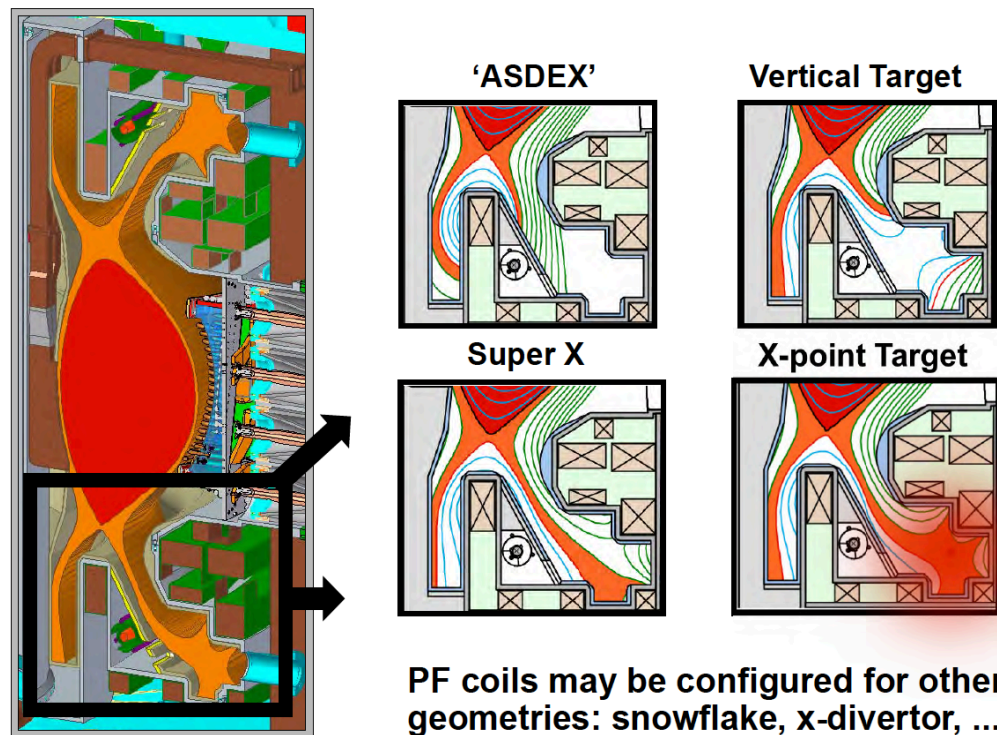
$$nT \tau_E \sim \frac{\beta_N H}{q_*^2} R^{1.3} B^3$$

- **Steady-state scenario using high safety-factor, moderate Beta approach**
- **Scenario ACHIEVED in present moderate-B devices (e.g. DIII-D)**



# Modularity and small size should be enabling to solving critical issue of divertor heat exhaust

- Large linear size, low B unfavorable for heat exhaust
  - At fixed fusion power density, Eich scaling →  $q// \sim R B$
  - Lawson criterion:  $R \sim 1/B^{2.3}$
  - $q// \sim 1 / B^{1.3}$
- Advanced divertor coils built into modular core as replaceable components
  - Exploit physics advances from expanded volume divertors



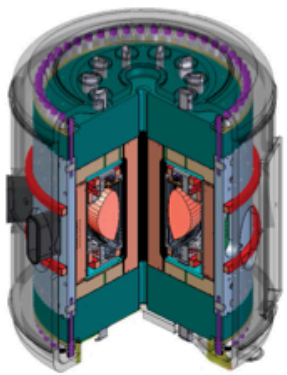
*ADX presentations*

LaBombard SO10-3 Tue AM

Posters: SP3 Tue PM

# Near-term, *small-scale* research can pursue this exciting path for fusion energy

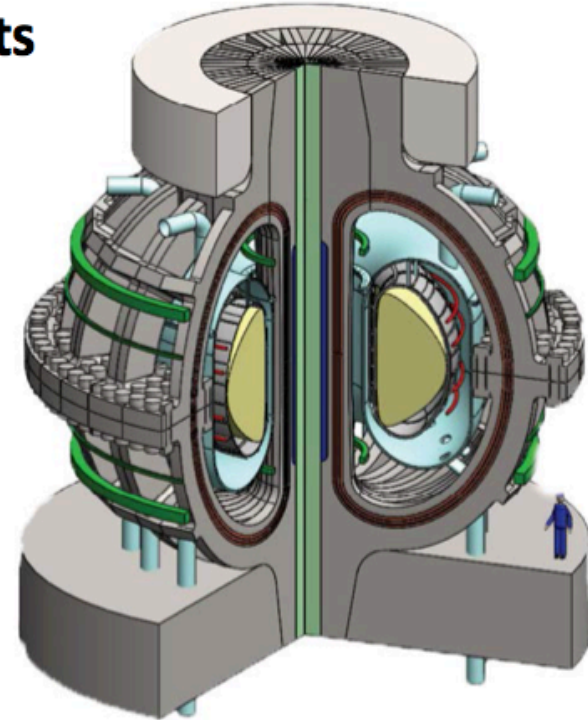
## High-Field, High Power Density Plasma Science Experiments



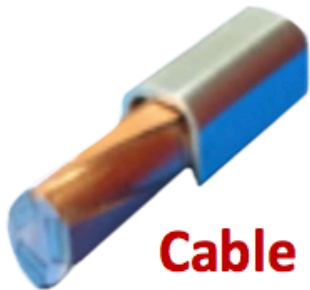
**Alcator  
C-Mod**



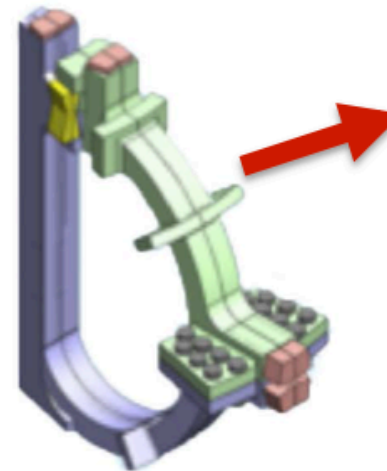
**ADX**



**ARC**



**Cable**

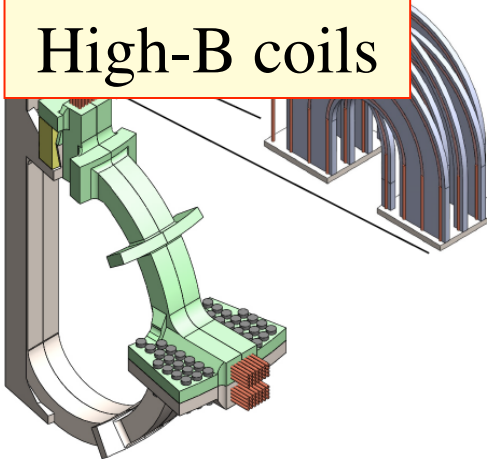


**Magnet  
Assembly**

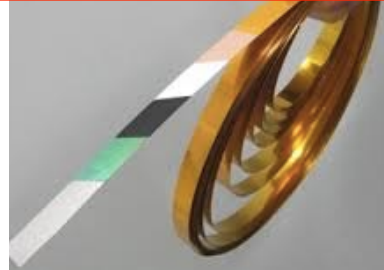
## High-Field Superconducting Magnet Development

# The disruptive innovation of high field, high-T superconductors

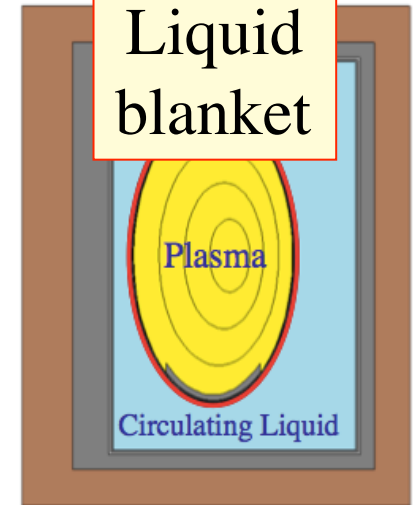
Demountable High-B coils



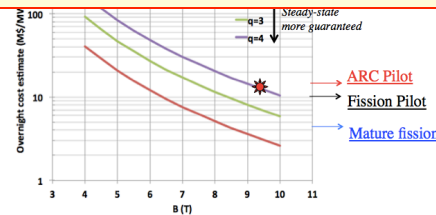
Superconductor



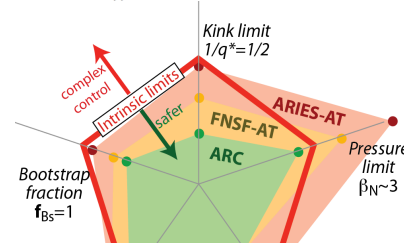
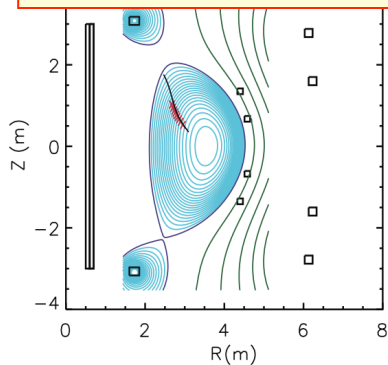
Liquid blanket



Smaller, sooner Viable fusion energy



Steady-state



Operation robustness

Small & Modular



# Summary

- Fusion is hard ...as a community we need to be continually looking for both technology and science innovations that will accelerate fusion's development
- Exciting technology opportunities recently available:  
High-temperature, high-field superconductors  
Additive manufacturing
- Conceptual reactor design shown here give a sense of technology limits and integrated effects on magnetic fusion...  
those effects appear to be positive and revolutionary
- **The near-term pace of fusion science development will also be accelerated by exploiting these technologies**