

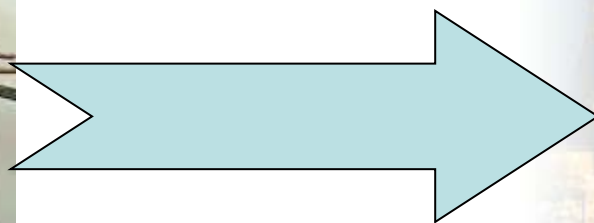
# ***VISI MIX – PRODUCTIVITY TOOL FOR THE ANALYSIS, SCALE-UP AND DESIGN OF MIXING PROCESSES IN STIRRED TANKS***

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Victor Atiemo-Obeng, Hua Bai, Richard Cope, The Dow Chemical Company  
Cesar Gonzalez, Styron LLC

VisiMix International Conference  
Boston, MA  
July 13-15th 2011

# PROCESS DEVELOPMENT & SCALE-UP



# PROCESS DEVELOPMENT & SCALE-UP

## Engineer/ Chemist Interface Opportunities

- Reaction Chemistry
- Technology Development
- Minimum Scale Up Issues
- **Mixing Phenomena**
- Heat Transfer/ Heat of Reaction
- Kinetic Modeling
- Particle Formation and Control
- Distillation/ Recycle/ Purification
- Liquid/ Liquid (Phase) Separation
- Solid/ Liquid Separation

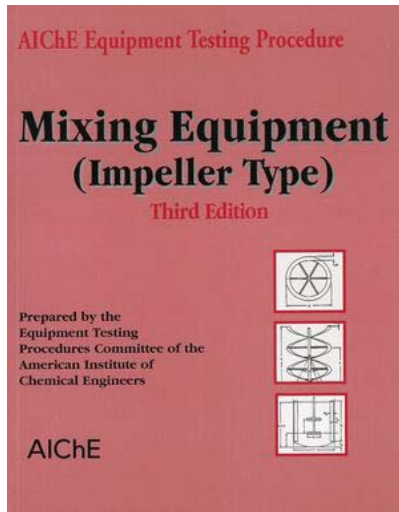
# IMPORTANT LESSON FOR PROCESS DEVELOPMENT

## Early assessment of effect of mixing on process

- Opportunity is higher to
  - influence process decisions
  - avoid /prevent process scale-up problems !!
  - achieve process goals
- Cost to make changes is lower



# RESOURCES



**Dickey, D., et al (2001) AIChE Equipment Testing Procedure - Mixing Equipment (Impeller Type), 3rd Edition**





# Key Steps in Process / Mixing Consulting & Problem Solving

**Define the correct problem to be solved**

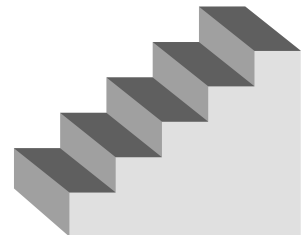
- Establish mixing objective/**desired process result**

**Perform analysis**

- **Determine required hydrodynamic environment and operating conditions, relevant physicochemical phenomena and controlling parameters necessary for process success**
- **Confirm with basic calculations, experiments and/or modeling**

**Recommend / select equipment and/or operating conditions to achieve process result**

**Ascertain reliability of mechanical design**



# MIXING PROCESSES: KEY VARIABLES TO EXPLORE

## Effects of

- impeller geometry (type, size, etc.)
- impeller speed (rpm)
- feed location (sub-surface, near impeller)
- feed time in semi-batch
- feed concentration
- temperature
- fluid viscosity
- Etc.

# Mixing Problem Solving

## Process engineer asks-

- What kind of mixer?
- Which impeller type?
- How many impellers?
- What's impeller speed?
- What's motor horsepower?
- What's size of gear box?
- Etc.

Good questions but ...





## Key questions for process development



What is success for the desired process?

How does mixing affect the desired process?

What kind of mixing will achieve success for process?

What kind of mixing will hurt the process?

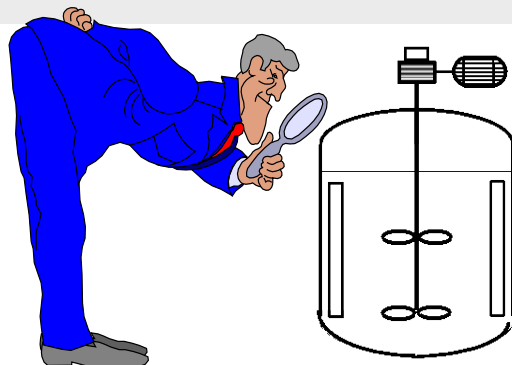
When and why is it important?

What measures characterize the effects?

How important are the effects on the process?

What equipment design and/or operations will produce the desired process result?

# NEED FOR MIXING PRODUCTIVITY TOOL



Effective capture and use knowledge of

- mixing phenomena
- fluid mechanics
- characteristics of mixing equipment, etc.

at different levels of sophistication

to quickly analyze, scale-up, design, troubleshoot mixing processes in stirred tanks.

## RELEVANCE OF



## *MIXING ASPECTS COVERED:*

*Hydrodynamics*

*Turbulence*

*Single phase Mixing (Blending & Reaction)*

*Batch, Semi-Batch, Continuous*

*Liquid-Solid mixing*

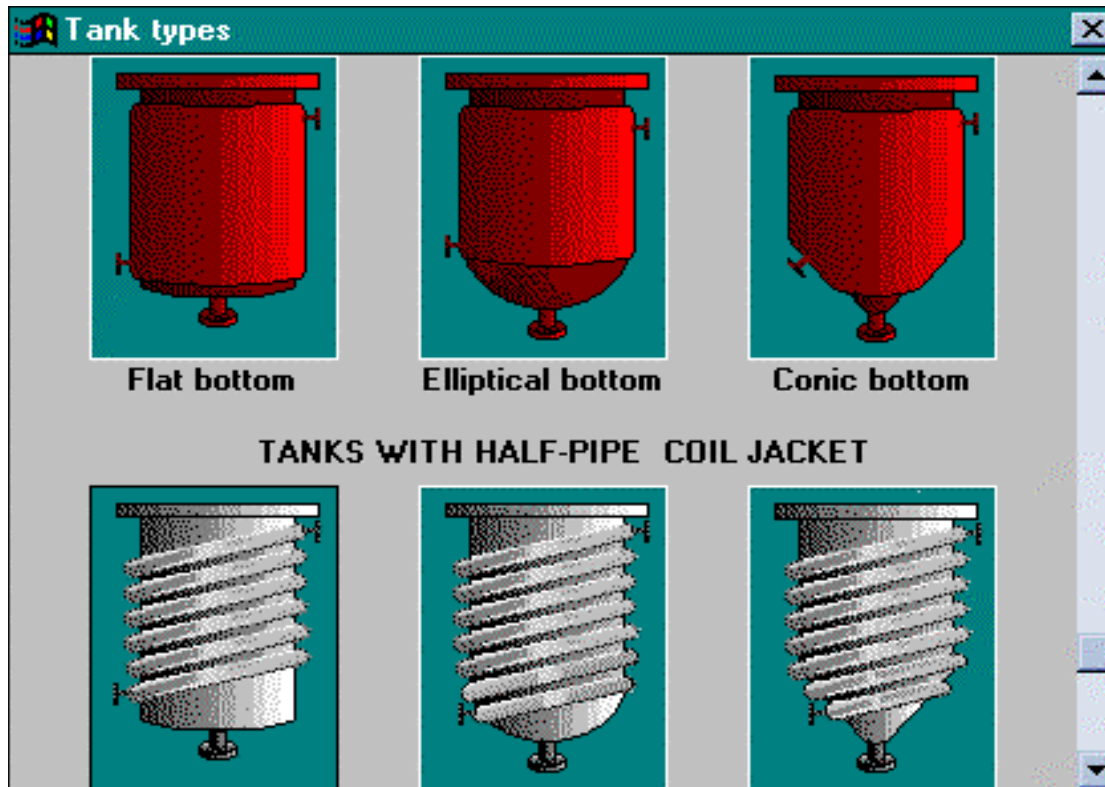
*Liquid-liquid mixing (liquid dispersion)*

*Liquid-gas mixing (gas dispersion)*

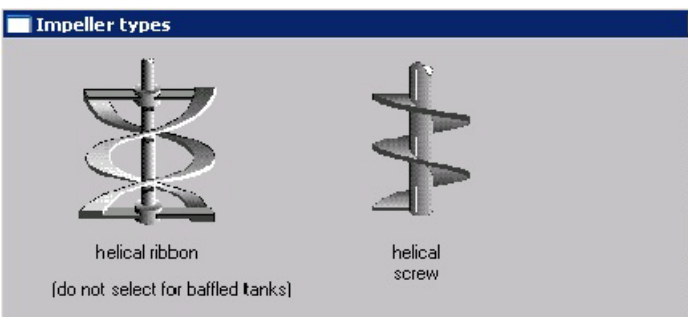
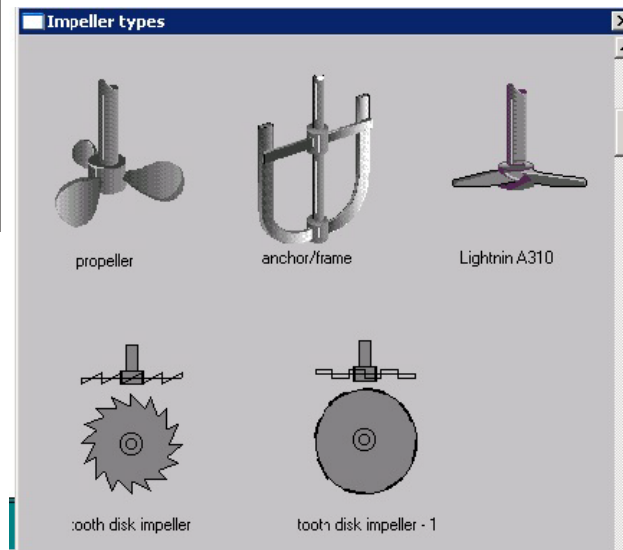
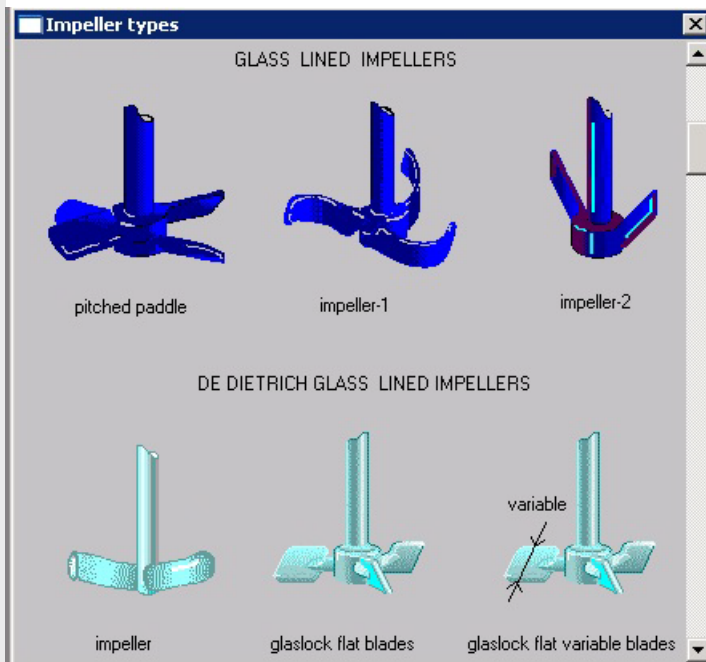
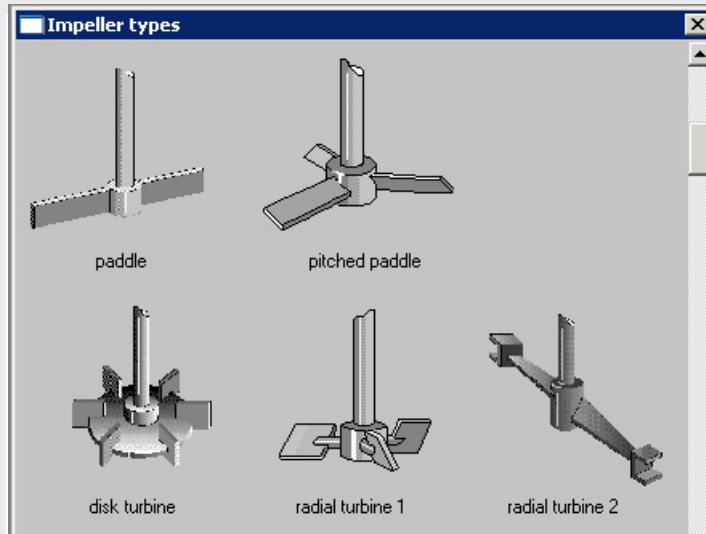
*Heat Transfer*

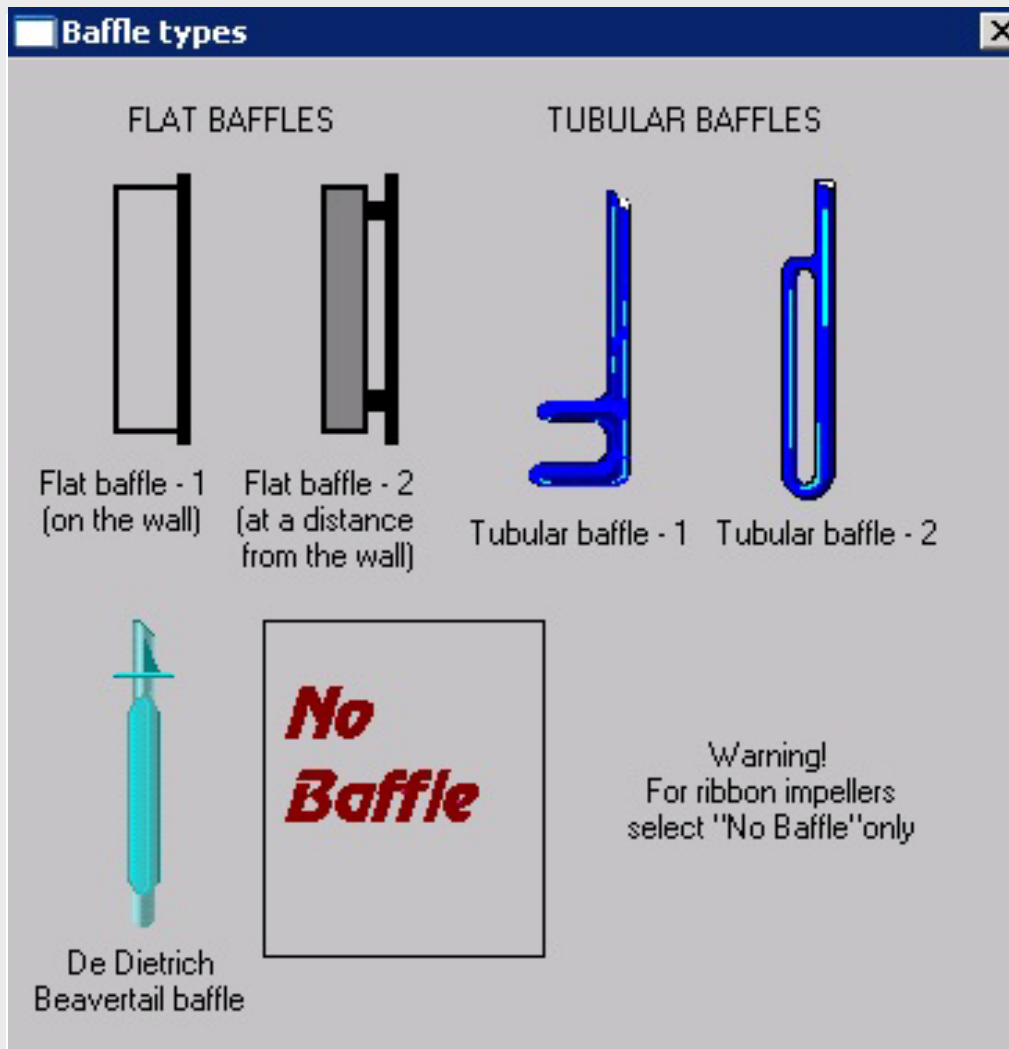
*Mass Transfer in Liquid-solid systems*

*Mechanical Calculation of Shaft*



# VISI MIX IMPELLERS





# RELEVANCE OF VisiMix

- Broad Range of Stirred Tank Mixing Problems
- Wide Variety of Impellers, Vessels and Baffles
- Scale/size
  - Lab, pilot, plant scale
- Hydrodynamic regimes
  - VisiMix Turbulent for flow Reynolds Number  $>1500$
  - VisiMix Laminar for flow Reynolds Number  $< 1500$



# ACCESSIBILITY OF



# ACCESSIBILITY

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## TANK WITH ELLIPTICAL BOTTOM

Inside diameter	1800	mm
		m
		ft
Total tank height	2100	mm
		micron
		in
Total volume	4962	l
Level of media	1525	mm
Volume of media	3499	l

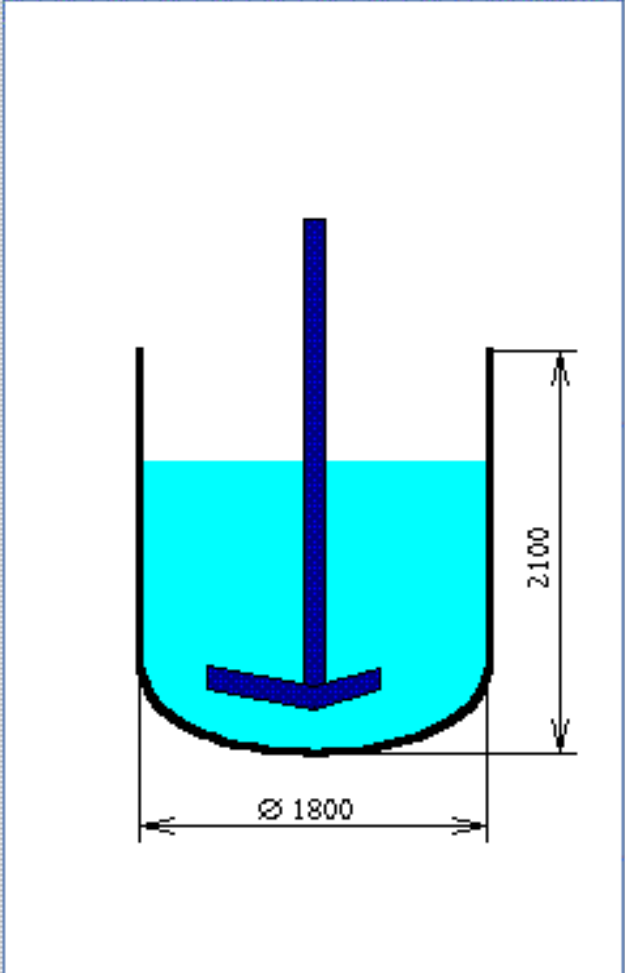
OK Cancel Choose new tank Print Help

## ACCESSIBILITY

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**PFAUDLER-2**

Tip diameter	<input type="text" value="1100"/>	mm
Number of blades	<input type="text" value="3"/>	
Width of blade	<input type="text" value="110"/>	mm
Dist. from bottom	<input type="text" value="275"/>	mm
Number of revolutions	<input type="text" value="100"/>	Rpm
Power of drive	<input type="text" value="1500"/>	W



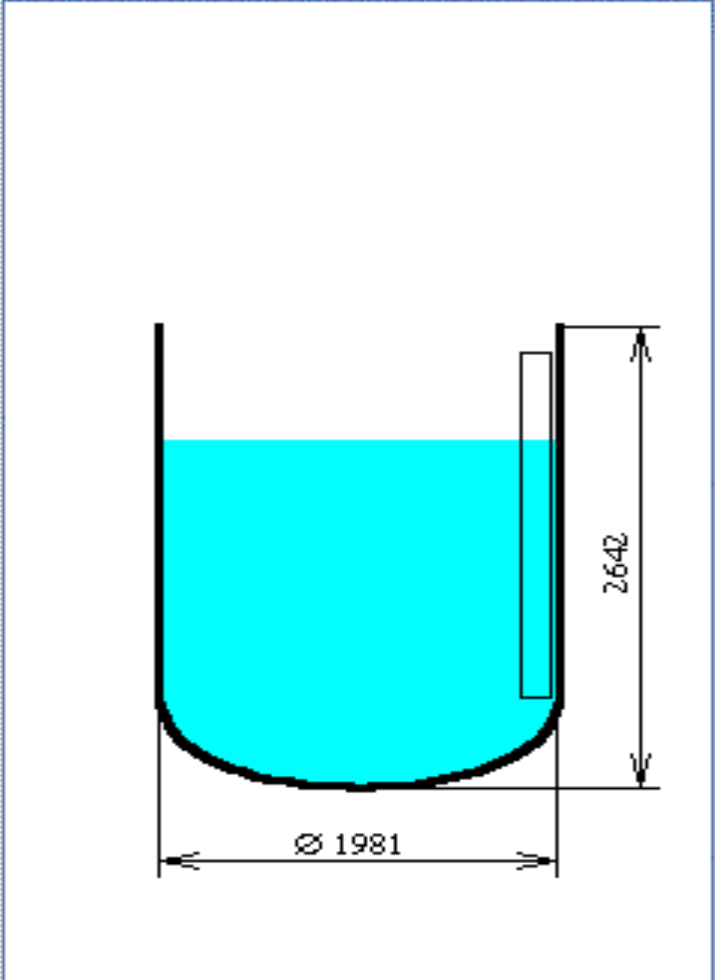
OK Cancel Choose new agitator Print Help

# ACCESSIBILITY

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## FLAT BAFFLE-2

Number	<input type="text" value="4"/>
Width	<input type="text" value="152.4"/> <input type="text" value="mm"/>
Length	<input type="text" value="1981"/> <input type="text" value="mm"/>
Dist. from bottom	<input type="text" value="508"/> <input type="text" value="mm"/>
Dist. from wall	<input type="text" value="25.4"/> <input type="text" value="mm"/>
Angle to radius	<input type="text" value="0"/> <input type="text" value="deg"/>



OK Cancel Choose new baffle Print Help

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## AVERAGE PROPERTIES OF MEDIA

Type of media

☒ Newtonian
 ☐ Non-Newtonian

Average density  kg/cub.m

Dynamic viscosity  Pa\*s

Kinematic viscosity  sq.m/s

Constant K  Pa\*(sec)<sup>1-m</sup>

Exponent m

Behavior of Non-Newtonian media is approximated with the functions:

$$\tau = K * \dot{\gamma}^{1-m}$$

$$\mu = K * \dot{\gamma}^{-m}$$

where  $\mu$  - dynamic viscosity, Pa\*sec;  
 $\dot{\gamma}$  - shear rate, 1/sec;  
 $\tau$  - shear stress, Pa.

## ACCESSIBILITY

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**PROPERTIES OF SOLID AND LIQUID PHASES.**

Density of liquid phase	<input type="text" value="1000"/>	<input type="text" value="kg/cub.m"/>
Dyn. viscosity of cont. phase	<input type="text" value="0.001"/>	<input type="text" value="Pa*s"/>
Concentration of solid phase	<input type="text" value="150"/>	<input type="text" value="kg/cub.m"/>
Density of solid phase	<input type="text" value="2500"/>	<input type="text" value="kg/cub.m"/>
Average particle size	<input type="text" value="80"/>	<input type="text" value="micron"/>
Size of largest particles *	<input type="text" value="300"/>	<input type="text" value="micron"/>
Position of outlet-height	<input type="text" value="0"/>	<input type="text" value="mm"/>

\* signifificant fraction - 5% of solid phase

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## PROPERTIES OF CONTINUOUS AND DISPERSE LIQUID PHASES.

## Continuous phase

Density

1150

kg/cub.m

Dynamic viscosity

0.001

Pa\*s

Interfacial  
surface tension

0.03

N/m

## Disperse phase

Volume fraction

0.12

Density

950

kg/cub.m

Dynamic viscosity

0.016

Pa\*s

Index of admixtures

-0.1

-1 - -0.5 - coagulants (de-emulsifiers)  
-0.5 - -0.1 - 2- and 3-valent ions of electrolytes  
-0.1 - 0.1 - no significant admixtures  
(pure oil - water)  
0.1 - 0.25 - electrolytes  
0.25 - 0.5 - small quantities of detergents  
0.5 - 1 - detergents, emulsifiers

OK

Cancel

Print

Help

## ACCESSIBILITY

E:\PROGRA~1\VISIMIX\VISIMIX3\DEM2.VSM

SINGLE PHASE BLENDING AND REACTORS.  
HOMOGENEOUS CHEMICAL REACTION

## MAIN REACTION



Reactant A charged initially to the tank

## SIDE REACTION

Side reaction is assumed to be slow  
compared to the main reaction

Specific reaction rate

for BLENDING - enter 0 (zero)  
for FAST reaction - enter F I/(mol\*sec)Reaction type Init. concentration of  
reactant A mol/literRelation of loads -  
B[mol]/A[mol]Specific  
reaction rate I/(mol\*sec)

OK

Cancel

Print

Help



# ACCESSIBILITY OF



INTERFACE: Simple, Intuitive, Context-Relevant Interface

- Input data: equipment dimensions, fluid properties, process or operational parameters
- SI or US Customary Units
- Fast Solver
- Values of Relevant Hydrodynamic, Turbulent and other Mixing parameters returned
- **Desired process result IS NOT an Input**

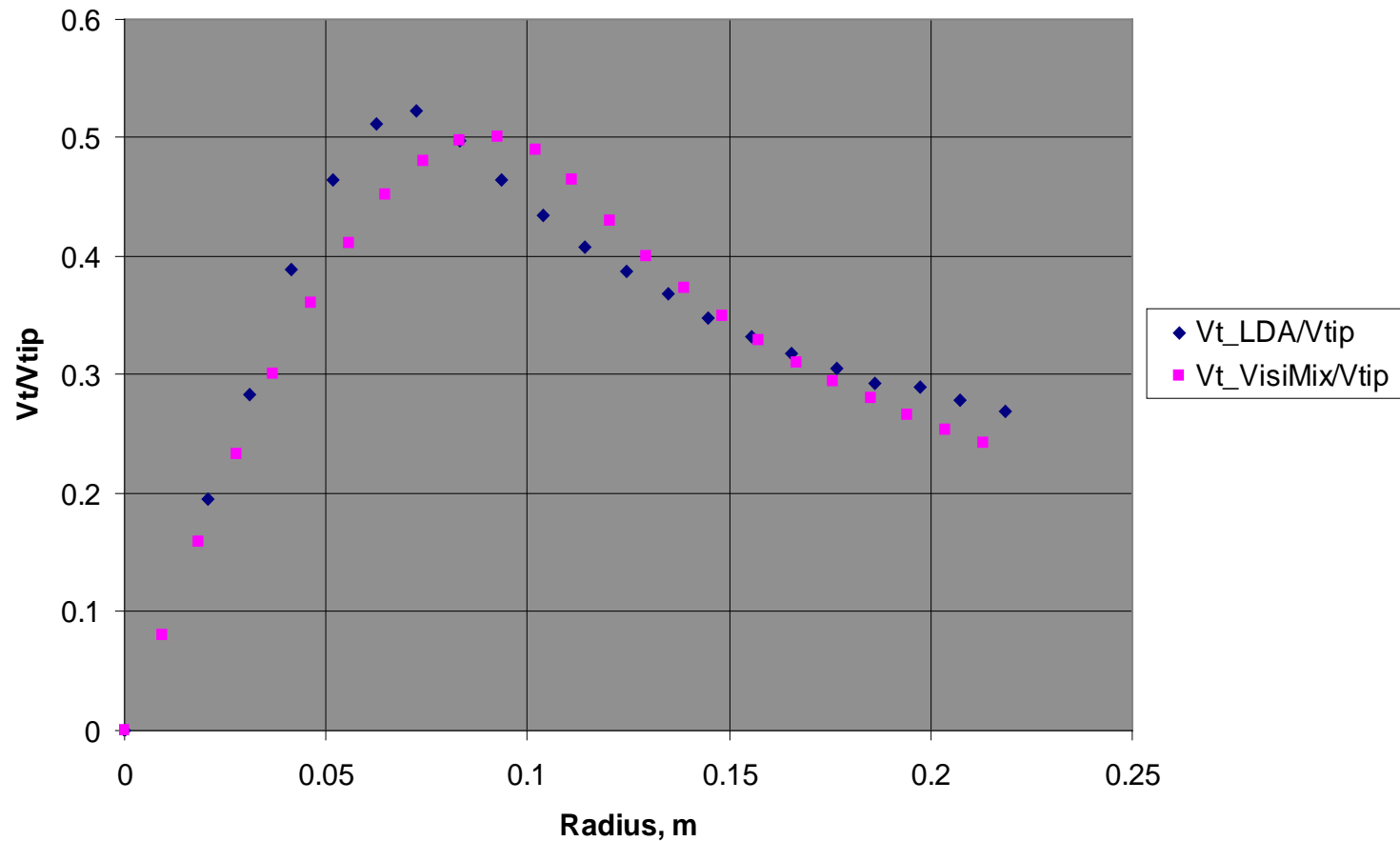
# RELIABILITY OF



- Comparison with
  - data
  - established correlations
- Magnitude as well as functional dependence on key properties and parameters

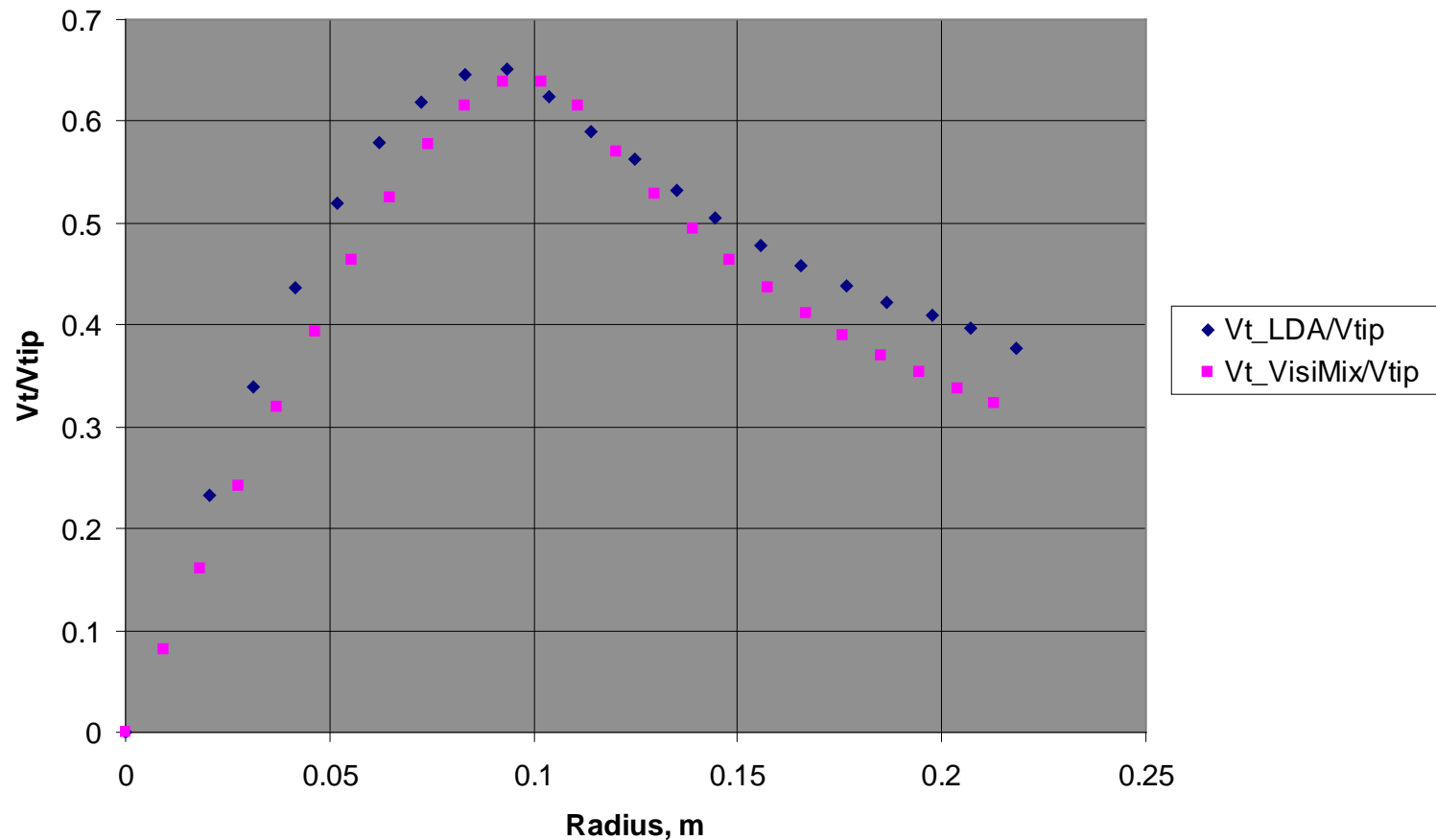
## Radial Distribution of mean tangential velocity PBT4-9" @ 150 rpm in unbaffled vessel

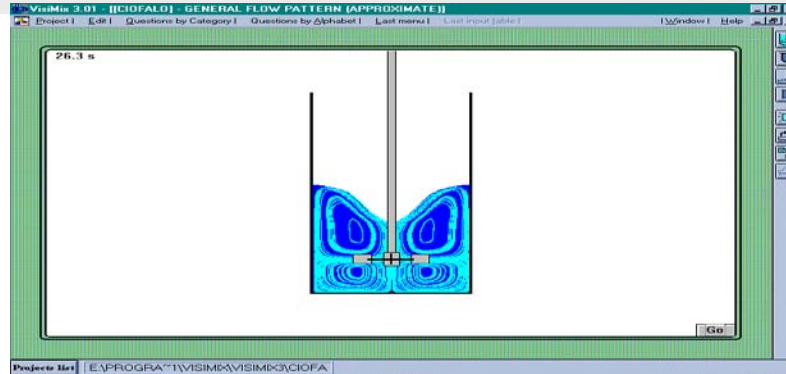
LDA Data by S.P. Wood & K. Barton, 1993



## Radial Distribution of mean tangential velocity DT6-9" @ 150 rpm in unbaffled vessel

LDA Data by S.P. Wood & K. Barton, 1993





Ref.: Ciofalo, M. et al (1996) "Turbulent flow in Closed and Free-surface Unbaffled Tanks Stirred by Radial Impellers", Chem. Eng. Sci. 51 (14), pp 3557-3573.

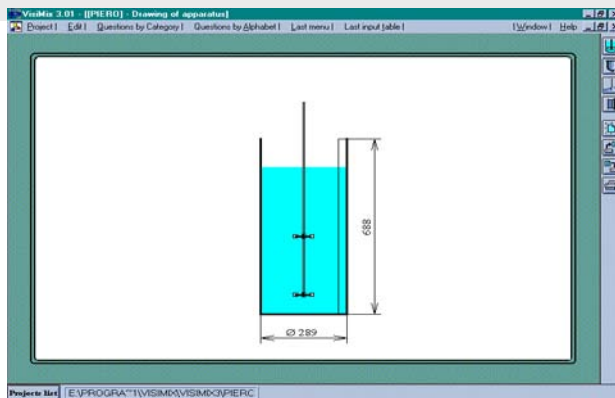
	Measured data	VisiMix Results
Vortex Depth @ 139 rpm, m	0.026	0.024
Vortex Depth @ 194 rpm, m	0.047	0.047
Vortex Depth @ 240 rpm, m	0.073	0.073

System: Water

$T=78$  in,  $H=T$ ,  $D=T/3$ ,  $C=T/3$ , 4 Std. Baffles,  $N=125$

	<u>RDT</u>	<u>PBT</u>	<u>A310</u>
Power Number, $Po$	4.71 <b>5.2</b>	1.67 <b>1.31</b>	0.29 <b>0.3</b>
Ave. Specific Power, W/kg	0.78 <b>1.0</b>	0.28 <b>0.26</b>	0.06 <b>0.06</b>
Mixing time 99%, s	15 <b>23</b>	16 <b>36</b>	31 -

Note: Results calculated with correlations from BHRG-FMP in shaded bold italics



Ref.: Armenante, P. M. And Chang, G. (1998) "Power Consumption in Agitated Vessels Provided with Multiple Disk Turbines", Ind. Eng. Chem. Res. 37, pp.284-291.

Two Rushton turbines	Measured data	VisiMix Results
Power Number @ $S=D$	7.5	9.9
Power Number @ $S=3D$	9.6	10.8



Ref. Harrop et al (1997) "Impact of suspended solids on the homogenisation of the liquid phase under turbulent conditions in a stirred vessel", Proceedings of Mixing IX, Paris:

Recent Adv. in Mixing 11 (52), pp41-48

System: Water, T=720 mm, H=T, 4 Std. Baffles

A315, D/T=0.42, C=T/4

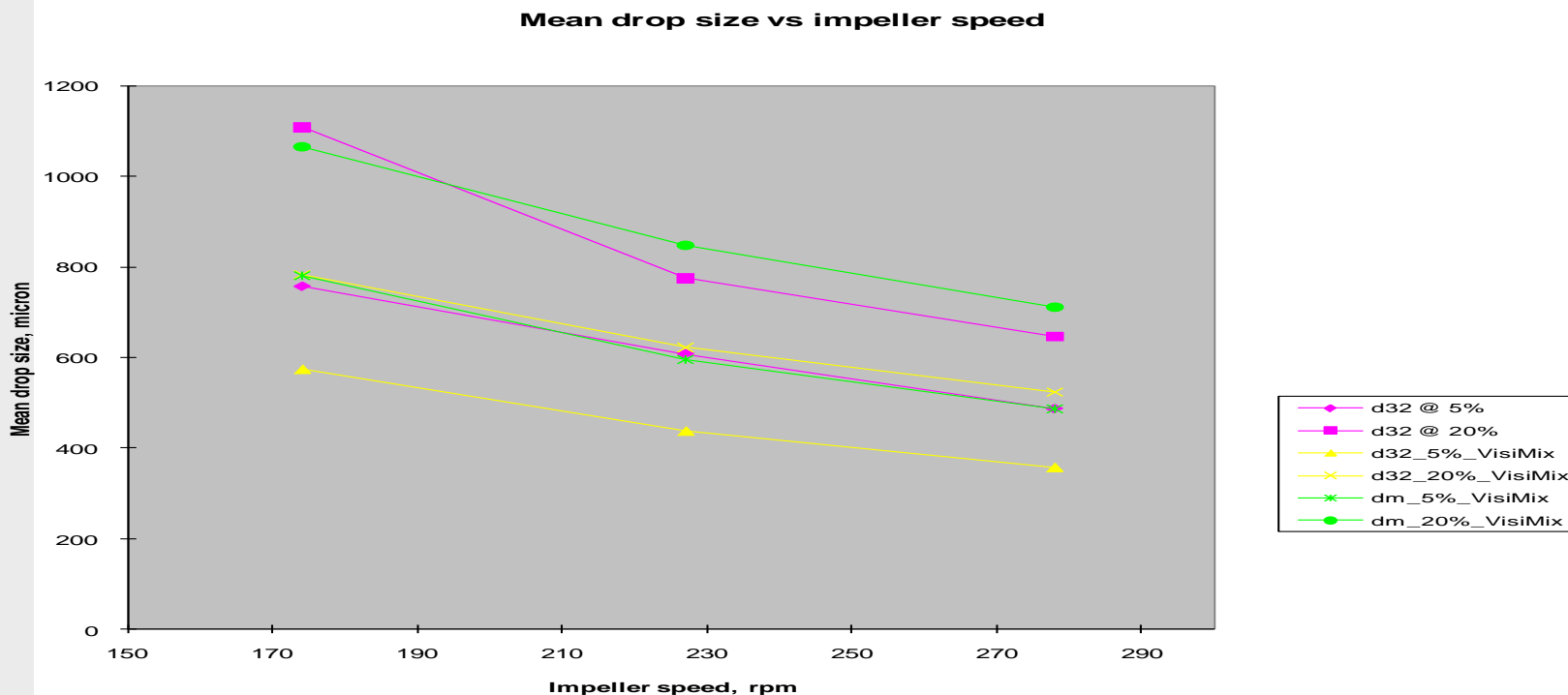
N, rpm	W/kg Expt.	W/kg VisiMix	Mixing time, s Conducti- vity	Mixing time, s Decolori- zation	Mixing time, s BHRG- FMP	Mixing time, s VisiMix
100	0.038	0.035	19.3	26.6	19.0	24.8
150	0.128	0.117	12.3	16.7	12.7	16.6
200	0.293	0.278	9.3	11.5	9.6	12.4
250	0.544	0.542	7.3	10.0	7.8	9.92
300	0.921	0.937	7.3	8.0	6.5	8.27
350	1.421	1.490	6.7	7.5	5.7	7.09
400	2.123	2.223	5.3	5.8	5.0	6.2

Note: VisiMix Results courtesy of Dr. Braginsky

Ref.: Ross, et al. (1978) "Droplet Breakage and Coalescence Processes in an Agitated Dispersion. 2. Measurement and Interpretation of Mixing Experiments", Ind. Eng. Chem. Fundam., 17 (2) pp 101-108

Liquid/Liquid: 39.1%v Dowtherm E, 61.9%v Shell No. 3747 Oil/Water Vessel: T=11.1 cm Impeller: RDT, D/T=0.46, C=T/3	Data	VisiMix Results	VisiMix Results
	$d_{32}$ $\mu\text{m}$	$d_{32}$ $\mu\text{m}$	$d_{\text{mean}}$ $\mu\text{m}$
@ 5.0 % (v) dispersed phase, N=174	758	781	574
@ 5.0 % (v) dispersed phase, N=227	608	596	438
@ 5.0 % (v) dispersed phase, N=278	486	486	358
@ 20.0 % (v) dispersed phase, N=174	1108	1065	783
@ 20.0 % (v) dispersed phase, N=227	775	847	622
@ 20.0 % (v) dispersed phase, N=278	646	711	523

Ref.: Ross, et al. (1978) "Droplet Breakage and Coalescence Processes in an Agitated Dispersion. 2. Measurement and Interpretation of Mixing Experiments", Ind. Eng. Chem. Fundam., 17 (2) pp 101-108

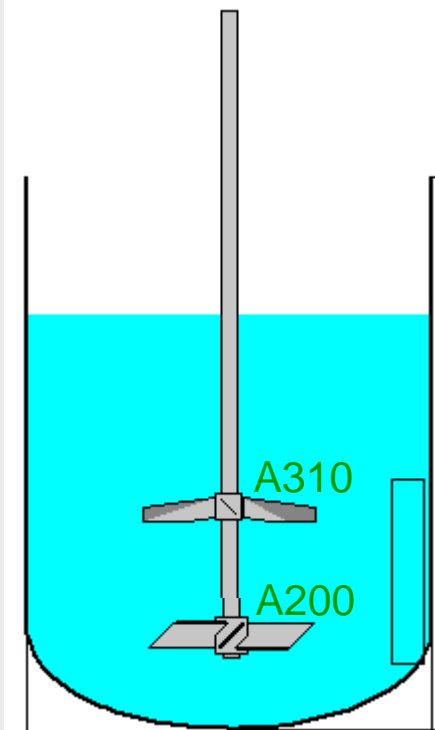


- Reasonable match with data or results from established correlations in several selected cases
- Acceptable trends in calculated values
- Some results deviate significantly from data and results from established correlations

# VISI MIX APPLICATION CASE #1

## Troubleshooting

Modified agitation setup to improve powder drawdown



### The problem:

- Poor mixing due to problem with powder drawdown

### Constraints:

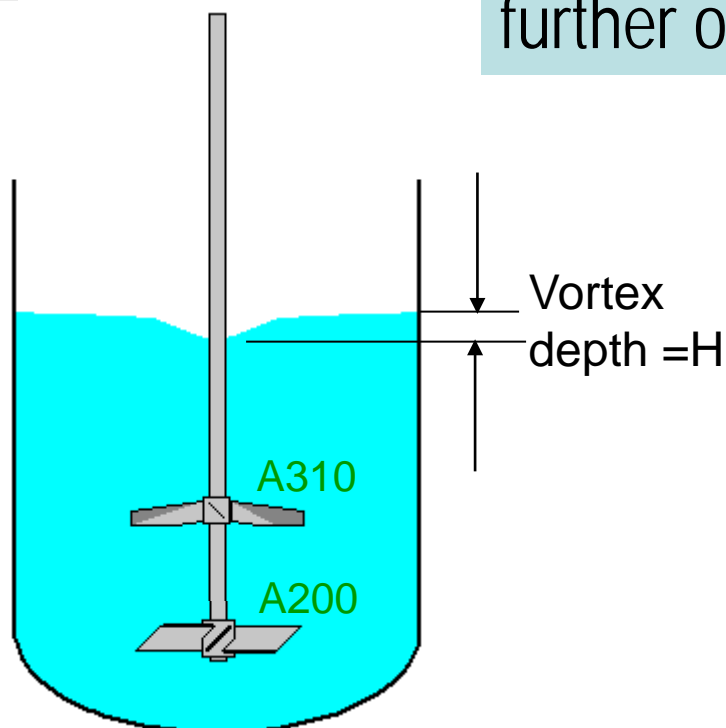
- Impeller already operated at maximum rotation speed (RPM)
- Solution required to avoid risks of powder attrition
- Air entrainment is undesired for process

### Process Loads:

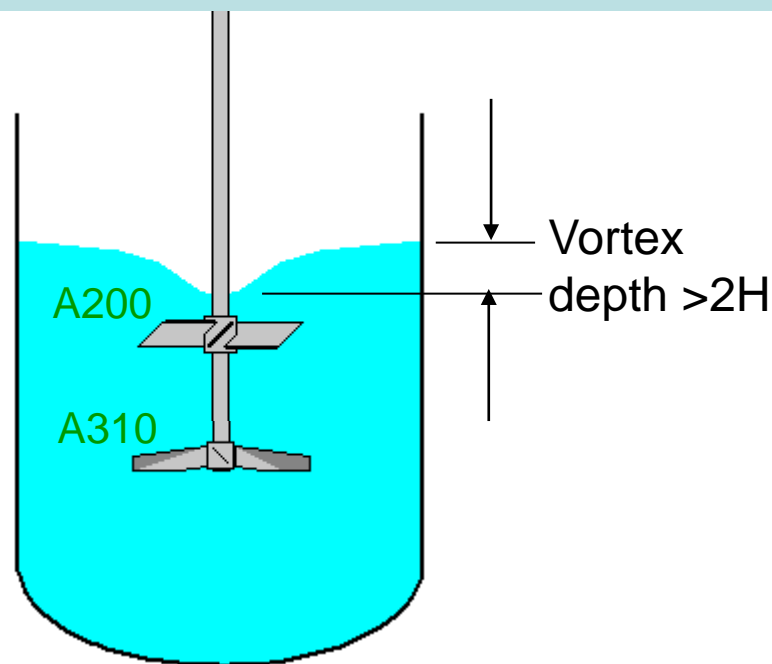
5200 gal liquid  
7400 lbs powder

# VISI MIX APPLICATION CASE #1

Modification ideas tested / evaluated and further optimized in VISIMIX



Previous setup



Modified setup

- Switch upper/lower impeller to let A200 (with much higher flow # than A310) at the top
- New positions of both impellers **optimized by VISIMIX** for maximum powder drawdown but without causing gas entrainment
- Maintain same shaft RPM to avoid risk of powder attrition
- **Implementation:** successful modification with almost zero capital

## Scale-up from lab to commercial production



Liquid volume: 700 cc

Liquid weight: 0.6 kg

**Problem definition:**

Scale up to the commercial production of 6000 kg per batch (10,000 times!!)

-- What reactor to choose?

choose from a few available/idle vessels & agitation systems to reduce capital

-- How to scale up agitation?

lab tests showed that the product quality was very sensitive to mixing or agitation. Too much or too little agitation would negatively affects product

-- What is the mixing time?

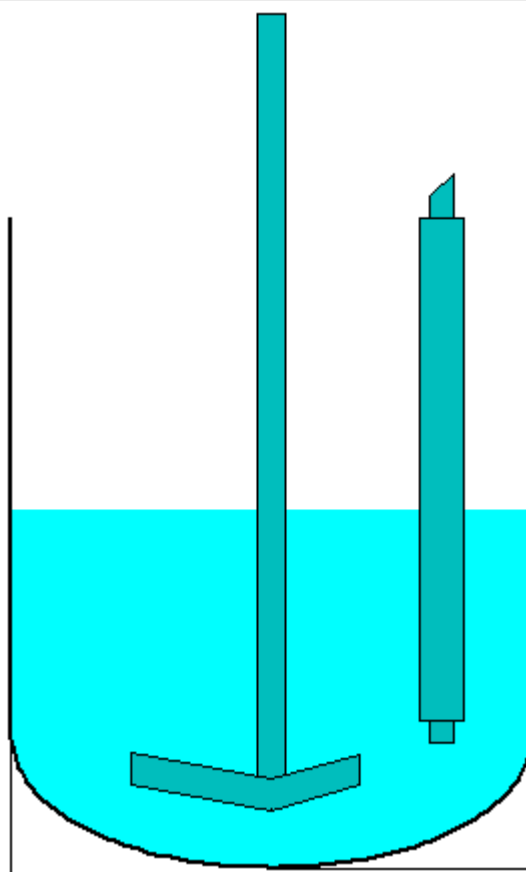
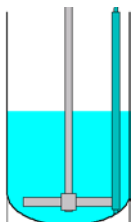
# VISI MIX APPLICATION CASE #2

Scale up by 10,000 times  
with VISIMIX

**Lab Reactor:**

Batch size: 700 cc

Batch weight: 0.6 kg



**Commercial production  
Reactor:**

Batch size: 7 m<sup>3</sup>

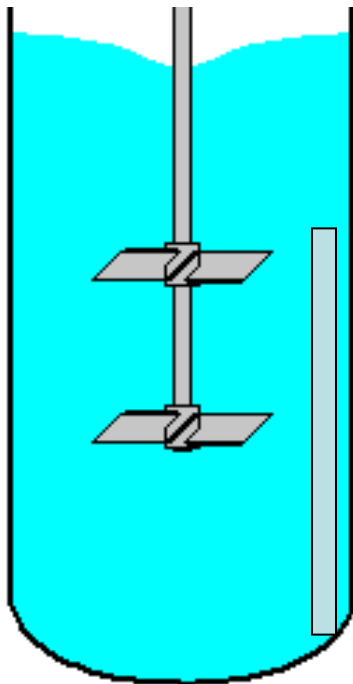
Batch weight: 6000 kg

**Scale-up by mixing power per unit mass:**

- Simulate the lab setup to obtain “mixing power per unit mass”
- Simulate the commercial production with available vessels and agitation systems, adjust the impeller speed to match the “mixing power per unit mass”
- Verify mixing time
- Successful scale-up implementation



## VISI MIX predicts surface vortex and exports to CFD



Liquid volume 18 m<sup>3</sup>  
Liquid level above baffles

Most CFD simulations of stirred tank ignore surface vortex

- flat surface assumed, usually OK for fully baffled tank

Surface vortex effect needs to be included in CFD *if*

- near-surface hydrodynamics is critical (e.g., powder drawdown)
- the tank is not fully baffled

Directly modeling the free surface in CFD significantly increases the complicity and cost of CFD simulations

- turn single-phase flow into 2-phase flow, or
- turn 2-phase flow into 3-phase flow,
- turn steady-state flow into transient flow simulation (sliding mesh)

Use VISIMIX to predict the free surface (surface vortex)

Export the free surface geometry into CFD which is used as the domain top boundary specified with "slippery-wall" condition

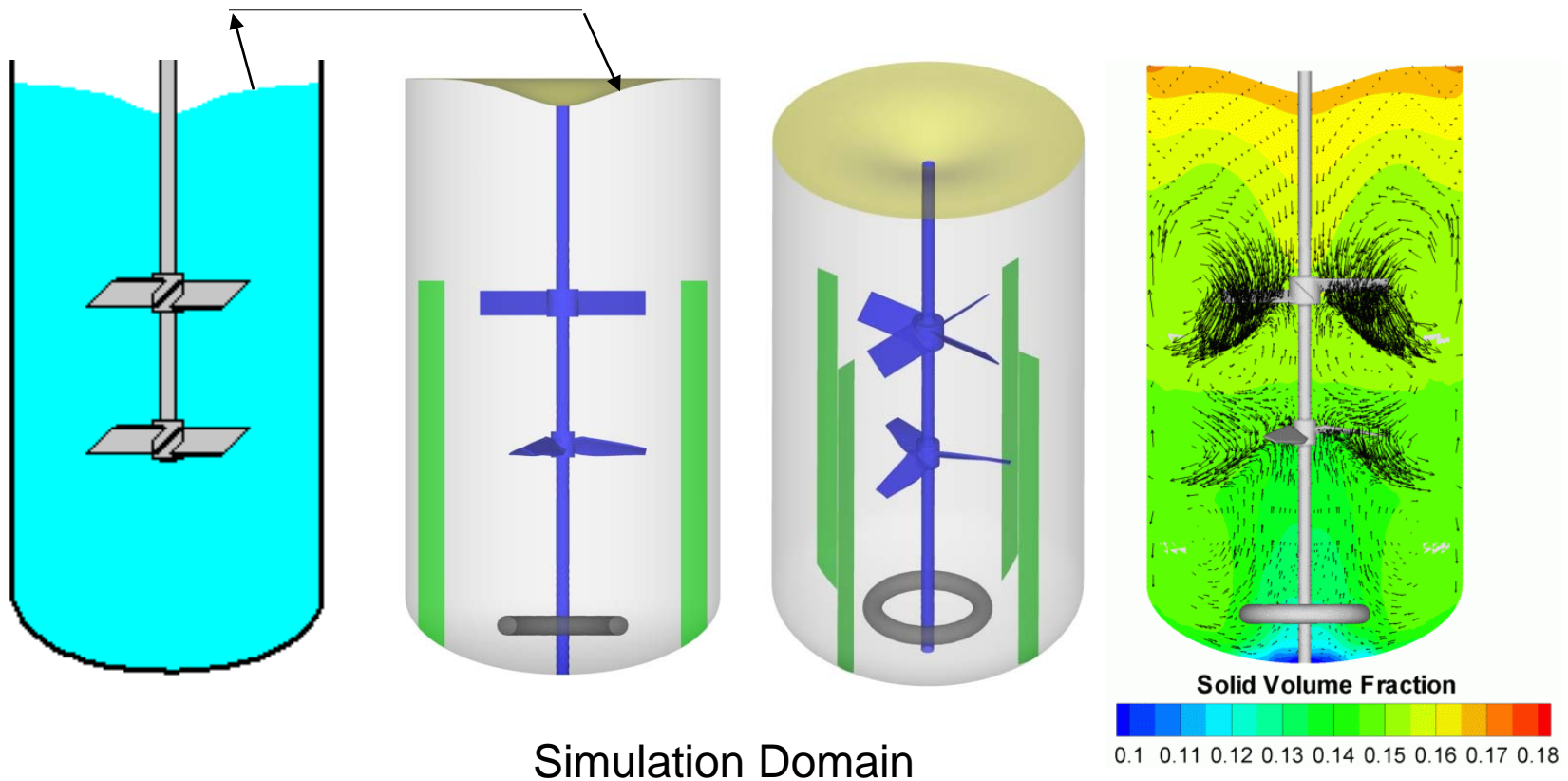
This approach significantly improves efficiency of CFD simulations with reasonable approximation of the surface vortex

# VISI MIX APPLICATION CASE #3

**VISI MIX**

**CFD**

CFD domain top boundary based on VISIMIX prediction



# VISI MIX APPLICATION CASE #4

comparing VISIMIX and lab experiments

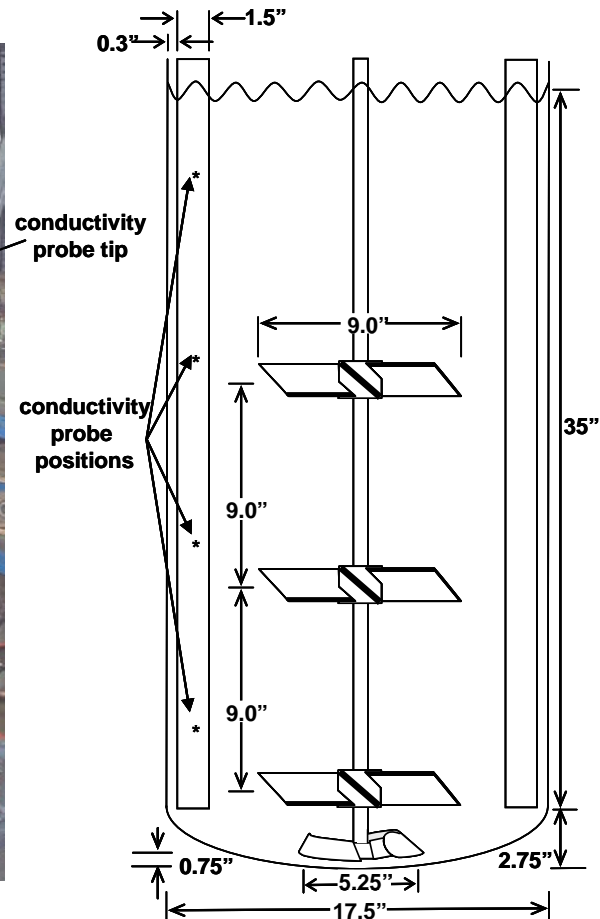
## Laboratory system to measure axial distribution of heavy solids

### chemical system

40 wt% solids in NaCl  
60 wt% salt tap water  
2 g NaCl / kg tap water

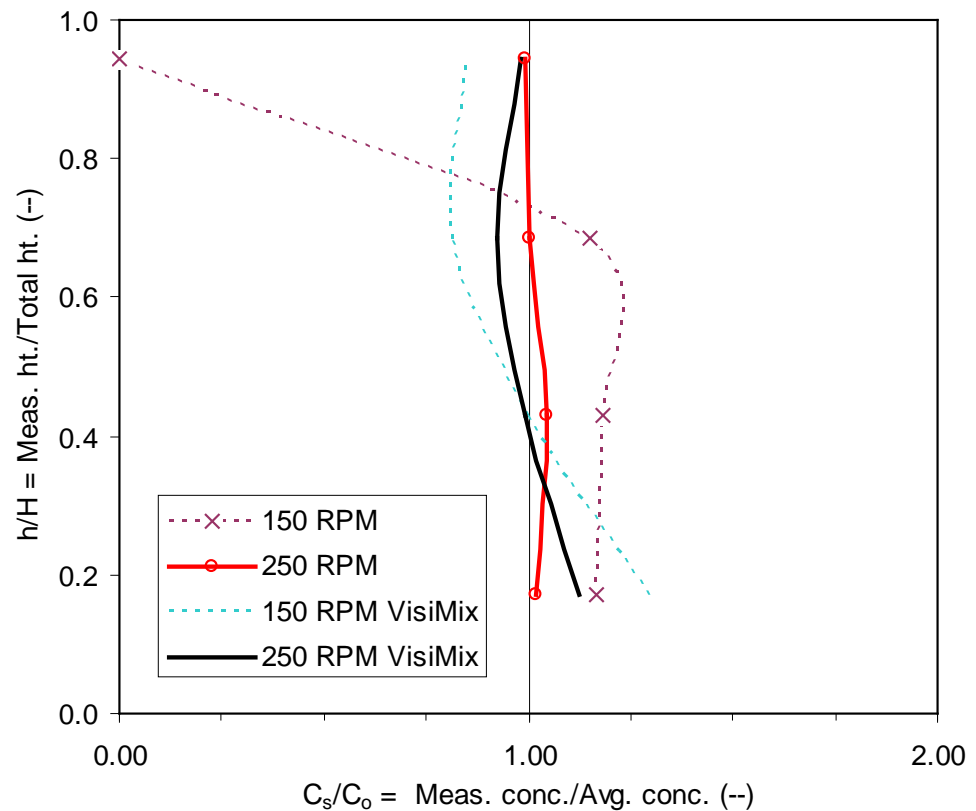
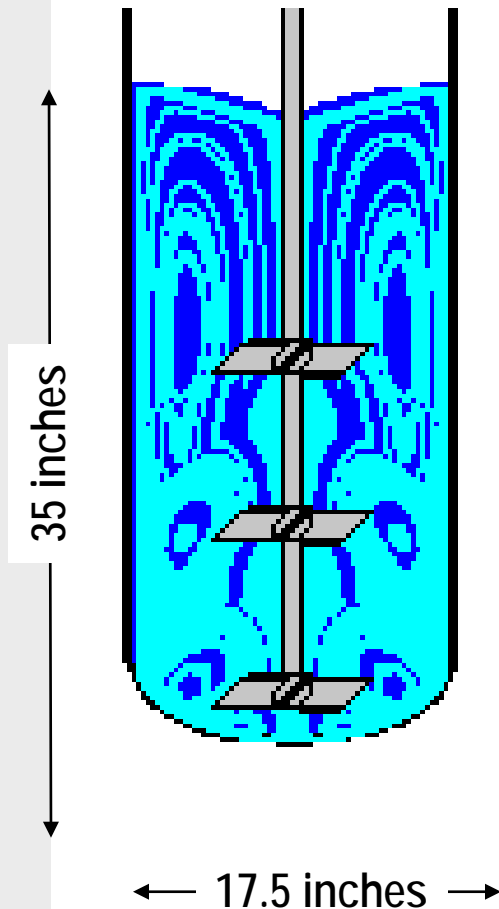
### Property of solid spheres

$\rho_{app} = 1.7 \text{ g/cc}$   
 $d_p = 285 \text{ } \mu\text{m}$  vol. med.  
(<1 wt% 15-100  $\mu\text{m}$ )  
(<1.5 wt% 425-600  $\mu\text{m}$ ).



## Normalized, axial solids distribution VisiMix vs. measured

Simulation: three standard PBTs



## VisiMix as an Engineering Productivity Tool

- + Simple, Intuitive, Context-Relevant
- + Useful for characterizing and comparing well defined mixing systems
- + No other tool with similar coverage!
- Rating tool NOT design tool
- Limited to included equipment geometries
- Limits of applicability not well defined

