

# The Radio Channel



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COS 463: Wireless Networks

Lecture 14

**Kyle Jamieson**

[Parts adapted from I. Darwazeh, A. Goldsmith, T. Rappaport, P. Steenkiste]

# Motivation

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- The **radio channel** is what **limits** most radio systems – the main challenge!
  - Understanding its **properties** is therefore key to understanding radio systems' **design**
- There is **no single radio channel**, but instead **variation in many different properties**
  - Carrier frequency, environment (e.g. indoors, outdoors, satellite, space)
- Many different **models** covering **many different scenarios**

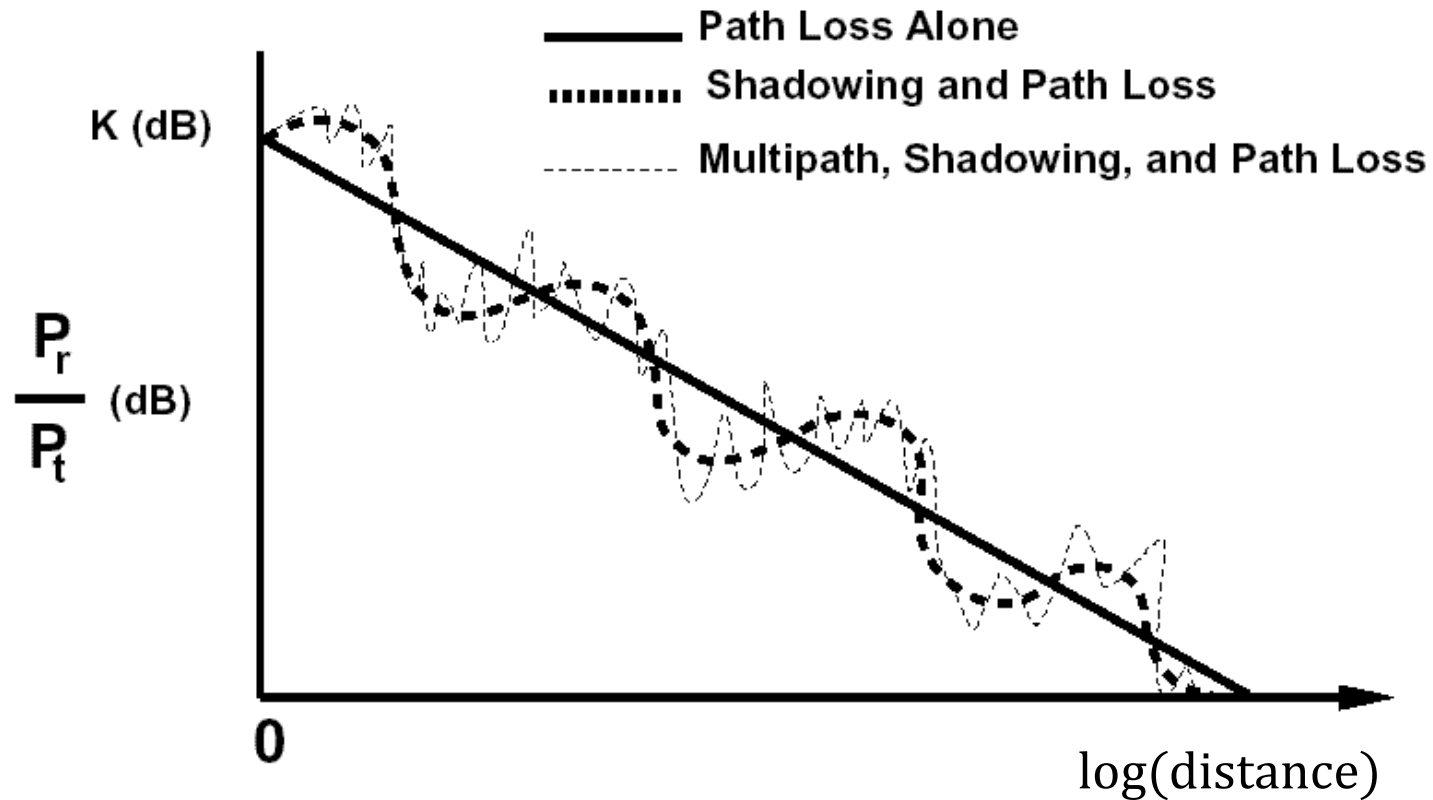
# Channel and Propagation Models

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- A *channel model* describes **what happens**
  - Gives channel output power for a particular input power
  - “Black Box” – no explanation of mechanism
  - Requires appropriate statistical parameters (e.g. loss, fading)
  
- A *propagation model* describes **how it happens**
  - How signal gets from transmitter to receiver
  - How energy is redistributed in time and frequency
  - Can **inform channel model** parameters

# Modeling (from a high-level perspective)

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# Today

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## 1. Large scale channel models

- Free space model
- Two-ray ground model

## 2. Small-scale channel models

## 3. Equalization: Coping with the channel

# The dBm unit

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- If we take one milliwatt as a reference then we have a unit of absolute power called **dBm**:

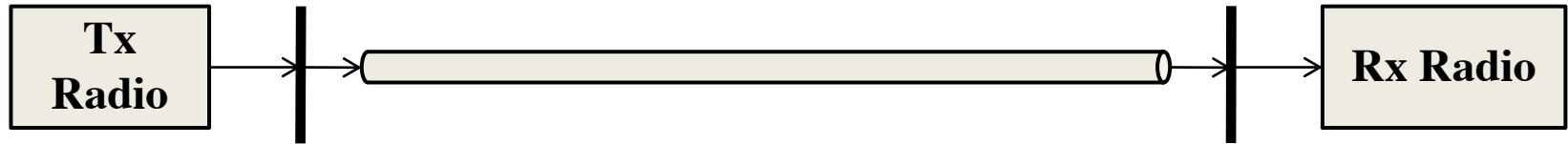
$$P_{dBm} = 10 \log_{10} \left( \frac{P_1}{10^{-3}} \right)$$

- Where  $P_1$  is the power we want to express in dBm, **in Watts**

Power (linear)	Power (dBm)
10 W	40 dBm
1 W	30 dBm
100 mW	20 dBm
10 mW	10 dBm
1 mW	0 dBm
10 $\mu$ W	-20 dBm
1 $\mu$ W	-30 dBm
1 nW	-60 dBm
1 pW	-90 dBm

# Goal: Power Budget

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$$P_{RX} \text{ (dBm)} = P_{TX} \text{ (dBm)} + \text{Gains (dB)} - \text{Losses (dB)}$$

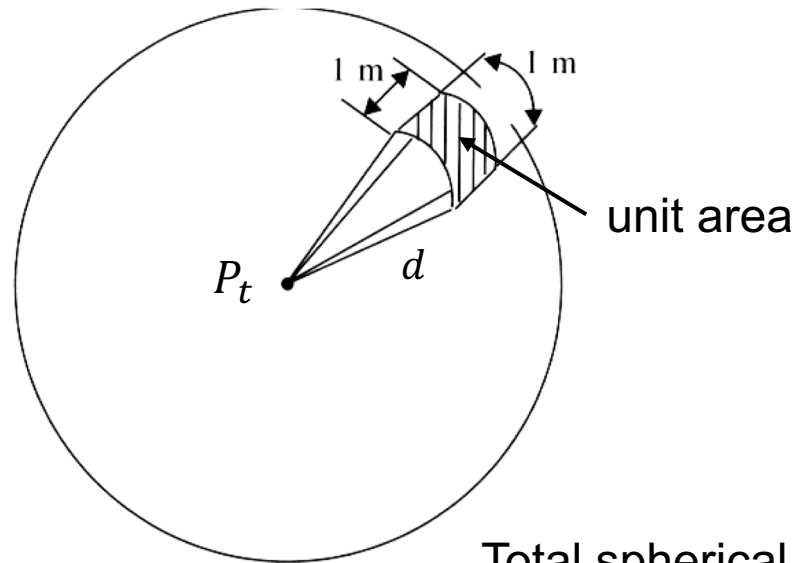
- Receiver needs a certain SINR to be able to decode the signal
- **Factors reducing power budget:**
  - Noise, attenuation (multiple sources), longer range, fading
- **Factors improving power budget:**
  - Antenna gain, transmit power

**Goal:** Predict **average** received signal strength given a transmitter-receiver separation distance

# LARGE-SCALE CHANNEL MODELS



# Transmitting in Free Space



Total spherical surface area:  $4\pi d^2$

- Deliver  $P_t$  Watts to an omnidirectional transmitting antenna
- So then **power density** (Watts per unit area) at **range  $d$**  is  $p = \frac{P_t}{4\pi d^2} \text{ W/m}^2$ 
  - Independent of wavelength (frequency)

# Idealized Receive Antenna

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- **Effective aperture  $A_e$** : fraction of incident power density  $p$  captured and received

$$- A_e = \frac{\lambda^2}{4\pi}$$

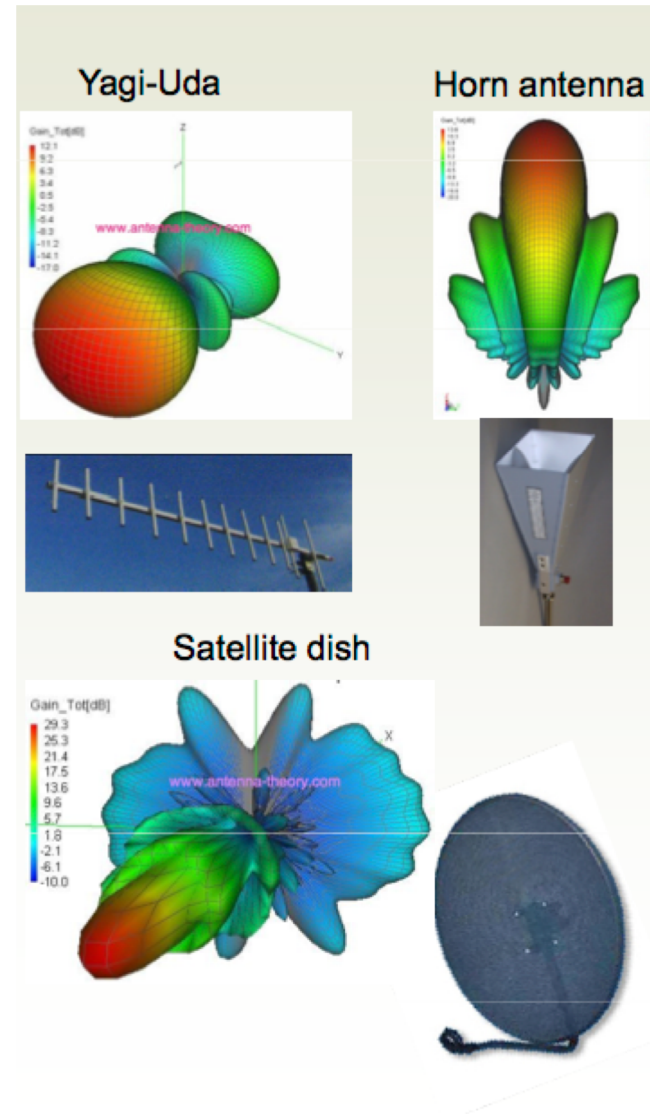
- Larger antennas at greater  $\lambda$  **capture more power**

- So **power received**  $P_r$  is the product of the power density and effective aperture:

$$P_r = \frac{P_t \lambda^2}{(4\pi)^2 d^2}$$

# Antenna Gain

- Antennas **don't radiate power equally in all directions**
  - Specific to the antenna design
- Model these gains in the directions of interest between transmitter, receiver:
  - **Transmit antenna gain**  $G_t$
  - **Receive antenna gain**  $G_r$



# Friis Free Space Channel Model

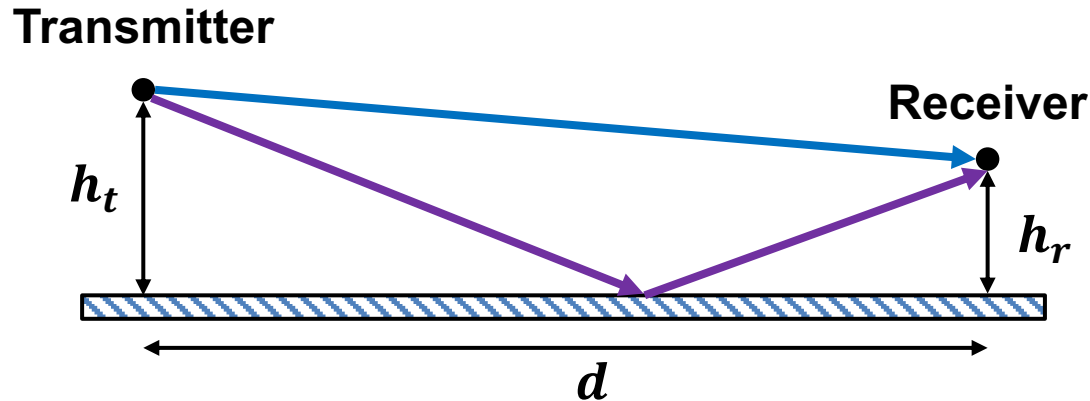
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- **Power received**  $P_r$  is the product of the power received by idealized antennas, times transmit and receive antenna gains:

$$P_r = \frac{P_t G_t G_r \lambda^2}{(4\pi)^2 d^2}$$

# Ground Reflection (Two-Ray) Propagation Model

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- Commonly occurs in mobile cellular environments
- Near transmitter: multipath oscillation due to constructive and destructive interference
- Far from transmitter ( $d \gg h_t, h_r$ ), reflection always approximately out of phase with line of sight path: rapid attenuation

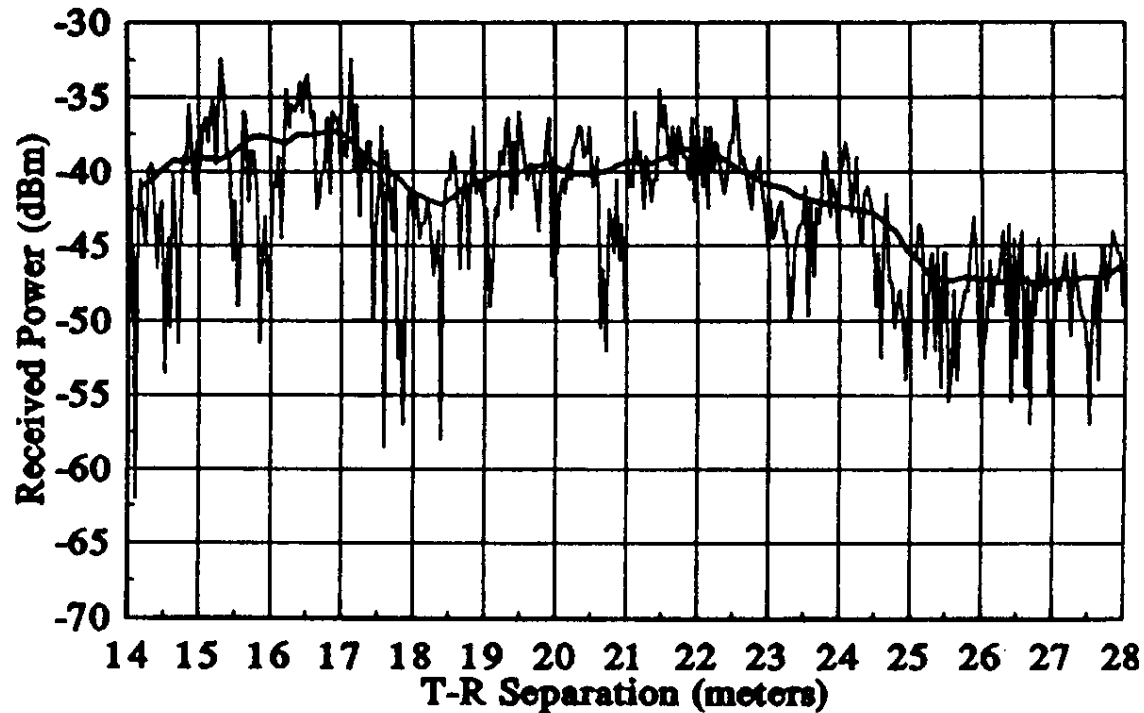
# Today

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1. Large scale channel models
- 2. Small-scale channel models**
3. Equalization: Coping with the channel

# Small-scale versus large-scale modeling

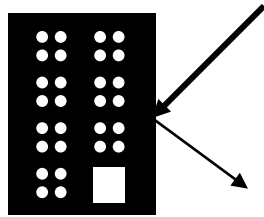
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- **Small-scale models:** Characterize the channel over **at most** a few **wavelengths** or a few **seconds**

# Radio Propagation Mechanisms

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reflection



scattering



diffraction

- Reflection
  - Propagation wave impinges on object large compared to  $\lambda$ 
    - e.g. the surface of the Earth, buildings, walls, etc.
- Diffraction
  - Path from transmitter to receiver obstructed by surface with sharp irregular edges
  - Waves bend around obstacle, even when LOS (line of sight) does not exist
- Scattering
  - Objects smaller than radio wavelength (i.e. foliage, street signs etc.)



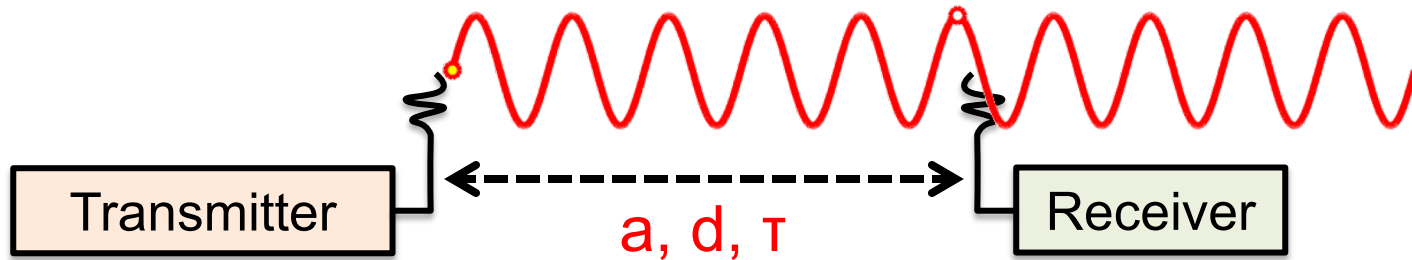
# Multipath Radio Propagation

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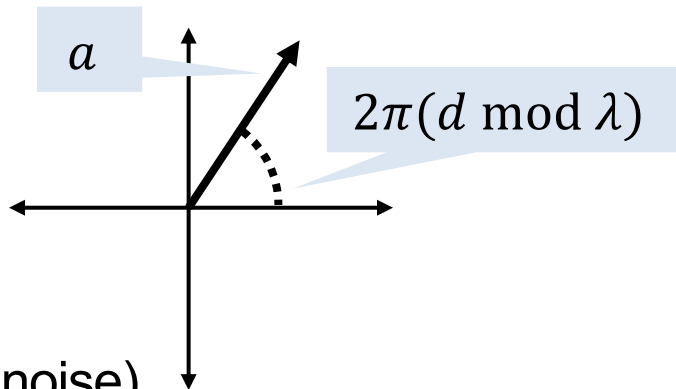
- Receiver gets **multiple copies** of signal
  - Each copy follows **different path**, with **different path length**
  - Copies can **either strengthen or weaken** each other
    - Depends on whether they are **in or out of phase**
- Enables communication even when transmitter and receiver are not in “line of sight”
  - Allows radio waves effectively to propagate around obstacles, thereby **increasing the radio coverage area**
- Transmitter, receiver, or environment object **movement** on the order of  $\lambda$  significantly affects the outcome
  - e.g. 2.4 GHz  $\rightarrow \lambda = 12$  cm, 900 MHz  $\rightarrow \approx 1$  ft

# Sinusoidal carrier, line of sight only

- Baseband transmitted signal:  $x(t) = 1 + 0j$ 
  - Transmitted signal:  $\cos(2\pi f_c t)$

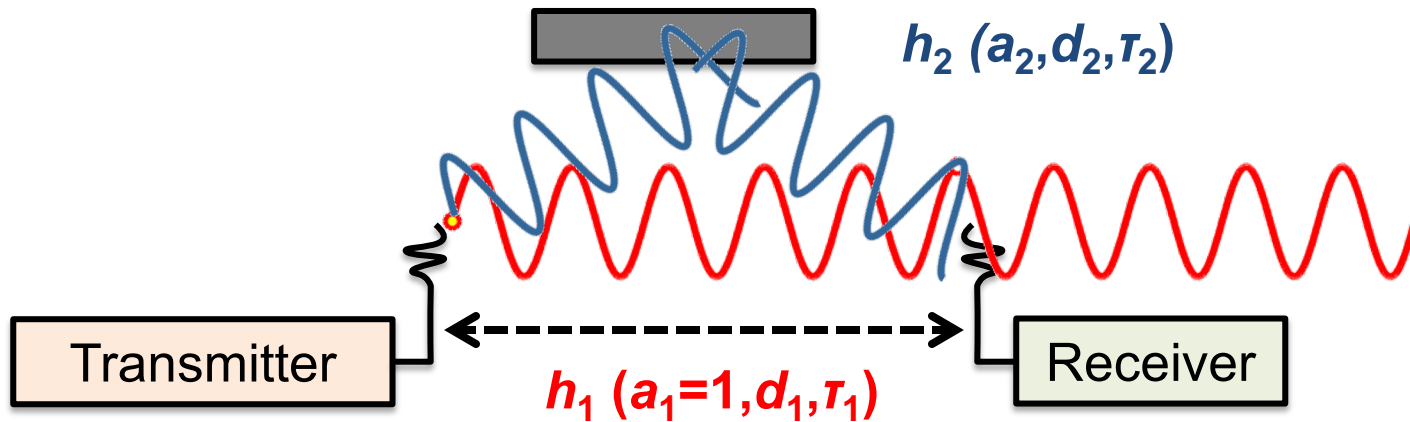


- Represent path **attenuation**  $a$ , **length**  $d$  with a complex number:
  - **Complex channel**  $h = ae^{j2\pi d/\lambda}$

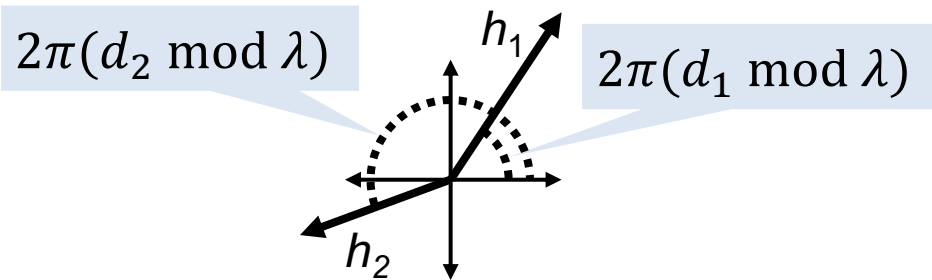


- **Received signal:**  $y(t) = h \cdot x(t)$  (no noise)

# Adding a reflecting path



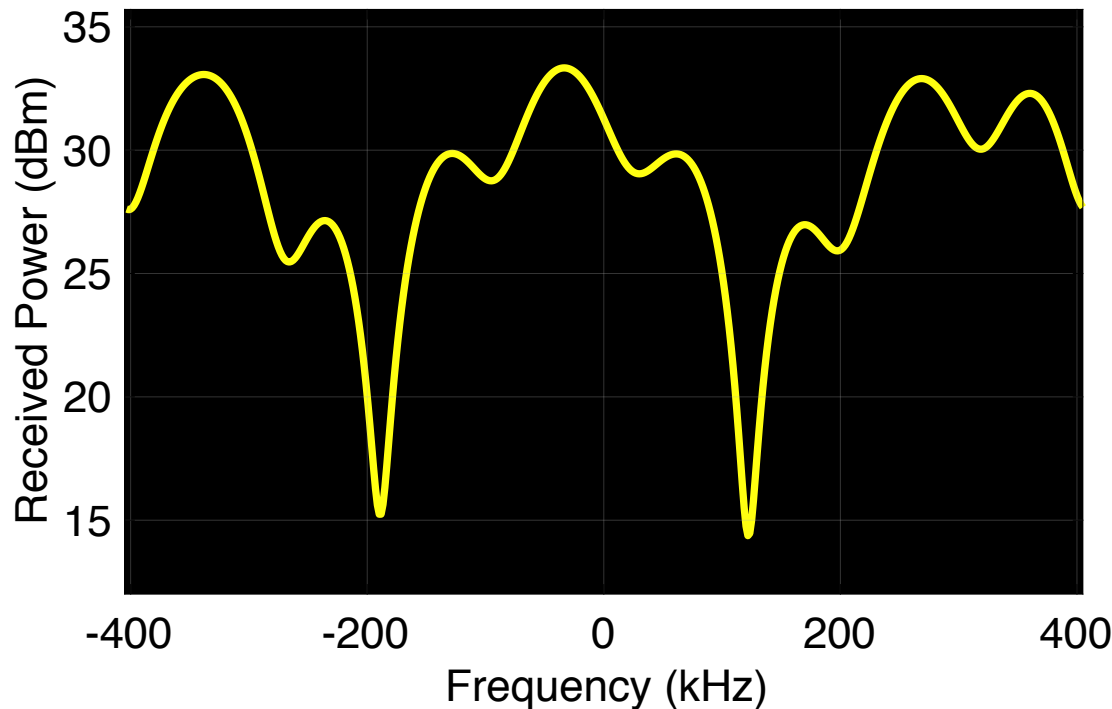
- Channel is now  $h = h_1 + h_2 = a_1 e^{j2\pi d_1/\lambda} + a_2 e^{j2\pi d_2/\lambda}$



- Conclusion:** At different  $\lambda$ , fading is **different** in frequency

# Reflections cause frequency selectivity

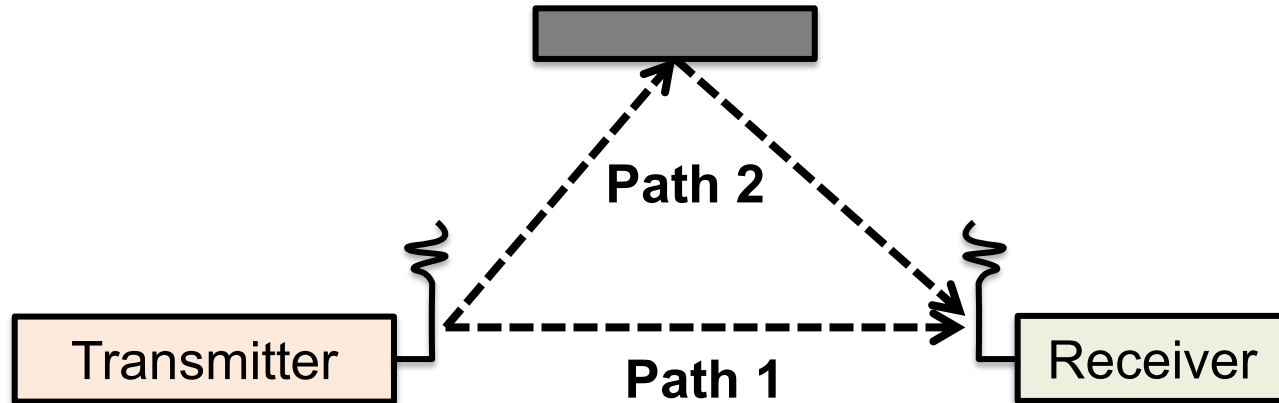
- Interference between reflected and line-of-sight radio waves results in **frequency dependent fading**



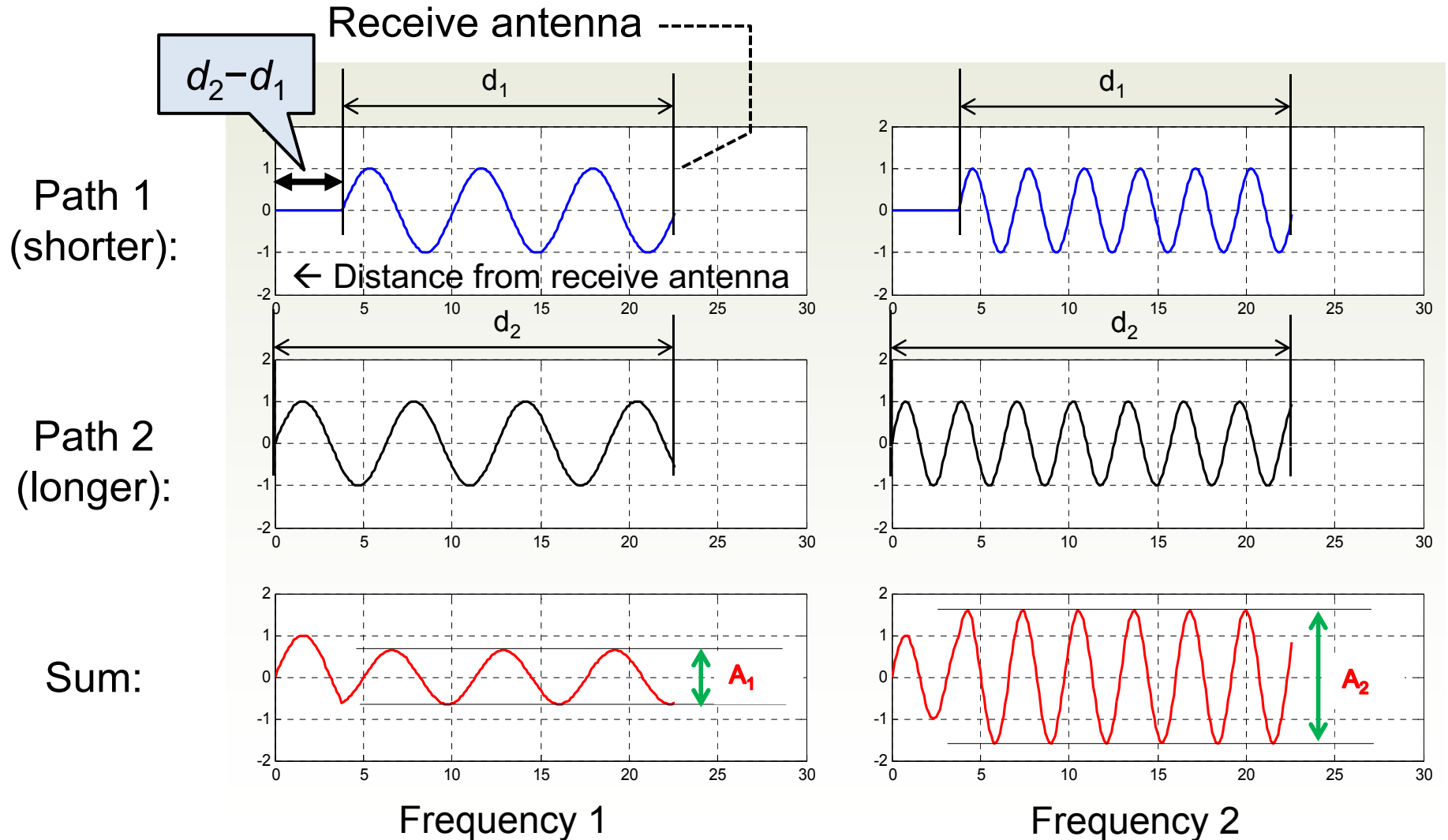
- Coherence bandwidth  $B_c$** : **Frequency range** over which the channel is roughly the **same** (“flat”)

# How does frequency selectivity arise? (Another look)

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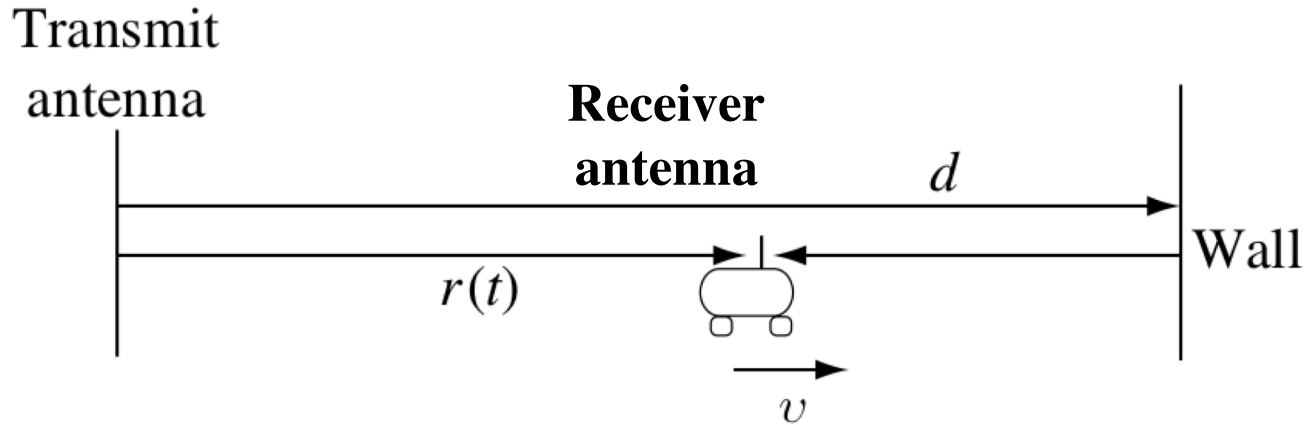


# How does frequency selectivity arise? (Another look)



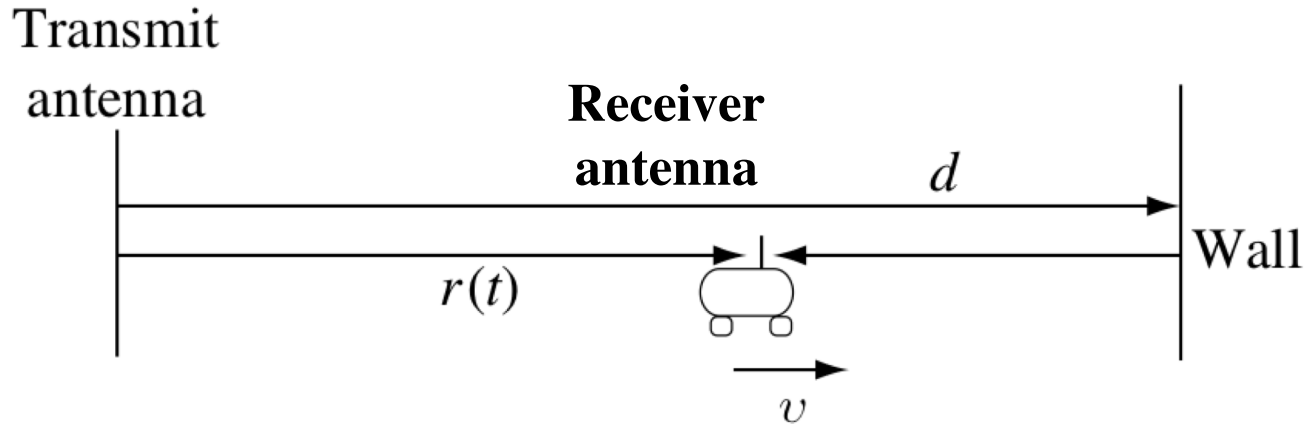
# Stationary transmitter, moving receiver

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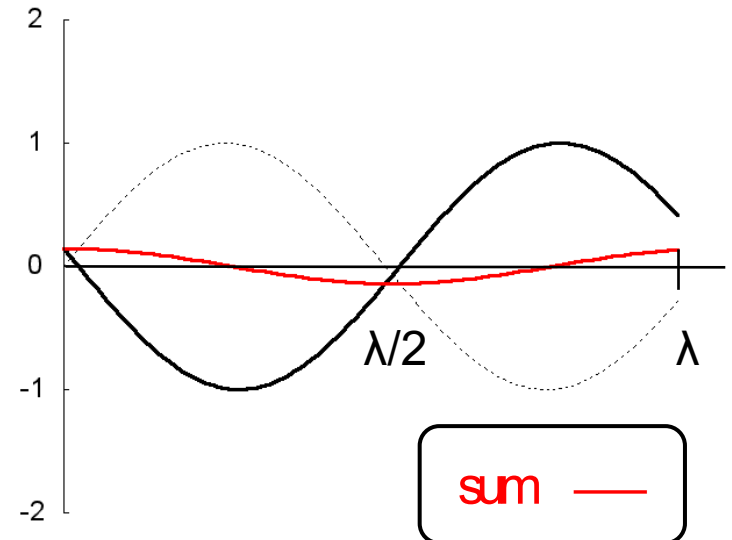


- Suppose **reflecting wall**, fixed transmit antenna, no other objects
  - Receive antenna moving rightwards at velocity  $v$
- **Two arriving signals** at receiver antenna with **path length difference**  $2(d - r(t))$

# How does fading in time arise?



- **Path length difference**  $\Delta = 2(d - r(t))$
- If  $\Delta \pmod{\lambda} = \frac{\lambda}{2} \rightarrow$  receive  $\approx 0$ 
  - **Destructive interference**
- If  $\Delta \pmod{\lambda} = 0 \rightarrow$  receive  $\approx 2$ 
  - **Constructive interference**





# Channel Coherence Time

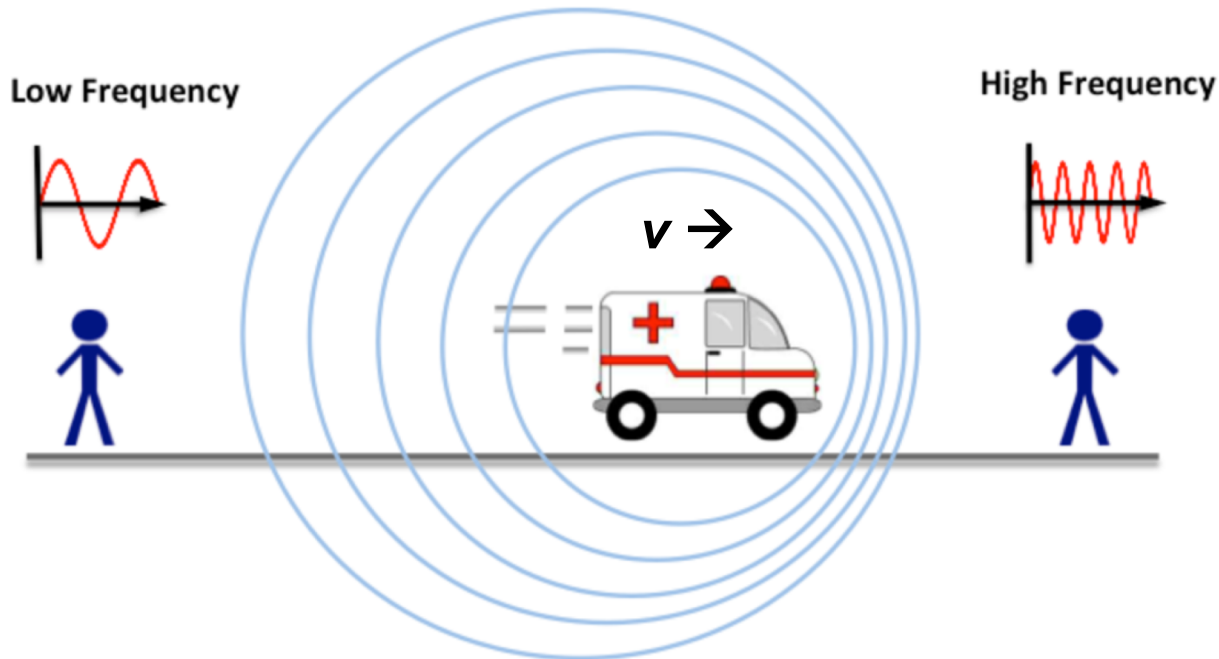
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- Radio carrier frequency  $f = c/\lambda$ 
  - Speed of light:  $c$ ; Wavelength of the signal:  $\lambda$
- Change in path length difference of  $\lambda/2$  moves from constructive to destructive interference
  - Receiver movement of  $\lambda/4$ : **coherence distance**
  - **Time** transmitter, receiver, or objects in environment take to move a coherence distance: **channel coherence time  $T_c$** 
    - Walking speed (2 mph) @ 2.4 GHz:  $\approx 15$  milliseconds
    - Driving speed (20 mph) @ 1.9 GHz:  $\approx 2.5$  milliseconds
    - Train/freeway speed (75 mph) @ 1.9 GHz:  $< 1$  millisecond

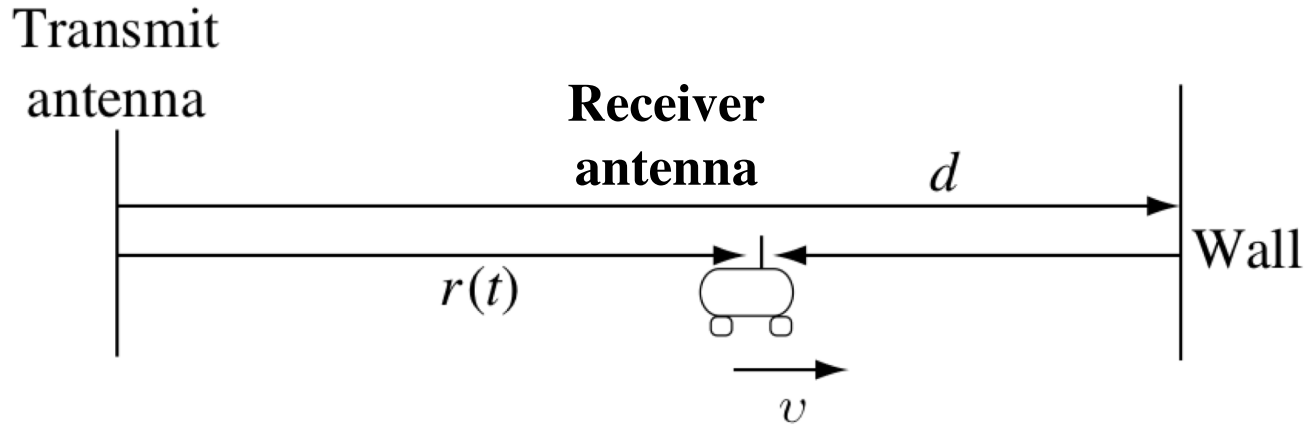
# Another perspective: Doppler Effect

- Movement by the transmitter, receiver, or objects in the environment creates a **Doppler Shift**

$$\Delta f = \left(\frac{v}{c}\right) f$$



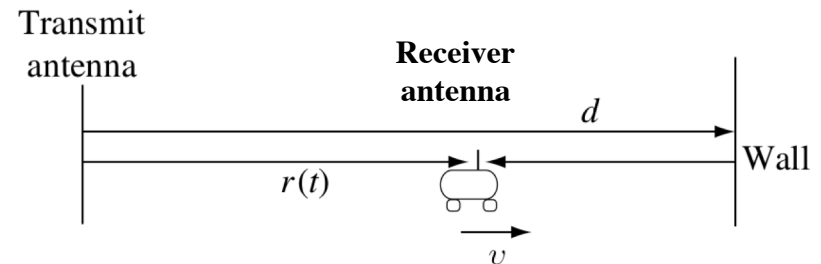
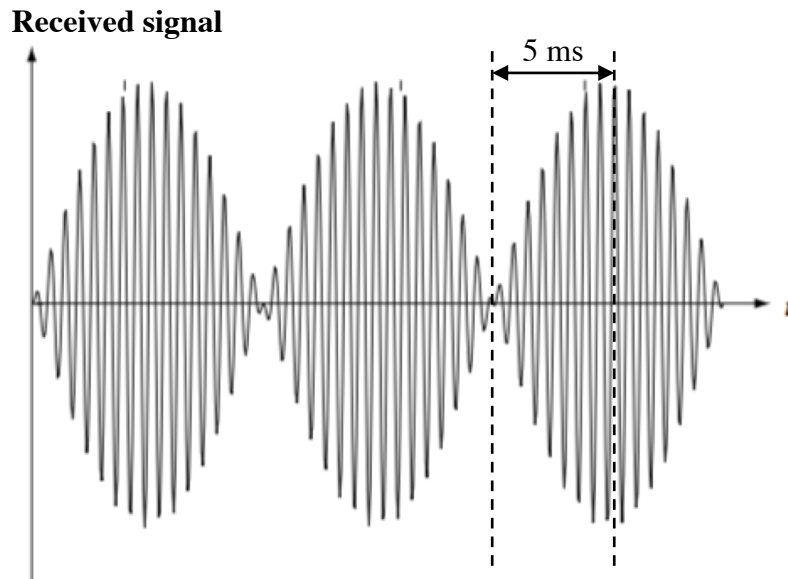
# Stationary transmitter, moving receiver: From a Doppler Perspective



- **Doppler Shift of a path**  $\Delta f = \frac{f_c \cdot v_{radial}}{c}$ 
  - $v_{radial}$  is the **radial** component of the receiver's velocity vector **along the path**
    - **Positive  $\Delta f$**  with **decreasing path length**, **negative  $\Delta f$**  with **increasing path length**
- Suppose  $v = 60$  km/h,  $f_c = 900$  MHz
  - Direct path  $\Delta f = -50$  Hz, reflection path  $\Delta f = +50$  Hz

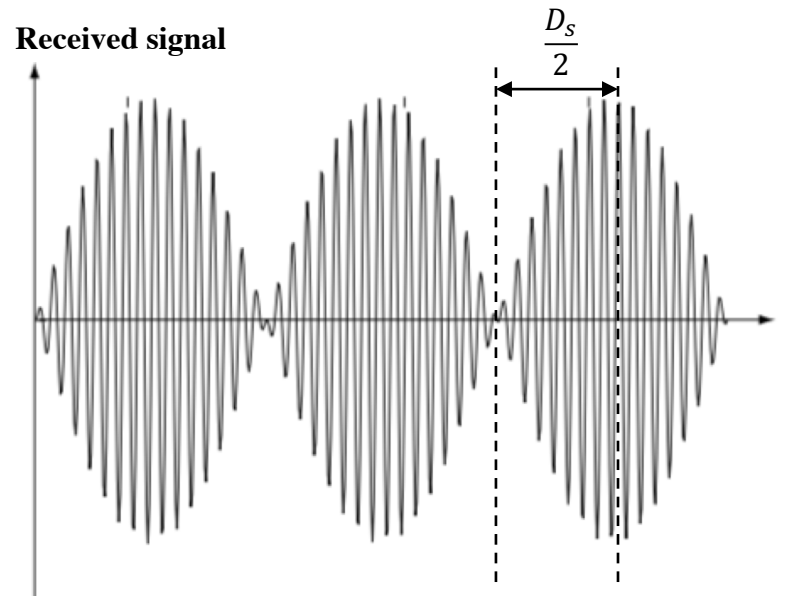
# Stationary transmitter, moving receiver: From a Doppler Perspective

- **Channel Doppler Spread  $D_s$** : maximum path Doppler shift, minus minimum path Doppler shift
- Suppose  $v = 60 \text{ km/h}$ ,  $f_c = 900 \text{ MHz}$ 
  - Direct path  $\Delta f = -50 \text{ Hz}$ , reflection path  $\Delta f = +50 \text{ Hz}$
  - Doppler Spread: **100 Hz**
- Results in sinusoidal “envelope” at frequency  $D_s / 2$ :



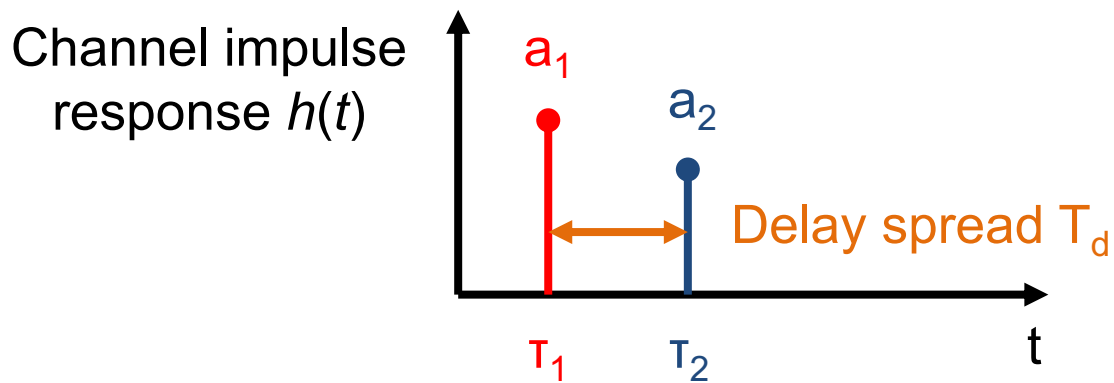
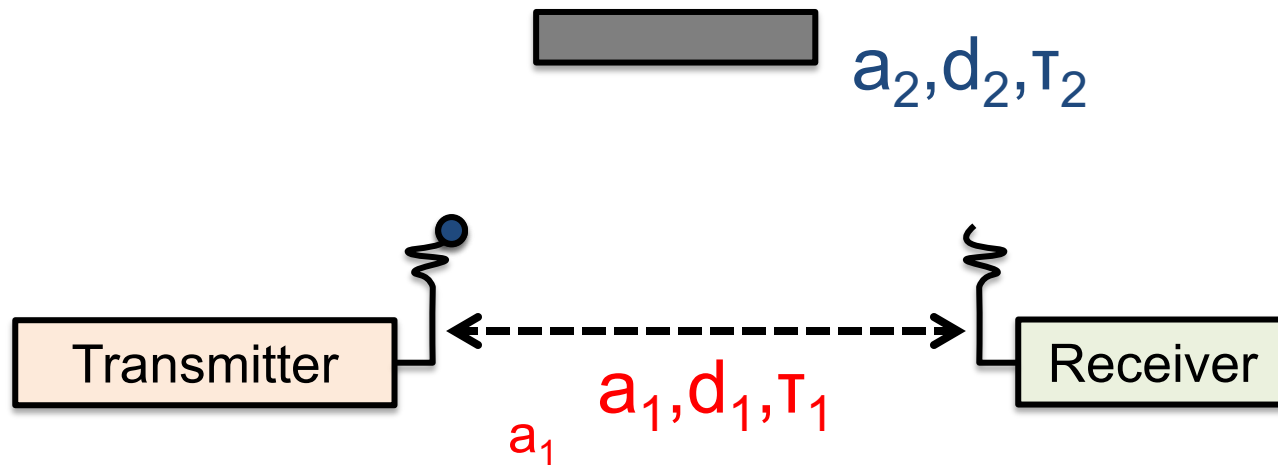
# Channel Coherence Time: From a Doppler Perspective

- Sinusoidal “envelope” at frequency  $\frac{D_s}{2}$ :



- Transition from 0 to peak in  $\frac{1}{2D_s}$ 
  - So **qualitatively significant** change in time  $T_c = \frac{1}{4D_s}$ 
    - Alternate definition of **channel coherence time**

# What does the channel look like in time?

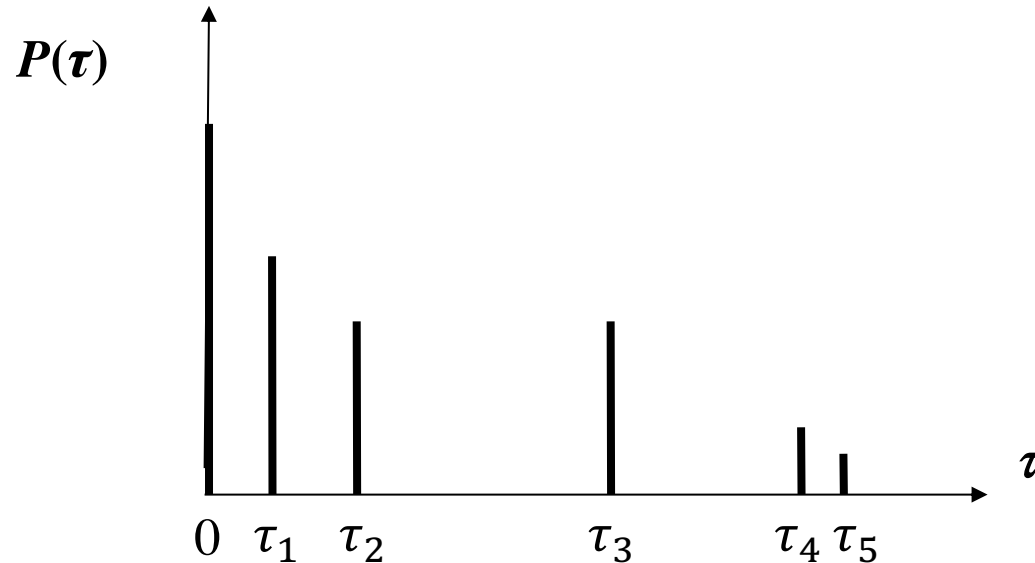


# Power delay profile (PDP)

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- **Power** received via the path with **excess time delay**  $\tau_i$  is the value (height) of the discrete PDP component at  $\tau_i$

$P(\tau)$  corresponds to  $|h(\tau)|^2$



# Characterizing a power delay profile

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- Given a PDP  $P(\tau_k)$  sampled at time steps  $\tau_k$ :

- **Mean excess delay**  $\bar{\tau}$ : Expected value of  $P(\tau_k)$ :

$$\bar{\tau} = \frac{\sum_k P(\tau_k) \tau_k}{\sum_k P(\tau_k)}$$

- **Root mean squared (RMS) delay spread**  $\sigma_\tau$  measures the spread of the power's arrival in time
  - RMS delay spread is the variance of  $P(\tau_k)$ :

$$\sigma_\tau = \sqrt{\overline{\tau^2} - (\bar{\tau})^2}, \text{ where } \overline{\tau^2} = \frac{\sum_k P(\tau_k) \tau_k^2}{\sum_k P(\tau_k)}$$

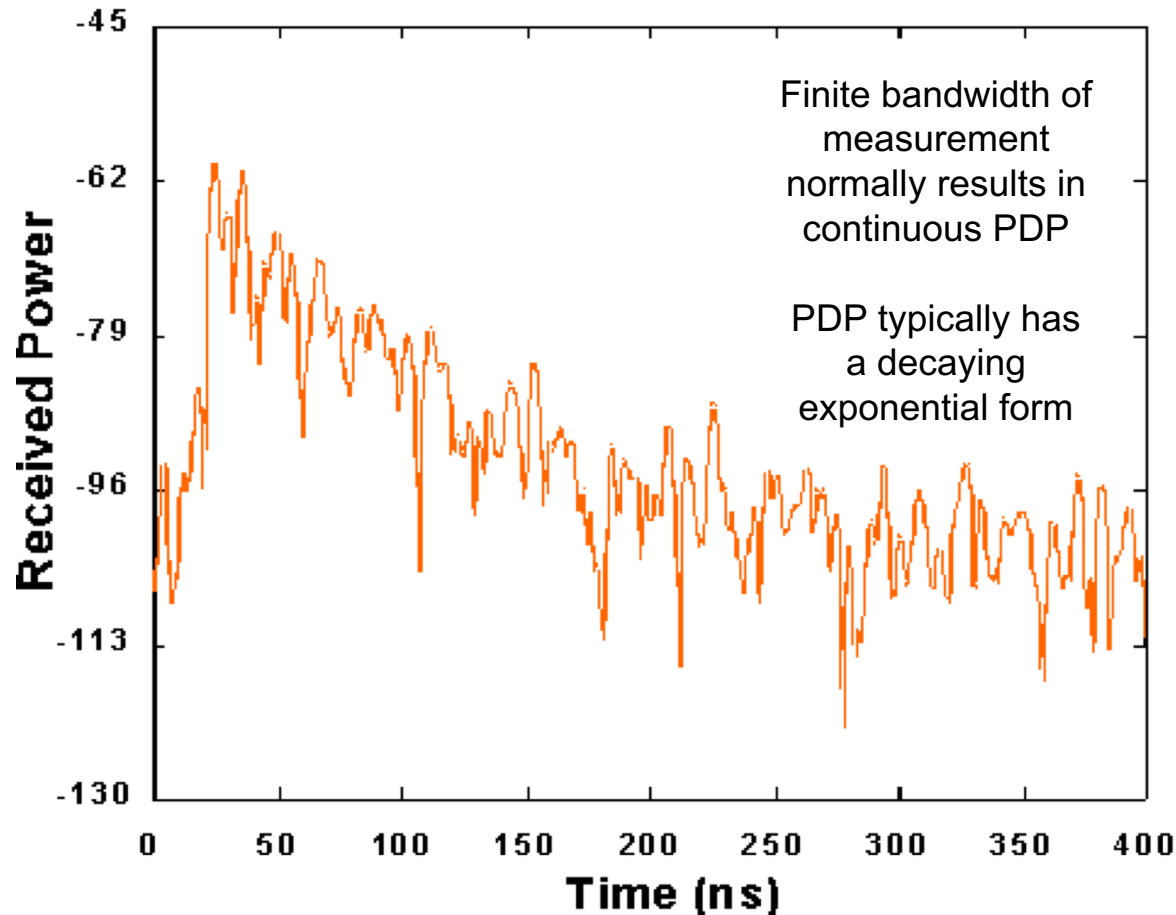
- **Maximum excess delay < X dB**  $\tau_{<X}$  is the **greatest** delay at which the PDP is **greater than X dB below** the strongest arrival in the PDP



# Example Indoor PDP Estimation

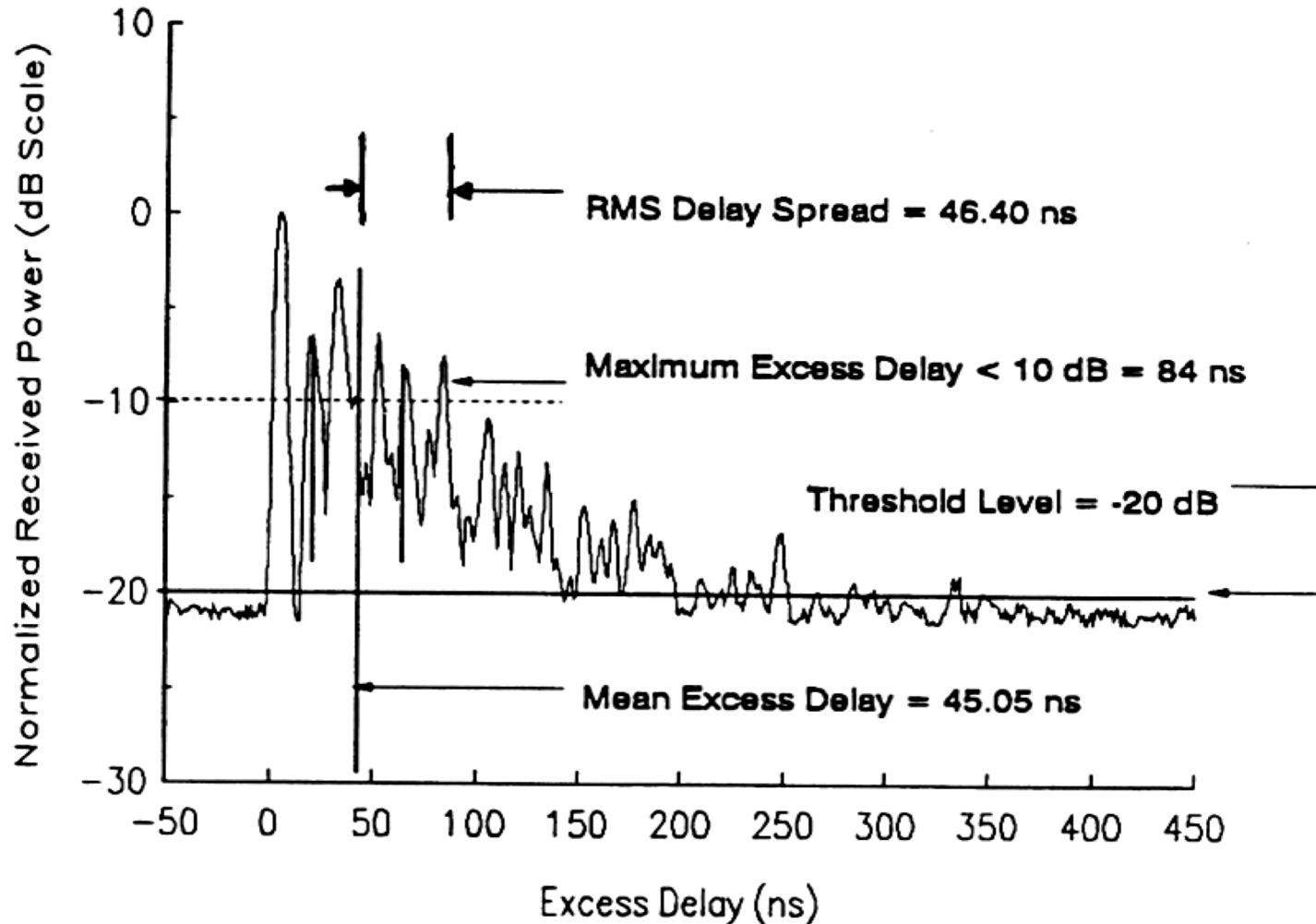
## Typical RMS delay spreads

Instantaneous Impulse Response

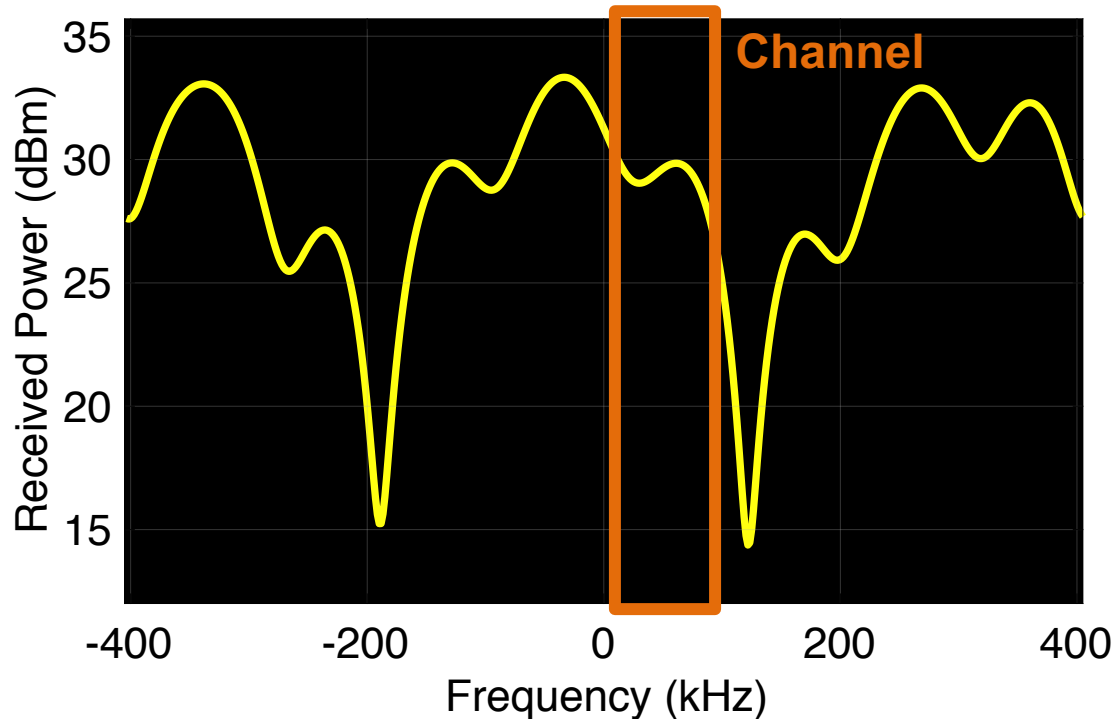


Environment	RMS delay spread
Indoor cell	10 – 50 ns
Satellite mobile	40 – 50 ns
Open area (rural)	< 0.2 $\mu$ s
Suburban macrocell	< 1 $\mu$ s
Urban macrocell	1 – 3 $\mu$ s
Hilly macrocell	3 – 10 $\mu$ s

# Indoor power delay profile



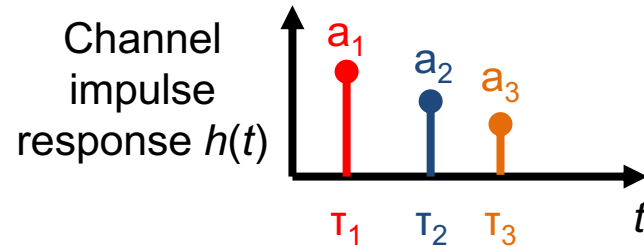
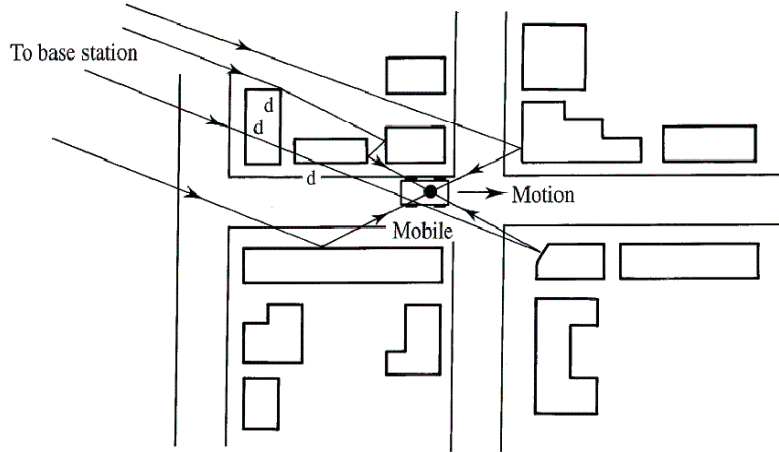
# Flat Fading



- Slow down → sending data over a **narrow bandwidth** channel
  - Channel is **constant** over its bandwidth
  - **Multipath is still present**, so channel strength fluctuates **over time**
    - **How to model this fluctuation?**

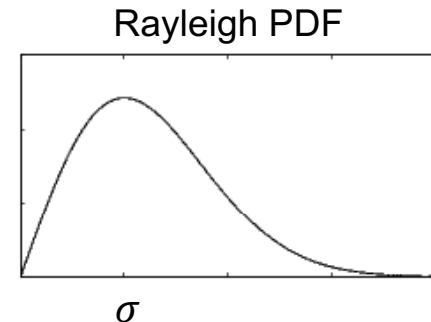
Not shown above!

# Rayleigh Fading Model

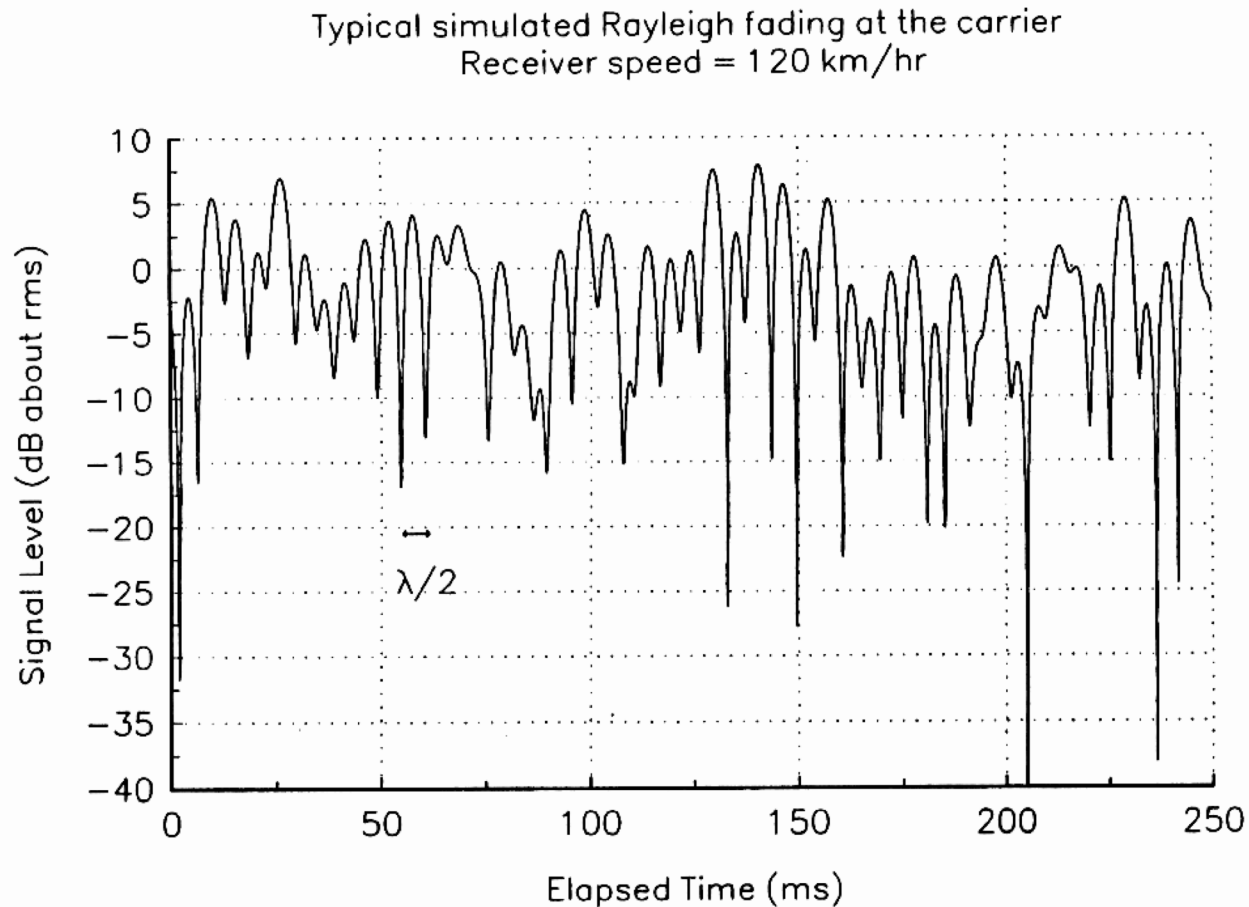


- Random gain of  $k^{\text{th}}$  arriving path:  $a_k = a_k^I + ja_k^Q$
- Therefore, the I and Q **channel components**  $h_I, h_Q$  are **zero-mean Gaussian distributed**

- So  $|h| = \sqrt{h_I^2 + h_Q^2}$  is **Rayleigh-distributed**



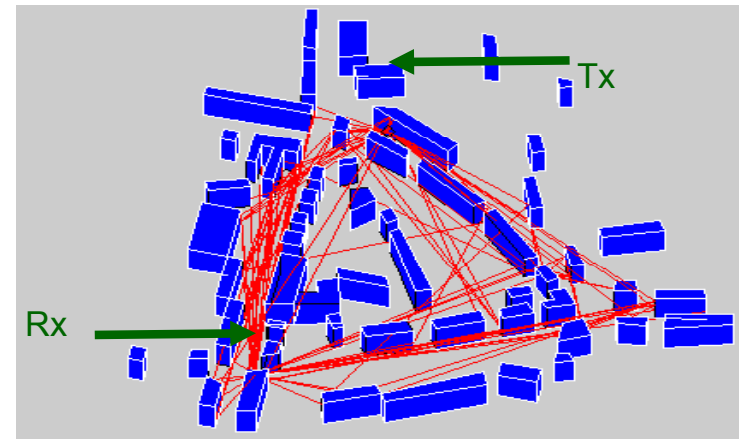
# Rayleigh fading example



**Figure 5.15** A typical Rayleigh fading envelope at 900 MHz [from [Fun93] © IEEE].

# Putting it all Together: Ray Tracing

- Approximate solutions to Maxwell's electromagnetic equations by instead **representing wavefronts as particles, traveling along rays**
  - Apply geometric reflection, diffraction, scattering rules
    - Compute angle of reflection, angle of diffraction
- Error is smallest when **receiver is many  $\lambda$  from nearest scatterer**, and all **scatterers are large relative to  $\lambda$**
- Good match to empirical data in rural areas, along city streets (radios close to ground), and indoors
- **Completely site-specific**
  - Changes to site may **invalidate model**

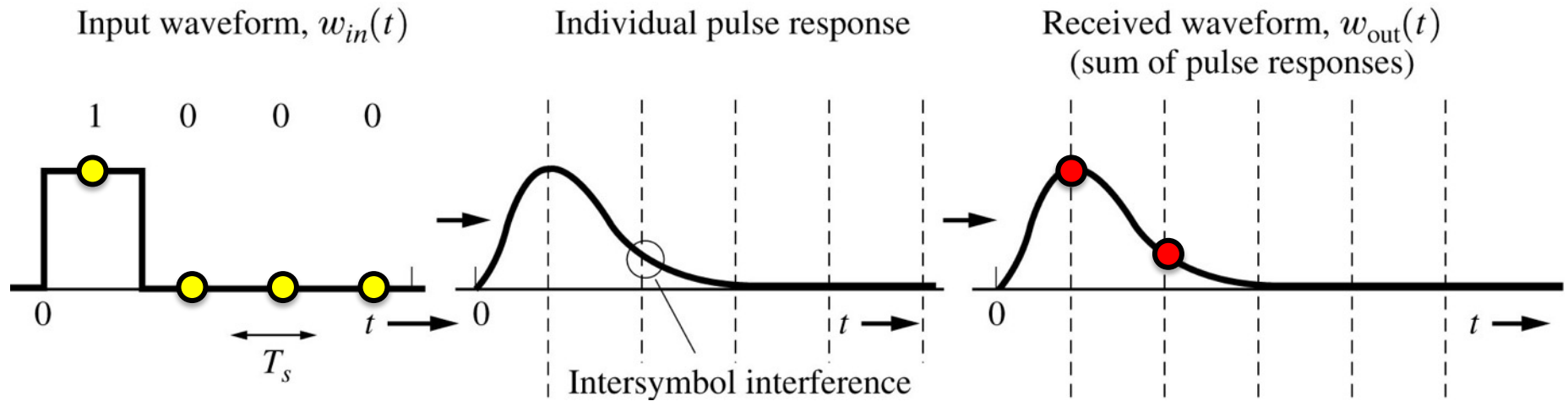


# Today

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1. Large scale channel models
2. Small-scale channel models
- 3. Equalization: Coping with the channel**

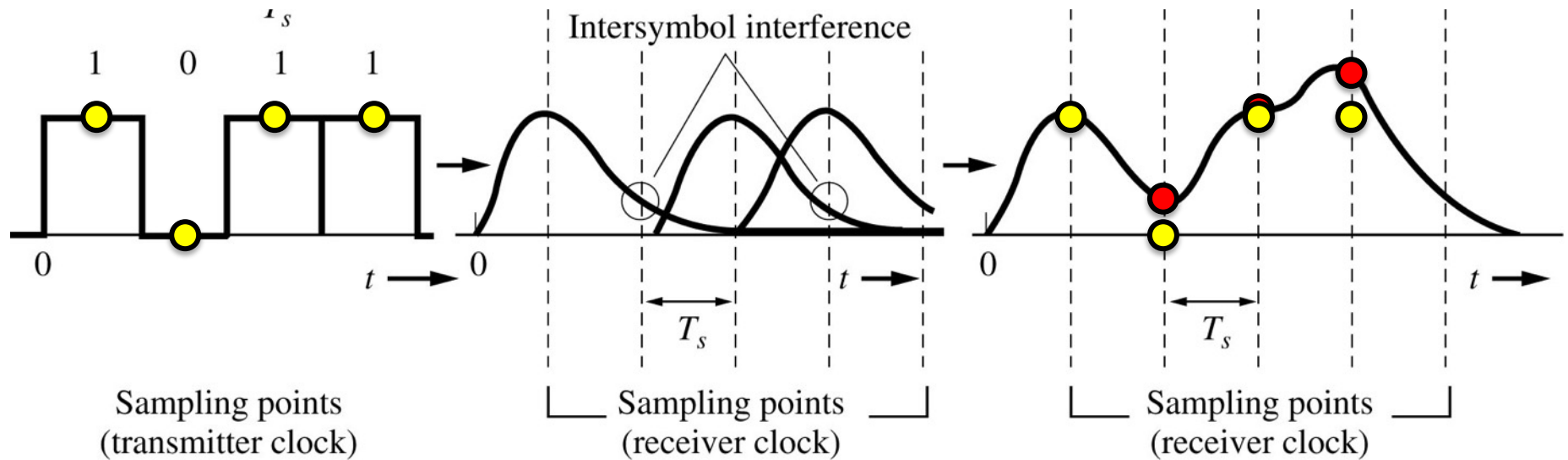
# Problem: Inter-symbol interference (ISI)



- Transmitted signal ●
- Received signal with ISI ●

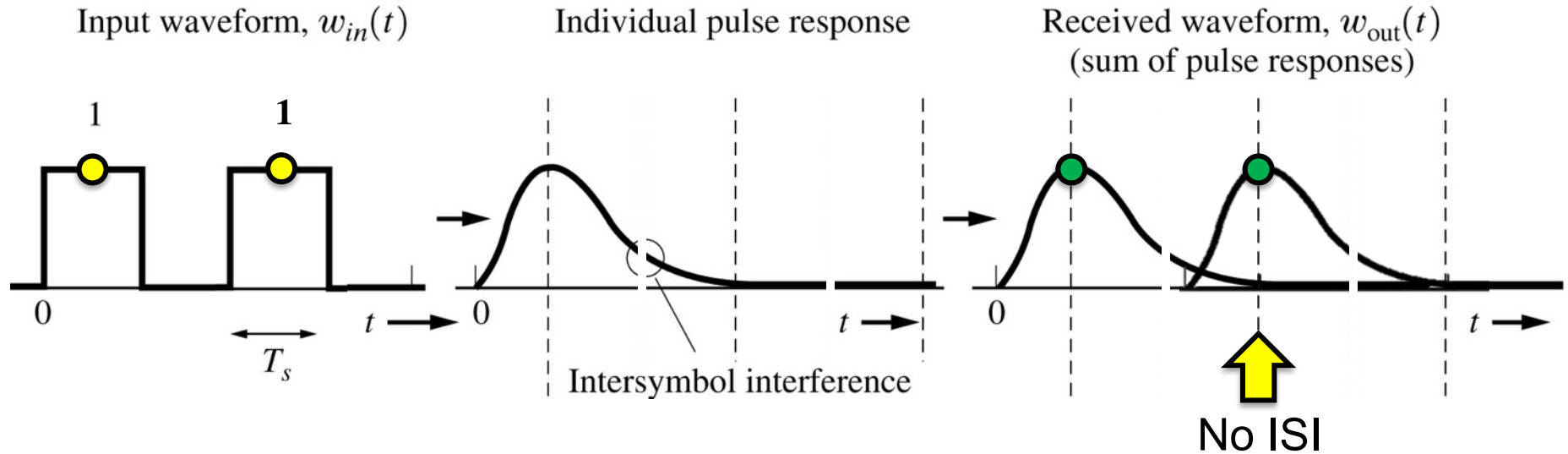


# Problem: Inter-symbol interference (ISI)



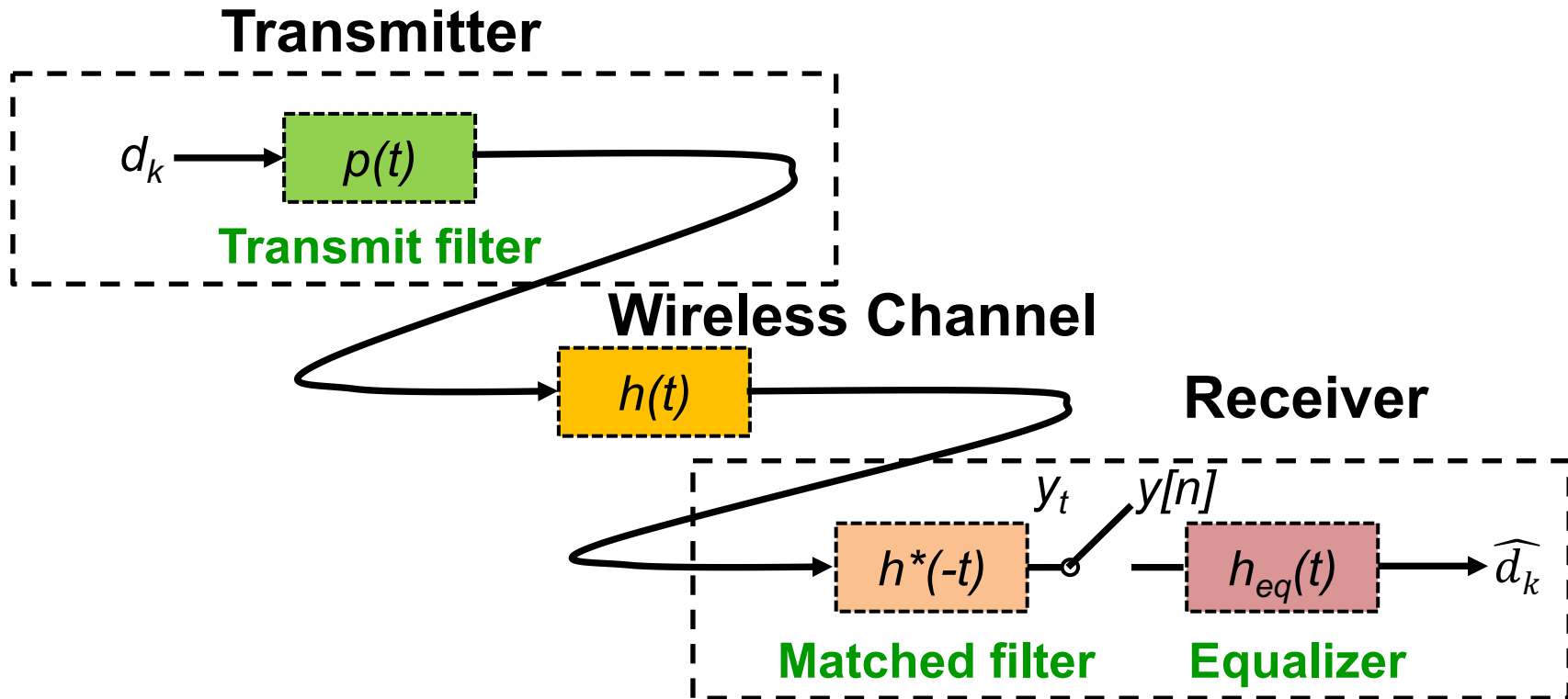
- Transmitted signal ●
- Received signal with ISI ●
- ISI at one symbol **depends on** the value of **other** symbols

# One Solution: Slow down



- Transmitted signal ●
- Received signal ●

# Channel Model

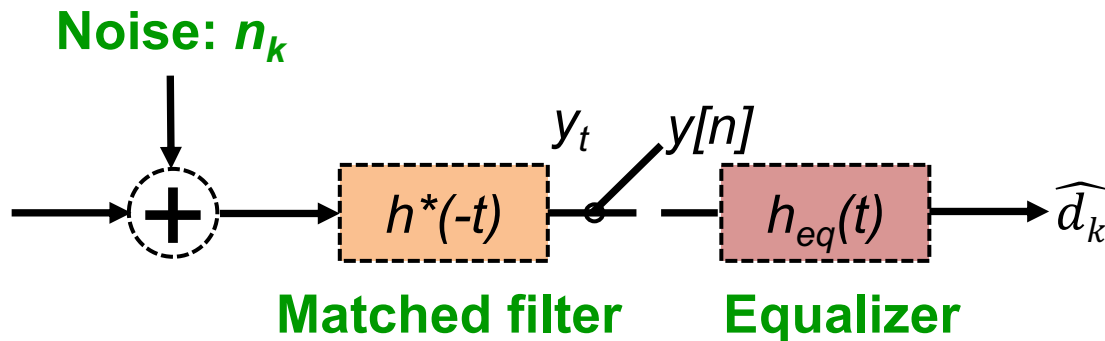


$$f(t) = (p * h)(t) * h^*(-t)$$

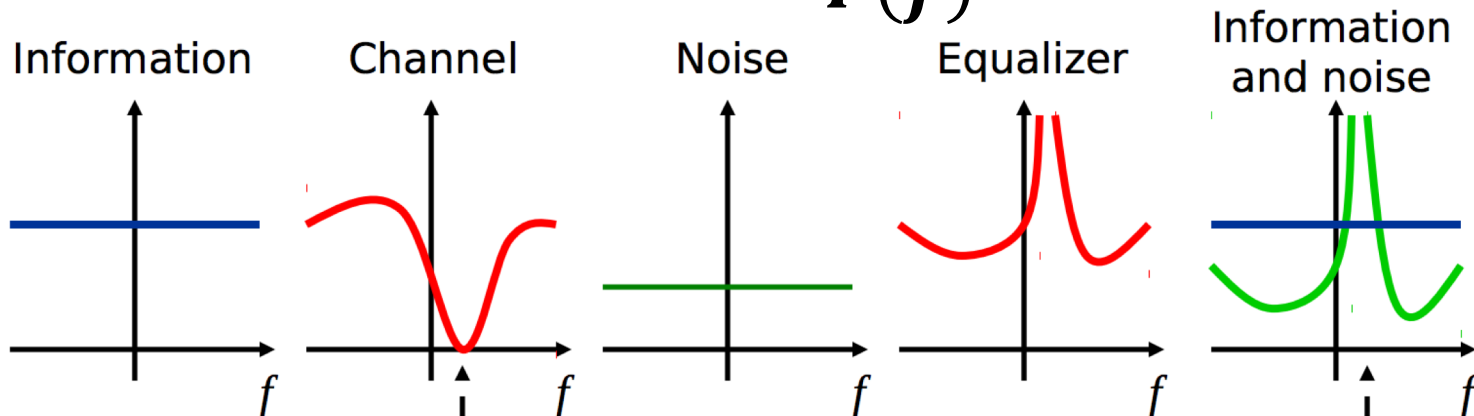
- **Composite channel** (made up of pulse shape, radio channel, and matched filter)

# Another Solution I: Zero-forcing Equalizer

## Receiver



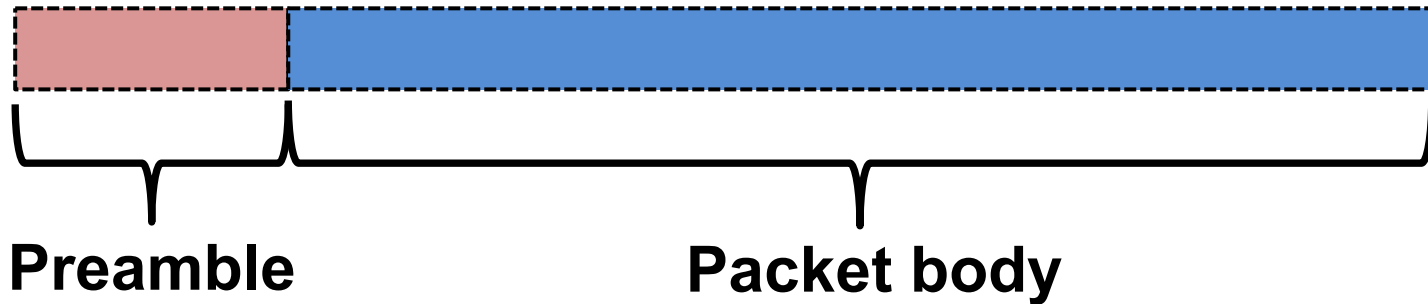
$$H_{eq}(f) = \frac{1}{F(f)}$$



**Noise enhancement!**

# Preamble

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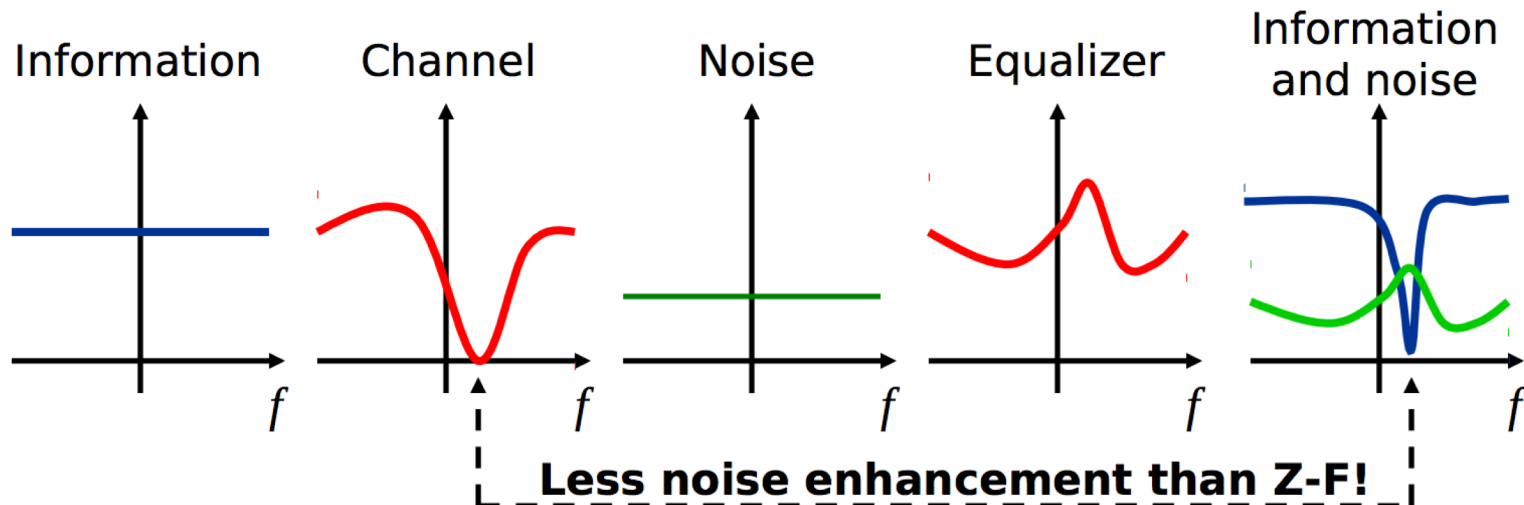
- Sequence of symbols **known to both transmitter & receiver**

# Another Solution II: MSE Equalizer

- **Goal:** Minimizing mean-squared error (MSE) between **received symbols** & **transmitted symbols**

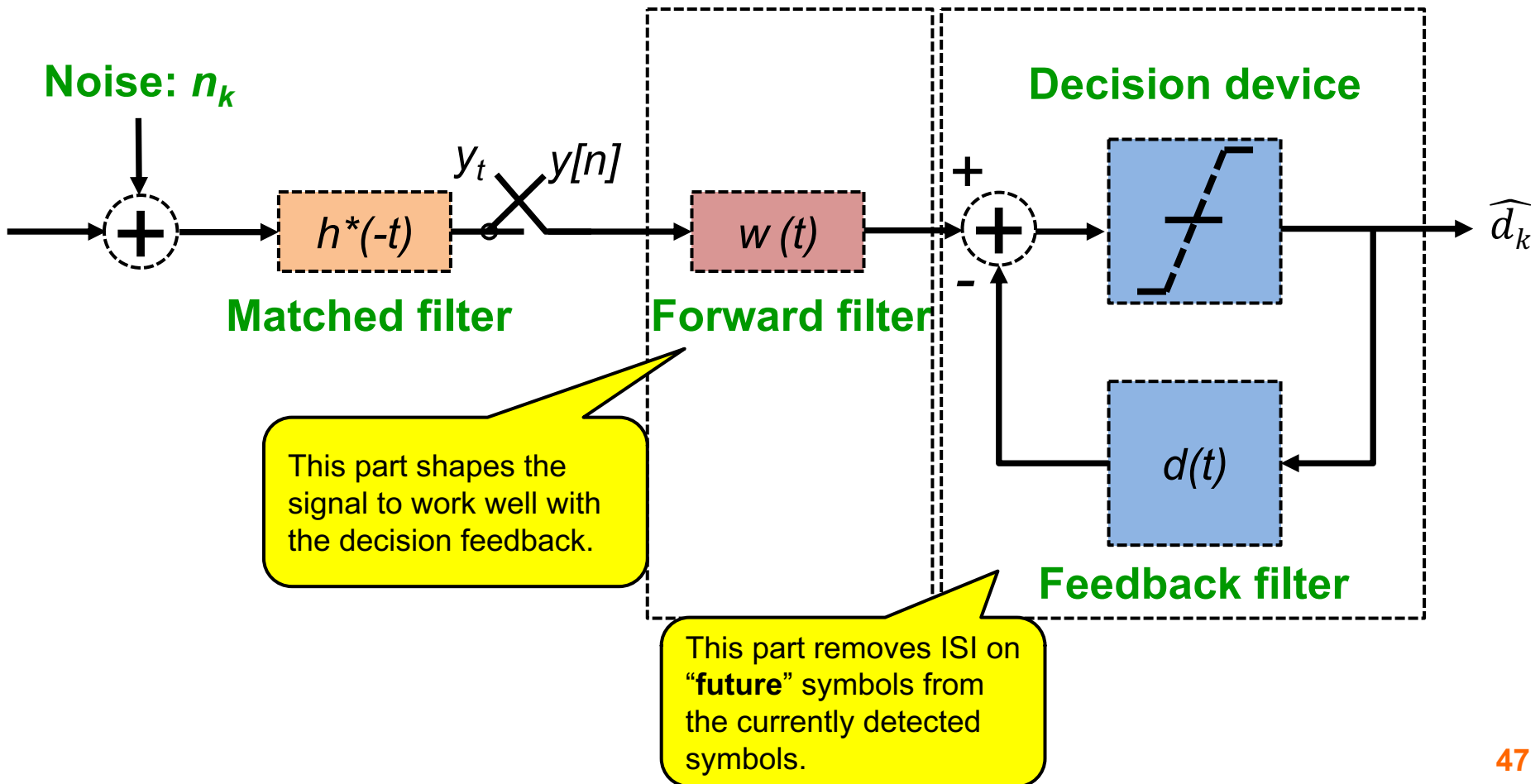
$$MSE = \sum_{k=0}^K |d_k - \widehat{d}_k|^2$$

- **Assumes Receiver has a preamble**



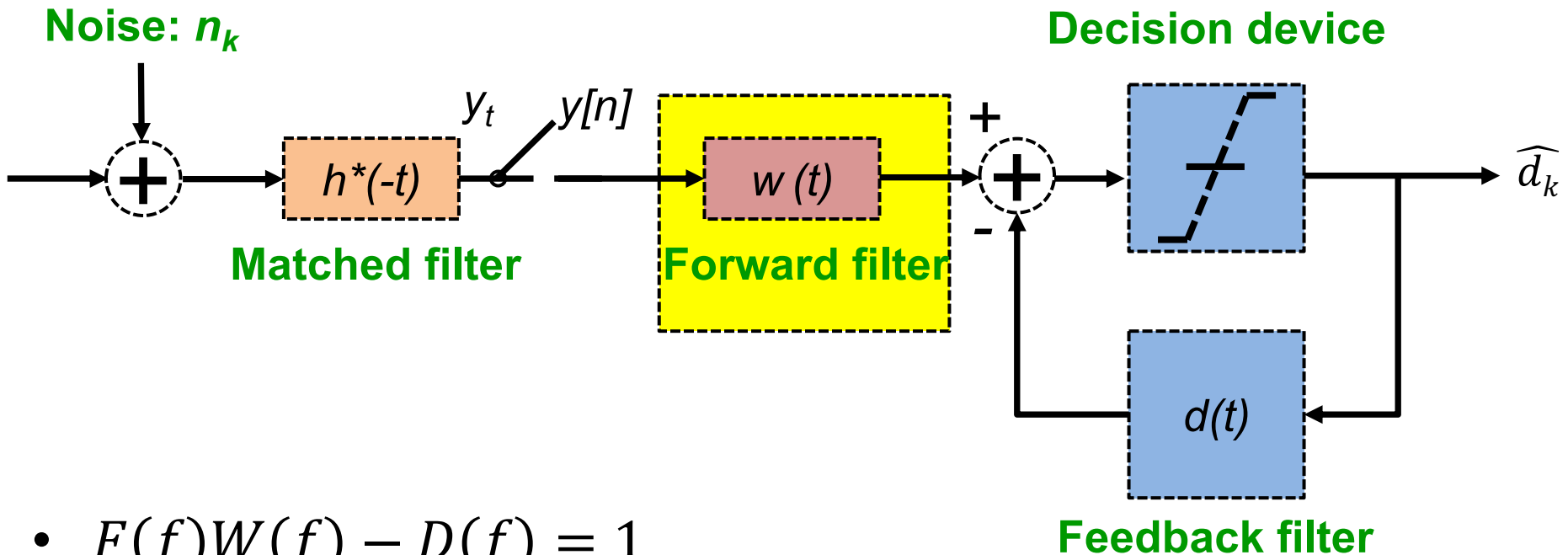
# Another Solution II: Decision-feedback Equalizer

- **Idea:** Subtract the **interference** caused by already detected data (symbols)



# Another Solution II: Decision-feedback Equalizer

- The forward filter  $w(t)$  here uses a **linear equalizer**
  - e.g., **zero-forcing, MSE**



- $F(f)W(f) - D(f) = 1$
- The DFE has access to the symbol decisions



**Thursday Topic:**  
**OFDM**

**Friday Precept:**  
**Lab 4: BPSK Radio**