

Time-of-Flight and Ranging Experiments on the Lunar Laser Communication Demonstration



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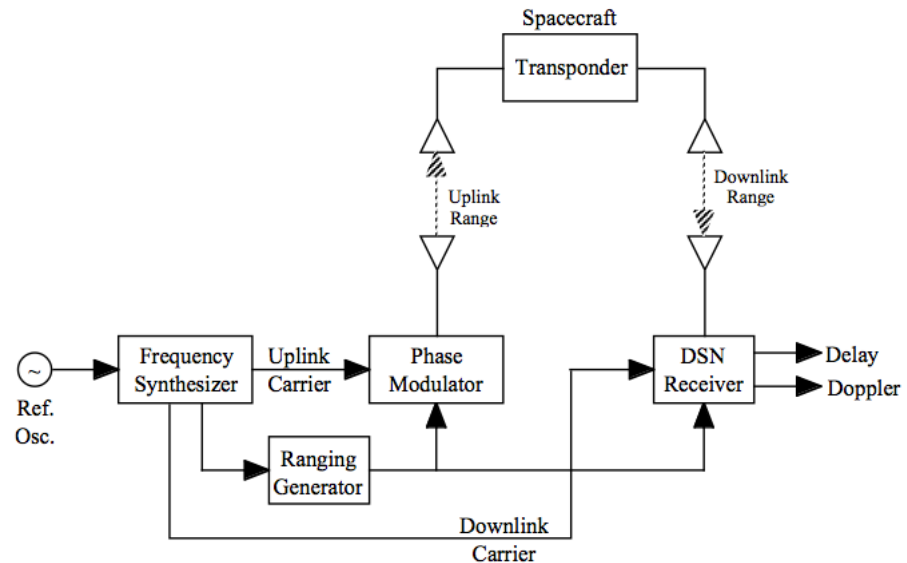
NASA Metric Tracking System



- RF satellite ranging performed using specialized 1-MHz waveforms applied to communication loop-back links
- Precision ranging requires dedicated measurements performed over a period of several hours
- Range accuracies of the order of 10 meters are achievable



**White Sands
S-Band Tracking Antenna**



Loop-Back Configuration

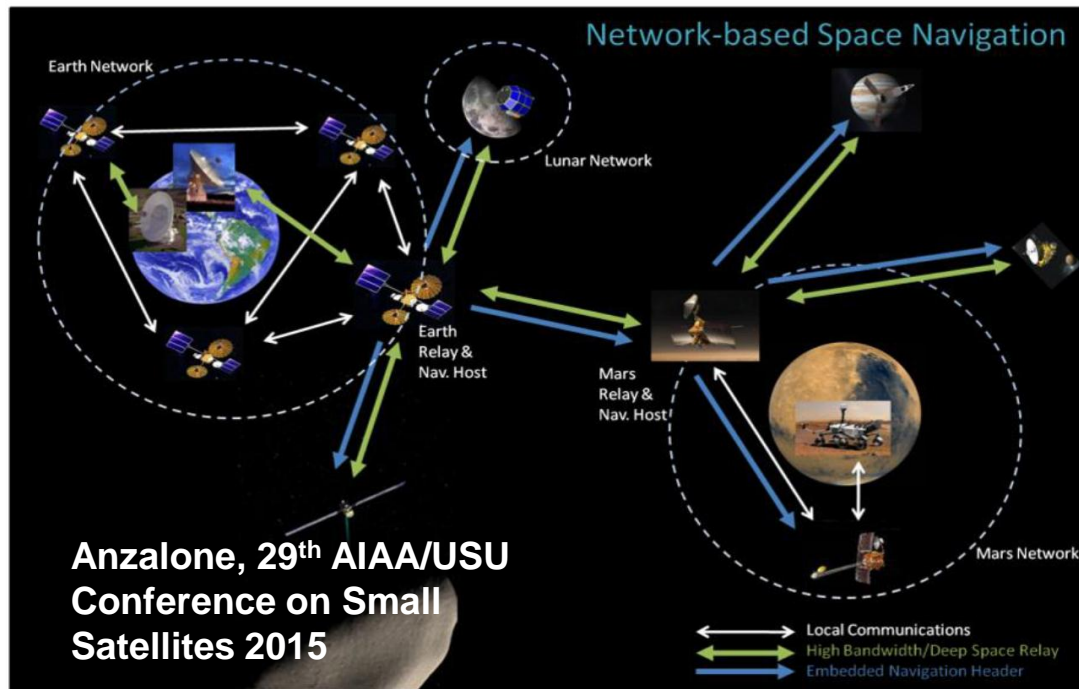


Autonomous Navigation Concept



- NASA MSFC is developing a system architecture for solar-system wide navigation using embedded headers in comm links
- LEO cubesat demo concept in development

NASA's Multi-spacecraft Autonomous Positioning System

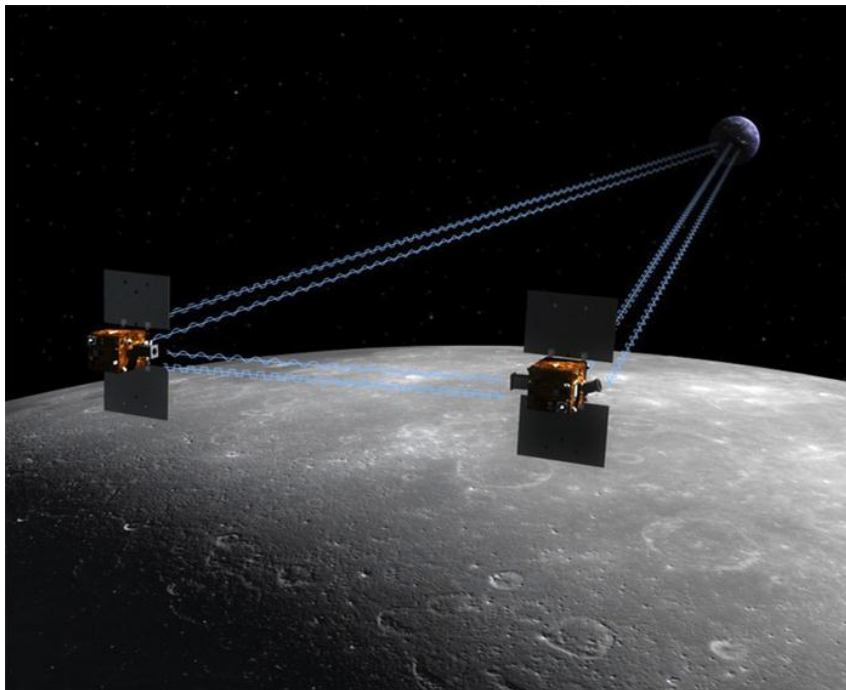




TOF Enables Planetary Science

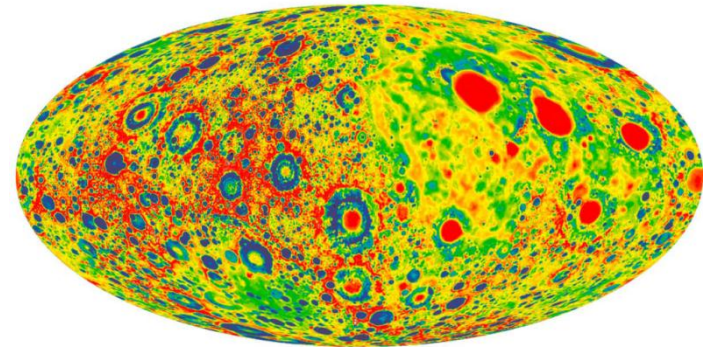


- Time-of-Flight (TOF) measurements are an enabler for:
 - Planetary science, gravity, internal structure of planets, moons



GRAIL: Gravity Recovery and Interior Laboratory
LOLA: Lunar Orbiter Laser Altimeter

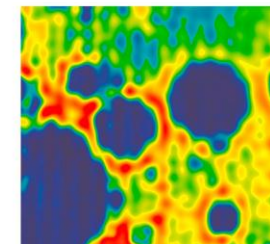
Mollweide Projection of Lunar Gravity Anomalies



Far side

Near side

LOLA laser altimeter



GRAIL gravity anomalies

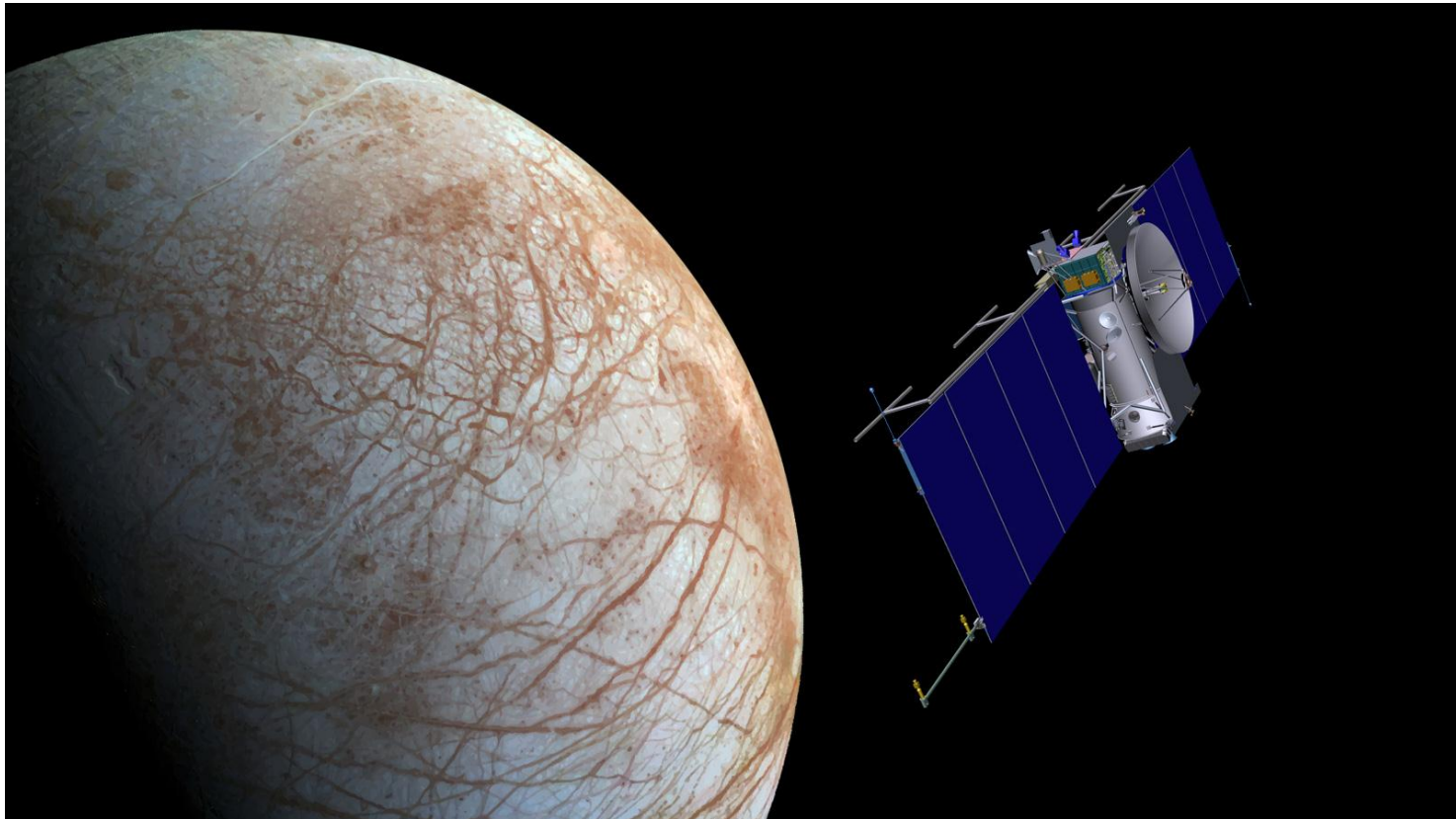
Lemoine, et al.
“High Degree GRAIL Gravity Models”
Journal of Geophysical Research: Planets (2013)



Europa Clipper Mission



- **Primary mission: measure Europa gravity**
 - Look for tidal changes indicative of a liquid ocean that might harbor life





Outline



- **LLCD Mission**
- **TOF System Architecture**
- **TOF Data**



LLCD and LADEE



Lunar Laser Comm Demo

LLCD

- NASA's first lasercom
- High-rate duplex comm
- cm-class real-time ranging using comm signals
- Novel space and ground technologies
- 30-day mission

Lunar Atmosphere and Dust Environment Explorer (LADEE) Science mission – 100 days

- Orbit Moon
- Measure fragile lunar atmosphere
- Measure electrostatically transported dust grains



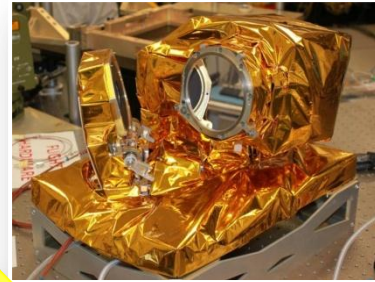


LLCD Space Terminal on LADEE

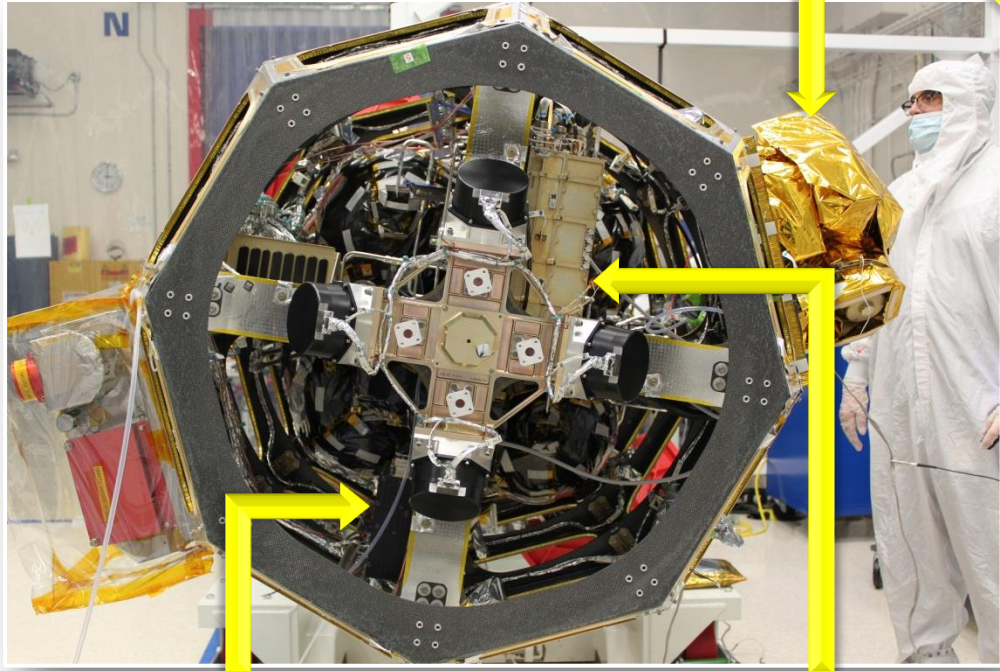


Modular design allowed for balanced placement in small spacecraft. Units fiber- and cable-connected.

LLCD Optical Module



**0.5-W transmitter
4-inch telescope
Fully-gimballed
Inertial stabilization**



LLCD Controller Module LLCD Modem Module

Space Terminal: mass ~ 30 kg; power ~ 90 W





Primary LLCD Ground Terminal (LLGT) at White Sands



Ground Terminal Design

- Single gimbal
- Four 16-inch receive telescopes
- Four 6-inch transmit telescopes
- All fiber-coupled superconducting nanowire single-photon detectors
- Air-conditioned globe for optics
- Clamshell dome for weather protection

Transportable Design

- Novel architecture allows transportability
- Shipping container houses modem, computers, office
- Transported to White Sands NASA site



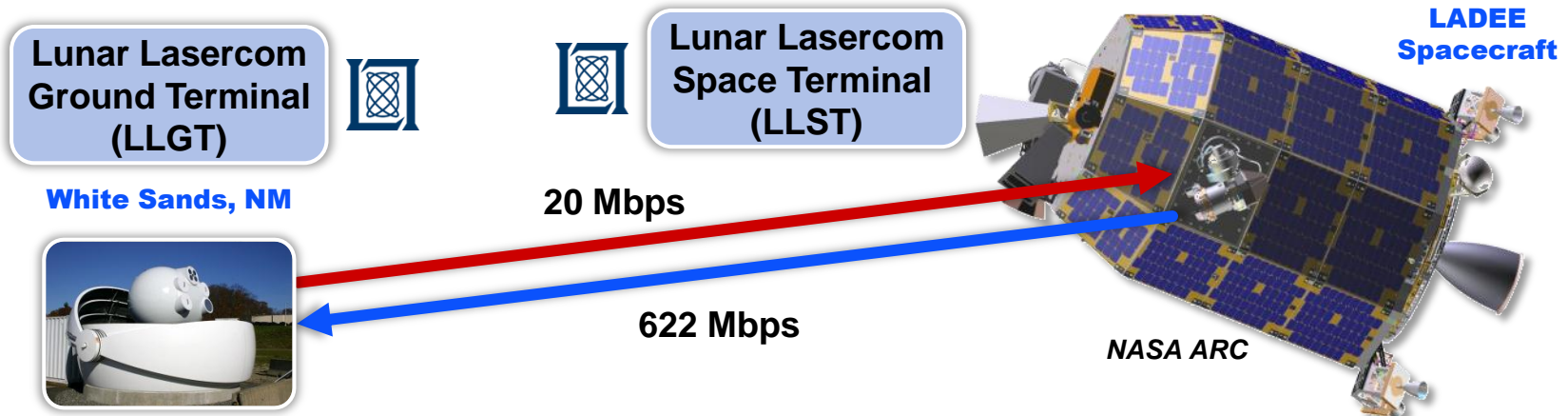
19-meter antennas in background
LLGT gimbal on pedestal is ~4-meters tall



Major Accomplishments



- Longest laser communication link ~400,000 km
- Highest data rates ever demonstrated to/from moon
 - 20 Mbps up, 622 Mbps down
- Operation through the atmosphere under a wide range of conditions
 - Including thin clouds
- Real-time reliable command and data delivery via Lasercom
 - Demonstrated RF-free operation
 - Entire spacecraft buffer downlinked in minutes
 - Loopback of multiple high-rate video streams and other file transfers

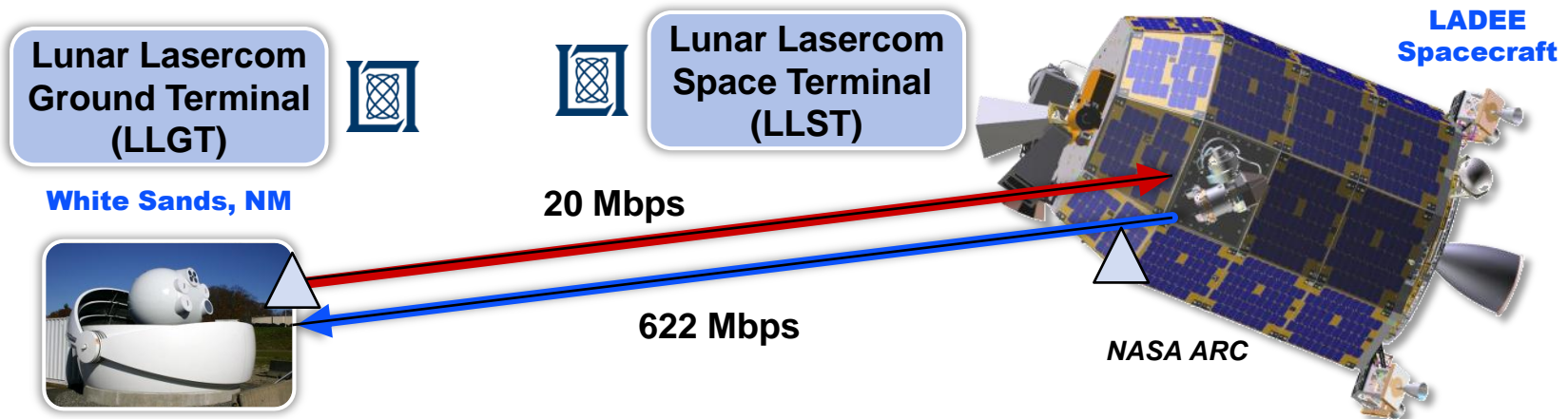




... and Time-of-Flight



- Time-of-Flight (TOF) of signals using high-rate uplink and downlink communication system clocks
- In addition to duplex communication, 2-way TOF requires:
 - Common time reference on forward and return links
 - Downlink phase-locked to received uplink in space terminal
 - High-stability time reference for measuring two-way time-of-flight

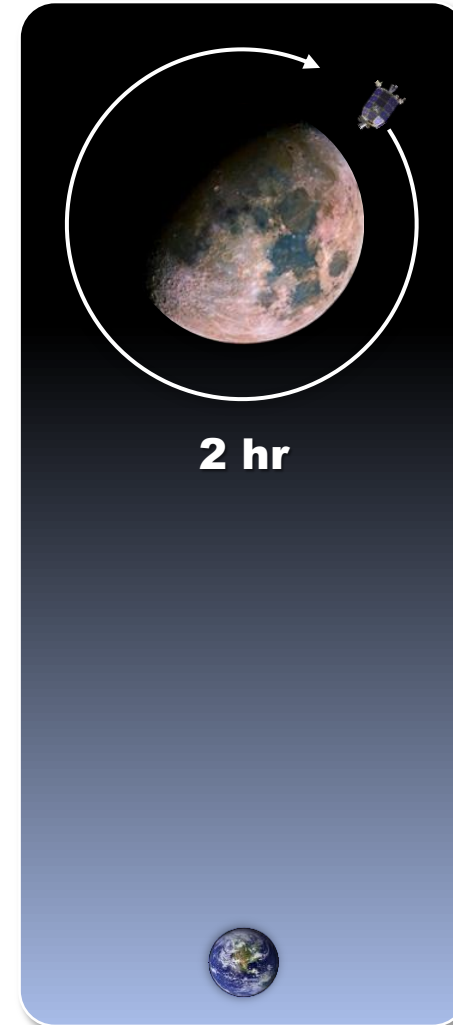




LADEE / LLCD Mission Parameters



- **LADEE orbital period ~ 2 hrs**
 - Visible from earth for about half of orbit
- **Communication links available when LADEE is visible**
 - Duplex phase-locked communications required for LLCD TOF
- **Lasercom intervals limited to ~20 minutes by power and temperature**
 - 100 passes, 135 intervals of duplex comm (14.2 hours)
- **LADEE ephemeris (orbit parameters) measured using NASA's Satellite Tracking Network in dedicated ranging sessions**

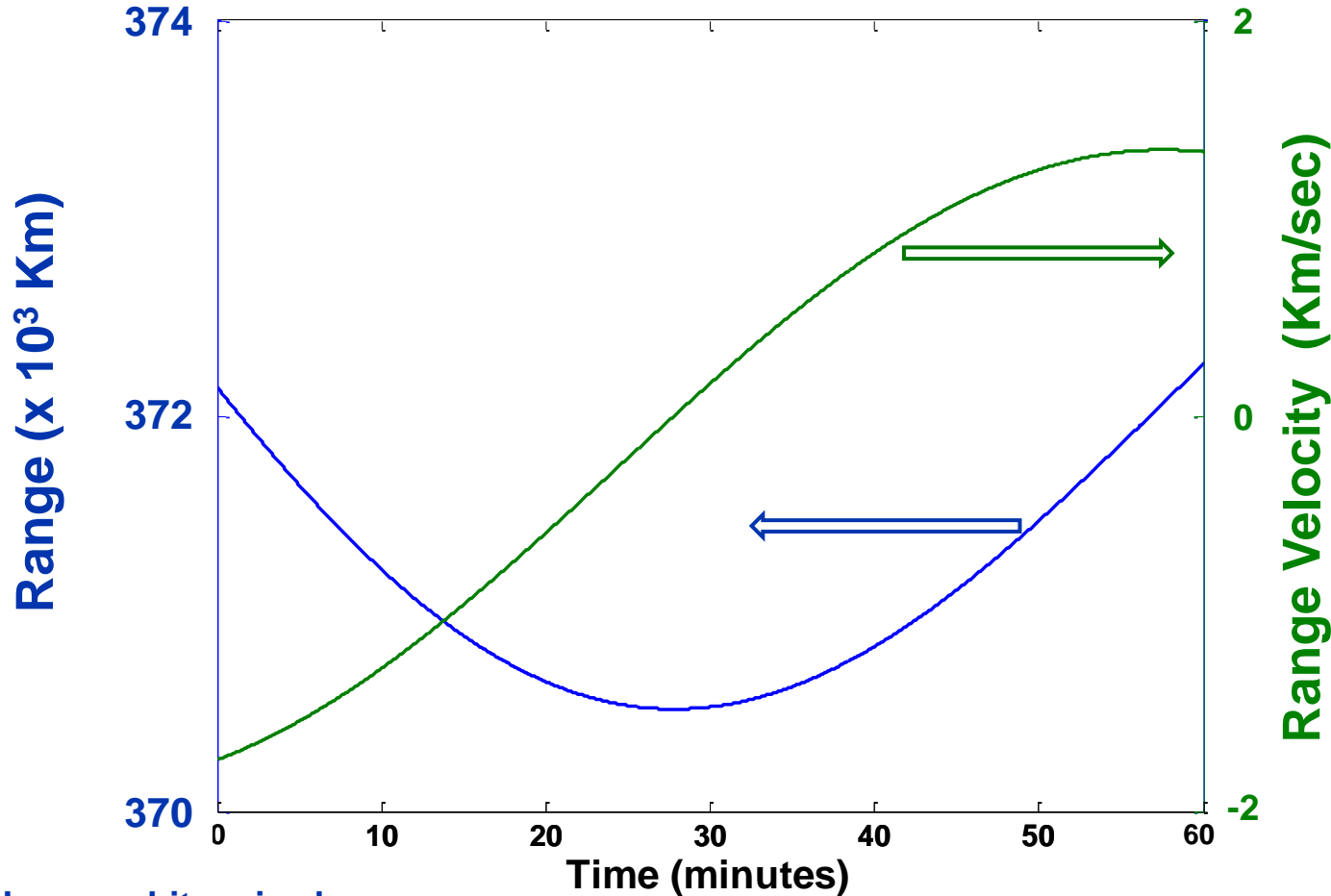




LLGT-LADEE Range and Doppler in Lunar Orbit



Example Pass



Doppler (one-way)

relative	± 6.7 ppm
carrier	± 1.3 GHz
DL slot clock	± 33 kHz
UL slot clock	± 2.1 kHz

Lunar orbit varies by 40,000 km over month



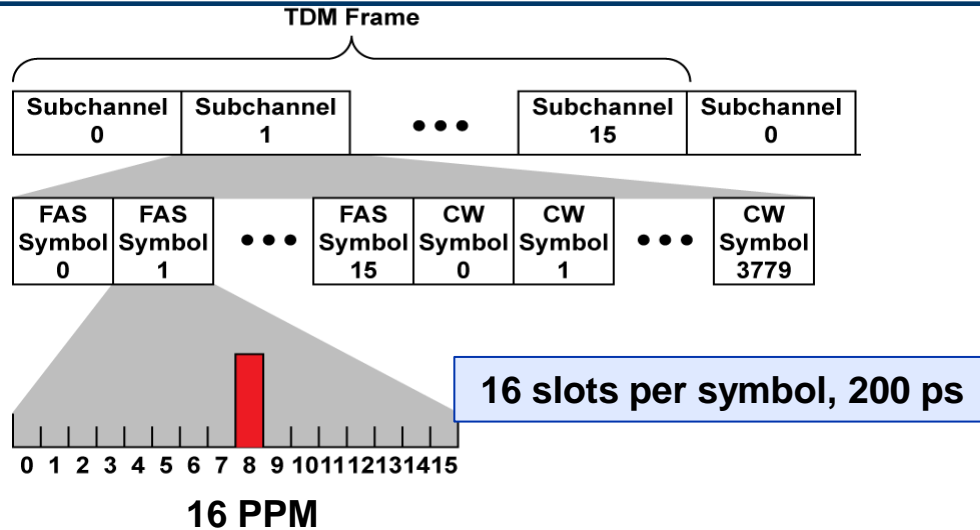
Outline



- **LLCD Mission**
- • **TOF System Architecture**
- **TOF Data**



Ranging Based on Communication Synchronization

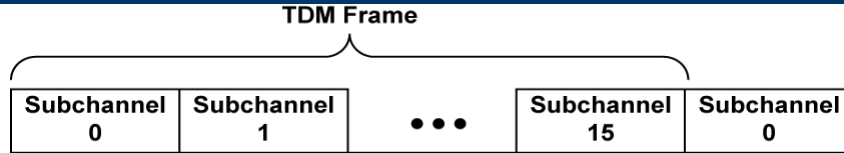


FAS Frame Alignment Sequence
CW Codeword

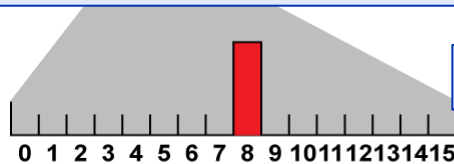
- Need perfect bit-alignment of symbols, codewords, frames, to have any communication
- Slot timing errors typically reduced to where communication loss is < 0.1 dB
 - Usually only a few % of a slot time
- Phase- and frequency-locking loops are designed as part of communication receivers
 - Designed to track through Doppler, fades, clock imperfections, delay variations, etc
- Symbol, codeword, and frame synchronization often accomplished using embedded symbols as part of communication signaling



Ranging Based on Communication Synchronization



Everything we need for TOF is already built into the communication hardware



16 PPM

16 slots per symbol, 200 ps

FAS Frame Alignment Sequence
CW Codeword

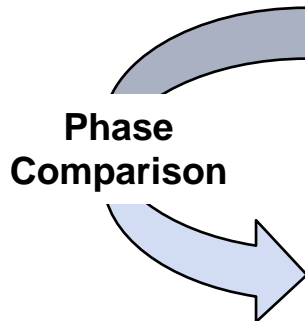
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Communication System Time Scales



- Uplink and Downlink clocks are phase locked and fractionally related
 - 1 uplink slot (3.2 ns) = 16 downlink slots (200 ps) = 1 downlink symbol
 - Phase difference measured, integrated phase yields change in distance
- Synchronous UL / DL frame clocks compared at ground terminal
 - Time delay measurement yields absolute distance offset



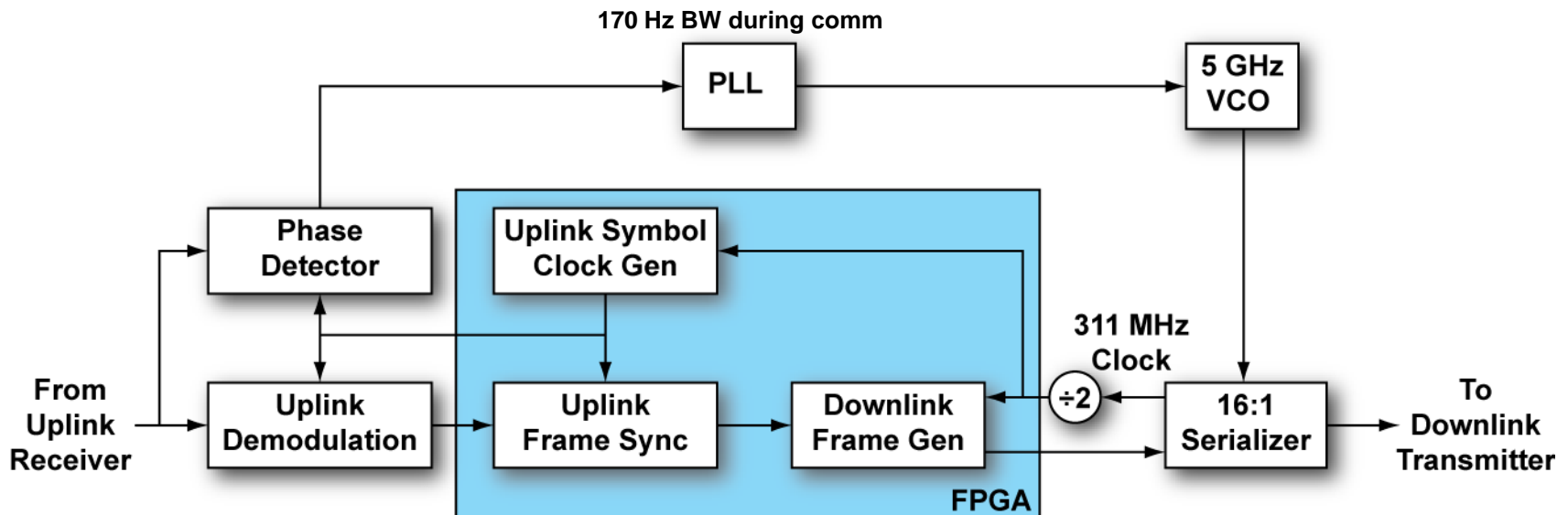
LLCD Designs	Frequency	Duration	Distance
Downlink			
Slot	4.977 GHz	200 ps	6 cm
Symbol	311 MHz	3.2 ns	96 cm
Codeword	81.9 kHz	12.2 us	3.7 km
TDM Frame	5.1 kHz	195.27 us	58.5 km
Uplink			
Slot	311 MHz	3.2 ns	96 cm
Symbol	19.4 MHz	51.4 ns	15.4 m
Codeword	2.5 kHz	390 us	117 km
TDM Frame	160 Hz	6.25 ms	1873 km

Comm requires accuracy to << 200 ps

Coarse Range ambiguity



Space Terminal Clock Architecture

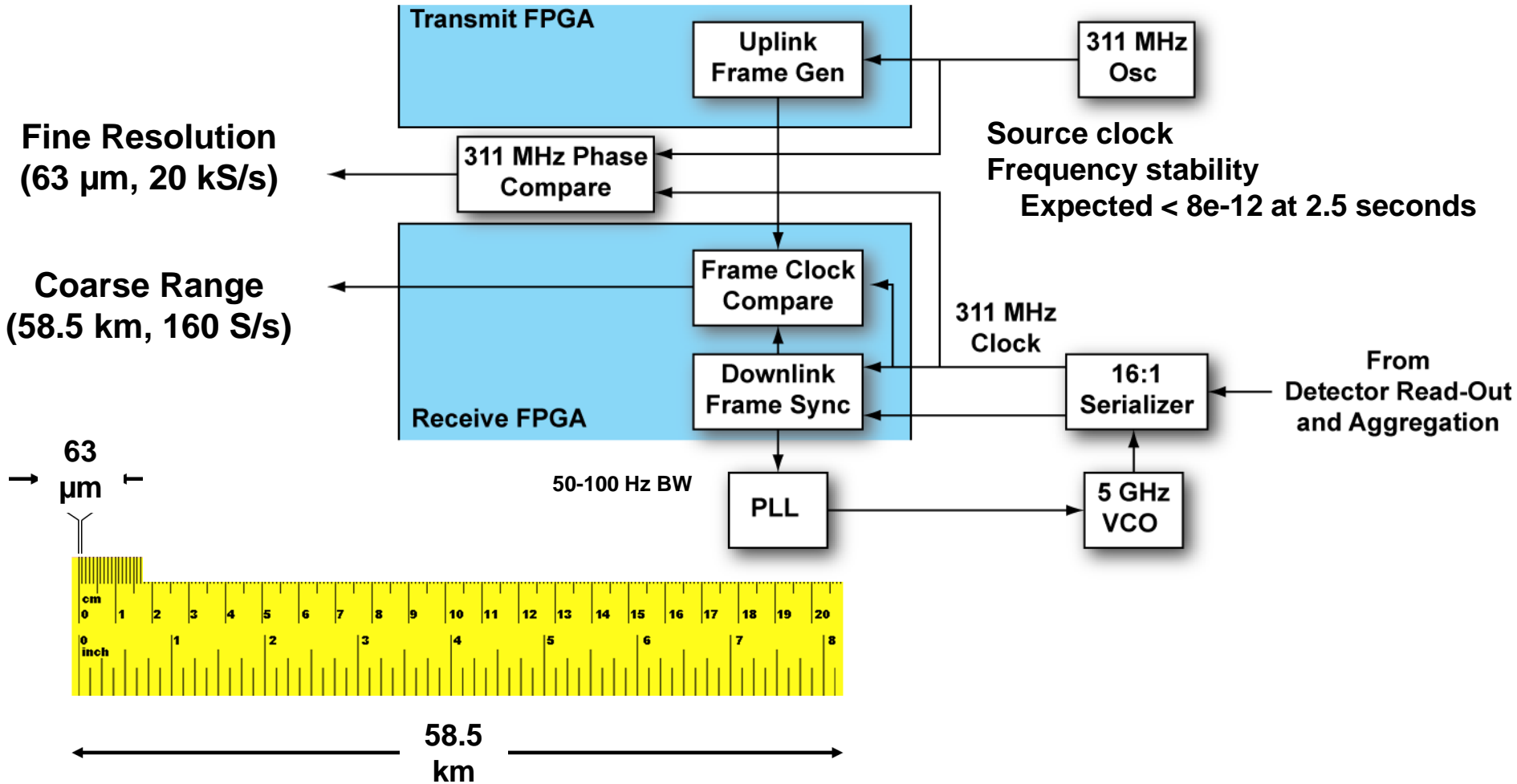


- Downlink clock is phase locked to received uplink clock
- Downlink frame is synchronized to uplink frame by command for absolute distance measurements
 - 39 measurement intervals synchronized by command
 - Automated synchronization possible in future missions

Single master clock locks downlink to uplink



Ground Terminal Time-of-Flight Systems



- Measured and archived all system performance metrics – 12.6 GB of fine and coarse resolution TOF data



Outline



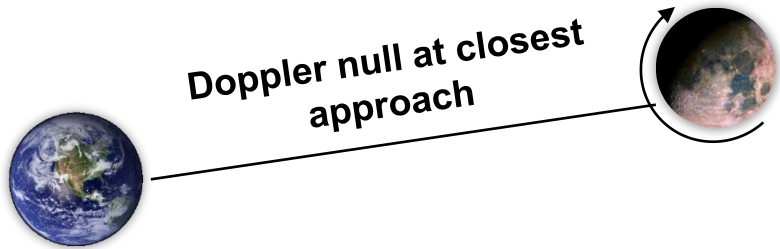
- **LLCD Mission**
- **TOF System Architecture**
- • **TOF Data**



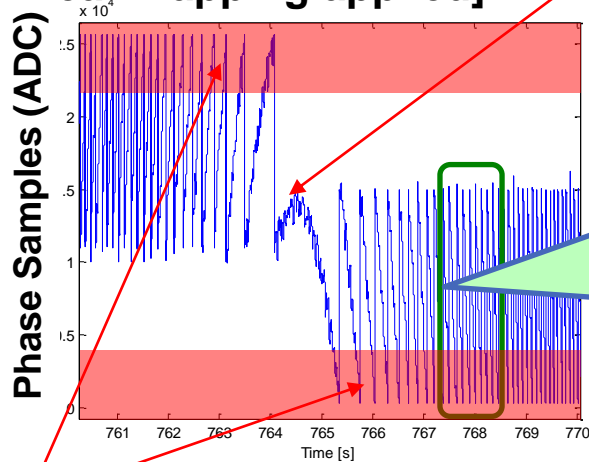
Processing Issues of TOF Phase Data



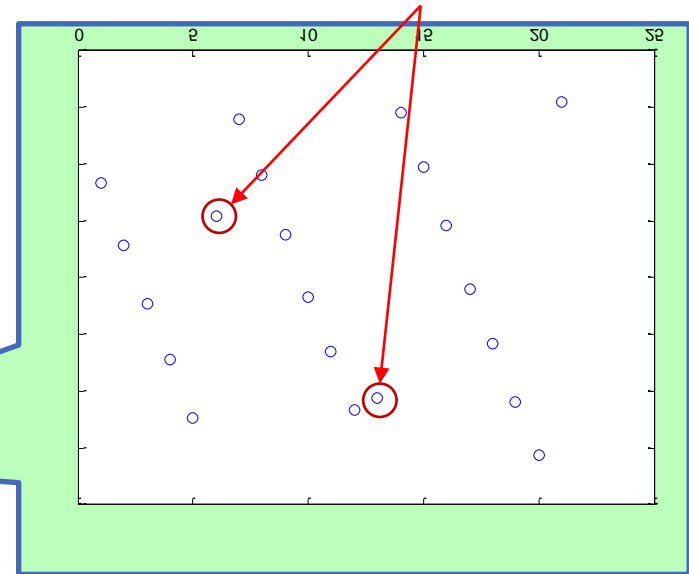
- Each sawtooth is one cycle (360°) of 311.04 MHz



1. Phase shift reversal at Doppler null [simple linear mapping applied]



2. Samples in rollover regions result in phase errors [straight-line fit correction applied]



3. Slight non-linearity of detector results in residual beat-frequency noise in data [removed with filter]

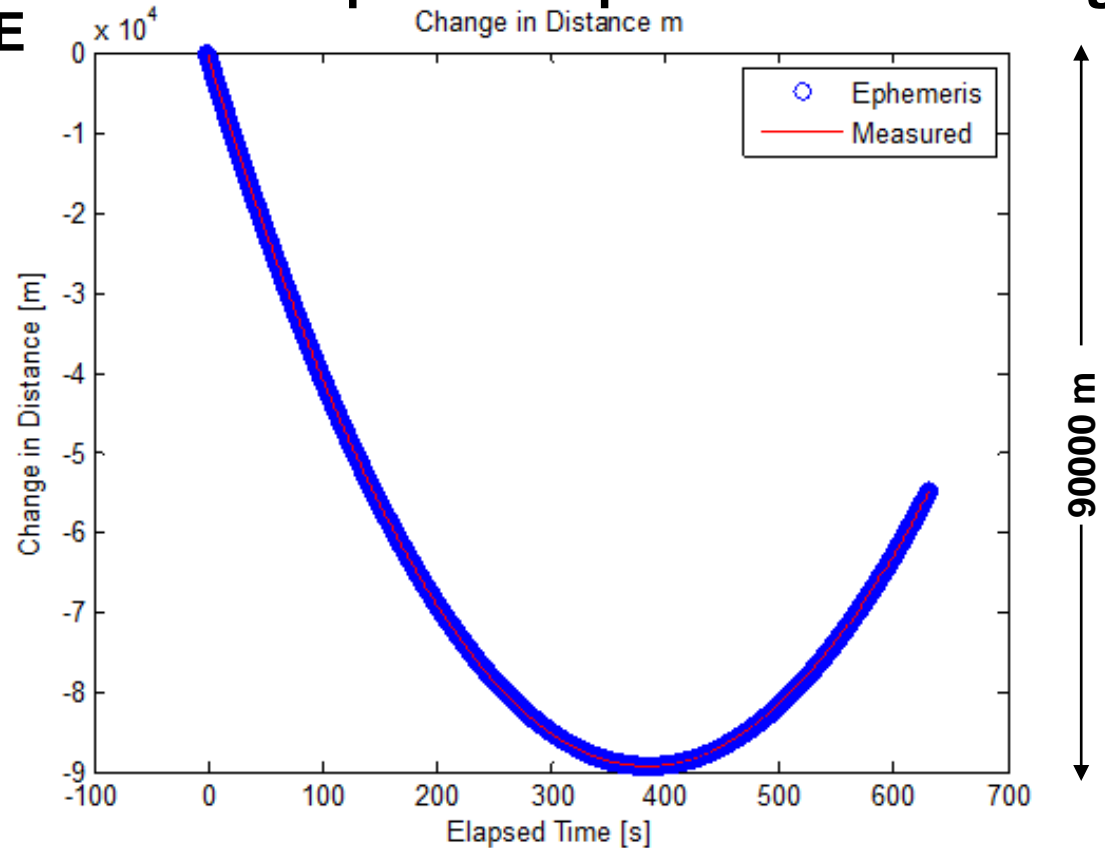
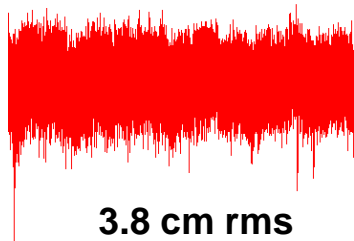


Relative Change in Distance



- Using only fine data
- Measured and ephemeris set to zero at start
- Comparison of measured to ephemeris prediction at time light arrives at LADEE

Residual Noise After
Removing
Polynomial Fit

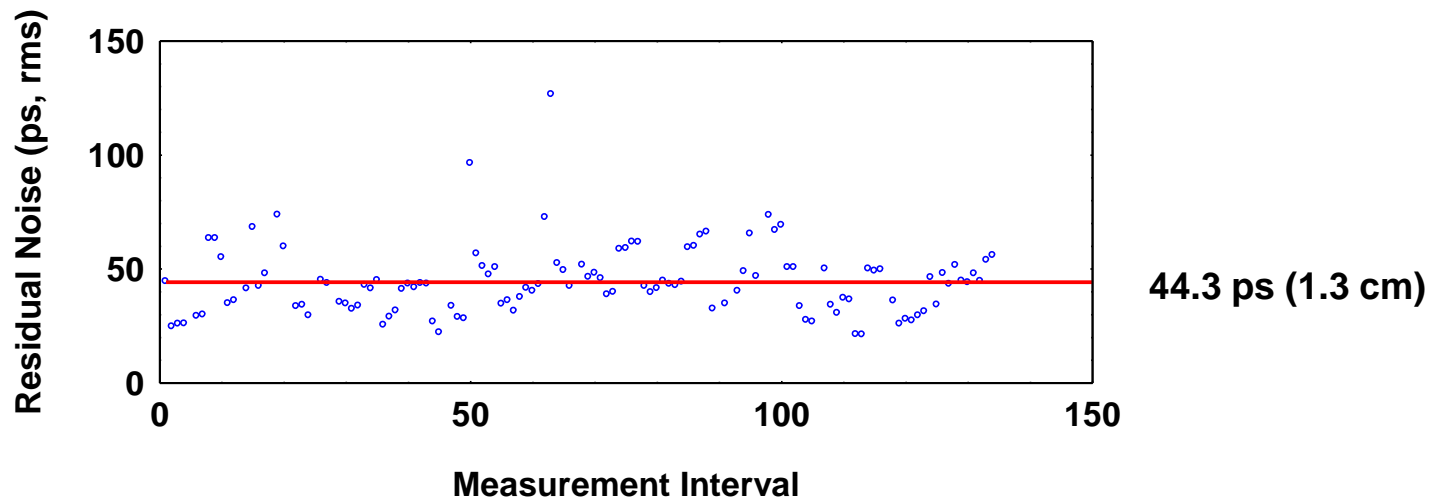




Mission TOF Engineering Data



- Two-way time-of-flight residual noise measured
 - Standard deviation in 1 s blocks calculated
 - Averaged over all data
 - $\sigma = 44.3$ ps (1.3 cm)
 - Very close to expected
 - Much better than 200ps promised
- Data archives, extraction and processing software sent to NASA science and navigation teams



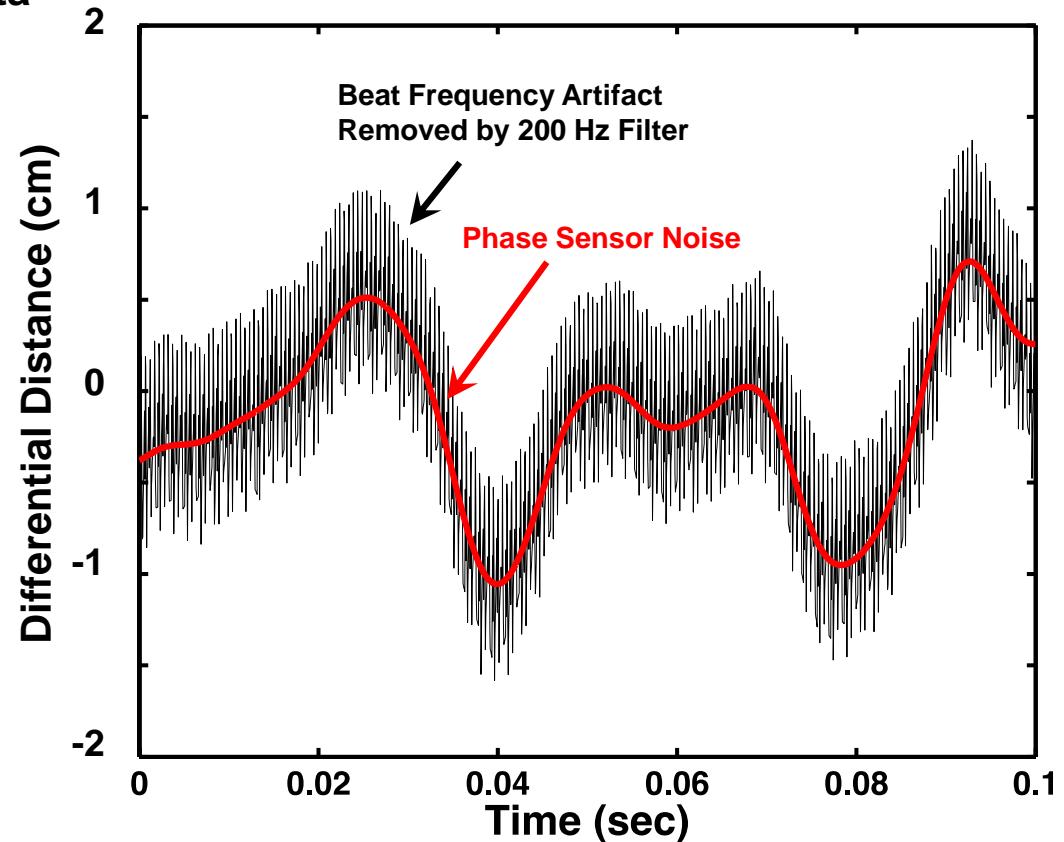
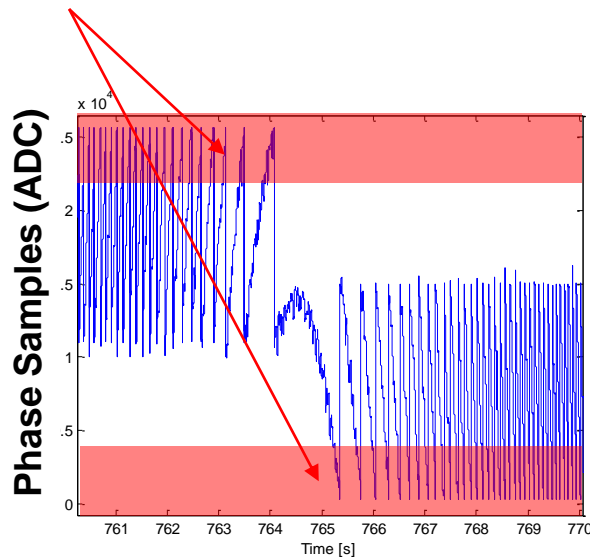


Detector Non-Linearity



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Slight non-linearity of detector results in residual beat-frequency noise in data



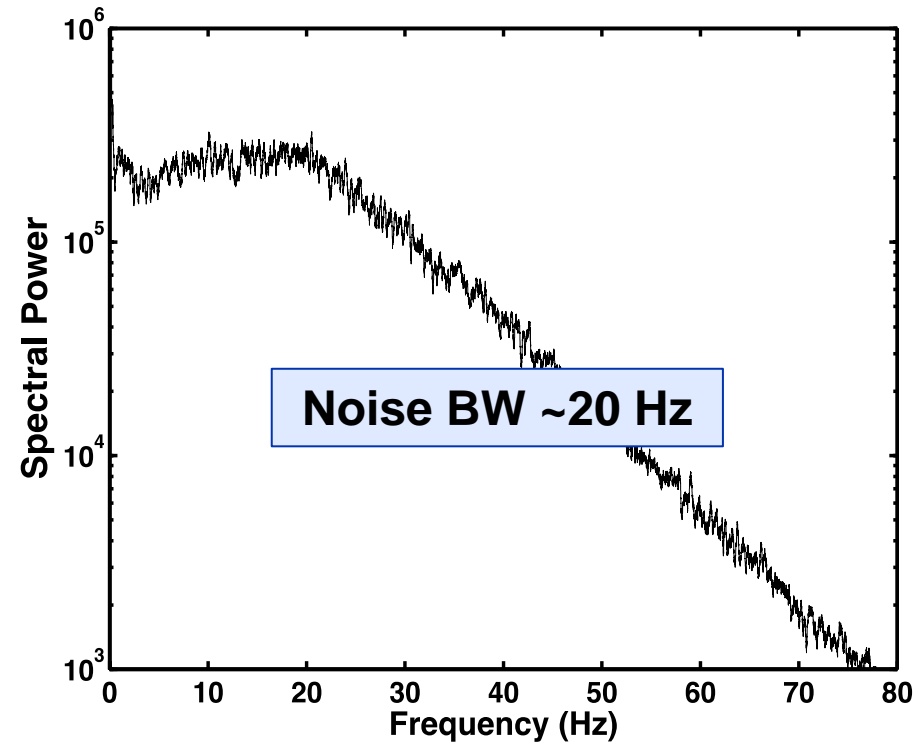
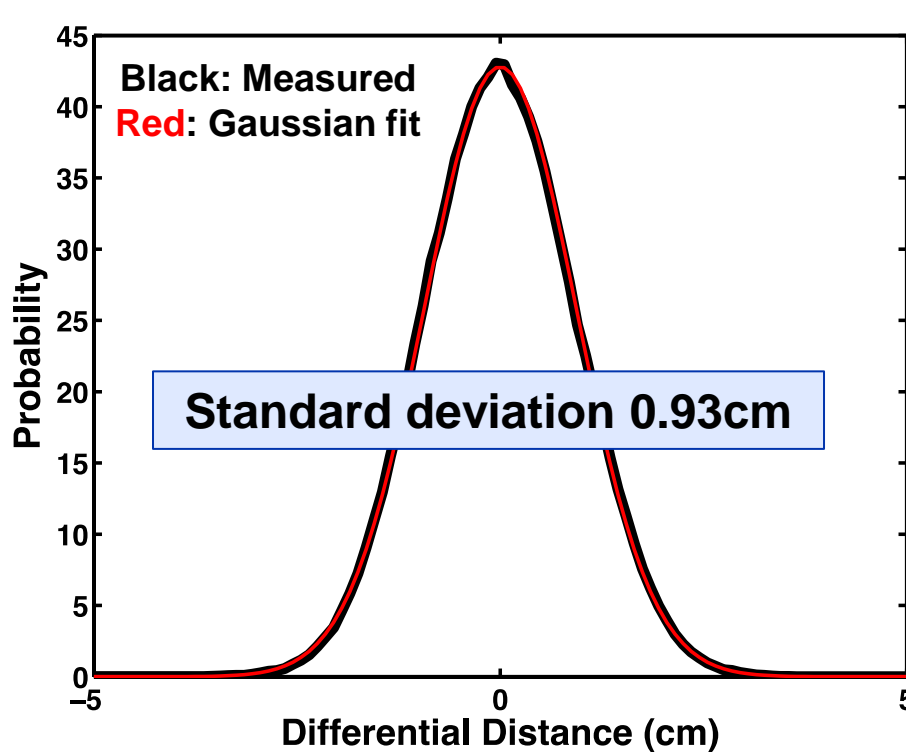
Residual beat-frequency noise removed
with post-processing filtering



One-way Residual Gaussian Noise



Gaussian fit to filtered noise



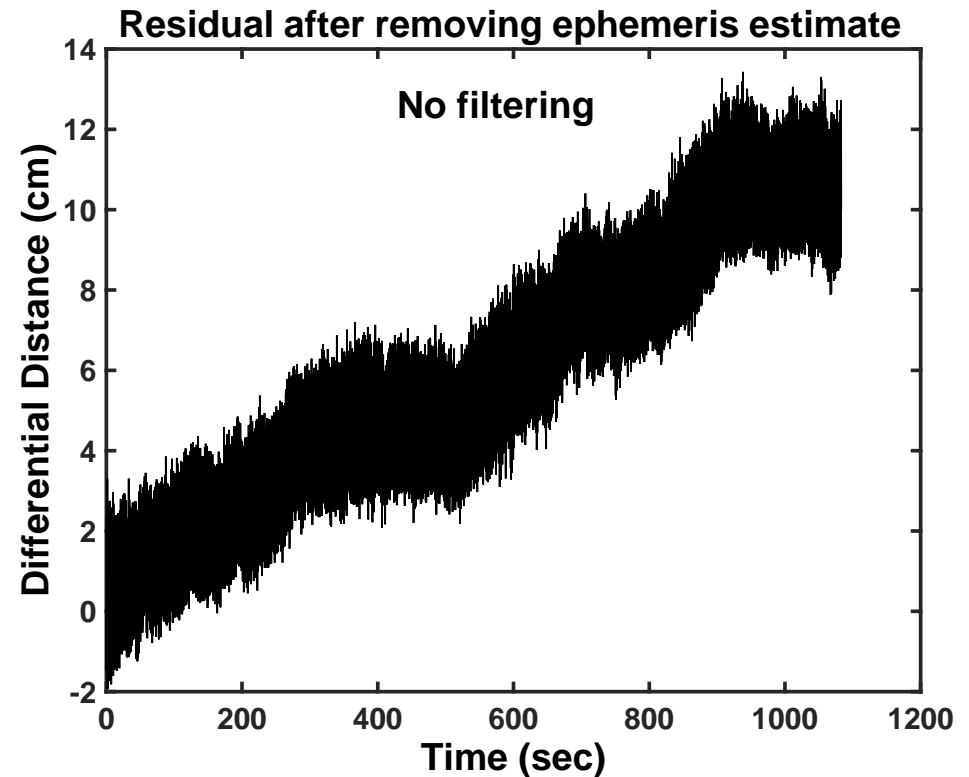
LLCD TOF precision is 2 orders of magnitude finer than RF ranging systems currently in use



Low-Frequency Variations



- Some measurements show **low-frequency variations**
- **Possible causes**
 - Measurement noise
 - Platform movement
 - Roll, pitch, yaw
 - Temperature or signal power
 - Real orbital disturbance
- Resolution pending further analysis



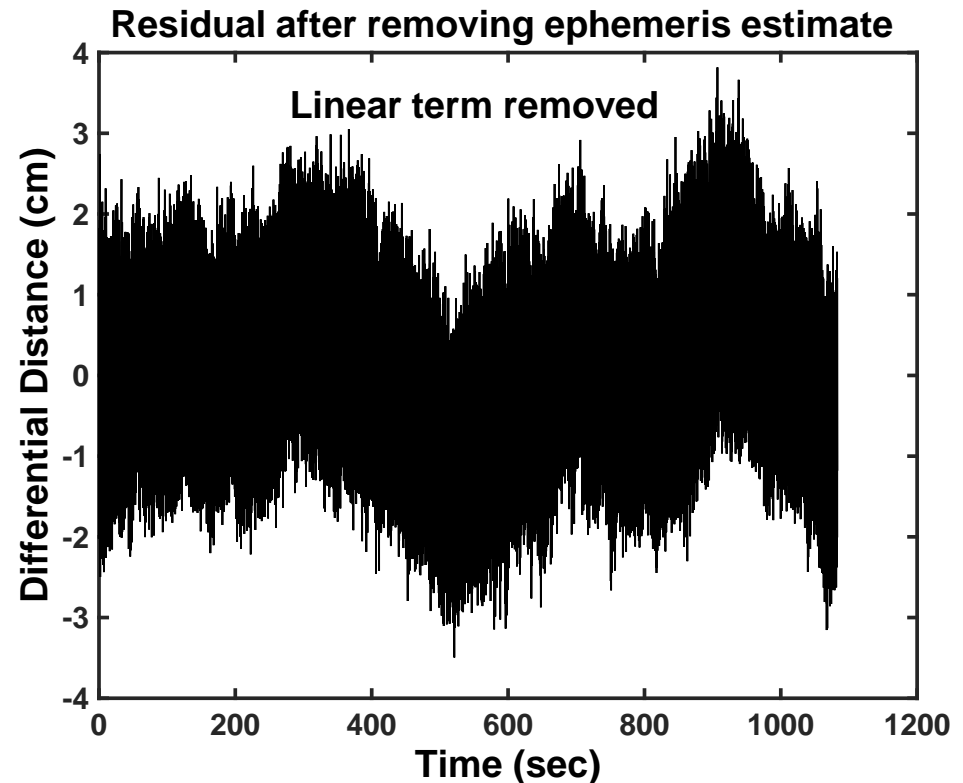
Is this noise or real orbital disturbance?



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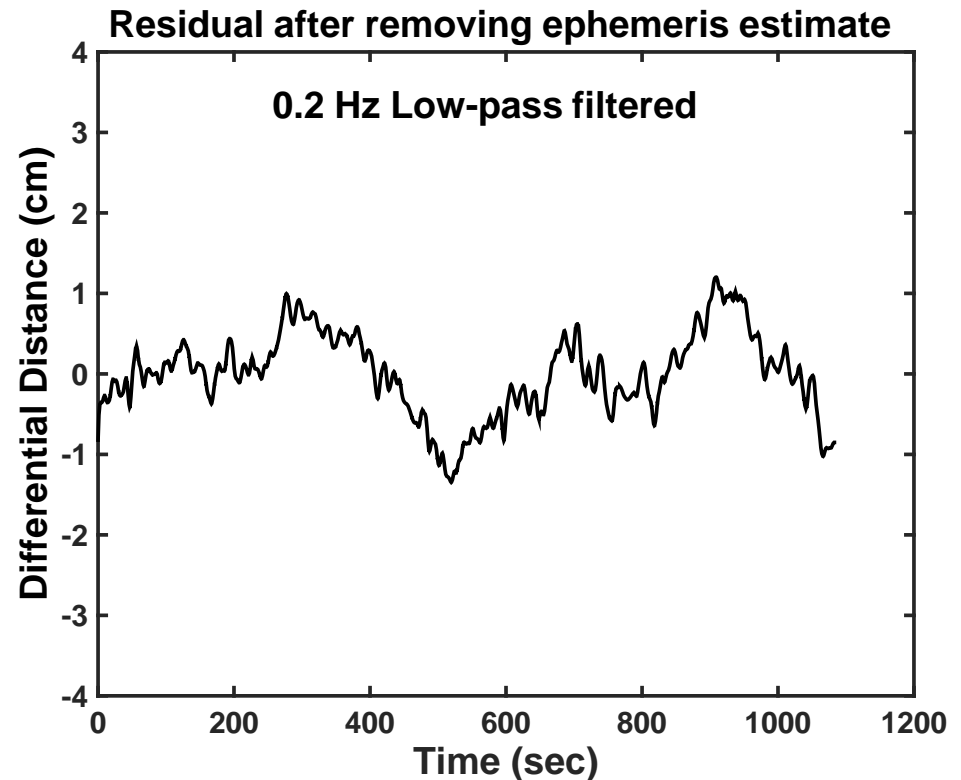
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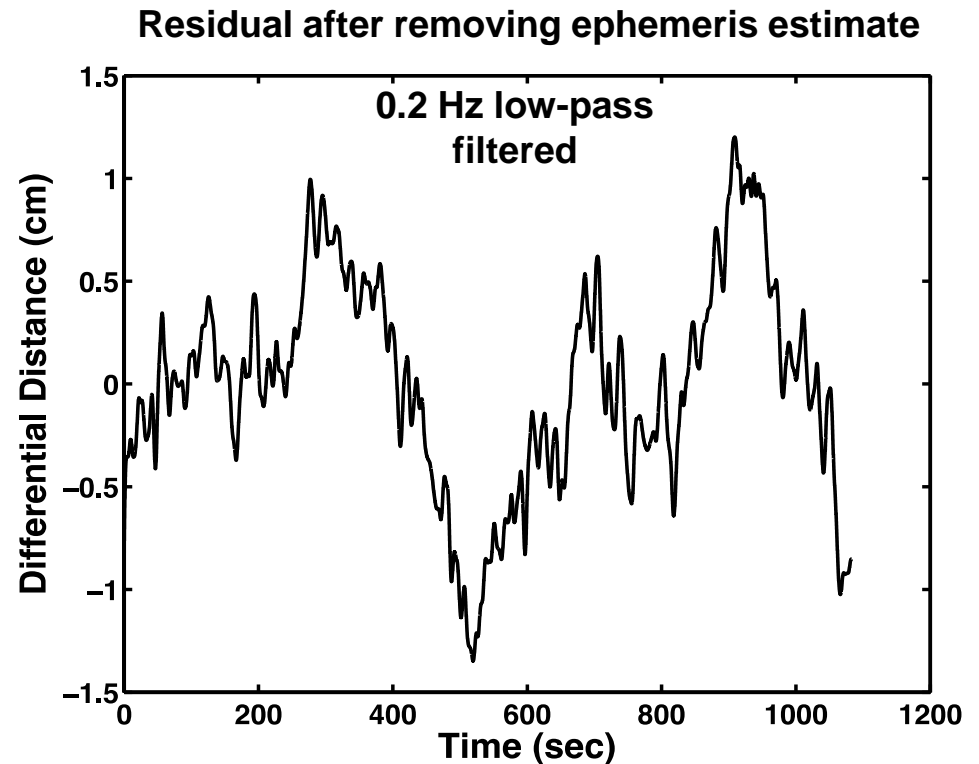
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Is this noise or real orbital disturbance?



Summary



- **LLCD included a measurement of time-of-flight using the high-speed clocks in the communication system**
- **Mission completed 100 passes**
 - 14.2 hours of duplex comm
 - 12.6 GB of TOF data
 - Standard deviation of residual noise in 2-way TOF = 44.3 ps (1.3 cm)
- **Preliminary ranging estimates show:**
 - Centimeter precision of one-way relative distance
 - Gaussian residual noise with typical standard deviation of 0.93cm
 - Two orders of magnitude better than RF ranging systems in use
- **NASA science and navigation teams are performing fine analysis of ranging**



We believe that high-rate communication-signal-based time-of-flight systems could be highly useful in future navigation and science missions



References



We believe that high-rate communication-signal-based time-of-flight systems could be highly useful in future navigation and science missions

- D.M. Boroson, B.S. Robinson, D.A. Burianek, D.V. Murphy, F.I. Khatri, J.M. Kovalik, Z. Sodnik, Overview and results of the Lunar laser communication demonstration. Proc. SPIE 8971 (2014)
- B.S. Robinson, D.M. Boroson, D. Burianek, D. Murphy, F. Khatri, A. Biswas, Z. Sodnik, J. Burnside, J. Kinsky, D. Cornwell, *“The NASA Lunar Laser Communication Demonstration—Successful High-Rate Laser Communications to and from the Moon”*; *Space Ops* (2014)
- Willis, M.M.; Robinson, B.S.; Stevens, M.L.; Romkey, B.R.; Matthews, J.A.; Greco, J.A.; Grein, M.E.; Dauler, E.A.; Kerman, A.J.; Rosenberg, D.; Murphy, D.V.; Boroson, D.M., "Downlink synchronization for the lunar laser communications demonstration," in *Space Optical Systems and Applications (ICSOS), 2011 International Conference on* , vol., no., pp.83-87, 11-13 May 2011