



42C08SE0004 0026 STOVER

010

Mining Lands Section

File No 2.6953

Control Sheet

TYPE OF SURVEY

- GEOPHYSICAL
- GEOLOGICAL
- GEOCHEMICAL
- EXPENDITURE

MINING LANDS COMMENTS:

200 meter  $\frac{1}{8}$  mi line spacing  
 206 km flown  $\rightarrow$  128 miles, 203 claims  $\approx$  26 days per survey  
 assessed as total geophysical 26 days  $\times$  3 surveys = 78 days  
 approved as 80 days to account for approximations

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Signature of Assessor

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Date

DIGHEM<sup>III</sup> SURVEY

OF THE

RENNIE LAKE AREA, ONTARIO

FOR

ROBERT J, MCGOWAN

BY

DIGHEM LIMITED

RECEIVED

JUL 17 1984

MINING LANDS SECTION

TORONTO, ONTARIO  
MAY 31, 1984

63.2278 v1.  
2.6953  
D.C. Fraser

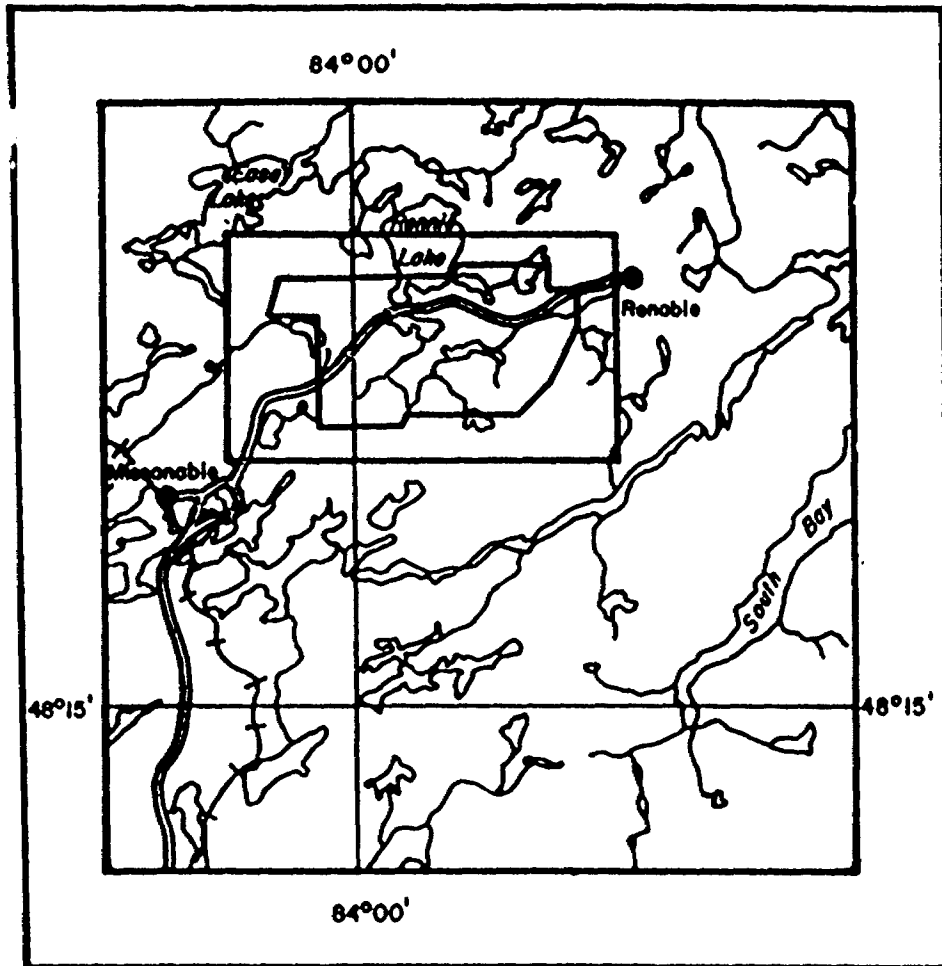
D.C. FRASER  
PRESIDENT

## SUMMARY AND RECOMMENDATIONS

A total of 206 km of survey was flown with the DIGHEM<sup>III</sup> system in April 1984, over a property held by Robert J. McGowan near Rennie Lake, Ontario.

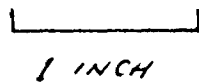
The survey outlined a number of discrete bedrock conductors associated with areas of low resistivity. Most of these anomalies appear to warrant further investigation using appropriate surface exploration techniques. Areas of interest may be assigned priorities for follow-up work on the basis of supporting geological and other information. The survey area has been explored a number of times by others. It had been surveyed earlier with the now obsolete DIGHEM<sup>II</sup> system. A review of assessment files will undoubtedly eliminate many conductors.

LOCATION MAP



SCALE 1:250,000

FIGURE 1  
THE SURVEY AREA





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## INTRODUCTION

A DIGHEM<sup>III</sup> survey totalling 206 line-km was flown with a 200 m line-spacing for Robert J. McGowan, on April 13 and 14, 1984 in the Rennie Lake area of Ontario (Figure 1).

The NSM Astar turbine helicopter flew at an average airspeed of 100 km/h with an EM bird height of approximately 32 m. Ancillary equipment consisted of a Sonotek PMH 5010 magnetometer with its bird at an average height of 47 m, a Sperry radio altimeter, a Geocam sequence camera, an RMS GR33-1 analog recorder, a Sonotek SDS 1200 digital data acquisition system and a DigiData 9-track 800-bpi magnetic tape recorder. The analog equipment recorded four channels of EM data at approximately 900 Hz, two channels of EM data at approximately 7200 Hz, an ambient EM noise channel (for the coaxial receiver), two channels of magnetics (coarse and fine count), two VLF-EM channels and a channel of radio altitude. The digital equipment recorded the EM data with a sensitivity of 0.2 ppm and the magnetic field to one nT (i.e., one gamma).

Appendix A provides details on the data channels, their respective sensitivities, and the flight path recovery

procedure. Noise levels of less than 2 ppm are generally maintained for wind speeds up to 35 km/h. Higher winds may cause the system to be grounded because excessive bird swinging produces difficulties in flying the helicopter. The swinging results from the 5 m<sup>2</sup> of area which is presented by the bird to broadside gusts. The DIGHEM system nevertheless can be flown under wind conditions that seriously degrade other AEM systems.

It should be noted that the anomalies shown on the electromagnetic anomaly map are based on a near-vertical, half plane model. This model best reflects "discrete" bedrock conductors. Wide bedrock conductors or flat-lying conductive units, whether from surficial or bedrock sources, may give rise to very broad anomalous responses on the EM profiles. These may not appear on the electromagnetic anomaly map if they have a regional character rather than a locally anomalous character. These broad conductors, which more closely approximate a half space model, will be maximum coupled to the horizontal (coplanar) coil-pair and are clearly evident on the resistivity map. The resistivity map, therefore, may be more valuable than the electromagnetic anomaly map, in areas where broad or flat-lying conductors are considered to be of importance.

In areas where magnetite causes the inphase components to become negative, the apparent conductance and depth of EM anomalies may be unreliable.

There are several areas where EM responses are evident only on the quadrature components, indicating zones of poor conductivity. Where these responses are coincident with strong magnetic anomalies, it is possible that the inphase component amplitudes have been suppressed by the effects of magnetite. Most of these poorly-conductive magnetic features give rise to resistivity anomalies which are only slightly below background. These weak features are evident on the resistivity map but may not be shown on the electromagnetic anomaly map. If it is expected that poorly-conductive sulphides may be associated with magnetite-rich units, some of these weakly anomalous features may be of interest.



SECTION I: SURVEY RESULTS

CONDUCTORS IN THE SURVEY AREA

The survey covered a block of claims with 206 km of flying, the results of which are shown on one map sheet for each parameter. Table I-1 summarizes the EM responses with respect to conductance grade and interpretation.

The electromagnetic anomaly map shows the anomaly locations with the interpreted conductor shape, dip, conductance and depth being indicated by symbols. Direct magnetic correlation is also shown if it exists. The strike direction and length of the conductors are indicated when anomalies can be correlated from line to line. When studying the map sheets for follow-up planning, consult the anomaly listings appended to this report to ensure that none of the conductors are overlooked.

The resistivity map shows the conductive properties of the survey area. Some of the resistivity lows (i.e., conductive areas) coincide with bedrock conductors and others indicate lakes. The resistivity is generally greater than 300 ohm-m over the lakes, but can be below 10 ohm-m over bedrock conductors. The resistivity patterns may aid geologic mapping and in extending the length of known zones.

TABLE I-1

EM ANOMALY STATISTICS OF THE RENNIE LAKE AREA

CONDUCTOR GRADE	CONDUCTANCE RANGE	NUMBER OF RESPONSES
6	> 99 MHOS	2
5	50-99 MHOS	3
4	20-49 MHOS	14
3	10-19 MHOS	22
2	5- 9 MHOS	29
1	< 5 MHOS	132
X	INDETERMINATE	27
TOTAL		229

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
B	DISCRETE BEDROCK CONDUCTOR	112
S	CONDUCTIVE COVER	113
(BLANK)		4
TOTAL		229

(SEE EM MAP LEGEND FOR EXPLANATIONS)

The magnetic map is extremely active, probably reflecting iron formation in places. The primary geologic trend is northwest-southeast. Magnetic dikes intersect this trend, and commonly strike N30°W.

The enhanced magnetic map shows the individual magnetic zones more distinctly than the total field magnetic map. For example, there is a magnetic correlation with 23I\* which shows clearly on the enhanced map but which does not appear on the total field map.

The VLF-EM map contains a large number of northwest-southeast striking features. These reflect the geology to a large extent. Some distortion occurs due to lakes and, perhaps, due to cross-cutting faults. The VLF-EM map is unusually definitive, and may help in the exploration program.

The following description of EM anomalies focusses primarily on the probably bedrock conductors (interpretive symbol "B" or "B?"). Anomalies which have been interpreted as due to conductive overburden (interpretive symbol "S" or "S?") are generally ignored in this discussion.

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\* EM anomaly I on line 23.

<u>Anomaly</u>	<u>Length</u>	<u>Conductance Grade</u>	<u>Features</u>
2xA-8I	4,600 ft.	1-4	The conductor occurs within a resistivity low, and this map suggests the conductor extends to 15M. The total field and enhanced magnetic maps, however, do not support this extension.
3D, 5B-9C 8G-9B	200 to 3,300 ft.	1-3, 6	The conductor occurs on the northeast flank of a very strong magnetic high having iron formation characteristics. The EM anomalies generally occur within a resistivity low apart from the grade 6 EM anomaly 3D. This highly conductive EM anomaly is suspicious because of the lack of an associated resistivity low. It probably reflects a very short, thin conductor without value economically.
8D	200 ft.	1	A small but distinct resistivity low coincides with this non-magnetic single-line EM anomaly.
10D, 11G-12H, 13E-15M, 10B-12F	200 to 1,700 ft.	1-3	The EM and resistivity maps suggest that the multi-line conductors of this grouping form the southeast extension of the two conductive groups described first above. The magnetic maps, however, do not support this association. Anomaly 10D is not particularly attractive although it is believed to reflect poorly conductive bedrock material. Anomalies 10D, 11G-12H and 13E-15M occur on the southwest flank on an enhanced magnetic high. Anomaly 10B-12F has a slight magnetic correlation which can only be seen on the enhanced map.

Anomaly	Length	Conductance Grade	Features
18D-20L, 22N, 23K	200, 2,000 ft.	1-4	A number of essentially single-line anomalies occur which probably reflect bedrock conductors. A questionable line-to-line correlation is shown. The correlation is supported by resistivity and VLF-EM, but poorly so by magnetics.
13D, 15L-18C, 21H-24J, 26I-27G, 31B-45A	200 - 10,000 ft.	1-4	A series of EM anomalies appears to occur along a single conductive horizon, as is also supported by the VLF-EM map. The conductors occasionally have a magnetic correlation; in particular note 22J-23I. Thick conductive sections may occur at 24J and 34C, the latter having a magnetic correlation. The resistivity map indicates that the conductor is part of a wide conductive zone which encompasses the EM grouping described immediately below.
22L-35C, 22M, 24L-26K, 32G, 33C, 37C-39D, 45B	200 - 10,000 ft.	1-6	The EM anomalies of this grouping occur within the large conductive zone described immediately above. A sporadic magnetic correlation exists; in particular note 24K-28G and 33E-35C on the enhanced magnetic map. The correlation is not evident on the total field map for 24K-28G. This illustrates the superior resolving power of the enhanced map.
16H, 20G, 22I-23H, 24I	200 - 1,300 ft.	1-3	Discontinuous bedrock conductors occur along the southwest flank of the above described large conductive zone. They may, in part, reflect conductive sections within iron

Anomaly	Length	Conductance Grade	Features
11A-16D, 19E, 22F, 25H-28D	200 - 4,400 ft.	1-4	formation, particularly 20G and 22I-23H. All the EM anomalies of this grouping, except 24I, lie within a VLF-EM high. This high also encompasses 19F, 21G, 24H and 25I which may reflect conductive overburden.  A single magnetic horizon encompasses these bedrock conductors, and also 21E, 24E, 29A and 30A which probably reflect conductive cover. The VLF-EM map contains all these anomalies within a single high. The resistivity map contains some distortions due to conductive cover, but resistivity lows generally coincide with the bedrock anomalies.
11B	200 ft.	1	The EM anomaly occurs on a single line and has an interpretive symbol "S?", indicating conductive overburden. The resistivity map shows the anomaly extends to line 12. The VLF-EM map indicates the EM anomaly forms part of a trend that extends from line 7 to 16, and possibly longer in both directions. It encompasses EM anomaly 8C, which has an interpretive symbol "S". The zone is non-magnetic and could reflect a structural weakness rather than conductive cover.
13A, 15E, 15D-17C, 16B, 17D 19D	200 - 2,000 ft.	1-2	The anomalies of this grouping occur on the north flank of an enhanced magnetic high, apart from 16B which occurs close to the magnetic peak. The resistivity and VLF-EM maps suggest that 13A, 15D-17C and

<u>Anomaly</u>	<u>Length</u>	<u>Conductance Grade</u>	<u>Features</u>
			19D may occur along a single conductive horizon.
17A, 20D, 24A, 24B	200 ft.	1	These four single-line anomalies probably reflect short bedrock conductors. All are non-magnetic except for 20D. A weak magnetic correlation occurs with 20D that can only be seen on the profiles. A magnetic high occurs close to 24B.
26N	200 ft.	1	A weak magnetic correlation occurs with this weak single-line conductor. The resistivity map suggests that the conductor may extend east-southeast to line 28.
39K-47xB	6,600+ft.	1-5	A distinctive resistivity low and VLF-EM high encompass this long conductor. It has yielded some high conductances (e.g., 42G is of grade 6), and thick conductive sections appear to exist (40I, 42G). The magnetic maps, however, do not support this line-to-line correlation, suggesting, instead, that a series of short en echelon conductors may actually occur.

SECTION II: BACKGROUND INFORMATION

ELECTROMAGNETICS

DIGHEM electromagnetic responses fall into two general classes, discrete and broad. The discrete class consists of sharp, well-defined anomalies from discrete conductors such as sulfide lenses and steeply dipping sheets of graphite and sulfides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulfide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, and geothermal zones. A vertical conductive slab with a width of 200 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the electromagnetic map are analyzed according to this model. The following section entitled Discrete conductor analysis describes this model in detail, including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

The conductive earth (half space) model is suitable for broad conductors. Resistivity contour maps result from the



use of this model. A later section entitled Resistivity mapping describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulfide bodies.

#### Geometric interpretation

The geophysical interpreter attempts to determine the geometric shape and dip of the conductor. This qualitative interpretation of anomalies is indicated on the map by means of interpretive symbols (see EM map legend). Figure II-1 shows typical DIGHEM anomaly shapes and the interpretive symbols for a variety of conductors. These classic curve shapes are used to guide the geometric interpretation.

#### Discrete conductor analysis

The EM anomalies appearing on the electromagnetic map are analyzed by computer to give the conductance (i.e., conductivity-thickness product) in mhos of a vertical sheet model. This is done regardless of the interpreted geometric shape of the conductor. This is not an unreasonable procedure, because the computed conductance increases as the electrical quality of the conductor increases, regardless of its true shape. DIGHEM anomalies are divided into six

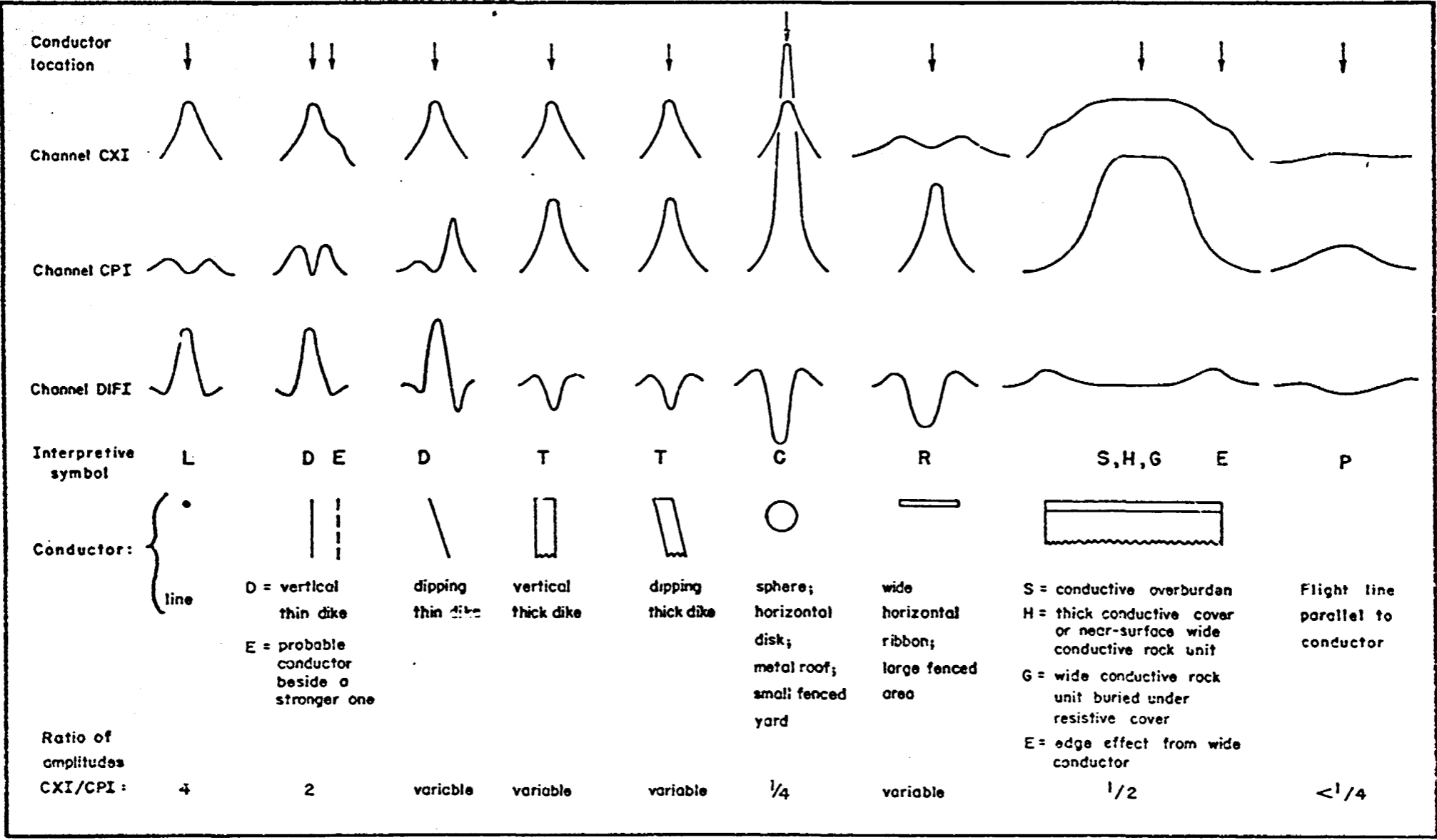


Figure II - 1

Typical DIGHEM anomaly shapes

grades of conductance, as shown in Table II-1. The conductance in mhos is the reciprocal of resistance in ohms.

Table II-1. EM Anomaly Grades

<u>Anomaly Grade</u>	<u>Mho Range</u>
6	> 99
5	50 - 99
4	20 - 49
3	10 - 19
2	5 - 9
1	< 5

The conductance value is a geological parameter because it is a characteristic of the conductor alone; it generally is independent of frequency, and of flying height or depth of burial apart from the averaging over a greater portion of the conductor as height increases.<sup>1</sup> Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger conductance values.

Conductive overburden generally produces broad EM responses which are not plotted on the EM maps. However, patchy conductive overburden in otherwise resistive areas

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<sup>1</sup> This statement is an approximation. DIGHEM, with its short coil separation, tends to yield larger and more accurate conductance values than airborne systems having a larger coil separation.

can yield discrete anomalies with a conductance grade (cf. Table II-1) of 1, or even of 2 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities can be below 10 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such conductors to be recognized, and these are indicated by the letters S, H, G and sometimes E on the map (see EM legend).

For bedrock conductors, the higher anomaly grades indicate increasingly higher conductances. Examples: DIGHEM's New Inesco copper discovery (Noranda, Canada) yielded a grade 4 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Sturgeon Lake, Canada) and Whistle (nickel, Sudbury, Canada) gave grade 5; and DIGHEM's Montcalm nickel-copper discovery (Timmins, Canada) yielded a grade 6 anomaly. Graphite and sulfides can span all grades but, in any particular survey area, field work may show that the different grades indicate different types of conductors.

Strong conductors (i.e., grades 5 and 6) are characteristic of massive sulfides or graphite. Moderate conductors (grades 3 and 4) typically reflect sulfides of a less massive character or graphite, while weak bedrock conductors

(grades 1 and 2) can signify poorly connected graphite or heavily disseminated sulfides. Grade 1 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche Mining Corporation near Bathurst, Canada, yielded a well defined grade 1 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction.

Faults, fractures and shear zones may produce anomalies which typically have low conductances (e.g., grades 1 and 2). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

On the electromagnetic map, a letter identifier and an interpretive symbol are plotted beside the EM grade symbol. The horizontal rows of dots, under the interpretive symbol, indicate the anomaly amplitude on the flight record. The

vertical column of dots, under the anomaly letter, gives the estimated depth. In areas where anomalies are crowded, the letter identifiers, interpretive symbols and dots may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the inphase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The conductance grade and depth estimate illustrates which of these possibilities fits the recorded data best.

Flight line deviations occasionally yield cases where two anomalies, having similar conductance values but dramatically different depth estimates, occur close together on the same conductor. Such examples illustrate the reliability of the conductance measurement while showing that the depth estimate can be unreliable. There are a

number of factors which can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock onto the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes which may define the geological structure over portions of the survey area. The absence of

conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

DIGHEM electromagnetic maps are designed to provide a correct impression of conductor quality by means of the conductance grade symbols. The symbols can stand alone with geology when planning a follow-up program. The actual conductance values are printed in the attached anomaly list for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike and dip, geometric shape, conductance, depth, and thickness (see below). The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

The attached EM anomaly list provides a tabulation of anomalies in ppm, conductance, and depth for the vertical sheet model. The EM anomaly list also shows the conductance and depth for a thin horizontal sheet (whole plane) model, but only the vertical sheet parameters appear on the EM map. The horizontal sheet model is suitable for a flatly dipping thin bedrock conductor such as a sulfide sheet having a thickness less than 10 m. The list also shows the



resistivity and depth for a conductive earth (half space) model, which is suitable for thicker slabs such as thick conductive overburden. In the EM anomaly list, a depth value of zero for the conductive earth model, in an area of thick cover, warns that the anomaly may be caused by conductive overburden.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute local anomaly amplitudes. This contrasts with the use of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth. Not shown in the EM anomaly list are the true amplitudes which are used to compute the horizontal sheet and conductive earth parameters.

#### X-type electromagnetic responses

DIGHEM maps contain x-type EM responses in addition to EM anomalies. An x-type response is below the noise threshold of 3 ppm, and reflects one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of the flight line, or aerodynamic noise. Those responses that

have the appearance of valid bedrock anomalies on the flight profiles are indicated by appropriate interpretive symbols (see EM map legend). The others probably do not warrant further investigation unless their locations are of considerable geological interest.

The thickness parameter

DIGHEM can provide an indication of the thickness of a steeply dipping conductor. The amplitude of the coplanar anomaly (e.g., CPI) increases relative to the coaxial anomaly (e.g., CXI) as the apparent thickness increases, i.e., the thickness in the horizontal plane. (The thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line.) This report refers to a conductor as thin when the thickness is likely to be less than 3 m, and thick when in excess of 10 m. Thin conductors are indicated on the EM map by the interpretive symbol "D", and thick conductors by "T". For base metal exploration in steeply dipping geology, thick conductors can be high priority targets because many massive sulfide ore bodies are thick, whereas non-economic bedrock conductors are often thin. The system cannot sense the thickness when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when

the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

Resistivity mapping

Areas of widespread conductivity are commonly encountered during surveys. In such areas, anomalies can be generated by decreases of only 5 m in survey altitude as well as by increases in conductivity. The typical flight record in conductive areas is characterized by inphase and quadrature channels which are continuously active. Local EM peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the correct interpretation of the airborne data. The advantage of the resistivity parameter is that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conductivity changes. The resistivity analysis also helps the interpreter to differentiate between conductive trends in the bedrock and those patterns typical of conductive overburden. For example, discrete conductors will generally appear as narrow lows on the contour map and broad conductors (e.g., overburden) will appear as wide lows.

The resistivity profile (see table in Appendix A) and the resistivity contour map present the apparent resistivity using the so-called pseudo-layer (or buried) half space model defined in Fraser (1978)<sup>2</sup>. This model consists of a resistive layer overlying a conductive half space. The depth channel (see Appendix A) gives the apparent depth below surface of the conductive material. The apparent depth is simply the apparent thickness of the overlying resistive layer. The apparent depth (or thickness) parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half space exists. The apparent depth parameter must be interpreted cautiously because it will contain any errors which may exist in the measured altitude of the EM bird (e.g., as caused by a dense tree cover). The inputs to the resistivity algorithm are the inphase and quadrature components of the coplanar coil-pair. The outputs are the apparent resistivity of the

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<sup>2</sup> Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v. 43, p. 144-172.

conductive half space (the source) and the sensor-source distance. The flying height is not an input variable, and the output resistivity and sensor-source distance are independent of the flying height. The apparent depth, discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter.

The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. The DIGHEM system has been flown for purposes of permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel can be of significant help in distinguishing between overburden and bedrock conductors.

The resistivity map often yields more useful information on conductivity distributions than the EM map. In

comparing the EM and resistivity maps, keep in mind the following:

- (a) The resistivity map portrays the absolute value of the earth's resistivity.  
(Resistivity =  $1/\text{conductivity}$ .)
  
- (b) The EM map portrays anomalies in the earth's resistivity. An anomaly by definition is a change from the norm and so the EM map displays anomalies, (i) over narrow, conductive bodies and (ii) over the boundary zone between two wide formations of differing conductivity.

The resistivity map might be likened to a total field map and the EM map to a horizontal gradient in the direction of flight<sup>3</sup>. Because gradient maps are usually more sensitive than total field maps, the EM map therefore is to be preferred in resistive areas. However, in conductive areas, the absolute character of the resistivity map usually causes it to be more useful than the EM map.

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<sup>3</sup> The gradient analogy is only valid with regard to the identification of anomalous locations.

Interpretation in conductive environments

Environments having background resistivities below 30 ohm-m cause all airborne EM systems to yield very large responses from the conductive ground. This usually prohibits the recognition of discrete bedrock conductors. The processing of DIGHEM data, however, produces six channels which contribute significantly to the recognition of bedrock conductors. These are the inphase and quadrature difference channels (DIFI and DIFQ), and the resistivity and depth channels (RES and DP) for each coplanar frequency; see table in Appendix A.

The EM difference channels (DIFI and DIFQ) eliminate up to 99% of the response of conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. An edge effect arises when the conductivity of the ground suddenly changes, and this is a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic

noise. The recognition of a bedrock conductor in a conductive environment therefore is based on the anomalous responses of the two difference channels (DIFI and DIFQ) and the two resistivity channels (RES). The most favourable situation is where anomalies coincide on all four channels.

The DP channels, which give the apparent depth to the conductive material, also help to determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When these channels ride above the zero level on the electrostatic chart paper (i.e., depth is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e., conductive overburden. If both DP channels are below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor. If the low frequency DP channel is below the zero level and the high frequency DP is above, this suggests that a bedrock conductor occurs beneath conductive cover.

Channels REC1, REC2, REC3 and REC4 are the anomaly recognition functions. They are used to trigger the conductance channel CDT which identifies discrete conductors. In highly conductive environments, channel REC2



is deactivated because it is subject to corruption by highly conductive earth signals. Similarly, in moderately conductive environments, REC4 is deactivated. Some of the automatically selected anomalies (channel CDT) are discarded by the geophysicist. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. The interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by the data, such as those arising from geologic or aerodynamic noise.

#### Reduction of geologic noise

Geologic noise refers to unwanted geophysical responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned above that the EM difference channels (i.e., channel DIFI for inphase and DIFQ for quadrature) tend to eliminate the response of conductive overburden. This marked a unique development in airborne EM technology, as DIGHEM is the only EM system which yields channels having an exceptionally high degree of immunity to conductive overburden.

Magnetite produces a form of geological noise on the inphase channels of all EM systems. Rocks containing less than 1% magnetite can yield negative inphase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the inphase EM channels may continuously rise and fall reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the inphase difference channel DIFI. This feature can be a significant aid in the recognition of conductors which occur in rocks containing accessory magnetite.

#### EM magnetite mapping

The information content of DIGHEM data consists of a combination of conductive eddy current response and magnetic permeability response. The secondary field resulting from conductive eddy current flow is frequency-dependent and consists of both inphase and quadrature components, which are positive in sign. On the other hand, the secondary field resulting from magnetic permeability is independent of frequency and consists of only an inphase component which

is negative in sign. When magnetic permeability manifests itself by decreasing the measured amount of positive inphase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative inphase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique was developed for the coplanar coil-pair of DIGHEM. The technique yields channel "FEO" (see Appendix A) which displays apparent weight percent magnetite according to a homogeneous half space model.<sup>4</sup> The method can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half space. It can individually resolve steeply dipping narrow magnetite-rich bands which are separated by 60 m. Unlike magnetometry, the EM magnetite method is unaffected by remanent magnetism or magnetic latitude.

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<sup>4</sup> Refer to Fraser, 1981, Magnetite mapping with a multi-coil airborne electromagnetic system: *Geophysics*, v. 46, p. 1579-1594.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as indicated by anomalies in the magnetite channel FEO.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

#### Recognition of culture

Cultural responses include all EM anomalies caused by man-made metallic objects. Such anomalies may be caused by inductive coupling or current gathering. The concern of the interpreter is to recognize when an EM response is due to culture. Points of consideration used by the interpreter, when coaxial and coplanar coil-pairs are operated at a common frequency, are as follows:

1. Channels CXS and CPS (see Appendix A) measure 50 and 60 Hz radiation. An anomaly on these channels shows

that the conductor is radiating cultural power. Such an indication is normally a guarantee that the conductor is cultural. However, care must be taken to ensure that the conductor is not a geologic body which strikes across a power line, carrying leakage currents.

2. A flight which crosses a line (e.g., fence, telephone line, etc.) yields a center-peaked coaxial anomaly and an m-shaped coplanar anomaly.<sup>5</sup> When the flight crosses the cultural line at a high angle of intersection, the amplitude ratio of coaxial/coplanar (e.g., CXI/CPI) is 4. Such an EM anomaly can only be caused by a line. The geologic body which yields anomalies most closely resembling a line is the vertically dipping thin dike. Such a body, however, yields an amplitude ratio of 2 rather than 4. Consequently, an m-shaped coplanar anomaly with a CXI/CPI amplitude ratio of 4 is virtually a guarantee that the source is a cultural line.
  
3. A flight which crosses a sphere or horizontal disk yields center-peaked coaxial and coplanar anomalies with a CXI/CPI amplitude ratio (i.e., coaxial/coplanar) of 1/4. In the absence of geologic bodies of this geometry, the most likely conductor is a metal roof or

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<sup>5</sup> See Figure II-1 presented earlier.

small fenced yard.<sup>4</sup> Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.

4. A flight which crosses a horizontal rectangular body or wide ribbon yields an m-shaped coaxial anomaly and a center-peaked coplanar anomaly. In the absence of geologic bodies of this geometry, the most likely conductor is a large fenced area.<sup>4</sup> Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.
  
5. EM anomalies which coincide with culture, as seen on the camera film, are usually caused by culture. However, care is taken with such coincidences because a geologic conductor could occur beneath a fence, for example. In this example, the fence would be expected to yield an m-shaped coplanar anomaly as in case #2 above. If, instead, a center-peaked coplanar anomaly occurred, there would be concern that a thick geologic conductor coincided with the cultural line.

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<sup>4</sup> It is a characteristic of EM that geometrically identical anomalies are obtained from: (1) a planar conductor, and (2) a wire which forms a loop having dimensions identical to the perimeter of the equivalent planar conductor.

6. The above description of anomaly shapes is valid when the culture is not conductively coupled to the environment. In this case, the anomalies arise from inductive coupling to the EM transmitter. However, when the environment is quite conductive (e.g., less than 100 ohm-m at 900 Hz), the cultural conductor may be conductively coupled to the environment. In this latter case, the anomaly shapes tend to be governed by current gathering. Current gathering can completely distort the anomaly shapes, thereby complicating the identification of cultural anomalies. In such circumstances, the interpreter can only rely on the radiation channels CXS and CPS, and on the camera film.

#### TOTAL FIELD MAGNETICS

The existence of a magnetic correlation with an EM anomaly is indicated directly on the EM map. An EM anomaly with magnetic correlation has a greater likelihood of being produced by sulfides than one that is non-magnetic. However, sulfide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Canada).

The magnetometer data are digitally recorded in the aircraft to an accuracy of one nT (i.e., one gamma). The digital tape is processed by computer to yield a total field magnetic contour map. When warranted, the magnetic data also may be treated mathematically to enhance the magnetic response of the near-surface geology, and an enhanced magnetic contour map is then produced. The response of the enhancement operator in the frequency domain is illustrated in Figure II-2. This figure shows that the passband components of the airborne data are amplified 20 times by the enhancement operator. This means, for example, that a 100 nT anomaly on the enhanced map reflects a 5 nT anomaly for the passband components of the airborne data.

The enhanced map, which bears a resemblance to a downward continuation map, is produced by the digital bandpass filtering of the total field data. The enhancement is equivalent to continuing the field downward to a level (above the source) which is 1/20th of the actual sensor-source distance.

Because the enhanced magnetic map bears a resemblance to a ground magnetic map, it simplifies the recognition of trends in the rock strata and the interpretation of



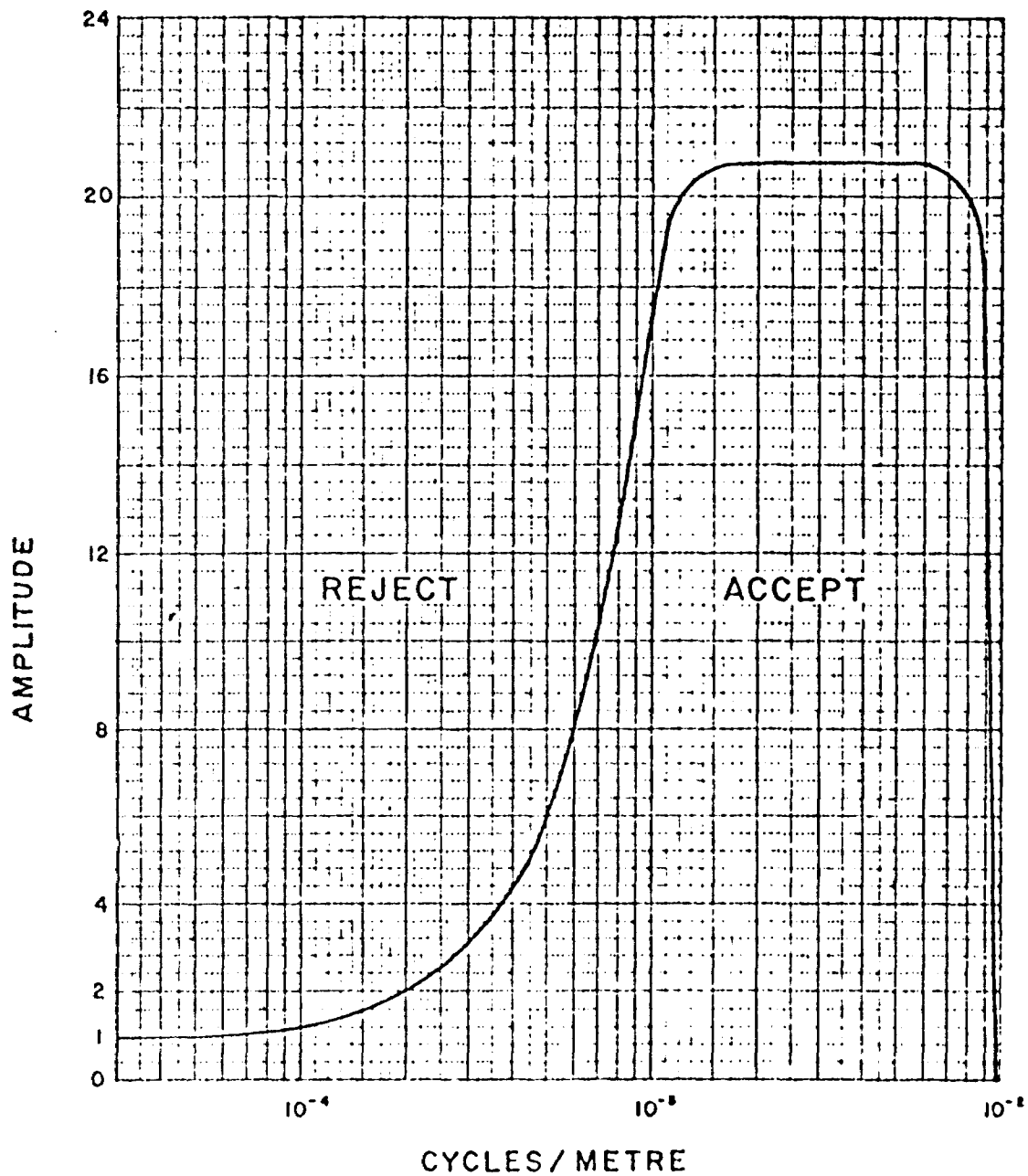


Figure II-2 Frequency response of magnetic enhancement operator.

geological structure. It defines the near-surface local geology while de-emphasizing deep-seated regional features. It primarily has application when the magnetic rock units are steeply dipping and the earth's field dips in excess of 60 degrees.

VLF-EM

VLF-EM anomalies are not EM anomalies in the conventional sense. EM anomalies primarily reflect eddy currents flowing in conductors which have been energized inductively by the primary field. In contrast, VLF-EM anomalies primarily reflect current gathering, which is a non-inductive phenomenon. The primary field sets up currents which flow weakly in rock and overburden, and these tend to collect in low resistivity zones. Such zones may be due to massive sulfides, shears, river valleys and even unconformities.

The Herz Industries Ltd Totem VLF-electromagnetometer measures the total field and vertical quadrature components. Both these components are digitally recorded in the aircraft with a sensitivity of 0.1 percent. The total field yields peaks over VLF-EM current concentrations

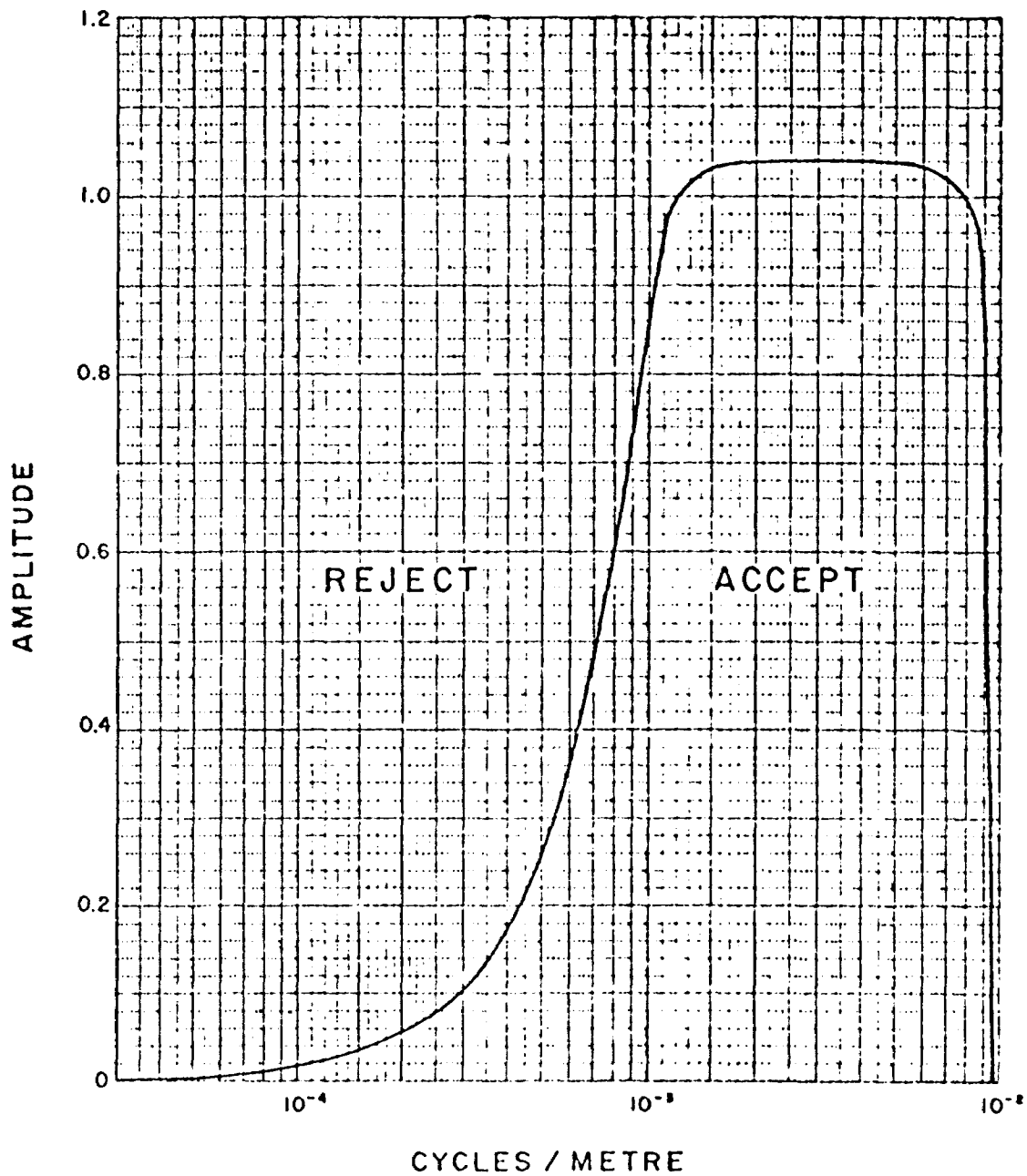


Figure II-3 Frequency response of VLF-EM operator.

whereas the quadrature component tends to yield crossovers. Both appear as traces on the profile records. The total field data also are filtered digitally and displayed on a contour map, to facilitate the recognition of trends in the rock strata and the interpretation of geologic structure.

The response of the VLF-EM total field filter operator in the frequency domain (Figure II-3) is basically similar to that used to produce the enhanced magnetic map (Figure II-2). The two filters are identical along the abscissa but different along the ordinant. The VLF-EM filter removes long wavelengths such as those which reflect regional and wave transmission variations. The filter sharpens short wavelength responses such as those which reflect local geological variations. The filtered total field VLF-EM contour map is produced with a contour interval of one percent.

MAPS ACCOMPANYING THIS REPORT

Five map sheets accompany this report:

Electromagnetic Anomalies	1 map sheet
Resistivity	1 map sheet
Total Field Magnetics	1 map sheet
Enhanced Magnetics	1 map sheet
Filtered total VLF-EM field	1 map sheet

Respectfully submitted,  
DIGHEM LIMITED



D.C. Fraser  
President

## A P P E N D I X A

### THE FLIGHT RECORD AND PATH RECOVERY

Both analog and digital flight records were produced. The analog profiles were recorded on chart paper in the aircraft during the survey. The digital profiles were generated later by computer and plotted on electrostatic chart paper at a scale of 1:15,840. The digital profiles are listed in Table A-1.

In Table A-1, the log resistivity scale of 0.03 decade/mm means that the resistivity changes by an order of magnitude in 33 mm. The resistivities at 0, 33, 67, 100 and 133 mm up from the bottom of the digital flight record are respectively 1, 10, 100, 1,000 and 10,000 ohm-m.

The fiducial marks on the flight records represent points on the ground which were recovered from camera film. Continuous photographic coverage allowed accurate photo-path recovery locations for the fiducials, which were then plotted on the geophysical maps to provide the track of the aircraft.

The fiducial locations on both the flight records and flight path maps were examined by a computer for unusual helicopter speed changes. Such speed changes may denote

an error in flight path recovery. The resulting flight path locations therefore reflect a more stringent checking than is normally provided by manual flight path recovery techniques.

Table A-1. The Digital Profiles

Channel Name (Freq)	Observed parameters	Scale units/mm
MAG	magnetics	10 nT
ALT	bird height	3 m
CXI ( 900 Hz)	vertical coaxial coil-pair inphase	1 ppm
CXQ ( 900 Hz)	vertical coaxial coil-pair quadrature	1 ppm
CXS ( 900 Hz)	ambient noise monitor (coaxial receiver)	1 ppm
CPI ( 900 Hz)	horizontal coplanar coil-pair inphase	1 ppm
CPQ ( 900 Hz)	horizontal coplanar coil-pair quadrature	1 ppm
CPI (7200 Hz)	horizontal coplanar coil-pair inphase	1 ppm
CPQ (7200 Hz)	horizontal coplanar coil-pair quadrature	1 ppm
VT1	VLF-EM total field	1 %
VQ2	VLF-EM vertical quadrature	1 %
<u>Computed Parameters</u>		
DIFI ( 900 Hz)	difference function inphase from CXI and CPI	1 ppm
DIFQ ( 900 Hz)	difference function quadrature from CXQ and CPQ	1 ppm
REC1	first anomaly recognition function	1 ppm
REC2	second anomaly recognition function	1 ppm
REC3	third anomaly recognition function	1 ppm
REC4	fourth anomaly recognition function	1 ppm
CDT	conductance	1 grade
RES ( 900 Hz)	log resistivity	.03 decade
RES (7200 Hz)	log resistivity	.03 decade
DP ( 900 Hz)	apparent depth	3 m
DP (7200 Hz)	apparent depth	3 m
FEO% ( 900 Hz)	apparent weight percent magnetite	0.25%

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A P P E N D I X B

EM ANOMALY LIST

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		COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH					
ANOMALY/ FID/INTERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 46	(FLIGHT 8)											
B 1961 B	16	6	14	7	28	12	33	19	2	112	31	80
LINE 45	(FLIGHT 8)											
A 1868 B	10	3	9	3	13	9	45	28	11	145	2	132
B 1870 B	9	3	9	3	13	8	38	29	1	167	673	39
E 1905 S	4	3	2	0	4	4	1	44	1	135	852	87
K 1925 B	5	4	6	4	18	22	11	43	1	160	151	104
LINE 44	(FLIGHT 8)											
B 1861 B	14	2	4	3	9	14	1	3	1	124	136	95
E 1828 S	0	1	0	1	0	11	1	10	1	58	5982	2
G 1817 S	0	2	0	5	0	41	1	0	1	0	2934	0
I 1809 B	0	5	2	4	4	31	1	0	1	7	2769	0
LINE 43	(FLIGHT 8)											
D 1779 S	0	0	0	3	0	21	1	0	1	187	1035	0
E 1784 B	9	11	12	14	43	33	8	22	1	101	229	49
F 1791 S	0	0	0	3	0	11	1	0	1	53	6414	0
LINE 42	(FLIGHT 8)											
A 1724 B?	4	0	2	1	3	7	1	0	1	183	386	138
B 1706 S	1	0	0	1	2	15	1	0	1	28	4137	0
E 1682 S	2	1	2	1	0	17	1	0	1	103	8280	0
G 1668 B	48	17	108	47	167	41	56	0	18	43	1	37
LINE 41	(FLIGHT 8)											
B 1603 B	53	14	72	20	94	16	95	16	3	104	14	80
C 1619 S?	1	2	1	3	13	11	1	22	1	95	227	66
E 1651 S	0	2	0	6	5	57	1	0	1	141	1035	0
P 1659 B	5	2	19	10	33	12	24	19	3	121	25	89
LINE 40	(FLIGHT 8)											
C 1583 B	8	6	10	10	25	18	11	20	2	101	34	69
D 1576 S	0	2	2	6	8	65	1	0	1	1	1547	0
E 1565 S	2	2	0	2	4	13	1	2	1	32	3691	0
I 1527 B	13	5	18	8	31	15	35	9	4	93	10	71
LINE 39	(FLIGHT 8)											
B 1427 S	2	2	0	9	5	78	1	0	1	0	1991	0
C 1434 B	6	3	5	3	18	8	15	42	1	127	69	86
D 1437 B	5	4	4	8	24	14	6	29	1	94	177	46

\* ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

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ANOMALY/ PID/INTERP	COAXIAL 900 HZ		COPLANAR 900 HZ		COPLANAR 7200 HZ		VERTICAL DIKE	COND MHOS	DEPTH* M	HORIZONTAL SHEET		CONDUCTIVE EARTH	
	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM				COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 39	(FLIGHT 8)												
G 1476 S	0	1	0	1	0	18	1	0	1	25	5075	0	
K 1496 B	31	12	69	30	115	31	46	0	3	69	18	45	
LINE 38	(FLIGHT 8)												
B 1415 S	0	2	1	3	11	51	1	0	1	10	1003	0	
C 1408 B	5	5	3	5	21	13	6	33	1	93	954	0	
D 1404 B	25	6	22	10	38	40	62	16	6	101	5	84	
F 1383 S	2	4	0	6	8	67	1	0	1	6	1399	0	
G 1371 S	0	1	0	1	1	13	1	3	1	39	5602	0	
LINE 37	(FLIGHT 8)												
A 1222 S	0	1	0	1	3	4	1	38	1	95	2293	39	
B 1232 B	0	5	2	4	9	12	1	24	1	104	144	78	
C 1235 B	6	4	5	4	19	18	12	22	1	123	182	67	
E 1257 S	0	0	0	2	2	21	1	0	1	14	4334	0	
H 1295 S	0	8	0	25	31	180	1	0	1	12	494	0	
I 1296 S?	0	10	0	35	64	31	1	12	1	20	431	0	
LINE 36	(FLIGHT 8)												
B 1198 B?	2	1	0	1	8	5	2	34	1	148	21	135	
G 1138 S	1	2	0	4	12	68	1	0	1	42	704	10	
LINE 35	(FLIGHT 8)												
B 1064 B	0	1	0	1	19	6	6	40	2	124	8	116	
C 1068 B	5	7	9	10	31	30	6	17	2	109	40	75	
F 1098 S	0	1	0	1	0	10	1	0	1	43	6169	0	
H 1126 S?	0	9	0	31	40	231	1	0	1	8	453	0	
LINE 34	(FLIGHT 8)												
C 1020 B	26	8	21	9	42	11	48	21	7	100	4	84	
D 1016 B	3	7	7	4	26	21	5	13	2	127	33	92	
E 1011 S	6	0	0	1	4	13	1	3	1	169	393	127	
LINE 33	(FLIGHT 8)												
B 890 B	4	9	5	9	21	26	9	36	1	61	758	4	
C 892 B	4	9	7	9	25	26	4	27	2	118	62	80	
E 896 B	12	8	21	12	33	30	19	24	2	101	55	66	
F 907 S	0	2	0	3	2	46	1	0	1	0	2796	0	
H 931 S	0	1	0	2	3	28	1	0	1	3	3606	0	
LINE 32	(FLIGHT 8)												
E 840 B	2	6	7	4	24	3	6	25	1	94	985	0	

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	COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH	ANOMALY/ PID/INTERP		REAL QUAD PPM	REAL QUAD PPM	REAL QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 32 (FLIGHT 8)																	
G 838 B	10	2	13	2	16	6	106	38	4	122	13	97					
H 835 B	6	5	9	4	14	6	14	37	1	119	188	66					
I 831 S	0	4	0	12	17	87	1	0	1	7	808	0					
J 803 S?	0	28	0	84	326	552	1	0	1	0	260	0					
LINE 31 (FLIGHT 8)																	
A 723 S?	0	1	0	0	0	6	1	0	1	48	6495	0					
B 725 S?	0	1	2	3	5	4	1	55	1	66	4838	4					
C 730 B	6	6	5	6	10	39	6	17	1	90	218	38					
D 737 S	1	1	0	2	0	14	1	0	1	14	4705	0					
LINE 30 (FLIGHT 8)																	
A 689 S	2	1	1	3	2	13	1	0	1	51	3796	0					
B 659 B	21	19	16	25	47	111	11	2	2	55	47	25					
D 626 S	3	2	0	11	31	70	1	0	1	8	350	0					
LINE 29 (FLIGHT 8)																	
A 509 S	2	1	0	1	9	5	2	32	1	118	210	87					
D 480 B	15	9	11	16	41	41	13	7	2	77	37	46					
E 462 S	0	2	0	3	6	31	1	0	1	21	1841	0					
G 446 S	2	2	0	4	12	50	1	0	1	15	854	0					
LINE 28 (FLIGHT 7)																	
D 2027 S?	0	3	0	7	5	66	1	0	1	0	2148	0					
E 2032 S	0	1	0	2	2	7	1	18	1	35	5658	0					
G 2056 B	25	20	22	35	89	59	12	9	2	81	38	51					
H 2070 S	1	1	0	1	4	6	4	70	1	164	1035	0					
I 2095 S	4	19	0	56	206	361	1	0	1	0	327	0					
LINE 27 (FLIGHT 7)																	
C 1983 S?	0	3	0	5	10	19	1	3	1	48	721	14					
G 1962 B	2	4	0	2	13	2	2	25	1	136	1035	0					
H 1958 B	17	11	12	19	55	39	12	7	1	63	60	30					
J 1952 S?	2	9	0	15	33	143	1	0	1	7	425	0					
K 1949 S	0	3	0	6	11	62	1	0	1	13	1023	0					
N 1926 S	0	10	0	17	36	154	1	0	1	7	414	0					
LINE 26 (FLIGHT 7)																	
E 1822 S	0	1	0	1	6	22	1	0	1	41	1312	1					
F 1829 S?	2	2	0	2	4	19	1	0	1	18	4762	0					
I 1852 B	11	14	15	14	48	38	9	15	2	87	31	58					

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	COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH							
ANOMALY/ FID/INTERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M	
LINE 26 (FLIGHT 7)													
J 1857 B	34	28	20	41	128	102	12	5	1	39	63	12	
K 1860 B?	0	11	20	31	81	318	1	0	1	8	131	0	
L 1862 S	0	15	0	34	76	274	1	4	1	13	425	0	
N 1892 B	0	2	3	10	33	35	1	20	1	68	341	22	
LINE 25 (FLIGHT 7)													
E 1788 S	0	2	0	3	8	12	1	0	1	138	1035	0	
H 1781 B	4	15	0	12	24	35	2	0	1	46	773	0	
I 1767 S	0	1	0	1	0	19	1	0	1	9	4663	0	
K 1756 B	10	17	9	35	98	31	4	0	1	63	99	26	
L 1754 B?	2	9	6	30	110	202	1	0	1	9	113	0	
LINE 24 (FLIGHT 7)													
A 1629 B	0	2	2	10	21	25	1	1	1	57	348	8	
B 1632 B?	0	1	0	1	6	9	1	29	1	101	769	59	
E 1645 S?	1	4	0	5	12	10	2	23	1	92	972	0	
H 1664 S?	0	3	0	3	15	8	1	0	1	99	966	4	
I 1668 B	12	9	7	8	31	11	12	31	1	111	132	64	
J 1672 B	28	17	31	35	120	72	17	21	2	69	25	45	
K 1679 B	18	19	8	58	46	186	5	1	1	63	114	26	
L 1682 B	11	46	7	106	348	708	2	0	1	5	297	0	
LINE 23 (FLIGHT 7)													
D 1564 S	0	1	0	3	6	33	1	0	1	123	1035	0	
E 1560 S	0	0	0	1	5	9	1	11	1	47	4246	0	
H 1552 B	0	2	0	3	10	3	4	37	1	120	164	90	
I 1545 B	47	26	39	41	136	66	24	0	3	56	15	34	
J 1540 B	18	10	13	10	49	52	19	9	2	73	46	41	
K 1530 B?	4	1	3	1	8	6	41	64	1	200	1035	0	
L 1517 S	0	2	0	6	18	45	1	0	1	21	512	0	
LINE 22 (FLIGHT 7)													
A 1435 S?	0	1	0	1	4	5	1	35	1	53	6339	0	
D 1441 S	0	3	0	6	8	35	1	0	1	73	867	0	
F 1449 B	1	17	3	17	29	33	6	10	1	27	652	0	
I 1468 B	0	6	0	8	7	13	8	39	1	80	846	6	
J 1474 B	20	17	9	17	31	39	11	16	1	62	156	22	
K 1477 S	0	12	6	29	60	230	1	0	1	9	252	0	
L 1482 B	0	4	0	1	8	21	1	1	1	65	297	37	
M 1484 B?	0	4	0	3	11	21	1	4	1	93	152	66	
N 1489 B	9	4	2	7	17	35	11	35	1	80	345	28	

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201 RENNIE LAKE

		COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH					
ANOMALY/ FID/INTERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 22	(FLIGHT	7)										
O 1504 S	0	3	0	8	38	69	1	0	1	19	234	0
LINE 21	(FLIGHT	7)										
C 1383 S	0	2	0	2	0	24	1	0	1	1	3714	0
E 1379 S	0	0	0	1	3	10	1	0	1	24	2723	0
F 1375 S	0	1	0	2	3	18	1	0	1	3	3879	0
G 1363 S?	0	1	0	1	5	3	2	41	1	127	399	88
H 1357 B	7	7	0	9	22	14	5	27	1	95	949	3
J 1354 S	0	4	0	10	31	62	1	0	1	12	331	0
LINE 2100	(FLIGHT	7)										
A 1196 S	2	2	2	6	29	54	1	0	1	17	299	0
LINE 20	(FLIGHT	7)										
C 1131 S	0	0	0	1	0	15	1	0	1	22	4649	0
D 1141 B?	0	2	0	6	3	63	1	0	1	0	2260	0
E 1146 S	0	2	0	6	2	61	1	0	1	0	2219	0
G 1150 B?	0	7	2	7	17	13	8	22	1	107	1035	0
J 1158 S	0	15	2	36	111	339	1	0	1	10	126	0
L 1170 B	5	6	9	14	40	39	6	33	1	100	62	64
N 1184 S	4	6	2	15	62	112	1	0	1	22	121	5
LINE 19	(FLIGHT	7)										
D 1070 B?	0	2	2	1	9	14	5	56	1	173	1035	0
E 1061 B?	0	5	0	3	6	11	7	33	1	128	1035	0
F 1045 S?	0	0	0	0	5	11	1	10	1	202	1035	0
G 1037 S	0	2	0	15	15	41	1	0	1	18	669	0
J 1023 B?	2	3	0	12	31	104	1	0	1	9	437	0
L 1011 S	3	3	0	9	32	71	1	0	1	21	157	0
LINE 18	(FLIGHT	7)										
A 958 S	0	1	0	3	0	45	1	0	1	0	2774	0
C 975 B	4	12	2	2	10	17	2	12	1	197	98	143
D 991 B?	0	4	0	17	41	116	1	0	1	12	318	0
F 998 S	0	3	0	9	34	71	1	0	1	15	332	0
LINE 17	(FLIGHT	7)										
A 856 B?	0	0	0	2	2	3	1	53	1	43	6065	0
C 844 B?	0	2	3	7	26	20	7	33	1	136	1035	0
D 842 B	1	6	12	9	28	29	4	23	1	104	91	63
E 834 S	5	15	0	31	44	117	1	0	1	10	439	0

\* ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

201 RENNIE LAKE

ANOMALY/ FID/INTERP	COAXIAL 900 HZ		COPLANAR 900 HZ		COPLANAR 7200 HZ		VERTICAL DIKE	COND MHOS	DEPTH* M	HORIZONTAL SHEET		CONDUCTIVE EARTH	
	PPM	PPM	PPM	PPM	PPM	PPM				COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
-----													
LINE 17	(FLIGHT 7)												
F 812 B?	2	2	1	3	10	8	2	13	1	93	230	62	
-----													
LINE 16	(FLIGHT 7)												
A 706 S	1	1	0	3	5	21	1	0	1	19	1982	0	
B 717 B?	0	1	1	8	21	35	1	0	1	144	986	17	
C 721 B	0	6	2	14	39	17	2	5	1	55	806	0	
D 729 B?	0	7	0	10	21	94	1	0	1	12	649	0	
E 731 S?	0	7	0	11	24	6	1	0	1	33	706	0	
H 754 B?	0	1	0	5	0	10	1	3	1	47	5858	0	
J 760 B	0	6	2	4	18	9	6	25	1	104	288	45	
K 766 S	1	3	0	2	10	12	1	26	1	94	418	60	
-----													
LINE 15	(FLIGHT 7)												
A 685 S	0	3	0	0	4	12	1	0	1	21	5383	0	
D 679 B?	0	3	4	8	20	15	7	26	1	84	949	0	
E 677 B	0	4	4	8	25	23	2	4	1	60	221	14	
G 670 B?	0	4	5	4	18	48	2	21	1	40	733	0	
L 645 B	9	4	2	4	13	8	17	26	1	95	772	0	
M 637 B	4	4	0	2	14	11	5	32	1	121	1035	0	
N 631 S?	0	6	0	17	32	139	1	0	1	5	486	0	
-----													
LINE 14	(FLIGHT 7)												
B 542 S	0	1	0	5	11	28	1	0	1	21	828	0	
H 557 S	2	2	0	7	11	51	1	0	1	8	866	0	
I 563 B	9	5	1	11	23	95	7	19	1	40	756	0	
J 588 S	0	1	0	2	0	29	1	0	1	2	3532	0	
K 596 S?	3	0	0	3	7	13	1	16	1	89	657	50	
L 603 B	12	6	3	8	22	4	13	29	1	103	281	47	
-----													
LINE 13	(FLIGHT 7)												
A 520 B?	0	1	0	6	7	5	1	36	1	75	827	35	
B 511 B	9	4	0	7	21	33	10	27	1	58	837	0	
D 485 B	0	1	5	3	14	2	6	56	2	155	32	118	
E 475 B	2	2	2	2	15	7	3	12	1	86	101	62	
-----													
LINE 12	(FLIGHT 7)												
B 376 S?	0	2	1	3	5	13	1	0	1	20	4374	0	
F 412 B	0	4	3	2	10	12	1	17	1	82	269	52	
H 419 B	13	18	7	13	37	57	7	9	1	41	513	0	
-----													
LINE 11	(FLIGHT 7)												
A 364 B	7	2	5	2	13	3	28	37	1	196	795	45	

\* ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

201 RENNIE LAKE

	COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH						
ANOMALY/ FID/INTERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 11 (FLIGHT 7)												
B 347 S?	1	1	0	1	5	4	4	77	1	205	1035	0
F 332 B	3	4	5	7	30	25	5	22	1	84	135	39
G 328 B	2	1	3	2	10	29	1	0	1	22	855	0
LINE 10 (FLIGHT 7)												
A 281 S	0	3	0	5	4	52	1	0	1	0	2217	0
B 308 B	0	3	2	3	14	10	6	41	1	117	317	50
D 315 B	4	2	0	3	12	6	8	62	1	161	1035	0
LINE 9 (FLIGHT 4)												
A 724 S	3	2	0	6	15	49	1	0	1	6	708	0
B 705 B	6	2	2	2	10	4	18	24	1	181	1035	0
C 704 B	6	2	2	2	8	3	3	25	1	103	53	83
LINE 8 (FLIGHT 4)												
C 592 S	3	1	0	1	0	10	1	0	1	73	7305	0
D 598 B?	3	0	1	2	4	2	2	48	1	105	867	59
G 606 B	11	10	9	9	18	21	1	2	1	51	315	23
H 608 B	11	10	9	9	24	21	10	8	2	101	59	63
I 613 B	23	9	18	18	53	32	25	10	2	74	35	44
LINE 7 (FLIGHT 4)												
A 561 S	0	2	0	6	6	48	1	0	1	0	1889	0
B 543 B	9	4	3	4	11	8	16	15	1	103	1035	0
C 539 B	19	4	10	7	13	5	48	6	3	127	26	94
LINE 6 (FLIGHT 4)												
A 494 S	0	3	0	5	5	55	1	0	1	0	1943	0
D 518 B	2	7	9	13	30	20	3	4	1	62	863	0
E 523 B	6	7	5	7	19	17	7	27	1	109	150	60
LINE 5 (FLIGHT 4)												
A 471 S	3	1	0	2	4	16	1	0	1	23	1861	0
B 451 B?	0	2	0	3	3	5	1	30	1	58	3106	8
C 445 B	3	1	1	1	1	3	25	51	1	182	1035	0
LINE 4 (FLIGHT 4)												
A 427 B	0	1	1	2	4	8	1	2	1	50	1700	4
LINE 3 (FLIGHT 4)												
D 361 B	10	1	1	1	0	5	207	15	1	173	1035	0

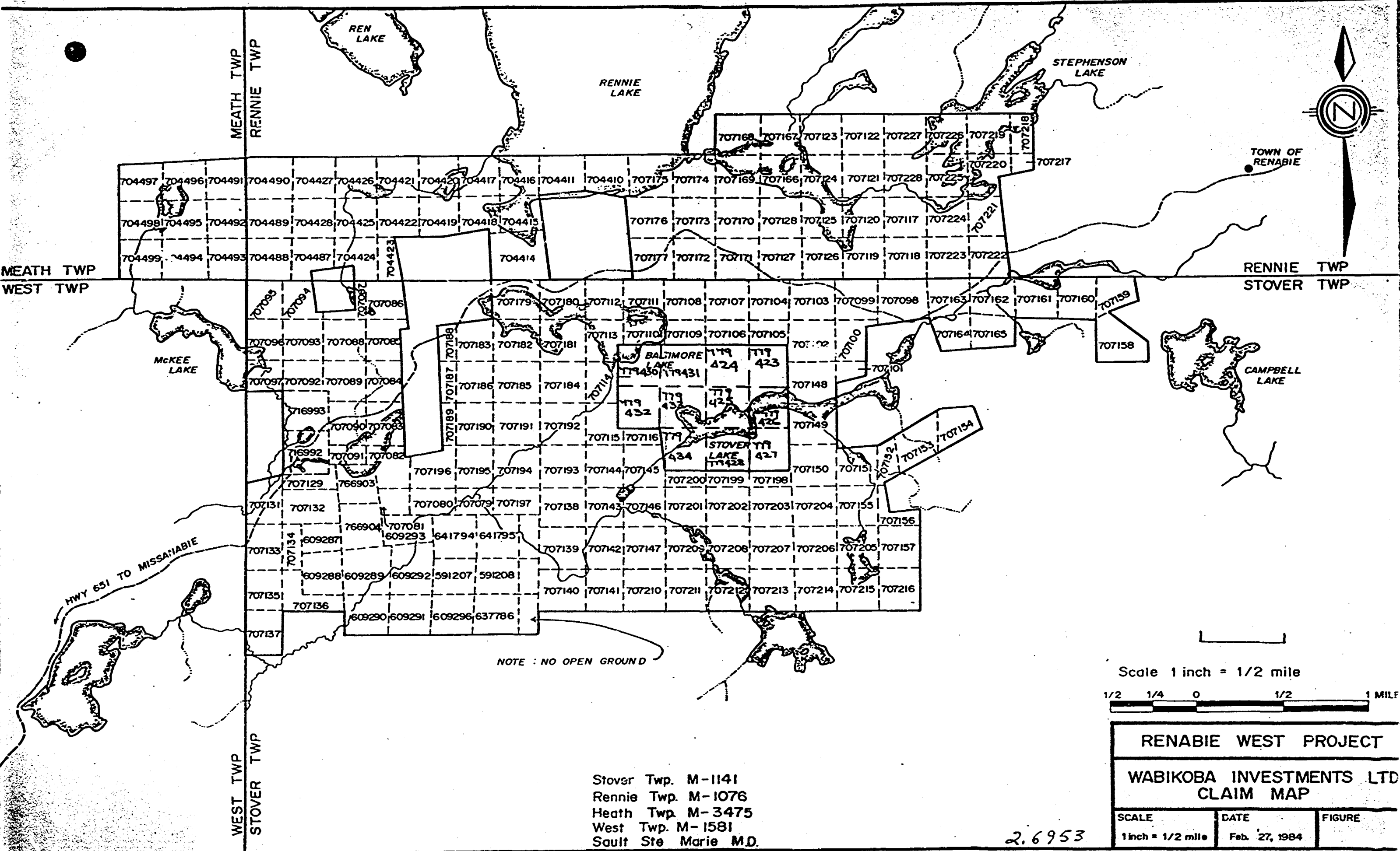
\* ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

201 RENNIE LAKE

	COAXIAL 900 HZ	COPLANAR 900 HZ	COPLANAR 7200 HZ	VERTICAL DIKE	HORIZONTAL SHEET	CONDUCTIVE EARTH				
ANOMALY/ FID/INTERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	COND MHOS	DEPTH* M	COND MHOS	DEPTH M	RESIS OHM-M	DEPTH M
LINE 3 (FLIGHT 4)										
E 356 B	2	1	2	1	6	7	20	42	1	163 888 8

. \* ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .  
 . OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .  
 . LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS. .





NOTE : NO OPEN GROUND

Scale 1 inch = 1/2 mile  
 1/2 1/4 0 1/2 1 MILE

RENABIE WEST PROJECT		
WABIKOBA INVESTMENTS LTD CLAIM MAP		
SCALE 1 inch = 1/2 mile	DATE Feb. 27, 1984	FIGURE

Stover Twp. M-1141  
 Rennie Twp. M-1076  
 Heath Twp. M-3475  
 West Twp. M-1581  
 Sault Ste Marie M.D.

2.6953



SELF POTENTIAL

Instrument \_\_\_\_\_ Range \_\_\_\_\_

Survey Method \_\_\_\_\_

Corrections made \_\_\_\_\_

RADIOMETRIC

Instrument \_\_\_\_\_

Values measured \_\_\_\_\_

Energy windows (levels) \_\_\_\_\_

Height of instrument \_\_\_\_\_ Background Count \_\_\_\_\_

Size of detector \_\_\_\_\_

Overburden \_\_\_\_\_  
(type, depth - include outcrop map)

OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)

Type of survey \_\_\_\_\_

Instrument \_\_\_\_\_

Accuracy \_\_\_\_\_

Parameters measured \_\_\_\_\_

Additional information (for understanding results) \_\_\_\_\_

AIRBORNE SURVEYS

Type of survey(s) MAQ, EM, VLF-EM

Instrument(s) DIQHEM LTD.  
(specify for each type of survey)

Accuracy \_\_\_\_\_  
(specify for each type of survey)

Aircraft used \_\_\_\_\_

Sensor altitude \_\_\_\_\_

Navigation and flight path recovery method \_\_\_\_\_

Aircraft altitude \_\_\_\_\_ Line Spacing \_\_\_\_\_

Miles flown over total area \_\_\_\_\_ Over claims only \_\_\_\_\_



SELF POTENTIAL

Instrument \_\_\_\_\_ Range \_\_\_\_\_

Survey Method \_\_\_\_\_

Corrections made \_\_\_\_\_

RADIOMETRIC

Instrument \_\_\_\_\_

Values measured \_\_\_\_\_

Energy windows (levels) \_\_\_\_\_

Height of instrument \_\_\_\_\_ Background Count \_\_\_\_\_

Size of detector \_\_\_\_\_

Overburden \_\_\_\_\_

(type, depth - include outcrop map)

OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)

Type of survey \_\_\_\_\_

Instrument \_\_\_\_\_

Accuracy \_\_\_\_\_

Parameters measured \_\_\_\_\_

Additional information (for understanding results) \_\_\_\_\_

AIRBORNE SURVEYS

Type of survey(s) VLF-EM, EM, MAG

Instrument(s) DIQHEM LTD.  
(specify for each type of survey)

Accuracy \_\_\_\_\_  
(specify for each type of survey)

Aircraft used \_\_\_\_\_

Sensor altitude \_\_\_\_\_

Navigation and flight path recovery method \_\_\_\_\_

Aircraft altitude \_\_\_\_\_ Line Spacing \_\_\_\_\_

Miles flown over total area \_\_\_\_\_ Over claims only \_\_\_\_\_



Ministry of Natural Resources

File \_\_\_\_\_

GEOPHYSICAL - GEOLOGICAL - GEOCHEMICAL  
TECHNICAL DATA STATEMENT

TO BE ATTACHED AS AN APPENDIX TO TECHNICAL REPORT  
FACTS SHOWN HERE NEED NOT BE REPEATED IN REPORT  
TECHNICAL REPORT MUST CONTAIN INTERPRETATION, CONCLUSIONS ETC.

Type of Survey(s) DIGHEM MAG & ~~DEF~~ EM  
Township or Area STOVER, RENNIE, MEATH  
Claim Holder(s) R. J. MCGOWAN  
E. PAQUETTE  
Survey Company DIGHEM LTD  
Author of Report D.C. FRASER  
Address of Author 1010- 1<sup>st</sup> Canadian Place, Toronto  
Covering Dates of Survey 13-14 APRIL 1984  
(linecutting to office)  
Total Miles of Line Cut —

MINING CLAIMS TRAVERSED  
List numerically

(prefix) (number)

SEE ATTACHED LIST

205 claims

Claim map in pocket

If space insufficient, attach list

SPECIAL PROVISIONS  
CREDITS REQUESTED

DAYS  
per claim

- Geophysical
  - Electromagnetic \_\_\_\_\_
  - Magnetometer \_\_\_\_\_
  - Radiometric \_\_\_\_\_
  - Other \_\_\_\_\_
- Geological \_\_\_\_\_
- Geochemical \_\_\_\_\_

ENTER 40 days (includes  
line cutting) for first  
survey.

ENTER 20 days for each  
additional survey using  
same grid.

AIRBORNE CREDITS (Special provision credits do not apply to airborne surveys)

Magnetometer 25 Electromagnetic 25 Radiometric \_\_\_\_\_  
(enter days per claim)

DATE: 13 JULY 84 SIGNATURE: [Signature]  
Author of Report or Agent

Res. Geol. \_\_\_\_\_ Qualifications \_\_\_\_\_

Previous Surveys

File No.	Type	Date	Claim Holder

TOTAL CLAIMS 205

SELF POTENTIAL

Instrument \_\_\_\_\_ Range \_\_\_\_\_

Survey Method \_\_\_\_\_

Corrections made \_\_\_\_\_

RADIOMETRIC

Instrument \_\_\_\_\_

Values measured \_\_\_\_\_

Energy windows (levels) \_\_\_\_\_

Height of instrument \_\_\_\_\_ Background Count \_\_\_\_\_

Size of detector \_\_\_\_\_

Overburden \_\_\_\_\_

(type, depth - include outcrop map)

OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)

Type of survey \_\_\_\_\_

Instrument \_\_\_\_\_

Accuracy \_\_\_\_\_

Parameters measured \_\_\_\_\_

Additional information (for understanding results) \_\_\_\_\_

AIRBORNE SURVEYS

Type of survey(s) VES EM, MAG

Instrument(s) DIGHEM  
(specify for each type of survey)

Accuracy \_\_\_\_\_  
(specify for each type of survey)

Aircraft used HELICOPTER

Sensor altitude \_\_\_\_\_

Navigation and flight path recovery method PHOTOGRAPHIC

Aircraft altitude \_\_\_\_\_ Line Spacing \_\_\_\_\_

Miles flown over total area 206 km Over claims only 206 km.

STOVER TWP

SSM ✓ 707092  
 707093  
 707094  
 707095  
 707096  
 707097

✓ 707129  
 707131  
 707132  
 707133  
 707134  
 707135  
 707136  
707137

~~SSM~~ ~~707100~~  
 SSM ✓ 707081  
 707082  
 707083  
 707084  
 707085  
 707086  
 707087  
 707088  
 707089  
 707090  
 707091

~~SSM~~ ~~707109~~  
 SSM 707079  
 707080

SSM 641794  
 641795

29 claims

SSM ✓ 766903  
 766904

SSM ✓ 609287  
 609288  
 609289  
 609290  
 609291  
 609292  
 609293

~~SSM~~ ~~707158~~  
 SSM ✓ 707159  
 707160  
 707161  
 707162  
 707163  
 707164  
 707165

SSM 707098  
 ✓ 707099  
 707100  
 707101  
 707102  
 707103  
 707104  
 707105  
 707106  
 707107  
 707108  
 707109  
 707110

30 claims

TOTALS	
page 1	59
2	60
3	21
4	9
5	56
	<u>205</u>

= 59 claims



STOVER TOWNSHIP (CONT.)

SSM 707111  
✓ 707112  
707113  
707114  
707115  
707116

SSM 707179  
✓ 707180  
707181  
707182  
707183  
707184  
707185  
707186  
707187  
707188  
707189

SSM 707190  
✓ 707191  
707192  
707193  
707194  
707195  
707196

SSM 707211  
✓ 707212  
707213  
707214  
707215  
707216

SSM 707197

SSM 707144  
707147

SSM 591207  
✓ 591208

✓SSM ✓ 609296  
✓SSM ✓ 687786

SSM 716993  
716992

SSM ✓ 707138  
707139  
707140  
707141  
707142  
707143  
707144  
707145  
707146  
707147

SSM ✓ 707198  
707199  
707200  
707201  
707202  
707203  
707204  
707205  
707206  
707207  
707208  
707209  
707210

---

31 claims

+

---

29

=

69 claims

STOVER TOWNSHIP (CONT)

SSM 707 148  
/ 707 149  
707 150  
707 151  
707 152  
707 153  
707 154  
707 155  
707 156  
707 157

MR. G. PAQUETTE'S CLAIMS /

SSM 779 423  
/ 779 424  
779 425  
779 426  
779 427  
779 428

SSM 779 430  
779 431  
779 432  
779 433  
779 434.

---

21 claims

MEATH TWP

SSM 704491  
704492  
704493  
704494  
704495  
704496  
704497  
704498  
704499

---

9 claims

RENNIE TWP

SSM 707218  
 707219  
 707220  
 707221  
 707222  
 707223  
 707224  
 707225  
 707226  
 707227  
 707228

SSM 707117  
 707118  
 707119  
 707120  
 707121  
 707122  
 707123  
 707124  
 707125  
 707126  
 707127  
 707128

SSM 704487  
 704488  
 704489  
 704490

SSM 707166  
 707167  
 707168  
 707169  
 707170  
 707171  
 707172  
 707173  
 707174  
 707175  
 707176  
 707177

SSM 704410  
 704411  
 704414  
 704415  
 704416  
 704417  
 704418  
 704419  
 704420  
 704421  
 704422  
 704423  
 704424  
 704425  
 704426  
 704427  
 704428  
 7044

27 claims

+

29 claims

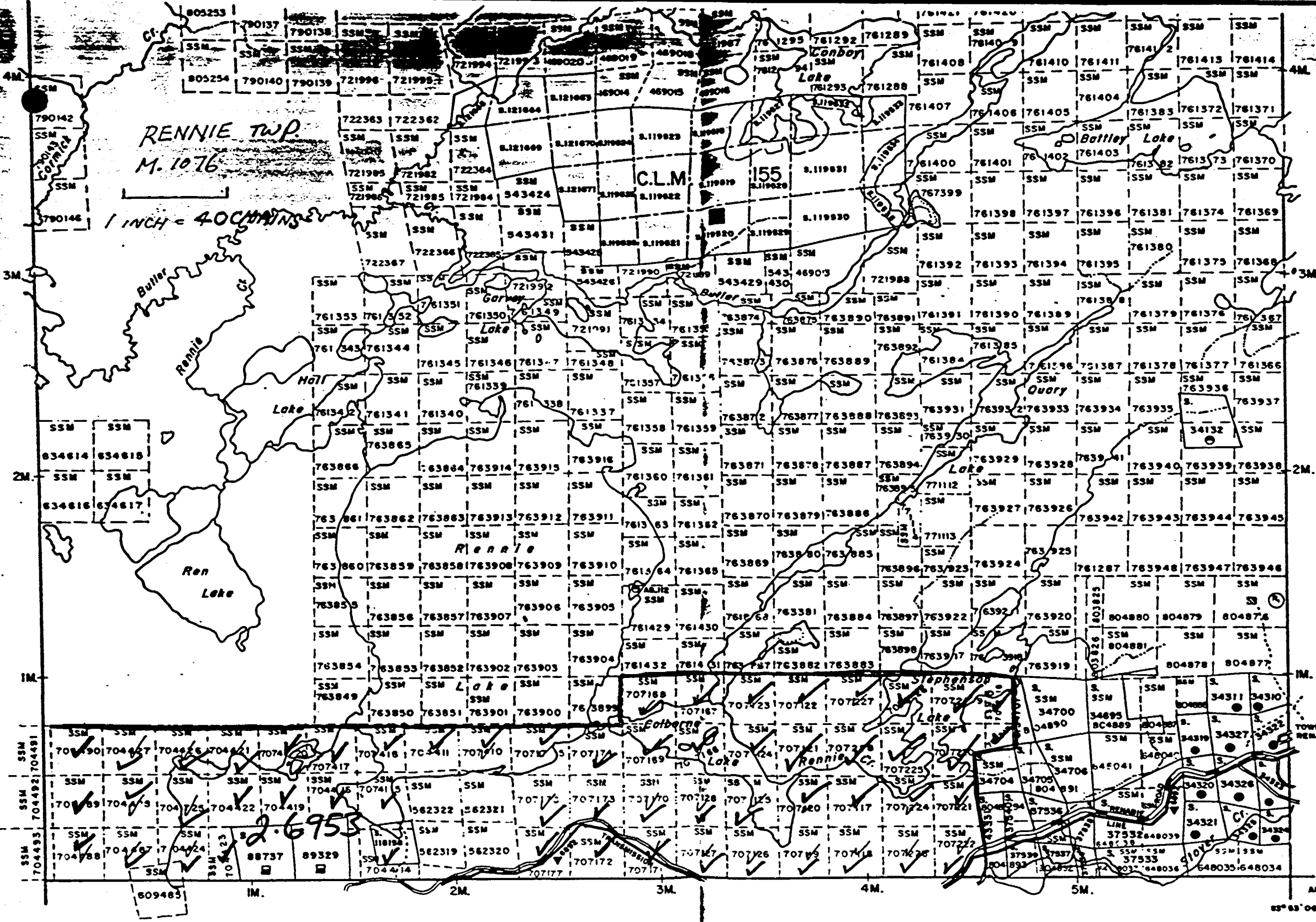
=

56 claims



MEATH TP. M.1265

LEESON TP. M.984



RENNIE TWP.  
M. 1076

1 INCH = 40 CHAINS

C.L.M.

155

Ren Lake

RENNIE

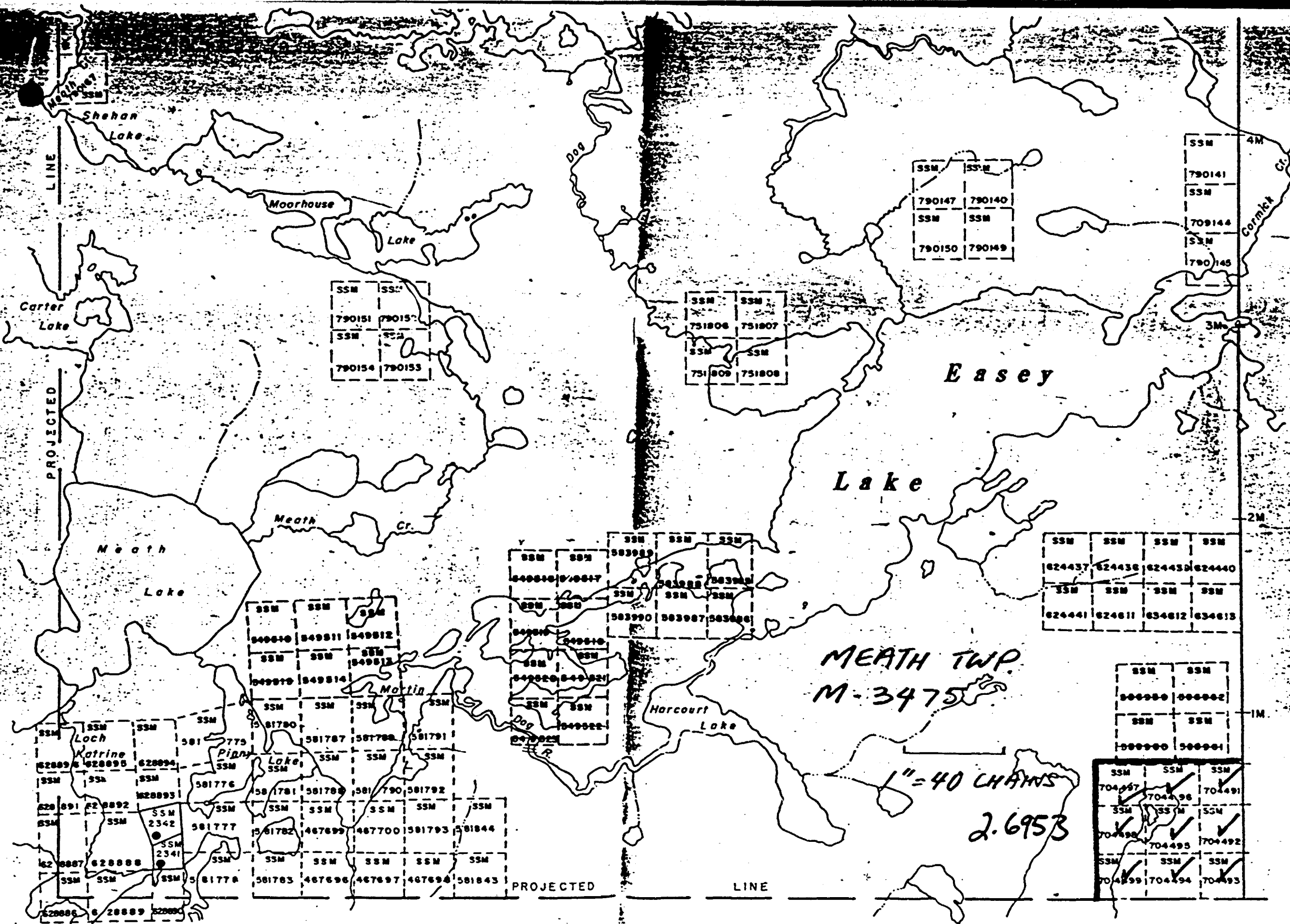
STEPHENSON  
Lake

STOVER TP. M.1141

48° 21' 00"  
APPROX.  
83° 03' 00"

GLASGOW TP. M - 1265

RENNIE TP. M - 1076



WEST TP. M - 1581







Ministry of  
Natural  
Resources  
Ontario

Report of Work  
(Geophysical, Geological,  
Geochemical and Expenditures)

2.6953  
2.6953

Instructions: - Please type or print  
- If number of mining claims traversed  
exceeds space on this form, attach a list.  
Note: - Only days credits calculated in the  
"Expenditures" section may be entered  
in the "Expend. Days Cr." columns.  
- Do not use shaded areas below.

The Mining Act

Type of Survey(s) <b>AIRBORNE EM, MAG, VLF-EM</b>	Township or Area <b>STOVER TSP</b>
Claim Holder(s) <b>DANIEL ST. PIERRE &amp; RICHARD LAVOIE / POR G. PAQUETTE</b>	Prospector's Licence No. <b>M21144 / M21092</b>
Address <b>BOX 2028, WAWA, ONT. POS 1K0</b>	
Survey Company <b>DIGHEM LTD</b>	Date of Survey (from & to) <b>13 04 84 / 14 04 84</b> Day   Mo.   Yr.   Day   Mo.   Yr.
Name and Address of Author (of Geo-Technical report) <b>D.C. FRASER, 4010-1<sup>ST</sup> CANADIAN PLACE, TORONTO ONT M5X 1C7</b>	

Credits Requested per Each Claim in Columns at right

Special Provisions	Geophysical	Days per Claim
For first survey: Enter 40 days. (This includes line cutting)	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
For each additional survey: using the same grid: Enter 20 days (for each)	Geological	
	Geochemical	
Man Days Complete reverse side and enter total(s) here	Geophysical	Days per Claim
	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
	Geological	
	Geochemical	
Airborne Credits Note: Special provisions credits do not apply to Airborne Surveys.	Electromagnetic	30
	Magnetometer	30
	VLF-EM	20
	Radiometric	

Mining Claims Traversed (List in numerical sequence)

Mining Claim		Expend. Days Cr.	Mining Claim		Expend. Days Cr.
Prefix	Number		Prefix	Number	
SSM	449423				
	449424				
	449425				
	449426				
	449427				
	449428				
	449430				
	449431				
	449432				
	449433				
	449434				

**RECEIVED**  
MINE LANDS SECTION  
JUL 31 1984

Expenditures (excludes power stripping)

Type of Work Performed

Performed on Claim(s)

Calculation of Expenditure Days Credits

Total Expenditures \$  + 15 =

Total Days Credits

Instructions  
Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected in columns at right.

Date **27 JULY 84** Record of Holder or Agent (Signature)

For Office Use Only

Total Days Cr. Recorded	Date Recorded	Mining Recorder
	Date Approved as Recorded	Branch Director

Certification Verifying Report of Work

I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.



(AMENDED)

The Mining Act

Type of Survey(s) <b>AIRBORNE EM, MAG, VLF-EM</b>	Township or Area <b>STOUCER TSP</b>
Claim Holder(s) <b>DANIEL ST. PIERRE &amp; RICHARD LAVOIE / FOR G. PAQUETTE</b>	Prospector's Licence No. <b>121144 / 121092</b>
Address <b>Box 2028, Wawa, Ont P0S 1K0</b>	
Survey Company <b>DIGHEM LTD</b>	Date of Survey (from & to) <b>13 04 84 / 14 04 84</b>
Name and Address of Author (of Geo-Technical report) <b>D.C. FRASER, 4010 - 1<sup>ST</sup> CANADIAN PLACE, TORONTO ONT. M5X 1C7</b>	

Credits Requested per Each Claim in Columns at right

Mining Claims Traversed (List in numerical sequence)

Special Provisions	Geophysical	Days per Claim
For first survey: Enter 40 days. (This includes line cutting)	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
For each additional survey: using the same grid: Enter 20 days (for each)	Geological	
	Geochemical	
	Geophysical	
	Geological	
Man Days Complete reverse side and enter total(s) here	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
Airborne Credits Note: Special provisions credits do not apply to Airborne Surveys.	Electromagnetic	30
	Magnetometer	30
	VLF-EM	20*
	Radiometric	

Mining Claim		Expend. Days Cr.	Mining Claim		Expend. Days Cr.
Prefix	Number		Prefix	Number	
SSM	779423				
	779424				
	779425				
	779426				
	779427				
	779428				
	779430				
	779431				
	779432				
	779433				
	779434				

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MINING LANDS SECTION

Expenditures (excludes power stripping)

Type of Work Performed

Performed on Claim(s)

Calculation of Expenditure Days Credits

Total Expenditures \$  + 15 =

Total Days Credits

Instructions  
Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected in columns at right.

For Office Use Only

Total Days Cr. Recorded	Date Recorded	ACTING Mining Recorder
880	July 30/84	G. A. Kurylo
	Day Approved as Recorded	Branch Director
	Sept 4/84	[Signature]

Total number of mining claims covered by this report of work.

Date **27 JULY 84**

Recorded by (Holder or Agent) (Signature)

Certification Verifying Report of Work

I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.

Name and Postal Address of Person Certifying  
**Mel de Quadros Box 2028 Wawa Ont P0S 1K0**

Date Certified **27 JULY 84**

Certified by (Signature)



MANWA EXPLORATION SERVICES LTD.

'SCHEDULE'

A. MEATH TWP.

- SSM 704491
- 704492
- 704493
- 704494
- 704495
- 704496
- 704497
- 704498
- 704499 X

B. RENNIE TWP.

- SSM 704487
- SSM 704488
- 704489
- 704490 X
- 704410
- 704411 X
- 704414
- 704415
- 704416
- 704417
- 704418
- 704419
- 704420
- 704421
- 704422
- 704423
- 704424
- 704425
- 704426
- 704427
- 704428 X

- SSM 707166
- 707167
- 707168
- 707169
- 707170
- 707171
- 707172
- 707173
- 707174
- 707175
- 707176
- 707177 X
- 707117
- 707118
- 707119
- 707120
- 707121
- 707122
- 707123
- 707124
- 707125 X

MANWA EXPLORATION SERVICES LTD.

SCHEDULE

B. RENNIE TWP (CONT)

SSM 707126  
707127  
707128 \

~~707217~~ 707217

707218  
707219  
707220  
707221  
707222  
707223  
707224  
707225  
707226  
707227  
707228.

C. STOVER TWP.

SSM 707098  
707099

SSM 707158  
707159  
707160  
707161  
707162  
707163  
707164  
707165 !

C. STOVER TWP

SSM 407092  
 707093  
 707094  
 707095  
 707096  
 707097 \

SSM 609287  
 609288  
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 609292  
 609293 \

SSM ~~707129~~  
~~707130~~ ~~rel~~  
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 707137 \

609296 \ :  
 637786 \ /  
~~591207~~ ~~rel~~  
~~591208~~  
~~641794~~  
~~641795~~ ~~rel~~

SSM 407081  
 707082  
 707083  
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 707088  
 707089  
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 707091 \

401179  
 407180  
 707181  
 707182  
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 707188  
 707189 |

SSM 466903  
 766904 |

407197 \ /  
 407079 \ /  
 707080 \ /

C. STOVER TWP (cont)

SSM 707190  
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 707192  
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 707196 \

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Field Office,  
Box 2028,  
Manwa, Ontario P0S 1K0  
13<sup>th</sup> July 1984.

The Mining Recorder,  
South St. Marie Mining Division,  
Box 669, 875 Queen St. East,  
South St. Marie, Ont. P6A 5H2

Dear Mrs. St. Jules,

Enclosed are two reports of work for claims in Stora Township.  
These claims belong to Mr. G. Paquette and Mr. P.J. McGowan, though  
they may not yet have been transferred.

The airborne work, which I am sending today to Toronto,  
forms a part of the large block of claims in the Stora, Meath  
and Benzie Townships which belong to Mr. McGowan and which  
are presently under extension.

Yours sincerely,



Mel de Quadros.



1984 07 24

Your File:  
Our File: 2.6953

Mrs. M.V. St. Jules  
Mining Recorder  
Ministry of Natural Resources  
875 Queen Street East  
P.O. Box 669  
Sault Ste. Marie, Ontario  
P6A 5N2

Dear Madam:

We have received reports and maps for an Airborne Geophysical (Electromagnetic & Magnetometer) Survey submitted on Mining Claims SSM 707092 et al in the Townships of Stover, Rennie and Meath.

This material will be examined and assessed and a statement of assessment work credits will be issued.

We do not have a copy of the report of work which is normally filed with you prior to the submission of this technical data. Please forward a copy as soon as possible.

Yours sincerely,

S.E. Yundt  
Director  
Land Management Branch

Whitney Block, Room 6643  
Queen's Park  
Toronto, Ontario  
M7A 1W3  
Phono: (416)965-6918

S. Hurst:sc

cc: R.J. McGowan/G. Paquette  
370 - 625 Howe Street  
Vancouver, B.c.  
V6C 2T6

cc: Dighem Limited  
29 Silverton Avenue  
Downsview, Ontario

MANWA EXPLORATION SERVICES LTD.

<b>RECEIVED</b>	
Land Management Branch	
CIRCULATE <input type="checkbox"/>	
COMMENTS PLEASE <input type="checkbox"/>	
BY	
JUL 31 1984	
W. L. GOOD ✓	

FIELD OFFICE,  
Box 2028,  
Wawa, Ontario P0S1K0  
27 JULY 1984

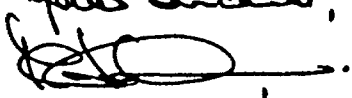
The Director,  
Land Management Branch,  
Whitney Block, Room 6450,  
Queen's Park, Toronto M7A 1W3

Dear Sir,  
Attention Mr. Denis Kinwig,

Further to our conversation today regarding my error in filing for airborne credits for Airborne work on the claims of R.S. McGowan in the Stover, Rennie and Meath Townships, please find enclosed new technical data statements to replace the two sent with the survey to you approximately two weeks ago.

I am also enclosing the amended reports of claims for 12 additional claims added to the survey and the earlier reports of work, which bear file numbers from the Land & Marine Division in hope these will help you trace the reports.

Also enclosed are two copies of the GM Survey that should form the third survey and should have been included in the reports I sent you.

Yours Sincerely,  
  
Mel de Quadros.

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JUL 31 1984  
MINING LANDS SECTION

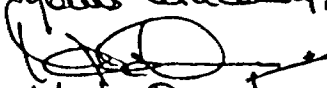
MANWA EXPLORATION SERVICES LTD.

Field Office,  
Box 2028,  
Wawa, Ontario P0S 1K0  
27th July 1984

Mrs. M. V. St. Jules,  
The Mining Recorder,  
P.O. Box 669-675 Queen Street East,  
Sault Ste. Marie Ontario P6A 2B3  
Dear Mrs. St. Jules,

I regret to inform you that yet again I have erred in filing a report of work, and I am enclosing two reports of work forms (amended) to replace previously sent ones (copies of which are also attached).

The reason for the amendments is that we actually flew three surveys - mag, EM and VLF-EM and not just the two that I claimed for. I am also informing Mr. Denis Kinwig at Lands Management regarding the error.

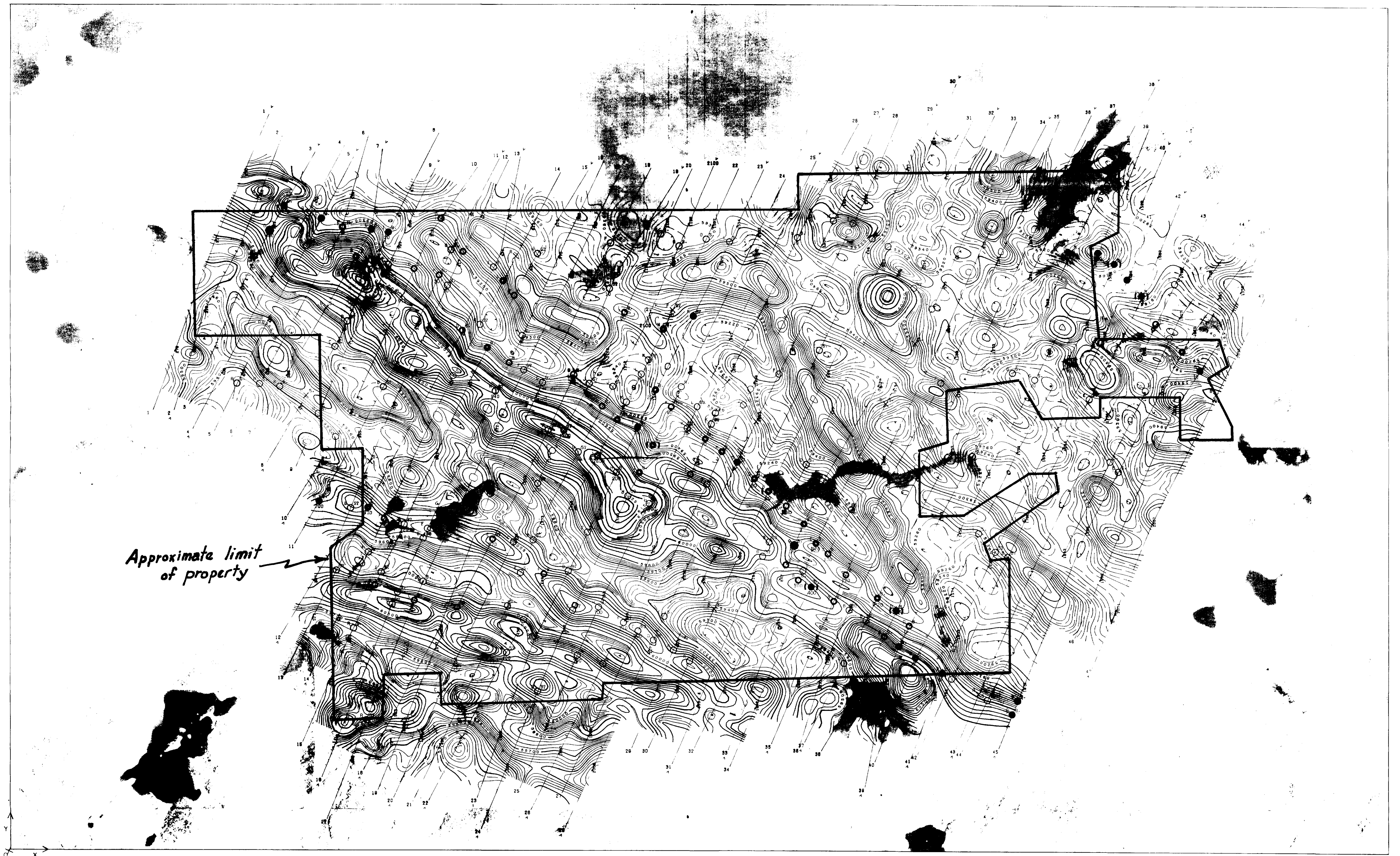
Mans Lucandy,  
  
Mel de Quadros.

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MINING LINES SECTION

• FOR ADDITIONAL  
INFORMATION

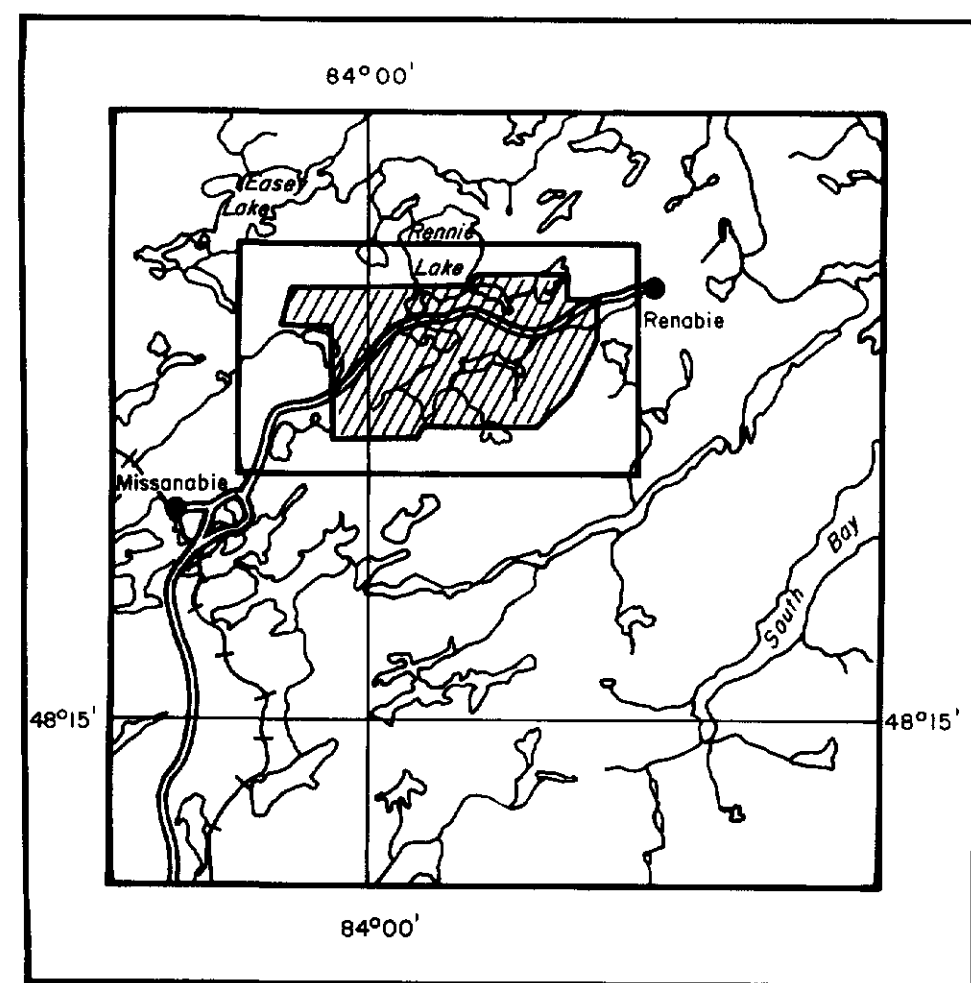
SEE MAPS:

STOVER-0026 # 1-3

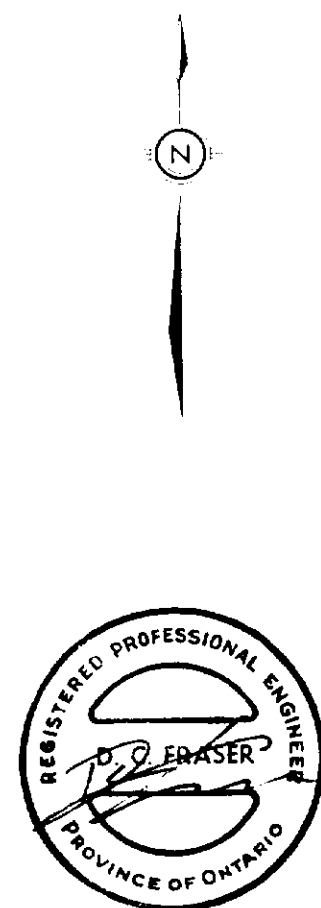


Approximate limit  
of property

LOCATION MAP



SCALE 1:250,000

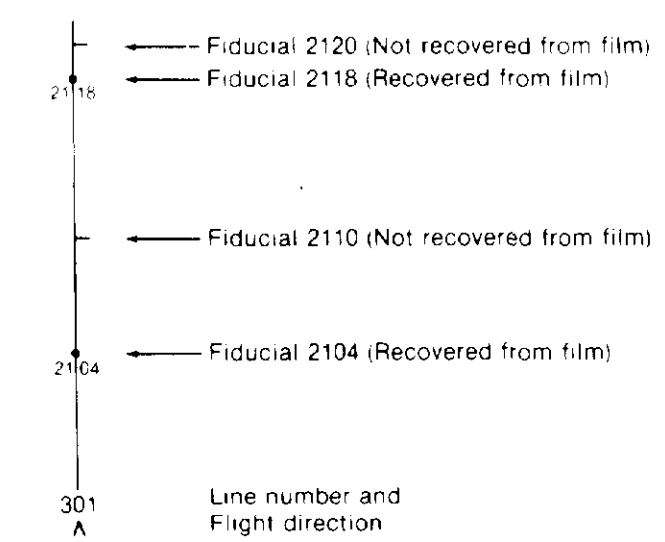


**DIGHEM<sup>III</sup> SURVEY**  
**RENNIE LAKE AREA, ONTARIO**  
**TOTAL FIELD MAGNETICS**  
**FOR**  
**ROBERT J. MCGOWAN**

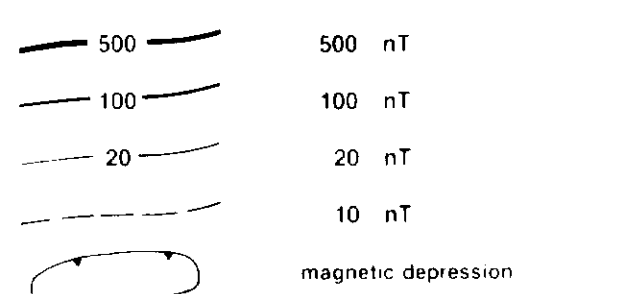
Scale 1:15,840



Flight Line



ISOMAGNETIC LINES  
(total field)

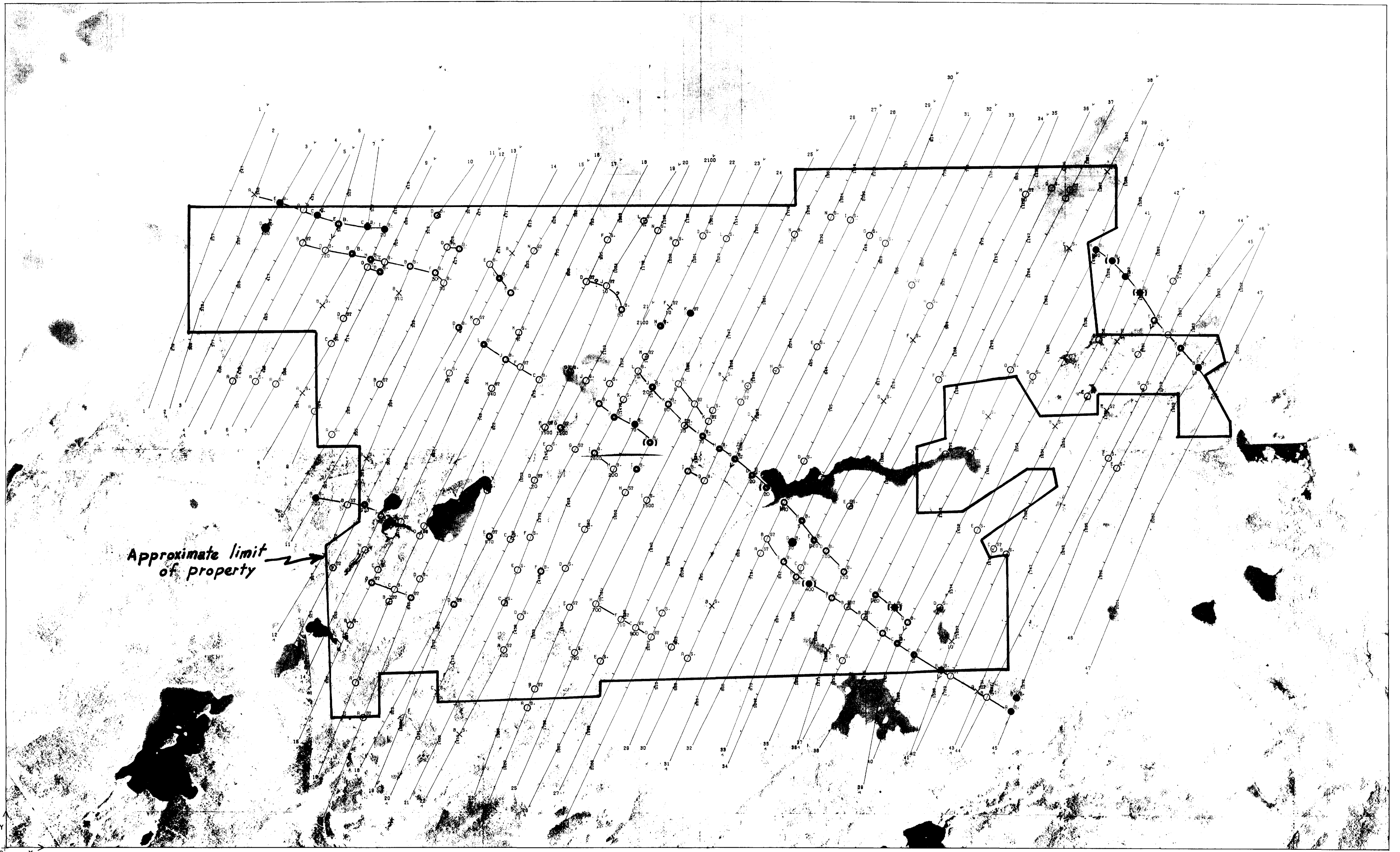


Magnetic Inclination within the survey area /6°

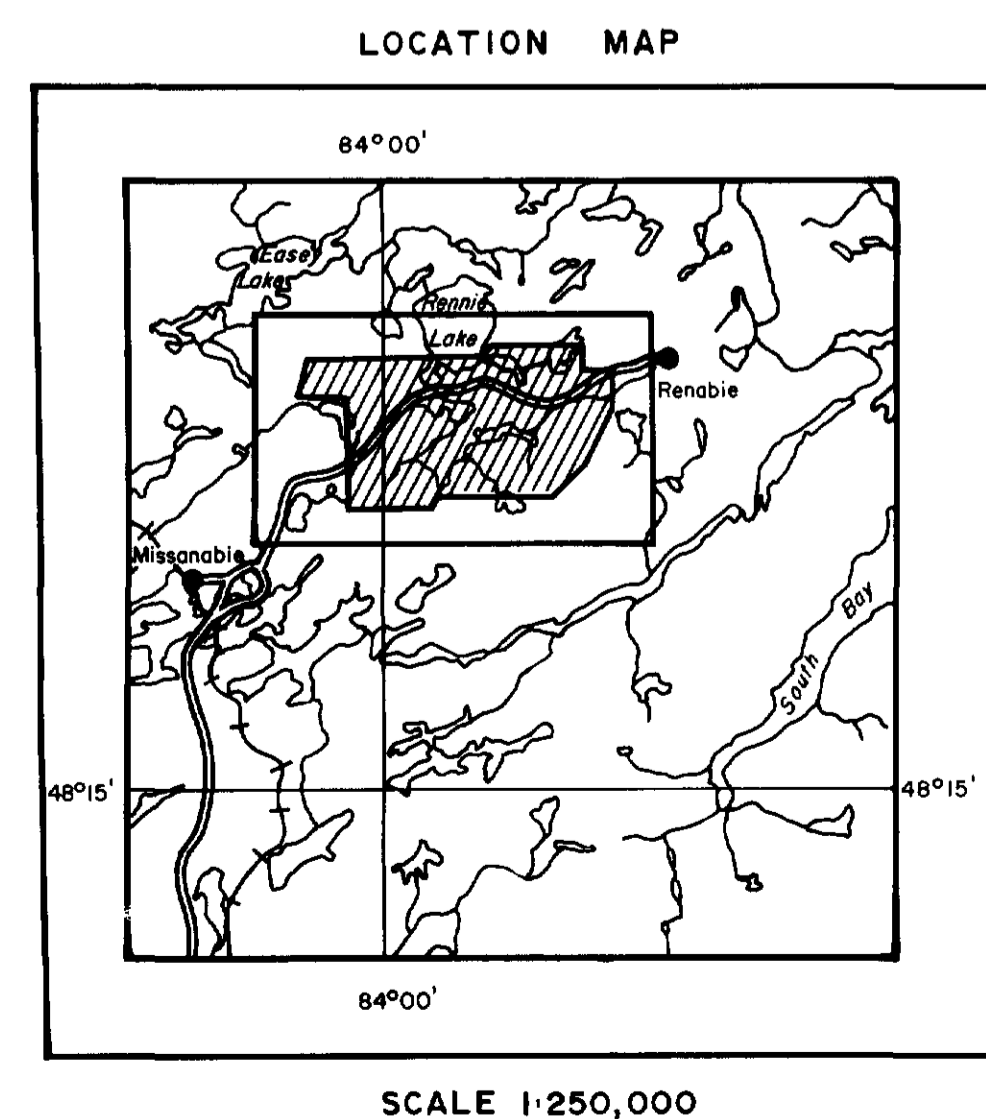
STOVER-0026, #1



JOB 201	DATE MAY, 84	DRAWN BY D.R.	CHECKED BY J.S.
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Approximate limit of property



# DIGHEM<sup>III</sup> SURVEY

## RENNIE LAKE AREA, ONTARIO

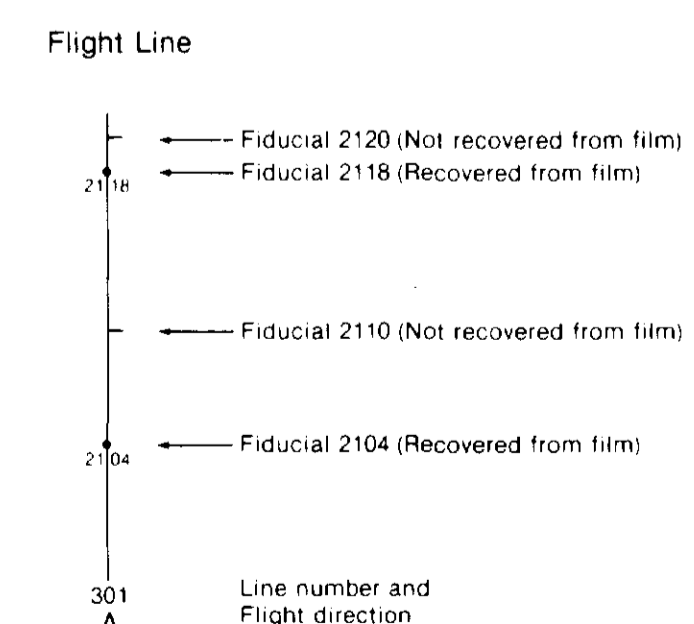
### ELECTROMAGNETIC ANOMALIES

FOR

### ROBERT J. MCGOWAN

Scale 1:15,840

1/2 0 1/2 1 Miles



ANOMALY GRADE	EM GRADE	CONDUCTANCE RANGE (MHOS)	Interpretive symbol
6	●	90-99	●
5	●	50-99	●
4	●	20-49	●
3	●	10-19	●
2	○	5-9	○
1	○	5	○
	×	Indeterminate	×

anomaly name	Interpretive symbol	Interpretive Conductor ("model")
Depth is greater than	●	B. Bedrock conductor
15 m	○	S. Conductive cover ("horizontal thin sheet")
30 m	○	H. Broad conductive rock unit, deep conductive weathering, thick conductive cover ("half space")
45 m	○	E. Edge of broad conductor ("edge of half space")
60 m	○	L. Culture, e.g. power line, building, fence

Symbol	Interpretation
—	dip direction
—	magnetic correlation in nT (gammas)
—	conductor axis
—	flight line

26953 dup  
2.6953 dup.

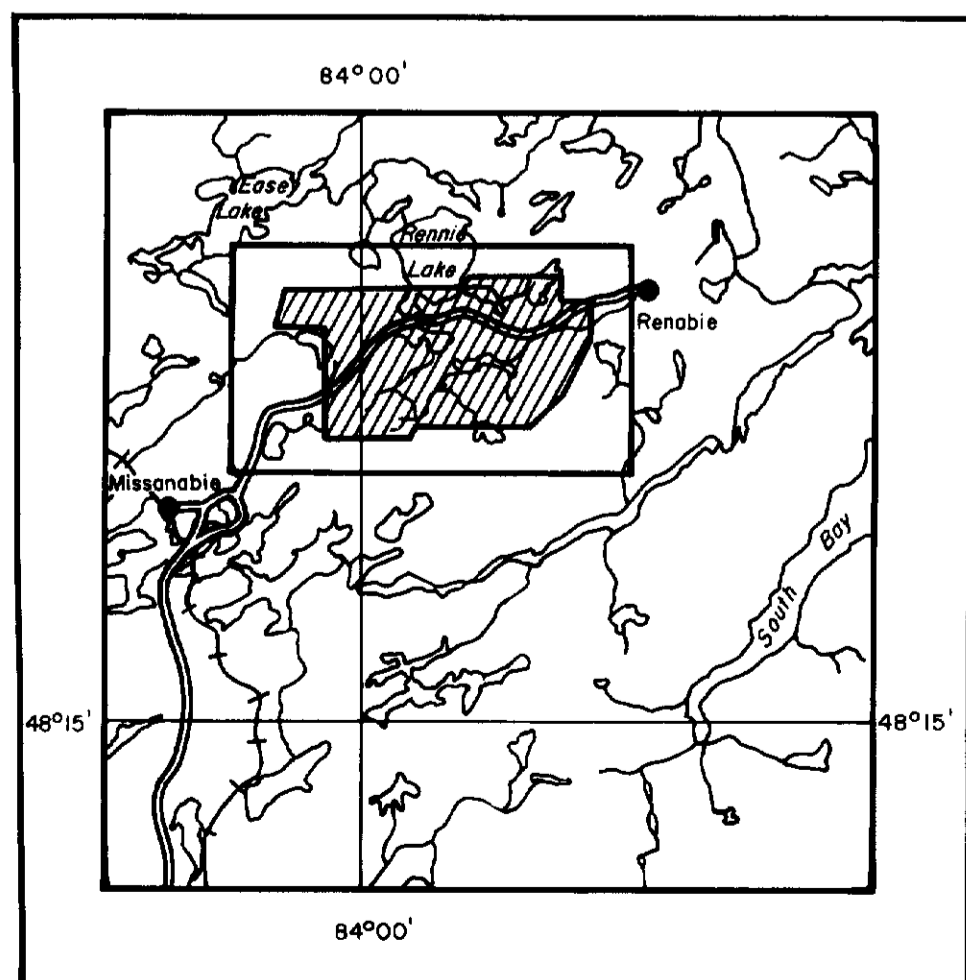
STOVER-0026.#2

JOB	DATE	DRAWN BY	CHECKED BY
201	MAY, 84	SR	JD





LOCATION MAP



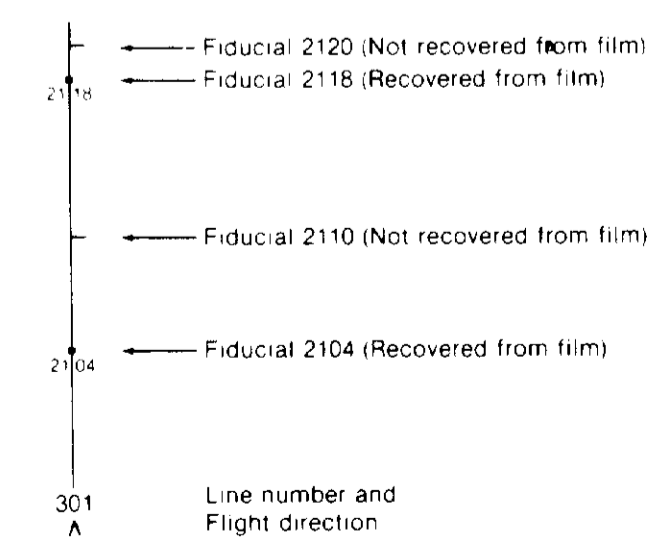
SCALE 1:250,000



**DIGHEM<sup>III</sup> SURVEY**  
**RENNIE LAKE AREA, ONTARIO**  
**FILTERED TOTAL VLF EM FIELD**  
**FOR**  
**ROBERT J. MCGOWAN**

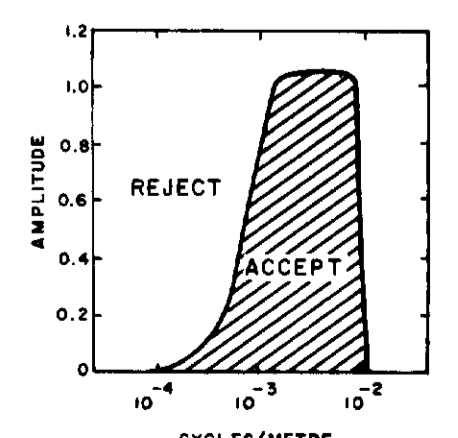
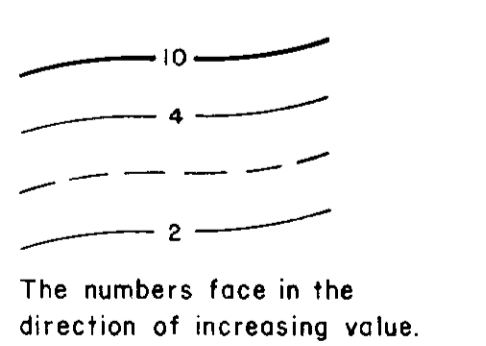
Scale 1:15,840  
 1/2 0 1/2 1 Miles

Flight Line



LEGEND

Contours in percent



Frequency response of VLF-EM filter  
 Tx: NSS ANNAPOLIS, Md.  
 f = 21.4 kHz

STOVER-0026, #3.

