

April 30, 2020

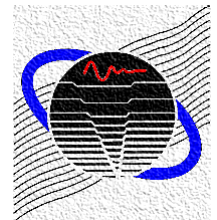
# Sound Absorptive Materials Basics and Future Trends

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Vibro-Acoustics Consortium Web Meeting  
University of Kentucky

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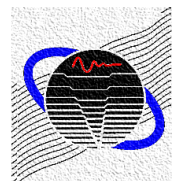
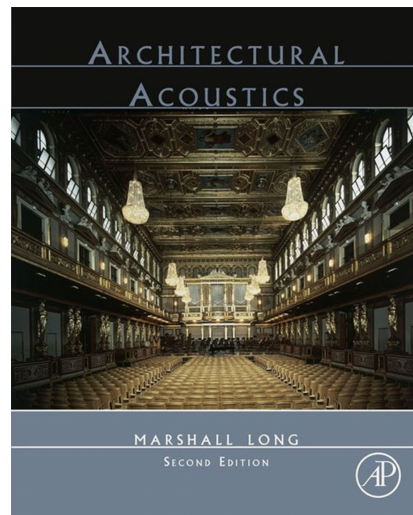
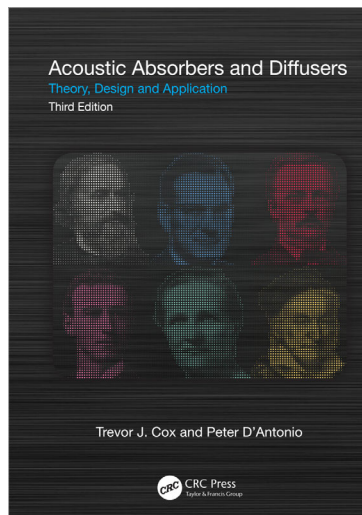
**Vibro-Acoustics Consortium**



# References

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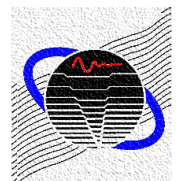
1. T. J. Cox and P. D'Antonio, *Acoustic Absorbers and Diffusers: Theory, Design and Application*, 3<sup>rd</sup> Edition, CRC Press, Boca Raton, FL (2017).
2. M. Long, *Architectural Acoustics*, 2<sup>nd</sup> Edition, Elsevier, Kidlington, Oxford (2014).



# Overview

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- [Porous Absorbers Overview](#)
- [Porous Absorbers Property Determination](#)
- [Porous Absorbers Basics for Designers](#)
- [Porous Absorbers Compressed](#)
- [Porous Absorbers Layered](#)
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- [Reactive Absorbers Example](#)



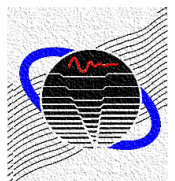
# Porous Absorbers Overview

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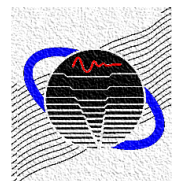
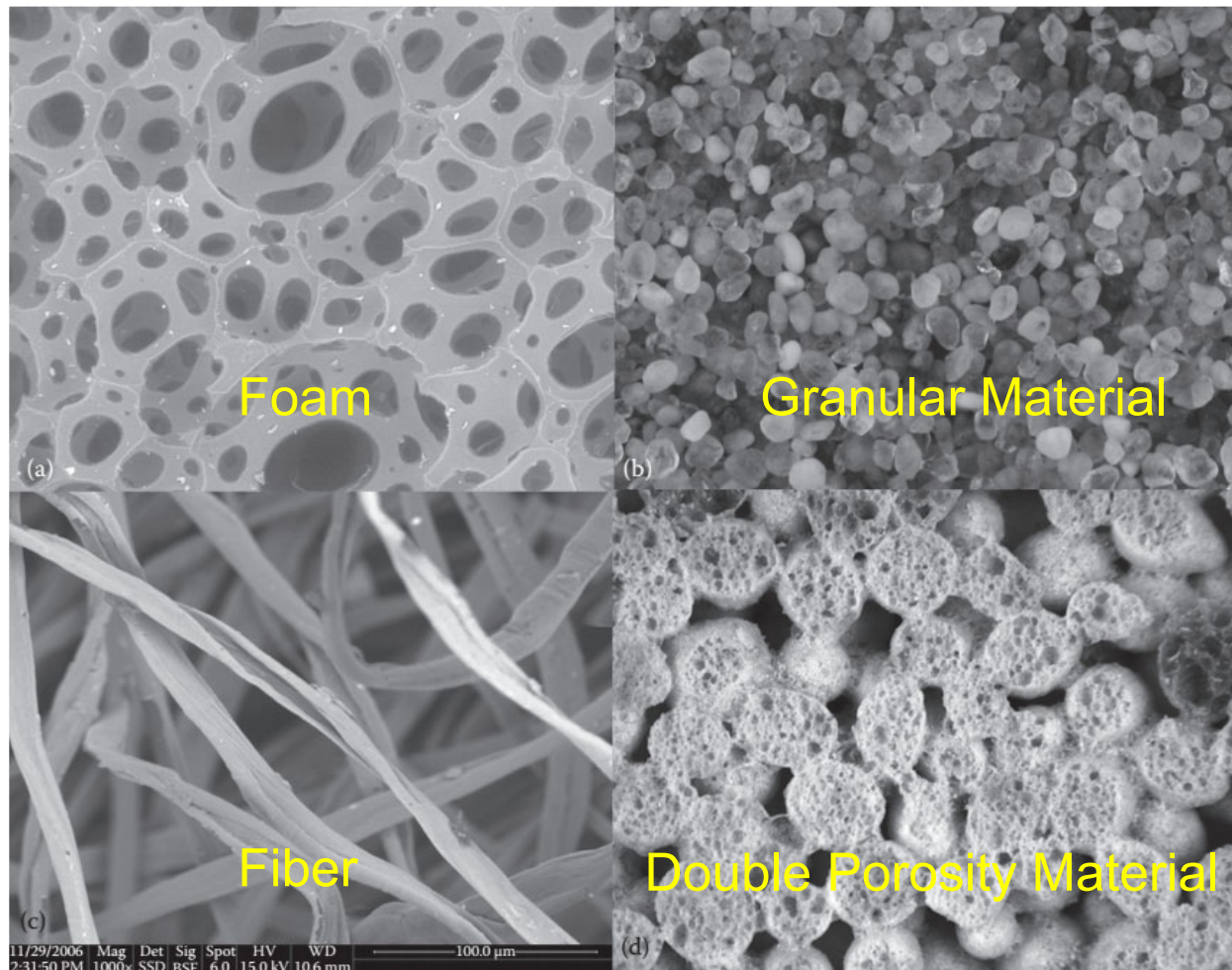
Sound is “absorbed” by converting sound energy to heat within the material, resulting in a reduction of the sound pressure.

Two primary mechanisms:

- vibration of the material skeleton - damping
- friction of the fluid on the skeleton - viscosity



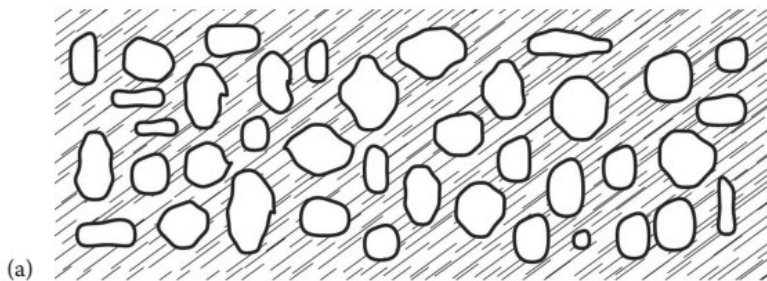
# Porous Absorbers Overview



# Porous Absorbers Overview

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- Foams are made of various materials including polyurethane, polyethylene, and polypropylene.
- Foams are created by a process that has been likened to bread rising.

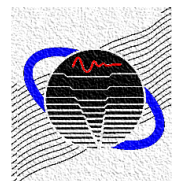


Closed Cell Foam



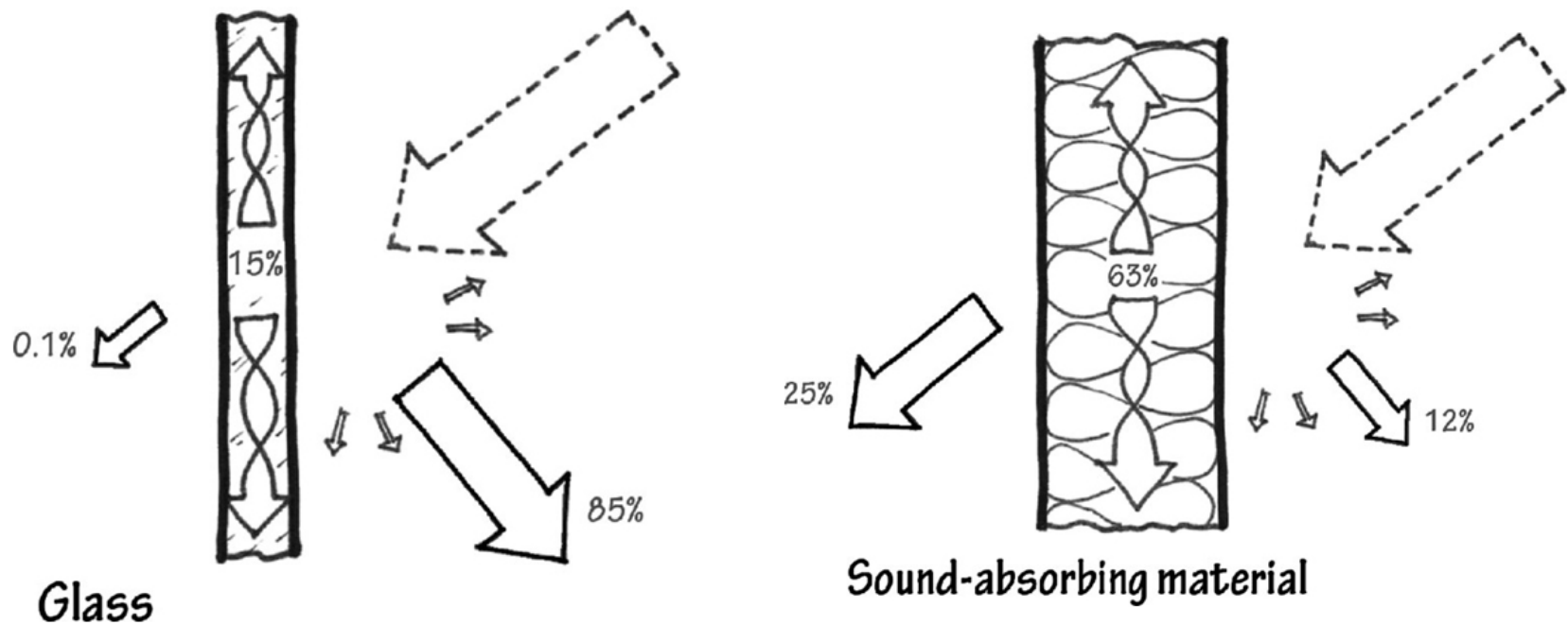
Open Cell Foam

T. J. Cox and P. D'Antonio, 2017 adapted from Cremer and Mueller, 1978



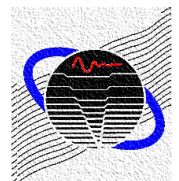
# Porous Absorbers Overview

Sound energy is converted to heat via damping or viscosity.



Ermann, 2015

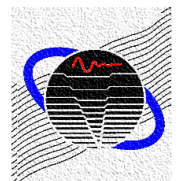
Vibro-Acoustics Consortium



# Overview

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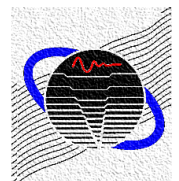
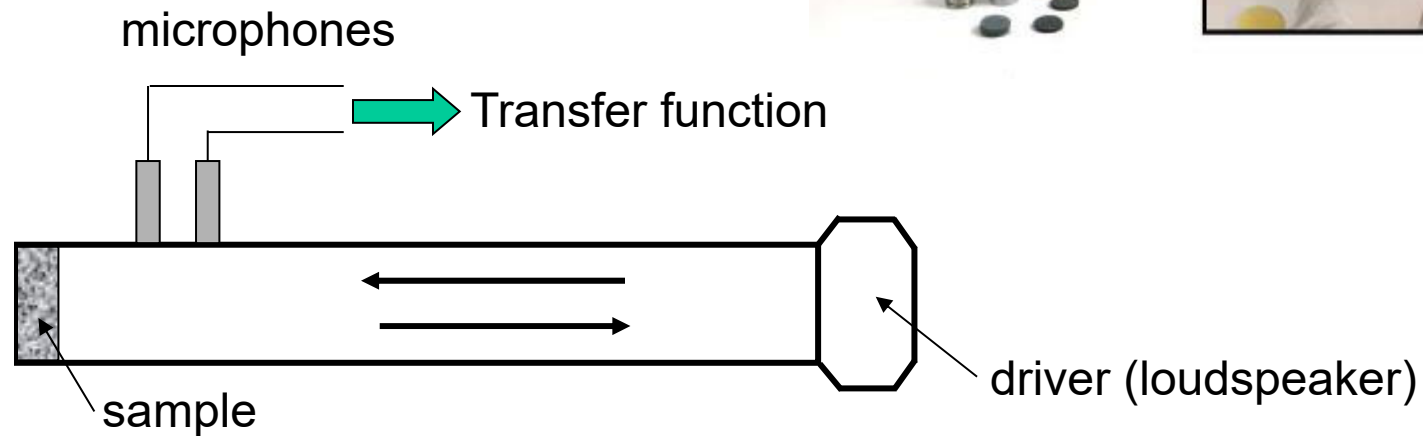
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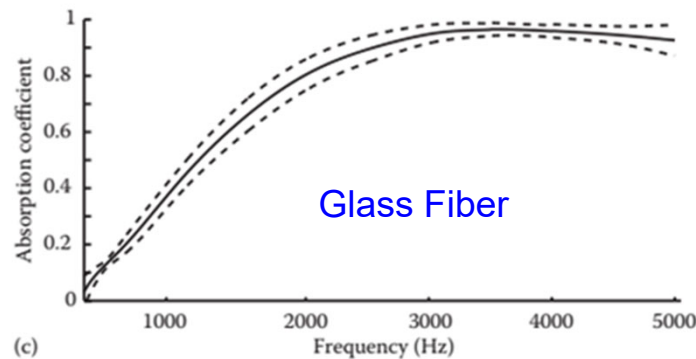
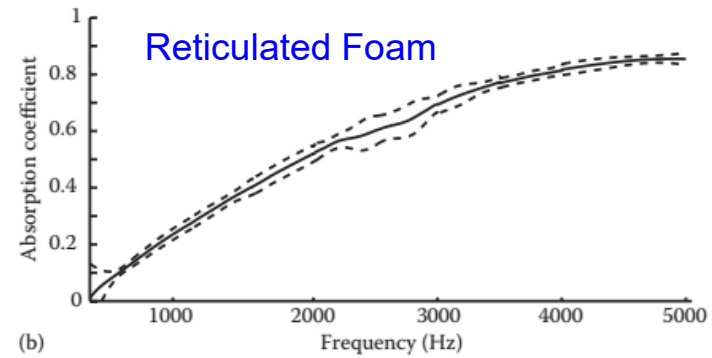
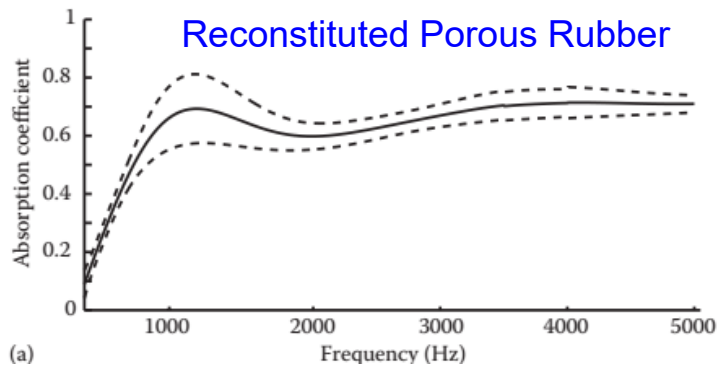
# Porous Absorbers Property Determination

ASTM E1050 – Normal Incident Sound Absorption



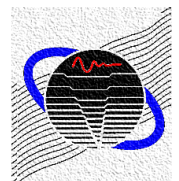
# Porous Absorbers Property Determination

## ASTM E1050



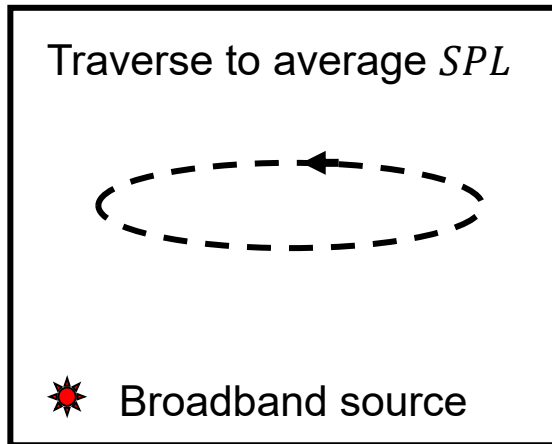
Solid line indicates the mean sound absorption. Error bars indicate the 95% confidence limit in any one laboratory based on round robin tests.

Cox and D'Antonio, 2017 adapted from Horoshenkov et al., 2007

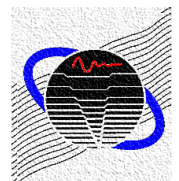
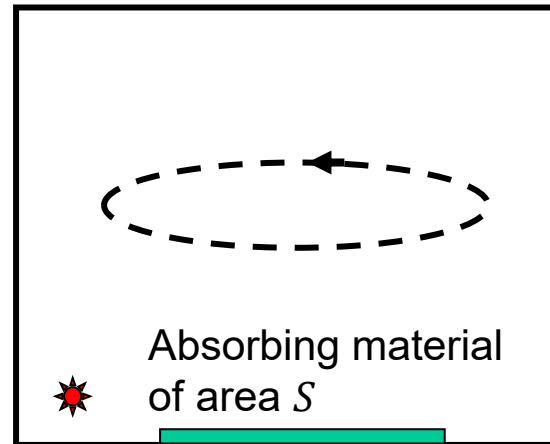


# Porous Absorbers Property Determination

ASTM C423 – Diffuse Field Sound Absorption

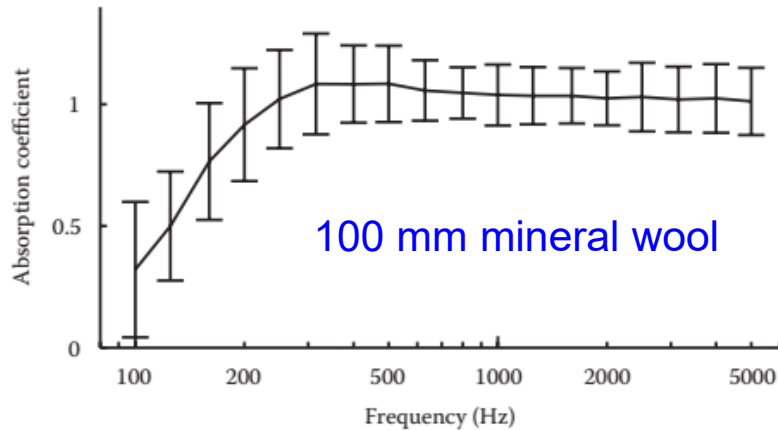


Reverberation Room

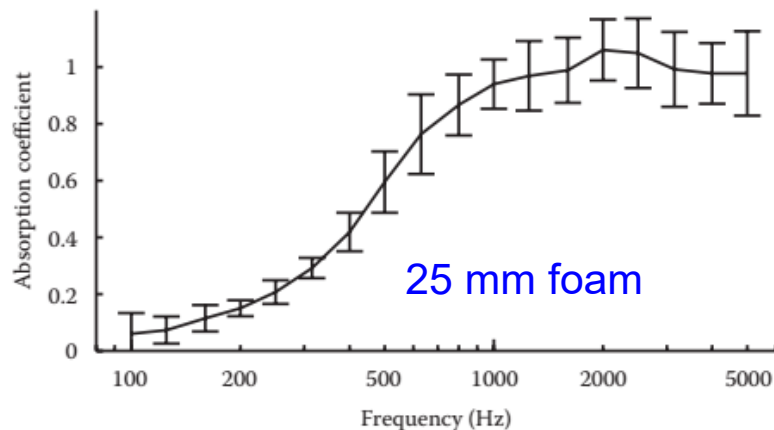


# Porous Absorbers Property Determination

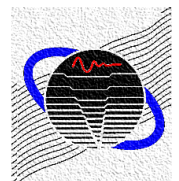
## ASTM C423



Solid line indicates the mean sound absorption. Error bars indicate the 95% confidence limit in any one laboratory measurement on round robin tests (13 laboratories).

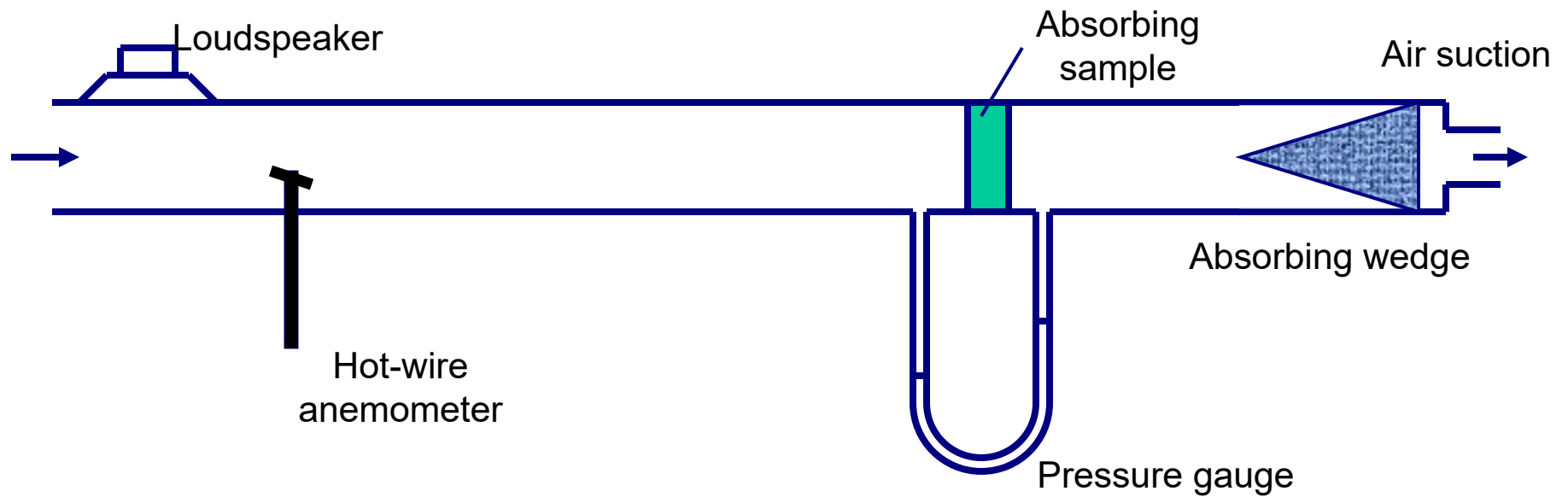


Cox and D'Antonio, 2017 adapted from Horoshenkov et al., 2007

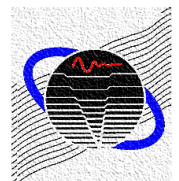


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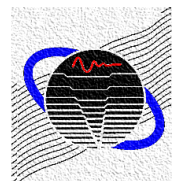
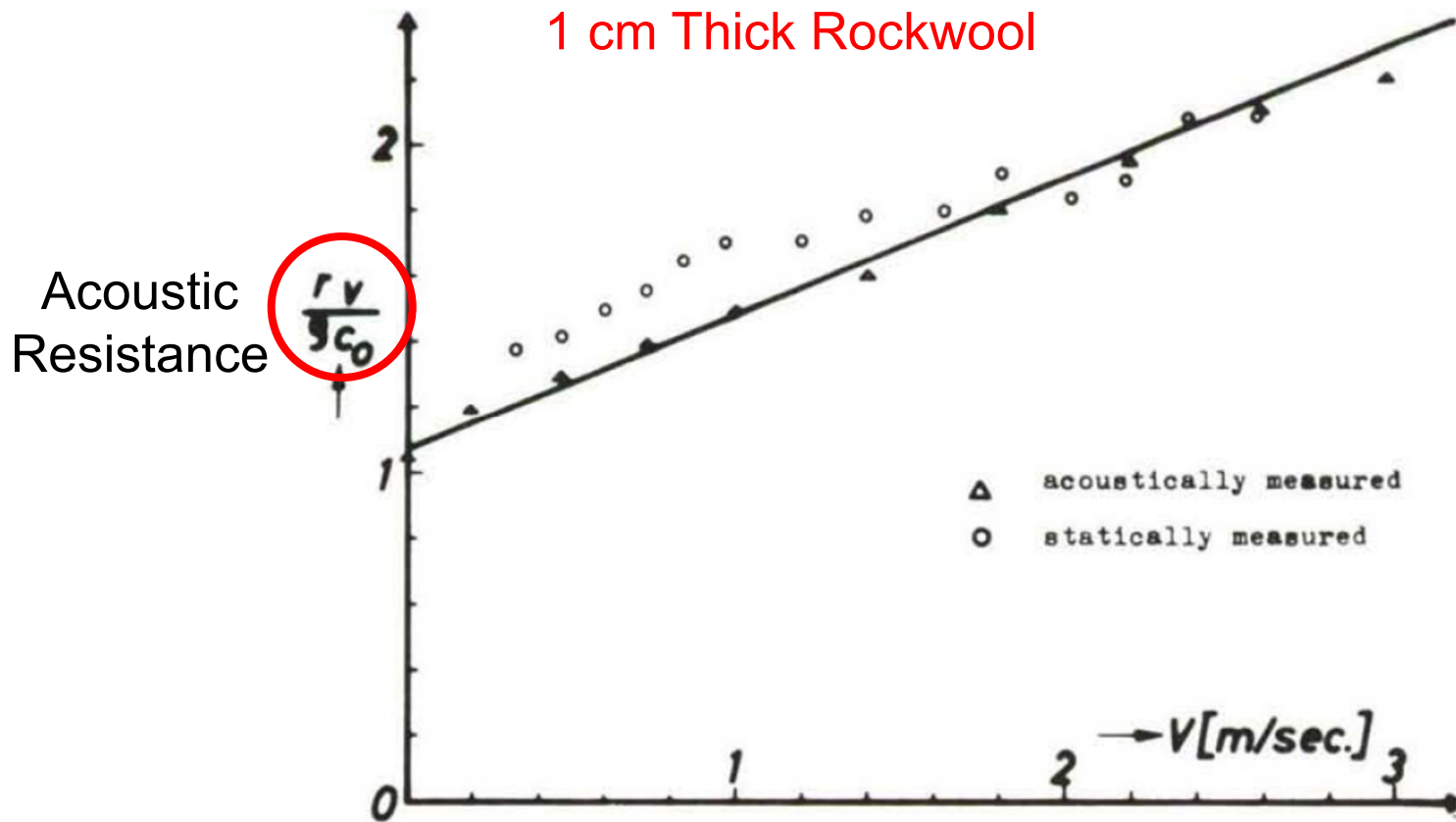
## Wright-Patterson AFB Study



Classic study where both the static and acoustic impedance were measured.

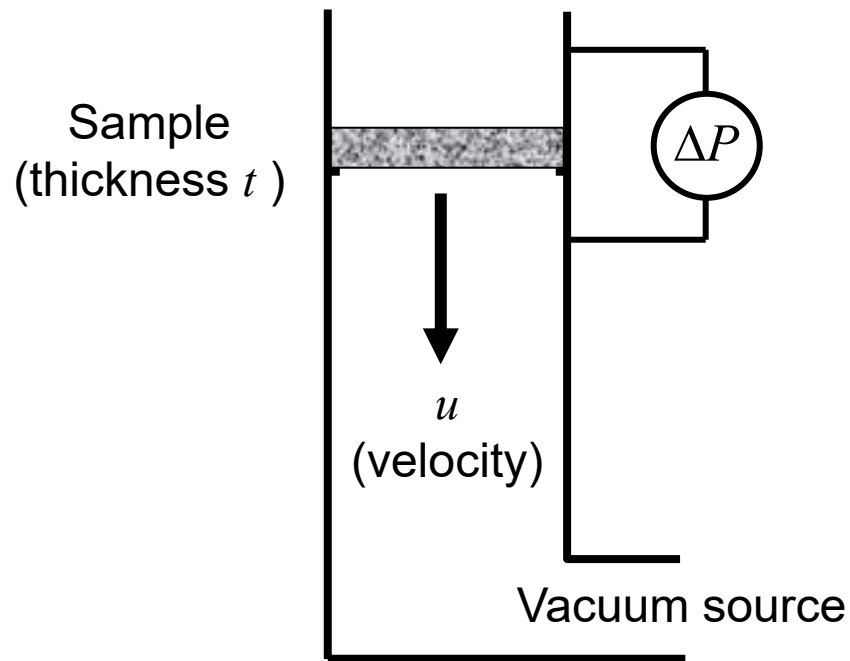


# Porous Absorbers Property Determination



# Porous Absorbers Property Determination

Standardized in ASTM C522

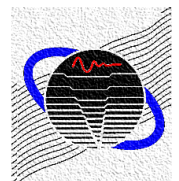


Flow resistance:

$$r_s = \frac{\Delta P}{u}$$

Flow resistivity:

$$\sigma = \frac{r_s}{t}$$



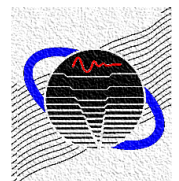
# Porous Absorbers Property Determination

Characteristic Impedance  $Z_m = \rho c(1 + C_1 X^{-C_2} - jC_3 X^{-C_4})$

$$X = \frac{\rho f}{\sigma}$$

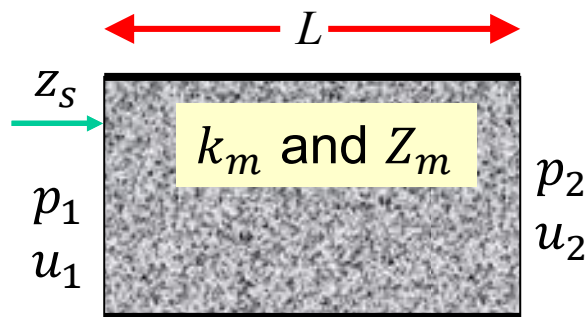
Complex Wavenumber  $k_m = \frac{\omega}{c}(1 + C_5 X^{-C_6} - jC_7 X^{-C_8})$

Material Type Reference	$C_1$	$C_2$	$C_3$	$C_4$	$C_5$	$C_6$	$C_7$	$C_8$
Rockwool/fiberglass Delaney and Bazley (1970)	0.0571	0.754	0.087	0.732	0.0978	0.700	0.189	0.595
Rockwool/fiberglass Miki (1989)	0.070	0.632	0.107	0.632	0.109	0.618	0.160	0.618
Polyester Garai and Pompoli (2005)	0.078	0.623	0.074	0.660	0.159	0.571	0.121	0.530
Polyurethane foam of low flow resistivity Dunn and Davern (1986)	0.114	0.369	0.0985	0.758	0.168	0.715	0.136	0.491
Porous plastic foams of medium flow resistivity Wu (1988)	0.209	0.548	0.105	0.607	0.188	0.554	0.163	0.592
Fiber Mechel (2002)								
$X > 0.025$	0.081	0.699	0.191	0.556	0.136	0.641	0.322	0.502
$X < 0.025$	0.0563	0.725	0.127	0.655	0.103	0.716	0.179	0.663





# Porous Absorbers Property Determination



$$k_m = \frac{\omega}{c'}$$

$$Z_m = \rho' c'$$

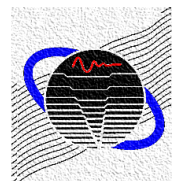
## Determination of Sound Absorption

$$\begin{Bmatrix} p_1 \\ u_1 \end{Bmatrix} = \begin{bmatrix} \cos(k_m L) & jZ_m \sin(k_m L) \\ j/Z_m \sin(k_m L) & \cos(k_m L) \end{bmatrix} \begin{Bmatrix} p_2 \\ u_2 \end{Bmatrix}$$

$$\rightarrow z_s = \frac{p_1}{u_1} = -jZ_m \cot(k_m L)$$

$$R = \frac{z_s - \rho c}{z_s + \rho c}$$

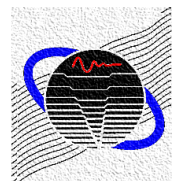
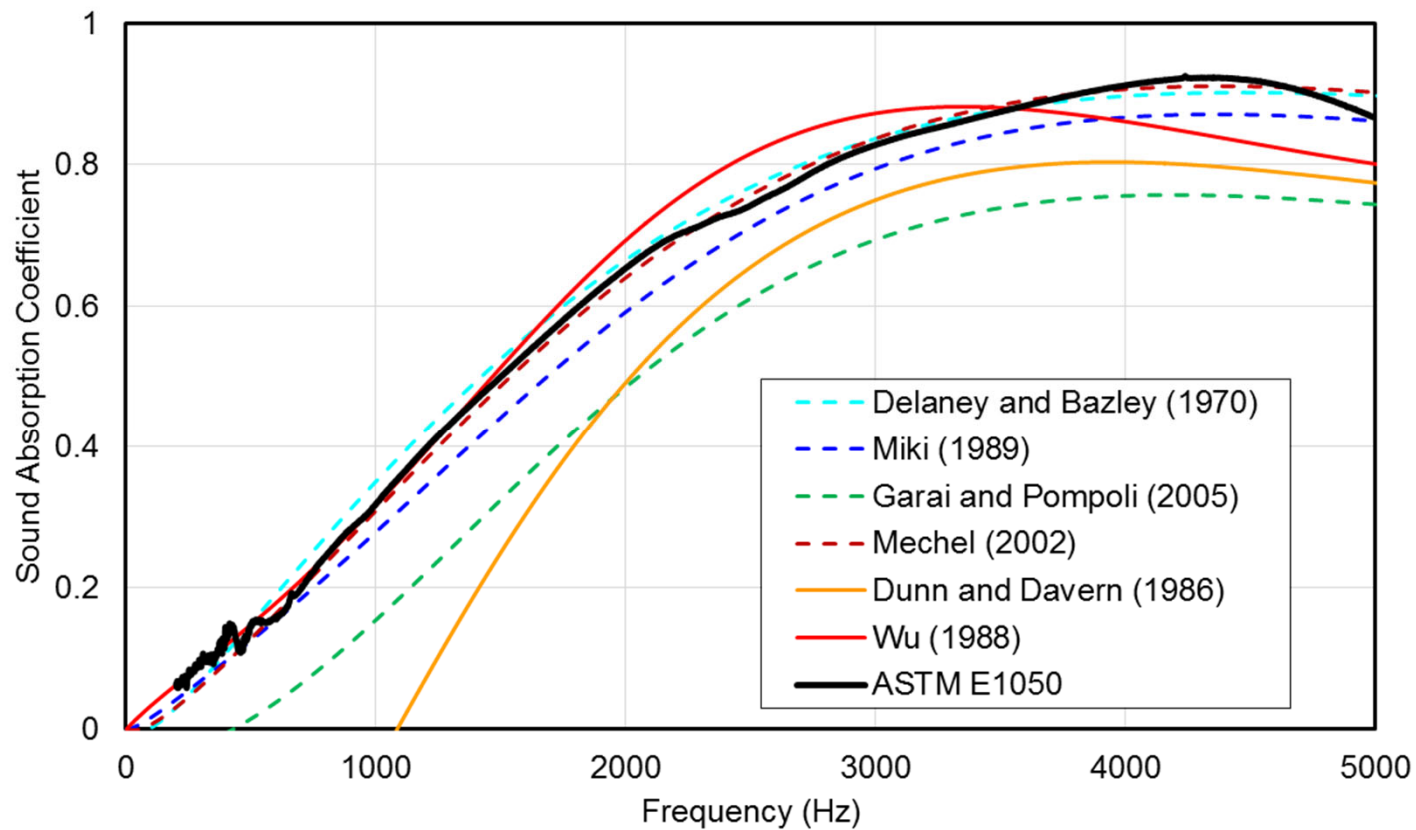
$$\rightarrow \alpha = 1 - |R|^2$$



# Porous Absorbers Property Determination

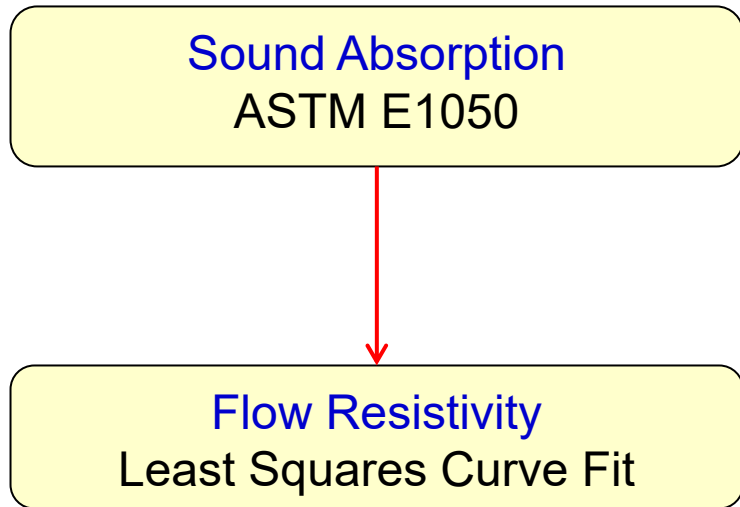
## Empirical Model Comparison

24 mm Melamine Foam (8400 Rays/m)

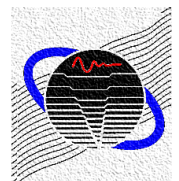


# Porous Absorbers Property Determination

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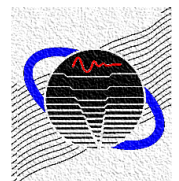
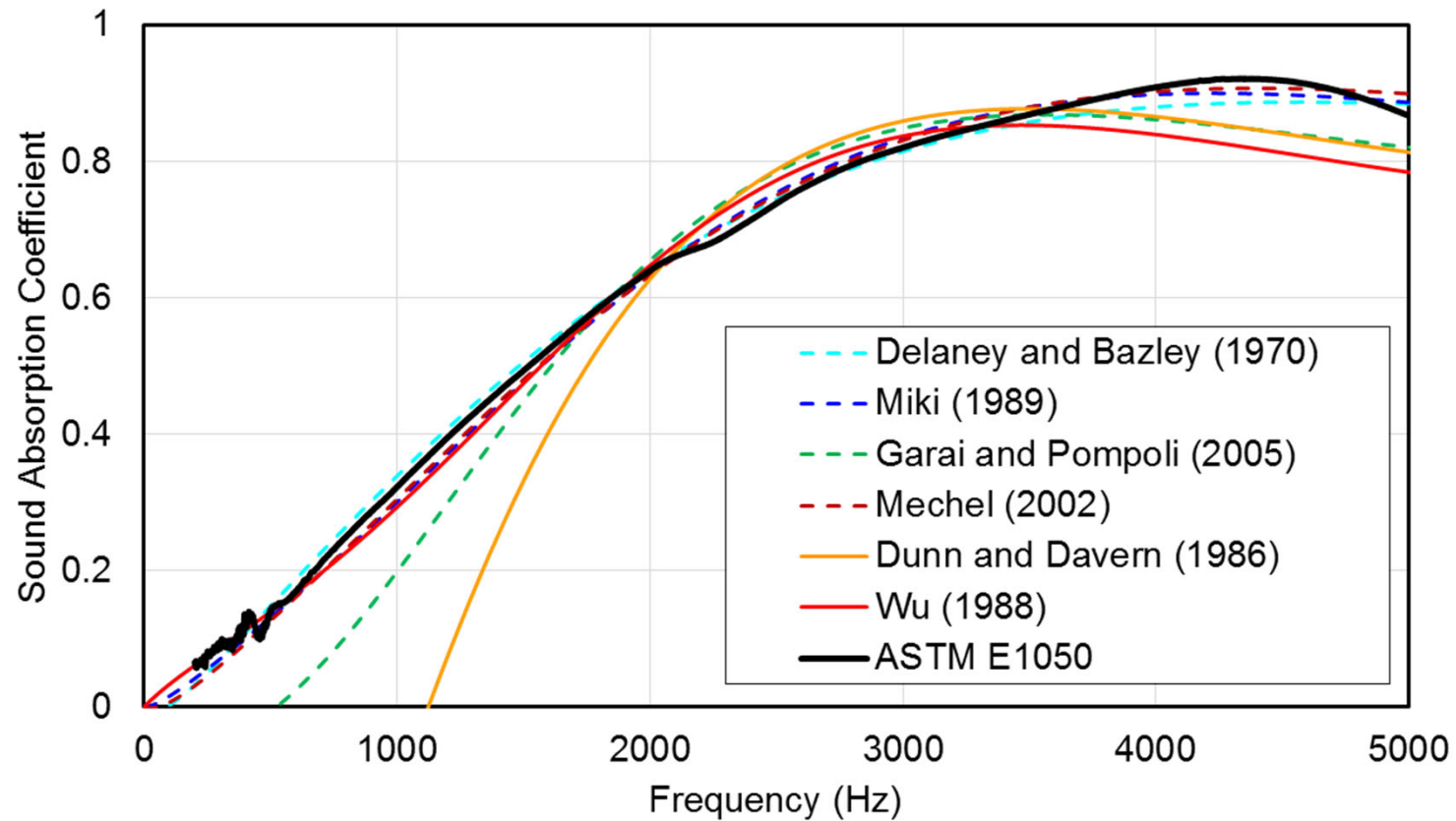
Based on Simón, Fernandez and Pfretzschner, 2006



# Porous Absorbers Property Determination

## Curve Fit Comparison

24 mm Melamine (8400 Rays/m)



# Porous Absorbers Property Determination

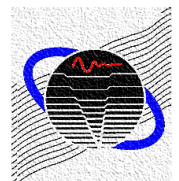
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## Champoux-Allard Model

- Flow Resistivity
- Porosity
- Tortuosity
- Viscous Characteristic Length
- Thermal Characteristic Length

## Johnson-Champoux-Allard Model

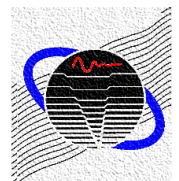
- Flow Resistivity
- Porosity
- Tortuosity
- Viscous Characteristic Length
- Thermal Characteristic Length
- Static Thermal Permeability
- Static Viscous Permeability



# Porous Absorbers Property Determination

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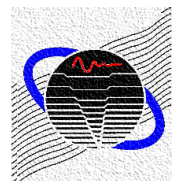
Regardless of whether the simple flow resistivity or the more advanced phenomenological models are used, impedance tube measurements are performed, and some material properties are determined via curve fit. Once materials become compressed, which is frequently the case, all bets are off. Hence, we have tended to use the simple flow resistivity models and have had satisfactory results.



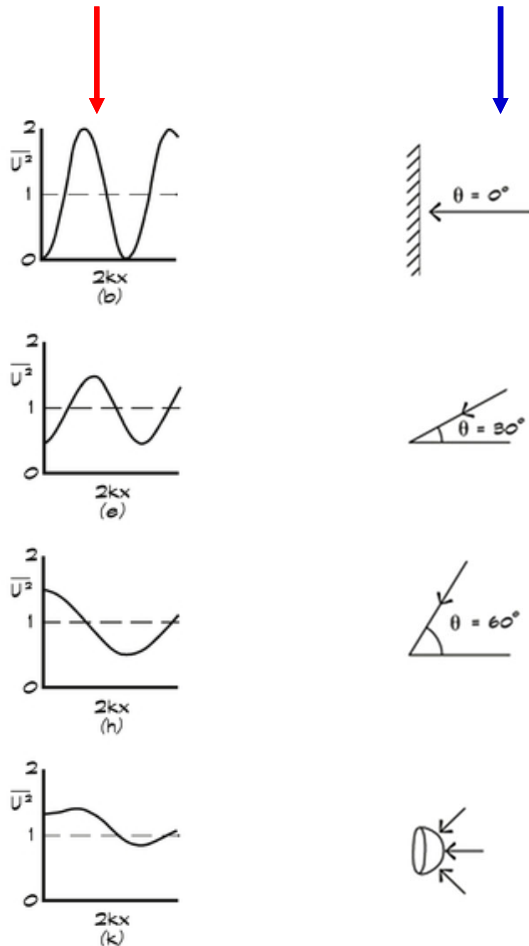
# Overview

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- Reactive Absorbers Overview
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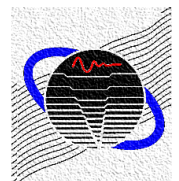
# Porous Absorbers Basics for Designers



## Takeaways

- Porous sound absorption is less effective at low frequencies because of the long wavelength, small particle velocity, and non-diffuse field.
- Relatively thin sound absorption will have some impact even at lower frequencies if the sound field is diffuse.

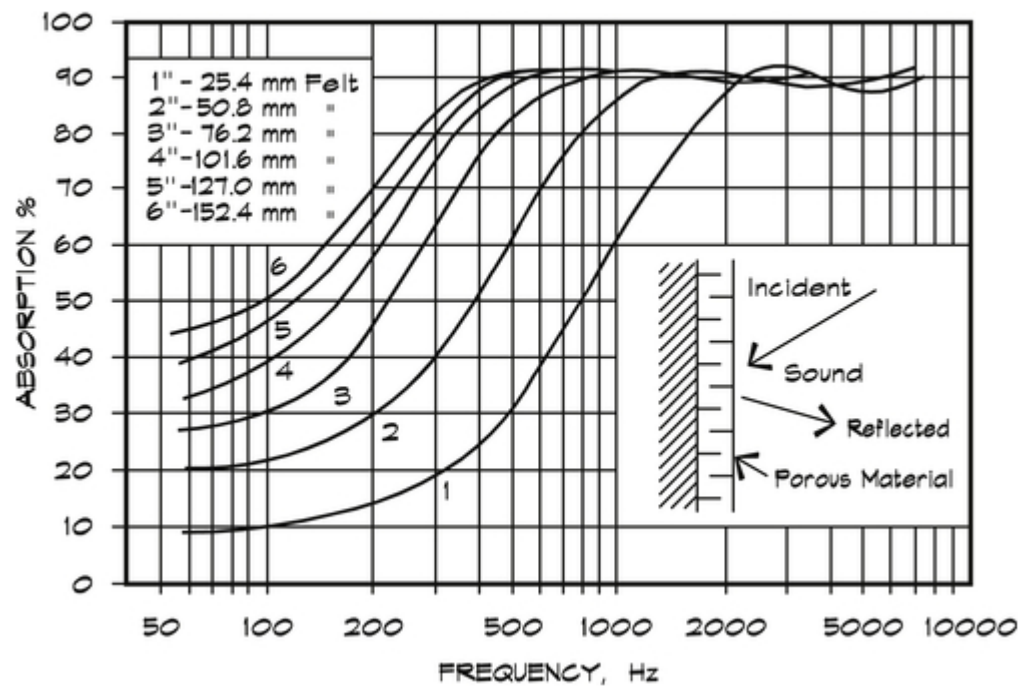
Long, 2014



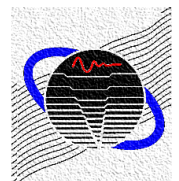


# Porous Absorbers Basics for Designers

## Measured Diffuse Field Sound Absorption

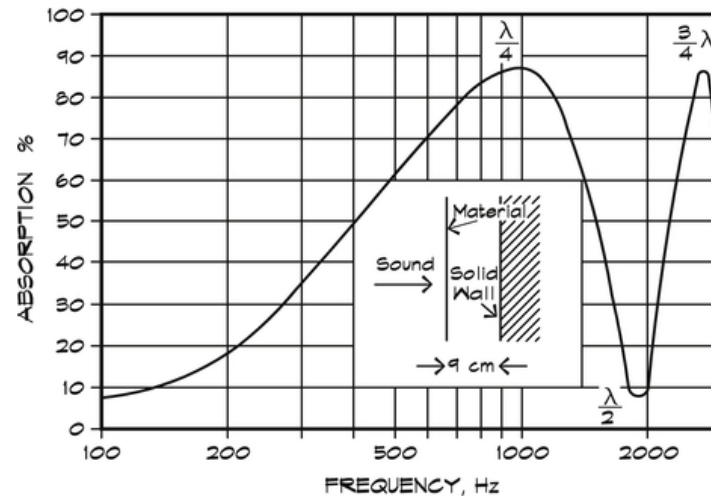


Ginn, 1978 (Reproduced by Long, 2014)

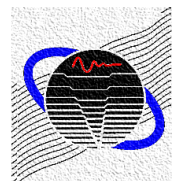


# Porous Absorbers Basics for Designers

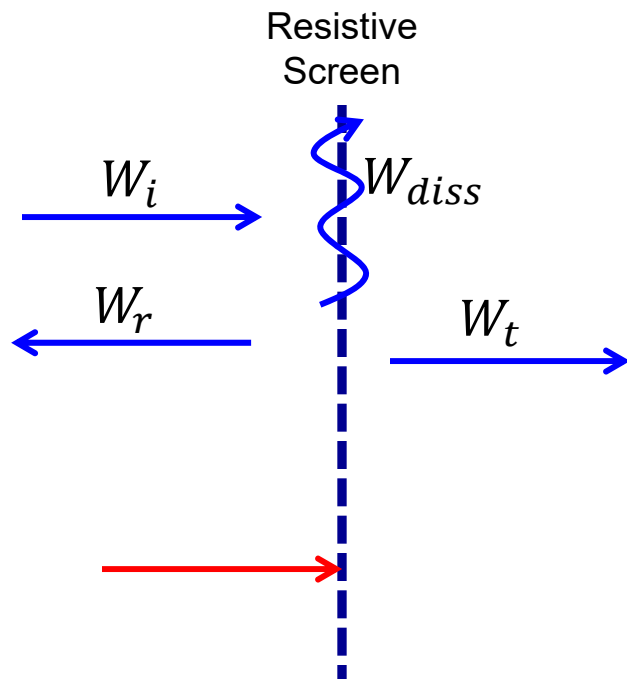
Thin layer with flow resistance  $\sigma_r t$  where  $\sigma_r$  is the flow resistivity and  $t$  is the thickness.



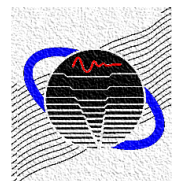
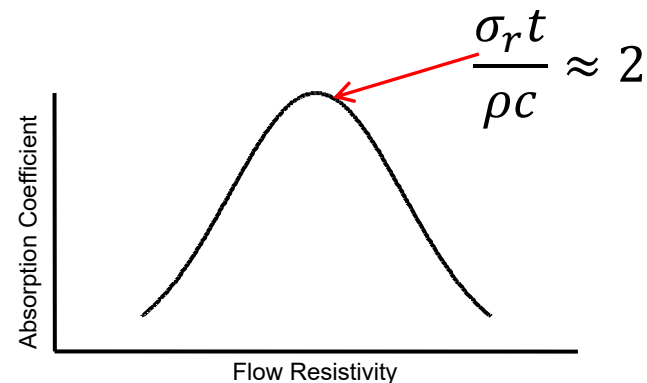
Long, 2014 based on Ginn, 1978



# Porous Absorbers Basics for Designers

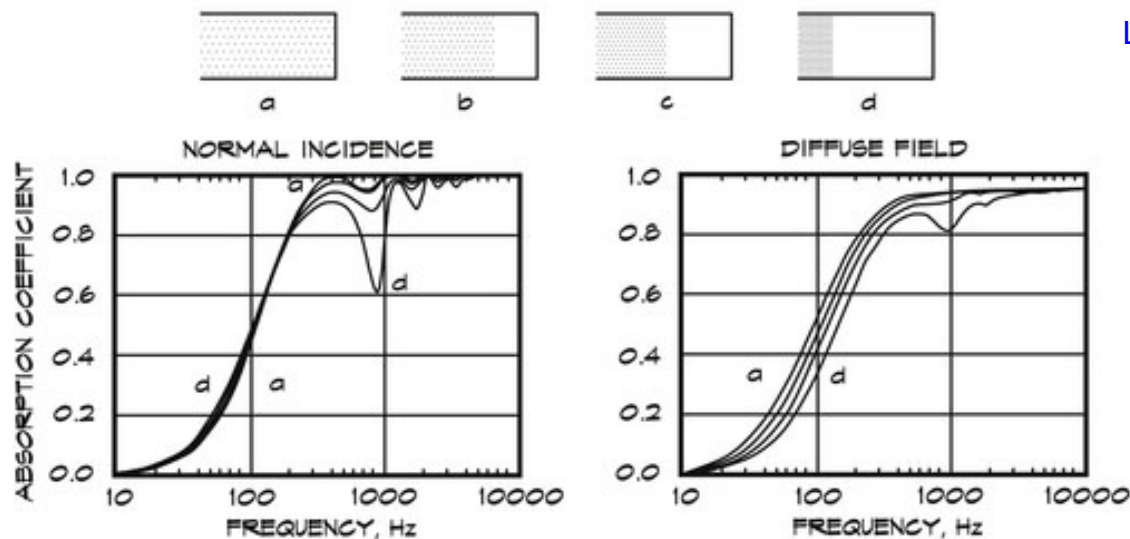


In theory, the dissipated power ( $W_{diss}$ ) is a maximum when  $\sigma_r t = 2\rho c$ . A general rule of thumb is that a sound absorber will be effective when  $\sigma_r t \approx n\rho c$  where  $n$  is on the order of 2. This assumes that the acoustic resistance is equal to the static flow resistance.



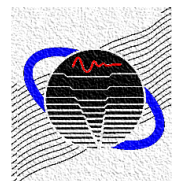
# Porous Absorbers Basics for Designers

Thin layer with flow resistance  $\sigma_r t$  where  $\sigma_r$  is the flow resistivity and  $t$  is the thickness.



Long, 2014 based on Ingard, 1994

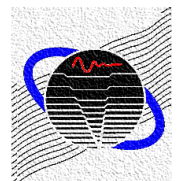
$$\sigma_r t = 2\rho c \text{ for each case}$$



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# Porous Absorbers Compressed

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24 mm  
Melamine Foam

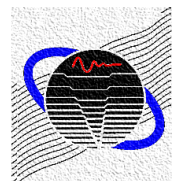
28.5 mm  
Polyurethane Foam



50.8 mm  
Glass Wool Fiber



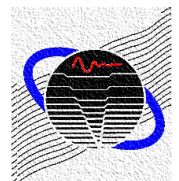
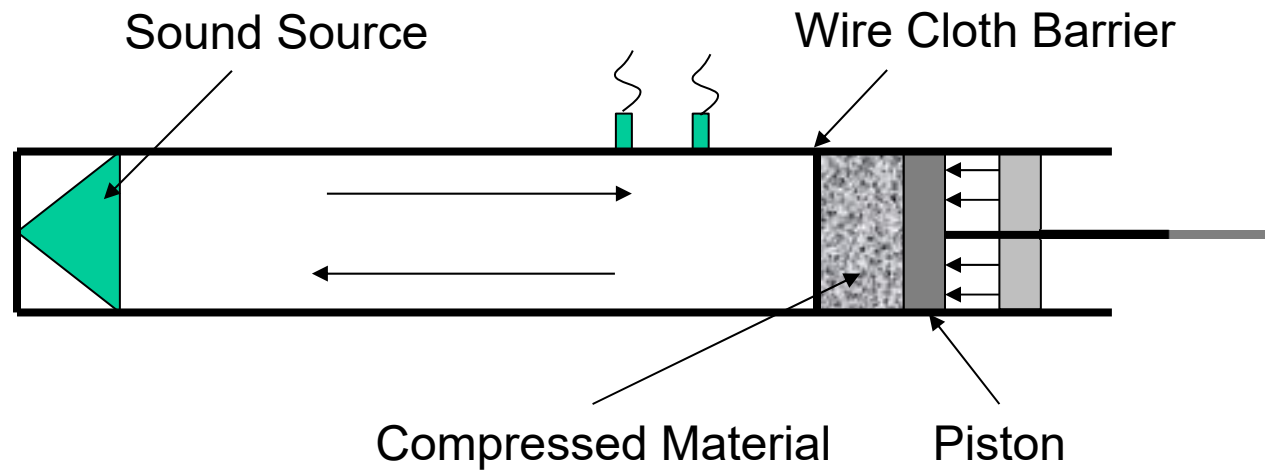
40 mm  
Polyester Fiber



# Porous Absorbers Compressed



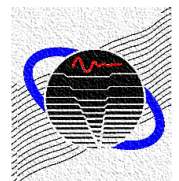
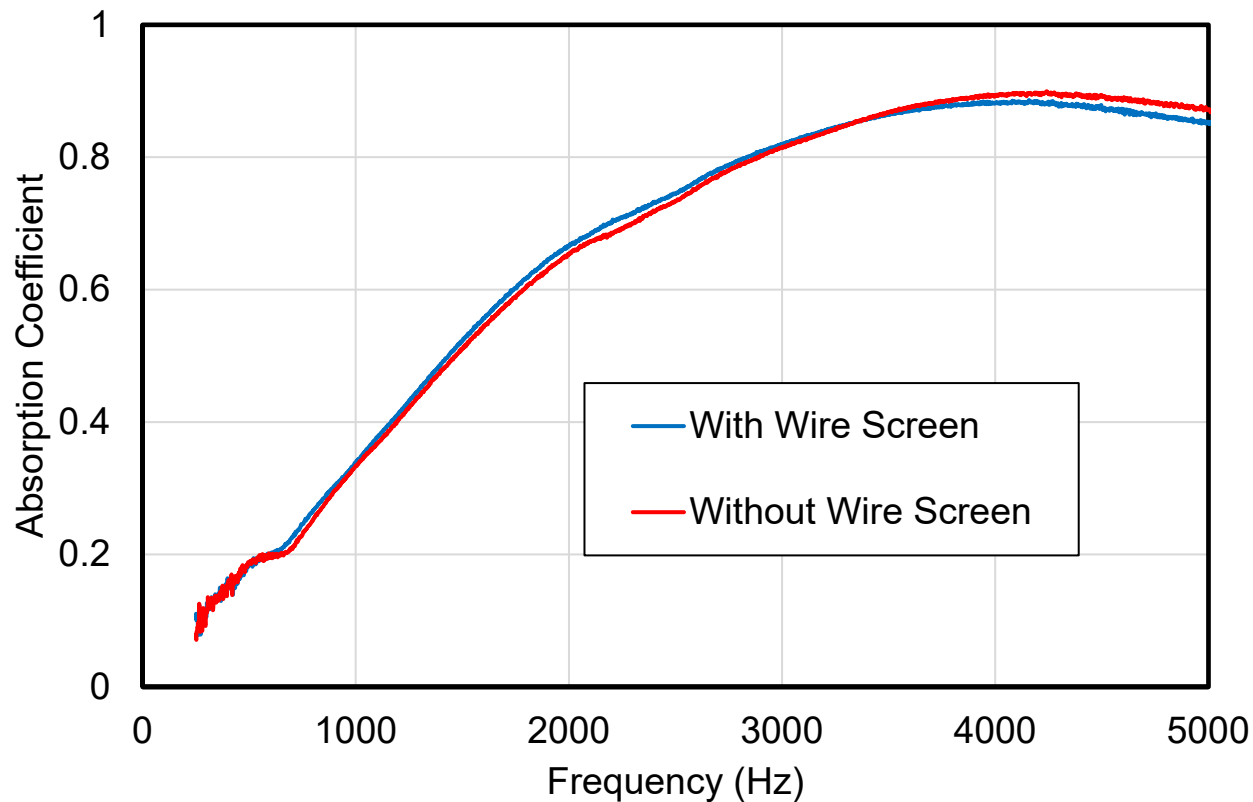
Wire Screen Barrier



# Porous Absorbers Compressed

## Effect of Wire Screen on Absorption

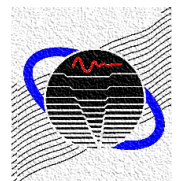
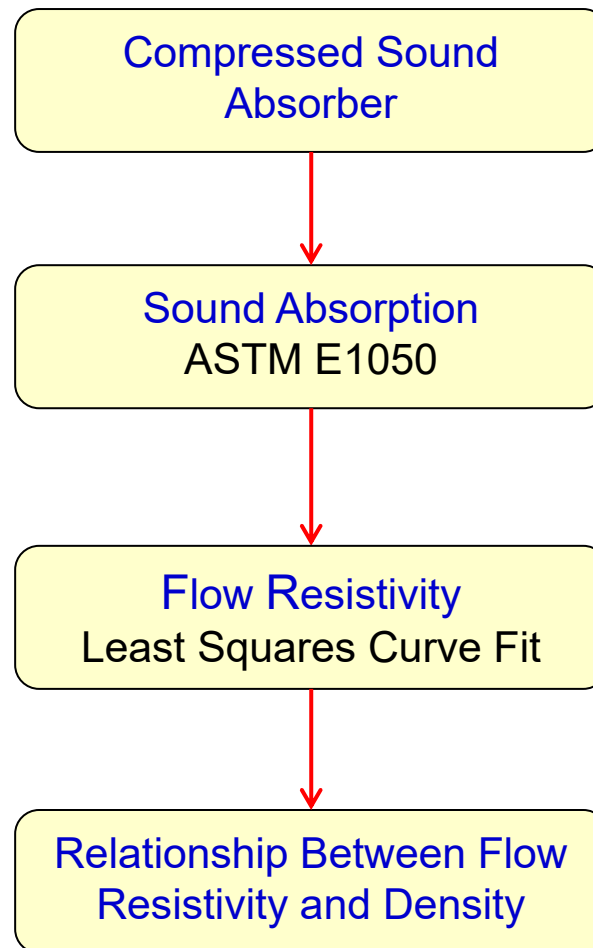
24 mm Melamine Foam Sample





# Porous Absorbers Compressed

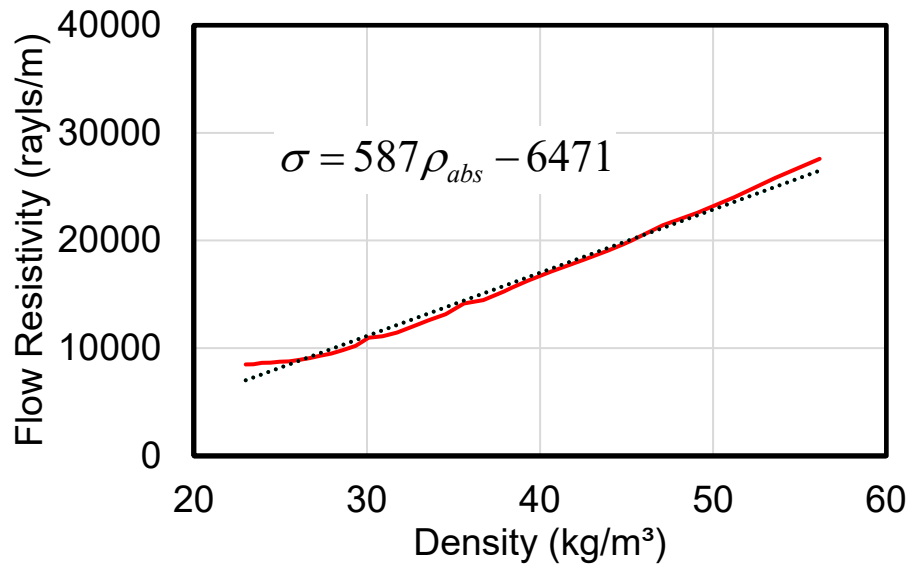
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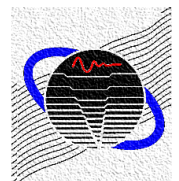
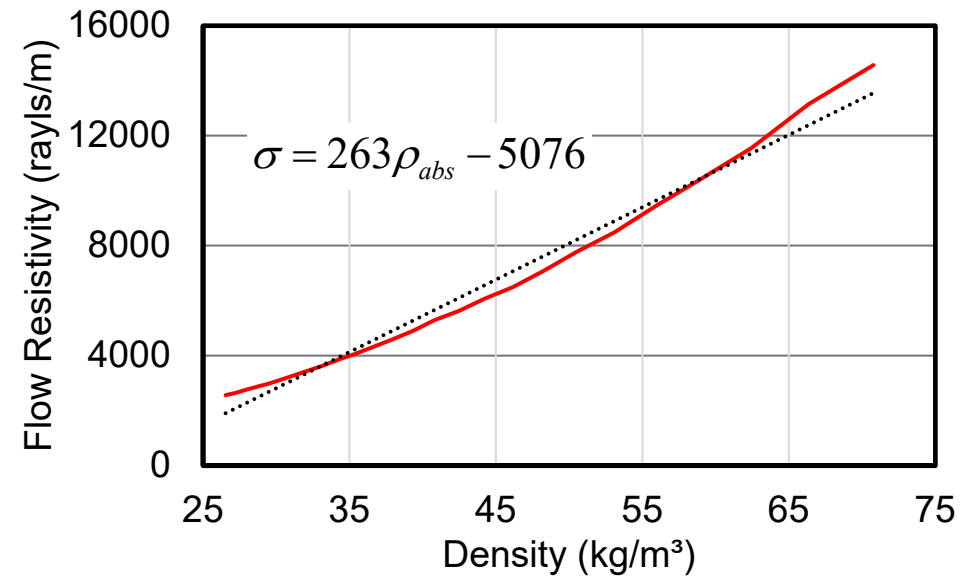
# Porous Absorbers Compressed

## Flow Resistivity vs. Density

### 50.8 mm Glass Wool

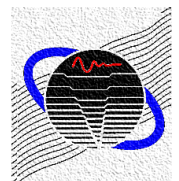
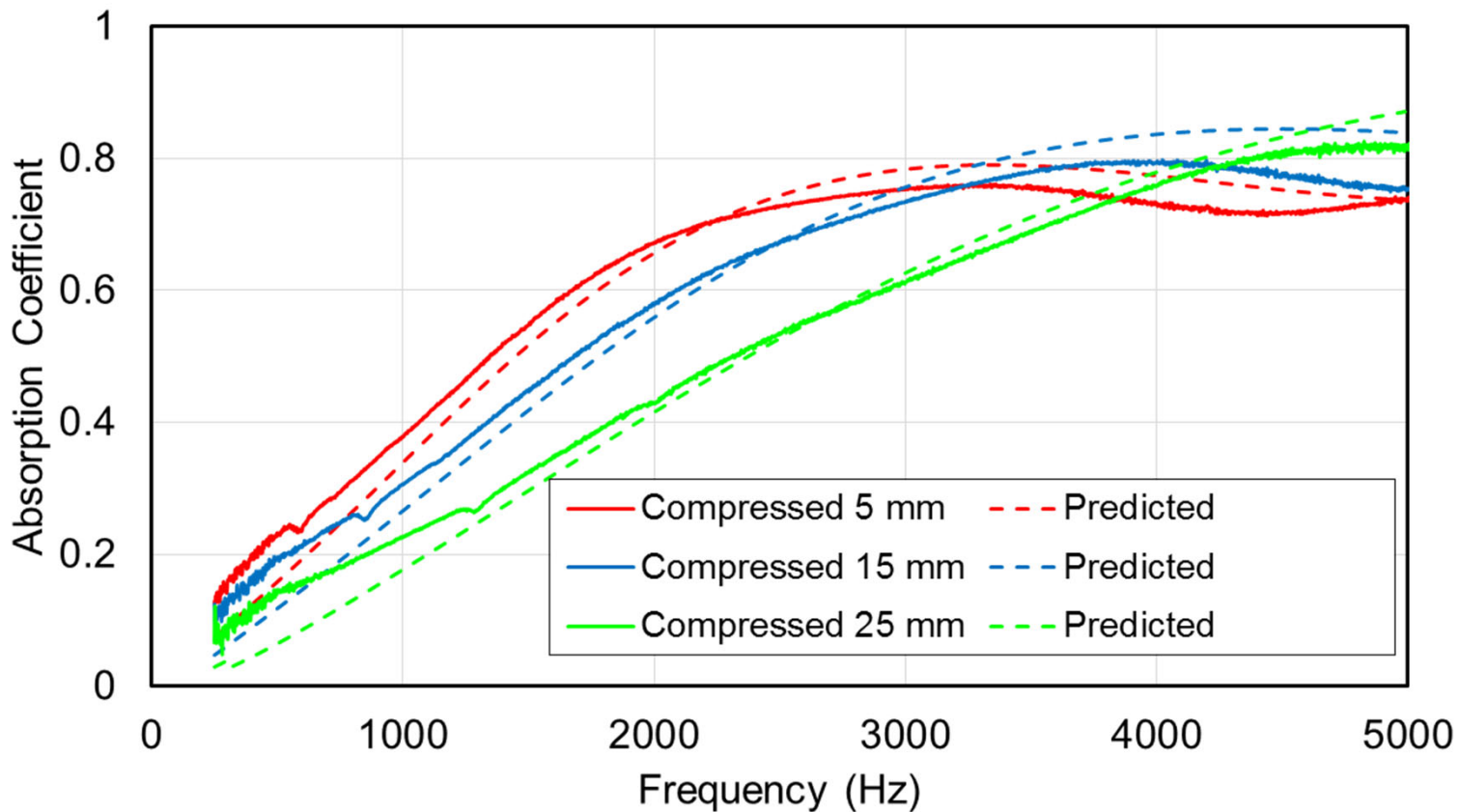


### 40 mm Polyester Fiber



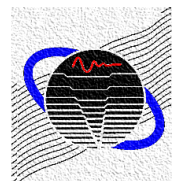
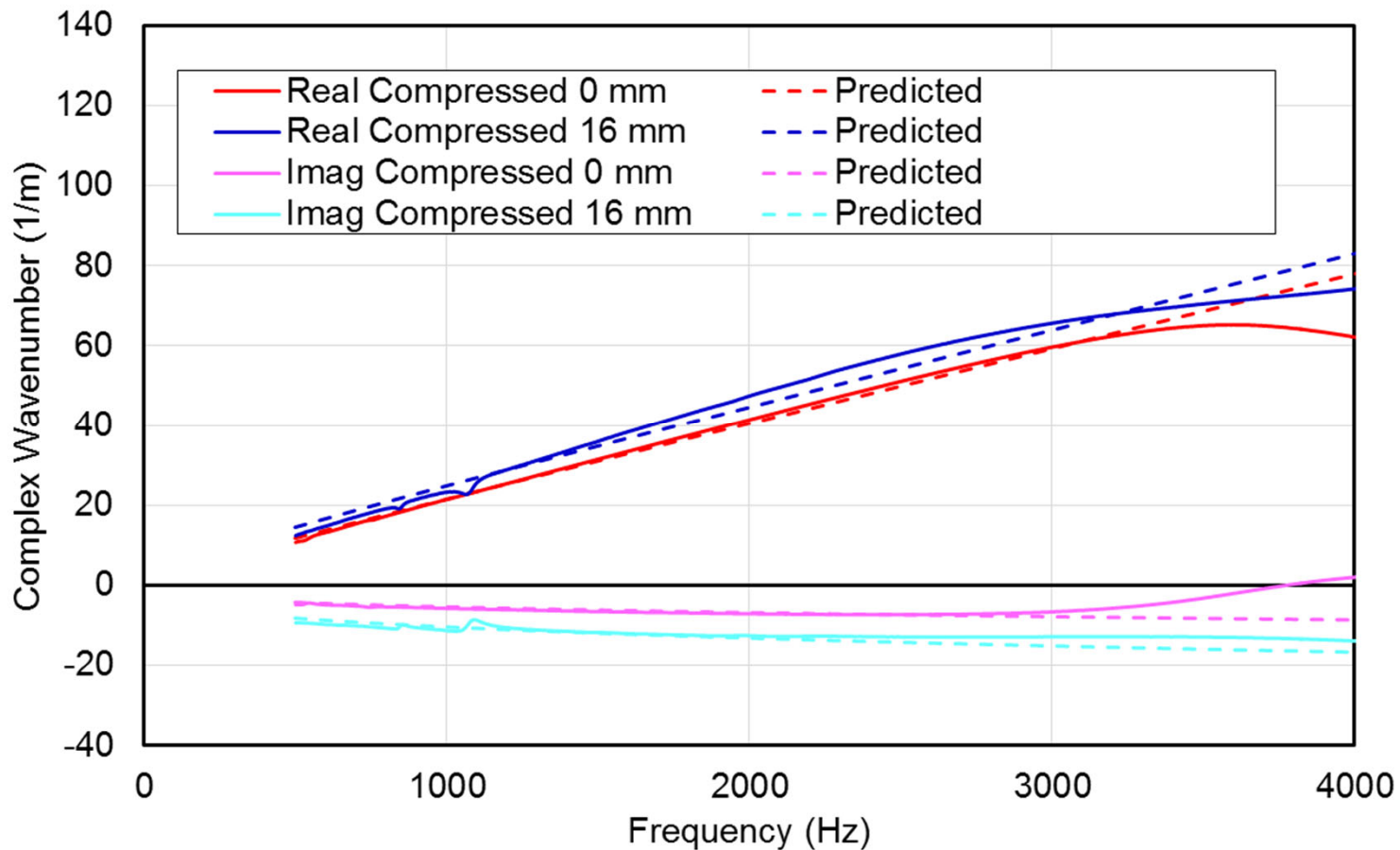
# Porous Absorbers Compressed

## 40 mm Polyester Fiber



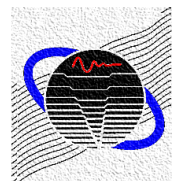
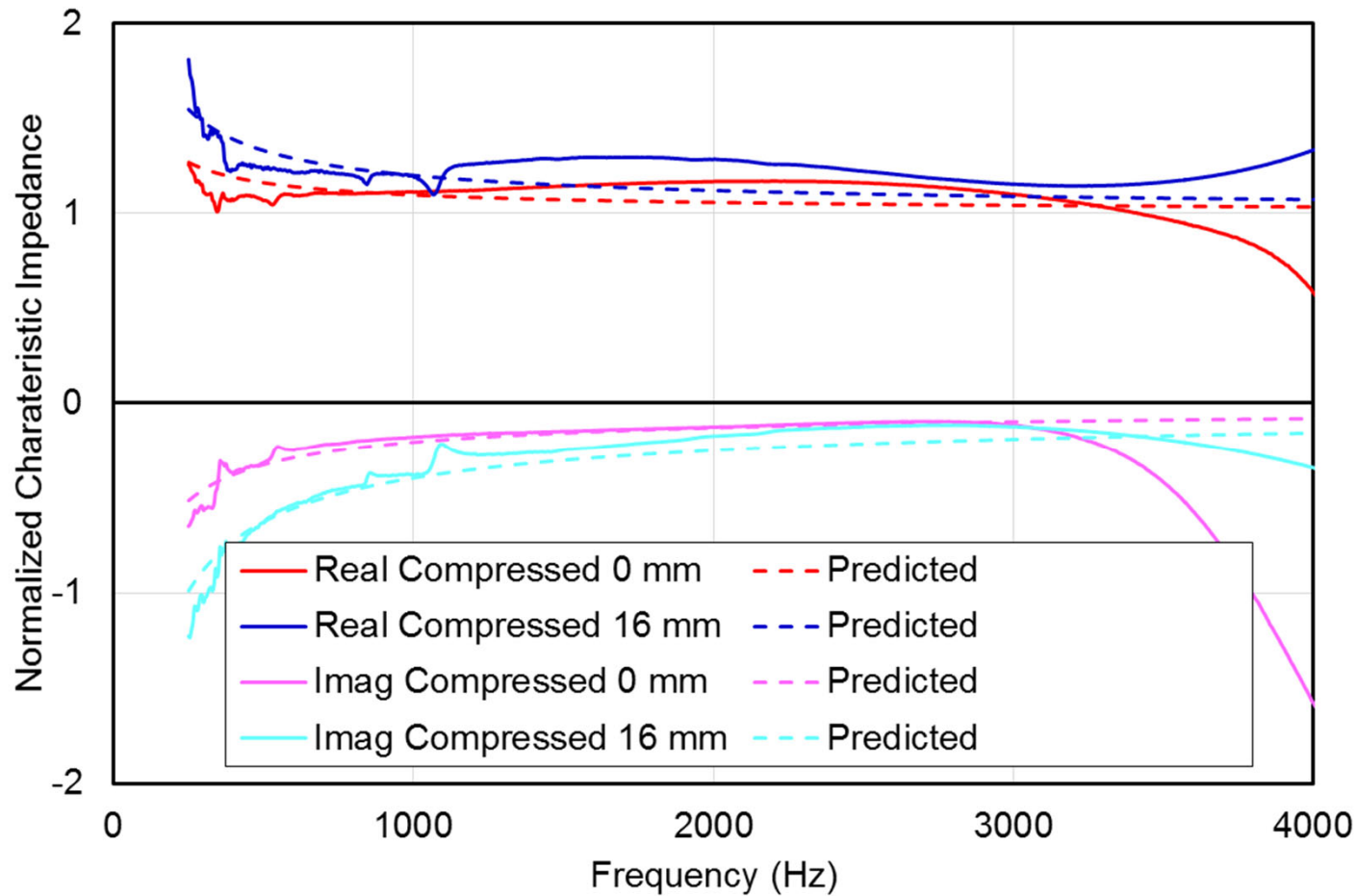
# Porous Absorbers Compressed

## Complex Wavenumber Polyester Fiber



# Porous Absorbers Compressed

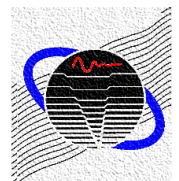
## Characteristic Impedance Polyester Fiber



# Overview

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- Porous Absorbers Overview
- Porous Absorbers Property Determination
- Porous Absorbers Basics for Designers
- Porous Absorbers Compressed
- Porous Absorbers Layered
- Reactive Absorbers Overview
- Reactive Absorbers Example



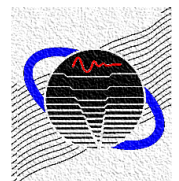
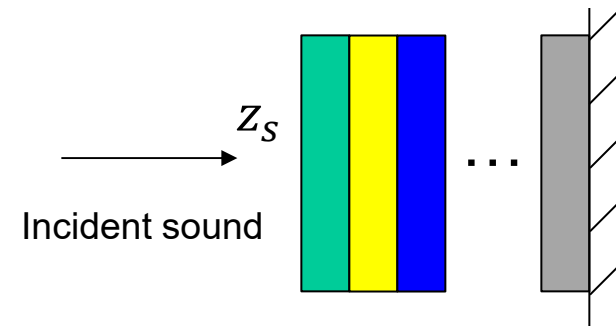
# Porous Absorbers Layered

$$[T] = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} = [T_1][T_2][T_3]\dots[T_n]$$

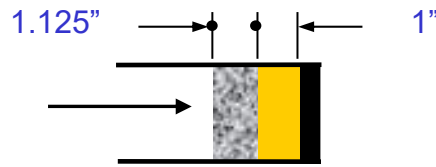
$$\rightarrow z_s = \frac{T_{11}}{T_{21}}$$

$$R = \frac{z_1 - \rho c}{z_1 + \rho c}$$

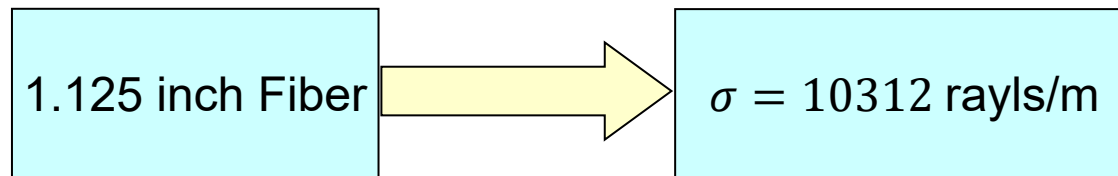
$$\rightarrow \alpha = 1 - |R|^2$$



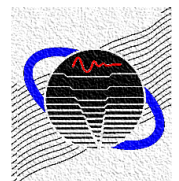
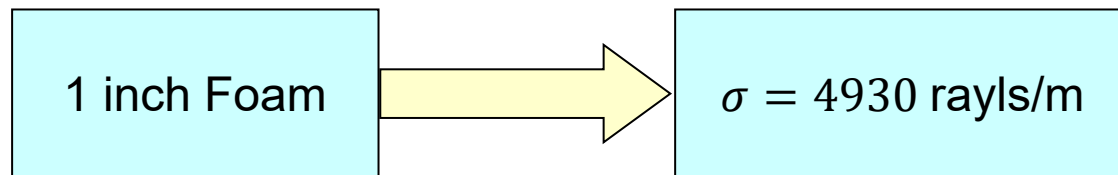
# Porous Absorbers Layered Materials



Curve Fit using Fiber Model

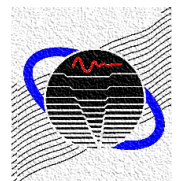
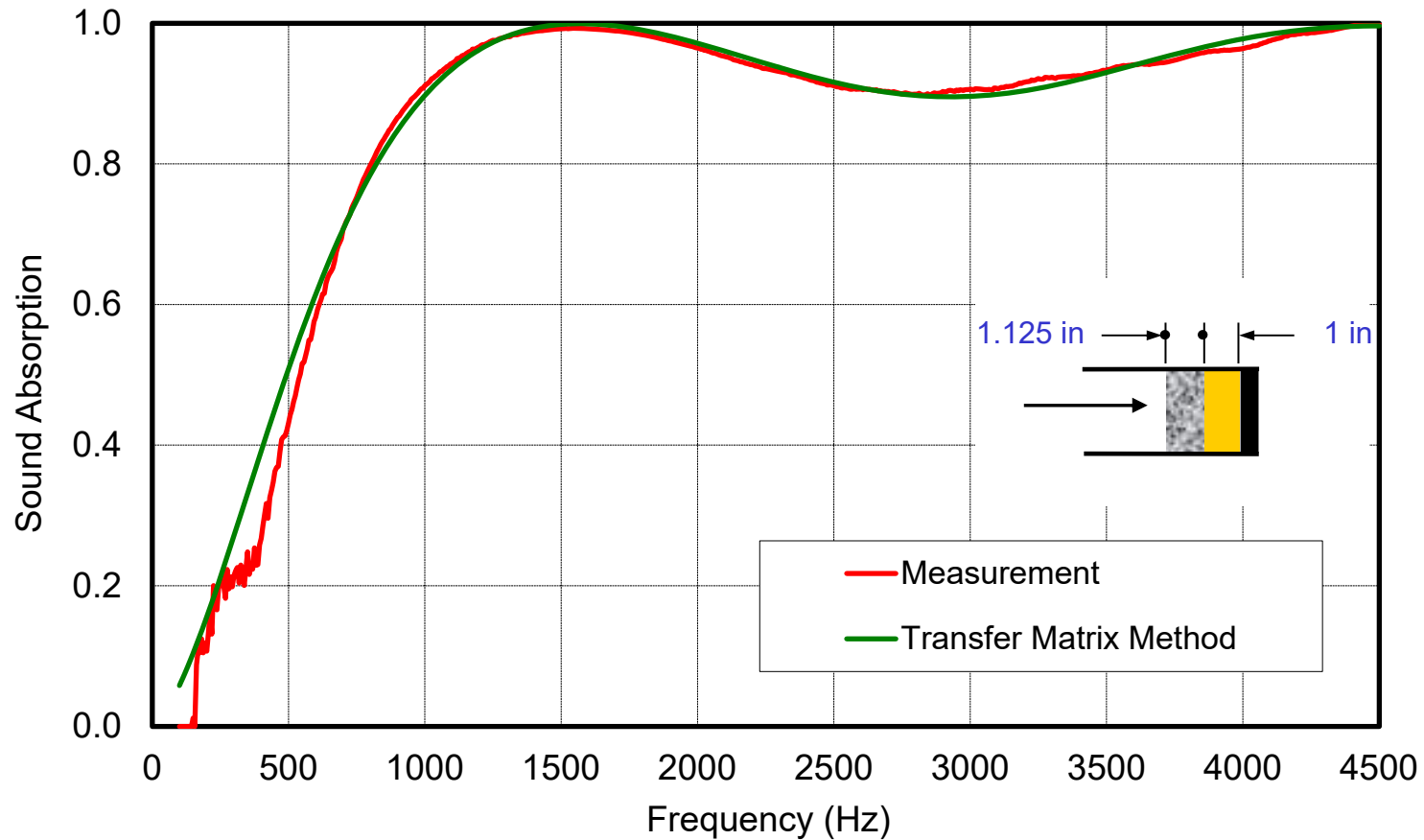


Curve Fit using Foam Model

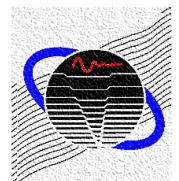
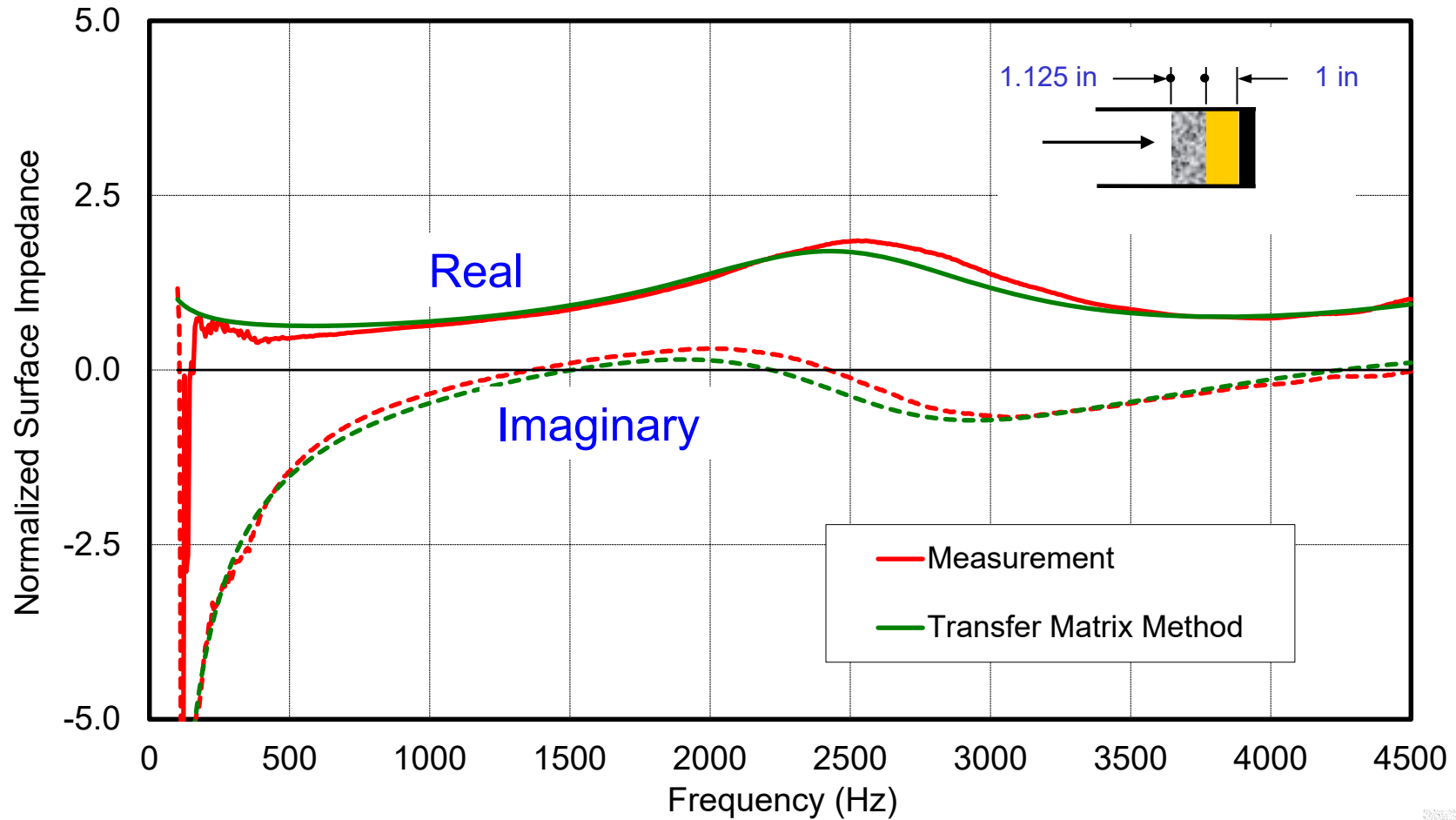




# Porous Absorbers Layered



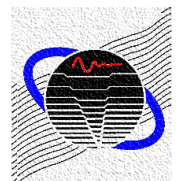
# Porous Absorbers Layered



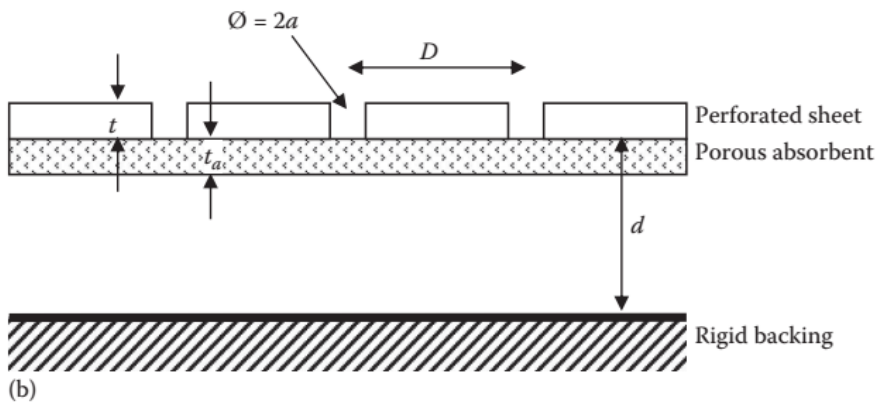
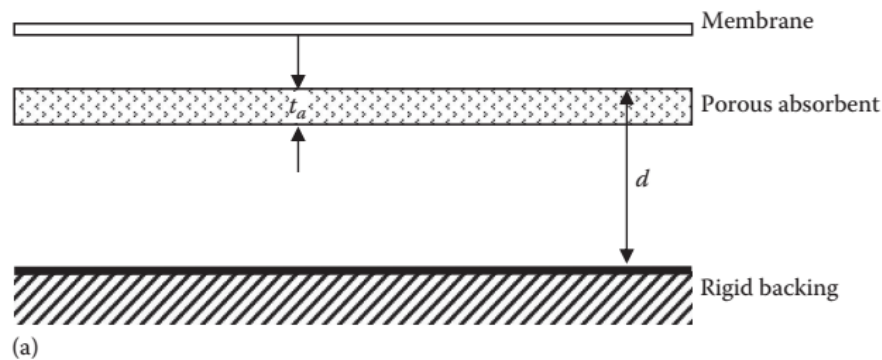
# Overview

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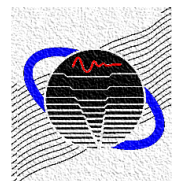
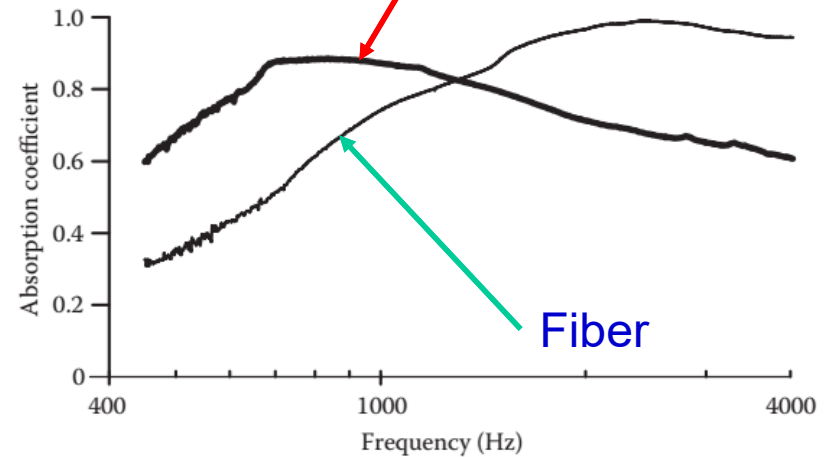
- Porous Absorbers Overview
- Porous Absorbers Property Determination
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- Porous Absorbers Compressed
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- Reactive Absorbers Overview
- Reactive Absorbers Example



# Reactive Absorbers Overview



Fiber with Perforated Cover

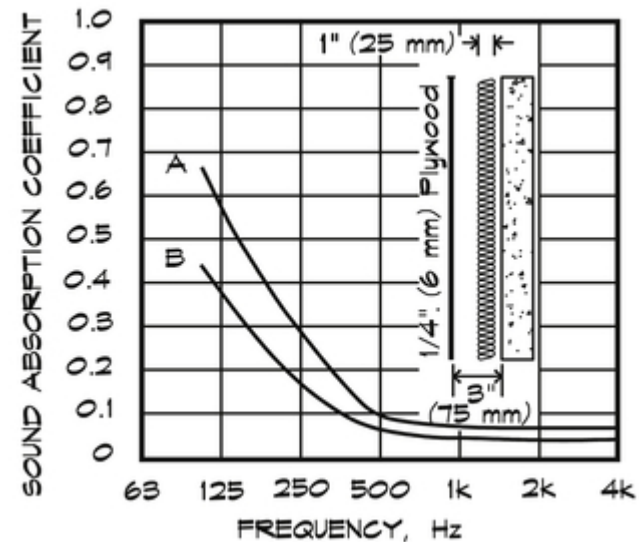


# Reactive Absorbers Overview

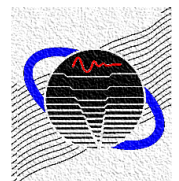
$$f_r = \frac{1}{2\pi} \sqrt{\frac{\rho c^2}{m_s d}}$$

$m_s$  surface mass density  
 $d$  spacing from wall

A – with 1 in glass fiber  
B – no glass fiber



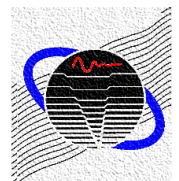
Long, 2014 based on Doelle, 1972



# Overview

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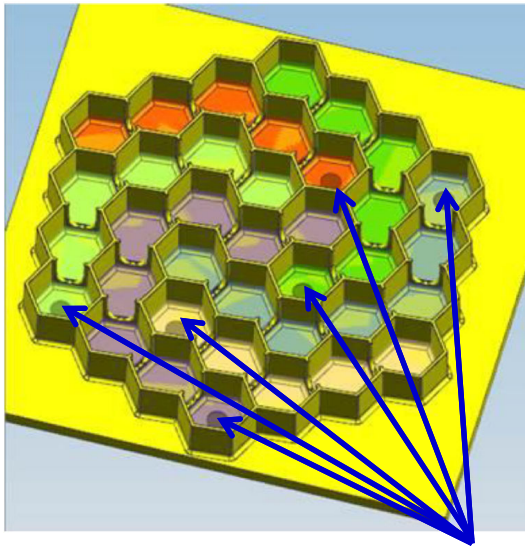
- Porous Absorbers Overview
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- Porous Absorbers Compressed
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# Reactive Absorbers Example

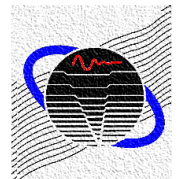
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Honeycomb with interconnected cells.



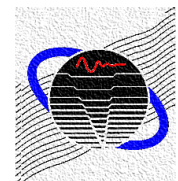
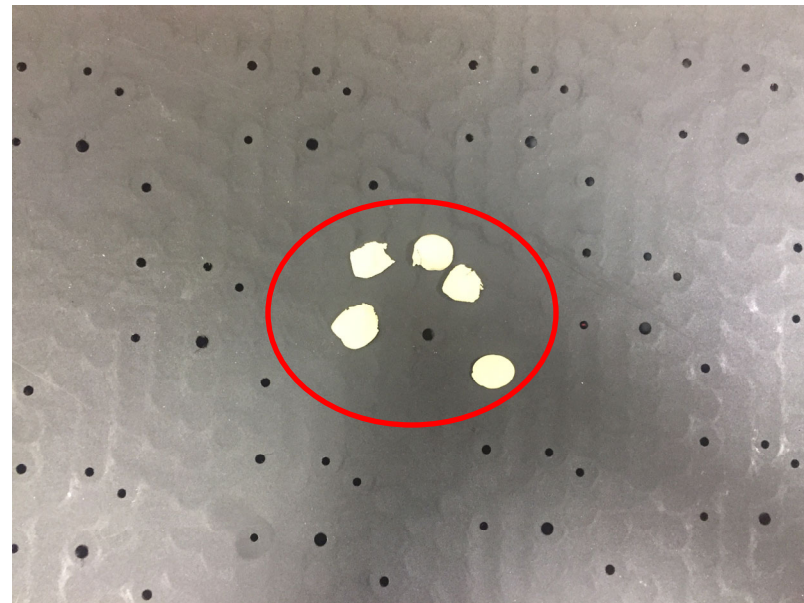
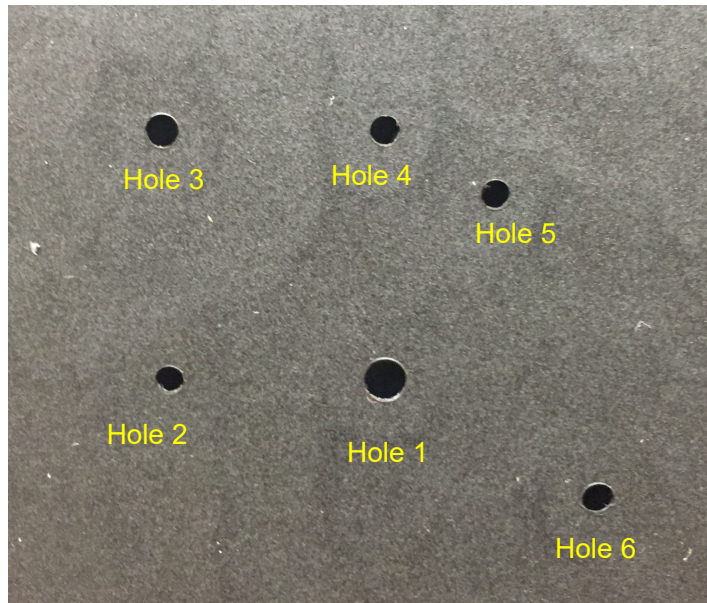
Holes

Jonza, J., Herdtle, T., Kalish, J., Gerdes, R., and Eichhorn, G.,  
Acoustically Absorbing Lightweight Thermoplastic Honeycomb  
Panels, SAE International Journal of Vehicle Dynamics, Stability,  
and NVH 1(2):2017, doi:10.4271/2017-01-1813.



# Reactive Absorbers Example

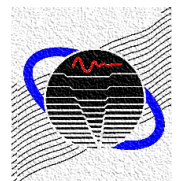
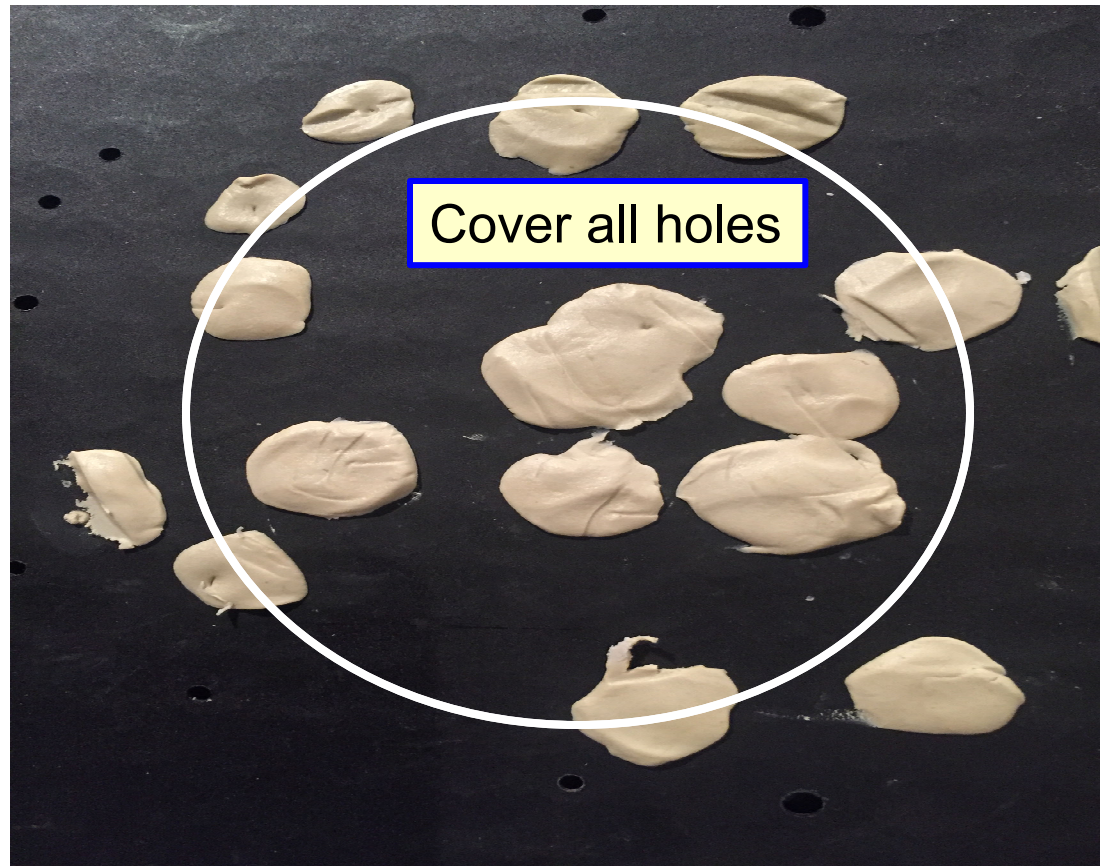
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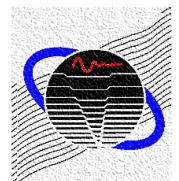
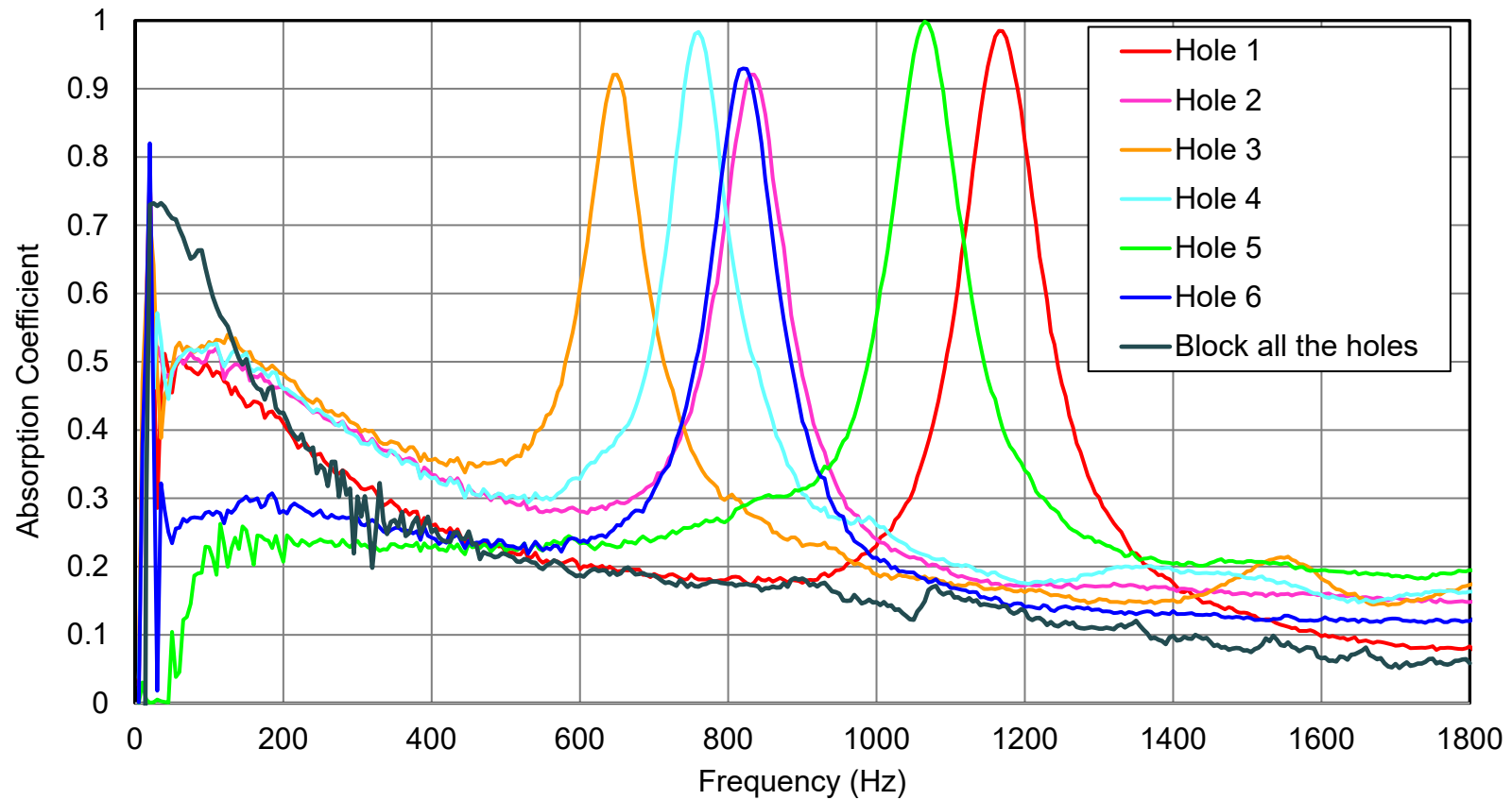


# Reactive Absorbers Example

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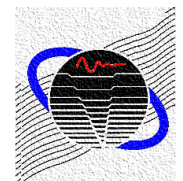
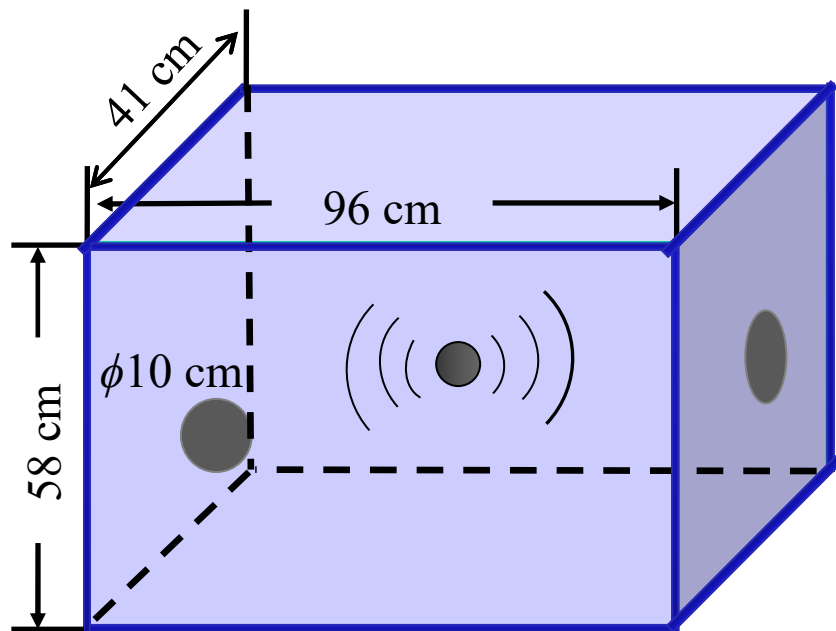


# Reactive Absorbers Example



# Reactive Absorbers Example

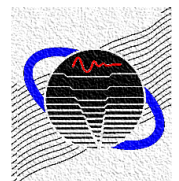
## Baseline Case



# Reactive Absorbers Example

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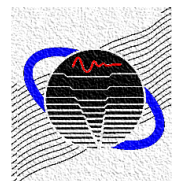
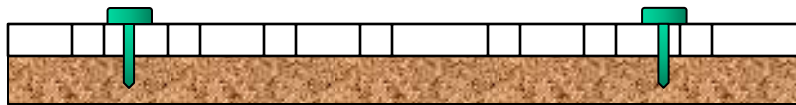
1.5 in Fiber Treatment



# Reactive Absorbers Example

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## Enclosure Study



# Reactive Absorbers Example

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$$IL = SWL_0 - SWL_1$$

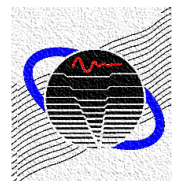
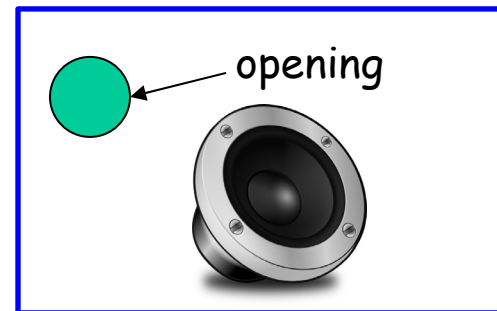
$SWL_0$  is the sound power level in dB for the speaker

$SWL_1$  is the dB level with the enclosure covered.

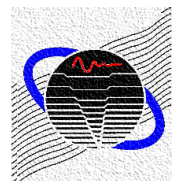
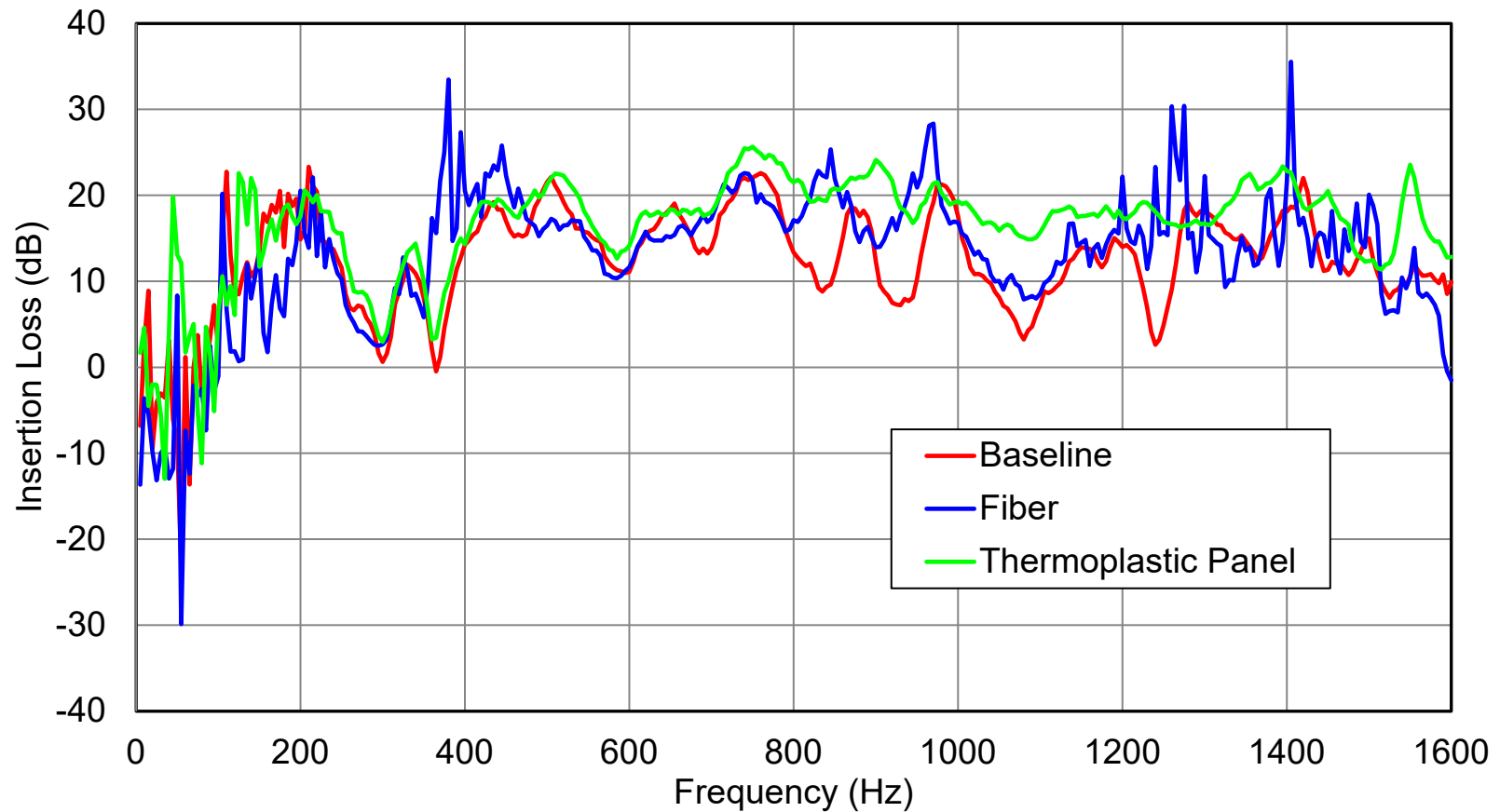
$SWL_0$



$SWL_1$

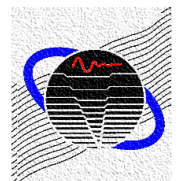


# Reactive Absorbers Example



# Reactive Absorbers Example

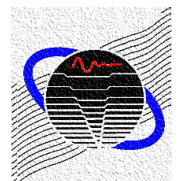
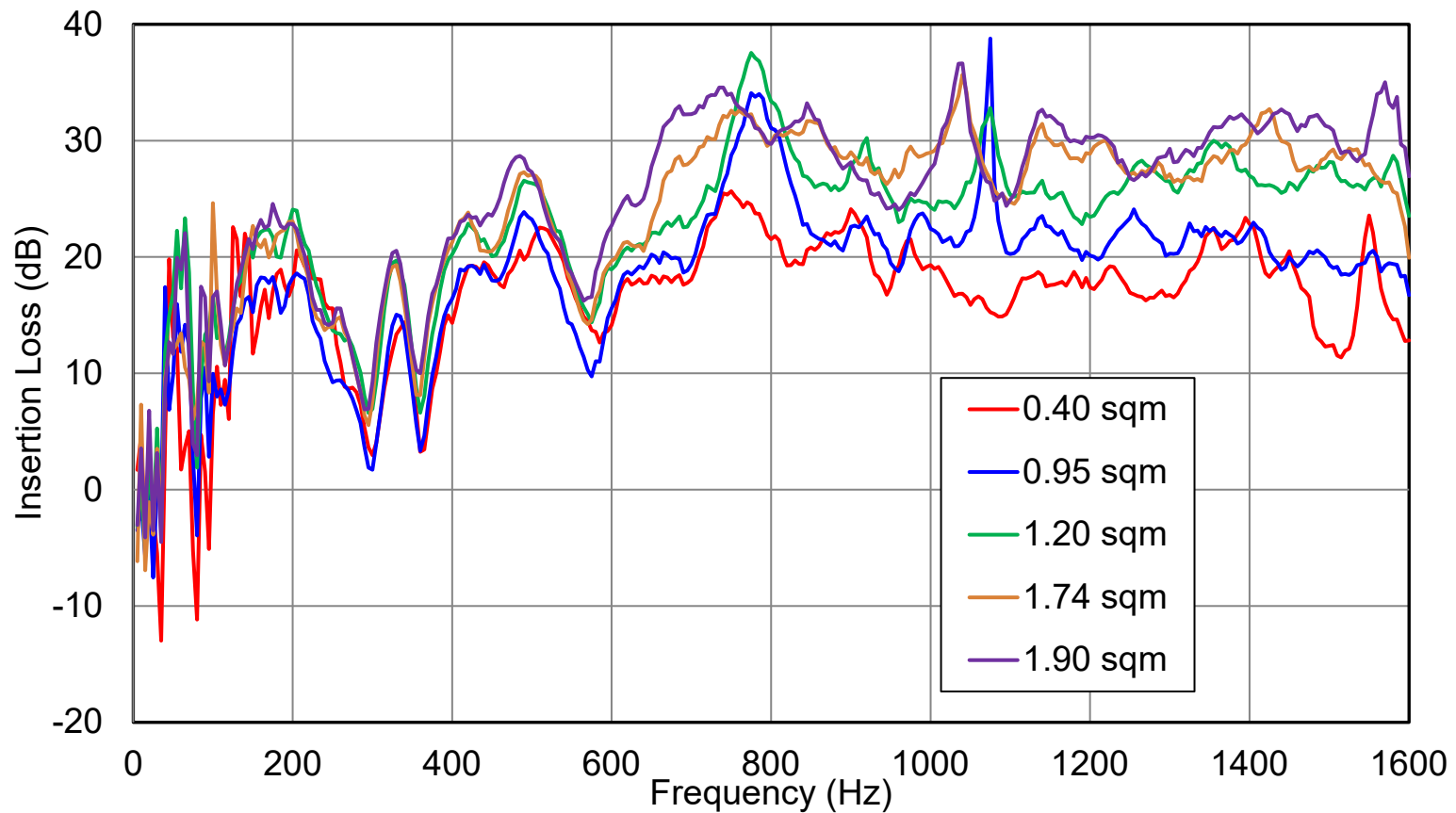
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# Reactive Absorbers Example

## Effect of Panel Area



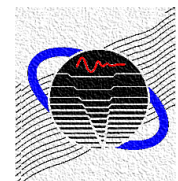
# Reactive Absorbers Example

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Reference Measurement



$$IL = L_{W,reference} - L_{W,silencer}$$

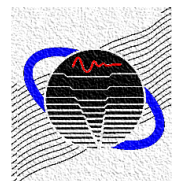
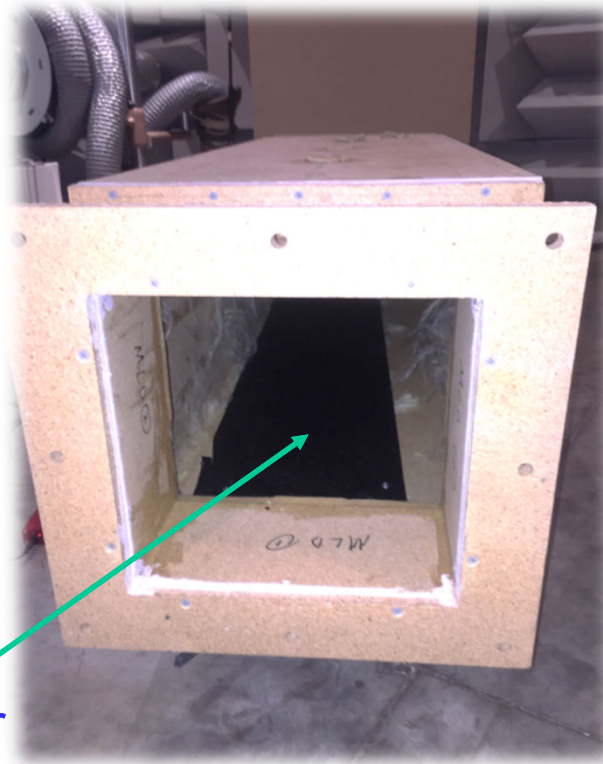


# Reactive Absorbers Example

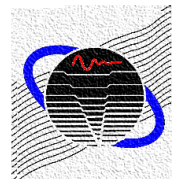
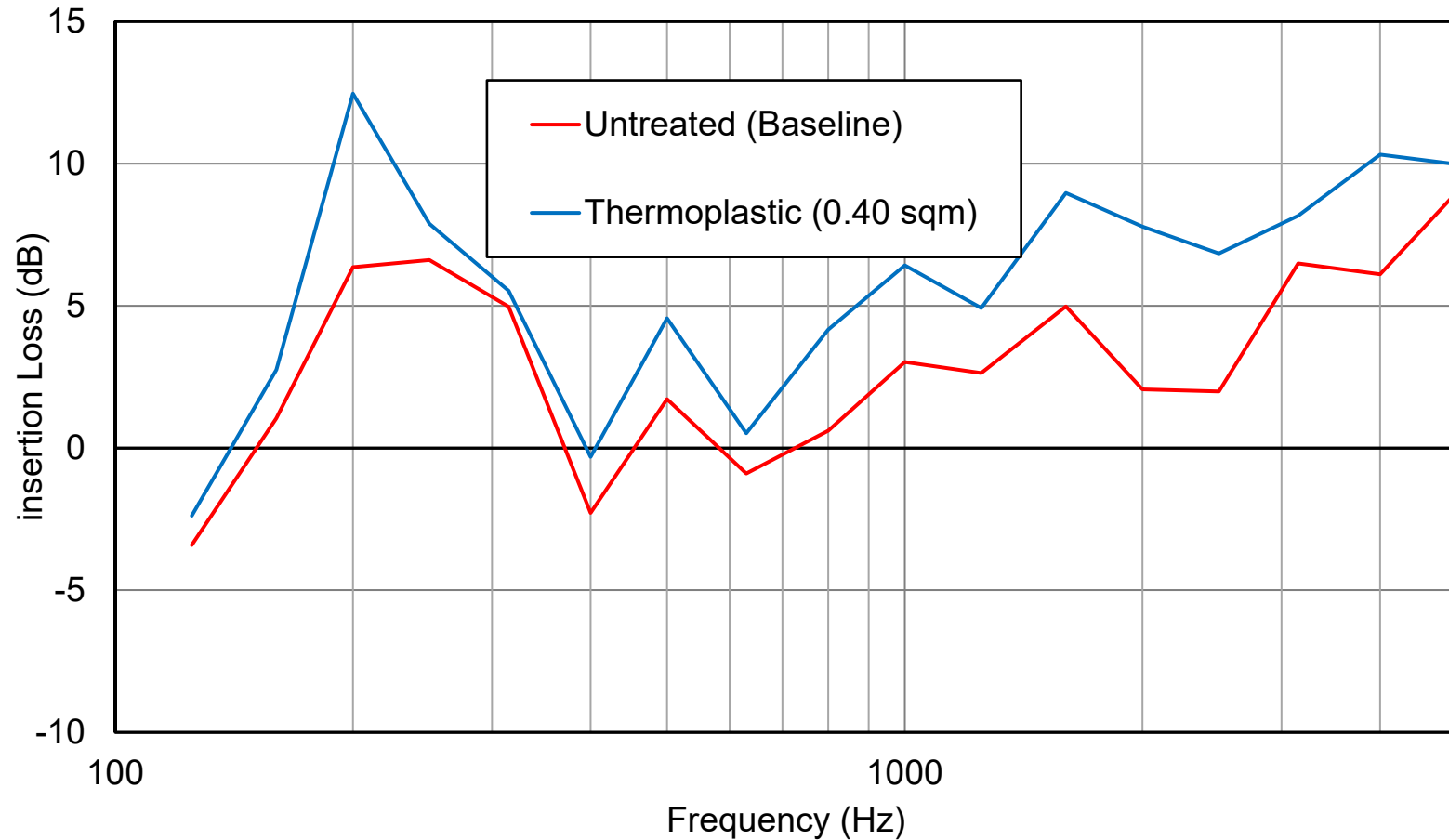
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Thermoplastic Panel Absorber



# Reactive Absorbers Example



# Future Trends

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- Hybrid dissipative – reactive sound absorbers
- 3D printed sound absorbers
- Microperforated panels
- Acoustic Fabrics

