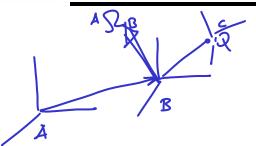


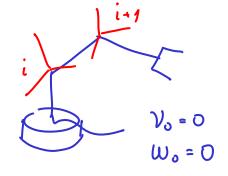
Velocity Propagation Between Robot Links 3/4





Introduction – Velocity Propagation





$$A_{\mathcal{Q}} = A_{\mathcal{B} \circ \mathcal{R} G} + A_{\mathcal{R}} \mathcal{R}^{\mathcal{B}} \mathcal{V}_{\mathcal{Q}} + A_{\mathcal{R}} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{\mathcal{Q}} \longrightarrow \mathcal{V}_{i+1} = \mathcal{R}^{i+1} \mathcal{R} \left(\mathcal{W}_{i} \mathcal{R}^{i} \mathcal{P}_{i+1} + \mathcal{V}_{i} \right) + \left(\mathcal{A}_{i+1} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{i+1} + \mathcal{V}_{i} \right) + \left(\mathcal{A}_{i+1} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{i} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{i+1} + \mathcal{V}_{i} \right) + \left(\mathcal{A}_{i+1} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{i} \mathcal{R}^{\mathcal{B}} \mathcal{P}_{i} \mathcal{P}_{i+1} + \mathcal{P}_{i} \mathcal{P}_{i+1} + \mathcal{P}_{i} \mathcal$$

$${}^{4}\Omega_{c} = {}^{4}\Omega_{B} + {}^{4}_{B}R^{B}\Omega_{c}$$

$$\longrightarrow^{i+1} W_{i+1} = iR^{i}W_{i} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{i+1} \end{bmatrix}$$

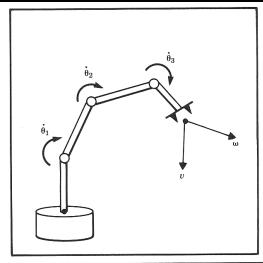


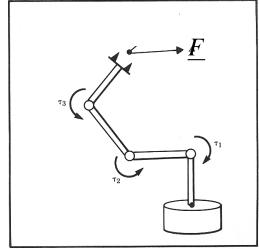
Jacobian Matrix - Introduction

In the field of robotics the Jacobian matrix describe the relationship between the joint angle rates $(\dot{\theta}_N)$ and the translation and rotation velocities of the end effector (\dot{x}) . This relationship is given by:

In addition to the velocity relationship, we are also interested in developing a relationship between the robot joint torques (τ) and the forces and moments (F) at the robot end effector (Static Conditions). This relationship is given by:

$$\underline{\tau} = J(\underline{\theta})^T \underline{F}$$

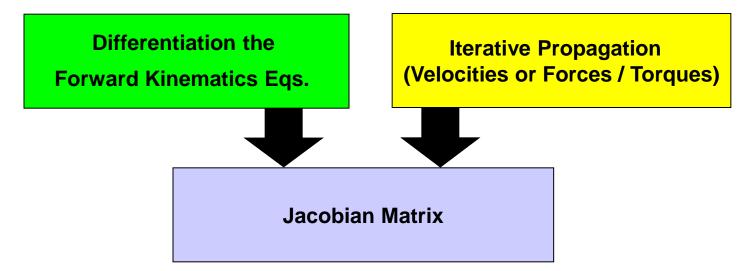








Jacobian Matrix - Calculation Methods







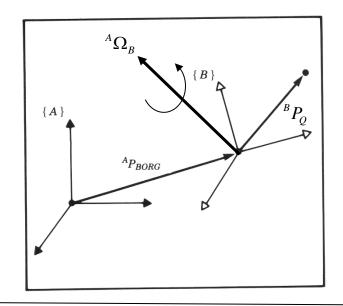
Summary – Changing Frame of Representation

- Linear and Rotational Velocity
 - Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

Matrix Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega} \left({}^{A}_{B}R^{B}P_{Q} \right)$$



- Angular Velocity
 - Vector Form

$$^{A}\Omega_{C} = ^{A}\Omega_{B} + ^{A}_{B}R^{B}\Omega_{C}$$

Matrix Form

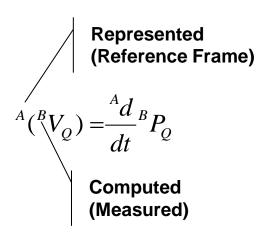
$${}_{C}^{A}\dot{R}_{\Omega} = {}_{B}^{A}\dot{R}_{\Omega} + {}_{B}^{A}R_{C}^{B}\dot{R}_{\Omega}^{A}R^{T}$$

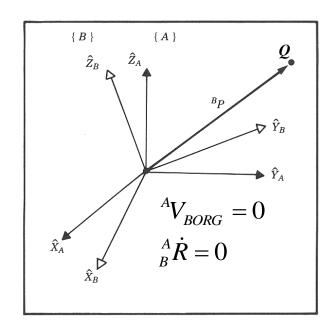




Frame - Velocity

- As with any vector, a velocity vector may be described in terms of any frame, and this frame of reference is noted with a leading superscript.
- A velocity vector <u>computed</u> in frame {B} and <u>represented</u> in frame {A} would be written









Position Propagation

- The homogeneous transform matrix provides a complete description of the linear and angular position relationship between adjacent links.
- These descriptions may be combined together to describe the position of a link relative to the robot base frame {0}.

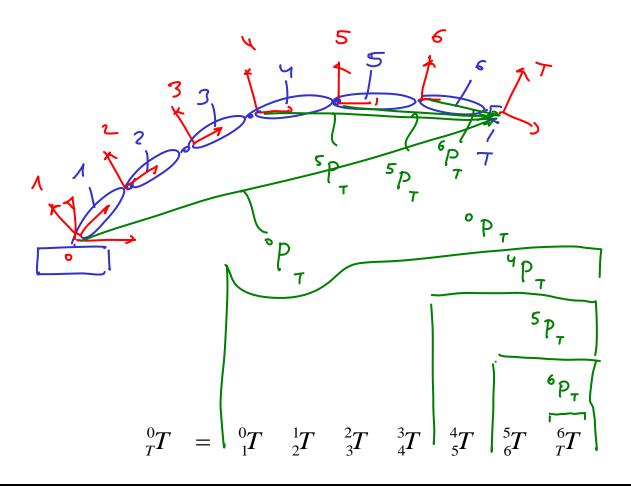
$$_{i}^{o}T = _{1}^{o}T_{2}^{1}T \cdots _{i}^{i-1}T$$

 A similar description of the linear and angular velocities between adjacent links as well as the base frame would also be useful.





Position Propagation







Motion of the Link of a Robot

• In considering the motion of a robot link we will always use link frame {0} as the reference frame (Computed AND Represented). However any frame can be used as the reference (represented) frame including the link's own frame (i)

Where: v_i - is the linear velocity of the origin of link frame (i) with respect to frame {0} (Computed AND Represented)

 ω_i - is the angular velocity of the origin of link frame (i) with respect to frame {0} (Computed AND Represented)

• Expressing the velocity of a frame {i} (associated with link i) relative to the robot base (frame {0}) using our previous notation is defined as follows:

$$v_i \equiv {}^{0} \left[{}^{0}V_i \right] = \left[{}^{0}V_i \right]$$

$$\omega_{i} \equiv {}^{0} \left[{}^{0} \Omega_{i} \right] = \left[{}^{0} \Omega_{i} \right]$$



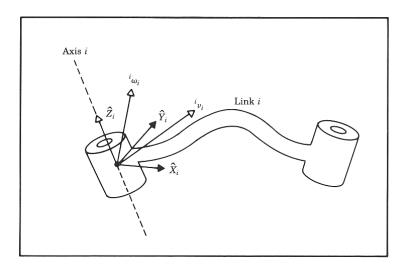


Velocities - Frame & Notation

• The velocities differentiate (computed) relative to the base frame $\{0\}$ are often represented relative to other frames $\{k\}$. The following notation is used for this conditions

$${}^{k}v_{i} \equiv {}^{k} \left[{}^{0}V_{i} \right] = {}^{k}R \left[{}^{0}V_{i} \right] = {}^{k}R \cdot v_{i}$$

$${}^{k}\omega_{i} \equiv {}^{k} \left[{}^{0}\Omega_{i} \right] = {}^{k}R \left[{}^{0}\Omega_{i} \right] = {}^{k}R \cdot \omega_{i}$$



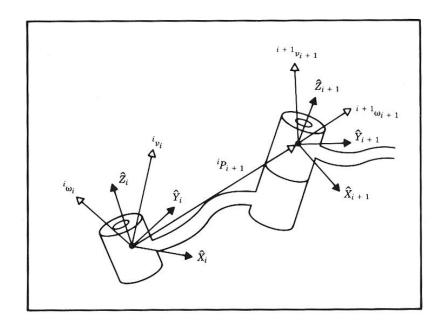




Velocity Propagation

- Given: A manipulator A chain of rigid bodies each one capable of moving relative to its neighbor
- Problem: Calculate the linear and angular velocities of the link of a robot
- Solution (Concept): Due to the robot structure (serial mechanism) we can compute the velocities of each link in order starting from the base.

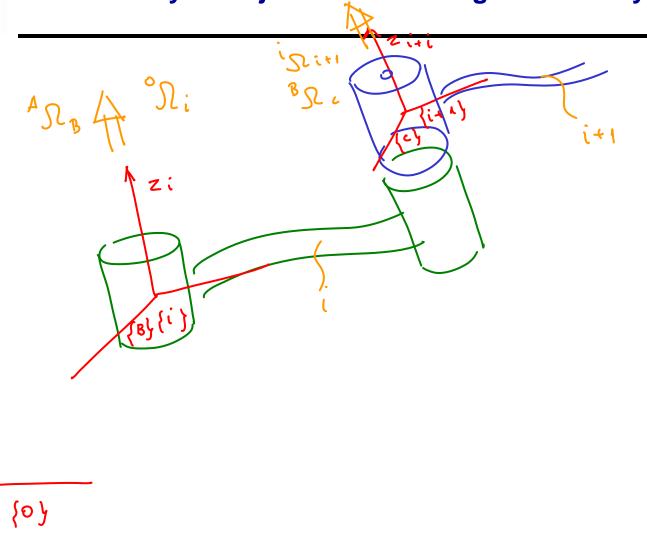
The velocity of link i+1 will be that of link i, plus whatever new velocity components were added by joint i+1







Velocity of Adjacent Links - Angular Velocity 0/5







Velocity of Adjacent Links - Angular Velocity 1/5

From the relationship developed previously

$$\longrightarrow {}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

 we can re-assign link names to calculate the velocity of any link i relative to the base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i+1 \end{cases}$$

$${}^{0}\Omega_{i+1} = {}^{0}\Omega_{i} + {}^{0}_{i}R^{i}\Omega_{i+1}$$

• By pre-multiplying both sides of the equation by ${}^{i+1}_{0}R$,we can convert the frame of reference for the base $\{0\}$ to frame $\{i+1\}$





Velocity of Adjacent Links - Angular Velocity 2/5

 ${}^{i+1}_{0}R^{0}\Omega_{i+1} = {}^{i+1}_{0}R^{0}\Omega_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}\Omega_{i+1}$

Using the recently defined nøtation, we have

$$\omega_{i+1} = \omega_i + \sum_{i=1}^{i+1} R^i \Omega_{i+1}$$

- Angular velocity of frame $\{i+1\}$ measured relative to the robot base, and expressed in frame $\{i+1\}$ - **Recall the car example** ${}^c [{}^wV_{a}] = {}^c v_{a}$

- Angular velocity of frame $\{i\}$ measured relative to the robot base, and expressed in frame $\{i+1\}$

 ${}^{i+1}_{i}R^{i}\Omega_{i+1}$ - Angular velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$





Velocity of Adjacent Links - Angular Velocity 3/5

$$\omega_{i+1} = \overline{\omega_i} + \overline{\omega_i} + \overline{\Omega_i} + \overline{\Omega_i}$$

 Angular velocity of frame {i} measured relative to the robot base, expressed in frame {i+1}

$$i^{i+1}\omega_{i} = i^{i+1}R^{i}\omega_{i}$$

$$i^{i+1}R \left[iR \circ \Omega \right]$$

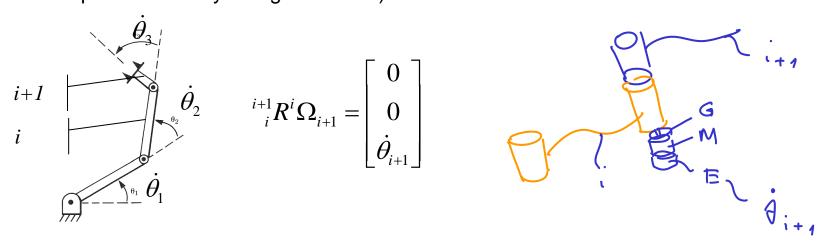




Velocity of Adjacent Links - Angular Velocity 4/5

$$^{i+1}\omega_{i+1}=^{i+1}\omega_{i}+^{i+1}_{i}R^{i}\Omega_{i+1}$$

- Angular velocity of frame $\{i+1\}$ measured (differentiate) in frame $\{i\}$ and represented (expressed) in frame $\{i+1\}$
- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (angular velocity) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the i+1 joint axis such that the two are coincide (rotations of a link is preformed only along its Z- axis) we can rewrite this term as follows:







Velocity of Adjacent Links - Angular Velocity 5/5

• The result is a <u>recursive equation</u> that shows the angular velocity of one link in terms of the angular velocity of the previous link plus the relative motion of the two links.

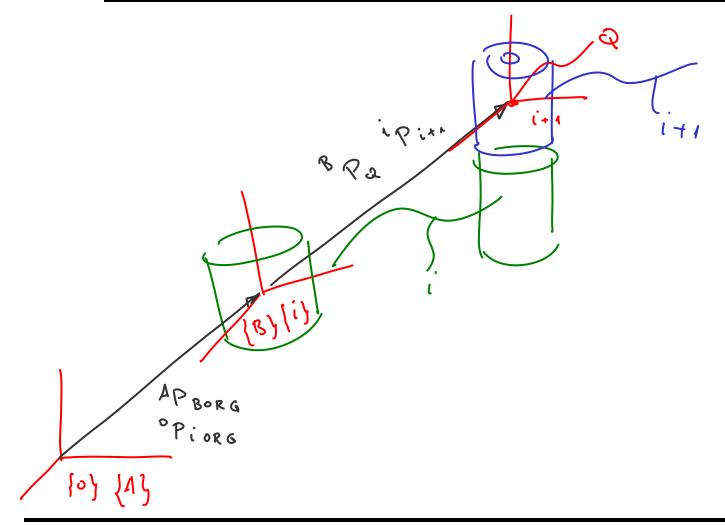
$$^{i+1}\omega_{i+1}=^{i+1}_{i}R^{i}\omega_{i}+\begin{bmatrix}0\\0\\\dot{ heta}_{i+1}\end{bmatrix}$$

• Since the term $^{i+1}\omega_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.





Velocity of Adjacent Links - Linear Velocity 0/6







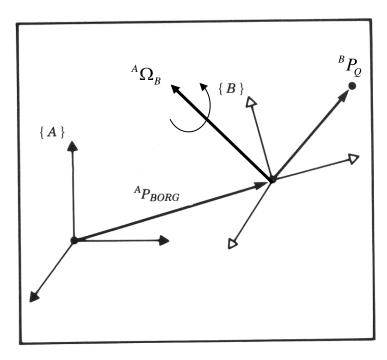
Velocity of Adjacent Links - Linear Velocity 1/6

- Simultaneous Linear and Rotational Velocity
- The derivative of a vector in a moving frame (linear and rotation velocities) as seen from a stationary frame
- Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

Matrix Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega} \left({}^{A}_{B}R^{B}P_{Q} \right)$$







Velocity of Adjacent Links - Linear Velocity 2/6

From the relationship developed previously (matrix form)

$$\longrightarrow {}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega} \left({}^{A}_{B}R^{B}P_{Q} \right)$$

• we re-assign link frames for adjacent links (i and i +1) with the velocity computed relative to the robot base frame $\{0\}$

$$\begin{cases}
A \to 0 \\
B \to i \\
C \to i+1
\end{cases}$$

$$\overset{\circ}{\longrightarrow} \overset{\circ}{V_{i+1}} = \overset{\circ}{i} \dot{R}_{\Omega} \begin{pmatrix} {}^{\circ}_{i} R^{i} P_{i+1} \end{pmatrix} + {}^{\circ}_{i} V_{i} + \overset{\circ}{i} R^{i} V_{i+1}$$

• By pre-multiplying both sides of the equation by ${}^{i+1}R$,we can convert the frame of reference for the left side to frame $\{i+1\}$





Velocity of Adjacent Links - Linear Velocity 3/6

Which simplifies to

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}\dot{R}_{\Omega} {}^{0}_{i}R^{i}P_{i+1} + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{i}R^{i}V_{i+1}$$

• Factoring out ${}^{i+1}_iR$ from the left side of the first two terms

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}V_{i+1}$$





Velocity of Adjacent Links - Linear Velocity 4/6

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}) + {}^{i+1}_{i}R^{i}V_{i+1}$$

 ${}^{i+1}_i R^i V_{i+1}$ - Linear velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$

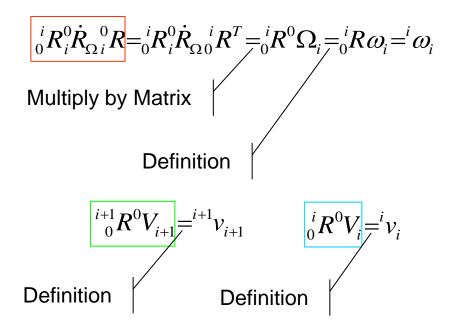
- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (angular velocity) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis
 pointing along the i+1 joint axis such that the two are coincide (translation of a
 link is preformed only along its Z- axis) we can rewrite this term as follows:

$$\begin{bmatrix}
 i^{i+1}R^{i}V_{i+1} = \begin{bmatrix}
 0 \\
 0 \\
 \dot{d}_{i+1}
 \end{bmatrix}$$





Velocity of Adjacent Links - Linear Velocity 5/6







Velocity of Adjacent Links - Linear Velocity 6/6

• The result is a <u>recursive equation</u> that shows the linear velocity of one link in terms of the previous link plus the relative motion of the two links.

• Since the term ${}^{i+1}\nu_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.





Velocity of Adjacent Links - Summary

Angular Velocity

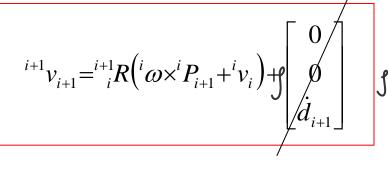
0 - Prismatjc Joint

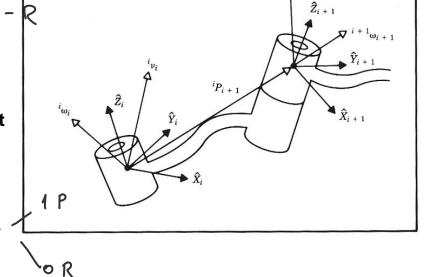
$$\omega_{i+1} = i+1 \atop i R^i \omega_i + 0 \atop \dot{\theta}_{i+1}$$

J 0-P

Linear Velocity

0 - Revolute Joint

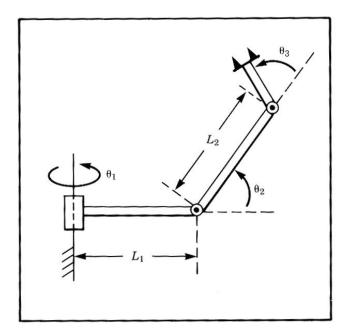








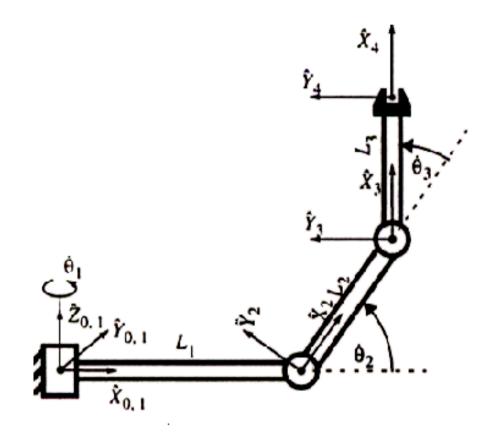
For the manipulator shown in the figure, compute the angular and linear velocity of the "tool" frame relative to the base frame expressed in the "tool" frame (that is, calculate ${}^4\omega_{_4}$ and ${}^4v_{_4}$).







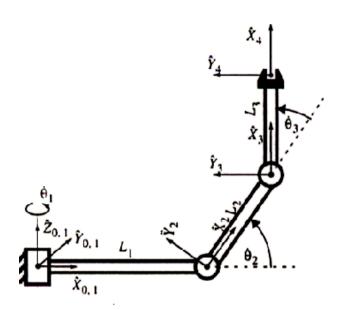
Frame attachment







DH Parameters



i	$lpha_{i-1}$	a_{i-1}	d_i	$ heta_{\scriptscriptstyle i}$
1	0	0	0	$\theta_{\scriptscriptstyle 1}$
2	90	L1	0	θ_2
3	0	L2	0	θ_3
4	0	L3	0	0





• From the DH parameter table, we can specify the homogeneous transform matrix for each adjacent link pair:





• Compute the angular velocity of the end effector frame relative to the base frame expressed at the end effector frame.

$$^{i+1}\omega_{i+1}=^{i+1}_{i}R^{i}\omega_{i}+\begin{bmatrix}0\\0\\\dot{ heta}_{i+1}\end{bmatrix}$$

$${}^{1}\omega_{1} = {}^{1}_{0}R^{0}\omega_{0} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} c1 & s1 & 0\\-s1 & c1 & 0\\0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix}$$





$${}^{2}\omega_{2} = {}^{2}R^{1}\omega_{1} + \begin{bmatrix} 0\\0\\\dot{\theta}_{2} \end{bmatrix} = \begin{bmatrix} c2&0&s2\\-s2&0&c2\\0&-1&0 \end{bmatrix} \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{2} \end{bmatrix} = \begin{bmatrix} s2\dot{\theta}_{1}\\c2\dot{\theta}_{1}\\\dot{\theta}_{2} \end{bmatrix}$$

• For
$$i=2$$

$${}^{3}\omega_{3} = {}^{3}R^{2}\omega_{2} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{3} \end{bmatrix} = \begin{bmatrix} c3 & s3 & 0 \\ -s3 & c3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} s2\theta_{1} \\ c2\dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{3} \end{bmatrix} = \begin{bmatrix} s23\theta_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix}$$

$${}^{4}\omega_{4} = {}^{4}_{3}R^{3}\omega_{3} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} s23\theta_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} s23\theta_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix}$$

$$^{3}\omega_{3}=^{4}\omega_{4}$$



- Compute the linear velocity of the end effector frame relative to the base frame expressed at the end effector frame.
- Note that the term involving the prismatic joint has been dropped from the equation (it is equal to zero).

$$v_{i+1} = {i+1 \choose i} R(i\omega \times i P_{i+1} + iv_i) + \begin{bmatrix} 0 \\ 0 \\ \dot{d}_{i+1} \end{bmatrix}$$





• For i=0

$${}^{1}v_{1} = {}^{1}R \left\{ {}^{0}\omega_{0} \times {}^{0}P_{1} + {}^{0}v_{0} \right\} = \begin{bmatrix} c1 & s1 & 0 \\ -s1 & c1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$${}^{2}v_{2} = {}^{2}R \left\{ {}^{1}\omega_{1} \times {}^{1}P_{2} + {}^{1}v_{1} \right\} = \begin{bmatrix} c2 & 0 & s2 \\ -s2 & 0 & c2 \\ 0 & -1 & 0 \end{bmatrix} \left\{ \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{1} \end{bmatrix} \times \begin{bmatrix} L1 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ -L_{1}\dot{\theta}_{1} \end{bmatrix}$$









$${}^{4}v_{4} = {}^{4}R \left\{ {}^{3}\omega_{3} \times {}^{3}P_{4} + {}^{3}v_{3} \right\} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s23\dot{\theta}_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix} \times \begin{bmatrix} L3 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} L2s3\dot{\theta}_{2} \\ L2c3\dot{\theta}_{2} \\ (-L1-L2c2)\dot{\theta}_{1} \end{bmatrix} \right\}$$

$$= \begin{bmatrix} L2s3\dot{\theta}_{2} \\ (L2c3 + L3)\dot{\theta}_{2} + L3\dot{\theta}_{3} \\ (-L1 - L2c2 - L3c23)\dot{\theta}_{1} \end{bmatrix}$$





- Note that the linear and angular velocities (${}^4\omega_4, {}^4v_4$) of the end effector where differentiate (measured) in frame {0} however represented (expressed) in frame {4}
- In the car example: Observer sitting in the "Car" $\begin{bmatrix} ^C [^W V_C] \end{bmatrix}$ Observer sitting in the "World" $\begin{bmatrix} ^W V_C \end{bmatrix}$

$${}^{k}v_{i} \equiv {}^{k} \left[{}^{0}V_{i} \right] = {}^{k}R \left[{}^{0}V_{i} \right] = {}^{k}R \cdot v_{i}$$

$${}^{k}\omega_{i} \equiv {}^{k} \left[{}^{0}\Omega_{i}\right] = {}^{k}R\left[{}^{0}\Omega_{i}\right] = {}^{k}R \cdot \omega_{i}$$

Solve for v_4 and ω_4 by multiply both side of the questions from the left by ${}_0^4R^{-1}$

$$^4V_4 = {}_0^4R \cdot V_4$$

$${}^4\omega_4 = {}^4R \cdot \omega_4$$





 Multiply both sides of the equation by the inverse transformation matrix, we finally get the linear and angular velocities expressed and measured in the stationary frame {0}

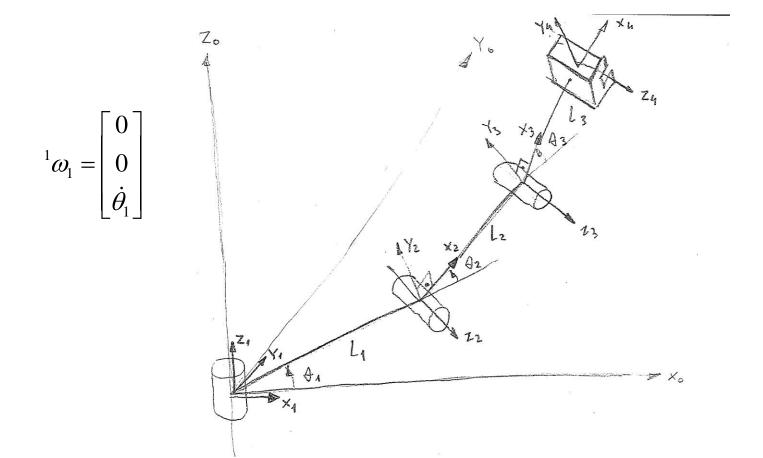
$$v_{4} = {}_{0}^{4}R^{-1} \cdot {}_{4}^{4} v_{4} = {}_{0}^{4}R^{T} \cdot {}_{4}^{4} v_{4} = {}_{0}^{0}R \cdot {}_{4}^{4} v_{4}$$

$$\omega_{4} = {}_{0}^{4}R^{-1} \cdot {}_{4}^{4} \omega_{4} = {}_{0}^{4}R^{T} \cdot {}_{4}^{4} \omega_{4} = {}_{0}^{0}R \cdot {}_{4}^{4} \omega_{4}$$

$${}_{4}^{0}T = {}_{1}^{0}T {}_{2}^{1}T {}_{3}^{2}T {}_{4}^{3}T$$

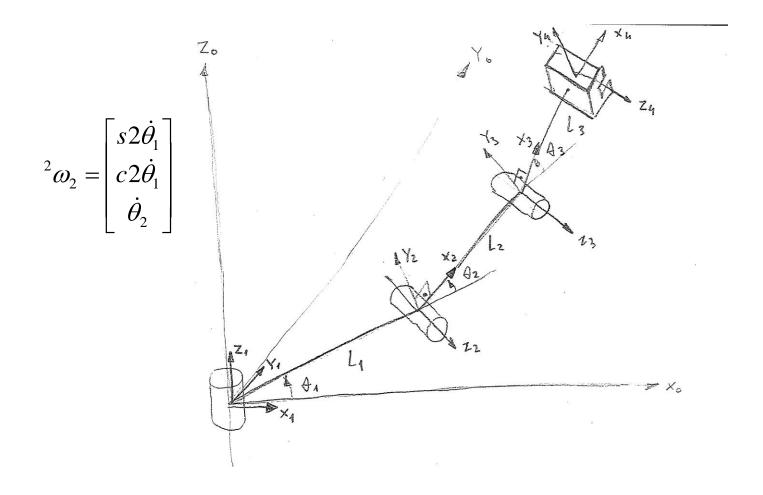






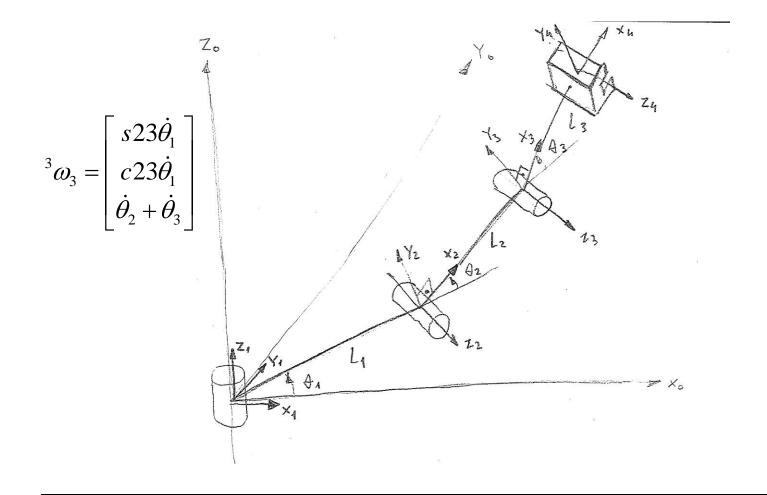








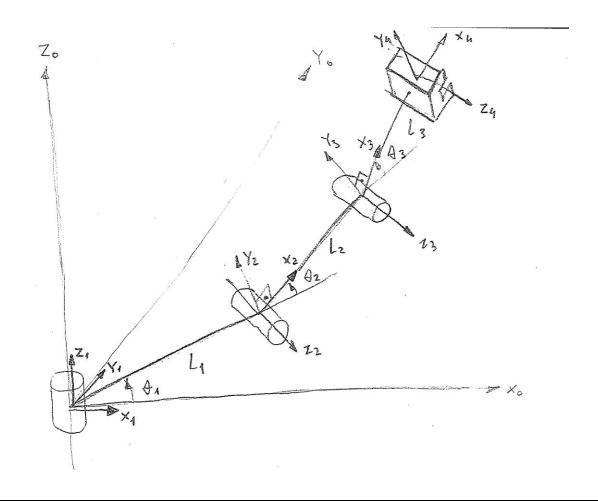




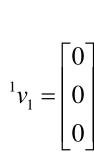


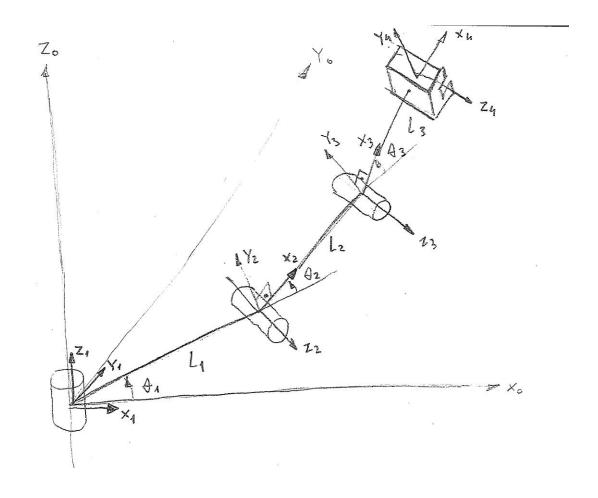






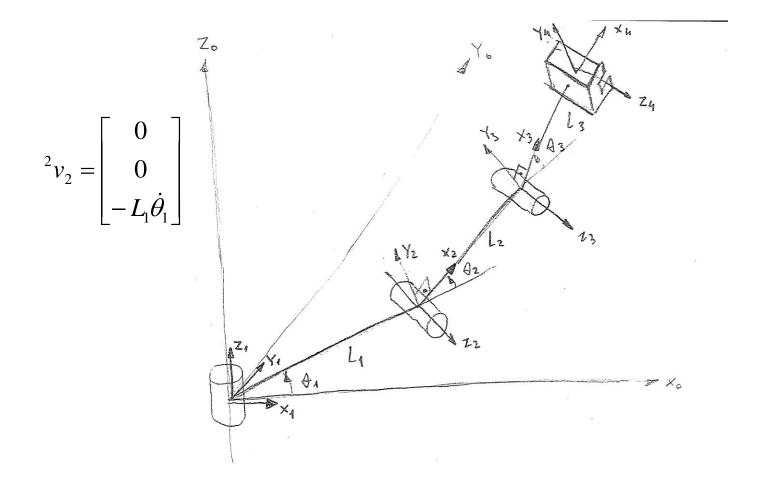






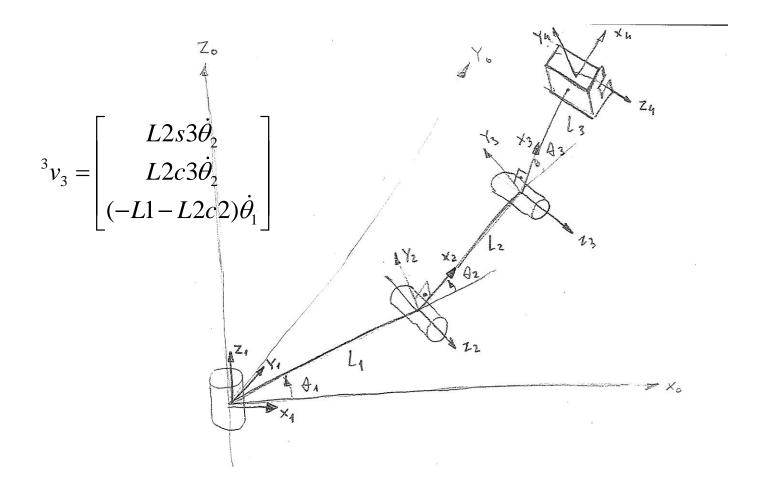






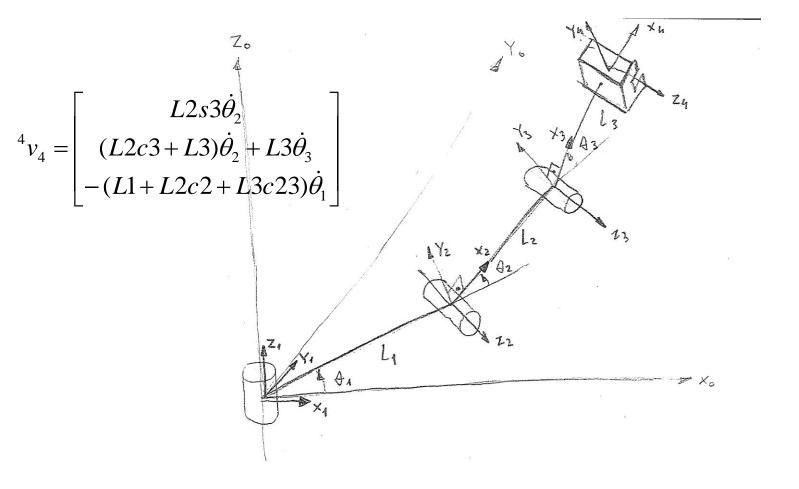






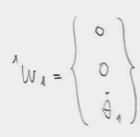


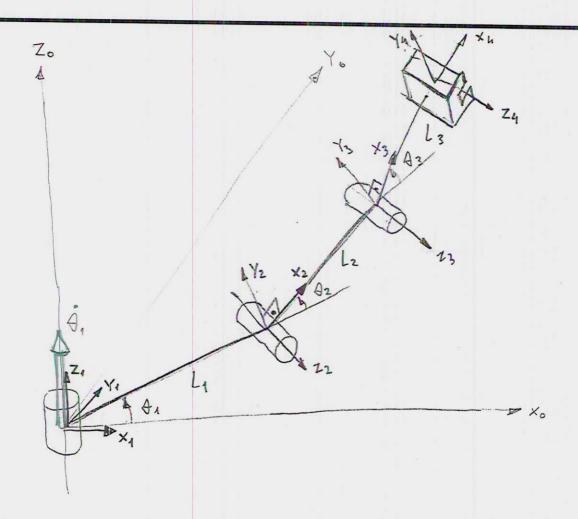




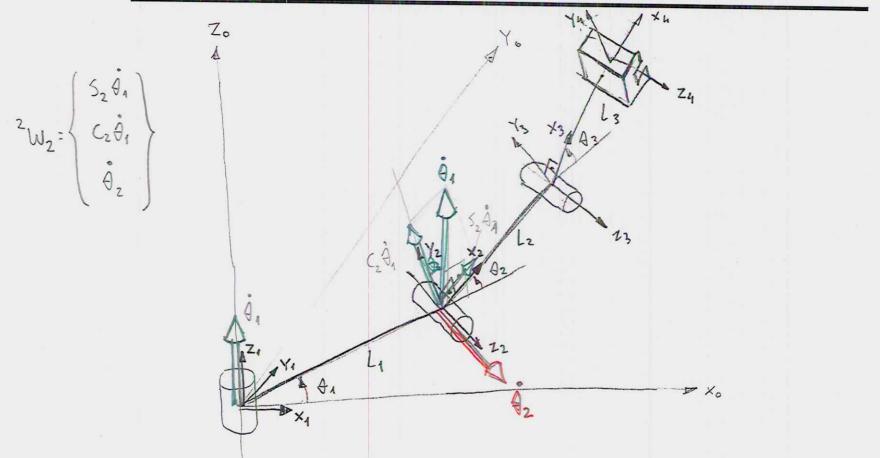




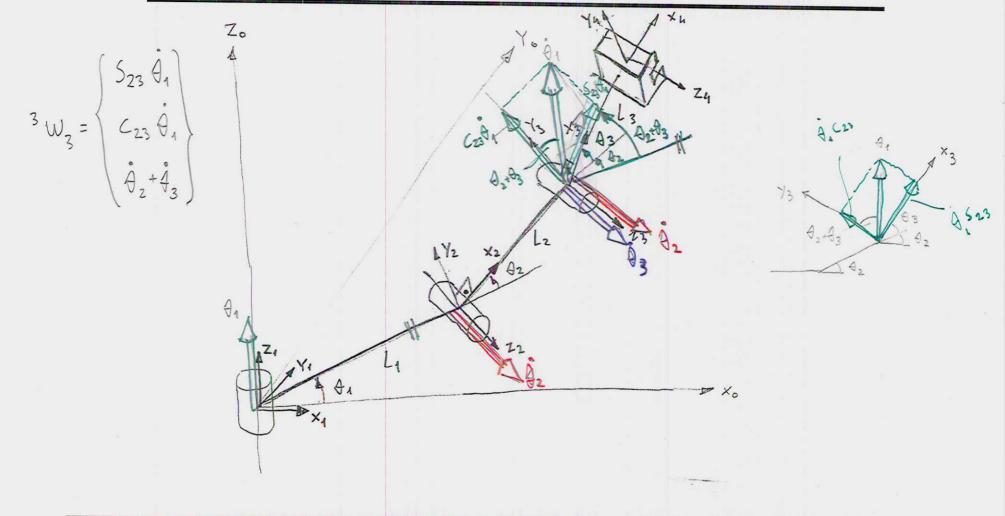




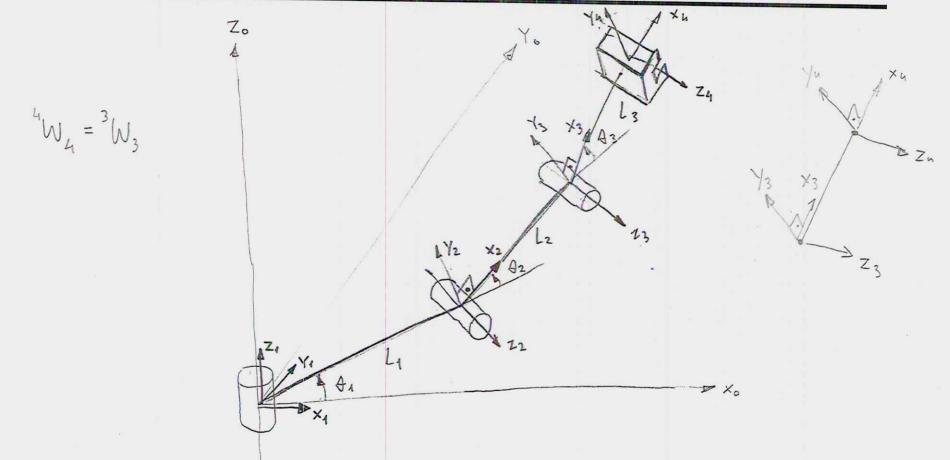




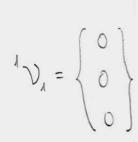


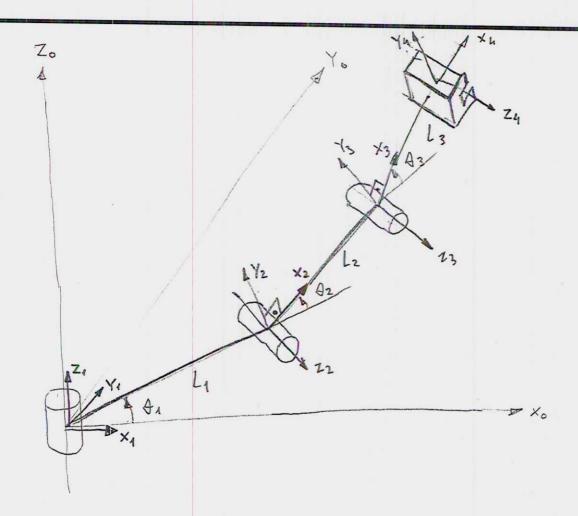




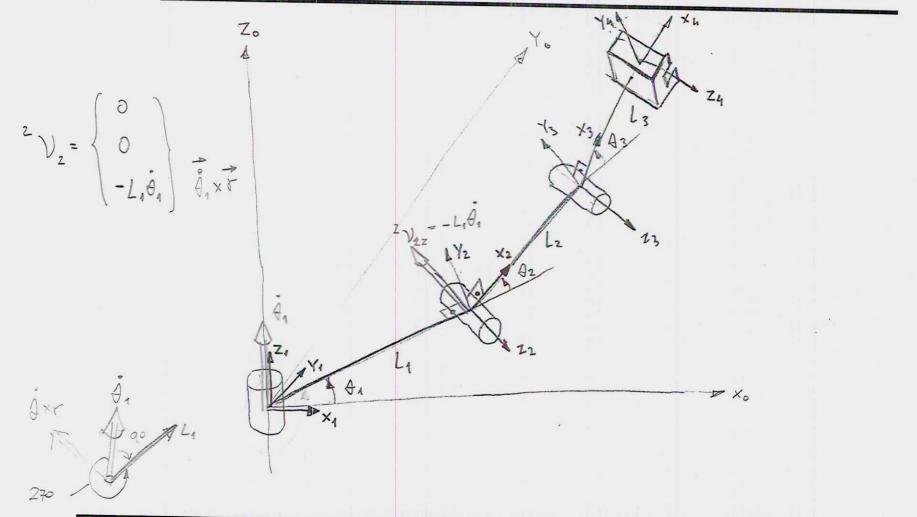




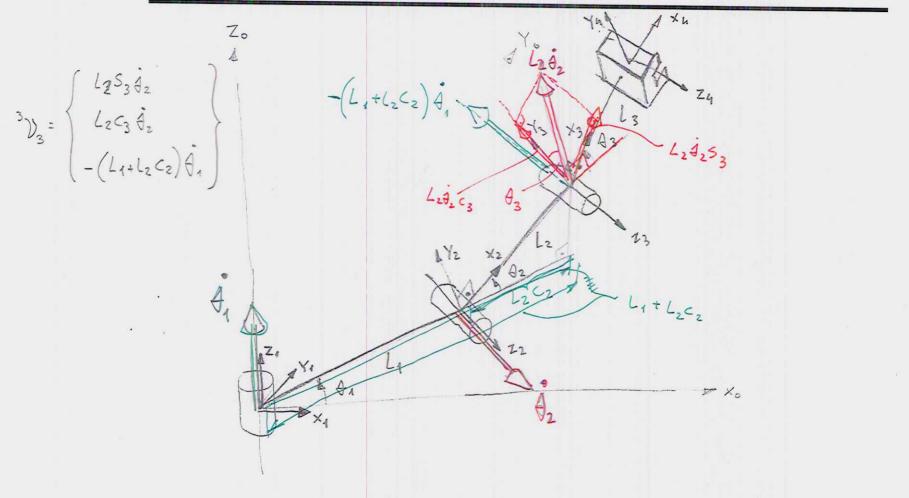














Az (L2 C3 + L3)

