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## **Generator Slot Liner Selection Guide**

### What is a Slot Liner?

A slot liner is a primary insulation component in a generator rotor, which provides an insulation barrier between the copper windings and the rotor core steel.

The slot liner must be sufficient to protect the winding from grounding to the rotor body during all phases of operation. First, it must be strong enough to withstand the physical wear and tear of the assembly process during winding. During operation, the liner must also endure the large centrifugal forces of generator start-up/shutdown and the generator's wide temperature variations from ambient at idle and up to 130°C in operation depending on the design. Generator slot liners are typically a composite construction. The composite layup of different materials provides both electrical and mechanical properties to meet the specific demands of the application. The following selection guide will provide information on the different constructions available, the unique advantages and disadvantages of each, and tips for best practices in slot liner design in order to help engineers make more robust

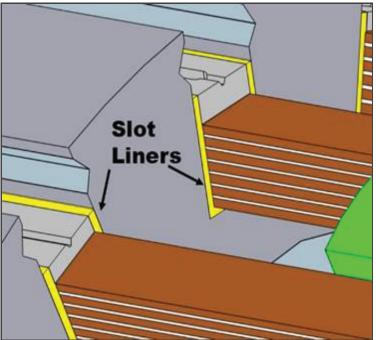


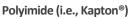
Figure 1 - Location of slot liners inside a rotor

## **Slot Liner Construction**

slot liner insulation specifications.

There are many choices of materials that can be used to build a composite slot liner. The most common materials used are:





pton<sup>®</sup>) Aramid Paper (i.e., Nomex<sup>®</sup>)



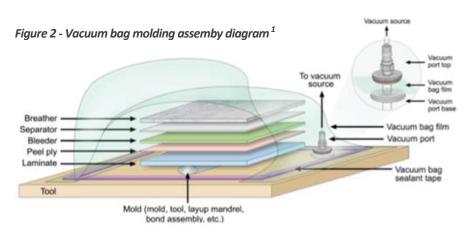
High Temperature Epoxy Resin



Each of these materials has specific electrical and mechanical properties that create a unique set of characteristics when combined in the slot liner composite. Epoxy has historically been used as the primary adhesive in slot liner composites due to its high temperature electrical and mechanical properties. Woven glass fabric is often pre-impregnated with the epoxy resin and stabilized for further processing. This material is commonly known as glass-epoxy prepreg or b-stage. When heated and put under pressure, the epoxy prepreg resin will flow and bond the composite laminate layers.

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Several methods can be used to mold slot liners, including compression molding, bladder molding, vacuum bag molding (see fig. 2), and autoclave molding. Methods that incorporate vacuum such as vacuum bag molding and autoclave molding will typically produce composites with fewer voids and greater uniformity.

When properly used, a vacuum will evacuate entrapped air within the layers of the composite and produce a composite with higher electrical and mechanical performance and fewer defects.

The construction of the composite laminate and the pressing operation will determine the final properties of the slot liner. As previously mentioned, the glass epoxy b-stage acts as the laminate's backbone while other materials enhance the electrical and mechanical properties. For example, aramid paper provides tear resistance. Polyimide film provide puncture resistance and also increases dielectric strength.

Туре	Construction Type	Relative Cost	Installation Toughness	Mechanical Strength	Flexibility	Dielectric Strength		Thick Wall (> 0.030")
0	All Epoxy Glass (EG)	Ş	Low	High	Low	Low	Х	Х
	EG – Nomex <sup>®</sup> – EG	\$\$	Medium	Med-high	Medium	Medium	Х	Х
11	Nomex <sup>®</sup> -EG-Nomex <sup>®</sup>	\$\$\$	Med-High	Medium	Med-High	Medium	Х	Х
	EG – Nomex® – EG – Polyimide – EG – Nomex® – EG	\$\$\$\$	High	Medium	Med-High	Med-High		Х
IV	Nomex <sup>®</sup> – EG – Polyimide – EG – Nomex <sup>®</sup>	\$\$\$\$	High	Medium	Med-High	High		Х
Ν	All Nomex®	\$\$	Medium	Low	High	Medium	Х	

Some typical constructions for slot liners are listed in the table below, along with the relative characteristics of each:

Typically slot liners will be designed in either an L or U format. If an L format is used, two L's are used to make a U shape by having them in opposing directions. The rotor slot diagram (see fig. 3) shows two L slot liners used along with sub slot insulation. Sub slot insulation is placed at the bottom of the slot providing insulation between the windings, the butt-joint of the L-shaped slot liners, and the rotor forging.

If a full U shape format is used, the sub slot insulation does not have to be used since there is no gap to fill. The U format is more common with smaller rotors since mold costs increase, and manufacturability decreases considerably at longer lengths making it more difficult to specify the U format for larger rotors. Each "type" of construction can be used for various wall thicknesses. The above table shows what range of thickness the market tends to use broken down into a "thin wall" or "thick wall" with 0.030 inches (0.77mm) being nominal.

The overall fit within the slot is very important when designing and producing slot liners. If slot liners do not mate up to the shape of the slot, specifically, they need to match the radii of the slot, the force of the coil will easily crack or sever any liner once in operation. Likewise, if the liner shape does not match the initial layer of copper's shape, the likelihood of failure increases tremendously. One common failure occurs when slot liners are not straight. The copper damages the liner during installation due to the winders' inability to keep the liner away from the descending copper. A second common failure occurs when the liner angle is incorrect and bends inward towards the slot opening. When this defect is encountered, the copper can also catch the liner when descending, causing failures.

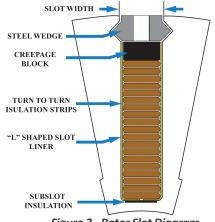


Figure 3 - Rotor Slot Diagram

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Another typical enhancement found in many slot liners is low friction materials applied to the inside surface. Low friction additives such as PTFE can be applied via a sprayed coating to the slot liner's inner surfaces to allow copper coils to slide easily into the liner without damage the insulation material. Some PTFE materials can be bonded onto the liner to create a permanent slip plane that can increase liner life by decreasing friction wear due to generator cycling.

Lastly, slot liners can be vented with holes in the bottom to match the rotor's cooling slots. Some ventilated rotor coils require slot cells with ventilation slots that must be carefully measured to match up with the copper coils and rotor slot

vents. The axial growth of the copper and abrasion against the insulation can cause ventilation slots to be partially covered, potentially causing localized hot spots in the rotor. Ventilation hole design must consider the movement of the copper in order to prevent the ventilation holes from being blocked.

### **Typical Testing and Properties**

While many of the tests performed on slot liners for electrical and mechanical characterization are from the ASTM or ISO standards, there are also some customized tests specifically created for slot liners.

### **Electrical Testing**

- Dielectric Strength ASTM D149 Method B with a choice of electrode shape and diameter.
- Voltage Endurance Electrode sizes are called out and referenced to ASTM D149, and the test is conducted to
  determine if partial discharge occurs on the surface of the slot liner over a period of time when a specified voltage is
  applied.
- Voltage Withstand (Hipot) Electrodes can be designed for a pass-through test or full slot liner test. The test was designed to detect flaws or weak spots in the liner.
- Electrical Creepage Measures the resistance to forming a current path across the material's surface or around an edge. It is tested by applying a voltage across two electrodes on the sample surface and then gradually increasing the voltage to a specified maximum current flow.

### **Mechanical Testing**

- Impact Resistance ASTM D5420 and a specific striker diameter called out to be used in the test.
- Flexural Strength ASTM D790 or ISO 178 with specific instructions called out.
- Flexural Modulus ASTM D790 or ISO 178 with specific instructions called out.
- Water Absorption ASTM D570.
- **Tensile Creep** ASTM D2990 with a high tensile load for an extended period of time at temperatures near the typical rotor operating temperature.
- Static Coefficient of Friction ASTM D1894.
- Shrinkage in the Length Direction Conducted to see if shrinkage occurs after a high temperature is applied to a sample for an extended period of time. A sample is measured before and after temperature application to calculate a percentage of shrinkage.
- **Thermal Endurance** Can be done in accordance with ASTM or ISO standards, but generally, a group of multiple samples are placed in an oven at the high end of the operating temperature for up to 8 weeks. Samples are removed each week and tested to see how they perform mechanically.
- Resistance to Compressive Buckling, Ball-On-Cavity Compression Test, and shear test Are little less common, but are used to test the slot liners ability to withstand the stresses of field assembly.

Figure 4 - slot machined into slot liner









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#### What construction is right for your design?

The construction of a slot liner depends on the type of rotor that one is designing or repairing. OEM's and repair companies have different requirements. The operating environment of the liner will influence the materials used in the composite. In any case, the design variations are nearly endless. From simple liners for small rotors to large, complex liners with venting, TGC can help with the fabrication of almost any design. Our aerospace-grade autoclave process produces the straightest void-free slot liners in the world.

Be confident in your selection of RotoGuard<sup>®</sup> slot liners and contact one of our customer service specialists today to see how we can help you with your needs.



For more information on Rotoguard<sup>®</sup> slot liners, please visit https://thegundcompany.com/rotoguard

For more details on The Gund Company, go to https://thegundcompany.com/

#### **References:**

1. "Composites Technology - NSC STEM Pathways". *Open Learning Initiative*. 2020: https://oli.cmu.edu/courses/composites-technology-nsc-stem-p`athways/.

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Item: RotoGuard <sup>®</sup> Slot Insulation							
Description:	RotoGuard <sup>®</sup> Slot Insulation from The Gund Company is a high performance glass epoxy laminate. It can be produced in five standard constructions as well as custom constructions. The aerospace manufacturing technology used to produce this insulation provides uniform, high quality thickness and straightness down the entire length of each part. Every part is 100% inspected for quality and can be hipot tested up to 20kV.						
	Standard Inside Radius	.100" +/010"	2.54 +/25 mm				
	Radius Range Available	.027"125"	.7 - 3.2 mm				
Dimensions:	Angle	90 +/- 3° Standard					
	Max Leg Dimensions	7" x 1.8" +/008	177.8 x 45.7 +/2 mm				
	Available Thickness	.030"125" +/003"	.78 mm - 50.8 mm +/076 mm				
	Shapes	Standard "U" and "L" shapes are available. Custom shapes available upon request.					
	Туре 0	All Epoxy Glass					
	Туре І	Glass - Nomex <sup>®</sup> - Glass					
	Type II	Nomex <sup>®</sup> - Glass - Nomex <sup>®</sup>					
Construction:	Type III	Glass - Nomex <sup>®</sup> - Glass - Polyimide - Glass - Nomex <sup>®</sup> - Glass					
	Type IV	Nomex® - Glass - Polyimide - Glass - Nomex®					
	Type N Nomex®						
	Special Requests	Custom construction available to meet most customer requests					

Key Characteristics <sup>1</sup>	Units	Test Method	Condition	Type 0	Type I	Type II	Type III	Type IV	Type N
Apparent Density	g/cm <sup>1</sup>	ASTM D-792	А	2.0	1.7	1.7	1.6	1.7	1.08
Water Absorption	%	ASTM D-570	D-24/23	0.4	1.3	4.0	1.5	3.7	
Tensile	ksi	ASTM D-638	А	32.9	26.6	18.3	26.0	17.5	2.2
Eloyural Strongth	h MPa	ASTM D-790	А	87.71	54.72	50.58	65.20	60.10	
Flexural Strength			E-1/160 T160	46.60	50.58	32.68	52.50	41.36	
Dielectric Strength	V/mil	ASTM D-149	А	1,050	1,050	1,400	1,200	1,200	810
Permittivity		ASTM D-150	А	4.6	4.2	3.8	4.2	3.8	3.4
Dissipation Factor		ASTM D-150	А	0.03	0.02	0.02	0.022	0.02	0.07
Compressive Strength (1/2")	ksi	ASTM D-695	А			40	48		
Thermal Conductivity	W/(m.K)	ASTM E-1461		0.25 - 0.21	0.23 - 0.19	0.25 - 0.21	0.25 - 0.21	0.24 - 0.20	157
Comparative Tracking Index		IEC-60112		200	200	250	200	250	200

<sup>1</sup> Indicates a thickness of 0.050"

All of the information, suggestions and recommendations pertaining to the properties and uses of the products herein are based upon tests and data believed to be accurate; however, the final determination regarding suitability of any material described herein for the use contemplated, the manner of such use, and whether the use infringes any patents is the sole responsibility of the user. There is no warranty, expressed or implied, including, without limitation warranty of merchantability or fitness for a particular purpose. Under no circumstances shall we be liable for incidental or consequential loss or damage. TGCR 0720