## UNIT-5

## PART-A (2 MARKS)

## THIN CYLINDERS, SPHERES AND THICK CYLINDERS

1) How does a thin cylinder fail due to internal fluid pressure?
(May / June 2017)
Thin cylinder failure due to internal fluid pressure by the formation of circumferential stress and longitudinal stress.
2) Name the stress develops in the cylinder. [NOV/DEC 2016]

The stresses developed in the cylinders are:

1. Hoop or circumferential stresses.
2. Longitudinal stresses
3. Radial stresses
3) Define radial pressure in thin cylinder. [NOV/DEC 2016]

The internal pressure which is acting radially inside the thin cylinder is known as radial pressure in thin cylinder.
4)Differentiate between thin and thick cylinders [MAY/JUNE 2016] [APR/MAY 2015](Nov/Dec 2018) (Apr/May 2019)

| S.No | Thin | Thick |
| :---: | :--- | :--- |
| 1 | Ratio of wall thickness to the <br> diagram of cylinder is less than <br> $1 / 20$. | Ratio of wall thickness to the <br> diagram of cylinder is more than <br> $1 / 20$ |
|  | Hoop stress is assumed to be <br> constant throughout the wall <br> thickness. | Hoop stress varies from inner to <br> outer wall thickness. |

5) Describe the lame's theorem: [MAY/JUNE 2016][NOV/DEC 2014] [MAY/JUNE 2017] (Apr/May 2018)
(Apr/May 2019)
Ratio stress, $\sigma_{r}=\mathrm{b} / \mathrm{r}^{2}-\mathrm{a}$
Hoop stress, $\sigma_{c}=\mathrm{b} / \mathrm{r}^{2}+\mathrm{a}$
6) State the expression for max shear stress in a cylinder shell [NOV/DEC 2015]

In a cylindrical shell, at any point on it circumference there is a set of two mutually perpendicular stresses $\sigma_{c} \sigma_{\gamma}$ which are principal stresses and as such the planes in which these act are the principal planes.
$\tau_{\max }=\frac{\sigma_{\mathrm{c}}-\sigma_{\gamma}}{2}=\frac{\frac{\mathrm{pd}}{2 \mathrm{t}}-\frac{\mathrm{pd}}{4 \mathrm{t}}}{2}=\frac{\mathrm{pd}}{8 \mathrm{t}}$

$$
\tau_{\max }=\frac{\mathrm{pd}}{8 \mathrm{t}}
$$

7) Define-hoop stress \& longitudinal stress
[NOV/DEC 2015](Apr/May 2018)

## (i) Hoop stress: $\left(\boldsymbol{\sigma}_{\mathrm{c}}\right)$

These act in a tangential dirn, to the circumference of the shell.

$$
\sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}
$$

## (ii) Longitudinal stress: $\left(\boldsymbol{\sigma}_{\boldsymbol{t}}\right)$

The stress in the longitudinal direct due to tendency of busting the cylinder along the transverse place is called longitudinal stress

$$
\sigma_{1}=\frac{\mathrm{pd}}{4 \mathrm{t}}
$$



## 8) State the assumption made in lame's theorem for thick cylinder analysis. [APR/MAY 2015] [NOV/DEC 2017] [NOV/DEC 2018]

1. The material is homogeneous and Isotropic.
2. The material is stressed within elastic limit.
3. All the fibers of the material are to expand (or) contract independently without being constrained by the adjacent fibers.
4. Plane section perpendicular to the longitudinal axis of the cylinder remain plane after the application of internal pressure.

## 9) What is meant by circumferential stress?

[NOV/DEC 2014]
The stress in the circumferential direction in due to tendency of bursting the cylinder along the longitudinal axis is called circumferential stress (or) hoop stress.

$$
\sigma_{c}=\frac{\mathrm{pd}}{2 \mathrm{t}}
$$

10) A storage tank of internal diameter 280 mm is subjected to an internal pressure of 2.56 MPa . Find the thickness of the tank. If the hoop \& longtudital stress are 75 MPa and $\mathbf{4 5} \mathrm{MPa}$ respectively

$$
\begin{aligned}
& \sigma_{\mathrm{c}}=75 \mathrm{MPa}, \quad \sigma_{1}=45 \mathrm{MPa}, \mathrm{~d}=280 \mathrm{~mm}, \mathrm{p}=2.5 \mathrm{MPa} \\
& \sigma_{\mathrm{c}}>\sigma_{1} \Rightarrow \text { use } \sigma_{\mathrm{c}} \\
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}} \\
& \mathrm{t}
\end{aligned}=\frac{\mathrm{pd}}{2 \sigma_{\mathrm{c}}}=\frac{2.5 \times 280}{2 \times 75} .
$$

11) A spherical shell of 1 m internal diameter undergoes a diameter strain of $10^{-4}$ due to internal pressure. What is the corresponding change in volume?

$$
\begin{aligned}
\delta \mathrm{V} & =\mathrm{e}_{\mathrm{v}} \times \mathrm{V} \\
& =3 \times \mathrm{e} \times \mathrm{V}=3 \times 10^{-4} \times \frac{\pi}{6} \times(1000)^{3} \\
\delta \mathrm{~V} & =157.079 \mathrm{~mm}^{3}
\end{aligned}
$$

12) A thin cylindrical closed at both ends is subjected to an internal pressure of 2 MPa . Internal diameter is 1 m and the wall thickness is 10 mm . What is the maximum shear stress in the cylinder material?

$$
\begin{aligned}
& \mathrm{p}=2 \mathrm{mPa}=\frac{2 \mathrm{~N}}{\mathrm{~mm}^{2}} \quad \mathrm{~d}=1 \mathrm{~m}=100 \mathrm{~mm} \mathrm{t}=10 \mathrm{~mm} \\
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{2 \times 1000}{2 \times 10}=100 \mathrm{~N} / \mathrm{mm}^{2} \\
& \sigma_{1}=\frac{\mathrm{pd}}{4 \mathrm{t}}=\frac{2 \times 1000}{4 \times 10}=50 \mathrm{~N} / \mathrm{mm}^{2} \\
& \tau_{\max }=\frac{\sigma_{\mathrm{c}}-\sigma_{1}}{2}=\frac{100-50}{2}=\frac{50}{2} \\
& \tau_{\max }=25 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

13) Find the thickness of the pipe due to an internal pressure of $10 \mathrm{~N} / \mathrm{mm}^{2}$ if the permissible stress is 120 $\mathrm{N} / \mathrm{mm}^{2}$ and the diameter of the pipe is $\mathbf{7 5 0} \mathbf{~ m m}$

$$
\mathrm{p}=10 \mathrm{~N} / \mathrm{mm}^{2}, \sigma_{\mathrm{c}}=120 \mathrm{~N} / \mathrm{mm}^{2}, \mathrm{~d}=750 \mathrm{~mm}
$$

$$
\begin{aligned}
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}} \\
& \mathrm{t}=\frac{\mathrm{pd}}{2 \sigma_{\mathrm{c}}}=\frac{10 \times 750}{2 \times 120}=31.25 \mathrm{~mm}
\end{aligned}
$$

14) A spherical shell of 1 m diameter is subjected to an internal pressure $0.5 \mathrm{~N} / \mathrm{mm}^{2}$. Find the thickness if the allowable stress in the material of the shell is $75 \mathrm{~N} / \mathrm{mm}^{2}$.

$$
\begin{aligned}
\mathrm{d}=1 \mathrm{~m}= & 1000 \mathrm{~mm}, \quad \mathrm{p}=0.5 \mathrm{~N} / \mathrm{mm}^{2} \quad \sigma_{\mathrm{c}}=75 \mathrm{~N} / \mathrm{mm}^{2} \\
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{4 \mathrm{t}} \\
\mathrm{t} & =\frac{\mathrm{pd}}{4 \sigma_{\mathrm{c}}} \\
= & \frac{0.5 \times 1000}{4 \times 75}=1.67 \mathrm{~mm}
\end{aligned}
$$

## 15) Define thick cylinder

When the ratio of thickness ( t ) to internal diameter of cylinder is more than $1 / 20$ then the cylinder is known as thick cylinder

## 16) In a thick cylinder will the radial stress is vary over the thickness of wall?

Yes, in thick cylinder radial stress is maximum at inner and minimum at the outer radius.
17) Define thin cylinder. (Nov/Dec 2017)

If the thickness of wall of the cylinder vessel is less than $1 / 15$ to $1 / 20$ of its internal diameter, the cylinder vessels is known as thin cylinder.

## 18) In a thin cylinder will the radial stress over the thickness of wall?

No, In the cylinder radial stress developed in its wall is assumed to be constant since the wall thickness is very small as compared to the diameter of cylinder
19) What is the ratio of circumference stress to longitudinal stress of a thin cylinder?

The ratio of circumferential stress to longitudinal stress of a thin cylinder is two.
20) Distinguish between cylinder shell and spherical shell.

| S.No. | Cylindrical shell | Spherical shell |
| :--- | :--- | :--- |
| 1. | Circumferencial stress is twice the longitudinal stress | Only hoop stress presents |
| 2. | It withstands low pressure than spherical shell for the same <br> diameter | It withstand more pressure than <br> cylinder shell for the same <br> diameter |

## 21) What is the effect of riveting a thin cylinder shell?

Riveting reduce the area offering the resistance. Due to this, the circumferential and longitudinal stresses are more. It reduces the pressure carrying capacity of the shell.

## PART-B

1) A cylindrical thin drum 80 cm in diameter and 3 m long has a shell thickness of 1 cm . If the drum is subjected to an internal pressure of $2.5 \mathrm{~N} / \mathrm{mm}^{2}$, determine (i) change in diameter (ii) change in length and (iii) change in volume $E=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poisons ratio $=0.25$
(Apr/May 2019)
$\mathrm{d}=80 \mathrm{~cm}$
$\mathrm{L}=3 \mathrm{~m}=300 \mathrm{~cm}$
$\mathrm{t}=1 \mathrm{~cm}$
$\mathrm{p}=250 \mathrm{~N} / \mathrm{cm}^{2}$
$\mathrm{E}=2 \times 10^{7} \mathrm{~N} / \mathrm{cm}^{2}$
$\mu=0.25$
Change in diameter ( $\delta \mathbf{d}$ )

$$
\begin{aligned}
\delta \mathrm{d} & =\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{\mu}{2}\right] \\
& =\frac{250 \times 80^{2}}{2 \times 1 \times 2 \times 10^{7}}\left[1-\frac{0.25}{2}\right] \\
& \delta \mathrm{d}=0.35 \mathrm{~cm}
\end{aligned}
$$

Change in length ( $\delta \boldsymbol{\delta}$ )

$$
\begin{aligned}
\delta \ell & =\frac{\mathrm{pdL}}{2 \mathrm{tE}}\left[\frac{1}{2}-\mu\right] \\
& =\frac{250 \times 80 \times 300}{2 \times 1 \times 2 \times 10^{7}}[0.5-0.25] \\
\delta \ell & =0.0375 \mathrm{~cm}
\end{aligned}
$$

Change in volume ( $\delta \mathbf{v}$ )
$\frac{\delta \mathrm{V}}{\mathrm{V}}=2 \frac{\delta \mathrm{~d}}{\mathrm{~d}}+\frac{\delta \mathrm{l}}{\mathrm{l}}$
$\frac{\delta \mathrm{V}}{\mathrm{V}}=2 \frac{0.035}{80}+\frac{0.0375}{300}=0.001$
original volume, $\mathrm{V}=\frac{\pi}{4} \mathrm{~d}^{2} \times \ell=\frac{\pi}{4} \times 80^{2} \times 300$

$$
\mathrm{V}=1507964.473 \mathrm{~cm}^{3}
$$

$\delta \mathrm{V}=0.001 \times \mathrm{V}=0.001 \times 1507964.473=1507.96 \mathrm{~cm}^{3}$
2) A spherical shell of internal diameter 0.9 m and of thickness 10 mm is subjected to an internal pressure of $1.4 \mathrm{~N} / \mathrm{mm}^{2}$. Determine the increase in diameter and increase in volume.
$\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poissons ratio=1/3 (Apr/May 2019)
$d=0.9 \mathrm{~m}=900 \mathrm{~mm}$
$\mathrm{t}=10 \mathrm{~mm}$
$\mathrm{p}=1.4 \mathrm{~N} / \mathrm{mm}^{2}$
$\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
$\mu=\frac{1}{3}$

Change in diameter: ( $\mathbf{\delta d}$ )
$\delta \mathrm{d}=\frac{\mathrm{pd}^{2}}{4 \mathrm{tE}}\left[1-\frac{1}{\mathrm{~m}}\right]$
$=\frac{1.4 \times 900^{2}}{4 \times 10 \times 2 \times 10^{5}}\left[1-\frac{1}{3}\right]$
$\delta \mathrm{d}=0.0945 \mathrm{~mm}$

Change in volume ( $\boldsymbol{\delta v}$ )
$e_{v}=3 x \frac{\delta d}{d}=3 \times \frac{0.0945}{900}=315 \times 10^{-6}$
$\frac{\delta \mathrm{V}}{\mathrm{V}}=315 \times 10^{-6}$
$\mathrm{V}=\left(\frac{\pi}{6}\right) \mathrm{xd}^{3}=\left(\frac{\pi}{6}\right) \times 900^{3}$
$\delta \mathrm{V}=12028.5 \mathrm{~mm}^{3}$
3) A boiler shell is to be made of 15 mm thick plate having tensile stress of $120 \mathrm{~N} / \mathrm{mm}^{2}$ If the efficiencies of the longitudinal and circumferential joints are $\mathbf{7 0 \%}$ and $30 \%$. Determine the maximum permissible diameter of the shell for an internal pressure of $2 \mathrm{~N} / \mathrm{mm}^{2}$ (Nov/Dec 2018)

Maximum diameter of circumference stress

$$
\begin{aligned}
\sigma_{\mathrm{c}} & =\frac{\mathrm{pd}}{2 \mathrm{t} \eta_{\mathrm{l}}} \\
120 & =\frac{2 \times \mathrm{d}}{2 \times 15 \times 0.7} \\
\mathrm{~d} & =\frac{120 \times 2 \times 15 \times 0.7}{2} \\
\mathrm{~d} & =1260 \mathrm{~mm}
\end{aligned}
$$

Maximum diameter for longitudinal stress

$$
\begin{aligned}
\sigma_{1} & =\frac{\mathrm{pd}}{4 \mathrm{t} \times \eta_{\mathrm{c}}} \\
120 & =\frac{2 \times \mathrm{d}}{4 \times 15 \times 0.3} \\
\mathrm{~d} & =\frac{120 \times 4 \times 15 \times 0.3}{2} \\
\mathrm{~d} & =1080 \mathrm{~mm}
\end{aligned}
$$

4) A thin cylindrical shell with following dimensions is filled with a liquid at atmospheric pressure. Length $=1.2 \mathrm{~m}$, external diameter $=20 \mathrm{~cm}$, thickness of metal $=8 \mathrm{~mm}$, Find the value of the pressure exerted by the liquid on the walls of the cylinder and the hoop stress induced if an additional volume of $25 \mathrm{~cm}^{3}$ of liquid is pumped into the cylinder. Take $\mathrm{E}=2.1 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poisons ratio= 0.33 (Nov/Dec 2018)
$L=1.2 \mathrm{~m}=1200 \mathrm{~mm}$
$D=20 \mathrm{~cm}=200 \mathrm{~mm}$
$t=8 \mathrm{~mm}$
$d=D-2 t=184 m m$
$\delta V=25 \mathrm{~cm}^{3}=25000 \mathrm{~mm}^{3}$
$E=2.1 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
$\mu=0.33$

Volume, $\mathrm{V}=\frac{\pi}{4} \times \mathrm{d}^{2} \times \ell$

$$
\begin{aligned}
& =\frac{3.14}{4} \times 184^{2} \times 1200 \\
& =31908528 \mathrm{~mm}^{3}
\end{aligned}
$$

$\delta \mathrm{V}=\mathrm{V} \times \frac{\mathrm{pd}}{2 \mathrm{tE}}\left(\frac{5}{2}-\frac{2}{\mathrm{~m}}\right)$
$25000=31908528 \times \frac{\mathrm{p} \times 184}{2 \times 8 \times 2.1 \times 10^{5}}\left[\frac{5}{2}-2(0.33)\right]$
$\mathrm{p}=7.7 \mathrm{~N} / \mathrm{mm}^{2}$
$\sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{7.7 \times 184}{2 \times 8}=89.42 \mathrm{~N} / \mathrm{mm}^{2}$
5) A cylindrical shell 3 m long which is closed at the ends has an internal diameter of 1.5 m and a wall thickness of 20 mm . Calculate the circumferential and longitudinal stresses induced and also change in the dimensions of the steel. If it is subjected to an internal pressure of $1.5 \mathrm{~N} / \mathrm{mm}^{2}$ Take $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poisons ratio=0.3 (Apr/May 2018)
$l=3 m=3000 \mathrm{~mm}$
$t=20 \mathrm{~mm}$
$d=1.5 \mathrm{~m}=1500 \mathrm{~mm}$
$p=1.5 \mathrm{~N} / \mathrm{mm}^{2}$
$E=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
$\mu=0.3$

Hoop stress, $\sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{1.5 \times 1500}{2 \times 20}=56.25$
$\sigma_{\mathrm{c}}=56.25 \mathrm{~N} / \mathrm{mm}^{2}$

Longitudinal stress, $\sigma_{\ell}=\frac{\mathrm{pd}}{4 \mathrm{t}}=\frac{1.5 \times 1500}{4 \times 20}=28.125$
$\sigma_{\ell}=28.125 \mathrm{~N} / \mathrm{mm}^{2}$

Change in diameter ( $\delta \mathrm{d}$ )

$$
\begin{aligned}
\delta \mathrm{d} & =\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{\mu}{2}\right] \\
& =\frac{1.5 \times 1500^{2}}{2 \times 20 \times 200 \times 10^{3}}\left[1-\frac{0.3}{2}\right] \\
& \delta \mathrm{d}=0.7225 \mathrm{~mm}
\end{aligned}
$$

Change in length ( $\delta \ell$ )

$$
\begin{aligned}
\delta \ell & =\frac{\mathrm{pdL}}{2 \mathrm{tE}}\left[\frac{1}{2}-\mu\right] \\
& =\frac{1.5 \times 1500 \times 3000}{2 \times 20 \times 200 \times 10^{3}} \quad[0.5-0.3] \\
\delta \ell & =0.16875 \mathrm{~mm}
\end{aligned}
$$

Change in volume ( $\delta \mathbf{v}$ )

$$
\frac{\delta \mathrm{V}}{\mathrm{~V}}=\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right]
$$

original volume, $V=\frac{\pi}{4} \mathrm{~d}^{2} \times \ell=\frac{\pi}{4} \times 1500^{2} \times 3000$

$$
\begin{aligned}
& \mathrm{V}=5301437603 \mathrm{~mm}^{3} \\
& \delta \mathrm{~V}=\frac{1.5 \times 1500 \times 5301437603}{2 \times 20 \times 200 \times 10^{3}}\left[\frac{5}{2}-2 \times 0.3\right] \\
& \delta \mathrm{V}=2832955.72 \mathrm{~mm}^{3}
\end{aligned}
$$

6) A compound cylinder formed by shrinking one tube to another is subjected to an internal pressure of $90 \mathrm{MN} / \mathrm{m}^{2}$. Before the fluid is admitted, the internal and external diameter of the compound cylinders are 180 mm and 300 mm respectively and the diameter at the junction is $\mathbf{2 4 0} \mathbf{m m}$. If after shrinking on, the radial pressure at the common surface is $12 \mathrm{MN} / \mathrm{m}^{2}$. Determine the final stresses developed in the compound cylinder (Apr/May 2018)

Solution. Internal pressure in the cylinder,

$$
p_{1}=90 \mathrm{MN} / \mathrm{m}^{2}
$$

Internal radius of the cylinder, $r_{1}=\frac{180}{2}=90 \mathrm{~mm}=0.09 \mathrm{~m}$
External radius of the cylinder, $r_{3}=\frac{300}{2}=150 \mathrm{~mm}=0.15 \mathrm{~m}$
Radius at the junction, $\quad r_{2}=\frac{240}{2}=120 \mathrm{~mm}=0.12 \mathrm{~m}$
Radial pressure at the common surface after shrinking on,

$$
p=12 \mathrm{MN} / \mathrm{m}^{2}
$$

## Final stresses developed:

Let the Lame's equations be:
For inner tube:

$$
\sigma_{r}=\frac{b}{r^{2}}-a
$$

and,

$$
\sigma_{c}=\frac{b}{r^{2}}+a
$$

For outer tube:

$$
\sigma_{r}=\frac{b^{\prime}}{r^{2}}-a^{\prime}
$$

and,

$$
\sigma_{c}=\frac{b^{\prime}}{r^{2}}+a^{\prime}
$$

meter tube:
Ah
$\therefore \quad 123.456 b-a=0$
of,
Ah

$$
\frac{b}{0.0081}-a=0
$$

A.

$$
\begin{equation*}
r=r_{2}=0.12 \mathrm{~m}, \tag{i}
\end{equation*}
$$

$$
\sigma_{r}=12 \mathrm{MN} / \mathrm{m}^{2}
$$

$$
\frac{b}{0.0144}-a=12
$$

$$
\begin{equation*}
69.44 b-a=12 \tag{ii}
\end{equation*}
$$

From ens. (i) and (ii), we get

$$
b=-0.222 \text { and } a=-27.41
$$

Hence circumferential stress at any point in the inner tube will be given by

$$
\sigma_{c}=-\frac{0.222}{r^{2}}-27.41
$$

The minus sign indicates that the stress will be wholly compressive.
At,

$$
r=r_{1}=0.09 \mathrm{~m}
$$

$$
\sigma_{c(0.09)}=-\frac{0.222}{0.09^{2}}-27.41=54.82 \mathrm{MN} / \mathrm{m}^{2} \text { (comp.) }
$$

At,

$$
r=0.12 \mathrm{~m},
$$

$$
\sigma_{c(0.12)}=-\frac{0.222}{0.12^{2}}-27.41=42.82 \mathrm{MN} / \mathrm{m}^{2} \text { (comp.) }
$$

Outer tube:
At,

$$
\begin{align*}
r & =0.15 \mathrm{~m}, \sigma_{r}=0 \\
\frac{b^{\prime}}{0.15^{2}}-a^{\prime} & =0 \tag{iii}
\end{align*}
$$

$\therefore$
or,

$$
44.44 b^{\prime}-a^{\prime}=0
$$

At,

$$
r=0.12 \mathrm{~m}, \sigma_{r}=12 \mathrm{MN} / \mathrm{m}^{2}
$$

or,

$$
\begin{align*}
\frac{b^{\prime}}{0.12^{2}}-a^{\prime} & =0  \tag{iv}\\
69 \cdot 44 b^{\prime}-a^{\prime} & =12
\end{align*}
$$

From eqns. (iii) and (iv), we get

$$
b^{\prime}=+0.48, \text { and } a^{\prime}=+21.33
$$

Hence the circumferential stress at any point in the outer tube will be given by

$$
\sigma_{c}=\frac{0.48}{r^{2}}+21.33
$$

At,

$$
r=0.12 \mathrm{~m},
$$

At,

$$
\begin{aligned}
r & =0.12 \mathrm{IL}, \\
\sigma_{c(0.12)} & =\frac{0.48}{0.12^{2}}+21.33=54.66 \mathrm{MN} / \mathrm{m}^{2} \text { (tensile) } \\
r & =0.15 \mathrm{~m}, \\
\sigma_{c(0.15)} & =\frac{0.48}{0.15^{2}}+21.33=42.66 \mathrm{MN} / \mathrm{m}^{2} \text { (tensile) }
\end{aligned}
$$

## 650 - Strength of Materials

## (b) After the fluid is admitted:

Let the Lame's equation be:

At,

$$
\sigma_{r}=\frac{b}{r^{2}}-a
$$

$$
r=0.09 \mathrm{~m}, \sigma_{r}=90 \mathrm{MN} / \mathrm{m}^{2}
$$

$\therefore \quad 90=\frac{b}{0.09^{2}}-a$
or,
At,

$$
90=123.45 b-a
$$

$$
r=0.15 \mathrm{~m}, \sigma_{r}=0
$$

$\therefore \quad 0=\frac{b}{0.15^{2}}-a$
or $\quad 0=44.44 b-a$
From eqns. (v) and ( $v i$ ), we get

$$
b=1.139 \text { and } a=50.61
$$

Hence, the circumferential stress at any point in the compound tube is given by,

$$
\sigma_{c}=\frac{b}{r^{2}}+a
$$

At,

$$
\begin{aligned}
& r=0.09 \mathrm{~m}, \sigma_{c(0.09)}=\frac{1.139}{0.09^{2}}+50.61=191.23 \mathrm{MN} / \mathrm{m}^{2} \text { (tensile) } \\
& r=0.12 \mathrm{~m}, \sigma_{c(0.12)}=\frac{1.139}{0.12^{2}}+50.61=129.71 \mathrm{MN} / \mathrm{m}^{2} \text { (tensile) } \\
& r=0.15 \mathrm{~m}, \sigma_{c(0.15)}=\frac{1.139}{0.15^{2}}+50.61=101.23 \mathrm{MN} / \mathrm{m}^{2} \text { (tensile) }
\end{aligned}
$$

The final circumferential stresses at different points are tabulated below:
Tensile stress........ +
Compressive stress..... -

| Circumferential <br> (or hoop) stress <br> $\left(M N / m^{2}\right)$ | Inner tube |  | Outer tube |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $r=0.09 \mathrm{~m}$ | $r=0.12 \mathrm{~m}$ | $r=0.12 \mathrm{~m}$ | $r=0.15 \mathrm{~m}$ |
| (i) Initially | -54.82 | -42.82 | +54.66 | +42.66 |
| (ii)Due to fluid <br> pressure | +191.23 | +129.71 | +129.71 | +10123 |
| Final | +136.41 | +86.89 | +184.31 | +143.89 |

Hence the final circumferential stresses are:


## 7) Determine the maximum and minimum hoop stress across the section of a pipe of 400 mm

 internal diameter and 100 mm thick, when the pipe contains a fluid at a pressure of $\mathbf{8 N} / \mathrm{mm}^{\mathbf{2}}$. Also sketch the radial pressure distribution and hoop stress distribution across the section.(May 2017) (Nov/Dec 2017)

## Solution,

Given:
Internal dia $=400 \mathrm{~mm}$
$\therefore$ Internal radius,

$$
r_{1}=\frac{400}{2}=200 \mathrm{~mm}
$$

Thickness $\quad=100 \mathrm{~mm}$
$\therefore$ External radius $\quad r_{2}=\frac{600}{2}=300 \mathrm{~mm}$
Fluid pressure, $\quad \mathrm{p}_{0}=8 \mathrm{~N} / \mathrm{mm}^{2}$
or at $x=r_{1}, p_{x}=p_{0}=8 \mathrm{~N} / \mathrm{mm}^{2}$

The radial pressure $\left(p_{x}\right)$ is given by equation (18.1) as

$$
\mathrm{p}_{\mathrm{x}}=\frac{\mathrm{b}}{\mathrm{x}^{2}}-\mathrm{a}
$$

Now apply the boundary conditions to the above equation. The boundary conditions are:

1. At $x=r_{1}=200 \mathrm{~mm}, p_{x}=8 \mathrm{~N} / \mathrm{mm}^{2}$
2. At $x=r_{2}=300 \mathrm{~mm}, \mathrm{p}_{\mathrm{x}}=0$

Substituting these boundary conditions in equation(i), we get
and

$$
\begin{equation*}
8=\frac{b}{200^{2}}-a=\frac{b}{40000}-a \tag{ii}
\end{equation*}
$$

$$
\begin{equation*}
0=\frac{b}{300^{2}}-a=\frac{b}{90000}-a \tag{iii}
\end{equation*}
$$

subtracting equation (iii) from equation (ii), we get

$$
\begin{aligned}
& 8=\frac{b}{40000}-\frac{b}{90000}=\frac{9 b-4 b}{360000}=\frac{5 b}{360000} \\
& b=\frac{360000 \times 8}{5}=5760000
\end{aligned}
$$

Substituting this value in equation (iii), we get

$$
0=\frac{5760000}{90000}-\mathrm{a} \quad \text { or } \mathrm{a}=\frac{5760000}{90000}=6.4
$$

The values of ' $a$ ' and ' $b$ ' are substituted in the hoop stress.
Now hoop stress at any radius $x$ is given by equation (18.2) as

$$
\sigma_{\mathrm{x}}=\frac{\mathrm{b}}{\mathrm{x}^{2}}+\mathrm{a}=\frac{576000}{\mathrm{x}^{2}}+6.4
$$

At $x=200 \mathrm{~mm}, \sigma_{200}=\frac{576000}{200^{2}}+6.4=14.4+6.4=20.8 \mathrm{~N} / \mathrm{mm}^{2}$. Ans.

At $x=300 \mathrm{~mm}, \sigma_{300}=\frac{576000}{300^{2}}+6.4=6.4+6 \cdot 4=12.8 \mathrm{~N} / \mathrm{mm}^{2}$. Ans.

Fig. 15 Shows the radial pressure distribution and hoop stress distribution across the section. $A B$ is taken a horizontal line. $A C=8 \mathrm{~N} / \mathrm{mm}^{2}$. The variation between $B$ and $C$ is parabolic. The curve $B C$ shows the variation of radial pressure across $A B$.


Fig. 15
The curve DE which is also parabolic, shows the variation of hoop stress across AB. Value BD = 12.8 $\mathrm{N} / \mathrm{mm}^{2}$ and $A E=20.8 \mathrm{~N} / \mathrm{mm}^{2}$. The radial pressure is compressive whereas the hoop stress is tensile.
8) A cylindrical vessel is 2 m diameter and 5 m long is closed at ends by rigid plates. It is subjected to an internal pressure of $4 \mathrm{~N} / \mathrm{mm}^{2}$ of the maximum principal stress is not to exceed $210 \mathrm{~N} / \mathrm{mm}^{2}$. Find the thickness of the shell. Assume $E=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poisons ratio=0.3, find the change in diameter, length and volume of the shell. [MAY/JUNE 2016-8 marks]

## Given data:

Diameter, $\mathrm{d}=2 \mathrm{~m}=2000 \mathrm{~mm}$
Length, $\quad \mathrm{l}=5 \mathrm{~m}=5000 \mathrm{~mm}$
Initial pressure, $p=4 \mathrm{~N} / \mathrm{mm}^{2}$

Maximum principal stress means the circumferential stress $=\sigma_{c}=210 \mathrm{~N} / \mathrm{mm}^{2}$
Young modulus $=\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
Poisons ratio $=\mathrm{u}=0.3$

## To find:

1.) Thickness of the shell ( t )
2.) Change in diameter ( $(\mathrm{d})$
3.) Change in length and ( $\int \ell$ )
4.) Change in volume ( $(\mathrm{V})$

## Solution:

$$
\begin{aligned}
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{\mathrm{zt}} \\
& \mathrm{t}=\frac{\mathrm{pd}}{2 \times \sigma_{\mathrm{c}}}=\frac{4 \times 2000}{2 \times 210}=19.047 \mathrm{~mm}
\end{aligned}
$$

## Change in diameter ( $(\mathrm{d})$

$$
\begin{aligned}
\int \mathrm{d} & =\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{1}{2} \times \mu\right] \\
& =\frac{4 \times 2000^{2}}{2 \times 19.047 \times 2 \times 10^{5}}[1-0.5 \times 0.3] \\
& \int \mathrm{d}=1.785 \mathrm{~mm}
\end{aligned}
$$

## Change in length ( $(\ell)$

$\int_{\ell}=\frac{\mathrm{pd} \ell}{2 \mathrm{t} \mathrm{E}}\left[\frac{1}{2}-\mu\right]$

$$
=\frac{4 \times 2000 \times 5000}{2 \times 19.047 \times 2 \times 10^{5}}\left[\frac{1}{2}-0.3\right]
$$

$\int \ell=1.050 \mathrm{~mm}$

## Change in volume ( $(\mathbf{v})$

$\frac{\int_{\mathrm{v}}}{\mathrm{v}}=\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[\frac{5}{2}-2 \times \mu\right]=\frac{4 \times 2000}{2 \times 19.047 \times 2 \times 10^{5}}\left[\frac{5}{2}-2 \times 0.3\right]$
$\int_{\mathrm{v} / \mathrm{v}=1.995 \times 10^{-3} \mathrm{~mm}^{3}} \quad\left[\mathrm{~V}=\frac{\pi}{4} \times \mathrm{d}^{2} \times \mathrm{L}\right]$
$\int_{\mathrm{v}}=1.995 \times 10^{-3} \times \frac{\pi}{4} \times 2000^{2} \times 5000$
$\int_{\mathrm{v}}=313121500 \mathrm{~mm}^{3}$
9) A spherical sheet of 1.50 m internal diameter and 12 mm shell thickness is subjected to pressure of $\mathbf{2 N} / \mathrm{mm}^{2}$. Determine the stress induced in the material of the shell [APR/-MAY/JUNE 2016-8marks]

## Given data:

Internal diameter, $\mathrm{d}=1.5 \mathrm{~m}=1500 \mathrm{~mm}$
Shell thickness, $\mathrm{t}=12 \mathrm{~mm}$
Pressure, $\mathrm{P}=2 \mathrm{~N} / \mathrm{mm}^{2}$

To find:
(1) Stress induced in the material of shell

$$
\begin{aligned}
\sigma_{1} & =\frac{\mathrm{p}}{4 \mathrm{t}} \\
& =\frac{2 \times 1500}{4 \times 12} \\
& =62.5 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

10) A spherical shell of internal diameter 1.2 m and of thickness 12 mm is subjected to an internal pressure of $4 \mathrm{~N} / \mathrm{mm}^{2}$. Determine the increase in diameter and increase in volume. Take $E=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=0.33$. [APR.MAY/JUNE 2016] 8marks

## Given data:

Internal diameter of spherical shell, $\mathrm{d}=1.2 \mathrm{~m}=1200 \mathrm{~mm}$
Thickness of spherical shell, $\mathrm{t}=12 \mathrm{~mm}$
Internal pressure, $\mathrm{P}=4 \mathrm{~N} / \mathrm{mm}^{2}$
Young's modulus, $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
Poisons ratio $=\mu=\frac{1}{\mathrm{~m}}=0.33$

## To find:

(i) Increase in diameter, $\delta \mathrm{d}$
(ii) Increase in volume, $\delta v$.

Change in diameter: ( $\delta \mathbf{d}$ )
$\delta \mathrm{d}=\frac{\mathrm{pd}^{2}}{4 \mathrm{tE}}\left[1-\frac{1}{\mathrm{~m}}\right]$

$$
\begin{aligned}
& =\frac{4 \times 1200^{2}}{4 \times 12 \times 2 \times 10^{5}}[1-0.33] \\
& \delta \mathrm{d}=0.402 \mathrm{~mm}
\end{aligned}
$$

## Change in volume ( $\mathbf{\delta v}$ )

$$
\begin{aligned}
\delta \mathrm{v} & =\mathrm{v} \times \mathrm{ev} \\
& =\mathrm{v} \times \frac{3 \mathrm{pd}}{4 \mathrm{tE}}\left[1-\frac{1}{\mathrm{~m}}\right] \\
& =\frac{\pi \mathrm{d}^{2}}{6} \times \frac{3 \mathrm{pd}}{4 \mathrm{tE}}\left[1-\frac{1}{\mathrm{~m}}\right] \\
& =\frac{\pi \mathrm{pd}^{4}}{8 \mathrm{tE}}[1-0.33] \\
& =\frac{3.14 \times 4 \times 1200^{4}}{8 \times 12 \times 2 \times 10^{5}}[1-0.33] \\
\delta & =908,841.6 \mathrm{~mm}^{3}
\end{aligned}
$$

## Result:

1) Change in diameter $=\delta \mathrm{d}=0.402 \mathrm{~mm}$
2.) Change in volume $=\delta v=908841.6 \mathrm{~mm}$
2) A steel cylinder of 300 mm external diameter is to be shrunk to another steal cylinder of 150 mm internal diameter. After shrinking the diameter at the function is 250 mm and radial pressure at the common function is $28 \mathrm{~N} / \mathrm{mm}^{2}$. Find the original difference in radial function. Take $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ [Apr/May 2016-8 marks]

## Given:

External diameter of outer cylinder $=300 \mathrm{~mm}$
Radius of outer cylinder $=r_{2}=150 \mathrm{~mm}$
Internal diameter of inner cylinder $=150 \mathrm{~mm}$
Radius of inner cylinder $=r_{1}=75 \mathrm{~mm}$
Diameter at the function $=250 \mathrm{~mm}$
$\square$ radius at the function $=\mathrm{r}^{*}=125 \mathrm{~mm}$
Radial pressure at the function, $\mathrm{P}^{*}=\mathrm{N} / \mathrm{mm}^{2}$
Young modulus $=\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
Original difference of radius at the function $=\frac{2 r^{*}}{E}\left(a_{1}-a_{2}\right)---(1)$
Find the values of $a_{1}$ and $a_{2}$ using the lame's equation.

## For outer cylinder

$\mathrm{P}_{\mathrm{x}}=\frac{\mathrm{b}_{1}}{\mathrm{X}_{1}{ }^{2}}-\mathrm{a}_{1}$
(i) At function $\quad \mathrm{x}=\mathrm{r}^{*}=125 \mathrm{~mm}$ and $\mathrm{P}^{*}=28 \mathrm{~N} / \mathrm{mm}^{2}$
(ii) At $\mathrm{x}=150 \mathrm{~mm}, \mathrm{P}_{\mathrm{x}}=0$

Substitute in above equation, we get
$28=\frac{\mathrm{b}_{1}}{125^{2}}-\mathrm{a}_{1}=\frac{\mathrm{b}_{1}}{15625}-\mathrm{a}_{1}----(2)$
$0=\frac{\mathrm{b}_{1}}{150}-\mathrm{a}_{1}=\frac{\mathrm{b}_{1}}{22500}-\mathrm{a}_{1}----$ (3)
solving equation $(2) \times(3)$ we get

$$
b_{1}=1432000 \quad a_{1}=63.6
$$

For inner cylinder
$\mathrm{P}_{\mathrm{x}}=\frac{\mathrm{b}_{2}}{\mathrm{x}^{2}}-\mathrm{a}_{2}$
(i) At function $\mathrm{x}=\mathrm{r}^{*}=125 \mathrm{~m} \quad \mathrm{P}_{\mathrm{x}}=\mathrm{P}^{*}=28 \mathrm{~N} / \mathrm{mm}^{2}$
(ii) At $\mathrm{x}=75 \mathrm{~mm}, \mathrm{P}_{\mathrm{x}}=0$

Substitute these two condition ion above equation
$28=\frac{62}{75^{2}}-\mathrm{a}_{2}=\frac{\mathrm{b}_{2}}{15625}-\mathrm{a}_{2}-----(4)$
$0=\frac{\mathrm{b}_{2}}{75^{2}}-\mathrm{a}_{2}=\frac{\mathrm{b}_{2}}{15625}-\mathrm{a}_{2}------(5)$
solving equation (4) \& (3) we get
$b_{2}=-246100$
$\mathrm{a}_{2}=-43.75$
substitute the valuies of $\mathrm{a}_{2} \& \mathrm{a}_{1}$ in equation

$$
\begin{aligned}
& =\frac{2 r^{*}}{\mathrm{E}}\left(\mathrm{a}_{1}-\mathrm{a}_{2}\right) \\
& =\frac{2 \times 125}{2 \times 105} \quad[63.6-(-43.75)] \\
& =\frac{125}{105} \times 107.35 \\
& =0.13 \mathrm{~mm}
\end{aligned}
$$

12) Calculate (i) the change in diameter (ii) Change in length and (iii) Change in volume of a thin cylindrical shell 100 cm diameter, 1 cm thick and 5 m long, when subjected to internal pressure of $3 \mathrm{~N} / \mathrm{mm}^{2}$. Take the value of $E=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and poison's ratio, $\mu=0.3$ (Nov/Dec 2017)[Nov/Dec 2016][ 13 marks] [Nov/Dec 2015]

## Given data:

Diameter of cylindrical shell, (d) $=100 \mathrm{~cm}=1000 \mathrm{~mm}$
Thickness of shell $(\mathrm{t})=1 \mathrm{~cm}=10 \mathrm{~mm}$
Length of the shell $(\ell)=5 \mathrm{~m}=5000 \mathrm{~mm}$
Internal pressure $=\mathrm{P}=3 \mathrm{~N} / \mathrm{mm}^{2}$
Young modular $=\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$
Poison's ratio $=\mu=0.3$

## Solution:

Longitudinal stress,

$$
\begin{aligned}
& \sigma_{1}=\frac{\mathrm{pd}}{4 \mathrm{t}}=\frac{3 \times 1000}{4 \times 10}=75 \\
& \sigma_{1}=75 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

Hoop stress,

$$
\begin{aligned}
& \sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{3 \times 1000}{2 \times 10}=150 \\
& \sigma_{\mathrm{c}}=150 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

(i) Change in diameter

$$
\begin{aligned}
\delta \mathrm{d} & =\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left(1-\frac{1}{2 \mathrm{~m}}\right) \\
& =\frac{3 \times 1000^{2}}{2 \times 10 \times 2 \times 10^{5}}\left[1-\frac{1}{2} \times 0.3\right] \\
& \delta \mathrm{d}=0.637 \mathrm{~mm}
\end{aligned}
$$

(ii)Change in length ( $\boldsymbol{\delta} \ell$ )

$$
\begin{aligned}
\delta \ell & =\frac{\mathrm{pdL}}{2 \mathrm{tE}}\left[\frac{1}{2}-\mu\right] \\
& =\frac{3 \times 1000 \times 5000}{2 \times 10 \times 200 \times 10^{3}} \quad[0.5-0.3] \\
\delta \ell & =0.75 \mathrm{~mm}
\end{aligned}
$$

(iii) Change in volume,
$\delta \mathrm{v}=\mathrm{v} \times \frac{\mathrm{pd}}{2 \mathrm{tE}}\left(\frac{5}{2} \frac{-2}{\mathrm{~m}}\right)$
Volume, $\mathrm{v}=\frac{\pi}{4} \times \mathrm{d}^{2} \times \ell$

$$
\begin{aligned}
& =\frac{3.14}{4} \times 1000^{2} \times 5000 \\
& =39.25 \times 10^{8} \mathrm{~mm}^{3}
\end{aligned}
$$

$\delta \mathrm{v}=39.25 \times 10^{8} \times \frac{3 \times 1000}{2 \times 10 \times 2 \times \times 10^{5}}\left[\frac{5}{2}-2(0.3)\right]$
$\delta \mathrm{v}=5593125 \mathrm{~mm}^{3}$

## Result:

(i) Change in diameter $(\delta \mathrm{d})=0.637 \mathrm{~mm}$
(ii) Change in length $(\delta \ell)=0.75 \mathrm{~mm}$
(iii) Change in length $(\delta \mathrm{v})=5593125 \mathrm{~mm}^{3}$
13) Calculate the thickness of metal necessary for a cylindrical shell of internal diameter 16 mm ton with slant of internal pressure of $25 \mathrm{mN} / \mathbf{m}_{2}$. If maximum permissible shell stress is $\mathbf{1 2 5 M N} / \mathbf{m}_{\mathbf{2}}$. [NOV/DEC2016]

## Given data:

Internal diameter, $\mathrm{d}=160 \mathrm{~mm}$.
Internal pressure, $P=25 \mathrm{MN} / \mathrm{m}^{2}=25 \mathrm{~N} / \mathrm{Mm}^{2}$
Maximum permissible shell stress $=125 \mathrm{MN} / \mathrm{m}^{2}=125 \mathrm{~N} / \mathrm{mm}^{2}$

## To find:

Thickness (t)

## Solution:

$$
\begin{aligned}
\sigma_{\max } & =\frac{\mathrm{pd}}{8 \mathrm{t}} \\
125 & =\frac{25 \times 160}{8 \times \mathrm{t}} \\
\mathrm{t} & =\frac{25 \times 160}{125 \times 8} \\
\mathrm{t} & =4 \mathrm{~mm}
\end{aligned}
$$

Thickness of cylinderrical shell is 4 mm
14) A boiler is subjected to an internal steam pressure of $2 \mathrm{~N} / \mathrm{mm}^{2}$. The thickness of boiler plate is 2.6 cm and permissible tensile stress is $120 \mathrm{~N} / \mathrm{mm}^{2}$. Find the maximum diameter, when efficiency of longitudinal joint is $\mathbf{9 0 \%}$ and that of circumference joint is $\mathbf{4 0 \%}$.

## Given data:

Internal steam pressure, $\mathrm{P}=2 \mathrm{~N} / \mathrm{mm}^{2}$
Thickness boiler plate, $\mathrm{t}=2.6 \mathrm{~cm} \& 26 \mathrm{~mm}$
Permissible tensile stress $(\sigma)=120 \mathrm{~N} / \mathrm{mm}^{2}$
Efficiency of longitudinal joint, $\eta_{1}=90 \%=0.90$
Efficiency of circumferences joint, $\eta_{\mathrm{c}}=40 \%=0.40$
In case of joint the permissible stress may be longitudinal (or) circumferential stress.

## To find:

Maximum diameter (d)

## Solution:

## Maximum diameter of circumference stress

$$
\begin{aligned}
\sigma_{\mathrm{c}} & =\frac{\mathrm{pd}}{2 \mathrm{t} \eta_{\mathrm{l}}} \\
120 & =\frac{2 \times \mathrm{d}}{2 \times 0.90 \times 2.6} \\
\mathrm{~d} & =\frac{120 \times 2 \times 0.90 \times 26}{2} \\
\mathrm{~d} & =2808 \mathrm{~mm}
\end{aligned}
$$

## Maximum diameter for longitudinal stress

$$
\begin{aligned}
\sigma_{2} & =\frac{\mathrm{pd}}{4 \mathrm{t} \times \eta_{\mathrm{c}}} \\
120 & =\frac{2 \times \mathrm{d}}{4 \times 26 \times 0.40} \\
\mathrm{~d} & =\frac{120 \times 4 \times 0.40 \times 26}{2} \\
\mathrm{~d} & =2496 \mathrm{~mm}
\end{aligned}
$$

The longitudinal (or) circumferential stresses induced in the material directly proportional to diameter (d). Hence the stress induced will be less if the value of ' $d$ ' is less. Hence take the minimum value of diameter.

Hence, diameter (d) $=249.6 \mathrm{~cm}$
15) A thin cylindrical shell 2.5 long has 700 mm internal diameters and 8 mm thickness, if the shell is subjects to an internal pressure of 1 Mpa , find
(i) The hoop and longitudinal stresses developed
(ii) Maximum shell stress induced and
(iii) The change in diameter, length and volume. Take modulus of elasticity of the wall material as 200Gpa and poison's ratio as 0.3
[AP/MAY 2015-16 marks]

## Given data:

Length of cylindrical shell, $\ell=2.5 \mathrm{~m}=2500 \mathrm{~mm}$
Internal diameter $\ddagger \mathrm{d},=700 \mathrm{~mm}$
Thickness of shell, $\mathrm{t}=8 \mathrm{~mm}$
Internal pressure, $\mathrm{P}=1 \mathrm{mpa}=1 \mathrm{~N} / \mathrm{mm}^{2}$
Modulus of elasticity $=\mathrm{E}=200 \mathrm{Gpa}=200 \times 10^{3} \mathrm{~N} / \mathrm{mm}^{2}$
Poison's ratio $=\mu=0.3$
To find:
1.) Hoop stress and longitudinal stress
2.) Maximum shell stress induced.
3.) Change in diameter, ( $\delta \mathrm{d})$
4.) Change in volume, ( $\delta v)$
5.) Change in length ( $\delta \ell$ )

## Solution:

Hoop stress, $\sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{1 \times 700}{2 \times 8}=43.75$
$\sigma_{\mathrm{c}}=43.75 \mathrm{~N} / \mathrm{mm}^{2}$

$$
\text { Longitudinal stress, } \begin{aligned}
\sigma_{\ell} & =\frac{\mathrm{pd}}{\mathrm{ut}}=\frac{1 \times 700}{4 \times 8}=21.87 \\
\sigma_{\ell} & =21.875 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

## Change in diameter ( $\delta \mathbf{d}$ )

$$
\begin{aligned}
& \delta \mathrm{d}=\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{\mu}{2}\right] \\
&=\frac{1 \times 700^{2}}{2 \times 8 \times 200 \times 0^{3}}\left[1-\frac{0.3}{2}\right] \\
& \delta \mathrm{d}=0.130 \mathrm{~mm}
\end{aligned}
$$

## Change in length ( $\delta$ ©

$$
\begin{aligned}
\delta \ell & =\frac{\mathrm{pdL}}{2 \mathrm{tE}}\left[\frac{1}{2}-\mu\right] \\
& =\frac{1 \times 700 \times 2500}{2 \times 8 \times 200 \times 10^{3}} \quad[0.5-0.3] \\
\delta \ell & =0.109 \mathrm{~mm}
\end{aligned}
$$

## Change in volume ( $\delta \mathrm{v}$ )

$$
\delta \mathrm{v}=\frac{\mathrm{pdv}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right]
$$

original volume, $\mathrm{V}=\frac{\pi}{4} \mathrm{~d}^{2} \times \ell=\frac{\pi}{4} \times 700^{2} \times 2500$

$$
\begin{aligned}
& \mathrm{V}=961625000 \mathrm{~mm}^{3}=96.16 \times 10^{7} \mathrm{~mm}^{3} \\
& \delta \mathrm{v}=\frac{1 \times 700 \times 96.16 \times 10^{7}}{2 \times 8 \times 200 \times 10^{3}}\left[\frac{5}{2}-2 \times 0.3\right] \\
& \delta \mathrm{v}=399665 \mathrm{~mm}^{3}
\end{aligned}
$$

## Maximum shell stress induced (бmax)

$$
\begin{aligned}
& \sigma_{\max }=\frac{\mathrm{pd}}{\mathrm{t}}=\frac{1 \times 700}{8 \times 8}=10.937 \mathrm{~N} / \mathrm{mm}^{2} \\
& \sigma_{\max }=10.937 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

## Result:

1.) Hoop stress $\sigma_{c}=43.75 \mathrm{~N} / \mathrm{mm}^{2}$
2.) Longitudinal stress, $\sigma_{\ell}=21.875 \mathrm{~N} / \mathrm{mm}^{2}$
3.) Maximum shell stress, $\sigma_{\max }=10.937 \mathrm{~N} / \mathrm{mm}^{2}$
4.) Change in diameter, $\delta \mathrm{d}=0.130 \mathrm{~mm}$
5.) Change in length, $\delta \ell=0.109 \mathrm{~mm}$
6.) Change in length, $\delta v=399665 \mathrm{~mm}^{3}$
16) A thick cylinder with external diameter 320 mm and internal diameter 160 mm is subjected to an internal pressure of $\mathbf{8 N} / \mathrm{mm}^{2}$. Draw the variation of radial and hoop stresses in the cylinder wall. Also determine the maximum shell stress in the cylinder wall.
[APR/MAY- 2015-16marks]

## Given data:

Internal diameter, $\mathrm{d}_{1}=160 \mathrm{~mm}$
External diameter, $\mathrm{d}_{2}=320 \mathrm{~mm}$
Internal radius, $r_{1}=80 \mathrm{~mm}$
External radius, $r_{2}=160 \mathrm{~mm}$
Internal pressure, $\mathrm{P}_{1}=\left[8 \mathrm{~N} / \mathrm{mm}^{2}\right.$

To find:
1.) To draw variation of radial and hoop stress.
2.) The maximum shell stress in the cylinder.

Solution: we know that by lame's equation

$$
\begin{aligned}
& \sigma_{r}=\frac{\mathrm{b}}{\mathrm{r}^{2}}-\mathrm{a}-----(1) \\
& \sigma_{\mathrm{c}}=\frac{\mathrm{b}}{\mathrm{r}^{2}}+\mathrm{a}-----(2)
\end{aligned}
$$

At, $\mathrm{r}=\mathrm{r}_{1}=80$, and $\sigma_{\mathrm{r}}=\mathrm{P}_{1}=8 \mathrm{~N} / \mathrm{mm}^{2}$

$$
\mathrm{R}=\mathrm{r}_{2}=160 \mathrm{~mm} \text { and } \sigma_{\mathrm{r}}=\mathrm{P}_{2}=0
$$

Substitute in equation (1)

$$
\begin{aligned}
& 8=\frac{b}{(80)^{2}}-a \Rightarrow 8=1.562 \times 10^{-4} \mathrm{~b}-\mathrm{a}----(3) \\
& 0=\frac{\mathrm{b}}{(160)^{2}}-\mathrm{a} \Rightarrow 0=3.9 \times 10^{-5} \mathrm{~b}-\mathrm{a}-----(4)
\end{aligned}
$$

Equation (3) and (4) becomes

$$
\begin{aligned}
& a-1.562 \times 10^{-4} b=-8----(5) \\
& a-3.9 \times 10^{-4} b=0-----(6)
\end{aligned}
$$

Solving equation (5) and (6)

$$
\begin{aligned}
& \mathrm{A}=13.34 \\
& \mathrm{~B}=34217.27
\end{aligned}
$$

Substitute values of $a$ and $b$ in equation (2)
$\sigma_{c}=\frac{\mathrm{b}}{(80)^{2}}+\mathrm{a} \Rightarrow=\frac{34217.27}{80^{2}}+13.34$
$\sigma_{\mathrm{c}}=18.686 \mathrm{~N} / \mathrm{mm}^{2}$
Atr $=r_{2}=160 \mathrm{~mm}$
$\sigma_{c}=\frac{\mathrm{b}}{(160)^{2}}+\mathrm{a} \Rightarrow \frac{34217.27}{(160)^{2}}+13.34$
$\sigma_{\mathrm{c}}=14.67 \mathrm{~N} / \mathrm{mm}^{2}$

17) Desire relations for change in dimensions and change in volume of a thin cylinder subjected to internal pressure $\mathbf{P}$.
(May / June 2017) [NOV/DEC 2014]-16marks

Due to Internal pressure, the cylindrical shells are subjected to lateral and linear strain. Thus the change in dimensions such as length, diameter may increases.

We know that

$$
\mathrm{e}_{\mathrm{c}}=\frac{\delta \mathrm{d}}{\mathrm{~d}}=\frac{\sigma_{\mathrm{c}}}{\mathrm{E}}-\frac{\sigma_{\mathrm{a}}}{\mathrm{mE}}
$$

Where, $\delta \mathrm{d}$-change in diameter

Circumferential stress,

$$
\begin{aligned}
& \frac{1}{\mathrm{~m}}=\text { poison's ratio } \\
& \mathrm{E}-\text { young's Modulus } \\
& \mathrm{e}_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{tE}}-\frac{\mathrm{pd}}{\mu \mathrm{mE}} \\
& \mathrm{e}_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[1-\frac{1}{2 \mathrm{~m}}\right]
\end{aligned}
$$

Change in diameter, $\begin{aligned} & \delta \mathrm{d}=\mathrm{e}_{\mathrm{c}} \times \mathrm{d} \\ & \delta \mathrm{d}=\frac{\mathrm{pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{1}{2 \mathrm{~m}}\right]\end{aligned}$

$$
\begin{aligned}
& \mathrm{e}_{\mathrm{a}}=\frac{\delta \ell}{\ell}=\frac{\sigma_{\mathrm{a}}}{\mathrm{E}}-\frac{\sigma_{\mathrm{c}}}{\mathrm{mE}} \\
&=\frac{\mathrm{pd}}{4 \mathrm{tE}}-\frac{\mathrm{pd}}{2 \mathrm{tmE}} \\
& \mathrm{e}_{\mathrm{a}}=\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[\frac{1}{2}-\frac{1}{\mathrm{~m}}\right]
\end{aligned}
$$

Longitudinal strain, $\quad=\frac{\mathrm{pd}}{4 \mathrm{tE}}-\frac{\mathrm{pd}}{2 \mathrm{tmE}}$

Change in length,
$\delta \ell=e_{a} \times \ell$
$\delta \ell=\frac{\mathrm{pd} \ell}{2 \mathrm{tE}}\left[\frac{1}{2}-\frac{1}{\mathrm{~m}}\right]$
Volume strain,

$$
\begin{aligned}
\mathrm{e}_{\mathrm{v}} & =\frac{\text { final volume }- \text { initial volume }}{\text { initial volume }} \\
& =\frac{\frac{\pi}{4}\left(\mathrm{~d}+\delta \mathrm{d}^{2}\right)(\ell+\delta \ell)-\frac{\pi}{4} \mathrm{~d}^{2} \ell}{\frac{\pi}{4} \mathrm{~d}^{2} \ell}
\end{aligned}
$$

By neglecting higher order terms of $\delta \ell$ and $\delta d$

$$
\begin{aligned}
\mathrm{e}_{\mathrm{v}} & =\frac{2 \delta \mathrm{~d}}{\mathrm{~d}}+\frac{\delta \ell}{\ell} \\
& =2 \mathrm{e}_{\mathrm{c}}+\mathrm{e}_{\mathrm{a}} \\
& =\frac{2 \mathrm{pd}}{2 \mathrm{tE}}\left(1-\frac{1}{2 \mathrm{~m}}\right)+\frac{\mathrm{pd}}{2 \mathrm{tE}}\left(\frac{1}{2}-\frac{1}{\mathrm{~m}}\right) \\
& =\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[2-\frac{2}{2 \mathrm{~m}}+\frac{1}{2}-\frac{1}{\mathrm{~m}}\right] \\
& =\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[2+\frac{1}{2}-\frac{2}{\mathrm{~m}}\right] \\
\mathrm{e}_{\mathrm{v}} & =\frac{\mathrm{pd}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right]
\end{aligned}
$$

Change in volume,

$$
\begin{aligned}
\delta \mathrm{v} & =\mathrm{e}_{\mathrm{v}} \times \mathrm{v} \\
& =\frac{\mathrm{pdv}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right] \\
\delta \mathrm{v} & =\mathrm{v} \times \frac{\sigma_{\mathrm{c}}}{\mathrm{E}}\left(\frac{5}{2}-\frac{2}{\mathrm{~m}}\right)
\end{aligned}
$$

18) Find the thickness of metal necessary for a thick cylindrical shell of internal diameter 160 mm to withstand an internal pressure on $8 \mathrm{~N} / \mathrm{mm}^{2}$. The maximum hoop stress in section is not to exceed 35N/mm ${ }^{2}$.
[NOV/DEC-2014-] [16 marks]

## Given data:

Internal diameter, $\mathrm{d}_{1}=160 \mathrm{~mm}$
Internal radius $=r_{1}=\frac{d_{1}}{2}=\frac{160}{2}=80 \mathrm{~mm}$
Internal pressure, $=\mathrm{P}_{1}=8 \mathrm{~N} / \mathrm{mm}^{2}$
Maximum hoop stress $=\sigma_{c}=35 \mathrm{~N} / \mathrm{mm}^{2}$

## To find:

## Thickness of metal ( $\mathbf{t}$ )

## Solution:

The lame's equation's are
$\sigma_{\mathrm{r}}=\frac{\mathrm{b}}{\mathrm{r}^{2}}-\mathrm{a}-----(1)$
$\sigma_{\mathrm{c}}=\frac{\mathrm{b}}{\mathrm{r}^{2}}+\mathrm{a}-----(2)$

At $\mathrm{r}=\mathrm{r}_{\mathrm{i}}=80 \mathrm{~mm}$ and $\sigma_{\mathrm{r}}=\mathrm{P}_{1}=8 \mathrm{~N} / \mathrm{mm}^{2}$

$$
\left(\sigma_{\mathrm{c}}\right)_{\max }=35 \mathrm{~N} / \mathrm{mm}^{2}
$$

substituting in equation (1) and (2), we get

$$
\begin{aligned}
& 8=\frac{b}{(80)^{2}}-a \Rightarrow 8=1.56 \times 10^{-4} \mathrm{~b}-\mathrm{a}----(3) \\
& 35=\frac{\mathrm{b}}{(80)^{2}}+\mathrm{a} \Rightarrow 35=1.56 \times 10^{-4} \mathrm{~b}+\mathrm{a}----(4)
\end{aligned}
$$

Equation (3) and (4) becomes

$$
\begin{aligned}
& a-1.56 \times 10^{-4} b=-8----(5) \\
& -a-1.56 \times 10^{-4} b=-35---(6)
\end{aligned}
$$

Solving equation (5) and (6), we get
(5) $\times 1$

$$
\begin{aligned}
& -\mathrm{a}+1.56 \times 10^{-4} \mathrm{~b}=-8 \\
& -\mathrm{a}-1.56 \times 10^{-4} \mathrm{~b}=-35 \\
& -2 \mathrm{a} \\
& \mathrm{a}=13.5
\end{aligned}
$$

(6) $\times 1$

Substitute (a) value in equation (5)

$$
\begin{aligned}
13.5-1.56 \times 10^{-4} \mathrm{~b} & =-8 \\
-1.56 \times 10^{-4} \mathrm{~b} & =-8-13.5 \\
-1.56 \times 10^{-4} \mathrm{~b} & =-21.5 \\
\mathrm{~b} & =\frac{21.5}{1.56 \times 10^{-4}} \\
\mathrm{~b} & =137.82
\end{aligned}
$$

19) A cylindrical shell in diameter and 3 m length is subjected to an internal pressure of 2 MPa . Calculate the maximum thickness if the stress should not exceed 50 MPa . Find the change in diameter and volume of shell. Assume poisson's ratio of 0.3 and young's modulus of $200 \mathrm{kN} / \mathrm{mm}^{2}$.
[MAY/JUNE -2014-
16marks]

## Given data:

Diameter of cylindrical shell, $\mathrm{d}=1 \mathrm{~m}=1000 \mathrm{~mm}$
Length of cylindrical shell, $\ell=3, m=3000 \mathrm{~mm}$
Internal pressure, $\mathrm{P}=2 \mathrm{Mpa}=2 \mathrm{~N} / \mathrm{mm}^{2}$
Maximum stress,. $\sigma_{c}=50 \mathrm{Mpa}=50 \mathrm{~N} / \mathrm{mm}^{2}$
Young's modulus $=\mathrm{E}=200 \mathrm{KN} / \mathrm{mm}^{2}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$

Poison's ratio, $\frac{1}{\mathrm{~m}}=0.3$

## To find:

(i) Change in diameter, $\delta \mathbf{d}$
(ii) Change in volume, $\delta \mathbf{v}$.

## Solution:

$$
\sigma_{\mathrm{c}}=\frac{\mathrm{pd}}{2 \mathrm{t}}=\frac{2 \times 1000}{2 \times \mathrm{t}}
$$

Hoop stress, $50=\frac{2 \times 1000}{2 \times \mathrm{t}}$

$$
\mathrm{t}=20 \mathrm{~mm}
$$

Change in diameter, $\delta \mathrm{d}$
$\delta \mathrm{d}=\frac{\mathrm{Pd}^{2}}{2 \mathrm{tE}}\left[1-\frac{1}{2 \mathrm{~m}}\right]$

$$
=\frac{2 \times(1000)^{2}}{2 \times 20 \times 2 \times 10^{5}}\left[1-\frac{1}{2} \times 0.3\right]
$$

$\delta \mathrm{d}=0.2125 \mathrm{~mm}$
Change in volume,

$$
\begin{aligned}
\delta \mathrm{v} & =\frac{\mathrm{pdv}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right] \\
\text { Volume of cylinder, } \mathrm{V} & =\frac{\pi}{4} \mathrm{~d}^{2} \times \ell \\
& =\frac{\pi}{4}(1000)^{2} \times 3000 \\
& =2.355 \times 10^{9} \mathrm{~mm}^{3}
\end{aligned}
$$

$$
\delta \mathrm{v}=\frac{\mathrm{Pdv}}{2 \mathrm{tE}}\left[\frac{5}{2}-\frac{2}{\mathrm{~m}}\right]
$$

$$
=\frac{2 \times 1000 \times 2.35 \times 10^{9}}{2 \times 20 \times 2 \times 10^{5}} \quad[2.5-0.6]
$$

$$
\delta \mathrm{v}=118625 \mathrm{~mm}^{3}
$$

## Result:

(i) Thickness of cylinder. $\mathrm{t}=20 \mathrm{~mm}$
(ii) Change in diameter. $\delta \mathrm{d}=0.2125 \mathrm{~mm}$
(iii) Change in volume, $\delta v=1118625 \mathrm{~mm}^{3}$.

